New wall law treatment for the Large Eddy Simulation of turbulent heat transfer in a periodic channel ($\mathrm{Re}_\tau = 180$ and $\mathrm{Pr} = 0.71$, T0Q case)

1 Introduction

Validation made by : Pierre-Emmanuel Angeli.
Report generated 24/10/2013.

1.1 Description

• Turbulent channel flow with T0Q type conditions.
• Validated model: Robin boundary condition at walls for L.E.S. with wall function in VEF discretization.
• Validation with analytical laws (Reichardt [1]: $U^+ = R(y^+)$, and Kader [2]: $T^+ = K(y^+)$), DNS Moser-Kim-Mansour [3] and DNS Kawamura [4].

1.2 Parameters Trio_U

- Version Trio_U : 1.6.7 ;
- Version Trio_U from out: /work/trioform/PEA/Baltik_Pironneau/basic_opt (1.6.7)
- Type of problem: thermal hydraulics ;
- Discretizations: `VDF` and `VEFPreP1B` ;
- Equations: `Navier_Stokes_turbulent` and `convection_diffusion_temperature_turbulent` ;
- Turbulence model: Large Eddy Simulation ;
- Modeling of sub-filter scales: `sous_maille_WALE` (Wall-Adapting Local Eddy-viscosity [5]) ;
- Wall functions: `loi_standard_hydr` (velocity) and `loi_standard_hydr_scalaire` (temperature) ;
- Type of boundary conditions: periodicity in x and z directions, wall for top/low boundaries ;
- Time schemes: `Runge_Kutta_ordre_3` with `facsec` = 1 ;
- Convection schemes: `centre` (velocity) and `QUICK` (temperature) for VDF simulations ; `EF_stab` for VEF simulations.

1.3 Test cases

- T0Q_VDF/Cas.data :
- T0Q_VEF/Cas.data : */*jdd en annexe*/*
- T0Q_VEF_Pironneau/Cas.data : */*jdd en annexe*/*
- T0Q_VEF_Pironneau_maillage_decale/Cas.data :

1.4 References :

- [1] J. O. Hinze, *Turbulence*, McGraw-Hill, New York, 1959.
- [2] B. A. Kader, *Temperature and concentration profiles in fully turbulent boundary layers*, International Journal of Heat and Mass Transfer, 24(9):1541-1544, 1981.
- [3] R. D. Moser, J. Kim and N. N. Mansour, `http://turbulence.ices.utexas.edu/data/MKM/chan180`.
- [4] H. Kawamura, `http://murasun.me.noda.tus.ac.jp/turbulence`.
- [5] F. Nicoud and F. Ducros, *Subgrid-scale stress modelling based on the square of the velocity gradient tensor*, Flow, Turbulence and Combustion, 62:183-200,1999.
- [6] B. Mohammadi, O. Pironneau, P. G. Ciarlet and J.-L. Lions, *Analysis of the K-Epsilon turbulence model*, John Wiley & Sons - Masson, 1994.
- [7] R. B. Dean, *Reynolds Number Dependence of Skin Friction and Other Bulk Flow Variables in Two-Dimensional Rectangular Duct Flow*, Journal of Fluids Engineering, 100:215-223, 1978.
- [8] P.-E. Angeli, *Simulation numérique de la turbulence dans Trio_U : nouvelle méthode de prise en compte des lois de paroi via une condition aux limites de symétrie et un terme source de type Robin*, CEA Technical note, DEN_DANS_DM2S_STMF_LMSF_NT_13-011A, 2013.

2 Theoretical features

See the technical note [8] for detailed explanations.

• *Standard wall treatment approach in Trio_U*:

The wall laws for velocity and temperature used in the code can be written as $u_\tau = f(u_\tau)$ and $T_\tau = f(T_\tau)$. At each time step, a fixed point resolution of these equations gives respectively the values of u_τ and T_τ. Hence the velocity gradient and the temperature gradient at the wall are deduced. These gradients are used respectively in the momentum and energy balances for wall elements, were they replace the calculated gradients which are wrong due to the low resolution of the grid.

• *New approach validated here*:

The methodology is briefly described in [6] and is here referred to as the *Pironneau* approach. The idea is that the fixed walls are replaced by symetries, so that the velocity and temperature gradients appearing in the momentum and energy balances are zero. Formally, the gradients calculated from the wall laws are added then to these balances, instead of replacing wrong values like in the standard approach. Let y_1 be the distance from the wall of the first calculation point. The wall law results actually in a Robin boundary condition under the form $\left.\frac{\partial u}{\partial y}\right|_w = f[u(y_1)]$, which is implemented by a source term in the code. The same methodology is applied for temperature. More generally, the Robin condition can be evaluated at a distance δ from the wall: $\frac{\partial u}{\partial n}(\delta) = f[u(\delta)]$. Thus the user has to choose the value of δ, such that δ is located in the logarithmic layer. Here we choose $\delta = y_1$.

3 Tests description

The present calculations are L.E.S. of turbulence and heat transport in a 3D biperiodic channel flow with $Re_\tau = 180$ and Pr = 0.71. Temperature is treated like a passive scalar. Uniformly zero temperature at both walls and uniform volumetric heat source Q = 1 W $\cdot$ m^{-3} on the whole channel are applied. The dimensions of the channel are: L$_x$ = 6.4 m , L$_y$ = 2h = 2 m, L$_z$ = 3.2 m.

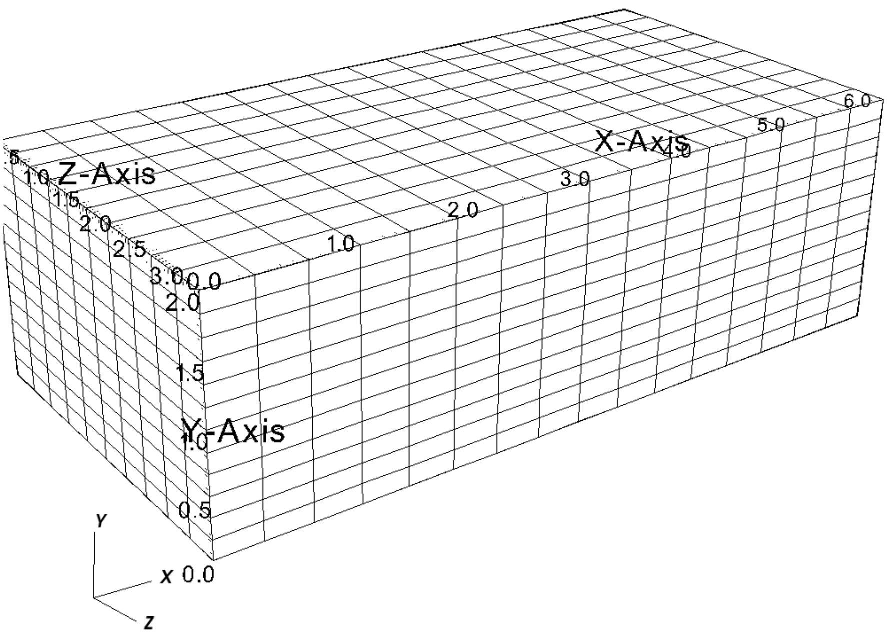
Two simulations using the standard methodology are first carried out (one using a VDF discretization and the other using a VEF discretization). Then two others simulations (in VEF) using the new approach are done. In the second one, the upper and lower walls of the channel are displaced from the distance δ toward the centerline of the channel, and a new mesh similar to the previous one is built.

3.1 VDF mesh

Number of nodes in each direction: N$_x$ = 17, N$_y$ = 13, N$_z$ = 11.

Total number of elements: (N$_x$-1)(N$_y$-1)(N$_z$-1) = 1920.

$$dx^+ = \frac{L_x}{N_x-1}\frac{\mathrm{Re}_\tau}{h} = 72 \ ; \ y^+ = \frac{L_y}{2(N_y-1)}\frac{\mathrm{Re}_\tau}{h} = 15 \ ; \ dz^+ = \frac{L_z}{N_z-1}\frac{\mathrm{Re}_\tau}{h} = 58.$$

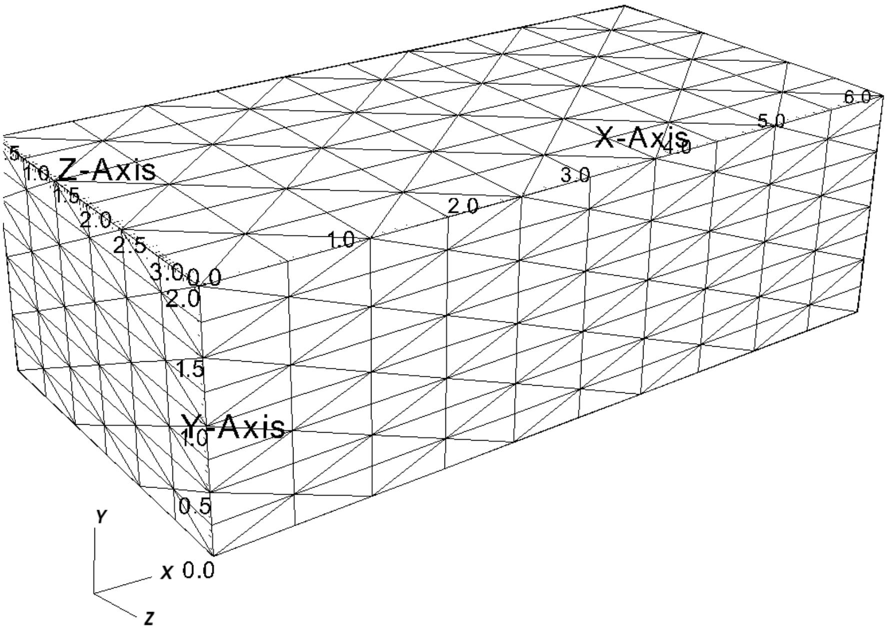


3.2 VEF mesh (entire channel)

Number of nodes in each direction: N$_x$ = 6, N$_y$ = 5, N$_z$ = 4.

