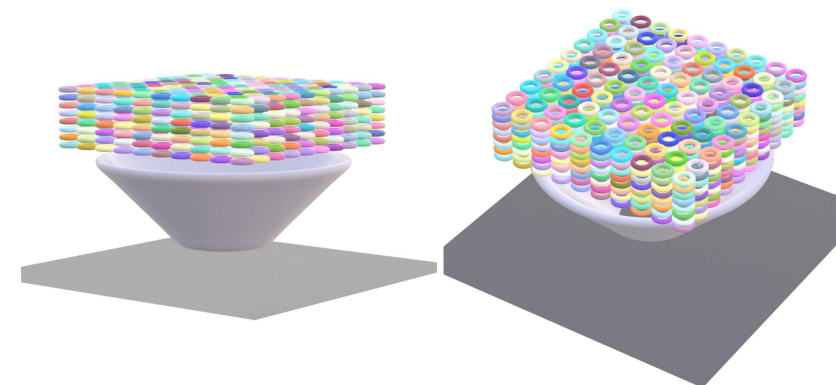
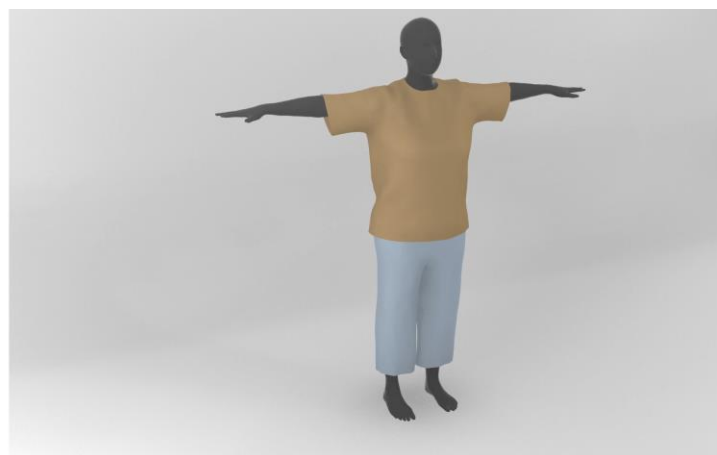
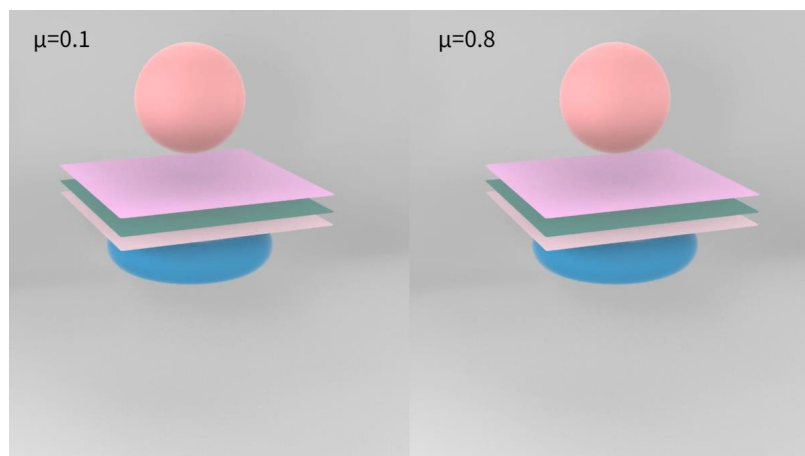


# Efficient frictional contacts for soft body dynamics via ADMM

Siyan Zhu<sup>1</sup>, Cheng Fang<sup>1</sup>, \*Peng Yu<sup>1</sup>, \*Xiao Zhai<sup>2</sup>, Aimin Hao<sup>1</sup>, \*Junjun Pan<sup>1</sup>

