# Department of Computer Science and Engineering (CSE) BRAC University

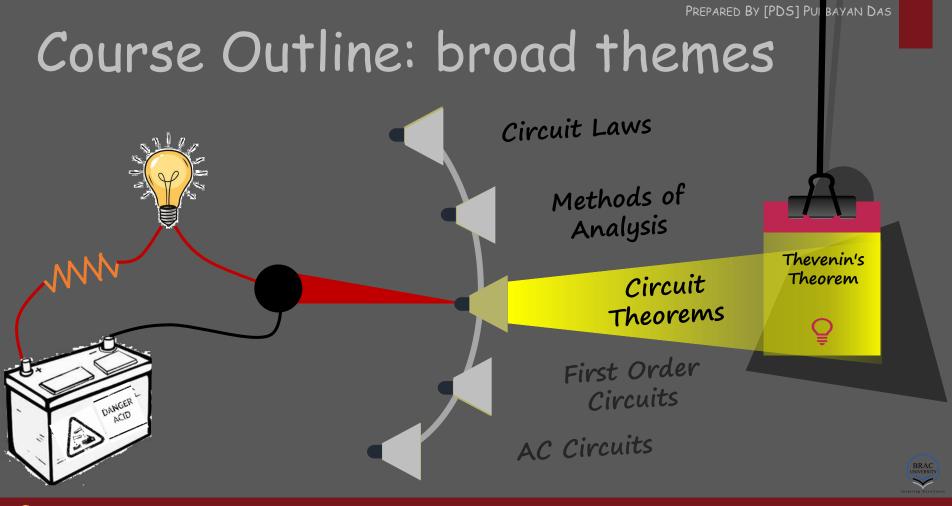
#### Lecture 9

CSE250 - Circuits and Electronics

#### THEVENIN'S AND NORTON'S THEOREM



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#### Thevenin's Theorem

• Thevenin's Theorem states that a linear two-terminal circuit can be replaced by an equivalent circuit consisting of a voltage source  $V_{Th}$  in series with a resistor  $R_{Th}$ , where  $V_{Th}$  is the open-circuit voltage at the terminals and  $R_{Th}$  is the input or equivalent resistance at the terminals when the independent sources are turned off.



Original Circuit The Thevenin equivalent circuit

• Two circuits are said to be equivalent if they have the same I-V characteristics at their terminals.



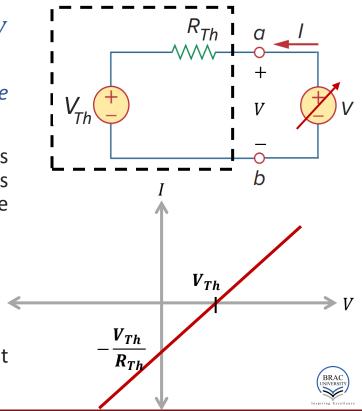
## I-V of Thevenin Equivalent

- We recall that an equivalent circuit is one whose I-V characteristics are identical with the original circuit.
- Let's first find out the I-V characteristics of the reduced circuit with respect to terminals a-b.
- The configuration is a voltage source  $(V_{Th})$  in series with a resistor  $(R_{Th})$ . To determine the configuration's I-V characteristics, if applying a voltage V gives rise to a current I, we can write using KVL,

$$V = V_{Th} + IR_{Th}$$

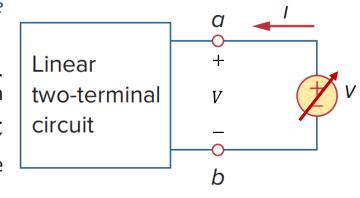
$$\Rightarrow I = \frac{1}{R_{Th}}V - \frac{V_{Th}}{R_{Th}}$$

• The equation results in a linear I vs V plot that intersects the axes at  $V_{Th}$  and  $-\frac{V_{Th}}{R_{TH}}$ .



#### I-V of Actual Circuit

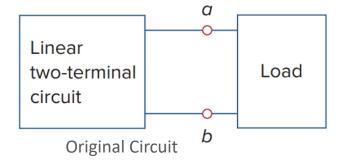
- Let's now find out the I-V characteristics of the original circuit with respect to terminals a-b.
- The circuit is a combination of linear circuit elements. We cannot theoretically derive exactly the relation between I and V unless we know the actual circuitry. However, as the circuit is linear, the I-V characteristic will be a straight line and the line can be drawn if minimum two points on the line are known.

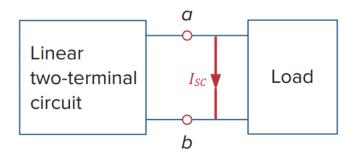


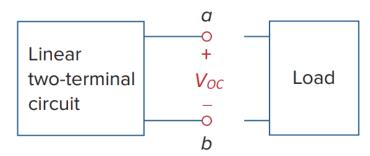
- The two points we can get are the intersecting points of x and y axis.
- To get the intersecting location on the voltage axis, current (I) at the terminals should be made equal to 0. That is, the terminals a-b must be open circuited.
- Similarly, for the intersecting location on current axis,  $V_{ab}=V=0$ . That is, the terminals a-b must be shorted.

#### OC Voltage & SC Current

• Let's denote  $V_{oc}$  be the voltage at the open terminals upon disconnecting the load and  $I_{sc}$  be the current through the shorted terminals upon short circuiting the load.





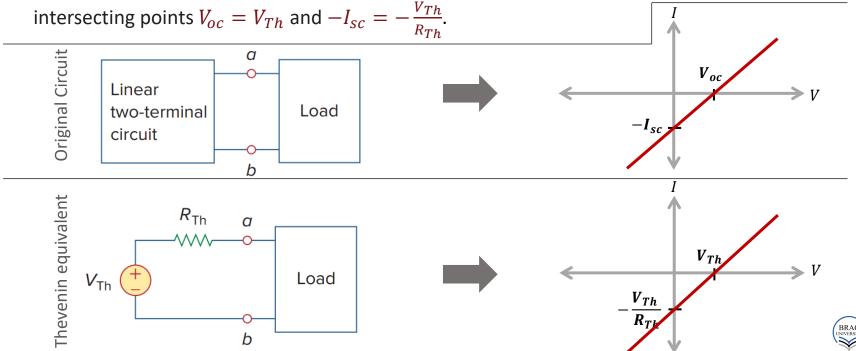


Open Circuited at the terminals

So, the I-V characteristic should be the straight line passing through the points  $(V_{oc}, 0)$  and  $(0, -I_{sc})$ . The reason for the negative sign is that  $I_{sc}$  is opposite to the current (I) plotted along the y-axis.

## Condition for Equivalence

• The original circuit and the reduced Thevenin equivalent circuit will be equivalent to each other if the I-V characteristics of the two are identical. They will indeed be identical if the



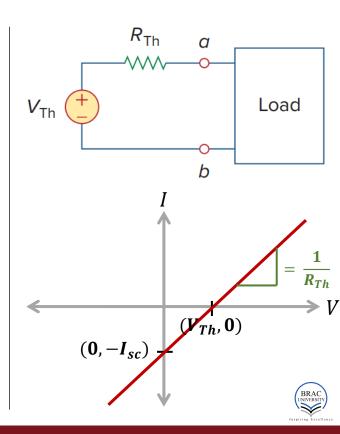
## How to determine R<sub>Th</sub>?

