

Open Loop Discrete Time Systems (Chapter 4)

So far we have seen how to deal with ideal sampling (via * transform) and ideal data reconstruction.

Now we will finally put these tools together to get discrete-time transfer functions.

The first step is to examine:

- Relationship between $E(z)$ and $E^*(s)$:

As we will see next $E^*(s)$ provides the link between $E(s)$ (continuous time) and $E(z)$ (discrete time). Let's compare definitions:

$$\left. \begin{aligned} E^*(s) &= \sum_{k=0}^{\infty} e(kT) e^{-ksT} \\ E(z) &= \sum_{k=0}^{\infty} e(kT) z^{-k} \end{aligned} \right\} \Rightarrow \boxed{E^*(s)|_{z=e^{Ts}} = E(z)}$$

(this relationship allows for considering the z-transform as a special case of the Laplace transform)

Suppose we sample a continuous time function and want to get its z-transform:

Old way:

- 1) expand $E(s)$ in partial fractions
- 2) find $e(t) = \mathcal{L}^{-1}[E(s)]$
- 3) find $e(kT)$
- 4) find $E(z) = \sum_{k=0}^{\infty} e(kT) z^{-k}$

Alternative

- 1) find $E^*(s)$
- 2) $E(z) = E^*(s)|_{z=e^{Ts}}$

Obviously the alternative works better only if we have an efficient way of computing $E^*(s)$ from $E(s)$. Here is where the residues formula becomes useful.

Recall that

$$E^*(s) = \sum_{\text{poles } E(\lambda)} \text{Res} \left[E(\lambda) \frac{1}{1 - e^{-Ts(\lambda)}} \right]$$

$$\Rightarrow \boxed{E(z) = \sum_{\text{poles } E(\lambda)} \left[\text{residues of } E(\lambda) \frac{1}{1 - \frac{1}{z} e^{\lambda T}} \right]}$$



Example:

$$E(s) = \frac{1}{(s+1)(s+2)}$$

Old way:

$$1) E(z) = \frac{1}{(z+1)} - \frac{1}{(z+2)}$$

$$2) e(t) = e^{-t} - e^{-2t}$$

$$3) e(kT) = e^{-kT} - e^{-2kT}$$

$$4) E(z) = \sum_0^{\infty} e^{-kT} \cdot z^{-k} - \sum_0^{\infty} e^{-2kT} \cdot z^{-k}$$

$$= \frac{1}{z - \frac{e^{-T}}{z}} - \frac{1}{z - \frac{e^{-2T}}{z}}$$

"New" way

$$E(z) = \sum_{\lambda=-1}^{\lambda=2} \text{Res} \left\{ \frac{1}{(z+\lambda)(z+2)} \frac{1}{z - e^{\lambda T} \frac{1}{z}} \right\}$$

$$= \frac{1}{z - \frac{e^{-T}}{z}} - \frac{1}{z - \frac{e^{-2T}}{z}}$$

=

Q: We just stated that we can view the z-transform as a special case of the Laplace Transform (by using the * transform). So, why do we need it? What's wrong with using $E^*(s)$?

A: Let's compare $E^*(s)$ versus $E(z)$. For the example above we have:

$$E^*(s) = \frac{e^{sT} (e^{-T} - e^{-2T})}{(e^{sT} - e^{-T})(e^{sT} - e^{-2T})}$$

$$E(z) = \frac{z(e^{-T} - e^{-2T})}{(z - e^{-T})(z - e^{-2T})}$$

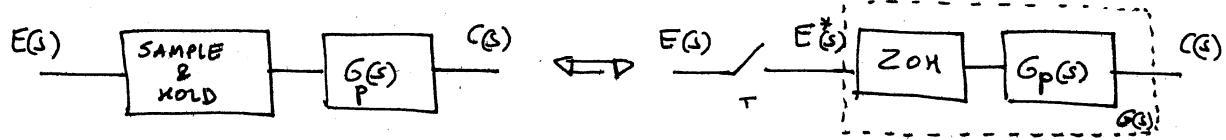
$$\begin{aligned} \infty \text{ poles at } s &= -1 \pm j\omega_s \\ s &= -2 \pm j\omega_s \end{aligned}$$

$$\begin{aligned} 2 \text{ poles: } z &= e^{-T} \\ z &= e^{-2T} \end{aligned}$$

\Rightarrow Any analysis based on pole/zeros will be far easier to carry out in the z-plane. We will see more advantages latter on.