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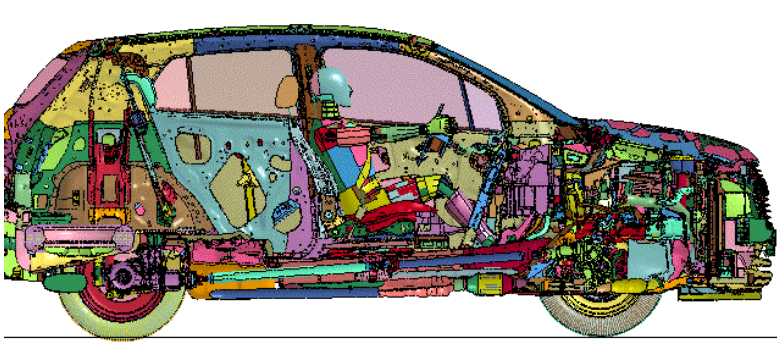
2. Weta FX, New Zealand



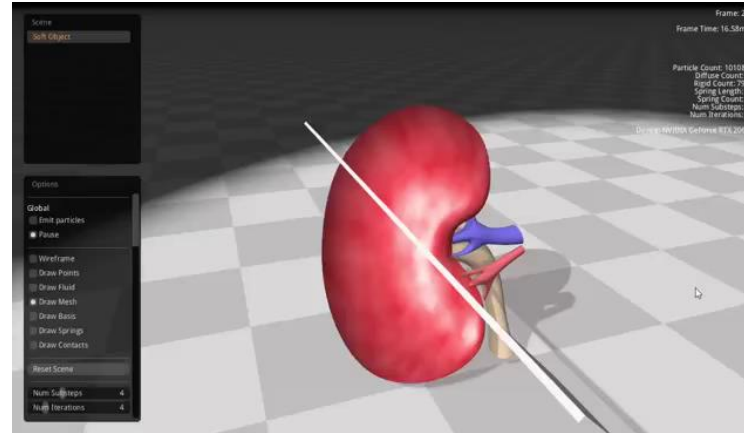
虚拟现实技术与系统全国重点实验室  
STATE KEY LABORATORY OF VIRTUAL REALITY TECHNOLOGY AND SYSTEMS

wētāFX

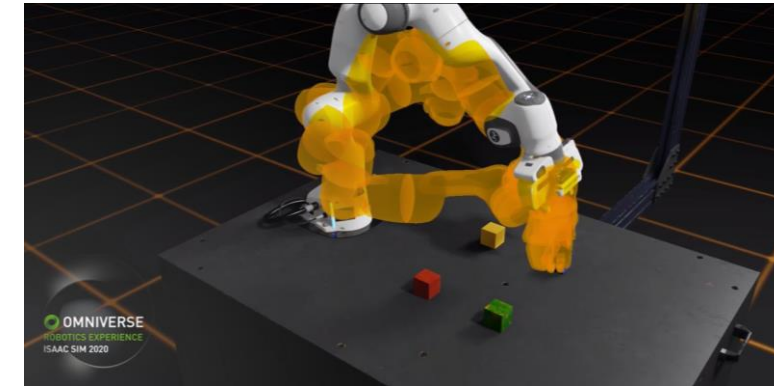
# Contact Simulation Applications



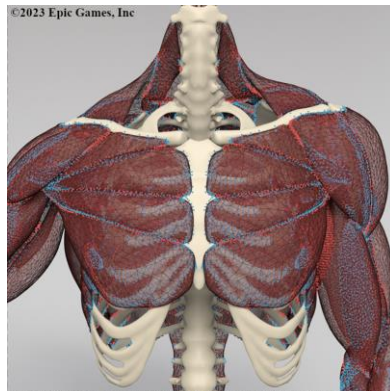
Industry Design



Virtual Surgery



Robotics



Biomechanics



Movies



Autopilot Training Platform

- ## Forward Euler Time Integration
- $$\mathbf{x}^{t+1} = \underset{\text{New Pos}}{\operatorname{argmin}_x} \underset{\text{Incremental Potential}}{E(\mathbf{x})} = \underbrace{\frac{1}{2h^2} (\mathbf{x} - \tilde{\mathbf{x}})^T \mathbf{M} (\mathbf{x} - \tilde{\mathbf{x}})}_{\text{Inertia Term}} + \underbrace{U(\mathbf{x})}_{\text{Elasticity Energy}}$$
- Mass Matrix      Predicted Position
- ↑      ↗

