


# EEE 141 ELECTRICAL CIRCUITS

Dr. Shaikh Asif Mahmood  
Associate professor, BUET

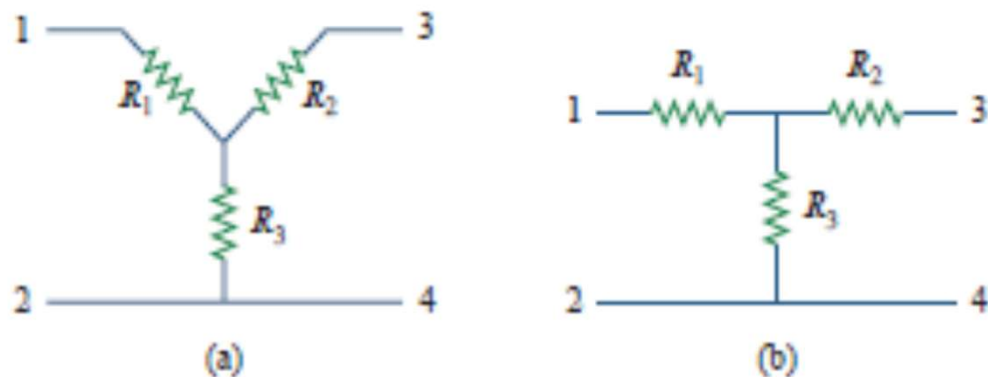
Adjunct Faculty, ECE, NSU



# BASIC LAWS

- Wye-Delta Transformations.
- Series-Parallel Networks.
- Ladder Network

## WYE-DELTA TRANSFORMATIONS



**Figure 2.47**

Two forms of the same network: (a) Y, (b) T.

$$R_{12}(Y) = R_1 + R_3$$

$$R_{12}(\Delta) = R_b \parallel (R_a + R_c)$$

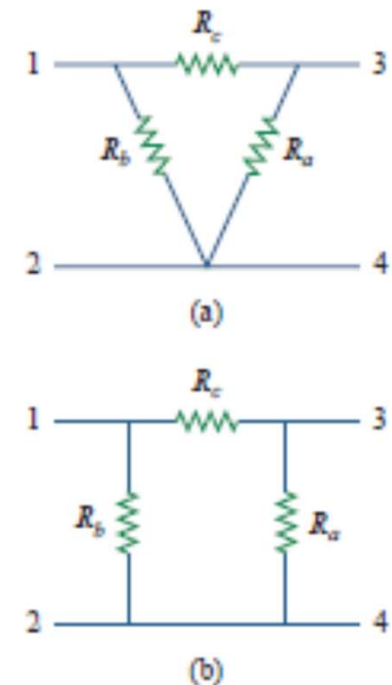
Setting  $R_{12}(Y) = R_{12}(\Delta)$  gives

$$R_{12} = R_1 + R_3 = \frac{R_b(R_a + R_c)}{R_a + R_b + R_c}$$

Similarly,

$$R_{13} = R_1 + R_2 = \frac{R_c(R_a + R_b)}{R_a + R_b + R_c}$$

$$R_{34} = R_2 + R_3 = \frac{R_a(R_b + R_c)}{R_a + R_b + R_c}$$



**Figure 2.48**

Two forms of the same network: (a)  $\Delta$ , (b)  $\Pi$ .

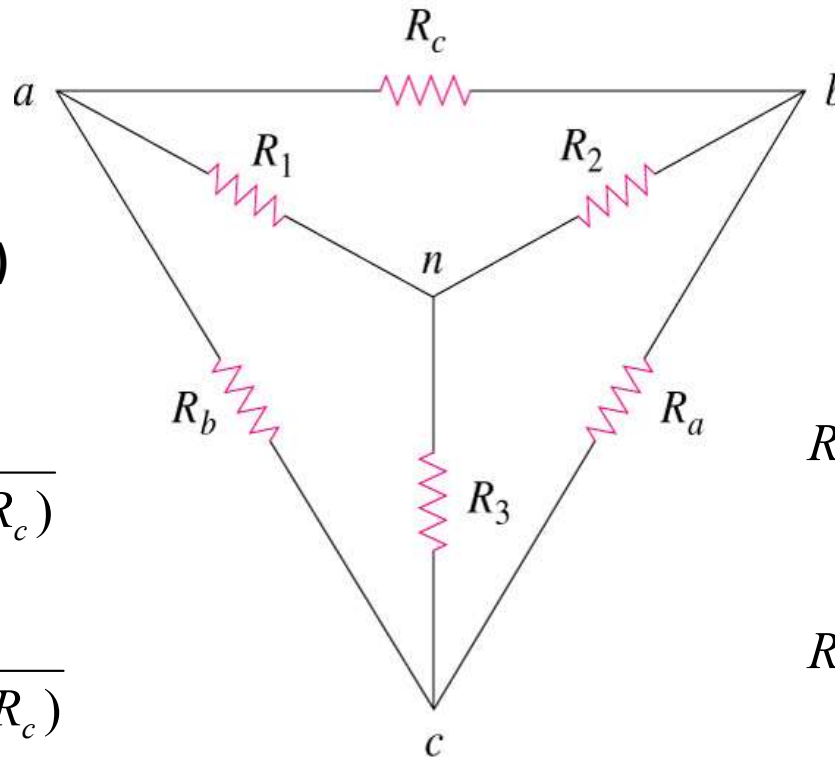
# WYE-DELTA TRANSFORMATIONS

**Delta -> Star (Wye)**

$$R_1 = \frac{R_b R_c}{(R_a + R_b + R_c)}$$

$$R_2 = \frac{R_c R_a}{(R_a + R_b + R_c)}$$

$$R_3 = \frac{R_a R_b}{(R_a + R_b + R_c)}$$



**Star (Wye) -> Delta**

$$R_a = \frac{R_1 R_2 + R_2 R_3 + R_3 R_1}{R_1}$$

$$R_b = \frac{R_1 R_2 + R_2 R_3 + R_3 R_1}{R_2}$$

$$R_c = \frac{R_1 R_2 + R_2 R_3 + R_3 R_1}{R_3}$$

# EXAMPLE

**EXAMPLE 8.29** Find the total resistance of the network of Fig. 8.80, where  $R_A = 3\ \Omega$ ,  $R_B = 3\ \Omega$ , and  $R_C = 6\ \Omega$ .