• Pulse Transfer Function:

Remember that our goal was to get a transfer function representation for



The idea is to group the plant & ZOH and consider it a single block $G(s)$

$$\Rightarrow \begin{array}{c} E(s) \\ \swarrow \\ E^*(s) \end{array} \xrightarrow{\quad} G(s) \xrightarrow{\quad} C(s) \quad \text{and} \quad C(s) = G(s) E^*(s)$$

Assume now that we only look at the output at discrete time instants: kT

$$E \xrightarrow{E^*} G(s) \xrightarrow{\quad} C / \xrightarrow{\quad} C^*$$

We want to find out an expression for $C^*(s)$ (as an intermediate step to finding $c(kT)$)

$$C^*(s) = \frac{1}{T} \sum_{-\infty}^{+\infty} c(s + jn\omega_s) = \frac{1}{T} \sum_{-\infty}^{+\infty} G(s + jn\omega_s) E^*(s + jn\omega_s)$$

But E^* is periodic $\Rightarrow E^*(s + jn\omega_s) = E^*(s)$

$$\Rightarrow C^*(s) = \frac{1}{T} \sum_{-\infty}^{+\infty} G(s + jn\omega_s) E^*(s) = E^*(s) \left[\frac{1}{T} \sum_{-\infty}^{+\infty} G(s + jn\omega_s) \right] = E^*(s) G^*(s)$$

\Rightarrow We have just shown that:

$$C^*(s) = [G(s) E^*(s)]^* = G^*(s) E^*(s) \#$$

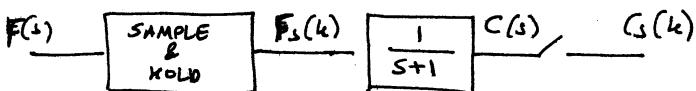
or, using z-transforms:

$$C(z) = G(z) E(z)$$

We will call $G(z)$ the pulse transfer function

(Roughly speaking: TF between sampled input & sampled output
at the sampling instants)

Suppose that we want to find the TF of a simple plant:



Brute force approach: $C(s) = \frac{1}{(s+1)} F_s \stackrel{s \rightarrow -1}{\Rightarrow} \dot{c}(t) + c(t) = f_s(t)$

Solving this first order differential equation yields:

$$c(t) = A e^{-(t-kT)} + f(kT) \quad (\text{recall that } f_s(t) = f(kT) \quad kT \leq t < (k+1)T)$$

Now we need to impose the initial condition $c(t)|_{t=kT} = c(kT)$ and solve for A:

$$A = c(kT) - f(kT) \Rightarrow$$

$$c(t) = c(kT) e^{-(t-kT)} + [1 - e^{-(t-kT)}] f(kT) \quad kT \leq t < (k+1)T$$

$$\Rightarrow c((k+1)T) = c(kT) e^{-T} + (1 - e^{-T}) f(kT)$$

$\Downarrow z$ transform

$$(z - e^{-T}) C(z) = (1 - e^{-T}) F(z) \Rightarrow \boxed{\frac{C(z)}{F(z)} = \frac{1 - e^{-T}}{z - e^{-T}}}$$

Let's of work, even for a very simple plant! Let's try now our tools:

$$F \xrightarrow{F^*} \boxed{\frac{1 - e^{-sT}}{s}} \xrightarrow{\frac{1}{s+1}} C^* \quad G(s) = \frac{1 - e^{-sT}}{s(s+1)} = \frac{C(s)}{F^*}$$

$$\Rightarrow \frac{C(z)}{F(z)} = \mathcal{Z} \left\{ \frac{1 - e^{-sT}}{s(s+1)} \right\} = \left[\frac{1 - e^{-sT}}{s(s+1)} \right]^* \Big|_{z=e^{sT}}$$