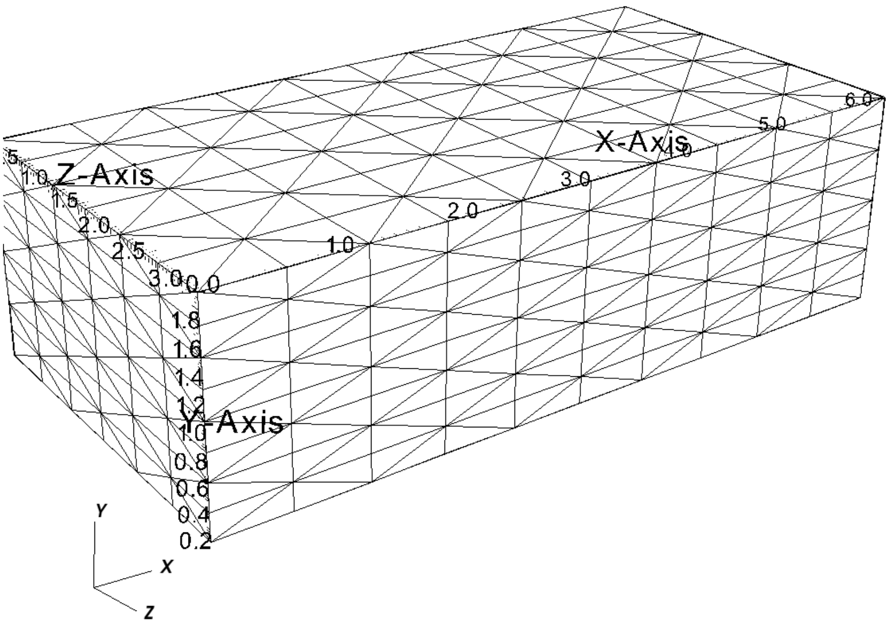
Total number of elements with `tetraedriser_homogene_fin`: 48(N$_x$-1)(N$_y$-1)(N$_z$-1) = 2880.

$$dx^+ = \frac{L_x}{3(N_x-1)}\frac{\mathrm{Re}_\tau}{h} = 77 \ ; \ y^+ = \frac{L_y}{6(N_y-1)}\frac{\mathrm{Re}_\tau}{h} = 15 \ ; \ dz^+ = \frac{L_z}{3(N_z-1)}\frac{\mathrm{Re}_\tau}{h} = 64.$$



3.3 VEF mesh (truncated channel)

Number of nodes in each direction: $N_x = 6$, $N_y = 5$, $N_z = 4$.
Total number of elements with `tetraedriser_homogene_fin`: $48(N_x\text{-}1)(N_y\text{-}1)(N_z\text{-}1) = 2880$.



3.4 Physical properties and dimensionless numbers

Physical properties:

- $\rho = 0.011928$ kg $\cdot$ m^{-3}
- $\mu = 2.84\text{e-}5$ kg $\cdot$ m^{-1} $\cdot$ s^{-1}
- $\lambda = 0.20772$ W $\cdot$ m^{-1} $\cdot$ K^{-1}
- $C_p = 5193$ J $\cdot$ kg^{-1} $\cdot$ K^{-1}

Dimensionless numbers:

- $\mathrm{Re}_b = \dfrac{\rho U_b h}{\mu} = 2770$, where $U_b = \dfrac{2}{3} U_c$ and $U_c = 9.8945$ m $\cdot$ s^{-1} (*cf.* initial condition)
- $\mathrm{Pr} = \dfrac{\mu C_p}{\lambda} = 0.71$
- $\mathrm{Pe} = \mathrm{Re}_b \times \mathrm{Pr} = 1967$
- $\mathrm{Re}_\tau = 0.175 \mathrm{Re}_b^{7/8} = 180$ (Dean's correlation [7])

3.5 Initial and boundary conditions

Initial conditions:

- Velocity: parabolic mean profile for x-component
  `Champ_init_canal_sinal 3 { Ucent 24.293 h 1 ampli_sin 0 omega 1 ampli_bruit 0.5 }`
- Temperature: $T = 0$

Hydraulic boundary conditions:

- Inlet/outlet (x-direction): periodicity
- Front/back boundaries (z-direction): periodicity
- Top/low boundaries:
  - `paroi_fixe` for the Trio_U "standard" approach
  - `paroi_decalee_Robin { _delta_value_ }` for the "Pironneau" approach$^{(*)}$

Fluid thermal boundary conditions:

- Inlet/outlet (x-direction): periodicity
- Front/back boundaries (z-direction): periodicity
- Top/low boundaries:
  - uniform temperature $T_0 = 0$ for the Trio_U "standard" approach
  - `paroi_decalee_Robin { _delta_value_ }` for the "Pironneau" approach$^{(*)}$

Source terms in the "Pironneau" approach:

- Navier-Stokes:
  `source_Robin 2 Haut Bas`
- Convection diffusion:
  `source_Robin_scalaire 2 Haut 0 Bas 0`

$^{(*)}$ where `_delta_value_` is set according the recommandation of section 2 ($\delta = y_1$).

3.6 Numerical schemes

VDF discretization:

- Time scheme: third order Runge-Kutta method with `facsec`=1
- Convection: centered scheme for velocity and `QUICK` scheme for temperature

VEF discretization:

- Time scheme: third order Runge-Kutta method with `facsec`=1
- Convection schemes: `EF_stab` ($\alpha = 0.2$ for velocity and $\alpha = 1$ for temperature)

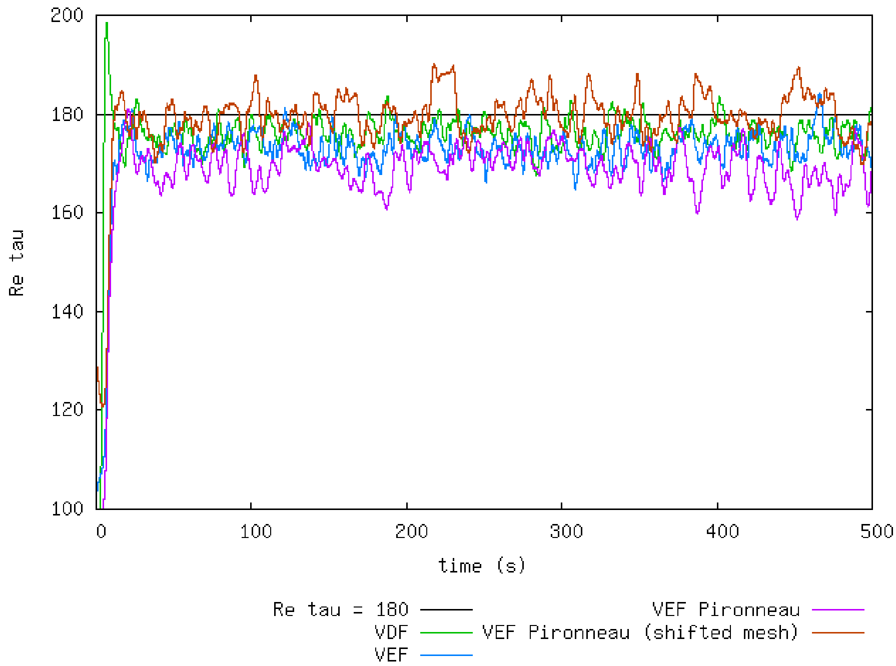
4 Friction velocity and friction Reynolds number calculated

4.1 Friction velocity u_τ

	time (s)	u_τ ($\mathrm{m \cdot s^{-1}}$)	Relative error (%)
Theoretical $^{(*)}$	-	0.42857	-
VDF	1000	0.41941	2.14
VEF	1000	0.41512	3.14
VEF Pironneau	1000	0.40793	4.82
VEF Pironneau (shifted mesh)	1000	0.43051	0.45

$^{(*)}$ according to Dean's correlation [7]: $\mathrm{Re}_\tau = 0.175\mathrm{Re}_b^{7/8}$, and using $\mathrm{Re}_\tau = \dfrac{\rho u_\tau h}{\mu}$.

4.2 Friction Reynolds Re_τ



5 Detailed results

In the next two sections, different time- and space-averaged profiles are plotted across the channel half-height: the components of velocity (u and w), the temperature (T), the components of the subscale stress tensors (T_{ij} and Q_i), the root mean square of temperature (T_{rms}), as well as the adimensional equivalent quantities.

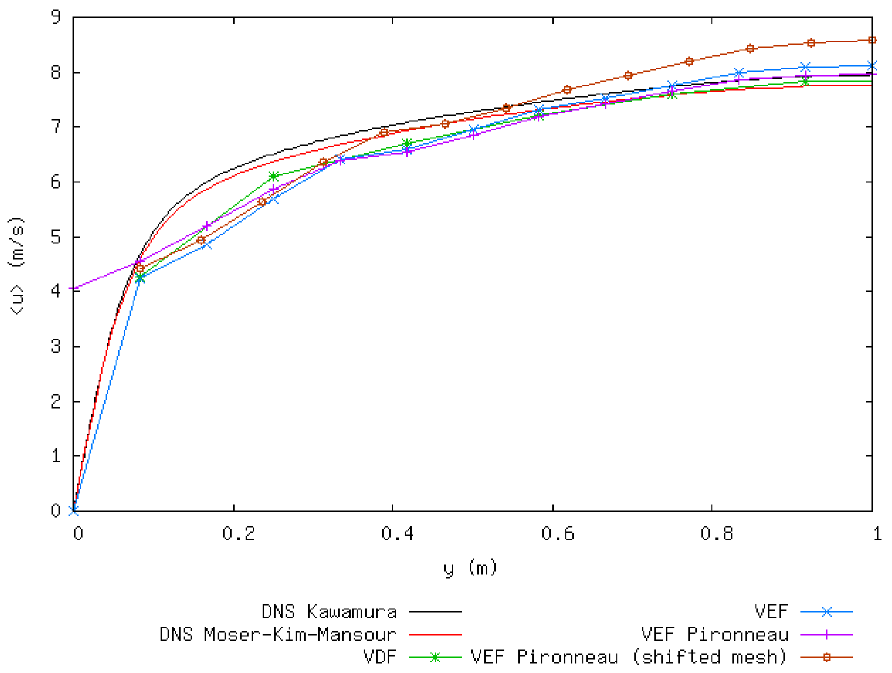
We compare the non-dimensional mean velocity profiles with the Reichardt's law [1]:

$U^+ = \frac{1}{\kappa}\ln(1+\kappa y^+) + A\left(1 - e^{-y^+/11} - \frac{y^+}{11}e^{-y^+/3}\right)$, were $\kappa = 0.415$ and A $= 7.44$.

