

Flow-Based Cost Allocation in Linear Optimized Power Systems are non-unique but localizable

F. Hofmann, Brown T.

August 13, 2020

Abstract

Highlights

- The LMP always breaks down into contributions of different cost terms (OPEX, CAPEX, etc.) of the system.
- Breaking the LMP further down into contributions of components (generator, transmission line, etc.) requires assumptions on power flow assignments.
- Methods like Average Participation or Flow Based Market Coupling allow for localizing the P2P cost assignments and prioritize assignments within one market zone.

Nomenclature

$\lambda_{n,t}$	Locational Market Price at bus n and time step t in €/MW
$d_{n,t}$	Electric demand per bus n , demand type a , time step t in MW
$g_{s,t}$	Electric generation of generator s , time step t in MW
$f_{\ell,t}$	Active power flow on line ℓ , time step t in MW
o_s	Operational price in €/MW
c_s	Capital Price in €/MW
c_ℓ	Capital Price in €/MW for transmission capacity on line ℓ
G_s	Generation capacity in MW
F_ℓ	Transmission capacity in MW
$K_{n,\ell}$	Incidence matrix

1 Economic Context

In long-term operation and investment planning models, the total costs \mathcal{TC} of a power system is the sum of multiple cost terms. Typically, these include operational expenditures (OPEX) \mathcal{O}^G for generators, expenditures for emissions \mathcal{E} , capital expenditures (CAPEX) for generators \mathcal{C}^G , CAPEX for the transmission system \mathcal{C}^F and possible other terms, *i.e.*

$$\mathcal{TC} = \mathcal{O}^G + \mathcal{E} + \mathcal{C}^G + \mathcal{C}^F + \dots \quad (1)$$

In turn, each of these terms $\mathcal{C} = \{\mathcal{O}^G, \mathcal{E}, \mathcal{C}^G, \mathcal{C}^F, \dots\}$ consists of cost associated to the asset i in the system,

$$\mathcal{C} = \sum_i \mathcal{C}_i \quad (2)$$

where an asset describes any component of the network, such as a generator, line, energy storage etc.

In a cost-optimal setup with minimized \mathcal{TC} , the Locational Marginal Price (LMP) describes the price for an incremental increase of electricity demand $d_{n,t}$ at node n . It is given by the derivative of the total system cost \mathcal{TC} with respect to the local demand $d_{n,t}$

$$\lambda_{n,t} = \frac{\partial \mathcal{TC}}{\partial d_{n,t}} \quad (3)$$

This leads to a nodal pricing where over the span of optimized timesteps t , the system costs are partially or totally payed back by the consumers

$$\mathcal{TC} - \mathcal{R} = \sum_{n,t} \lambda_{n,t} d_{n,t} \quad (4)$$

depending on the costs \mathcal{R} which are independent of the nodal demand

$$\frac{\partial \mathcal{R}}{\partial d_{n,t}} = 0 \quad (5)$$

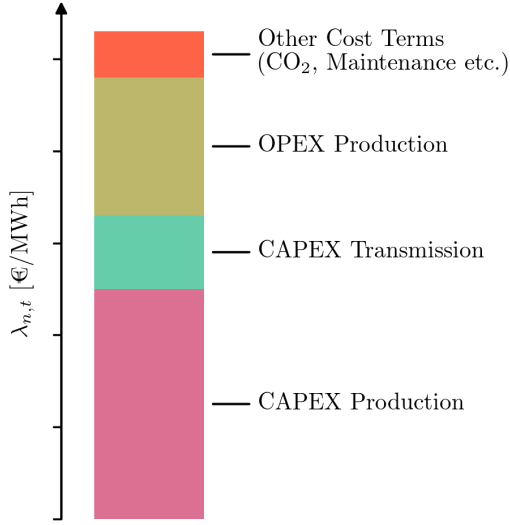


Figure 1: Schematic decomposition of the Locational Market Price $\lambda_{n,t}$. In power system model with optimal long-term operation and planning, the total system costs \mathcal{TC} split into different cost terms, *i.e.* OPEX and CAPEX for production and transmission and possibly other expenditures.

Generally speaking, the cost term \mathcal{R} , not covered by the consumers, results from additional demands on the network design, such as capacity expansion limits or minimum share of one technology in the power mix. However, in most cases, where $\mathcal{R} \ll \mathcal{TC}$, these play a minor role.

From feeding Eq. (1) into Eq. (3) it follows naturally that the LMP splits into contribution to the above mentioned cost terms. This relation, which we schematically show in Fig. 1, was already shown in extensive investigations of the LMP [8]. However the question of how the LMP can be decomposed into contributions of single cost terms \mathcal{C}_i associated with asset i remains unanswered. This work aims at presenting and illustrating an intuitive, peer-to-peer cost allocation including all network assets.

2 Dispatch-Based Cost Allocation

Let \mathcal{C}_i denote a general cost term associated with asset i . Consider a long-term equilibrium in a power system with perfect competition, then, according to the zero-profit condition, each cost term \mathcal{C}_i can be considered as a cost-weighted sum of the operational

state $s_{i,t}$ of asset i , *i.e.*

$$\mathcal{C}_i = \sum_t \gamma_{i,t} s_{i,t} \quad (6a)$$

where $\gamma_{i,t}$ denotes a cost factor in €/MW. If \mathcal{C}_i describes the OPEX occasioned by asset i , the cost factor $\gamma_{i,t}$ is simply given by the marginal operational price o_i . However, as we will show later, if it describes the CAPEX of asset i , $\gamma_{i,t}$ is a composition of shadow prices $\mu_{i,t}$ given at the optimum.

Following the implications of Eqs. (3) and (4), we define the cost $\mathcal{C}_{n \rightarrow i,t}$ that consumers at bus n have pay to asset i at time t , in order to compensate for \mathcal{C}_i , as

$$\mathcal{C}_{n \rightarrow i,t} = \gamma_{i,t} \frac{\partial s_{i,t}}{\partial d_{n,t}} d_{n,t} \quad (6b)$$