**Solution:**

Two resistors of the  $\Delta$  were equal; therefore, two resistors of the Y will be equal.

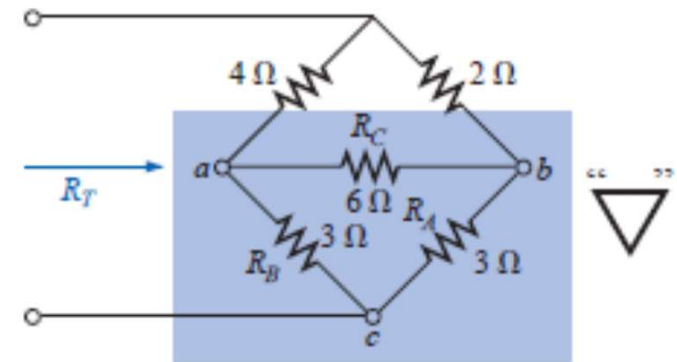
$$R_1 = \frac{R_B R_C}{R_A + R_B + R_C} = \frac{(3\ \Omega)(6\ \Omega)}{3\ \Omega + 3\ \Omega + 6\ \Omega} = \frac{18\ \Omega}{12} = 1.5\ \Omega$$

$$R_2 = \frac{R_A R_C}{R_A + R_B + R_C} = \frac{(3\ \Omega)(6\ \Omega)}{12\ \Omega} = \frac{18\ \Omega}{12} = 1.5\ \Omega$$

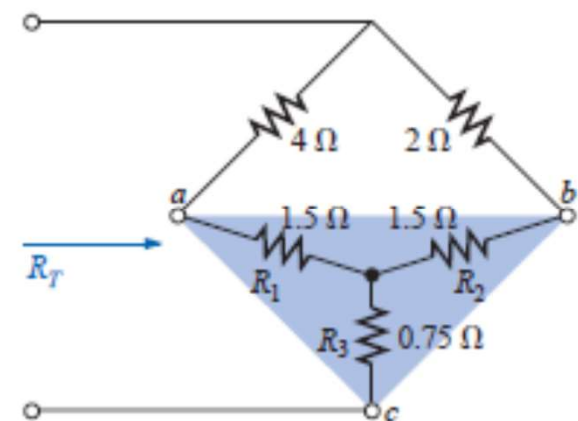
$$R_3 = \frac{R_A R_B}{R_A + R_B + R_C} = \frac{(3\ \Omega)(3\ \Omega)}{12\ \Omega} = \frac{9\ \Omega}{12} = 0.75\ \Omega$$

Replacing the  $\Delta$  by the Y, as shown in Fig. 8.81, yields

$$\begin{aligned} R_T &= 0.75\ \Omega + \frac{(4\ \Omega + 1.5\ \Omega)(2\ \Omega + 1.5\ \Omega)}{(4\ \Omega + 1.5\ \Omega) + (2\ \Omega + 1.5\ \Omega)} \\ &= 0.75\ \Omega + \frac{(5.5\ \Omega)(3.5\ \Omega)}{5.5\ \Omega + 3.5\ \Omega} \\ &= 0.75\ \Omega + 2.139\ \Omega \\ R_T &= 2.889\ \Omega \end{aligned}$$

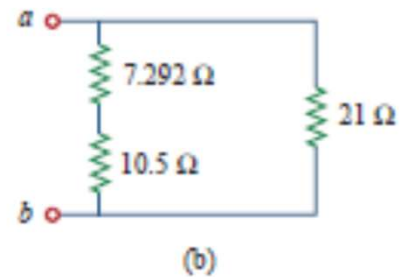
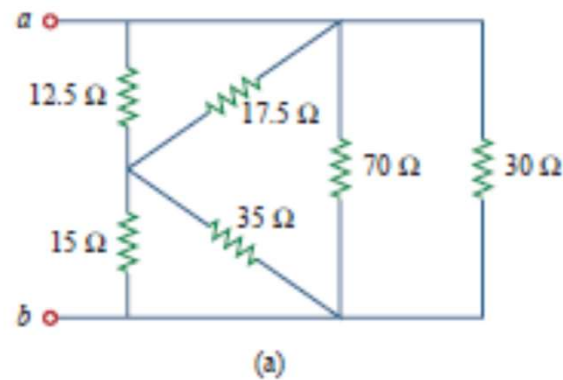
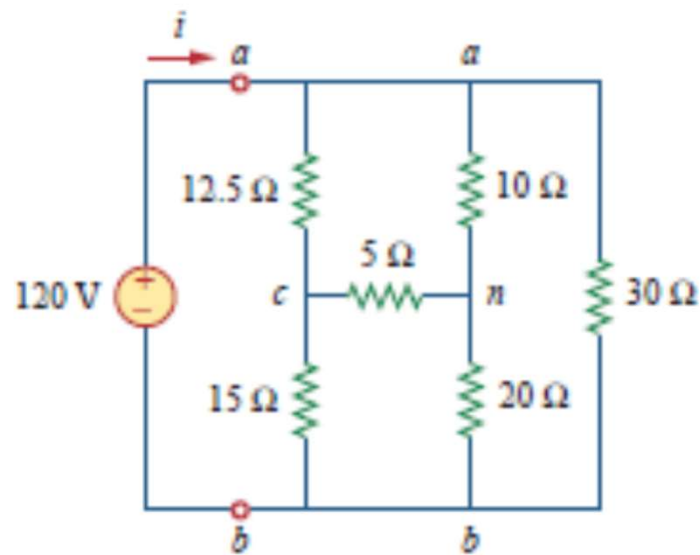