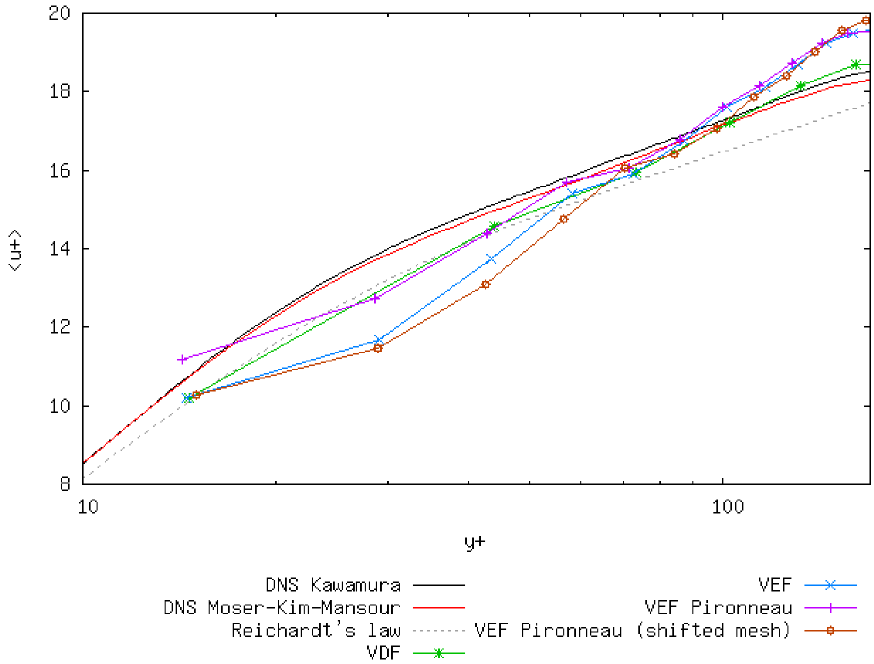
We compare the non-dimensional mean temperature profiles with the Kader's law [2]:

$T^+ = \text{Pr}y^+e^{-\Gamma} + \left[2.12\ \ln(1+y^+) + \beta\right]e^{-1/\Gamma}$, were $\beta = \left(3.85\ \text{Pr}^{1/3} - 1.3\right)^2 + 2.12\ \ln(\text{Pr})$ and $\Gamma = \frac{0.01(y^+\text{Pr})^4}{1+5y^+\text{Pr}^3}$.

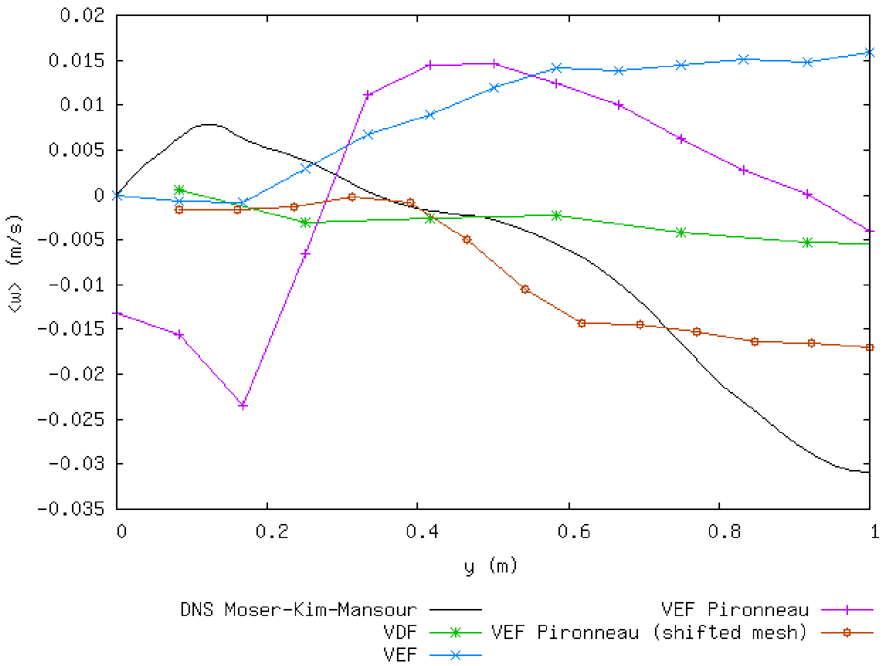
5.1 Mean x-velocity profile $< u >$



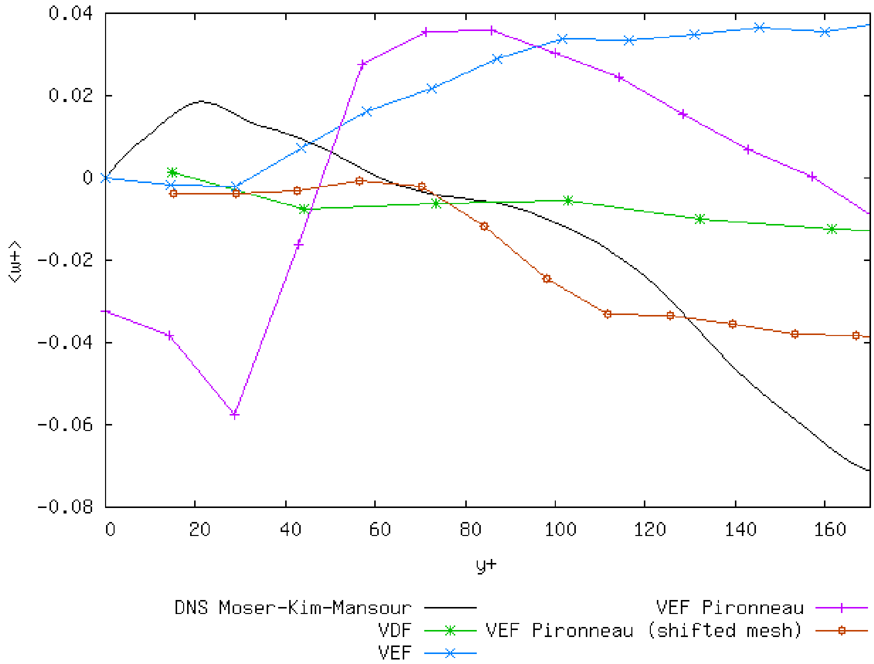
5.2 Non-dimensional mean x-velocity profile $< u^+ >$



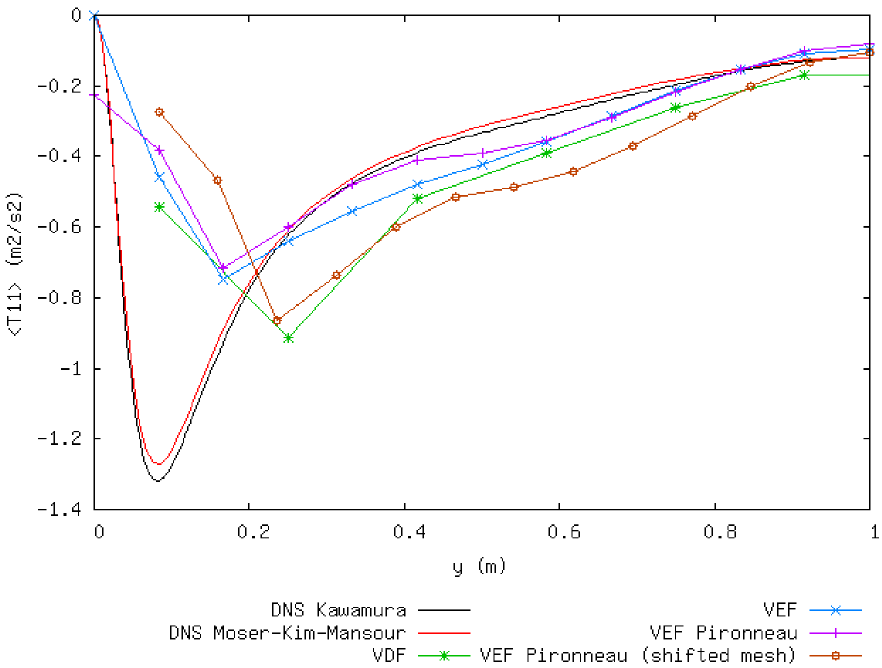
5.3 Mean z-velocity profile $< w >$



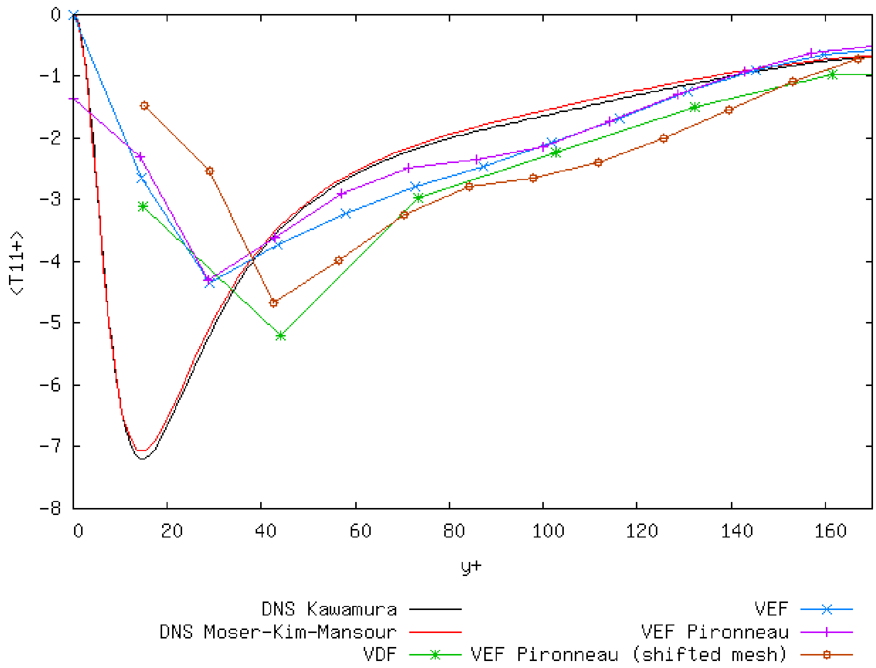
5.4 Non-dimensional mean z-velocity profile $< w^+ >$