- $$\mathbf{x}^{t+1} = \operatorname{argmin}_{\mathbf{x}} E(\mathbf{x}) + P(\mathbf{x})$$

- 
- Figure 1 shows the barrier energy as a function of distance for different interaction models. The y-axis represents the barrier energy, ranging from 0 to 3.5. The x-axis represents the distance, ranging from 0 to 1.5. Four curves are plotted: a blue curve for the 'discontinuous' model, a brown curve for 'C2,  $\hat{d} = 1$ ', a yellow curve for 'C2,  $\hat{d} = 0.8$ ', and a purple curve for 'C2,  $\hat{d} = 0.5$ '. Vertical dashed lines indicate the range of the interaction for each model: blue at 0, brown at 0.5, yellow at 0.8, and purple at 1.0.

# Backgrounds

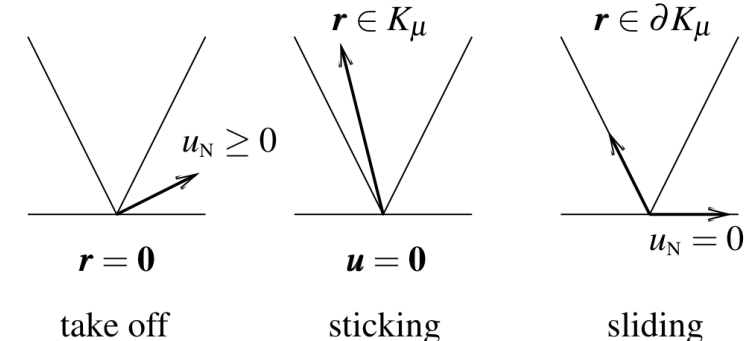
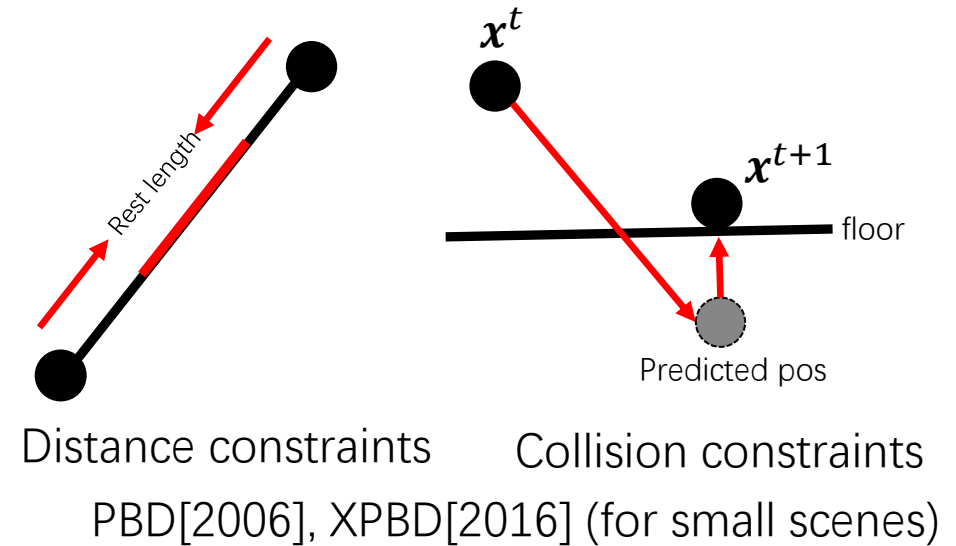
- Dual based method

$$\begin{aligned} \mathbf{x}^{t+1} = \operatorname{argmin}_{\mathbf{x}} \frac{1}{2} (\mathbf{x} - \tilde{\mathbf{x}})^T \mathbf{M} (\mathbf{x} - \tilde{\mathbf{x}}) \\ \text{s.t. } C_1(\mathbf{x}) \leq 0, \\ C_2(\mathbf{x}) = 0 \end{aligned}$$