 We have seen in the previous slides that, Thevenin's conversion is valid if

i. 
$$V_{oc} = V_{Th}$$
 and

ii. 
$$-I_{SC} = -\frac{V_{Th}}{R_{Th}}$$
 or  $I_{SC} = \frac{V_{Th}}{R_{Th}}$ 

- For the linear I-V characteristic,  $R_{Th}$  is the inverse of the slope of the straight line passing through the points  $(V_{Th}, 0)$  and  $(0, -I_{sc})$ . That is,
- $Slope = \frac{\Delta I}{\Delta V} = \frac{1}{R_{Th}} = \frac{0 (-I_{SC})}{V_{Th} 0}$
- $\Rightarrow$   $R_{Th} = \frac{V_{Th}}{I_{SC}}$
- Thus,  $R_{Th}$  may be found from this ohmic relation between  $V_{Th}$  and  $I_{sc}$ .



# Special Case: undefined R<sub>Th</sub>

- **Special Case**  $(V_{Th} = 0)$ : If  $V_{Th}$  is zero,  $I_{SC} = \frac{V_{Th}}{R_{Th}}$  is likewise zero, and the circuit becomes resistive with respect to the terminals where Thevenin conversion is taking place. In this situation, the I V characteristic line, as shown, passes through the origin.
- This can happen in two scenarios:

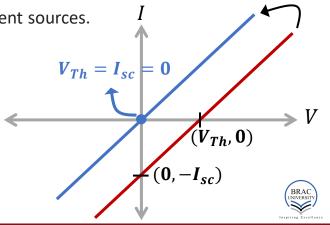
[See Example] i. if the network is erroneous in such a way that the load connected to the circuit gets no voltage and

[See Example] ii. if the portion of the network excluding load has no independent sources.

• This results in an undefined and indeterminant situation if we proceed to determine  $R_{Th}$ .

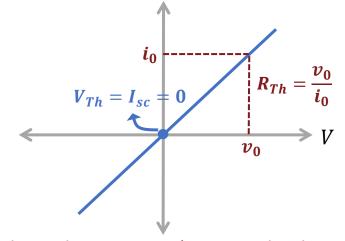
$$R_{Th} = \frac{V_{Th}}{I_{SC}} = \frac{0}{0}$$

• Let's think of a different approach to tackle this situation to determine  $R_{Th}$ .



## Universal Rule to determine R<sub>Th</sub>

- As  $V_{Th}=0$  results in a resistive I-V passing through the origin  $(V_{Th},\ 0)=(0,\ -I_{Sc})=(0,0)$ , we may still find the value of  $R_{Th}$  by measuring the slope of the line with any other arbitrary point  $(v_0,i_0)$  on the line.
- Interestingly, we can use this technique to determine  $R_{Th}$  whether or not  $V_{Th}$  is zero. This is what the term "Universal Rule" refers to.
- So, in general (whether or not  $V_{Th}$  is zero), the strategy is to forcefully make the I-V characteristic line to go through the origin. Then calculating  $R_{Th}$  as  $R_{Th} = \frac{v_0}{i_0}$ .



• This can be accomplished simply by turning off all the independent sources (or equivalently replacing them with their resistances). As a result, the circuit becomes resistive, and the characteristic line will pass through the origin.

## Universal Rule w/wo dependent source

- No dependent source: If a network has no dependent sources, then after turning off all the independent sources, the circuit will be a combination of resistors only. This simplifies the procedure as that, to determine  $R_{Th}$ , it is not even required to apply a voltage  $v_0$  (or current  $i_0$ ) and determine the corresponding current  $i_0$  (or voltage  $v_0$ ). Instead, use the series and/or parallel combinations of resistors to determine the equivalent resistance at the terminals, which is  $R_{Th}$ .
- **Dependent source:** However, if the network has dependent sources, then to get any point  $(v_0, i_0)$  on the line, apply a voltage source  $v_0$  at load terminals and determine the resulting current  $i_0$ . Then  $R_{Th} = v_0/i_0$ . Alternatively, insert a current source  $i_0$  at load terminals and find the terminal voltage  $v_0$ . Again  $R_{Th} = v_0/i_0$ . We call the applied source as dummy or test source. In either approach, we may assume any value of  $v_0$  or  $i_0$ .

 $v_{Th} = I_{sc} = 0$   $v_0$   $R_{Th} = \frac{v_0}{i_0}$  V

Note that, for an applied dummy or test source, polarity of  $v_0$  and direction of  $i_0$  must be such that, the current  $i_0$  leaves the +ve terminal of  $v_0$ .

#### Methods in a nutshell

Method to determine  $V_{Th}$ 

Disconnect the load (if any)

Determine the open circuit voltage

at the load terminals  $(V_{OC} = V_{Th})$ 

Methods to determine  $R_{Th}$ 

RBAYAN DAS

Is there

anv dependent

source(s)?

resistors to calculate

No

series-parallel

**Universal Rule** 

Kill all the Short the load terminals independent sources

Yes

Determine the current through the short circuit  $(I_{SC})$ 

Valid only if  $V_{Th} \neq 0$ 

 $R_{Th} = \frac{V_{Th}}{I_{SC}}$ 

or current source to the load terminals

Use Ohm's Calculate Law to calculate  $R_{Th} = \frac{v_0}{c}$ 

the current  $(i_0)$  supplied or voltage  $(v_0)$  across the voltage or current source respectively.

Add a dummy voltage

Use

combinations

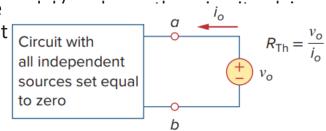
 $R_{ea} = R_{Th}$ 

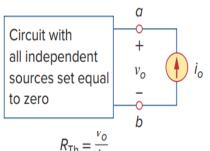
# Procedure to find parameters

•  $\blacksquare$  Finding  $V_{oc}=V_{Th}$ : Disconnect the load and use nodal/mesh or other circuit solving techniques

to find the open circuit voltage at the load terminals.

- **Finding**  $I_{sc}$ : Disconnect the load, short the terminals, use techniques to find the short circuit current at t
- $\blacksquare$  Finding  $R_{Th}$ 
  - Case 1: If  $V_{Th} \neq 0$ , Use  $R_{Th} = \frac{V_{Th}}{I_{SC}}$



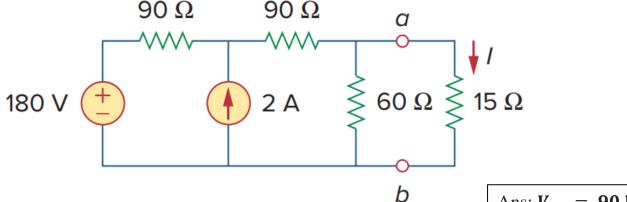


If  $V_{Th} = 0$ , turn off all the independent sources.

- If the network has no dependent sources,  $R_{Th}$  is the input resistance of the network looking between the load terminals.
- If the network has dependent sources, apply a voltage source  $v_0$  at load terminals determine the resulting current  $i_0$ . Then  $R_{Th} = v_0$

# Example 1

Using Thevenin's theorem, find the equivalent circuit to the left of the terminals in the circuit. Then find *I*.

