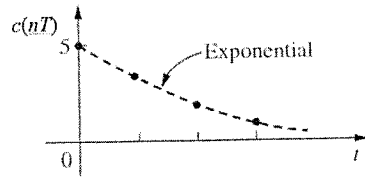


4.3-2

$$(a) \quad G(z) = \frac{z-1}{z} \mathcal{Z} \left[\frac{5s}{s(s+0.1)} \right] = \frac{z-1}{z} \times \frac{5z}{z - e^{-0.2}} = \frac{5(z-1)}{z-0.8187}$$

$$Y(z) = \left(\frac{z}{z-1} \right) \frac{5(z-1)}{z-0.8187} = \frac{5z}{z-0.8187}$$



$$\therefore c(nT) = 5(0.8187)^n$$

$$(b) \quad M(s) = \frac{1}{s}$$

$$\therefore Y(s) = \frac{5s}{s(s+0.1)} = \frac{5}{s+0.1}, \quad \therefore y(t) = 5e^{-0.1t}$$

$$\therefore y(nT) = y(2n) = 5e^{-0.1(2n)} = 5(e^{-0.2})^n = 5(0.8187)^n$$

$$(c) \quad \text{dc gain} = G_p(s) \Big|_{s=0} = \frac{5(0)}{0+0.1} = 0$$

$$\text{dc gain} = G(z) \Big|_{z=1} = \frac{5(1-1)}{1-0.8187} = 0$$

$$(d) \quad \text{Yes } -C_{ss}(kT) = (1)(\text{dc gain}) = 0 \text{ from (a), } \therefore \text{dc gain} = 0$$

$$C_{ss}(t) = (1)(\text{dc gain}) = 0 \text{ from (b), } \therefore \text{dc gain} = 0$$

4.3-7.

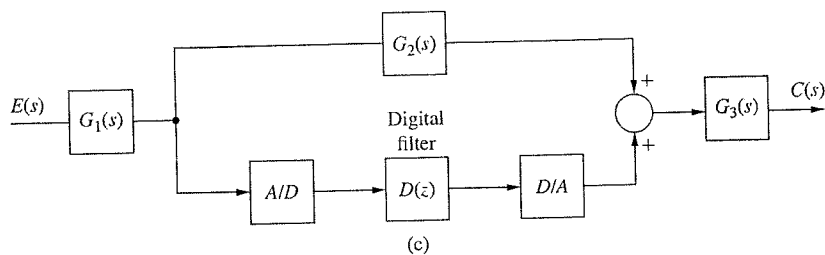
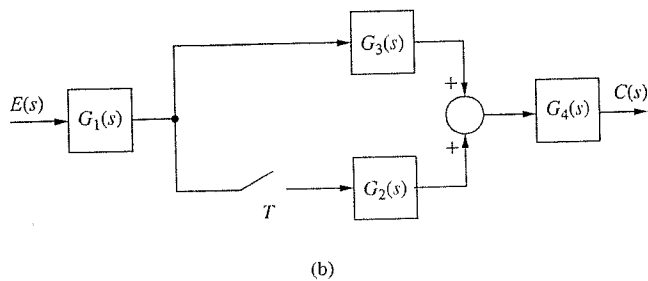
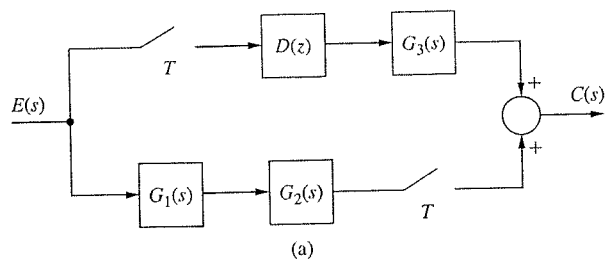


Fig. P4.3-7

(a) Express each $C(s)$ and $C(z)$ as functions of the input for the systems of Fig. P4.3-7.

(b) List those transfer functions in Fig. P4.3-7 that contain the transfer function of a data hold.