**FIG. 8.80**  
Example 8.29.



**FIG. 8.81**  
Substituting the Y equivalent for the bottom  $\Delta$  of Fig. 8.80.

# EXAMPLE

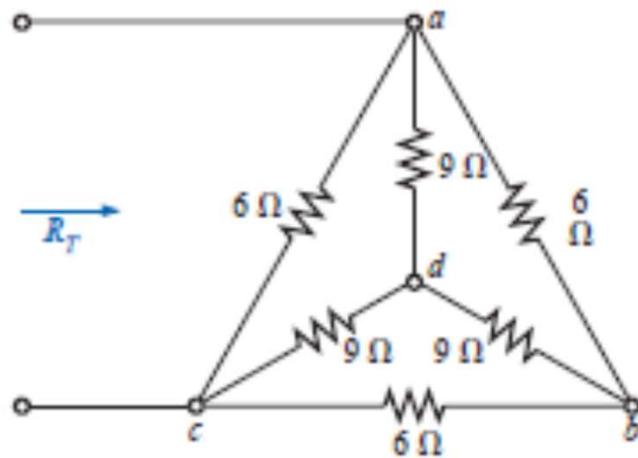


$$R_{ab} = (7.292 + 10.5) \parallel 21 = \frac{17.792 \times 21}{17.792 + 21} = 9.632 \, \Omega$$

Then

$$i = \frac{V_s}{R_{ab}} = \frac{120}{9.632} = 12.458 \, \text{A}$$

# EXAMPLE



$$R_Y = \frac{R_\Delta}{3} = \frac{6\ \Omega}{3} = 2\ \Omega \quad (\text{Fig. 8.83})$$

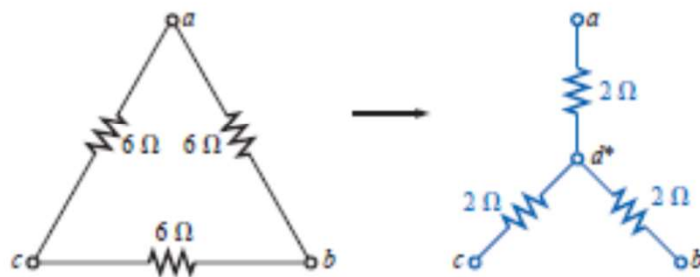
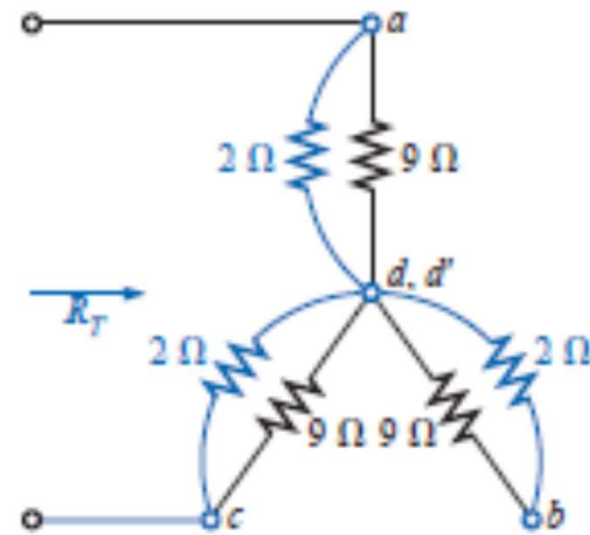


FIG. 8.83

Converting the  $\Delta$  configuration of Fig. 8.82 to a Y configuration.

The network then appears as shown in Fig. 8.84.

$$R_T = 2 \left[ \frac{(2\ \Omega)(9\ \Omega)}{2\ \Omega + 9\ \Omega} \right] = 3.2727\ \Omega$$



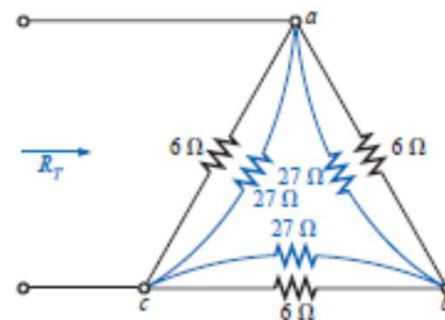
b. Converting the Y to a  $\Delta$ :

$$R_\Delta = 3R_Y = (3)(9\ \Omega) = 27\ \Omega \quad (\text{Fig. 8.85})$$

$$R'_T = \frac{(6\ \Omega)(27\ \Omega)}{6\ \Omega + 27\ \Omega} = \frac{162\ \Omega}{33} = 4.9091\ \Omega$$