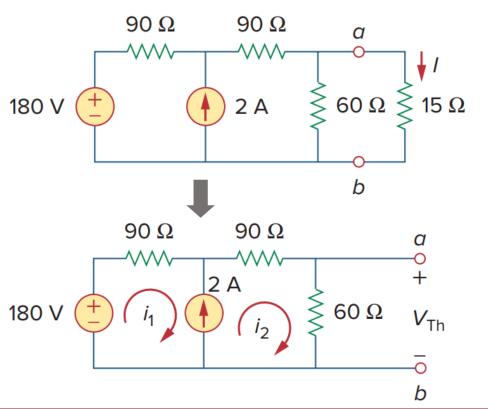


<u>Ans</u>:  $V_{Th} = 90 V$ ;  $R_{Th} = 45 \Omega$ ;  $i_x = 1.5 A$ 



<sup>\*</sup> See solution in the next slide if necessary

# Example 1: finding V<sub>Th</sub>



Step 1: Disconnecting the load and finding the open circuit voltage.

Let's use mesh analysis to find the  $V_{Th}$ 

KVL at mesh 1 and mesh 2 (forming supermesh),

$$-180 + 90i_1 + 90i_2 + 60i_2 = 0$$

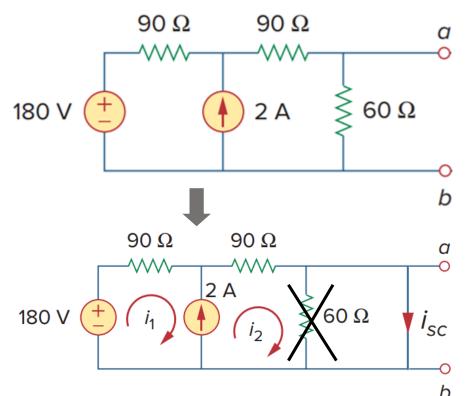
$$\Rightarrow 90i_1 + 150i_2 = 180 ------(i)$$

KCL at the supermesh,  $i_1 - i_2 = -2$  --- -(ii)

Solving ... ..., 
$$i_1 = -0.5 A$$
;  $i_2 = 1.5 A$ 

So, 
$$V_{Th} = 60i_2 = 60 \times 1.5 = 90 V$$

# Example 1: finding R<sub>Th</sub>



<u>Step 2</u>: As  $V_{Th} \neq 0$ , with the load disconnected, we find the short circuit current  $I_{sc}$ . The terminals a-b are shorted.

Let's use mesh analysis to find the  $I_{sc.}$  Note that the 60  $\Omega$  resistance is shorted out.

KVL at mesh 1 and mesh 2 (forming supermesh),  $-180 + 90i_1 + 90i_2 = 0$ 

$$\Rightarrow i_1 + i_2 = 2 -----(i)$$

KCL at the supermesh,

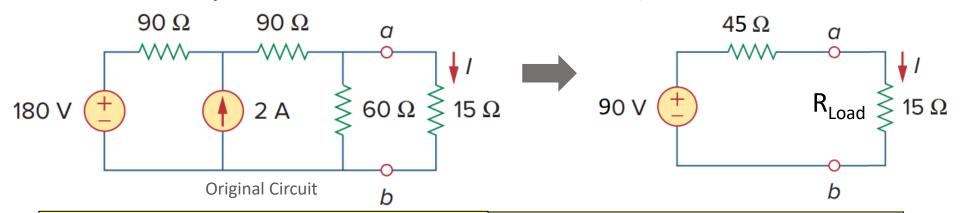
$$i_1 - i_2 = -2$$
 ----(ii)

Solving ... ..., 
$$i_1 = 0 A$$
;  $i_2 = 2 A$ 

So, 
$$I_{sc} = i_2 = 2 A$$

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## Example 1: Thevenin equivalent



Step 3: With  $V_{Th}$  and  $I_{sc}$  known, we can find  $R_{Th}$  as follows,

$$R_{Th} = \frac{V_{Th}}{I_{SC}} = \frac{90}{2} = 45 \ \Omega$$

So, the Thevenin equivalent circuit looks like the one shown above.

The load current *I* can be found as follows,

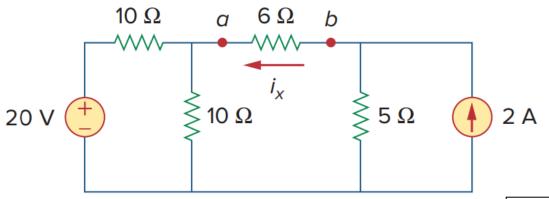
$$I = \frac{90}{45 + 15} = 1.5 A$$

[Calculate I from the original circuit and verify the Thevenin's theorem]

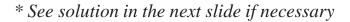


# Example 2

Find the Thevenin equivalent looking into terminals a-b of the circuit and solve for  $i_{\gamma}$ .



$$\mathbf{A} \mathbf{0} = \mathbf{i} \mathbf{i} \mathbf{0} \mathbf{0} \mathbf{1} = \mathbf{A} \mathbf{A} \mathbf{i} \mathbf{0} \mathbf{0} = \mathbf{A} \mathbf{A} \mathbf{i} \mathbf{0}$$





# Example 2: finding V<sub>Th</sub>

Step 1: Disconnecting the load and finding the open circuit voltage.

No current flows through the open circuit. So, the voltage across the 10  $\Omega$  resistance can be found by voltage division, that is,

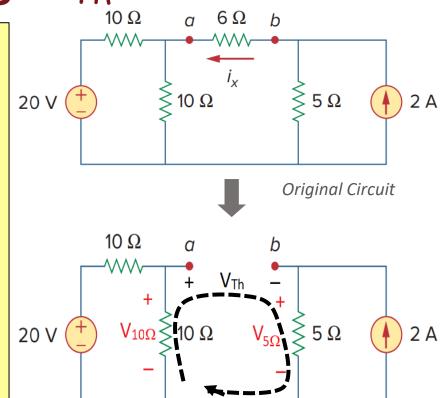
$$V_{10\Omega} = \frac{10}{10 + 10} \times 20 = 10 \, V.$$

The current 2 A flows through the 5  $\Omega$  resistor.

$$V_{5\Omega} = 5 \times 2 = 10 V$$

The voltages are indicated in the figure.  $V_{Th}$  can be found by applying KVL along the black dashed line shown. That is,

$$-10 + V_{Th} + 10 = 0$$
$$\Rightarrow V_{Th} = 0 V$$



## Example 2: finding R<sub>Th</sub>

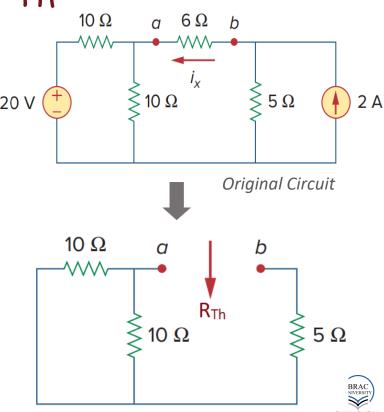
Step 2: As  $V_{Th} = 0$ ,  $I_{sc}$  will also be zero, hence,  $R_{Th} = \frac{V_{Th}}{I_{Th}}$  will result in a  $\frac{0}{0}$  situation. In this case we find  $R_{Th}$  by killing all the independent sources 20 V [Replace voltage sources by short circuits and current sources by open circuits].