Solution:

(a) (i) $C(z) = G_3(z)D(z)E(z) + \overline{G_1 G_2}E(z)$

$$(ii) \quad C(z) = \overline{G_1 G_3 G_4 E}(z) + \overline{G_2 G_4}(z) \overline{G_1 E}(z)$$

$$(iii) \quad C(z) = \overline{G_1 G_2 G_3 E}(z) + G_3^1(z) D(z) \overline{G_1 E}(z), \quad G_3^1(z) = \left(\frac{1 - \varepsilon^{-Ts}}{s} \right) G_3(s)$$

$$(b) \quad (i) \quad G_3(s)$$

$$(ii) \quad G_2(s)$$

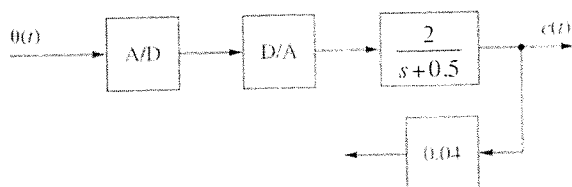
$$(iii) \quad G_3^1(s)$$

4.3-9. A digital control system is shown in Figure 4.3-9. The input is a unit step function, $u(t)$. The output is $c(t)$. The system is a closed-loop system with a feedback path. The forward path consists of an A/D converter, a D/A converter, and a continuous-time block $\frac{2}{s+0.5}$. The feedback path consists of a block 1.04 . The output $c(t)$ is sampled at $t = kT$ and converted back to analog by the D/A converter.

4.3-9

Solution:

(a)



$$\begin{aligned} \text{(b)} \quad G(z) &= \frac{z-1}{z} \mathcal{Z} \left[\frac{2}{s(s+0.5)} \right] - \frac{z-1}{z} \frac{2}{0.5} \left[\frac{z(1-\epsilon^{-0.5T})}{(z-1)(z-\epsilon^{-0.5T})} \right] \\ &= \frac{4(1-\epsilon^{-0.5T})}{z-\epsilon^{-0.5T}} \end{aligned}$$

$$\text{(c)} \quad G_p(0) = \text{dc gain} = \frac{2}{0.5} = 4, \therefore c_{ss}(kT) = 10(4) = 40^\circ\text{C}$$

$$\text{(d)} \quad G_d(0) = -\frac{2.5}{0.5} = -5, \therefore \Delta c_{ss}(kT) = (-5)(1) = -5^\circ\text{C}$$

$$\text{(e)} \quad C(s) = E^*(s) \left(\frac{1-\epsilon^{-Ts}}{s} \right) \left(\frac{2}{s+0.5} \right) - \frac{2.5}{s+0.5} D(s)$$

4.4-1. Example 4.3 calculates the step response of the system in Fig. 4-2. Example 4.4 calculates the step response of the same system preceded by a digital filter with the transfer function $D(z) = (2 - z^{-1})$. This system is shown in Fig. P4.4-1.

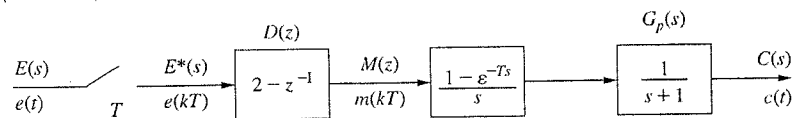


Fig. P4.4-1

- Solve for the output of the digital filter $m(kT)$.
- Let the response in Example 4.3 be denoted as $c_1(kT)$. Use the results in part (a) to express the output $c(kT)$ in Fig. P4.4-1 as a function of $c_1(kT)$.
- Use the response $c_1(kT)$ calculated in Example 4.3 and the results in part (b) to find the output $c(kT)$ in Fig. P4.4-1. This result should be the same as in Example 4.4.
- Use the response $C_1(z)$ calculated in Example 4.3 and the result in part (b) to find the output $C(z)$ in Fig. P4.4-1. This result should be the same as in Example 4.4.