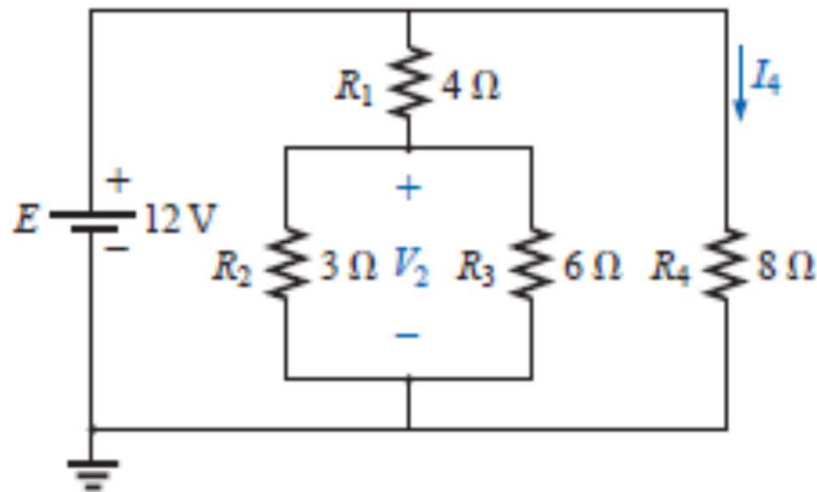
$$R_T = \frac{R'_T(R'_T + R'_T)}{R'_T + (R'_T + R'_T)} = \frac{R'_T 2R'_T}{3R'_T} = \frac{2R'_T}{3} \\ = \frac{2(4.9091\ \Omega)}{3} = 3.2727\ \Omega$$

which checks with the previous solution.



# SERIES-PARALLEL NETWORKS

Example



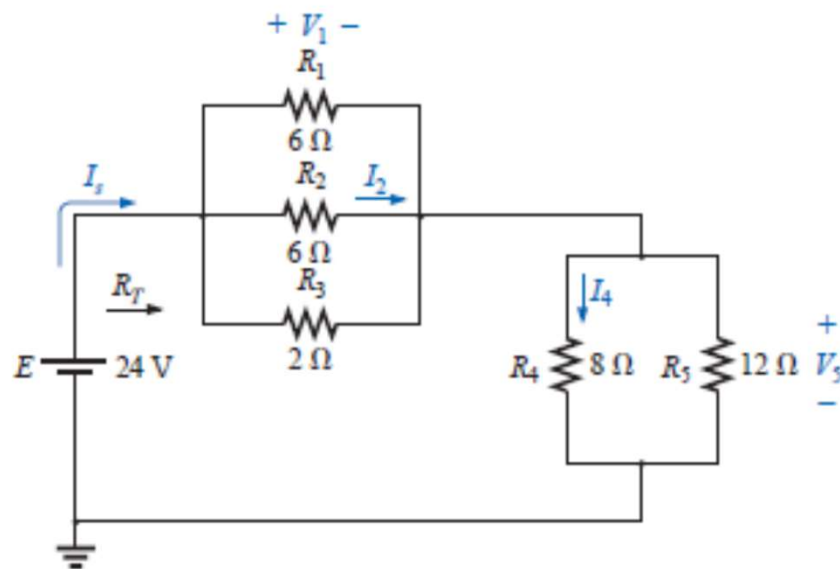
$$I_4 = \frac{E}{R_B} = \frac{E}{R_4} = \frac{12V}{8\Omega} = 1.5 A$$

$$R_D = R_2 // R_3 = 3\Omega // 6\Omega = 2\Omega$$

$$\begin{aligned} V_2 &= \frac{R_D E}{R_D + R_C} \\ &= \frac{(2\Omega)(12V)}{2\Omega + 4\Omega} = 4V \end{aligned}$$



# EXAMPLE



$$R_{1\parallel 2} = \frac{R}{N} = \frac{6\Omega}{2} = 3\Omega$$

$$R_A = R_{1\parallel 2\parallel 3} = \frac{(3\Omega)(2\Omega)}{3\Omega + 2\Omega} = \frac{6\Omega}{5} = 1.2\Omega$$

$$R_B = R_{4\parallel 5} = \frac{(8\Omega)(12\Omega)}{8\Omega + 12\Omega} = \frac{96\Omega}{20} = 4.8\Omega$$

The reduced form of Fig. 7.13 will then appear as shown in Fig. 7.15, and

$$R_T = R_{1\parallel 2\parallel 3} + R_{4\parallel 5} = 1.2\Omega + 4.8\Omega = 6\Omega$$

$$I_s = \frac{E}{R_T} = \frac{24\text{ V}}{6\Omega} = 4\text{ A}$$

with

$$V_1 = I_s R_{1\parallel 2\parallel 3} = (4\text{ A})(1.2\Omega) = 4.8\text{ V}$$

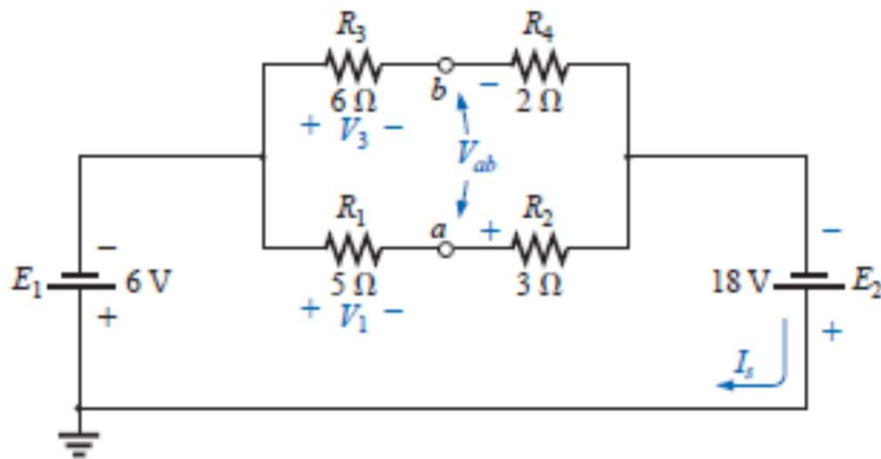
$$V_5 = I_s R_{4\parallel 5} = (4\text{ A})(4.8\Omega) = 19.2\text{ V}$$

Applying Ohm's law,

$$I_4 = \frac{V_5}{R_4} = \frac{19.2\text{ V}}{8\Omega} = 2.4\text{ A}$$

$$I_2 = \frac{V_2}{R_2} = \frac{V_1}{R_2} = \frac{4.8\text{ V}}{6\Omega} = 0.8\text{ A}$$