Now check if there are dependent sources in the reduced circuit. As there is none, we simply use series-parallel combination to find the equivalent resistance seen from the load terminal. That is,

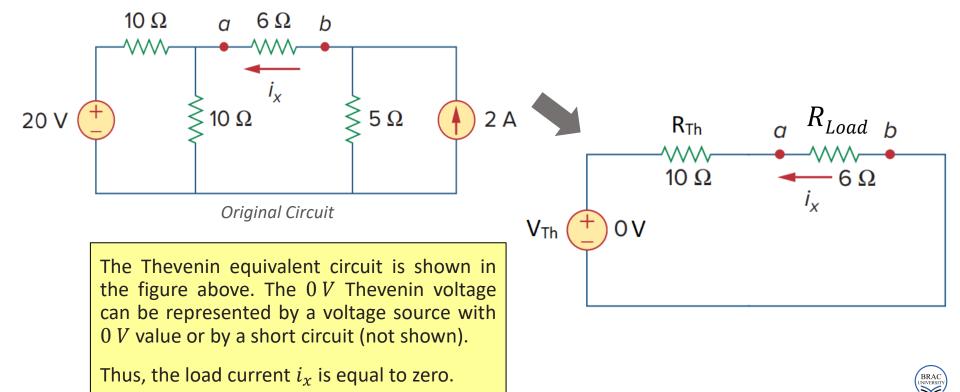
$$R_{Th} = (10 \mid \mid 10) + 5$$

$$\Rightarrow R_{Th} = 10 \Omega$$

[Keep in mind that, this method of determining  $R_{Th}$ by killing independent sources always works regardless of whether  $V_{Th}$  is equal to zero or not.]

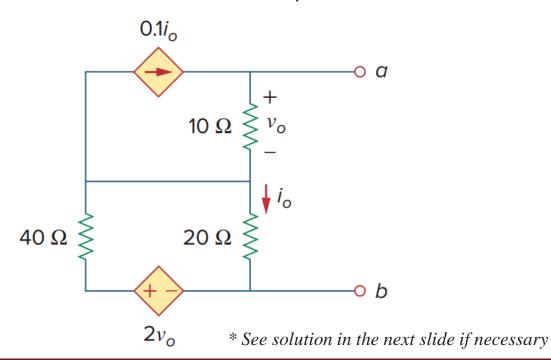


## Example 2: Thevenin equivalent



## Example 3

Obtain the Thevenin equivalent circuit at terminals a-b.





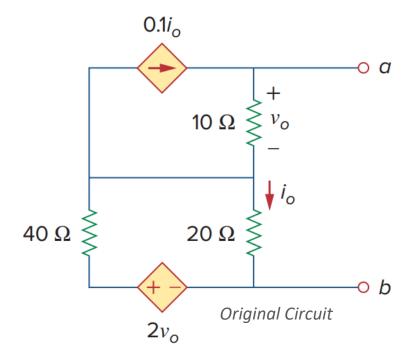
## Example 2: finding V<sub>Th</sub>

<u>Step 1</u>: Disconnecting the load and finding the open circuit voltage.

There are two dependent sources but no independent sources in this circuit. This means that all currents and voltages, including those on which dependent sources rely, will be zero. That is,  $i_0=0, v_0=0$ . As a result, there will be no contributions from the dependent sources. So, we can write,

$$V_{Th} = V_{ah} = 0 V.$$

[Circuit analysis can be used to confirm that  $V_{Th}=0$ ]



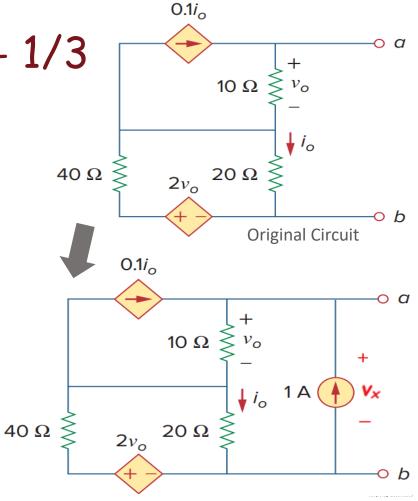


## Example 3: finding $R_{Th}$ - 1/3

Step 2: As  $V_{Th}=0$ ,  $I_{SC}$  will also be zero, hence,  $R_{Th}=\frac{V_{Th}}{I_{SC}}$  will result in a  $\frac{0}{0}$  situation. In this case we find  $R_{Th}$  by killing all the independent sources.

There are no independent sources in this circuit.

There are two dependent sources. So, we must add a dummy voltage/current source between terminals a-b. Let's add a current source of 1 A between the terminals a-b. We have to find the voltage  $v_{\chi}$  across the current source as shown in the circuit diagram.



# Example 3: finding R<sub>Th</sub> - 2/3

Let's apply mesh analysis to solve for  $v_0$ .

It can be seen from loop 3 that,

$$i_3 = -1 A$$

Also from loop 1,

$$i_1 = 0.1i_0 = 0.1(i_2 - i_3)$$
  $[i_0 = i_2 - i_3]$   
 $\Rightarrow i_1 - 0.1i_2 + 0.1i_3 = 0$ 

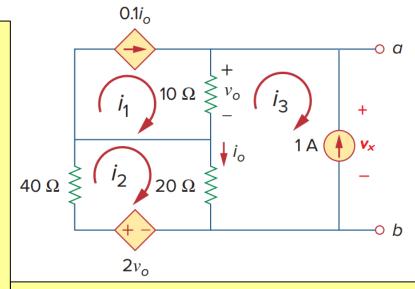
$$\Rightarrow i_1 - 0.1i_2 = 0.1 - - -(i) [i_3 = -1 A]$$

KVL at loop 2,

$$40i_2 + 20(i_2 - i_3) - 2v_0 = 0$$

$$\Rightarrow 40i_2 + 20(i_2 - i_3) - 2 \times 10(i_1 - i_3) = 0$$

$$\Rightarrow 20i_1 - 60i_2 = 0 -------(ii)$$



Solving (i) and (ii) yields,

$$i_1 = 0.103 A,$$
  
 $i_2 = 0.034 A.$ 

Let's find  $v_0$  now!

## Example 3: finding R<sub>Th</sub> - 3/3

#### Now,

$$v_0 = 10 \times (i_1 - i_3)$$
  
 $\Rightarrow v_0 = 10 \times \{0.103 - (-1)\} = 11.03 V$   
 $i_0 = i_2 - i_3$   
 $\Rightarrow i_0 = 0.034 - (-1) = 1.034 A$ 

The voltage across the  $20\,\Omega$  is  $=20i_0=20.68\,V$ .