- Hybrid method

$$\begin{aligned} \mathbf{x}^{t+1} = \operatorname{argmin}_{\mathbf{x}} E(\mathbf{x}) \\ \text{s.t. } C_1(\mathbf{x}) \leq 0, \\ C_2(\mathbf{x}) = 0 \end{aligned} \quad \longrightarrow \quad \begin{cases} M \frac{d\mathbf{v}}{dt} = \mathbf{f}(t, \mathbf{x}, \mathbf{v}) + \mathbf{J}_{\mathbf{f}^c}^T \mathbf{r} \\ \mathbf{u} = \mathbf{J} \mathbf{v} + \mathbf{u}_f \\ \forall i = 1 \dots n, (\mathbf{r}^i, \mathbf{u}^i) \in K_\mu. \end{cases}$$

Gilles Daviet [2021, 2023]

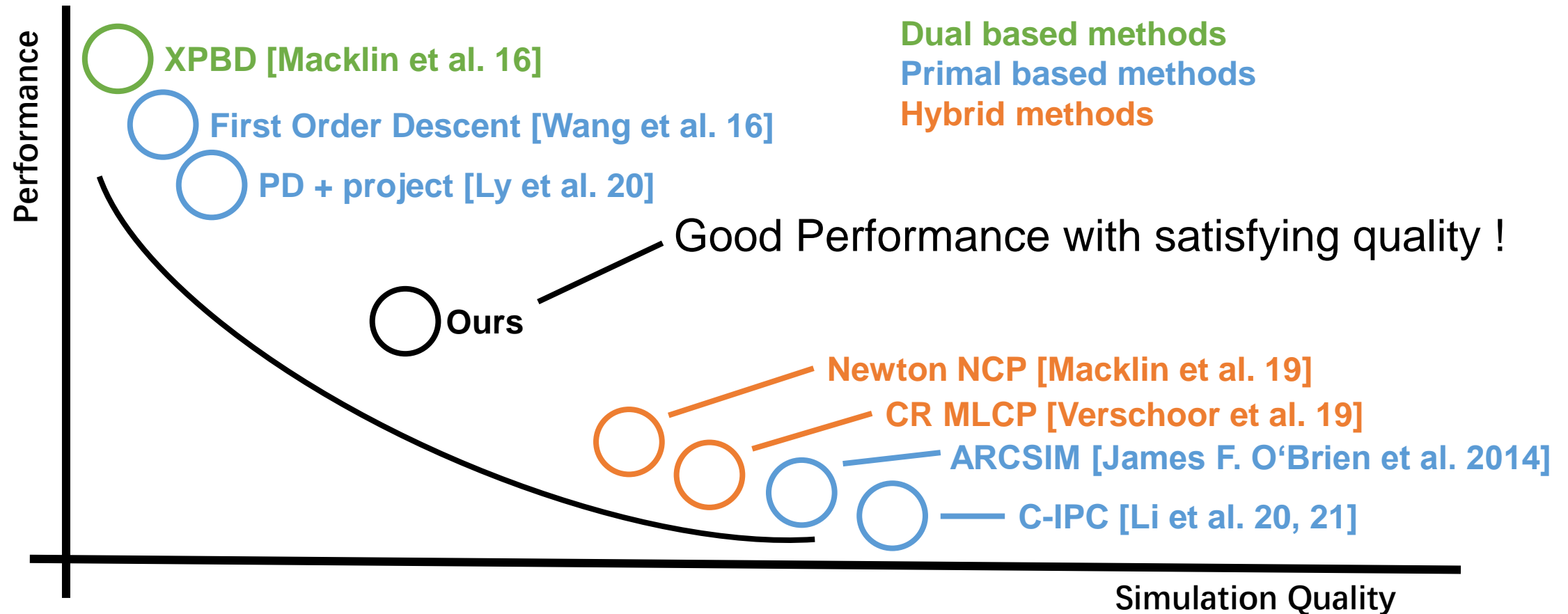


Coulomb friction model

- Delassus Operator  $\mathbf{J} \mathbf{A}^{-1} \mathbf{J}^T$  (Large Sparse Matrix Inversion, time consuming)