# EXAMPLE



$$V_1 = \frac{R_1 E}{R_1 + R_2} = \frac{(5 \Omega)(12 \text{ V})}{5 \Omega + 3 \Omega} = \frac{60 \text{ V}}{8} = 7.5 \text{ V}$$

$$V_3 = \frac{R_3 E}{R_3 + R_4} = \frac{(6 \Omega)(12 \text{ V})}{6 \Omega + 2 \Omega} = \frac{72 \text{ V}}{8} = 9 \text{ V}$$

The open-circuit voltage  $V_{ab}$  is determined by applying Kirchhoff's voltage law around the indicated loop of Fig. 7.17 in the clockwise direction starting at terminal  $a$ .

$$+V_1 - V_3 + V_{ab} = 0$$

and  $V_{ab} = V_3 - V_1 = 9 \text{ V} - 7.5 \text{ V} = 1.5 \text{ V}$

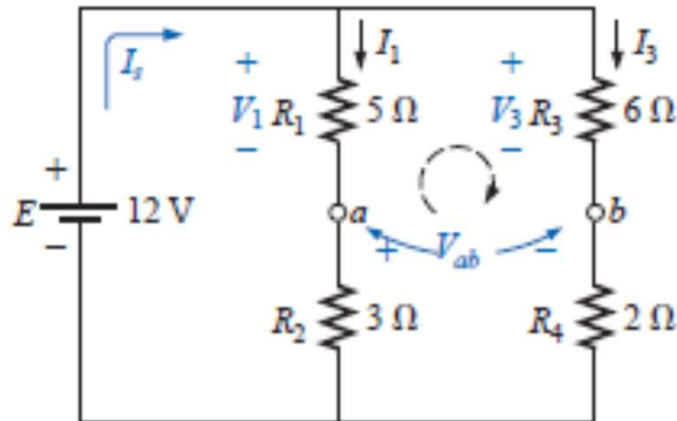
By Ohm's law,

$$I_1 = \frac{V_1}{R_1} = \frac{7.5 \text{ V}}{5 \Omega} = 1.5 \text{ A}$$

$$I_3 = \frac{V_3}{R_3} = \frac{9 \text{ V}}{6 \Omega} = 1.5 \text{ A}$$

Applying Kirchhoff's current law,

$$I_s = I_1 + I_3 = 1.5 \text{ A} + 1.5 \text{ A} = 3 \text{ A}$$



# EXAMPLE

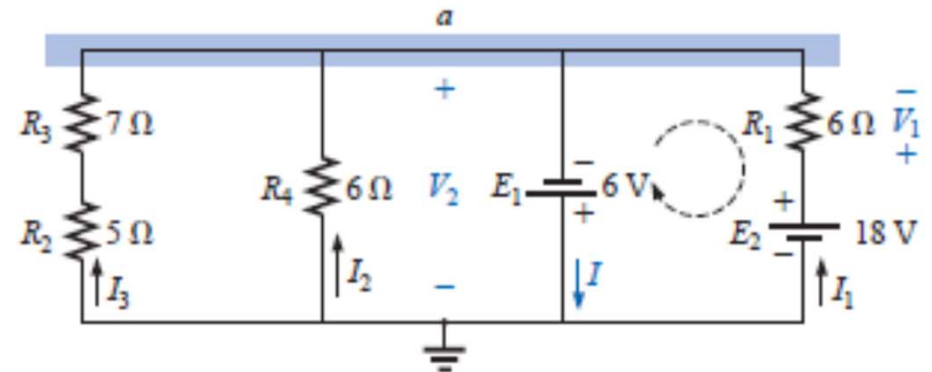
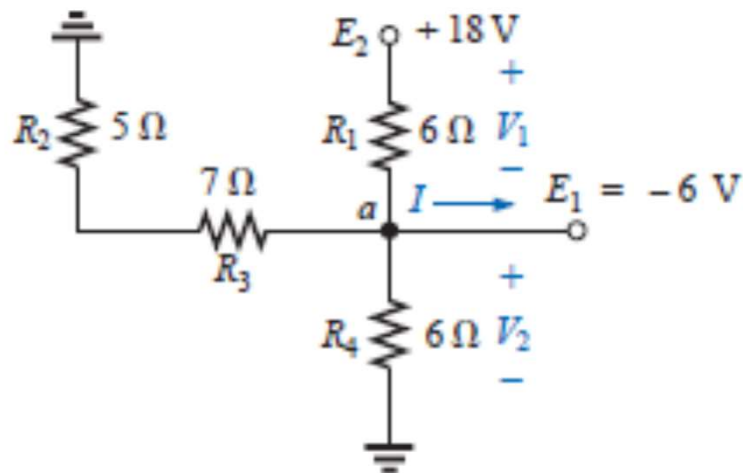


FIG. 7.19

Network of Fig. 7.18 redrawn.

and

$$V_1 = E_2 + E_1 = 18 \text{ V} + 6 \text{ V} = 24 \text{ V}$$

Applying Kirchhoff's current law to node  $a$  yields

$$\begin{aligned} I &= I_1 + I_2 + I_3 \\ &= \frac{V_1}{R_1} + \frac{E_1}{R_4} + \frac{E_1}{R_2 + R_3} \\ &= \frac{24 \text{ V}}{6 \Omega} + \frac{6 \text{ V}}{6 \Omega} + \frac{6 \text{ V}}{12 \Omega} \\ &= 4 \text{ A} + 1 \text{ A} + 0.5 \text{ A} \\ I &= 5.5 \text{ A} \end{aligned}$$