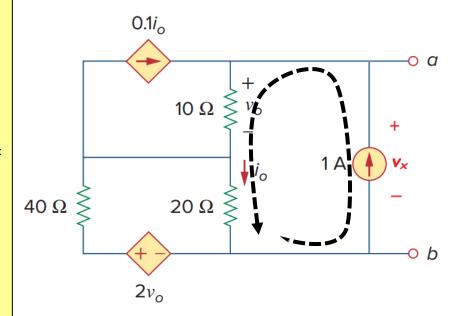
Applying KVL along the black dotted line,

$$-v_x + v_0 + 20.68 = 0$$

$$\Rightarrow v_x = 31.71 V \quad [v_0 = 11.03 V]$$

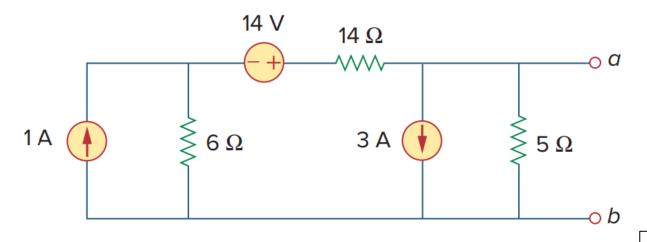
So,

$$R_{Th} = \frac{v_x}{1} = 31.71 \,\Omega$$





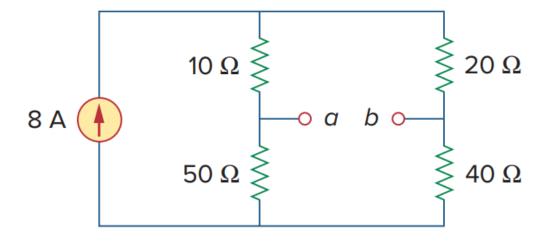
Find the Thevenin equivalent at terminals a-b.



$$\triangle \Lambda_{Ih} = -8 V; R_{Ih} = \Lambda \Omega$$



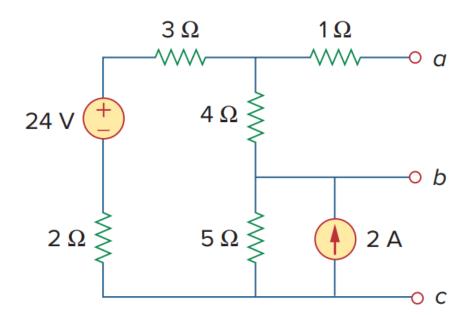
Find the Thevenin equivalent at terminals a - b.



$$\Omega \mathbf{Z} \cdot \mathbf{Z} \mathbf{Z} = \mathbf{A} \mathbf{D} \mathbf{V}; \mathbf{R}_{Th} = \mathbf{Z} \mathbf{Z} \cdot \mathbf{Z} \mathbf{D}$$



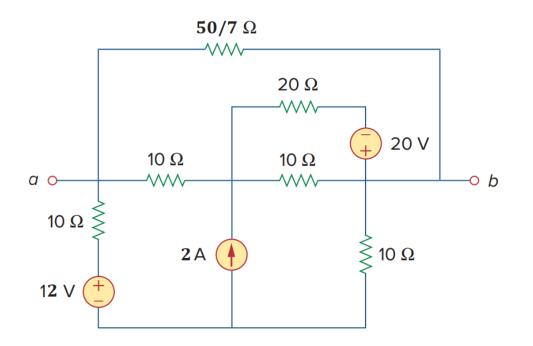
Find the Thevenin equivalent as seen from terminals (i) a - b and (ii) b - c.



<u>Ans</u>: (i)  $V_{Th} = 4 V$ ;  $R_{Th} = 3.857 \Omega$ ;  $(ii) V_{Th} = 15 V; R_{Th} = 3.214 \Omega;$ 



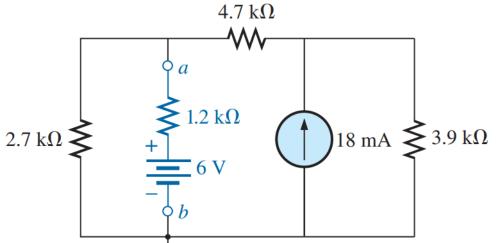
Find the Thevenin equivalent at terminals a-b.



Ans:  $V_{Th} = 0 V$ ;  $R_{Th} = 4 \Omega$ 



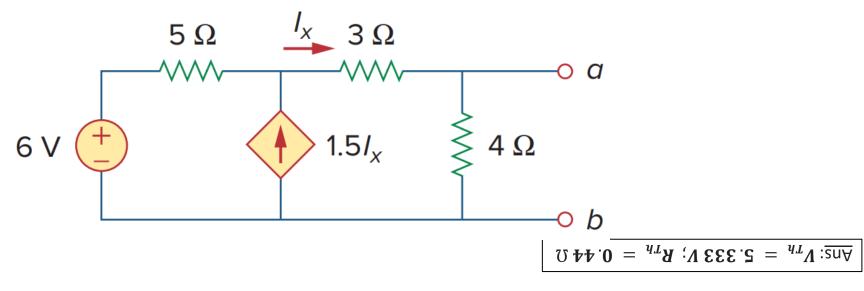
- i. Find the Thevenin equivalent circuit for the portions of the network below external to points a and b.
- ii. Redraw the network with the Thevenin circuit in place and find the current through the resistor.



Ans: (i)  $V_{Th} = 16.77 V$ ;  $R_{Th} = 2.054 k\Omega$ ; (ii)  $\pm 3.31 A$ 

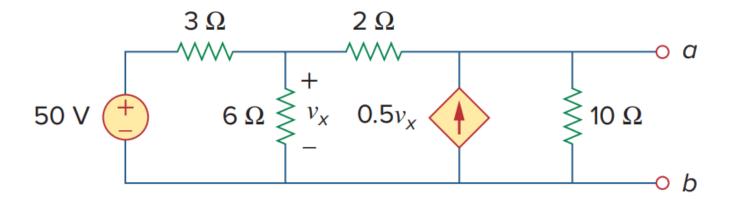


Find the Thevenin equivalent circuit of the circuit to the left of the terminals.





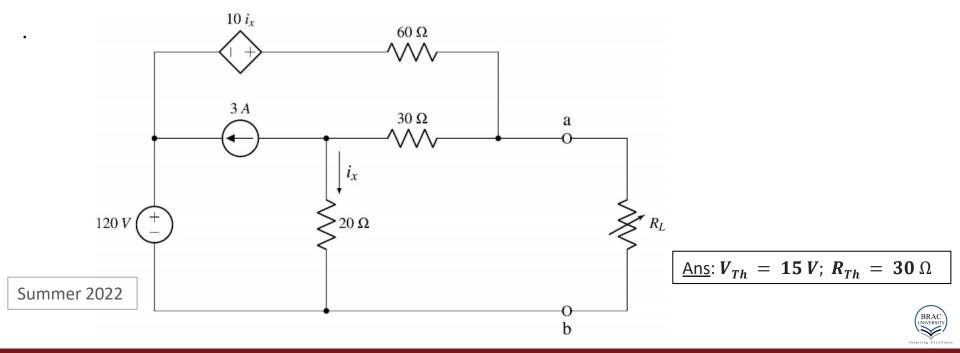
Obtain the Thevenin equivalent circuit at terminals a-b.



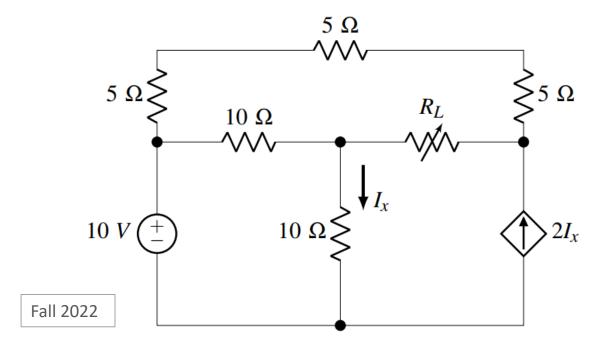
Ans:  $V_{Th} = 166.67 V$ ;  $R_{Th} = 10 \Omega$ 



Obtain the Thevenin equivalent circuit at terminals a-b.