Solution:

$$(a) \quad M(z) = (2 - z^{-1})E(z)$$

$$\therefore m(kT) = 2e(kT) - e[(k-1)T] = 2u(kT) - u[(k-1)T]$$

$$\therefore m(0) = 2, \quad m(k) = 1, \quad k \geq 1$$

$$(b) \quad C(kT) = 2C_1(kT) - C_1[(k-1)T]$$

$$(c) \quad C_1(kT) = (1 - e^{-kT})u(kT)$$

$$C(kT) = 2(1 - e^{-kT})u(kT) - u[(k-1)T] + e^{-(k-1)T}u[(k-1)T]$$

$$= \begin{cases} 0, & k=0 \\ 1 - (2 - \epsilon^{-T})\epsilon^{-kT}, & k \geq 1 \end{cases}$$

(d) Example 4.3, $C_1(kT) = \frac{z(1 - \epsilon^{-T})}{(z-1)(z - \epsilon^{-T})}$

$$\therefore C(z) = 2C_1(z) - z^{-1}C_1(z) = \frac{2z(1 - \epsilon^{-T})}{(z-1)(z - \epsilon^{-T})} - \frac{1 - \epsilon^{-T}}{(z-1)(z - \epsilon^{-T})}$$

$$= \frac{(2z-1)(1 - \epsilon^{-T})}{(z-1)(z - \epsilon^{-T})}$$

4.4-5. Consider the system of Fig. P4.4-5. The filter transfer function is $D(z)$.

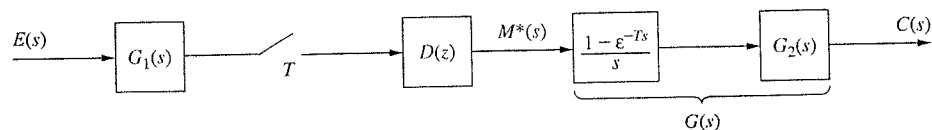


Fig. P4.4-5

- Express $C(z)$ as a function of E .
- A discrete state model of this system does not exist. Why?
- What assumptions concerning $e(t)$ must be made in order to derive an approximate discrete state model?

Solution:

(a)



$$C(s) = G(s)M^*(s)$$

$$C(z) = G(z)M(z) = G(z)D(z) \overline{G_1 E}(z)$$

- Cannot factor $E(z)$ from $\overline{G_1 E}(z)$.
- Assume that $e(t)$ changes so slowly that the system can be accurately approximated by placing a sampler/data-hold in front of $G_1(s)$. Then

$$C(z) = G(z) D(z) \left[\frac{1 - e^{-Ts}}{s} G_1(s) \right] E(z).$$

- 4.6-2.** For the thermal test chamber of Problems 4.3-9 and 4.6-1, let $T = 0.6$ s. Suppose that a proportional-integral (PI) digital controller with the transfer function

$$D(z) = 1.2 + \frac{0.1z}{z-1}$$

is inserted between the sampler and the zero-order hold in Fig. P4.3-9.

- (a) With $d(t) = 0$ and $e(t) = u(t)$, solve for $c(kT)$, with the time delay of 2 s omitted.
- (b) Explain what happens to the temperature in the chamber in part (a). Is this result physically possible?
- (c) In Fig. P4.3-9, calculate $m(kT)$, the signal that controls the valve in the steam line, for the inputs of part (a).
- (d) Considering the physical characteristics of a valve, what happens to the temperature in the physical test chamber?

Solution:

$$(a) \quad D(z) = 1.2 + \frac{0.1z}{z-1} = \frac{1.3z-1}{z-1}; \text{ From Prob. 4-21(a): } G(z) = \frac{1.037}{z-0.7408}$$

$$\therefore \frac{C(z)}{z} = \frac{1.037(1.3z-1)}{(z-1)^2(z-0.7408)} = \frac{1.20}{(z-1)^2} + \frac{0.5705}{z-1} + \frac{-0.5705}{z-0.7408}$$

$$\therefore C(z) = \frac{2(0.6z)}{(z-1)^2} + \frac{0.5705z}{z-1} + \frac{-0.5705z}{z-0.7408}$$

$$\therefore c(kT) = 2kT + 0.5705[1 - 0.7408^k]$$

- (b) The temperature increases without limit-*Not* physically realizable.

$$(c) \quad \frac{M(z)}{z} = \frac{1.3z-1}{(z-1)^2} = \frac{1.3(z-1)}{(z-1)^2} + \frac{0.3}{(z-1)^2} = \frac{0.3}{(z-1)^2} + \frac{1.3}{z-1}$$

$$\therefore m(kT) = kT + 1.3$$

- (d) The value will reach full open. Then $m(kT)$ is effectively constant and the temperature will settle to a constant value.