The product on the right hand side

$$A_{i,n,t} = \frac{\partial s_{i,t}}{\partial d_{n,t}} d_{n,t} \quad (6c)$$

may be interpreted as the amount of power that asset i supplies demand $d_{n,t}$ with. It heavily relies on the derivative of the operational state with respect to the nodal demand $\partial s_{i,t} / \partial d_{n,t}$. From the natural fact that the sum of all contributions must return the cost term,

$$\mathcal{C}_i = \sum_{n,t} \mathcal{C}_{n \rightarrow i,t} \quad (6d)$$

it follows that $A_{i,n,t}$ must fulfill

$$s_{i,t} = \sum_n A_{i,n,t} \quad (6e)$$

The last equation states that all power produced or processed by asset i must be totally consumed by the network demand $d_{n,t}$. Finally, the total contribution from node n at time t to the cost term \mathcal{C} amounts

$$\mathcal{C}_{n,t} = \sum_i \mathcal{C}_{n \rightarrow i,t} \quad (6f)$$

Now, assume a network with generators s , transmission lines ℓ and storage units r . Each asset $i = \{s, \ell, r\}$ adds an term for OPEX and a term for CAPEX to the total system cost \mathcal{TC} . The operational price for an asset i is given by o_i , the capital

	i	\mathcal{C}	\mathcal{C}_i	$\gamma_{i,t}$	$s_{i,t}$
OPEX Production	s	\mathcal{O}^G	$\sum_t o_s g_{s,t}$	o_s	$g_{s,t}$
OPEX Transmission	ℓ	\mathcal{O}^F	$\sum_t o_\ell f_{\ell,t} $	o_ℓ	$ f_{\ell,t} $
OPEX Storage	r	\mathcal{O}^E	$\sum_t o_r g_{r,t}^{\text{dis}}$	o_r	$g_{r,t}$
CAPEX Production	s	\mathcal{C}^G	$c_s G_s$	$\bar{\mu}_{s,t}$	$g_{s,t}$
CAPEX Transmission	ℓ	\mathcal{C}^F	$c_\ell F_\ell$	$(\bar{\mu}_{\ell,t} - \underline{\mu}_{\ell,t})$	$f_{\ell,t}$
CAPEX Storage	r	\mathcal{C}^E	$c_r G_r$	$\bar{\mu}_{r,t}^{\text{dis}} - \underline{\mu}_{r,t}^{\text{dis}} + (\eta_r^{\text{dis}})^{-1} \lambda_{r,t}^{\text{ene}}$	$g_{r,t}$
Emission Cost	s	\mathcal{E}	$\mu_{\text{CO2}} e_s g_{s,t}$	$\mu_{\text{CO2}} e_s$	$g_{s,t}$

Table 1: Mapping of different cost terms to the cost allocation scheme given in Eqs. (6). These include OPEX & CAPEX for production, transmission and storage assets in the network, as well as a cost term for the total Green House Gas (GHG) emissions.

price for one unit capacity expansion by c_i . For example the OPEX occasioned by generator s is given by

$$\mathcal{O}_s^G = \sum_t o_s g_{s,t} \quad (7)$$

where $g_{s,t}$ denotes its power generation at time t . As Eq. (7) matches the form of Eq. (6a) which allows us to use the above presented scheme in Eqs. (6). As a result we obtain

$$\mathcal{O}_{n \rightarrow s,t} = o_s A_{s,n,t} \quad (8)$$

which is the contribution of $d_{n,t}$ to the OPEX at generator s . The quantity

$$A_{s,n,t} = \frac{\partial g_{s,t}}{\partial d_{n,t}} d_{n,t} \quad (9)$$

can be considered as the power that is produced by generator s and consumed at node n at time t .

In the same manner, we can follow the scheme allocate OPEX for flow $f_{\ell,t}$ and storage unit dispatch $g_{r,t}^{\text{dis}}$. As we assume a bidirectional flow on line ℓ , the OPEX is set proportional to the absolute value of the flow. The upper section in Table 1 shows the mapping of variables to Eqs. (6) in order to define the full OPEX allocation.

For the CAPEX allocation, it becomes crucial to look at the individual relations between operational state $s_{i,t}$ and the capacity limit. All quantities for the CAPEX allocation, which we now discuss in detail in the following, are summarized in the middle section of Table 1.

Allocate CAPEX on Generators

The nominal capacity G_s constrains the generation $g_{s,t}$ in the form of

$$g_{s,t} - \bar{g}_{s,t} G_s \leq 0 \quad \perp \quad \bar{\mu}_{s,t} \quad \forall s, t \quad (10)$$

$$-g_{s,t} \leq 0 \quad \perp \quad \underline{\mu}_{s,t} \quad \forall s, t \quad (11)$$

where $\bar{g}_{s,t} \in [0, 1]$ is the capacity factor for renewable generators. At a cost-optimum, these two constraints yield the shadow prices $\bar{\mu}_{s,t}$ and $\underline{\mu}_{s,t}$. As shown in [3] and in detailed in Appendix A.3, over the whole time span, the CAPEX for generator s is payed back by the production $g_{s,t}$ times the shadow price $\bar{\mu}_{s,t}$,

$$\mathcal{C}_s^G = c_s G_s = \sum_t \bar{\mu}_{s,t} g_{s,t} \quad (12)$$

This representation connects the CAPEX with the operational state of generator s , *i.e.* matches the form in Eq. (6a) allows for using the cost allocation scheme. The resulting the CAPEX allocation is given by

$$\mathcal{C}_{n \rightarrow s,t}^G = \bar{\mu}_{s,t} A_{s,n,t} \quad (13)$$

How does this allocation behave? According to the polluter pays principle, it differentiates between consumers who are ‘responsible’ for investments and those who are not. If $\bar{\mu}_{s,t}$ (in literature often denoted as the Quality of Supply) is bigger than zero, the upper Capacity Constr. (10) is binding. Thus it is these times steps which push investments in G_s . If $\bar{\mu}_{s,t} = 0$, the generation $g_{s,t}$ is not bound and investments are not necessary. When summing over all CAPEX payments to generator s in Eq. (13), we can use Eqs. (6e) and (12) to see that each generator retrieves exactly the cost that were spent to build the capacity G_s .

Allocate CAPEX on Transmission Lines

The transmission capacity F_ℓ limits the flow $f_{\ell,t}$ in both directions,

$$f_{\ell,t} - F_\ell \leq 0 \perp \bar{\mu}_{\ell,t} \quad \forall \ell, t \quad (14)$$

$$-f_{\ell,t} - F_\ell \leq 0 \perp \underline{\mu}_{\ell,t} \quad \forall \ell, t \quad (15)$$

which yield the shadow prices $\bar{\mu}_{\ell,t}$ and $\underline{\mu}_{\ell,t}$. Again, we use the result of [3] (for details see Appendix A.4) which derives that over the whole time span, the investment in line ℓ is paid back by the shadow prices times the flow

$$\mathcal{C}_\ell^F = c_\ell F_\ell = \sum_t (\bar{\mu}_{\ell,t} - \underline{\mu}_{\ell,t}) f_{\ell,t} \quad (16)$$

From here, we follow the scheme in Eqs. (6) which finally defines the CAPEX allocation as

$$\mathcal{C}_{n \rightarrow \ell, t}^F = (\bar{\mu}_{\ell,t} - \underline{\mu}_{\ell,t}) A_{\ell, n, t} \quad (17)$$