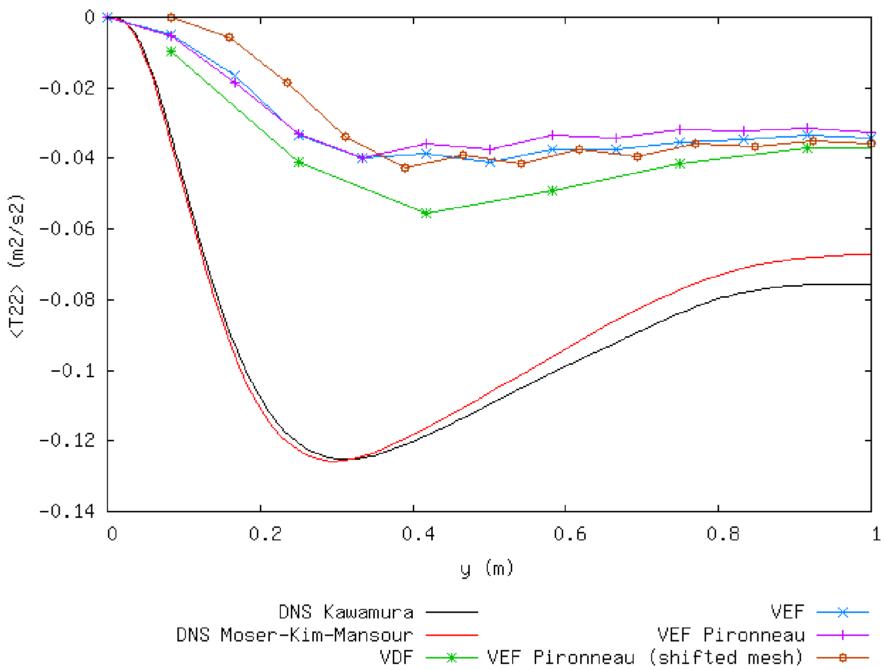
5.5 Mean xx-component of subgrid scale tensor $< T_{11} >$



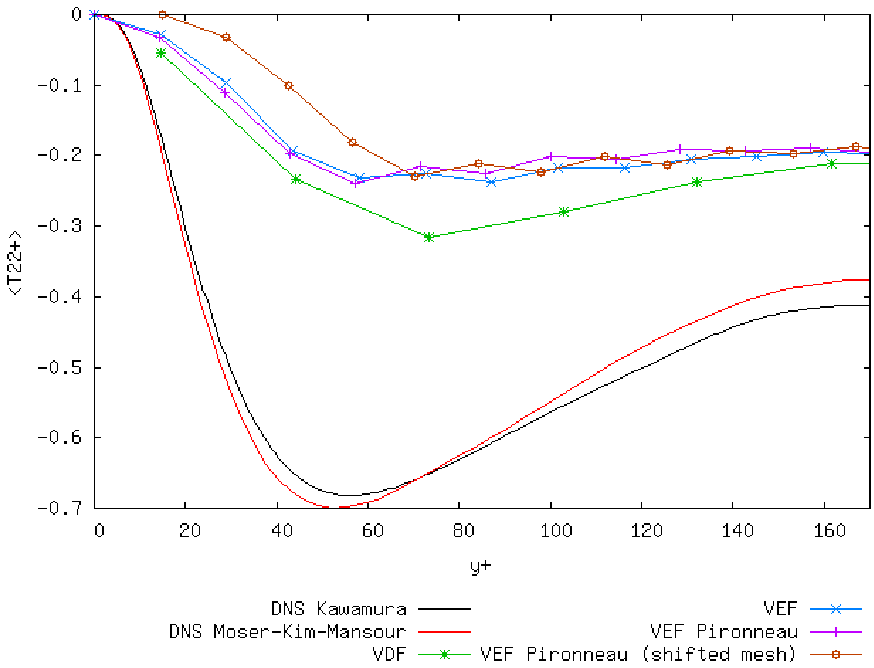
5.6 Non-dimensional mean xx-component of subgrid scale tensor $< T_{11}^{+} >$



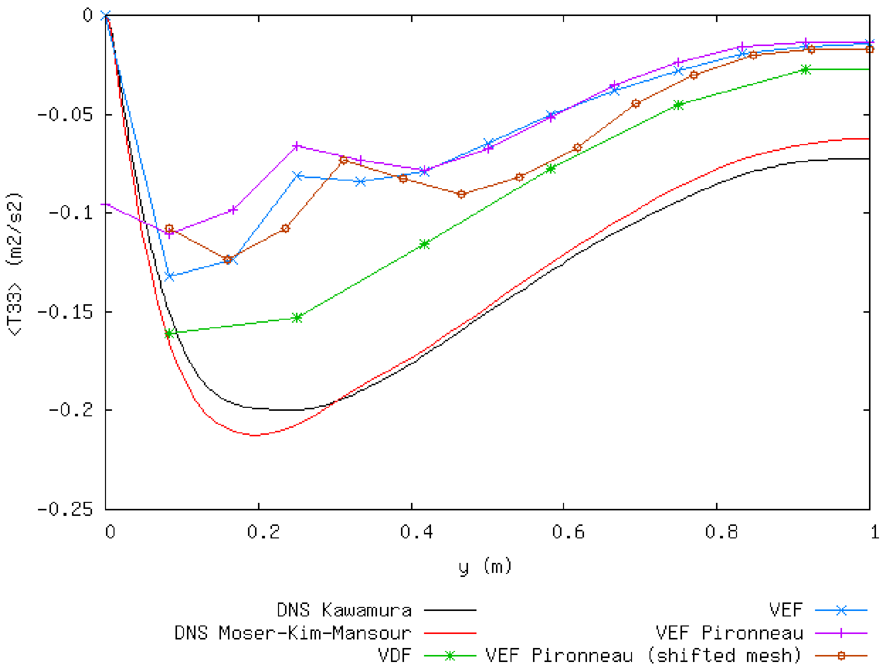
5.7 Mean yy-component of subgrid scale tensor $< T_{22} >$



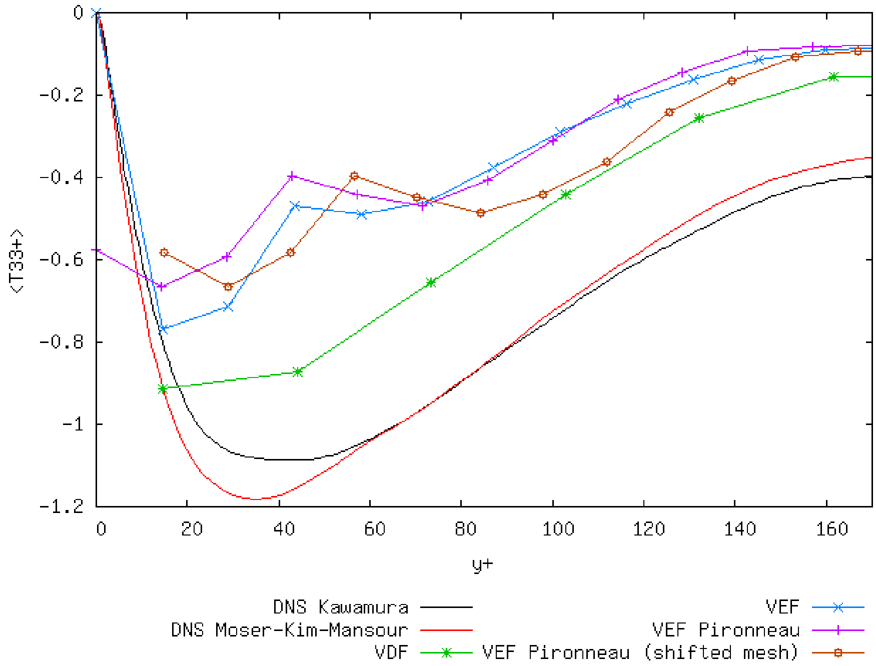
5.8 Non-dimensional mean yy-component of subgrid scale tensor $< T_{22}^{+} >$



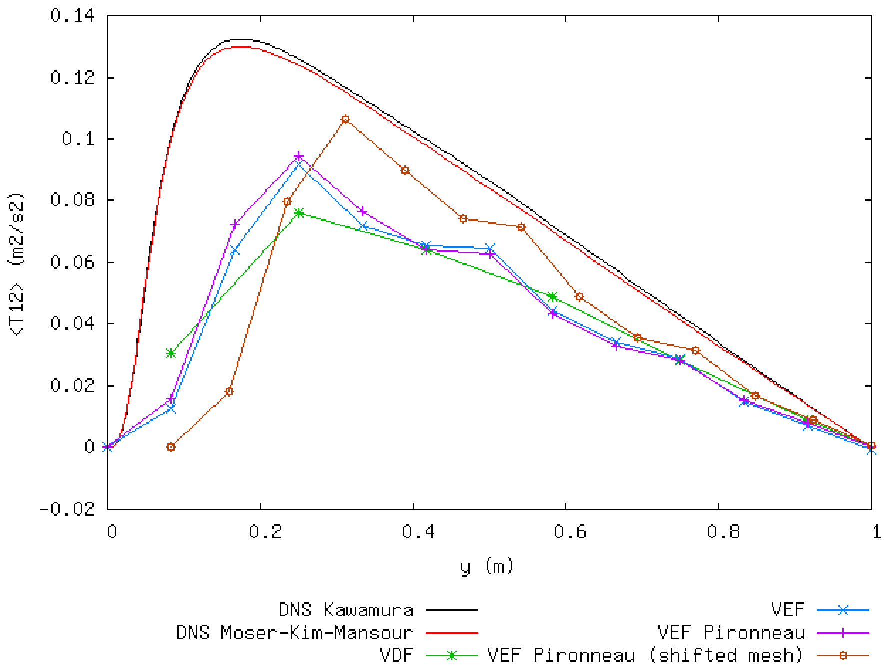
5.9 Mean zz-component of subgrid scale tensor $< T_{33} >$



