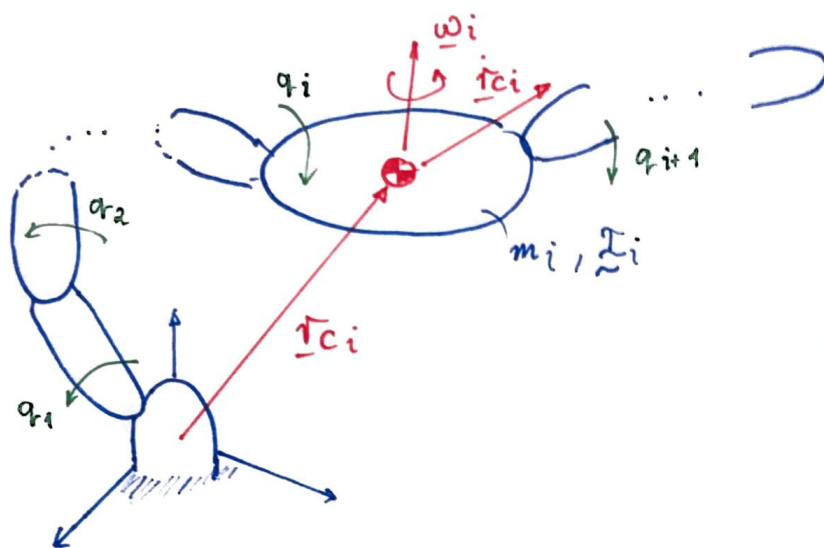


1. Dynamics of a fixed-base manipulator



$$\begin{aligned} \underline{\mathcal{V}}_{ICi}^h &= \begin{bmatrix} \underline{\dot{r}}_{ci} \\ \underline{\omega}_i \end{bmatrix} \\ &:= \begin{bmatrix} \underline{\dot{r}}_{ci} \\ \underline{s} \\ \underline{\omega}_{ICi} \end{bmatrix} \end{aligned}$$

Kinetic energy:
$$K = \frac{1}{2} \sum_{i=1}^n \left(m_i \underline{\dot{r}}_{ci}^T \underline{\dot{r}}_{ci} + \underline{\omega}_i^T \underline{I}_i \underline{\omega}_i \right)$$

Instantaneous rate of change of the generalized coordinates is mapped to the hybrid velocity of each link using Jacobians

$$\underline{\dot{r}}_{ci} = \frac{\partial \underline{r}_{ci}}{\partial \underline{q}} \underline{\dot{q}} = \underline{J}_{vi} \underline{\dot{q}}$$

$$\underline{\omega}_i = \underline{J}_{wi} \underline{\dot{q}}$$

$$\Rightarrow K = \frac{1}{2} \underline{\dot{q}}^T \underline{D}(\underline{q}) \underline{\dot{q}}$$
$$\underline{D}(\underline{q}) = \sum_{i=1}^n \left(m_i \underline{J}_{vi}^T \underline{J}_{vi} + \underline{J}_{wi}^T \underline{I}_i \underline{J}_{wi} \right)$$

Eq. of motion

$$\underline{D}(\underline{q}) \underline{\ddot{q}} + \underline{C}(\underline{q}) \underline{\dot{q}} + \underline{g}(\underline{q}) = \underline{\tau}$$

2. Dynamic model in spatial coordinates

- Interaction with the environment via end-links (e.g. end-effector, hands, feet)
- Tasks (desired motion / force) specified in spatial coordinates

→ How to express the eq. of motion wrt the end-link coordinates?

$$\underline{\tilde{D}} \underline{\dot{q}} + \underline{\tilde{C}} \underline{\dot{q}} + \underline{\tilde{g}} = \underline{\tau} \quad | \cdot \underline{J}^{-T}$$

assuming \underline{J} is invertible, then

$$\begin{aligned} \underline{\dot{q}} &= \underline{J}^{-1} \underline{\dot{\varphi}} \\ \underline{\dot{q}}^T &= \underline{\dot{\varphi}}^T (\underline{J}^{-1})^T \\ &= \underline{\dot{\varphi}}^T \underline{J}^{-T} \end{aligned}$$

$$\underline{\tilde{J}}^{-T} \underline{\tilde{D}} \underline{\dot{q}} + \underline{\tilde{J}}^{-T} \underline{\tilde{C}} \underline{\dot{q}} + \underline{\tilde{J}}^{-T} \underline{\tilde{g}} = \underline{\tilde{J}}^{-T} \underline{\tau}$$

$$\underline{\tilde{J}}^{-T} \underline{\tilde{D}} \underline{\tilde{J}}^{-1} \underline{\dot{\varphi}} - \underline{\tilde{J}}^{-T} \underline{\tilde{D}} \underline{\tilde{J}}^{-1} \underline{\dot{J}} \underline{\dot{q}} + \dots$$

$$\dots \underline{\tilde{J}}^{-T} \underline{\tilde{C}} \underline{\dot{q}} + \underline{\tilde{J}}^{-T} \underline{\tilde{g}} = \underline{\tilde{J}}^{-T} \underline{\tau}$$

$$\underline{\tilde{J}}^{-T} \underline{\tilde{D}} \underline{\tilde{J}}^{-1} = \underline{\tilde{\Lambda}} \quad \text{Operational space inertia matrix}$$

$$\underline{\tilde{J}}^{-T} (\underline{\tilde{C}} \underline{\dot{q}} - \underline{\tilde{D}} \underline{\tilde{J}}^{-1} \underline{\dot{J}} \underline{\dot{q}}) = \underline{\mu} \quad \text{Coriolis terms in operational space}$$

$$\underline{\tilde{J}}^{-T} \underline{\tilde{g}} = \underline{\rho} \quad \text{Gravitational terms in op. sp.}$$

$$\underline{F} = \underline{\tilde{J}}^{-T} \underline{\tau} \quad \text{End-effector wrench}$$