The quantity

$$A_{\ell, n, t} = \frac{\partial f_{\ell,t}}{\partial d_{n,t}} d_{n,t} \quad (18)$$

can be interpreted as the flow that the demand at (n, t) causes on line ℓ . The shadowprices $\bar{\mu}_{\ell,t}$ and $\underline{\mu}_{\ell,t}$ again can be seen as a measure for necessity of transmission investments at ℓ at time t . Hence, the definition of $\mathcal{C}_{n \rightarrow \ell, t}^F$ states that consumers, which retrieve power flowing on congested lines, yielding a bound Constr. (14) or (15), pay compensations for the resulting investments at ℓ . Again the sum of all CAPEX payments to line ℓ equals the total CAPEX spent. This is seen when summing Eq. (17) over all buses and time steps and using Eqs. (6e) and (16)

Allocate CAPEX on Storages

In a simplified storage model, G_r limits the storage dispatch $g_{r,t}^{\text{dis}}$ and charging $g_{r,t}^{\text{sto}}$. Further it limits the maximal storage capacity $g_{r,t}^{\text{ene}}$ by a fix ratio h_r , denoting the maximum hours at full discharge. The storage r dispatches power with efficiency η_r^{dis} , charges power with efficiency η_r^{sto} and preserves power from one time step t to the next, $t+1$, with an efficiency of η_r^{ene} . In Appendix A.5 we formulate the mathematical details. As already shown in [3], the total expenditures at r are fully paid back by differences of the LMP at which the storage

“buys“ and “sells“ power. Taking only the CAPEX into account the zero profit condition reduces to

$$\begin{aligned} \mathcal{C}^E &= c_r G_r \\ &= \sum_t \left(\bar{\mu}_{r,t}^{\text{dis}} - \underline{\mu}_{r,t}^{\text{dis}} + (\eta_r^{\text{dis}})^{-1} \lambda_{r,t}^{\text{ene}} \right) g_{r,t}^{\text{dis}} \\ &\quad - \sum_t \lambda_{n,t} K_{n,r} g_{r,t}^{\text{sto}} \quad \forall r \end{aligned} \quad (19)$$

where $\bar{\mu}_{r,t}^{\text{dis}}$ and $\underline{\mu}_{r,t}^{\text{dis}}$ are the shadow prices of the upper and lower capacity bound of the power dispatch of r and $\lambda_{r,t}^{\text{ene}}$ is the shadow price of the energy balance constraint. Equation (19) matches the form of Eq. (6a). However when applying Eq. (6b) it follows naturally that to assume $\partial g_{r,t}^{\text{sto}} / \partial d_{n,t} = 0$, implying that the when a storage charges power, it does not supply any demand. Rather it stands with the demand on the consumer side, retrieving power from producing assets. This leaves us with

$$\mathcal{C}_{n \rightarrow r, t}^E = \left(\bar{\mu}_{r,t}^{\text{dis}} - \underline{\mu}_{r,t}^{\text{dis}} + (\eta_r^{\text{dis}})^{-1} \lambda_{r,t}^{\text{ene}} \right) A_{r, n, t} \quad (20)$$

and the power allocation

$$A_{r, n, t} = \frac{\partial g_{r,t}^{\text{dis}}}{\partial d_{n,t}} d_{n,t} \quad (21)$$

The latter only allocates dispatched power of storage r . Note that this will break Eq. (6d) as the payments to r surpass the CAPEX by an amount \mathcal{R}_r^E . However the fact that storages themselves “buy“ power from other the assets, when charging, the cost allocation in Eqs. (6) may be applied to the consumption of storages themselves, by replacing the demand $d_{n,t}$ with the power charge $g_{r,t}^{\text{sto}}$ in Eqs. (6). This derives payments that a storage unit r has to pay to asset i , namely $\mathcal{C}_{r \rightarrow i}$. The sum of those payments due to r will the add up to \mathcal{R}_r^E .

Allocate Emission Expenditures

Given a fix price for emissions in CO₂ equivalents μ_{CO_2} , the cost term for emission adds up to

$$\mathcal{E} = \mu_{\text{CO}_2} \sum_s e_s g_{s,t} \quad (22)$$

where e_s denotes the emission factor in tonne-CO₂ per MWh_{el} for generator s . We use the same set of equation as given through Eqs. (6) and ?? but update the cost factor to $\gamma_{i,t} \Rightarrow \mu_{\text{CO}_2} e_s$. For consumers at bus n at time t this leads to the emission cost of

$$\mathcal{E}_{n \rightarrow s, t} = \mu_{\text{CO}_2} e_s A_{s, n, t} \quad (23)$$

associated with generator s .

3 Assumptions on Power Allocations

The presented cost allocation suits for any type of topology and network setup. But so far, the question of how $A_{i,n,t}$ for generators s , lines ℓ and storages r are defined was left open. We recap that all rely on derivatives of $g_{s,t}$, $f_{\ell,t}$ and $g_{r,t}^{\text{dis}}$ with respect to the nodal demand $d_{n,t}$ (see Eq. (6e)).

Let $g_{m,t}$ denote the nodal power generation which combines the power production of all producing assets, in this case generators S and storages R , at node n and time t . It is given by

$$g_{m,t} = \sum_{i \in \{S,R\}} K_{m,i} s_{i,t} \quad (24)$$

with $K_{m,i}$ being 1 if asset i is attached to bus m and zero otherwise. Further, let $A_{m \rightarrow n,t}$ collect the power produced by assets at node m and consumed at n , given by

$$A_{m \rightarrow n,t} = \sum_{i \in \{S,R\}} K_{m,i} A_{i,n,t} \quad (25)$$

Now, let $H_{\ell,n}$ denote Power Transfer Distribution Factors (PTDF) giving the changes in the flow on line ℓ for one unit (typically one MW) of net power production at bus n . The linear power flow equation can be written as

$$f_{\ell,t} = \sum_m H_{\ell,m} (g_{m,t} - d_{m,t}) \quad (26)$$

Note that for transport models or mixed AC-DC networks, $H_{\ell,n}$ can be artificially calculated using the formulation presented in [6]. Taking the derivative with respect to the demand,

$$A_{\ell,n,t} = \frac{\partial f_{\ell,t}}{\partial d_{n,t}} d_{n,t} = \sum_m H_{\ell,m} (A_{m \rightarrow n,t} - \delta_{n,m} d_{n,t}), \quad (27)$$

shows that $A_{\ell,n,t}$ is fully determined through the peer-to-peer allocation $A_{m \rightarrow n,t}$. In other words, we only need to know how much power produced at node m is consumed at node n in order to derive the allocated flow $A_{\ell,n,t}$. Further we can breakdown $A_{m \rightarrow n,t}$ to $A_{s,n,t}$ for generators and $A_{r,n,t}$ for storages proportionally to their contribution to the nodal generation $g_{m,t}$. Unfortunately, the solution for $A_{m \rightarrow n,t}$ is

non-unique and requires further assumptions. Established flow allocation schemes approach this problem from different directions. Principally two options exist *what* is allocated