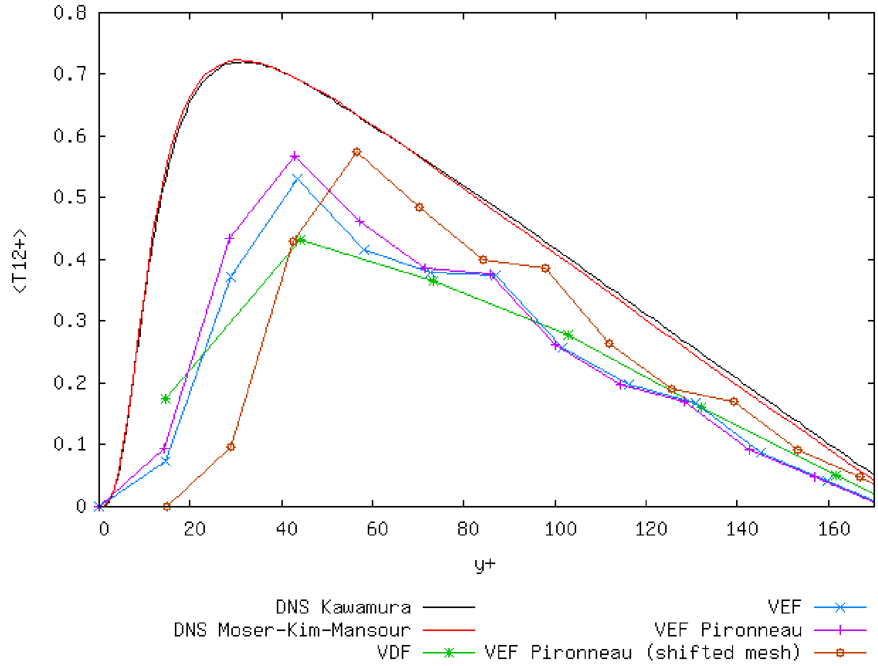
5.10 Non-dimensional mean zz-component of subgrid scale tensor $< T_{33}^{+} >$



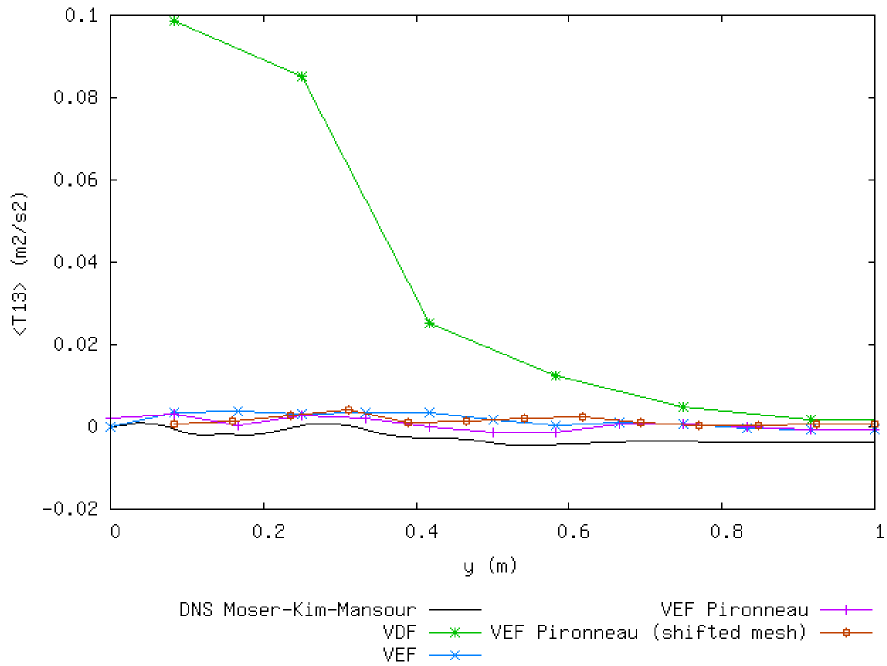
5.11 Mean xy-component of subgrid scale tensor $< T_{12} >$



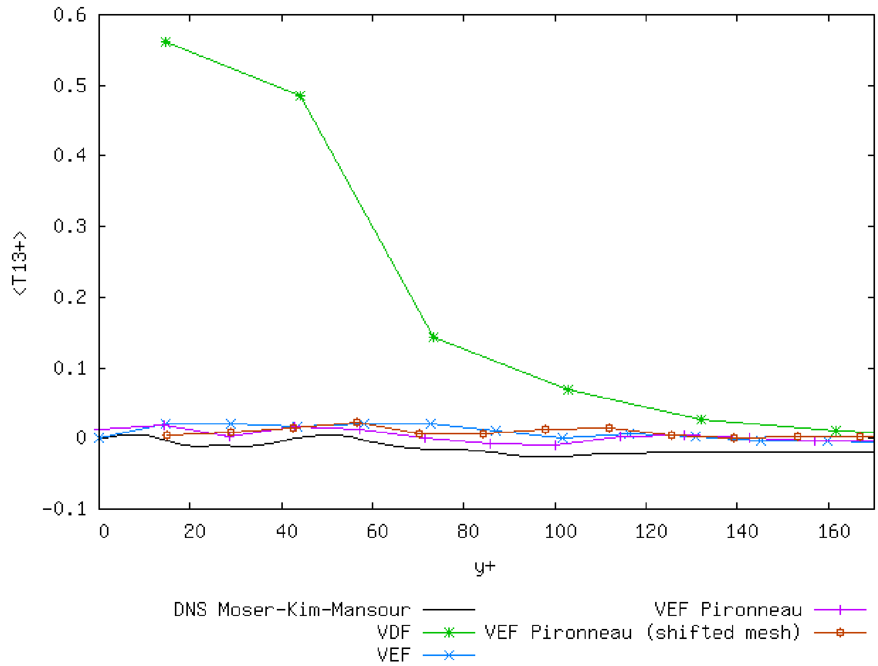
5.12 Non-dimensional mean xy-component of subgrid scale tensor $< T_{12}^{+} >$



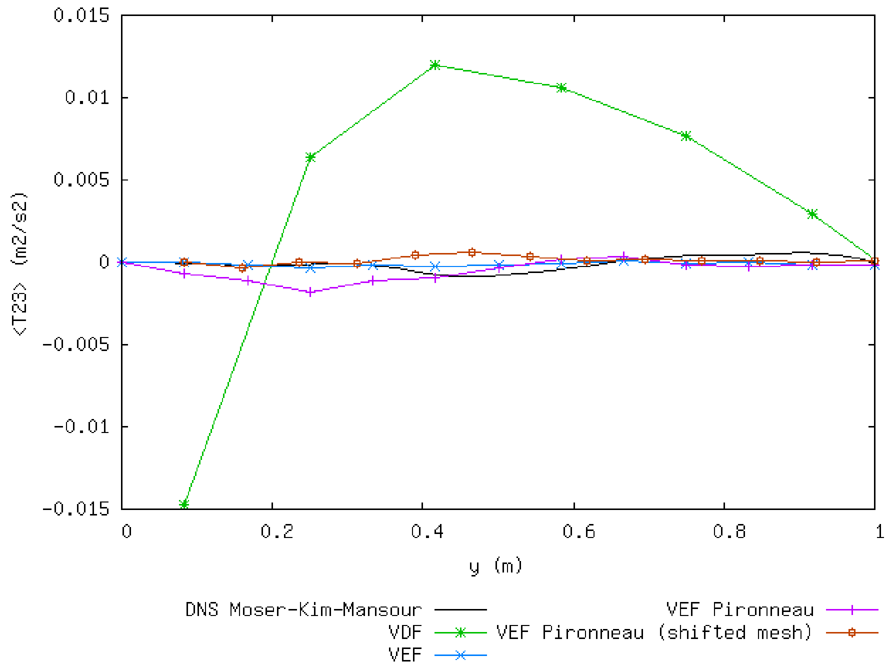
5.13 Mean xz-component of subgrid scale tensor $< T_{13} >$



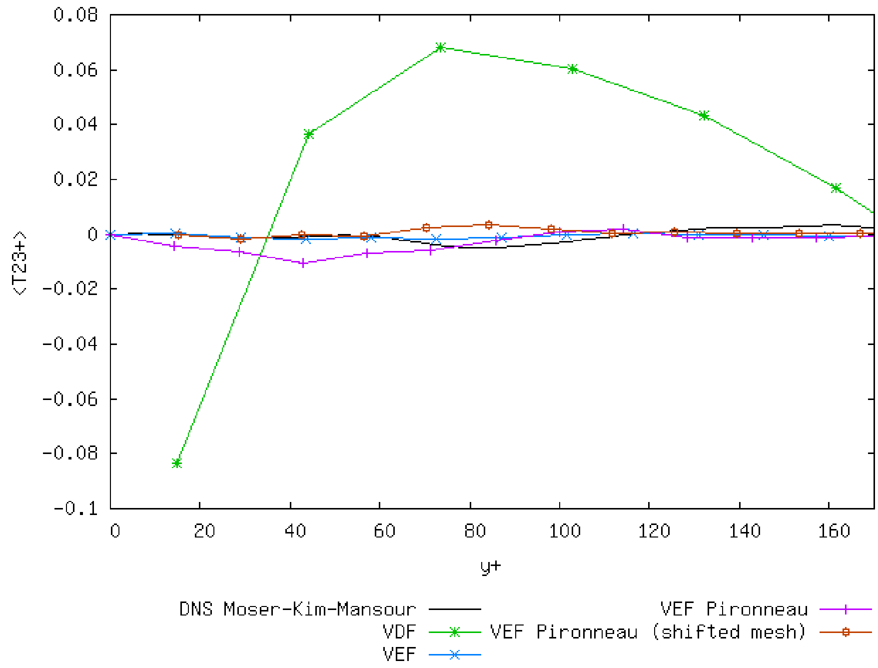
5.14 Non-dimensional mean xz-component of subgrid scale tensor $< T_{13}^{+} >$