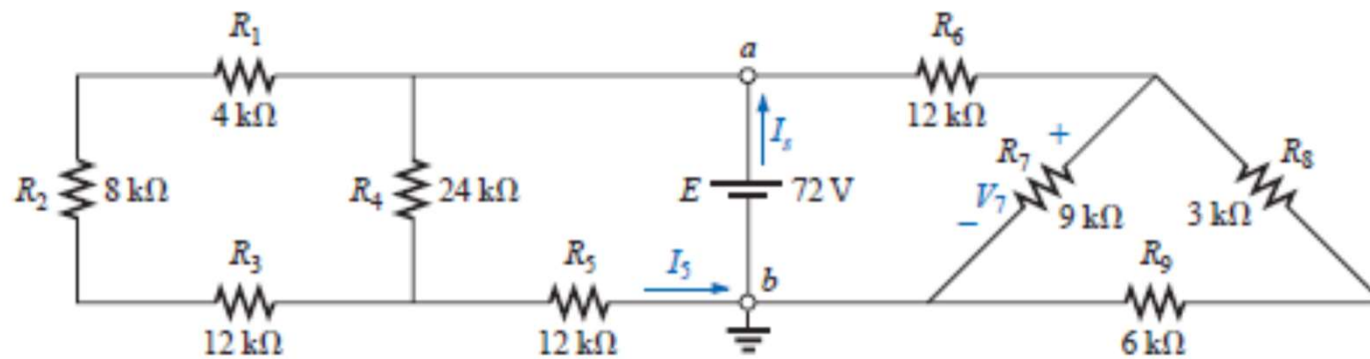
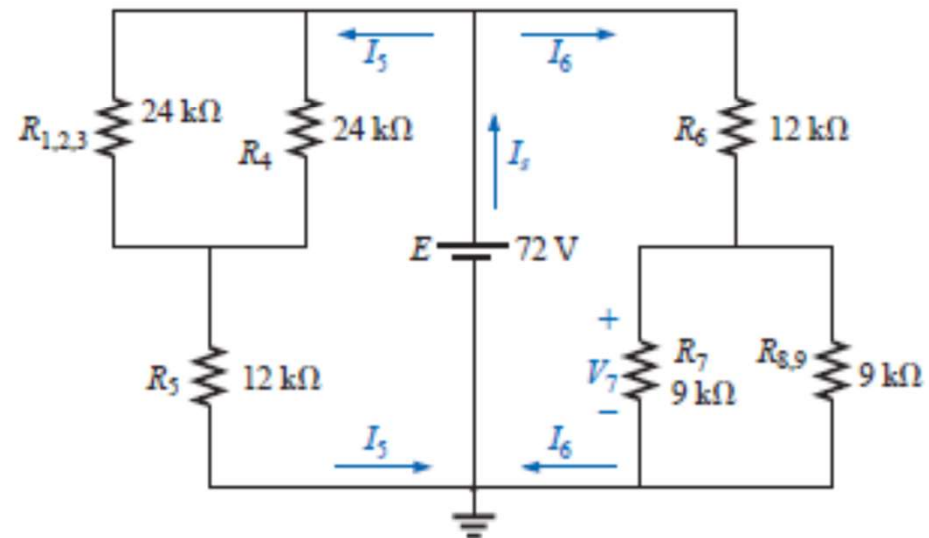


FIG. 7.22  
Example 7.9.

**Solution:** Redrawing the network after combining series elements yields Fig. 7.23, and



$$I_5 = \frac{E}{R_{(1,2,3)4} + R_5} = \frac{72 \text{ V}}{12 \text{ k}\Omega + 12 \text{ k}\Omega} = \frac{72 \text{ V}}{24 \text{ k}\Omega} = 3 \text{ mA}$$

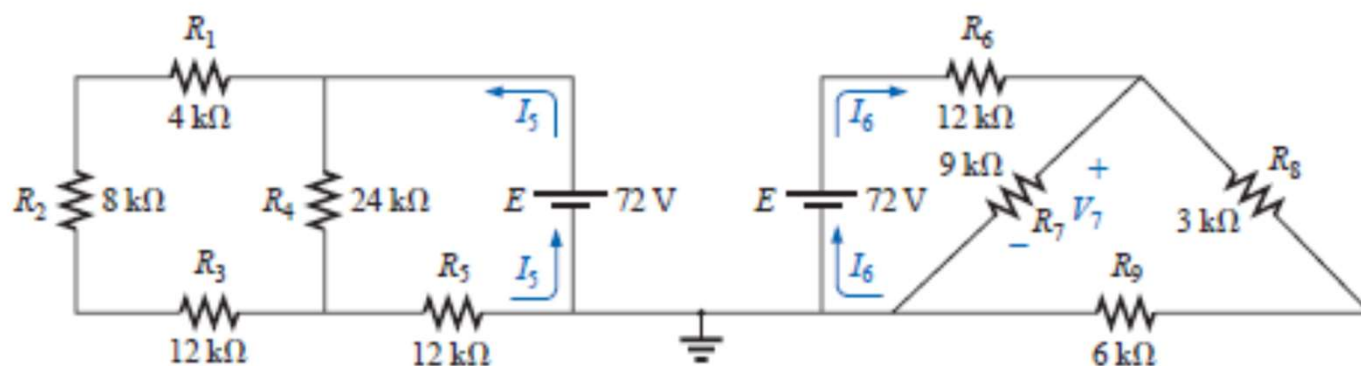
with

$$V_7 = \frac{R_{7(8,9)}E}{R_{7(8,9)} + R_6} = \frac{(4.5 \text{ k}\Omega)(72 \text{ V})}{4.5 \text{ k}\Omega + 12 \text{ k}\Omega} = \frac{324 \text{ V}}{16.5} = 19.6 \text{ V}$$

$$I_6 = \frac{V_7}{R_{7(8,9)}} = \frac{19.6 \text{ V}}{4.5 \text{ k}\Omega} = 4.35 \text{ mA}$$

and  $I_5 = I_5 + I_6 = 3 \text{ mA} + 4.35 \text{ mA} = 7.35 \text{ mA}$

Since the potential difference between points *a* and *b* of Fig. 7.22 is fixed at *E* volts, the circuit to the right or left is unaffected if the network is reconstructed as shown in Fig. 7.24.