Note that we have a delay \Rightarrow (3-10) does not apply. However since the delay is an integer number of periods we can use the alternative formula:

$$\left[e^{-mTs} G_1(s) \right]^* = e^{-mTs} \left[G_1(s) \right]^* \Leftrightarrow \mathcal{Z} \left[e^{-mTs} G_1(s) \right]^* = \frac{1}{z^m} G_1(z)$$

In this case we have: $G_1(s) = \frac{1}{s(s+1)} \Leftrightarrow G_1(z) = \sum_{\lambda=0}^{\infty} \text{Res} \left[\frac{1}{s(\lambda+1)} \cdot \frac{1}{(1 - \frac{e^{-sT}}{z})} \right]$

$$= \frac{1}{s-\frac{1}{2}} - \frac{1}{s-e^{-T}/2} = \frac{z(1-e^{-T})}{(z-1)(z-e^{-T})}$$

and $G(z) = G_1(z) - \frac{1}{z} G_1(z) = \left(\frac{z-1}{z} \right) G_1(z) =$

$$\boxed{\frac{1 - e^{-T}}{z - e^{-T}}}$$

same as before

(but we did not have to solve a differential eq.)

Assume now that the input is a step: $f(kT) = 1, 1, \dots$

$$F(z) = \frac{z}{z-1}$$

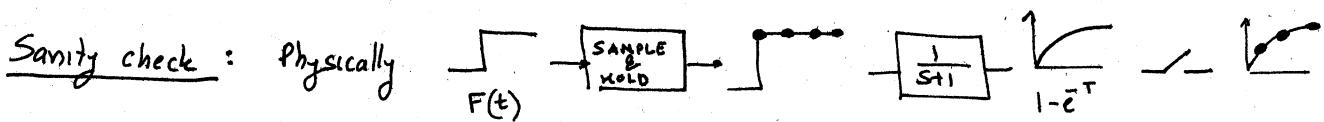
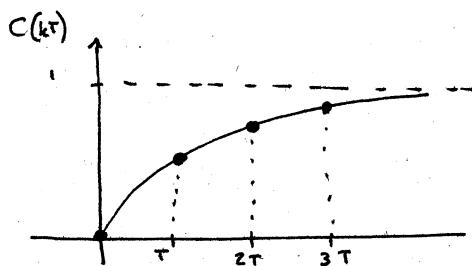
$$\Rightarrow C(z) = G(z)F(z) = \frac{z}{(z-1)} \frac{(1-e^{-T})}{(z-e^{-T})} = \frac{z}{z-1} - \frac{z}{z-e^{-T}}$$

Going back to the time domain we get:

$$c(kT) = \bar{z}^{-1}[C(z)] = \bar{z}^{-1}\left[\frac{z}{z-1} - \frac{z}{z-e^{-T}}\right] = 1 - e^{-kT} \#$$

(Note: you can get the same result from residues, without having to do partial fractions)

$$c_k = \sum_{\substack{z=1 \\ z=e^{-T}}}^{\infty} \text{Res} \left\{ z^{k-1} \frac{z(1-e^{-T})}{(z-1)(z-e^{-T})} \right\} = \frac{(1-e^{-T})}{(1-e^{-T})} + e^{-kT} \frac{(1-e^{-T})}{e^{-T}-1} = 1 - e^{-kT} \#$$



Important: You can get $c(kT)$ from $c(t)$ but the converse does not work. You cannot recover $c(t)$ from $c(kT)$

(obvious, since $c(kT)$ does not contain information about what happens in between samples)

(Final value theorem)

• Definition: DC gain:

$$\frac{\lim_{k \rightarrow \infty} c_k}{\lim_{k \rightarrow \infty} F_k} = \frac{c_{ss}}{F_{ss}} = \lim_{z \rightarrow 1} \frac{(z-1)G(z)}{F_{ss}}$$

$$= \lim_{z \rightarrow 1} \frac{(z-1)G(z)F(z)}{F_{ss}} = \lim_{z \rightarrow 1} \frac{(z-1)G(z)F_{ss}}{F_{ss}} \cancel{\frac{z}{(z-1)}}$$