1. gross power injections
2. net power injections

Further it is important *what assumptions* define the allocation, *i.e.* what method is used to define the pairs of sources and sinks. The three suitable approaches we present here are

- a. Equivalent Bilateral Exchanges (EBE) [4] which assumes that every producer supplies every consumer proportional to its share in the total consumption.
- b. Average Participation (AP) [2, 1] which traces the flow from producer to consumer following the law of proportional sharing.
- c. Flow Based Market Coupling (FBMC) which uses zonal PTDF for allocating power within predefined regions. The interregional exchange is only allocating net power deficit or excess of the regions.

We show the mathematical formulation for all combinations **a1** - **c2** in Appendices A.8 to A.11. Principally, type **2** leads to less P2P trades than type **1** as power from a bus m with $g_{m,t} \leq d_{m,t}$ is not assigned to other buses, only to m . Further, as literature has often pointed out, the EBE principal **a** does not suit for large networks where remote buses would interconnect in the same way as buses in close vicinity [5]. The AP based type **b** tackles this problem by restricting P2P trades to those which are traceable when applying the proportional sharing principal. Therefore $A_{s,n,t}$ denotes that part of power produced by bus m which, when only following in the direction of $f_{\ell,t}$, ends up at bus n . Type **c** further allows to control the regions or market zones which are netted out in a first step. If in a region R the generation undercuts the demand, $\sum_{n \in R} g_{n,t} \leq \sum_{n \in R} d_{n,t}$, none of the inner-regional generation is assigned to other regions.

3.1 Numerical Example

In the following, we illustrate the cost allocation and explain its functionality by taking the example of a

two bus system with one optimized time step, shown in Fig. 2.

The two buses are connected via one transmission line, each has one generator. Whereas generator 1 (at bus 1) has an operational price of 50 €/MWh_{el}, generator 2 (at bus 2) has a higher operational price of 200 €/MWh_{el}. For both the CAPEX rate is set to 500 €/MW and the maximal capacity is limited to $\bar{G}_s = 100$ MW. The transmission line has a CAPEX rate of 100 €/MW and no upper capacity limit. With a demand of 60 MW at bus 1 and 90 MW at bus 2, the optimization expands the cheaper generator at bus 1 to its full limit of 100 MW. The 40 MW excess power, not consumed at bus 1, flows to bus 2 where the generator is built with only 50 MW.

Allocating Gross Power using EBE (1a)

Figure 3 shows the allocated transactions on basis of equivalently traded gross power (type 1a) for both buses 1 & 2 separately. The resulting P2P payments are given in Fig. 4. The upper graph Fig. 3a shows that $A_{1 \rightarrow 1} = 40$ MW at bus 1 are self-sustained. With only one generator at bus 1, consumers at bus 1 consequently pay 2k € OPEX and 22k € CAPEX to the generator 1. The remaining 20 MW come from bus 2 and induce a subflow on line 1 of $A_{\ell=1,1} = -20$. As this flow is in contrary direction to the total flow, it is relieving the transmission system. This translates to a congestion reward for consumers at bus 1 of $c_{\ell=1} A_{\ell=1,1} = 2k$ € which is exactly the cost that had to be spent on the transmission system if bus 1 didn't induce a relieving flow, see again Fig. 4.

The lower graph Fig. 3b illustrates the impact of consumption at bus 2. As d_2 is higher than d_1 the retrievments from both generators are proportionately increased as well as the OPEX and CAPEX allocations to the generators. But instead of a relieving flow, consumers at bus 2 drive the burdening flow in direction of congestion. Hence the payoff to the transmission system is positive and much higher than for bus 1.

The sum of all rows in the payoff matrix in Fig. 4 yields the revenues of the assets m, ℓ . These values match their overall spendings, *e.g.* the total revenue of the transmission line is 4k € which equals the cost for investments $c_1 F_1$. The sum of all columns yields the total payment of consumers at bus n . For example the sum of payments of consumers at bus 1 is 36k €. This is exactly the electricity price of

600 €/MW times the consumption of 60 MW, $\lambda_1 d_1$.

The fact that OPEX and CAPEX allocations are proportional to the total consumption at a bus results from optimizing one time step only. In larger optimization problems with multiple time steps the CAPEX allocation takes effect only for time steps in which one or more of the capacity constraints Constrs. (10), (14) and (15) become binding.

Allocating Net Power using EBE (2a)

In contrast the to equivalent allocation of gross power production, netting out injections for each bus leads to less P2P payments. The resulting payment given in Fig. 5 builds on the allocated power flow shown Fig. A.1 in Appendix A.12. As bus 2 does not produce excess power, none of its power production is assigned to bus 1 and thus no payment of bus 1 to bus 2 allocated. Neither has bus 1 to pay fee to the transmission system as it only exports power. So all its consumers pay to its local generators. Bus 2 in constrast bear all CAPEX for the transmission system as well as CAPEX and OPEX for generators at bus 1. Again the cumulative payments per bus meet the nodal spendings $\lambda_{n,t} d_{n,t}$. The cumulative revenues per generator and transmission line meet the all CAPEX and OPEX.

As the other schemes b1 - c2 apart from the EBE scheme don't distinguishably modify allocations within the presented example, we move on to a more realistic setup where systemic and local effects show up.