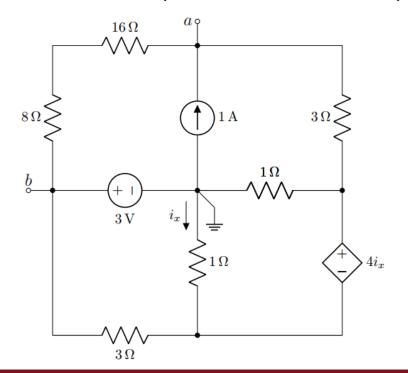
Obtain the Thevenin equivalent circuit at the load  $(R_L)$  terminals.



Ans:  $V_{Th} = \pm 20 V$ ;  $R_{Th} = 5 \Omega$ 

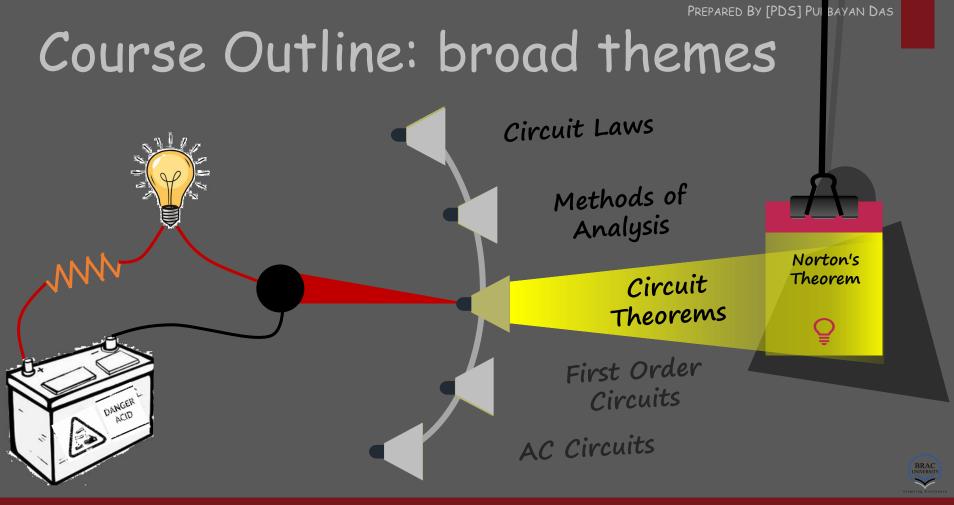


• Obtain the Thevenin equivalent circuit with respect to terminals a-b.



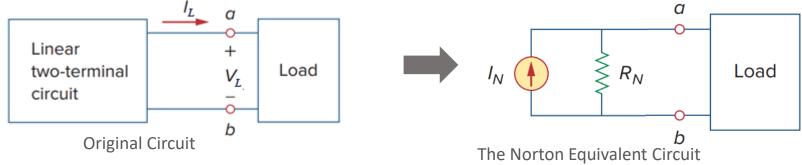
Ans:  $V_{Th} = 3 V$ ;  $R_{Th} = 4 \Omega$ 





## Norton's Theorem

• Norton's theorem states that a linear two-terminal circuit can be replaced by an equivalent circuit consisting of a current source  $I_N$  in parallel with a resistor  $R_N$ , where  $I_N$  is the short-circuit current through the terminals and  $I_N$  is the input or equivalent resistance at the terminals when the independent sources are turned off.



• Two circuits are said to be equivalent if they have the same I-V characteristics at their terminals.



# I-V of Norton Equivalent

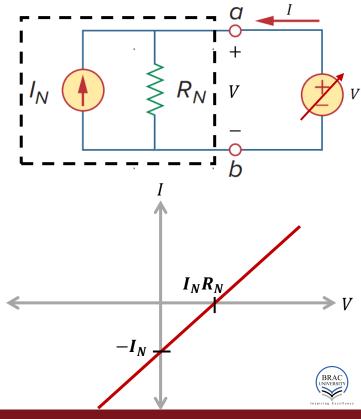
- We can derive the I-V characteristics of the Norton equivalent in a similar way as we did in for Thevenin.
- The configuration is a current source  $(I_N)$  in series with a resistor  $(R_N)$ . To determine the configuration's I-V characteristics, if applying a voltage V gives rise to a current  $i_{\chi}$  through the resistor, we can write using KCL,

$$i_x = I_N + I$$

So, voltage across the resistor can be written as,

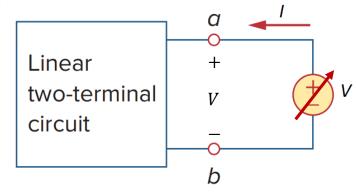
$$V = i_{x}R_{N} = (I_{N} + I)R_{N}$$
$$\Rightarrow I = \frac{1}{R_{N}}V - I_{N}$$

• The equation results in a linear I vs V plot that intersects the axes at  $I_N R_N$  and  $-I_N$ 



## I-V of Actual Circuit

- The procedure to derive the I-V characteristics of the original circuit is exactly the same as done in the Thevenin part. This is described here again.
- To theoretically derive exactly the relation between I and V it is required to know the actual circuitry. As the circuit is linear, the I-V characteristic will be a straight line and the line can be drawn if minimum two points on the line are known.

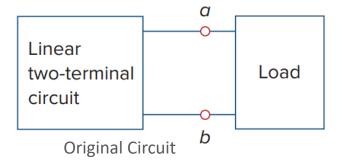


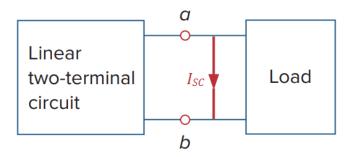
- The two points we can get are the intersecting points of x and y axis.
- To get the intersecting location on the voltage axis, current (I) at the terminals should be made equal to 0. That is, the terminals a-b must be open circuited.
- Similarly, for the intersecting location on current axis,  $V_{ab} = V = 0$ . That is, the terminals a-b must be shorted.

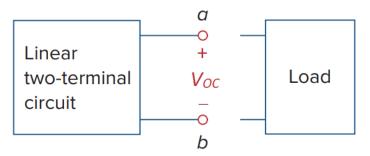


### OC Voltage & SC Current

• Let's denote  $V_{oc}$  be the voltage at the open terminals upon disconnecting the load and  $I_{sc}$  be the current through the shorted terminals upon short circuiting the load.