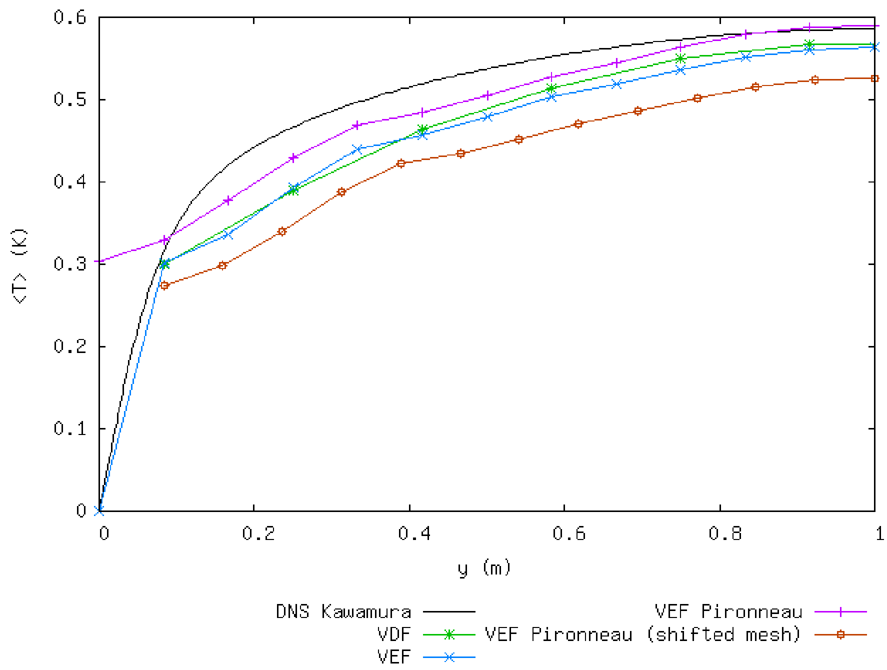
5.15 Mean yz-component of subgrid scale tensor $< T_{23} >$



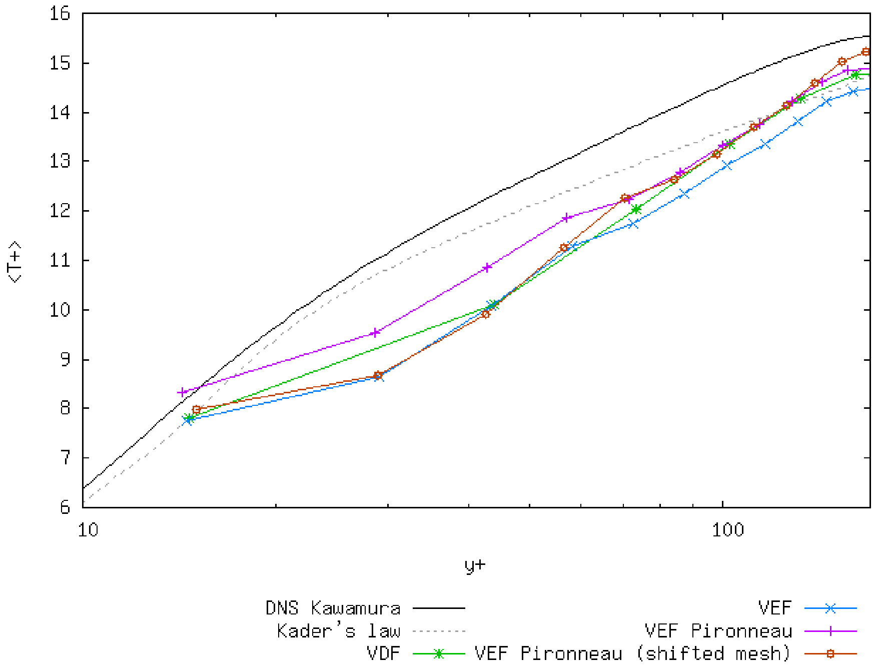
5.16 Non-dimensional mean yz-component of subgrid scale tensor $< T_{23}^{+} >$



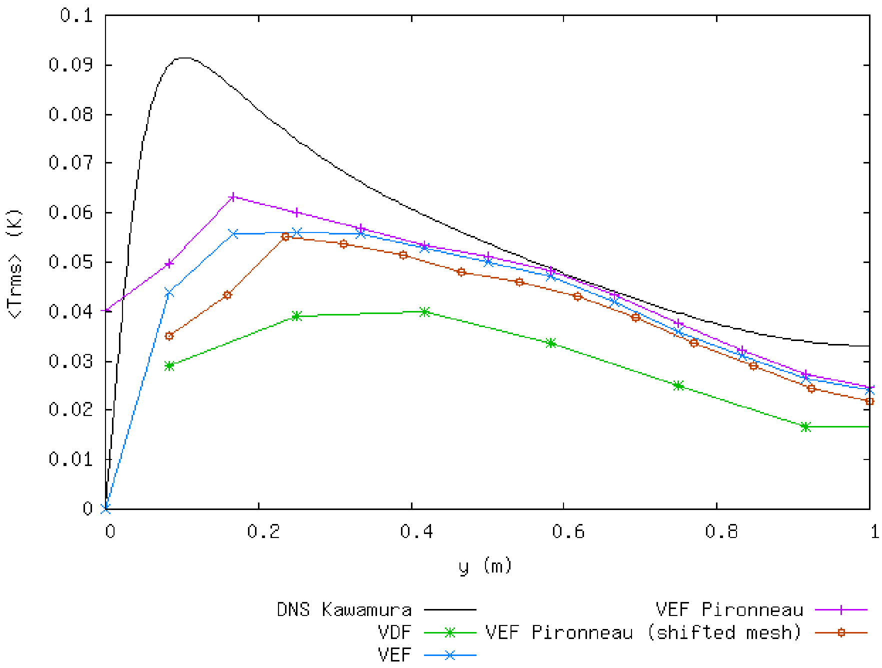
5.17 Mean temperature profile $< T >$



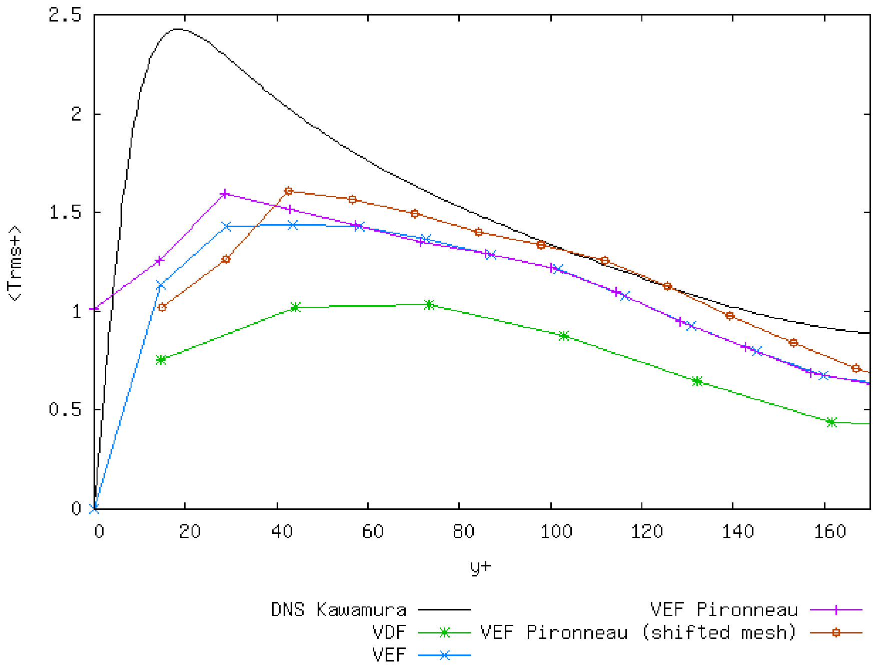
5.18 Non-dimensional mean temperature profile $< T^+ >$



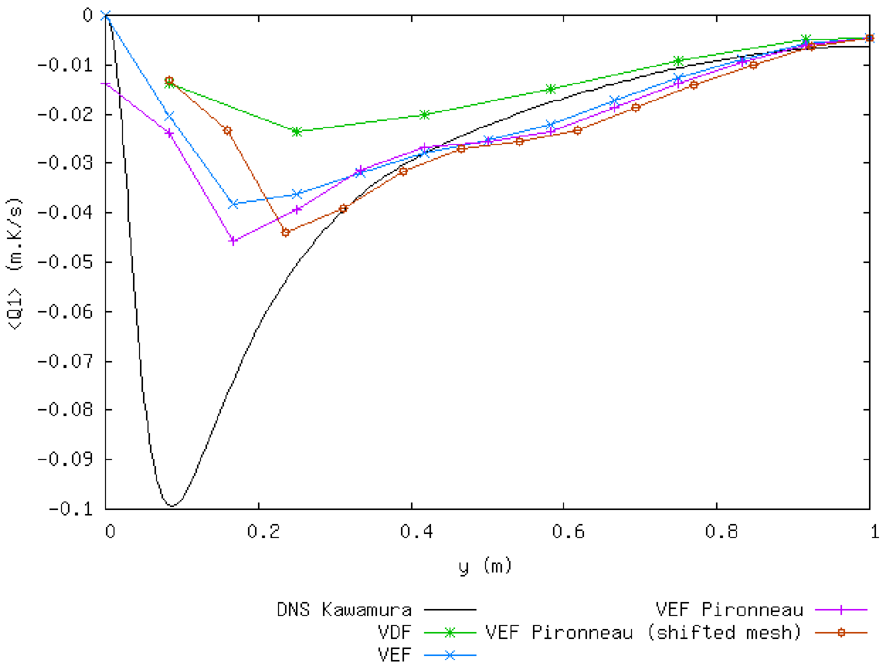
5.19 Quadratic mean of temperature $< T_{rms} >$