4 Application Case

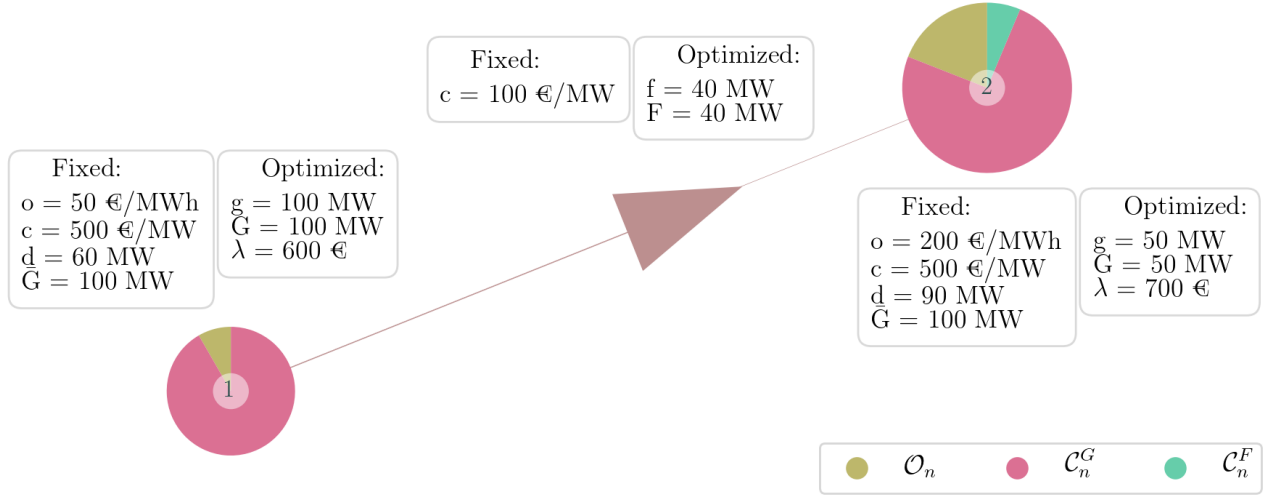


Figure 2: Illustrative example of a 2-bus network with one optimized time step. Fixed prices and constraining values are given in the left box for each bus and the transmission line. Optimized values are given in the right boxes. Bus 1 has a cheaper operational price o , capital prices are the same for both. As both generator capacities are constraint to 100 MW, the optimization also deploys the generator at bus 2. The resulting electricity prices λ are then a composition of all prices for operation and capital investments.

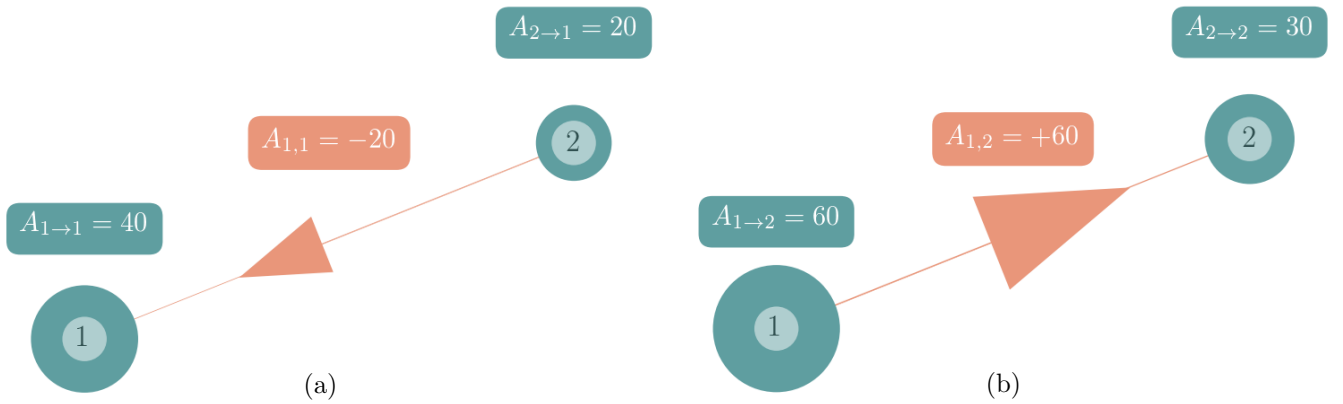


Figure 3: Power allocations of equivalently allocated gross power, type 1a, for bus 1 (a) and bus 2 (b) of the example network in Fig. 2. Bus 1 retrieves 40 MW from itself and 20 MW from bus 2. The latter in turn retrieves 60 MW from bus 1 and self supplies 30 MW. The sum of both net flows equals the resulting flow of $f_1 = 40 \text{ MW}$.

		\mathcal{O}		\mathcal{C}^G		\mathcal{C}^F
n	1	2k €	4k €	22k €	10k €	-2k €
	2	3k €	6k €	33k €	15k €	6k €
		1	2	1	2	1
		s		s		ℓ

Figure 4: Full P2P cost allocation for the example setup shown in Fig. 2. The payments are derived on the basis of Eqs. (8), (13) and (17). Consumers at bus n have to pay each generator proportional to their consumption. As we only consider one time step the proportionality applies for OPEX $\mathcal{O}_{n \rightarrow s, t}$ and CAPEX $\mathcal{C}_{n \rightarrow i}$. As bus 1 induces a relieving flow on line 1 and therefore “prevents” further transmission expansion, it is rewarded proportional to the relief.

		\mathcal{O}		\mathcal{C}^G		\mathcal{C}^F
n	1	3k €	0k €	33k €	0k €	0k €
	2	2k €	10k €	22k €	25k €	4k €
		1	2	1	2	1
		s		s		ℓ

Figure 5: Full P2P cost allocation for the example setup shown in Fig. 2 when equivalently allocation net power injection (scheme a2).

A Appendix

A.1 LMP from Optimization

The nodal balance constraint ensures that the amount of power that flows into a bus equals the power that flows out of a bus, thus reflects the Kirchhoff Current Law (KCL). Alternatively, we can the demand $d_{n,t}$ has to be supplied by the attached as-sets,

$$\sum_i K_{n,i} s_{i,t} = d_{n,t} \perp \lambda_{n,t} \quad \forall n, t \quad (\text{A.1})$$

where $K_{n,i}$ is +1 if i is attached to n and a positive operation $s_{i,t}$ delivers power to n , -1 if is attached to n and a positive operation retrieves power from n and zero else (note that for lines this results in the negative of the conventional Incidence Matrix). The shadow price of the nodal balance constraint mirrors the Locational Marginal Prizes (LMP) $\lambda_{n,t}$ per bus and time step. In a power market this is the €/MWh_{el}-price which a consumer has to pay.

A.2 Full Lagrangian

The Lagrangian for the investment model can be condensed to the following expression

$$\begin{aligned} \mathcal{L}(s_{i,t}, S_i, \lambda_{n,t}, \mu_j) = & \sum_{i,t} o_i s_{i,t} + \sum_i c_i S_i \\ & + \sum_{n,t} \lambda_{n,t} \left(d_{n,t} - \sum_i K_{n,i} s_{i,t} \right) \\ & + \sum_j \mu_j h_j(s_{i,t}, S_i) \end{aligned} \quad (\text{A.2})$$

where $h_j(s_{i,t}, S_i)$ denotes all inequality constraints attached to $s_{i,t}$ and S_i . In order to impose the Kirchhoff Voltage Law (KVL) for the linearized AC flow, the term

$$\sum_{\ell,c,t} \lambda_{c,t} C_{\ell,c} x_\ell f_{\ell,t} \quad (\text{A.3})$$

can be added to \mathcal{L} , with x_ℓ denoting the line's impedance and $C_{\ell,c}$ being 1 if ℓ is part of the cycle c and zero otherwise.