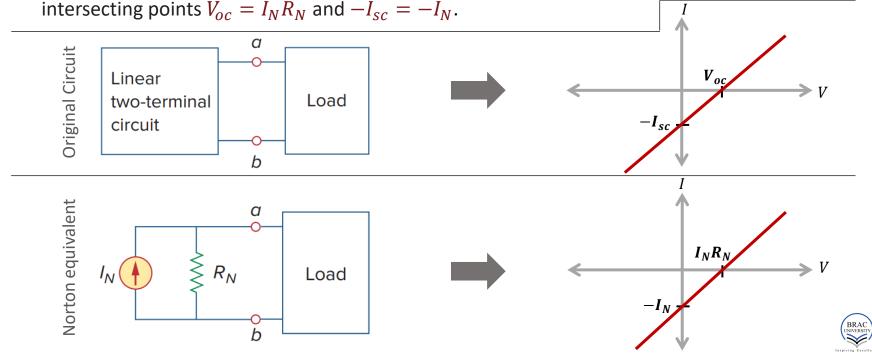


Open Circuited at the terminals

So, the I-V characteristic should be the straight line passing through the points  $(V_{oc}, 0)$  and  $(0, -I_{sc})$ . The reason for the negative sign is that  $I_{sc}$  is opposite to the current (I) plotted along the y-axis.

# Circuit Equivalence

The original circuit and the reduced Norton equivalent circuit will be equivalent to each other if the I-V characteristics of the two are identical. They will indeed be identical if the



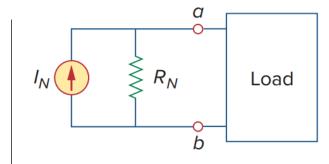
# How to determine R<sub>N</sub>?

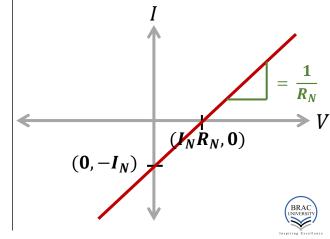
Refer to the previous slides, Norton's conversion is valid if

i. 
$$V_{oc} = I_N R_N \text{ or } I_N = \frac{V_{oc}}{R_N}$$

ii. 
$$-I_N = -I_{SC}$$
 or  $\frac{V_{OC}}{R_N} = I_{SC}$ 

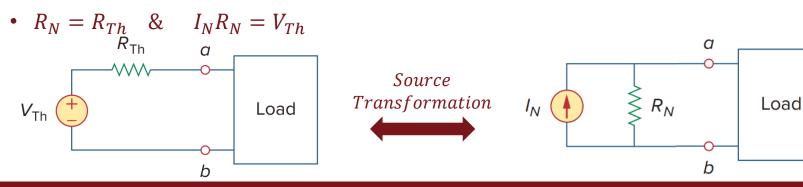
- For the linear I-V characteristic,  $R_N$  is the inverse of the slope of the straight line passing through the points  $(I_N R_N, 0)$  and  $(0, -I_N)$ . That is,
- Slope =  $\frac{\Delta I}{\Delta V} = \frac{0 (-I_N)}{I_N R_N 0} = \frac{1}{R_N}$
- Thus,  $R_N$  may be found from the open circuit voltage  $V_{oc}$  and the Norton current  $I_N$ .
- The undefined scenario that occurs when determining  $R_{Th}$  when  $V_{Th}$  is zero (see here) also occurs when determining  $R_N$  when  $I_{sc}=0$ . In that situation, the Universal Rule used to derive  $R_{Th}$  applies exactly to  $R_N$ .





## Thevenin ↔ Norton

- As you may have already noticed, Norton equivalent of a circuit can be derived from the Thevenin equivalent (or vice versa) of the same circuit by performing a source transformation.
- The requirement is that the two must have the same I-V characteristics.
- From the conditions for which source transformation is valid (shown in <u>slide 7 of Source Transformation</u>) or by comparing the I-V characteristics of the two, it can be seen that the conversion is valid if and only if,



### Methods in a nutshell

RBAYAN DAS Methods to determine  $R_N$ 

Method to determine  $I_N$ Short the load terminals Determine the current through the short circuit ( $I_{SC} = I_N$ )

Use Ohm's Calculate the current Law to  $(i_0)$  supplied or voltage calculate  $(v_0)$  across the voltage or  $R_N = \frac{v_0}{\dot{\cdot}}$ current source respectively.

Valid only if  $I_N \neq 0$ Open the load terminals Determine the voltage at the open terminals  $(V_{oc})$ 

> Add a dummy voltage or current source to the load terminals

Is there Yes anv dependent source(s)?

**Universal Rule** 

Use series-parallel combinations resistors to calculate  $R_{ea} = R_N$ 

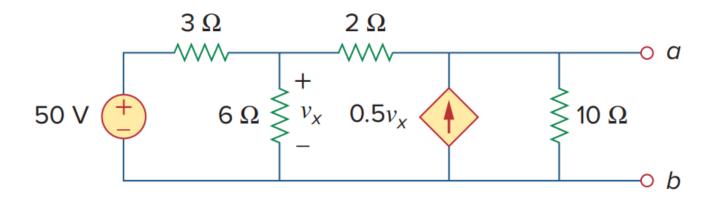
No

Kill all the

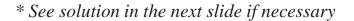
independent sources

# Example 4

Obtain the Norton equivalent circuit at terminals a - b.

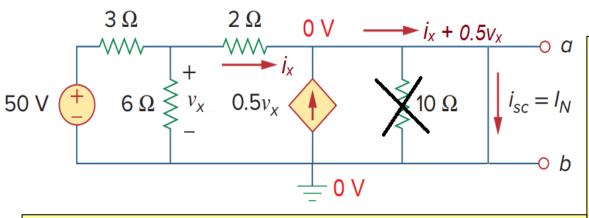


Ans:  $R_N = 10 \Omega$ ;  $I_N = 16.667 A$ 





# Example 4: finding I<sub>N</sub>



The 1st step is to disconnect the load and short the terminals.

Upon short circuiting the terminals a-b, the  $10\,\Omega$  is shorted out. The whole circuit to the left of the dependent source is shorted with respect to it. As a result, the  $0.5v_\chi$  current supplied by the dependent source will only flow through the short circuit.

Let's use nodal analysis to solve for the current  $i_x$  going towards the short circuit though the 2  $\Omega$  resistor.

KCL at 
$$v_x$$

$$\frac{v_x - 50}{3} + \frac{v_x}{6} + \frac{v_x}{2} = 0$$

$$\Rightarrow v_x = 16.667 V$$

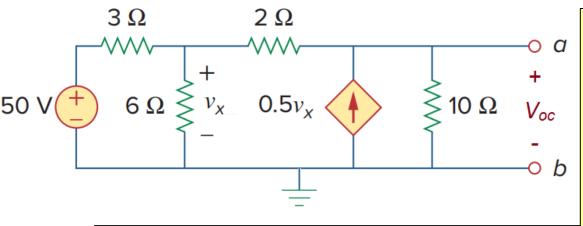
Now,

$$i_x = \frac{v_x - 0}{2} = 8.334 A$$

So,

$$I_N = i_x + 0.5v_x = 16.667 A$$

# Example 4: finding RN



 $R_N$  can be found by (i) determining  $V_{oc}$  and then using  $R_N = \frac{V_{oc}}{I_N}$  (as  $I_N \neq 0$ ) or (ii) first turning off all the independent sources and determining the  $R_{eq}$  at the terminals.

Let's employ the first method here.