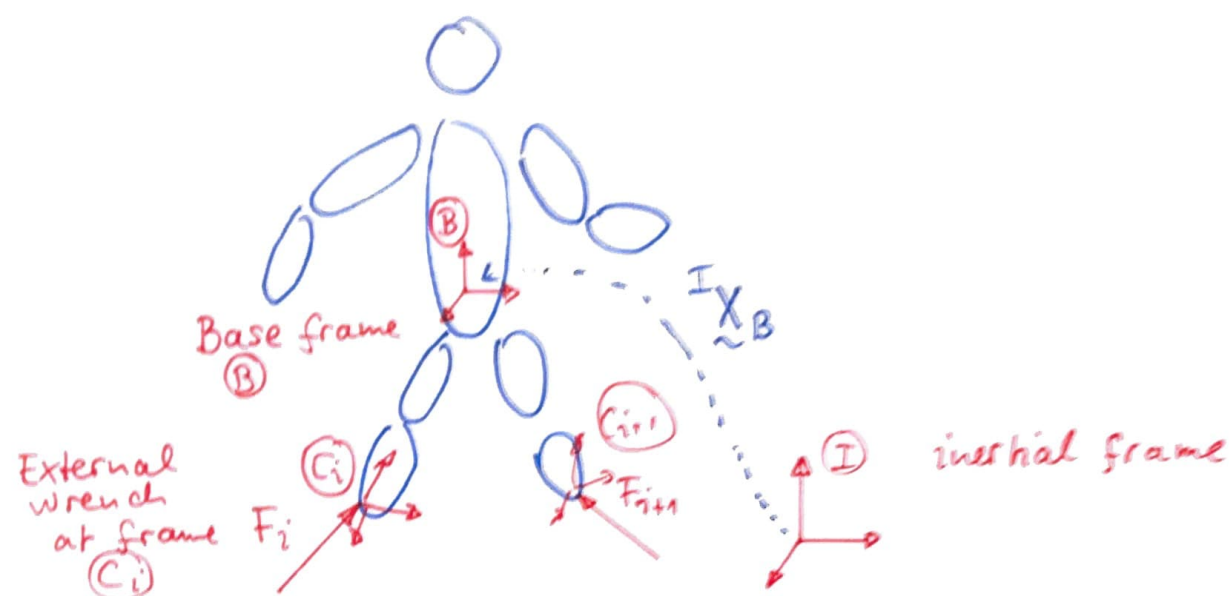
$$\Rightarrow \boxed{\underline{\tilde{\Lambda}} \underline{\dot{\varphi}} + \underline{\mu} + \underline{\rho} = \underline{F}}$$

$$\underline{\dot{\varphi}} = \underline{J}(\underline{q}) \underline{\dot{q}}$$

$$\underline{\dot{\varphi}} = \underline{J}(\underline{q}) \underline{\dot{q}} + \underline{\dot{J}}(\underline{q}) \underline{\dot{q}}$$

$$\underline{\dot{q}} = \underline{J}^{-1}(\underline{q}) \underline{\dot{\varphi}} - \underline{J}^{-1} \underline{\dot{J}} \underline{\dot{q}}$$

3. Floating-base dynamics



- Humanoid / legged robot : Base not mechanically connected to the inertial frame
- Base link has 6DoF which can be represented by a fictitious 6DoF (virtual) joint
- The floating-base DoFs are not actuated, thus legged robots are part of a special class of systems, namely underactuated systems (the number of control inputs is less than the number of DoFs)

The equations of motion can be obtained similar to the fixed-base case:

$$\begin{bmatrix} \tilde{\mathcal{D}}_b & \tilde{\mathcal{D}}_{bj} \\ \tilde{\mathcal{D}}_{bj}^T & \tilde{\mathcal{D}}_j \end{bmatrix} \begin{bmatrix} \dot{\underline{q}}_b \\ \dot{\underline{q}}_j \end{bmatrix} + \begin{bmatrix} \underline{c}_b \\ \underline{c}_j \end{bmatrix} + \begin{bmatrix} \underline{g}_b \\ \underline{g}_j \end{bmatrix} = \begin{bmatrix} \underline{0} \\ \underline{1} \end{bmatrix} + \underline{\tau}_{ext}$$

$$\underline{\tau}_{ext} = \sum_{i=1}^{nc} \begin{bmatrix} \tilde{Ad}_{B \times C_i}^B \\ \tilde{J}_i^T \end{bmatrix} \underline{F}_i$$

$\tilde{Ad}_{B \times C_i}^B$: Adjoint transformation relating an external wrench at (C_i) to the wrench expressed at the base frame (B)