The global maximum of the Lagrangian requires stationarity with respect to all variables:

$$\frac{\partial \mathcal{L}}{\partial s_{i,t}} = \frac{\partial \mathcal{L}}{\partial S_i} = 0 \quad (\text{A.4})$$

A.3 Zero Profit Generation

Constrs. (10) and (11), which yield the KKT variables $\bar{\mu}_{s,t}$ and $\underline{\mu}_{s,t}$, imply the complementary slackness,

$$\bar{\mu}_{s,t} (g_{s,t} - \bar{g}_{s,t} G_s) = 0 \quad \forall n, s, t \quad (\text{A.5})$$

$$\underline{\mu}_{s,t} g_{s,t} = 0 \quad \forall n, s, t \quad (\text{A.6})$$

The stationarity of the generation capacity variable leads to

$$\frac{\partial \mathcal{L}}{\partial G_s} = 0 \rightarrow c_s = \sum_t \bar{\mu}_{s,t} \bar{g}_{s,t} \quad \forall n, s \quad (\text{A.7})$$

and the stationarity of the generation to

$$\frac{\partial \mathcal{L}}{\partial g_{s,t}} = 0 \rightarrow o_s = K_{n,s} \lambda_{n,t} - \bar{\mu}_{s,t} + \underline{\mu}_{s,t} \quad \forall n, s \quad (\text{A.8})$$

Multiplying both sides of Eq. (A.7) with G_s and using Eq. (A.5) leads to

$$c_s G_s = \sum_t \bar{\mu}_{s,t} g_{s,t} \quad (\text{A.9})$$

The zero-profit rule for generators is obtained by multiplying Eq. (A.8) with $g_{s,t}$ and using Eqs. (A.6) and (A.9) which results in

$$c_s G_s + \sum_t o_s g_{s,t} = \sum_t \lambda_{n,t} K_{n,s} g_{s,t} \quad (\text{A.10})$$

It states that over the whole time span, all OPEX and CAPEX for generator s (left hand side) are payed back by its revenue (right hand side).

A.4 Zero Profit Transmission System

The yielding KKT variables $\bar{\mu}_{\ell,t}$ and $\underline{\mu}_{\ell,t}$ are only non-zero if $f_{\ell,t}$ is limited by the trasmission capacity in positive or negative direction, i.e. Constr. (14) or Constr. (15) are binding. For flows below the thermal limit, the complementary slackness

$$\bar{\mu}_{\ell,t} (f_{\ell,t} - F_\ell) = 0 \quad \forall \ell, t \quad (\text{A.11})$$

$$\underline{\mu}_{\ell,t} (f_{\ell,t} - F_\ell) = 0 \quad \forall \ell, t \quad (\text{A.12})$$

sets the respective KKT to zero.

The stationarity of the transmission capacity to

$$\frac{\partial \mathcal{L}}{\partial F_\ell} = 0 \rightarrow c_\ell = \sum_t (\bar{\mu}_{\ell,t} - \underline{\mu}_{\ell,t}) \quad \forall \ell \quad (\text{A.13})$$

and the stationarity with respect to the flow to

$$0 = \frac{\partial \mathcal{L}}{\partial f_{\ell,t}} \quad (\text{A.14})$$

$$0 = - \sum_n K_{n,\ell} \lambda_{n,t} + \lambda_{c,t} C_{\ell,c} x_{\ell} - \bar{\mu}_{\ell,t} + \underline{\mu}_{\ell,t} \quad \forall n, s \quad (\text{A.15})$$

When multiplying Eq. (A.13) with F_{ℓ} and using the complementary slackness Eqs. (A.11) and (A.12) we obtain

$$c_{\ell} F_{\ell} = \sum_t (\bar{\mu}_{\ell,t} - \underline{\mu}_{\ell,t}) f_{\ell,t} \quad (\text{A.16})$$

Again we can use this to formulate the zero-profit rule for transmission lines. We multiply Eq. (A.15) with $f_{\ell,t}$, which finally leads us to

$$c_{\ell} F_{\ell} = - \sum_n K_{n,\ell} \lambda_{n,t} f_{\ell,t} + \lambda_{c,t} C_{\ell,c} x_{\ell} f_{\ell,t} \quad (\text{A.17})$$

It states that the congestion revenue of a line (first term right hand side) subtracted by the cost for cycle constraint exactly matches its CAPEX.

A.5 Zero Profit Storage Units

For an simplified storage model, the upper capacity G_r limits the discharging dispatch $g_{r,t}^{\text{dis}}$, the storing power $g_{r,t}^{\text{sto}}$ and state of charge $g_{r,t}^{\text{ene}}$ of a storage unit r by

$$g_{r,t}^{\text{dis}} - G_r \leq 0 \quad \forall r, t \perp \bar{\mu}_{r,t}^{\text{dis}} \quad (\text{A.18})$$

$$g_{r,t}^{\text{sto}} - G_r \leq 0 \quad \forall r, t \perp \bar{\mu}_{r,t}^{\text{sto}} \quad (\text{A.19})$$

$$g_{r,t}^{\text{ene}} - h_r G_r \leq 0 \quad \forall r, t \perp \bar{\mu}_{r,t}^{\text{ene}} \quad (\text{A.20})$$

where we assume a fixed ratio between dispatch and storage capacity of h_r . The state of charge must be consistent throughout every time step according to what is dispatched and stored,

$$g_{r,t}^{\text{ene}} - \eta_r^{\text{ene}} g_{r,t-1}^{\text{ene}} - \eta_r^{\text{sto}} g_{r,t}^{\text{sto}} + (\eta_r^{\text{dis}})^{-1} g_{r,t}^{\text{dis}} = 0 \quad \perp \lambda_{r,t}^{\text{ene}} \quad \forall r, t \quad (\text{A.21})$$

We use the result of Appendix B.3 in [3] which shows that a storage recovers its capital (and operational) costs from aligning dispatch and charging to the LMP, thus

$$\sum_t o_r g_{r,t}^{\text{dis}} + c_r G_r = \sum_t \lambda_{n,t} K_{n,r} (g_{r,t}^{\text{dis}} - g_{r,t}^{\text{sto}}) \quad (\text{A.22})$$