# Motivation

- Habitat of our method



# ADMM (Alternating Direction Method of Multipliers)

- ADMM: solving convex optimization problem

$$\min_{\mathbf{x}, \mathbf{z}} f(\mathbf{x}) + g(\mathbf{z}), \text{ s.t. } \mathbf{Ax} + \mathbf{Bz} + \mathbf{c} = 0,$$



$$L(\mathbf{x}, \mathbf{z}, \boldsymbol{\lambda}) = f(\mathbf{x}) + g(\mathbf{z}) + \frac{\rho}{2} \|\mathbf{Ax} + \mathbf{Bz} + \mathbf{c} + \boldsymbol{\lambda}\|^2 + \mathbf{k}.$$

- ADMM use a Gauss-Seidel type iterative algorithm:

$$\mathbf{x}^{l+1} := \arg \min_{\mathbf{x}} L(\mathbf{x}, \mathbf{z}^l, \boldsymbol{\lambda}^l),$$

$$\mathbf{z}^{l+1} := \arg \min_{\mathbf{z}} L(\mathbf{x}^{l+1}, \mathbf{z}, \boldsymbol{\lambda}^l),$$

$$\boldsymbol{\lambda}^{l+1} := \boldsymbol{\lambda}^l + \rho(\mathbf{Ax}^{l+1} + \mathbf{Bz}^{l+1} + \mathbf{c}).$$



# Softbody Contacts Formulation

Softbody with contacts

$$\mathbf{x}_{t+1} = \arg \min_{\mathbf{x}} \frac{1}{2h^2} \underbrace{(\mathbf{x} - \tilde{\mathbf{x}})^T \mathbf{M}(\mathbf{x} - \tilde{\mathbf{x}})}_{\text{Inertia Term}} + \underbrace{U(\mathbf{x})}_{\text{Elasticity}} + \underbrace{F(\mathbf{x}, \mathbf{v})}_{\text{Contacts Potential}}$$

Introduce two auxiliary variables  $\mathbf{z}_i = \mathbf{D}_i \mathbf{x}, \mathbf{p} = \mathbf{v}$

$$\mathbf{x}_{t+1} = \arg \min_{\mathbf{x}, \mathbf{z}, \mathbf{p}} \frac{1}{2h^2} (\mathbf{x} - \tilde{\mathbf{x}})^T \mathbf{M}(\mathbf{x} - \tilde{\mathbf{x}}) + \sum_i U(\mathbf{z}_i) + F(\mathbf{p})$$

*s. t.*  $\mathbf{D}\mathbf{x} = \mathbf{z}, \mathbf{x} - \mathbf{x}_t - \mathbf{h}\mathbf{p} = \mathbf{0}$  (equation constraints)

Reform equation constraint

$$\begin{bmatrix} \mathbf{W}_e \mathbf{D} \\ \frac{1}{h} \mathbf{W}_c \end{bmatrix} \mathbf{x} + \begin{bmatrix} -\mathbf{W}_e & 0 \\ 0 & -\mathbf{W}_c \end{bmatrix} \begin{bmatrix} \mathbf{z} \\ \mathbf{p} \end{bmatrix} + \begin{bmatrix} 0 \\ -\mathbf{W}_c \frac{1}{h} \mathbf{x}_t \end{bmatrix} = \mathbf{0}$$

$$\begin{aligned} & \min_{\mathbf{x}, \mathbf{z}} f(\mathbf{x}) + g(\mathbf{z}) \\ & \text{s. t. } \mathbf{A}\mathbf{x} + \mathbf{B}\mathbf{z} + \mathbf{c} = \mathbf{0} \end{aligned}$$