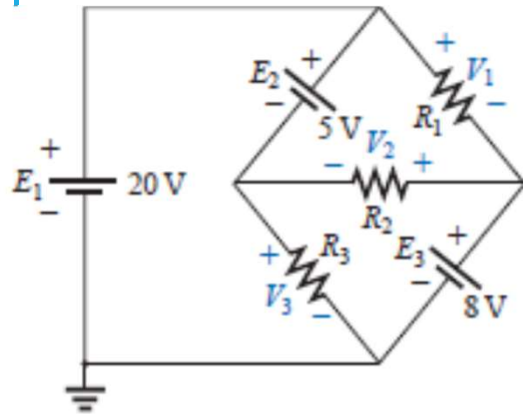


**FIG. 7.24**

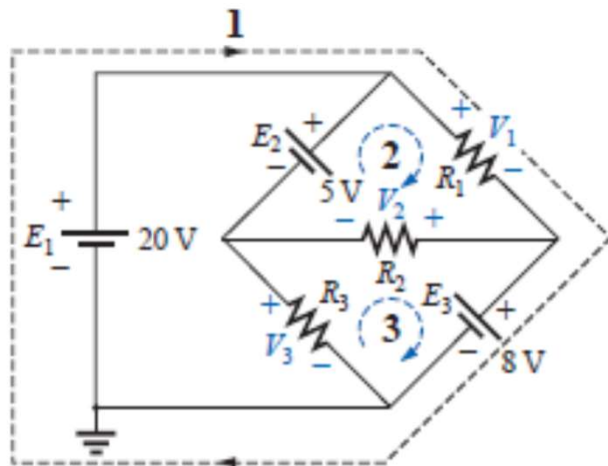
*An alternative approach to Example 7.9.*

We can find each quantity required, except  $I_5$ , by analyzing each circuit independently. To find  $I_5$ , we must find the source current for each

# EXAMPLE



**FIG. 7.25**  
Example 7.10.



**EXAMPLE 7.10** This example demonstrates the power of Kirchhoff's voltage law by determining the voltages  $V_1$ ,  $V_2$ , and  $V_3$  for the network of Fig. 7.25. For path 1 of Fig. 7.26,

$$E_1 - V_1 - E_3 = 0$$

and

$$V_1 = E_1 - E_3 = 20 \text{ V} - 8 \text{ V} = 12 \text{ V}$$

For path 2,

$$E_2 - V_1 - V_2 = 0$$

and

$$V_2 = E_2 - V_1 = 5 \text{ V} - 12 \text{ V} = -7 \text{ V}$$

indicating that  $V_2$  has a magnitude of 7 V but a polarity opposite to that appearing in Fig. 7.25. For path 3,

$$V_3 + V_2 - E_3 = 0$$

and

$$V_3 = E_3 - V_2 = 8 \text{ V} - (-7 \text{ V}) = 8 \text{ V} + 7 \text{ V} = 15 \text{ V}$$

Note that the polarity of  $V_2$  was maintained as originally assumed, requiring that  $-7 \text{ V}$  be substituted for  $V_2$ .



# EXAMPLE (LADDER NETWORK)

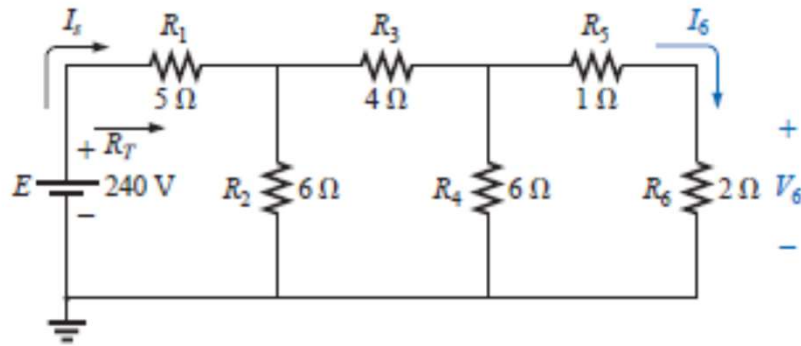


FIG. 7.27  
Ladder network.

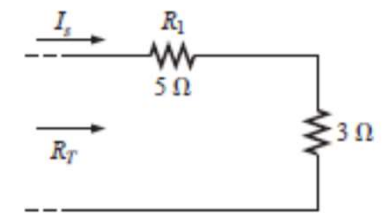
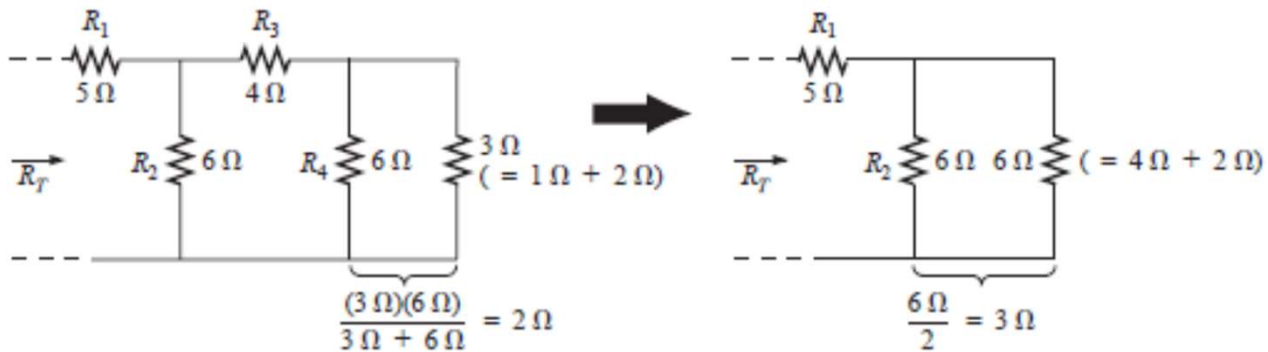


FIG. 7.29  
Calculating  $R_T$  and  $I_s$ .