The stationarity of the dispatched power leads us to

$$\frac{\partial \mathcal{L}}{\partial g_{r,t}^{\text{dis}}} = 0$$

$$o_r - \lambda_{n,t} K_{n,r} - \underline{\mu}_{r,t}^{\text{dis}} + \bar{\mu}_{r,t}^{\text{dis}} + (\eta_r^{\text{dis}})^{-1} \lambda_{r,t}^{\text{ene}} = 0 \quad (\text{A.23})$$

which we can use to define the revenue which compensates the CAPEX at r ,

$$c_r G_r = \sum_t \left(\bar{\mu}_{r,t}^{\text{dis}} - \underline{\mu}_{r,t}^{\text{dis}} + (\eta_r^{\text{dis}})^{-1} \lambda_{r,t}^{\text{ene}} \right) g_{r,t}^{\text{dis}} - \sum_t \lambda_{n,t} K_{n,r} g_{r,t}^{\text{sto}} \quad \forall r \quad (\text{A.24})$$

A.6 CO₂ constraint

Imposing an additional CO₂ constraint limiting the total emission to K ,

$$\sum_{n,s,t} e_s g_{s,t} \leq K \perp \mu_{\text{CO}_2} \quad (\text{A.25})$$

with e_s being the emission factor in tonne-CO₂ per MWh_{el}, returns an effective CO₂ price μ_{CO_2} in €/tonne-CO₂. As shown in ... the constraint can be translated in a dual price which shift the operational price per generator

$$o_s \rightarrow o_s + e_s \mu_{\text{CO}_2} \quad (\text{A.26})$$

A.7 Brownfield Optimization and Capacity Restrictions

Constraining the capacities G_s for a subset S of generators to lower or upper limits in the form of

$$\underline{G}_s - G_s \leq 0 \perp \underline{\mu}_s^{\text{nom}} \quad \forall s \in S \quad (\text{A.27})$$

$$G_s - \bar{G}_s \leq 0 \perp \bar{\mu}_s^{\text{nom}} \quad \forall s \in S \quad (\text{A.28})$$

alters the objective value as soon as one of those become bounding. The complementary slackness for both are

$$\bar{\mu}_s^{\text{nom}} (G_s - \bar{G}_s) = 0 \quad \forall s \in S \quad (\text{A.29})$$

$$\underline{\mu}_s^{\text{nom}} (\underline{G}_s - G_s) = 0 \quad \forall s \in S \quad (\text{A.30})$$

The CAPEX paybacks for generators and transmission lines Eqs. (A.9) and (A.16) change to

$$\frac{\partial \mathcal{L}}{\partial G_s} = 0 \rightarrow \quad (\text{A.31})$$

$$c_s = \sum_t \bar{\mu}_{s,t} \bar{g}_{s,t} + \underline{\mu}_s^{\text{nom}} - \bar{\mu}_s^{\text{nom}} \quad \forall s \in S \quad (\text{A.32})$$

for generators. Multiplying Eq. (A.32) by G_s leads us to

$$\mathcal{C}_s^G - \mathcal{R}_s = \sum_t \bar{\mu}_{s,t} g_{s,t} \quad \forall n, s \in S \quad (\text{A.33})$$

where we define the cost resulting from the capacity expansion limits as

$$\mathcal{R}_s = (\mu_s^{\text{nom}} - \bar{\mu}_s^{\text{nom}}) G_s \quad \forall s \quad (\text{A.34})$$

As $\mu_s^{\text{nom}} \geq 0$ and $\bar{\mu}_s^{\text{nom}} \geq 0$, the latter can be a net positive or net negative cost term.

Multiplying Eq. (A.8), which is still valid, with $g_{s,t}$ and inserting Eq. (A.33) will bring us to the zero profit rule for generators with capacity expansion limits,

$$\mathcal{C}_s^G + \mathcal{O}_s^G - \mathcal{R}_s = \sum_t \lambda_{n,t} K_{n,s} g_{s,t} \quad \forall s \in S \quad (\text{A.35})$$

We see that the revenue of generator s will not exactly pay back its full CAPEX and OPEX. The exogenous constraint shifts the zero-profit equations such that some of the expenditures for $s \in S$ cannot directly be allocated to consumers. In order to take this effect into account for the cost allocation, we update the shadow price $\bar{\mu}_{s,t}$ in Table 1, to

$$\bar{\mu}_{s,t} \rightarrow \frac{c_s}{c_s - \mu_s^{\text{nom}} + \bar{\mu}_s^{\text{nom}}} \bar{\mu}_{s,t} \quad (\text{A.36})$$

By doing so we ensure that the allocated CAPEX sum up to the actual CAPEX at generator s , thus

$$\mathcal{C}_s^G = \sum_{n,t} \mathcal{C}_{n \rightarrow s,t}^G \quad \forall s \in S \quad (\text{A.37})$$

Doing likewise with a subset L of transmission lines,

$$F_\ell \geq \underline{F}_\ell \perp \underline{\mu}_\ell^{\text{nom}} \quad \forall \ell \in L \quad (\text{A.38})$$

$$F_\ell \leq \bar{F}_\ell \perp \bar{\mu}_\ell^{\text{nom}} \quad \forall \ell \in L \quad (\text{A.39})$$

results in a shifted zero-profit rule for transmission line in the form

$$c_\ell F_\ell - \mathcal{R}_\ell = \sum_{n,t} \mathcal{C}_{n \rightarrow \ell,t}^F \quad \forall \ell \in L \quad (\text{A.40})$$

where \mathcal{R}_ℓ is given by

$$\mathcal{R}_\ell = (\underline{\mu}_\ell^{\text{nom}} - \bar{\mu}_\ell^{\text{nom}}) F_\ell \quad \forall \ell \in L \quad (\text{A.41})$$

A.8 Allocating Gross Injections with EBE

The allocation of gross generation to demands $d_{n,t}$ is straightforwardly obtained by a proportional distribution of the generation, *i.e.*

$$A_{s,n,t} = \frac{g_{s,t}}{\sum_s g_{s,t}} d_{n,t} \quad (\text{A.42})$$

A.9 Allocating Net Injections with EBE

Allocating net power injections using the EBE methods leads to the same result as the Marginal Participation (MP) [7] algorithm when allocating to consumers only, see [6] for further insight. We calculate it by setting

$$A_{m \rightarrow n,t} = \delta_{m,n} p_{m,t}^\circ + \gamma_t p_{n,t}^- p_{m,t}^+ \quad (\text{A.43})$$

where

- $p_{n,t}^+ = \min(g_{n,t} - d_{n,t}, 0)$ denotes the nodal net production
- $p_{n,t}^- = \min(d_{n,t} - g_{n,t}, 0)$ denotes the nodal net consumption
- $p_{n,t}^\circ = \min(p_{n,t}^+, p_{n,t}^-)$ the denotes nodal self-consumption. That is the power generated and at the same time consumed at node n and
- $\gamma_t = (\sum_n p_{n,t}^+)^{-1} = (\sum_n p_{n,t}^-)^{-1}$ is the inverse of the total injected/extracted power at time t .