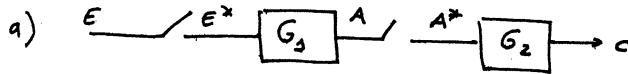
$$= G(1)$$

\Rightarrow DC gain: $G(1)$

(compare with continuous time: DC gain = $G(s)|_{s=0}$)

but then again: $z = e^{Ts} \Rightarrow s=0$ gets mapped to $z=1$

- Other configurations:



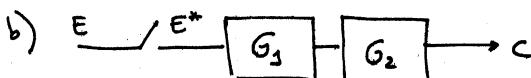
$$C(s) = G_2(s) A^*(s) \quad A(s) = G_1(s) E^*(s) \Rightarrow A^* = (G_1 E^*)^* = G_1^* E^*$$

$$C^*(s) = G_2^* A^* = G_2^* G_1^* E^*(s) E^*(s)$$



$$\boxed{C(z) = G_2(z) G_1(z) E(z)} \quad \text{or} \quad \boxed{G(z) = G_1(z) \cdot G_2(z)}$$

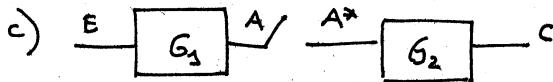
Key feature: we have an ideal sampler between G_1 & G_2



$$C(s) = G_2(s) G_1(s) E^*(s) \Rightarrow C^*(s) = [G_1 \cdot G_2]^* E^*(s) \quad \text{or}$$

$$C(z) = \mathbb{Z} \{ G_1 \cdot G_2 \} \cdot E(z) \Rightarrow \boxed{G(z) = \mathbb{Z} [G_1 \cdot G_2]}$$

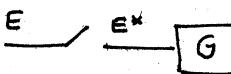
Note: $\mathbb{Z} [G_1 G_2] \neq G_1(z) G_2(z)$!!



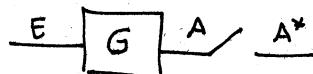
$$C = G_2 A^* \Rightarrow C^* = G_2^* [G_1 E]^*$$

For this system a transfer function cannot be written!
The reason is that you can't factor $E(z)$ out of $[G_1 E](z)$.

Physical reason:

When you have , E^* contains information about E only at the sampling instants. \Rightarrow When you compute C^* you can factor E^* out.

On the other hand, if you have something like this:



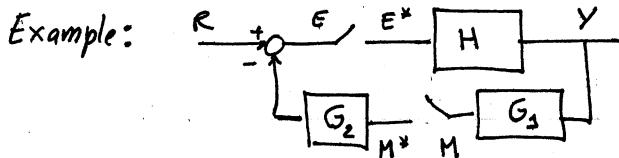
$$A(s) = \int_{-\infty}^t g(t-z) e(z) dz$$

$$a(t) = \int_0^t g(t-z) e(z) dz \Rightarrow$$

to compute A^* (and latter C^*) you need information about $e(t)$ at all times, not just the sampling instants.

Important consequence: If you want to have a discrete T.F. you have to select as your unknowns the inputs to the sampler

This variables will always "come free" after the equation sampling process and give a set of starred variables for which we can solve.



$$E(s) = R - G_2 M^*$$

$$E^* = R^* - [G_2 M]^* = R^* - G_2^* M^*$$

$$M = (G_3 H) E^* \Rightarrow M^* = (G_3 H)^* E^*$$

$$E^* = R^* G_2^* [G_3 H]^* E^*$$

$$\Rightarrow E^* = \frac{R^*}{1 + (G_3 H)^* G_2^*}$$

or:

$$\frac{E(z)}{R(z)} = \frac{1}{1 + [G_3 H](z) G_2(z)}$$

To obtain Y we can use the equation: $Y(s) = H E^* \Rightarrow Y^* = H^* E^*$

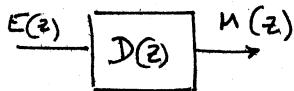
$$\Rightarrow \frac{Y^*}{R^*} = \frac{H^*}{1 + (G_3 H)^* G_2^*} \Leftrightarrow$$

$$\frac{Y(z)}{R(z)} = \frac{H(z)}{1 + (H G_3)(z) G_2(z)}$$

Note that in this case we have a TF. This is because R goes right through a sampler before entering other blocks.