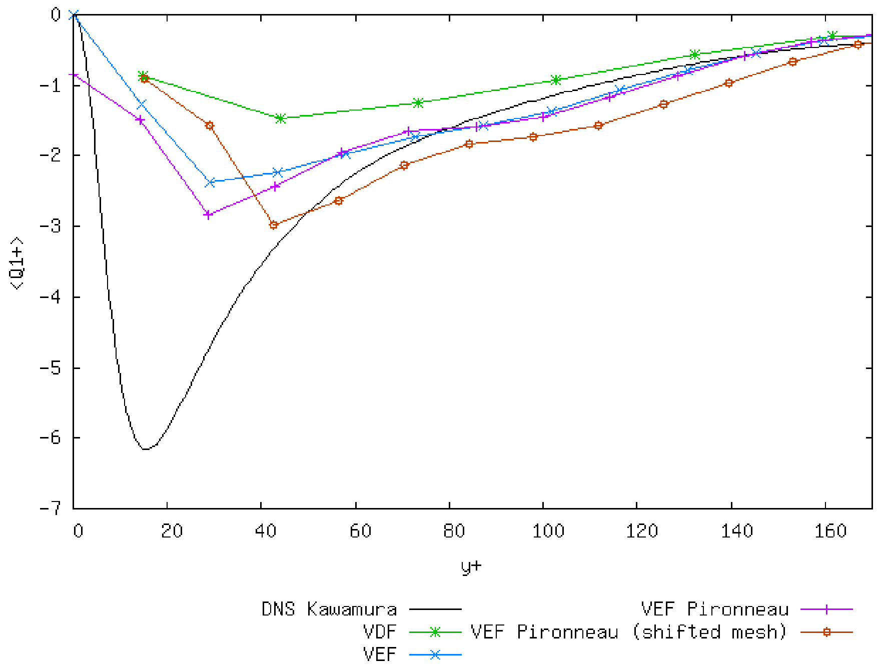
5.20 Non-dimensional quadratic mean of temperature $< T^+_{rms} >$



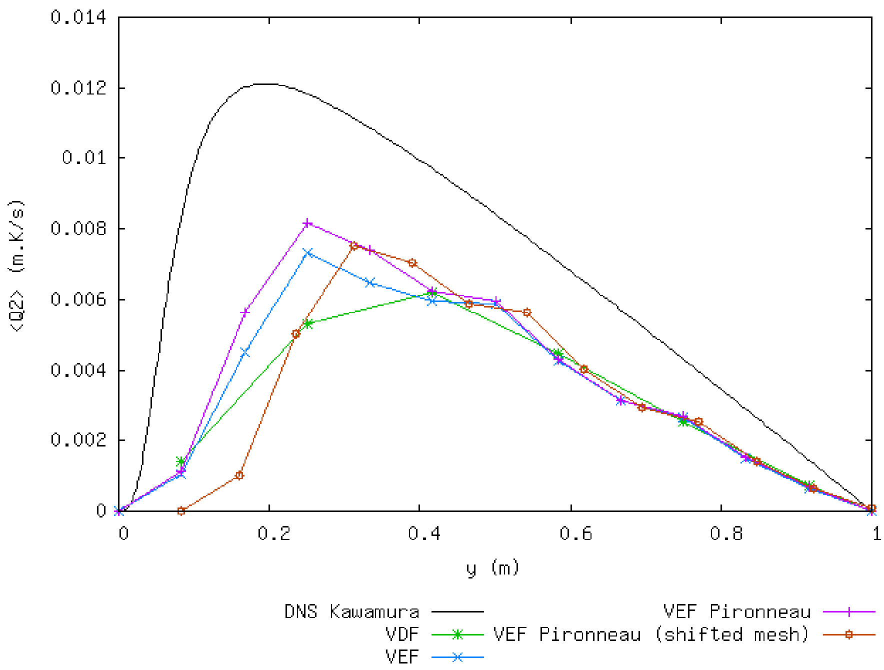
5.21 Streamwise turbulent heat flux $< Q_1 >$



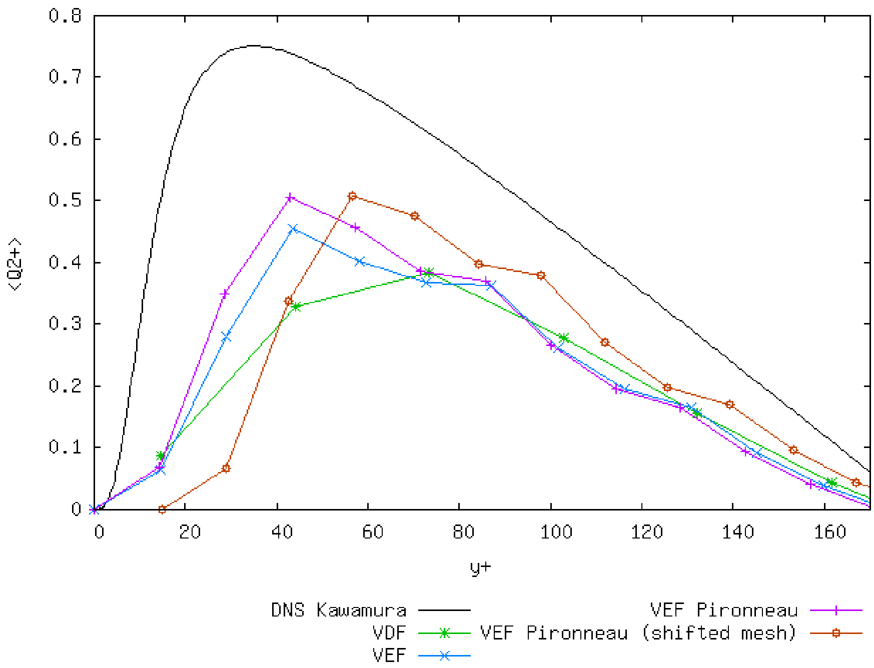
5.22 Non-dimensional streamwise turbulent heat flux $< Q_1^+ >$



5.23 Wall-normal turbulent heat flux $< Q_2 >$



5.24 Non-dimensional wall-normal turbulent heat flux $< Q_2^+ >$



6 Analysis of the results

- On the whole, all the simulations provide an analogous and good quality of results. None of them is found to be much better than the others.

- Friction velocity: the best friction velocity in the comparison with the theoretical value is obtained with the VEF simulation and the truncated channel, which yields a very accurate result (0.2% relative error). The other Pironneau simulation gives an almost as good relative error as the standard approach (3.36% vs. 5.31%)

- Velocity: for the non-dimensional mean x-velocity profile $< u >$, the first calculation points for all simulations are located on the Reichardt's law as expected, except for the VEF Pironneau. In this case, the real first point is not represented on the logarithmic graph because it corresponds to $y = 0$. Thus the first represented point of the VEF Pironneau profile (in fact the second calculated point) has no reason to satisfy the Reichardt's law.

- Temperature: the analysis is the same as for velocity.

- Subscale stress tensor components $< T_{ij} >$: the tendancies are in correct agreement with the DNS results of Kawamura and Moser-Kim-Mansour, except the VDF simulation which gives bad results on particular components.

- Subscale stress tensor components $< Q_i >$: all the simulations are in relatively good agreement with the DNS results of Kawamura.

7 Computer performance

	host	system	Total CPU Time	CPU time/step	number of cell
T0Q_VDF/Cas	vonnes	Linux	422.232	0.0132891	1920
T0Q_VEF/Cas	vonnes	Linux	8994.93	0.063183	2880
T0Q_VEF_Pironneau/Cas	vonnes	Linux	8955.56	0.0651347	2880
T0Q_VEF_Pironneau_maillage_decale/Cas	vonnes	Linux	11333.8	0.0731124	2880
Total			29706.5		