The allocation $A_{s,n,t}$ from generator s to n , is given by multiplying $A_{m \rightarrow n,t}$ with the nodal share $g_{s,t}/g_{n,t}$.

A.10 Allocating Net Power using AP

Allocating net injections using the AP method is derived from [1]. In a lossless network the downstream and upstream formulations result in the same P2P allocation which is why we restrict ourselves to the downstream formulation only. In a first step we define a time-dependent auxiliary matrix \mathcal{J}_t which is the inverse of the $N \times N$ with directed power flow $m \rightarrow n$ at entry (m,n) for $m \neq n$ and the total flow passing node m at entry (m,m) at time step t . Mathematically this translates to

$$\mathcal{J}_t = (\text{diag}(p^+) + \mathcal{K}^- \text{diag}(f) K)^{-1}_t \quad (\text{A.44})$$

where \mathcal{K}^- is the negative part of the directed Incidence matrix $\mathcal{K}_{n,\ell} = \text{sign}(f_{\ell,t}) K_{n,\ell}$. Then the distributed slack for time step t is given by

$$A_{m \rightarrow n,t} = \mathcal{J}_{m,n,t} p_{m,t}^+ p_{n,t}^- \quad (\text{A.45})$$

A.11 Allocating Gross Power using AP

We use the same allocation as in Appendix A.10 but replace the net nodal production $p_{n,t}^+$ by the gross nodal production $g_{n,t}$ which leads to

$$\mathcal{J}_t = (\text{diag}(g) + \mathcal{K}^- \text{diag}(f) K)^{-1} \quad (\text{A.46})$$

The distributed slack is for time step t is then given by

$$A_{s \rightarrow m,t} = \mathcal{J}_{m,n} g_{s,t} d_{n,t} \quad (\text{A.47})$$

A.12 Example: Power Flow Allocations of different Types

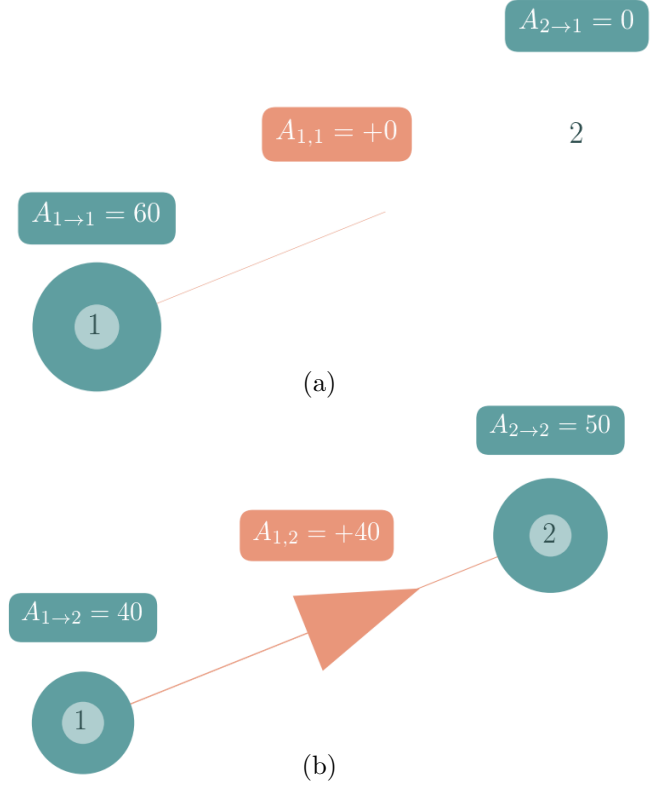


Figure A.1: Power allocations for bus 1 (a) and bus 2 (b) of the example network in Fig. 2 using equivalently allocated net power injections (scheme 2a). Bus 1 retrieves 60 MW from itself and nothing from bus 2. The latter in turn retrieves 40 MW from bus 1 and self supplies 50 MW. The P2P trades are less in number and more intuitive than with allocating gross flow.

References

- [1] Chira Achayuthakan et al. “Electricity Tracing in Systems With and Without Circulating Flows: Physical Insights and Mathematical Proofs”. en. In: *IEEE Transactions on Power Systems* 25.2 (May 2010), pp. 1078–1087. ISSN: 0885-8950, 1558-0679. DOI: [10.1109/TPWRS.2009.2037506](#).
- [2] J. Bialek. “Tracing the Flow of Electricity”. en. In: *IEE Proceedings - Generation, Transmission and Distribution* 143.4 (1996), p. 313. ISSN: 13502360. DOI: [10.1049/ip-gtd:19960461](#).
- [3] T. Brown and L. Reichenberg. “Decreasing Market Value of Variable Renewables Is a Result of Policy, Not Variability”. In: *arXiv:2002.05209 [econ, math, q-fin]* (Feb. 2020). arXiv: [2002.05209 \[econ, math, q-fin\]](#).
- [4] F.D. Galiana, A.J. Conejo, and H.A. Gil. “Transmission Network Cost Allocation Based on Equivalent Bilateral Exchanges”. en. In: *IEEE Transactions on Power Systems* 18.4 (Nov. 2003), pp. 1425–1431. ISSN: 0885-8950. DOI: [10.1109/TPWRS.2003.818689](#).
- [5] H.A. Gil, F.D. Galiana, and A.J. Conejo. “Multiarea Transmission Network Cost Allocation”. en. In: *IEEE Transactions on Power Systems* 20.3 (Aug. 2005), pp. 1293–1301. ISSN: 0885-8950. DOI: [10.1109/TPWRS.2005.851951](#).
- [6] Fabian Hofmann et al. “Flow Allocation in Meshed AC-DC Electricity Grids”. en. In: *Energies* 13.5 (Mar. 2020), p. 1233. ISSN: 1996-1073. DOI: [10.3390/en13051233](#).
- [7] H. Rudnick, R. Palma, and J.E. Fernandez. “Marginal Pricing and Supplement Cost Allocation in Transmission Open Access”. In: *IEEE Transactions on Power Systems* 10.2 (May 1995), pp. 1125–1132. ISSN: 08858950. DOI: [10.1109/59.387960](#).
- [8] Fred C. Schweppe et al. *Spot Pricing of Electricity*. en. Boston, MA: Springer US, 1988. ISBN: 978-1-4612-8950-0 978-1-4613-1683-1. DOI: [10.1007/978-1-4613-1683-1](#).