#### Nodal analysis:

KCL at  $v_{\gamma}$ ,

10 
$$\Omega$$
  $V_{oc}$  
$$\frac{v_x - 50}{3} + \frac{v_x}{6} + \frac{v_x - V_{oc}}{2} = 0$$
 
$$\Rightarrow 6v_x - 3V_{oc} = 100 - - - - (i)$$

KCL at  $V_{oc}$ 

$$\frac{V_{oc} - v_x}{2} + \frac{V_{oc}}{10} = 0.5v_x$$

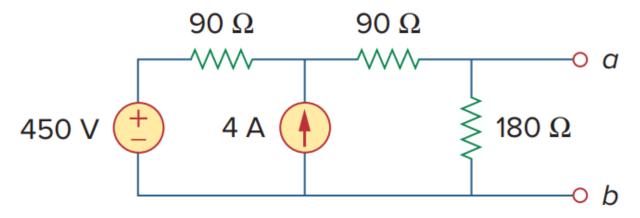
$$\Rightarrow 10v_x - 6V_{oc} = 0 ----(ii)$$

Solving (i) and (ii),

$$V_{oc} = 166.667 V$$

$$R_N = \frac{V_{oc}}{I_{sc}} = \frac{166.667}{16.667} = 10 \Omega$$

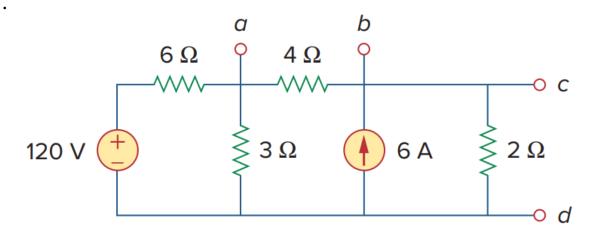
• Find the Norton equivalent circuit for the circuit at terminals a-b.



$$\Omega \mathbf{00} = {}_{N}\mathbf{A} : \mathbf{A} \mathbf{2} \cdot \mathbf{A} = {}_{N}\mathbf{I} : \underline{\mathsf{2nA}}$$



• Find the Norton equivalent circuit for the circuit at terminals (i) a-b and (ii) c-d.

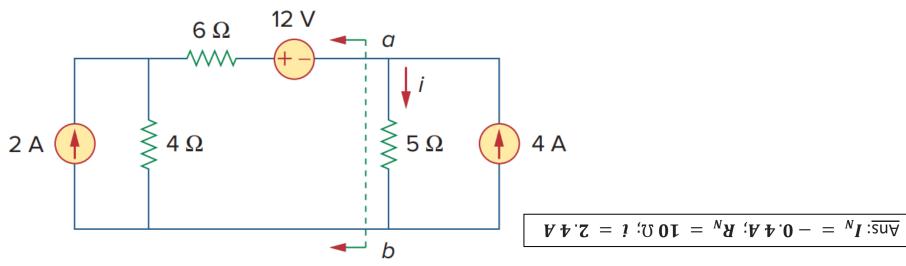


$$\Omega \mathbf{Z} = {}_{N}\mathbf{A} : \mathbf{A} \mathbf{V} = {}_{N}\mathbf{I} (\mathbf{i}) : \underline{\mathsf{2}\mathsf{n}\mathsf{A}}$$

$$\Omega \mathbf{Z} \cdot \mathbf{I} = {}_{N}\mathbf{A} : \mathbf{A} \nabla \mathbf{3} \partial . \mathbf{Z} \mathbf{I} = {}_{N}\mathbf{I} (\mathbf{i}\mathbf{i})$$

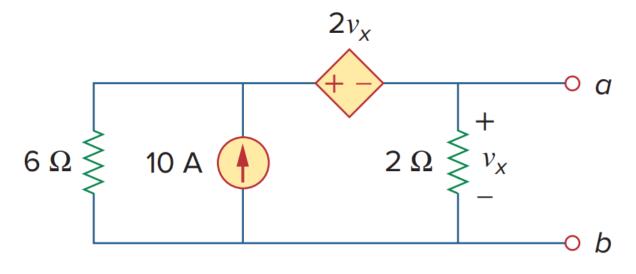


• Obtain the Thevenin/Norton equivalent of the circuit to the left of terminals a-b. Use the result to find current i.





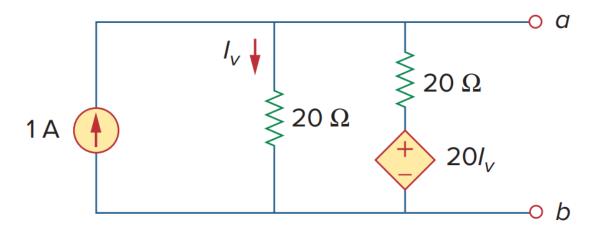
• Find the Norton equivalent circuit for the circuit at terminals a-b.



Ans:  $I_N = 10 A$ ;  $R_N = 1 \Omega$ 



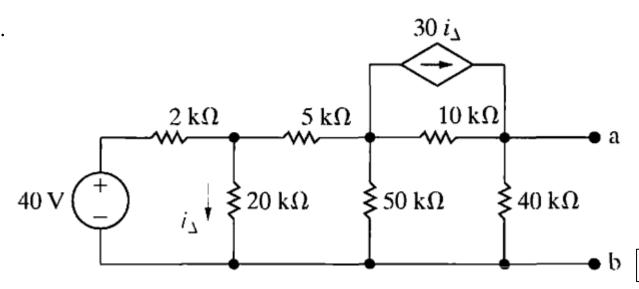
Obtain the Norton equivalent circuit with respect to terminals a and b.



Ans:  $I_N = 1 A$ ;  $R_N = 20 \Omega$ 



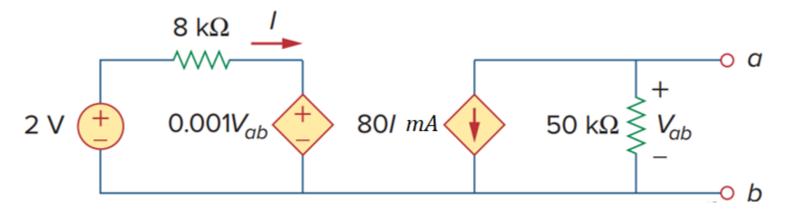
• Obtain the Norton equivalent circuit with respect to terminals a and b.



Ans:  $I_N = 14 \, mA$ ;  $R_N = 20 \, k\Omega$ 



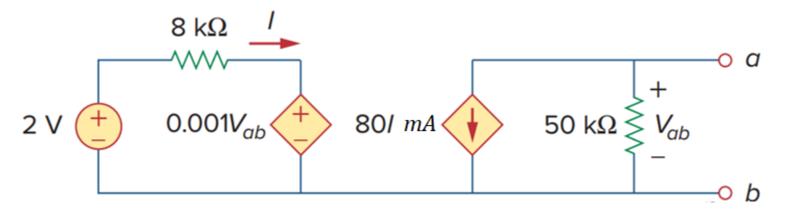
Obtain the Thevenin/Norton equivalent of the circuit to the left of terminals a-b.



Ans:  $V_{Th} = -2000 V$ ;  $I_N = -20 mA$ ;  $R_{Th} = R_N = 100 k\Omega$ 



• Obtain the Thevenin/Norton equivalent of the circuit to the left of terminals a-b.



<u>Ans</u>:  $V_{Th} = -2000 V$ ;  $I_N = -20 mA$ ;  $R_{Th} = R_N = 100 k\Omega$ 



### Practice Problems

- Additional recommended practice problems: here
- Other suggested problems from the textbook: here