8 Data Files

8.1 Cas

```
Dimension 3
Pb_Thermohydraulique_Turbulent pb
Domaine dom
Mailler dom
{
  Pave Cavite
  {
    Origine 0 0 0
    Nombre_de_Noeuds 6 5 4
    Longueurs 6.4 2 3.2
    Facteurs 1 1 1
  }
  {
    Bord PerioX X = 0    0 <= Y <= 2 0 <= Z <= 3.2
    Bord PerioX X = 6.4    0 <= Y <= 2 0 <= Z <= 3.2
    Bord PerioZ Z = 0    0 <= X <= 6.4      0 <= Y <= 2
    Bord PerioZ Z = 3.2    0 <= X <= 6.4      0 <= Y <= 2
    Bord Bas   Y = 0 0 <= X <= 6.4      0 <= Z <= 3.2
    Bord Haut Y = 2 0 <= X <= 6.4      0 <= Z <= 3.2
  }
}
Tetraedriser_homogene_fin dom
Reordonner_faces_periodiques dom PerioX
Reordonner_faces_periodiques dom PerioZ
VEFPreP1b dis
Runge_Kutta_ordre_3 sch_RK3
Lire sch_RK3
{
  tinit 0
  tmax 1000
  dt_start dt_calc
  dt_min 1e-7
  dt_max 1
  dt_impr 5
  dt_sauv 500
  seuil_statio 1e-15
  facsec 1
  no_check_disk_space
  periode_sauvegarde_securite_en_heures 11
}
Fluide_incompressible air
Lire air
{
  mu  champ_uniforme 1 2.84e-5
  rho champ_uniforme 1 0.011928
  lambda  champ_uniforme 1 0.20772
  Cp  champ_uniforme 1 5193
  beta_th champ_uniforme 1 1.9954e-3
}
Champ_uniforme gravite
```

```
Lire gravite 3 0 0 0
Associer air gravite
Associer pb dom
Associer pb sch_RK3
Associer pb air
Discretiser pb dis
Lire pb
{
  Navier_Stokes_turbulent
  {
    Solveur_pression  petsc Cholesky { }
    Convection   { EF_stab { volumes_etendus alpha 0.2 } }
    Diffusion   { }
    Conditions_initiales  { vitesse champ_init_canal_sinal 3 { Ucent 9.8945 h 1 ampli_sin 0 ome
    Conditions_limites  {
          PerioX  periodique
          PerioZ  periodique
          Haut  paroi_fixe
          Bas paroi_fixe
          }
    Modele_turbulence sous_maille_WALE
          {
          turbulence_paroi loi_standard_hydr
          dt_impr_ustar 20
          }
    Traitement_particulier  {
          canal {
            dt_impr_moy_spat 200
            dt_impr_moy_temp 200
            debut_stat 600
            }
          }
    Sources     { canal_perio { direction_ecoulement 0 } }
  }
  Convection_diffusion_temperature_turbulent
  {
    Convection   { EF_stab { volumes_etendus alpha 1 } }
    Diffusion   { }
    Conditions_initiales  { temperature champ_fonc_xyz dom 1 0 }
    Conditions_limites  {
          PerioX  periodique
          PerioZ  periodique
          Haut  paroi_temperature_imposee champ_front_uniforme 1 0
          Bas paroi_temperature_imposee champ_front_uniforme 1 0
          }
    Modele_turbulence Prandtl
          {
          turbulence_paroi loi_standard_hydr_scalaire
          dt_impr_nusselt 20
          }
    Sources     { puissance_thermique champ_uniforme 1 1 }
  }
  Postraitement
  {
```

```
  Definition_champs    {
          moyenne_vitesse    Moyenne { t_deb 600 t_fin 1000 source refChamp { Pb_champ pb vitess
          moyenne_temperature Moyenne { t_deb 600 t_fin 1000 source refChamp { Pb_champ pb tem
          ecart_type_vitesse  Ecart_type { t_deb 600 t_fin 1000 source refChamp { Pb_champ pb v
          ecart_type_temperature  Ecart_type { t_deb 600 t_fin 1000 source refChamp { Pb_champ
          min_temperature    Reduction_0D { methode min source refChamp { Pb_champ pb temperatur
          max_temperature    Reduction_0D { methode max source refChamp { Pb_champ pb temperatur
          }
    Sondes       {
          sonde_vitesse      nodes vitesse      periode 0.5 points 1 3.2 1 1.6
          sonde_temperature    nodes temperature    periode 0.5 points 1 3.2 1 1.6
          sonde_moyenne_vitesse    nodes moyenne_vitesse    periode 0.5 points 1 3.2 1 1.6
          sonde_moyenne_temperature nodes moyenne_temperature periode 0.5 points 1 3.2 1 1.6
          sonde_ecart_type_vitesse  nodes ecart_type_vitesse  periode 0.5 points 1 3.2 1 1.6
          sonde_ecart_type_temperature  nodes ecart_type_temperature  periode 0.5 points 1 3.2
          coupe_vitesse      nodes vitesse      periode 5 segment 9 0.213333 0 0.177778 0.213333
          coupe_temperature    nodes temperature    periode 5 segment 9 0.213333 0 0.177778 0.213
          coupe_moyenne_vitesse    nodes moyenne_vitesse    periode 5 segment 9 0.213333 0 0.1777
          coupe_moyenne_temperature nodes moyenne_temperature periode 5 segment 9 0.213333 0 0.
          coupe_ecart_type_vitesse  nodes ecart_type_vitesse  periode 5 segment 9 0.213333 0 0.
          coupe_ecart_type_temperature  nodes ecart_type_temperature  periode 5 segment 9 0.213
          }
    Format lata_v2
    Champs dt_post 200  {
          vitesse som
          temperature som
          min_temperature som
          max_temperature som
          }
    Statistiques dt_post 200
          {
          t_deb 600 t_fin 1000
          moyenne vitesse
          moyenne temperature
          ecart_type vitesse
          ecart_type temperature
          }
  }
  sauvegarde formatte pb.sauv
}
Resoudre pb
Fin
```

8.2 Cas

```
Dimension 3
Pb_Thermohydraulique_Turbulent pb
Domaine dom
Mailler dom
{
  Pave Cavite
  {
    Origine 0 0 0
    Nombre_de_Noeuds 6 5 4
```

```
    Longueurs 6.4 2 3.2
    Facteurs 1 1 1
  }
  {
    Bord PerioX X = 0    0 <= Y <= 2 0 <= Z <= 3.2
    Bord PerioX X = 6.4    0 <= Y <= 2 0 <= Z <= 3.2
    Bord PerioZ Z = 0    0 <= X <= 6.4      0 <= Y <= 2
    Bord PerioZ Z = 3.2    0 <= X <= 6.4      0 <= Y <= 2
    Bord Bas   Y = 0 0 <= X <= 6.4      0 <= Z <= 3.2
    Bord Haut Y = 2 0 <= X <= 6.4      0 <= Z <= 3.2
  }
}
Tetraedriser_homogene_fin dom
Reordonner_faces_periodiques dom PerioX
Reordonner_faces_periodiques dom PerioZ
VEFPreP1b dis
Runge_Kutta_ordre_3 sch_RK3
Lire sch_RK3
{
  tinit 0
  tmax 1000
  dt_start dt_calc
  dt_min 1e-7
  dt_max 1
  dt_impr 5
  dt_sauv 500
  seuil_statio 1e-15
  facsec 1
  no_check_disk_space
  periode_sauvegarde_securite_en_heures 11
}
Fluide_incompressible air
Lire air
{
  mu  champ_uniforme 1 2.84e-5
  rho champ_uniforme 1 0.011928
  lambda  champ_uniforme 1 0.20772
  Cp  champ_uniforme 1 5193
  beta_th champ_uniforme 1 1.9954e-3
}
Champ_uniforme gravite
Lire gravite 3 0 0 0
Associer air gravite
Associer pb dom
Associer pb sch_RK3
Associer pb air
Discretiser pb dis
Lire pb
{
  Navier_Stokes_turbulent
  {
    Solveur_pression  petsc Cholesky { }
    Convection    { EF_stab { volumes_etendus alpha 0.2 } }
    Diffusion   { }
```

```
    Conditions_initiales  { vitesse champ_init_canal_sinal 3 { Ucent 9.8945 h 1 ampli_sin 0 ome
    Conditions_limites  {
          PerioX  periodique
          PerioZ  periodique
          Haut  paroi_decalee_Robin { delta 0.083333 }
          Bas paroi_decalee_Robin { delta 0.083333 }
          }
    Modele_turbulence sous_maille_WALE
          {
          turbulence_paroi loi_standard_hydr
          dt_impr_ustar 20
          }
    Traitement_particulier  {
          canal {
            dt_impr_moy_spat 200
            dt_impr_moy_temp 200
            debut_stat 600
            }
          }
    Sources     { canal_perio { direction_ecoulement 0 } }
    Sources     { source_Robin 2 Haut Bas 0.005 }
  }
  Convection_diffusion_temperature_turbulent
  {
    Convection    { EF_stab { volumes_etendus alpha 1 } }
    Diffusion   { }
    Conditions_initiales  { temperature champ_fonc_xyz dom 1 0 }
    Conditions_limites  {
          PerioX  periodique
          PerioZ  periodique
          Haut  paroi_decalee_Robin { delta 0.083333 }
          Bas paroi_decalee_Robin { delta 0.083333 }
          }
    Modele_turbulence Prandtl
          {
          turbulence_paroi loi_standard_hydr_scalaire
          dt_impr_nusselt 20
          }
    Sources     { puissance_thermique champ_uniforme 1 1 }
    Sources     { source_Robin_scalaire 2 Haut 0 Bas 0 0.005 }
  }
  Postraitement
  {
  Definition_champs   {
          moyenne_vitesse   Moyenne { t_deb 600 t_fin 1000 source refChamp { Pb_champ pb vitess
          moyenne_temperature Moyenne { t_deb 600 t_fin 1000 source refChamp { Pb_champ pb temp
          ecart_type_vitesse  Ecart_type { t_deb 600 t_fin 1000 source refChamp { Pb_champ pb v
          ecart_type_temperature  Ecart_type { t_deb 600 t_fin 1000 source refChamp { Pb_champ
          min_temperature   Reduction_0D { methode min source refChamp { Pb_champ pb temperatur
          max_temperature   Reduction_0D { methode max source refChamp { Pb_champ pb temperatur
          }
    Sondes      {
          sonde_vitesse     nodes vitesse     periode 0.5 points 1 3.2 1 1.6
          sonde_temperature   nodes temperature   periode 0.5 points 1 3.2 1 1.6
```

```
        sonde_moyenne_vitesse    nodes moyenne_vitesse    periode 0.5 points 1 3.2 1 1.6
        sonde_moyenne_temperature nodes moyenne_temperature periode 0.5 points 1 3.2 1 1.6
        sonde_ecart_type_vitesse  nodes ecart_type_vitesse  periode 0.5 points 1 3.2 1 1.6
        sonde_ecart_type_temperature  nodes ecart_type_temperature  periode 0.5 points 1 3.2
        coupe_vitesse      nodes vitesse      periode 5 segment 9 0.213333 0 0.177778 0.213333
        coupe_temperature   nodes temperature   periode 5 segment 9 0.213333 0 0.177778 0.213
        coupe_moyenne_vitesse   nodes moyenne_vitesse   periode 5 segment 9 0.213333 0 0.1777
        coupe_moyenne_temperature nodes moyenne_temperature periode 5 segment 9 0.213333 0 0.
        coupe_ecart_type_vitesse  nodes ecart_type_vitesse  periode 5 segment 9 0.213333 0 0.
        coupe_ecart_type_temperature  nodes ecart_type_temperature  periode 5 segment 9 0.213
        }
    Format lata_v2
    Champs dt_post 200  {
        vitesse som
        temperature som
        min_temperature som
        max_temperature som
        }
    Statistiques dt_post 200
        {
        t_deb 600 t_fin 1000
        moyenne vitesse
        moyenne temperature
        ecart_type vitesse
        ecart_type temperature
        }
  }
  sauvegarde formatte pb.sauv
}
Resoudre pb
Fin
```