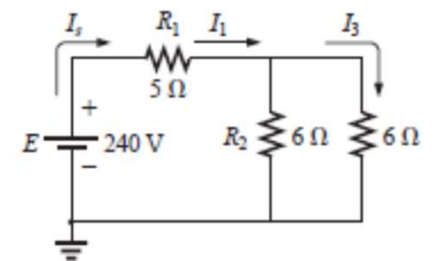


FIG. 7.30  
Working back toward  $I_6$ .

# EXAMPLE

$$R_T = 5 \, \Omega + 3 \, \Omega = 8 \, \Omega$$

$$I_s = \frac{E}{R_T} = \frac{240 \, \text{V}}{8 \, \Omega} = 30 \, \text{A}$$

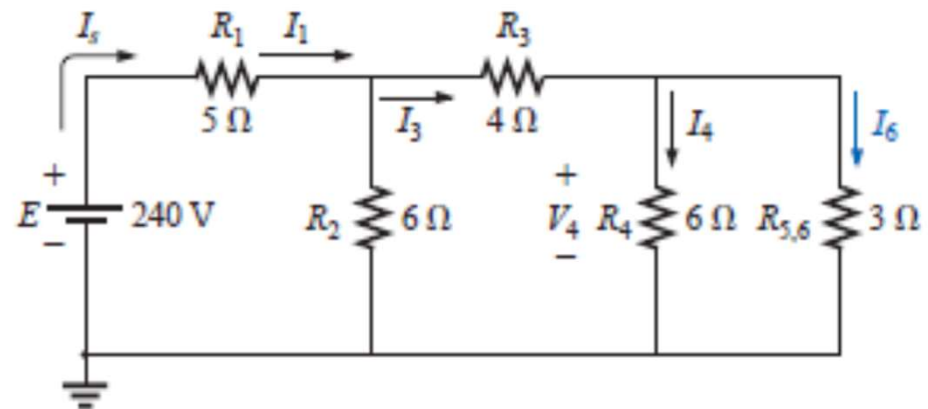
Working our way back to  $I_6$  (Fig. 7.30), we find that

$$I_1 = I_s$$

and

$$I_3 = \frac{I_s}{2} = \frac{30 \, \text{A}}{2} = 15 \, \text{A}$$

and, finally (Fig. 7.31),



$$I_6 = \frac{(6 \, \Omega)I_3}{6 \, \Omega + 3 \, \Omega} = \frac{6}{9}(15 \, \text{A}) = 10 \, \text{A}$$

$$V_6 = I_6 R_6 = (10 \, \text{A})(2 \, \Omega) = 20 \, \text{V}$$



# EXAMPLE

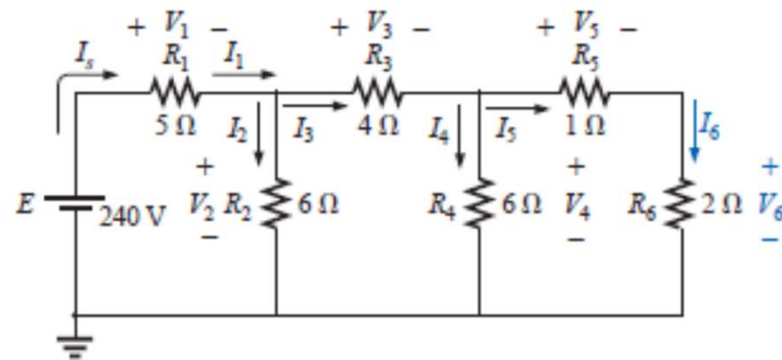


FIG. 7.32

*An alternative approach for ladder networks.*

The assigned notation for the current through the final branch is  $I_6$ :

$$I_6 = \frac{V_4}{R_5 + R_6} = \frac{V_4}{1\Omega + 2\Omega} = \frac{V_4}{3\Omega}$$

or 
$$V_4 = (3\Omega)I_6$$

so that 
$$I_4 = \frac{V_4}{R_4} = \frac{(3\Omega)I_6}{6\Omega} = 0.5I_6$$

and 
$$I_3 = I_4 + I_6 = 0.5I_6 + I_6 = 1.5I_6$$

$$V_3 = I_3 R_3 = (1.5I_6)(4\Omega) = (6\Omega)I_6$$

Also, 
$$V_2 = V_3 + V_4 = (6\Omega)I_6 + (3\Omega)I_6 = (9\Omega)I_6$$

so that 
$$I_2 = \frac{V_2}{R_2} = \frac{(9\Omega)I_6}{6\Omega} = 1.5I_6$$

and 
$$I_s = I_2 + I_3 = 1.5I_6 + 1.5I_6 = 3I_6$$

with 
$$V_1 = I_1 R_1 = I_s R_1 = (5\Omega)I_s$$

so that 
$$\begin{aligned} E = V_1 + V_2 &= (5\Omega)I_s + (9\Omega)I_6 \\ &= (5\Omega)(3I_6) + (9\Omega)I_6 = (24\Omega)I_6 \end{aligned}$$

and 
$$I_6 = \frac{E}{24\Omega} = \frac{240\text{ V}}{24\Omega} = 10\text{ A}$$

with 
$$V_6 = I_6 R_6 = (10\text{ A})(2\Omega) = 20\text{ V}$$