- Open-loop Systems with Digital Filters

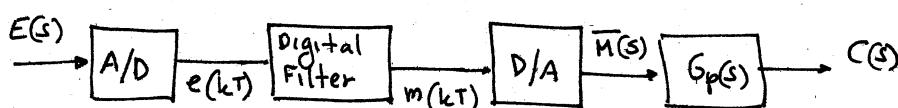
We consider now the case where the sampled-data system contains a digital filter



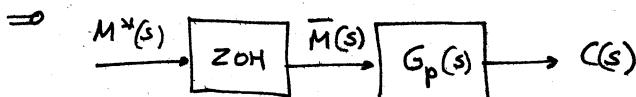
$$M(z) = D(z) E(z)$$

$$M^*(s) = D^*(s) E^*(s)$$

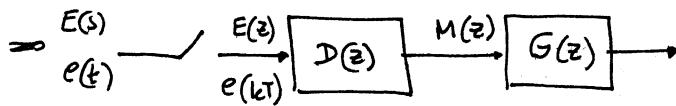
Physically:



We will assume that the D/A can be represented as a zero order hold



(Recall that $G_{h_0} = \frac{1-e^{-sT}}{s}$)



$$C(s) = \underbrace{G_{h_0}(s) \cdot G_p(s)}_{G(s)} M^*(s) \Rightarrow C(z) = G(z) M(z) = G(z) D(z) \bar{E}(z)$$

Example: Suppose that the digital filter is given by the following diff. eq.

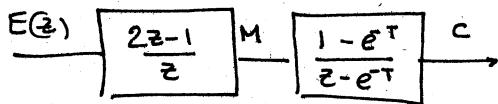
$$m(kT) = 2e(kT) - e[(k-1)T]$$

$$M(z) = 2E(z) - \frac{E(z)}{z} = \frac{2z-1}{z} E(z)$$

$$\Rightarrow D(z) = \frac{M}{E} = \boxed{\frac{2z-1}{z}}$$

$$G_p(s) = \frac{1}{(s+1)} \Rightarrow G(s) = G_{h_0} G_p = \frac{1-e^{-sT}}{s(s+1)}$$

$$G(z) = \left(1 - \frac{1}{z}\right) \bar{E} \left[\frac{1}{s(s+1)} \right] = \left(1 - \frac{1}{z}\right) \left[\frac{1}{z-1/z} - \frac{1}{z-e^{-T}/z} \right] \\ = \frac{1-e^{-T}}{z-e^{-T}}$$



Assume that $E(z)$ is a step: $E(z) = \frac{z}{z-1} \Rightarrow$

$$C(z) = \left(\frac{1-e^{-T}}{z-e^{-T}}\right) \left(\frac{2z-1}{z}\right) \left(\frac{z}{z-1}\right)$$

From here we can get $c(kT)$ either by doing partial fraction expansion or using the residues formula.

Effect of T_s

Recall they $C^*(s)$ or $C(z)$ gives you information only on what happens at the sampling instants, but not in-between.

Q: Is this a problem?

A: Depends on how fast the dynamics of your plant are, compared to the sampling rate

Example: $G_p(s) = \frac{25}{s^2 + 2s + 25} \Rightarrow \omega_n^2 = 25 \quad (\omega_n = 5)$
 $\zeta = 0.2 \quad (\text{underdamped})$

It can be shown that if we sample at $T=0.1$ and $T=1$ we get the following discrete time equivalents:

$$G(z) = Z \left\{ \left(\frac{1 - e^{-sT}}{s} \right) \cdot G_p(s) \right\} = \left(\frac{1 - \frac{1}{z}}{z} \right) Z \left[\frac{25}{s(s^2 + 2s + 25)} \right]$$

$$G_{T=1} = \frac{z - 0.007}{z^2 - 0.1365z + 0.1353}$$

$$G_{T=0.1} = \frac{0.115z - 0.107}{z^2 - 1.6z + 0.82}$$

Let's look at the step responses (next pages)

In one case the discrete output captures the relevant dynamics.
In the second case there is significant intersample ripple.