ADMM Formulation

# ADMM Solver

1. Global strain propagation  $\mathbf{x}^{l+1} \leftarrow \arg \min_{\mathbf{x}} L_1$

$$L_1 = \frac{1}{2h^2} (\mathbf{x} - \tilde{\mathbf{x}})^T \mathbf{M} (\mathbf{x} - \tilde{\mathbf{x}}) + \frac{1}{2} \left| \mathbf{W}_e^{\frac{1}{2}} (\mathbf{D}\mathbf{x} - \mathbf{z}^l + \boldsymbol{\lambda}_e^l) \right|^2 + \frac{1}{2} \left| \mathbf{W}_c^{\frac{1}{2}} (\mathbf{x} - h\mathbf{p}^l - \mathbf{x}_t + \boldsymbol{\lambda}_c^l) \right|^2$$

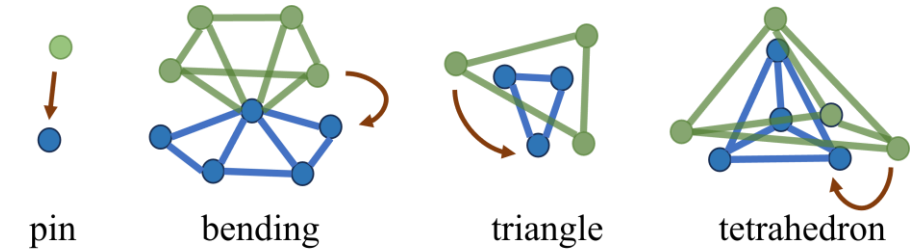
2. Local elasticity projection  $\mathbf{z}^{l+1} \leftarrow \arg \min_{\mathbf{z}} L_2$

$$L_2 = \sum_{i=1}^{n_e} U(\mathbf{z}_i) + \frac{1}{2} \left| \mathbf{W}_e^{\frac{1}{2}} (\mathbf{D}\mathbf{x} - \mathbf{z}^l + \boldsymbol{\lambda}_e^l) \right|^2$$

#m independent problems  
Solved in parallel

3. Frictional contact projection  $\mathbf{p}^{l+1} \leftarrow \arg \min_{\mathbf{p}} L_3$

$$L_3 = I_{K_\mu}(\mathbf{p}) + \frac{1}{2} \left| \mathbf{W}_c^{\frac{1}{2}} (\mathbf{x} - h\mathbf{p}^l - \mathbf{x}_t + \boldsymbol{\lambda}_c^l) \right|^2$$



4. Dual update

$$\boldsymbol{\lambda}_e^{l+1} = \boldsymbol{\lambda}_e^l + \mathbf{D}\mathbf{x}^{l+1} - \mathbf{z}^{l+1}$$

$$\boldsymbol{\lambda}_c^{l+1} = \boldsymbol{\lambda}_c^l + \mathbf{x}^{l+1} - h\mathbf{p}^{l+1} - \mathbf{x}_t$$

Simple vector addition



# ADMM Solver

1. Global strain propagation  $\mathbf{x}^{l+1} \leftarrow \arg \min_{\mathbf{x}} L_1$

$$L_1 = \frac{1}{2h^2} (\mathbf{x} - \tilde{\mathbf{x}})^T \mathbf{M} (\mathbf{x} - \tilde{\mathbf{x}}) + \frac{1}{2} \left| \mathbf{W}_e^{\frac{1}{2}} (\mathbf{D}\mathbf{x} - \mathbf{z}^l + \boldsymbol{\lambda}_e^l) \right|^2 + \frac{1}{2} \left| \mathbf{W}_c^{\frac{1}{2}} (\mathbf{x} - h\mathbf{p}^l - \mathbf{x}_t + \boldsymbol{\lambda}_c^l) \right|^2$$

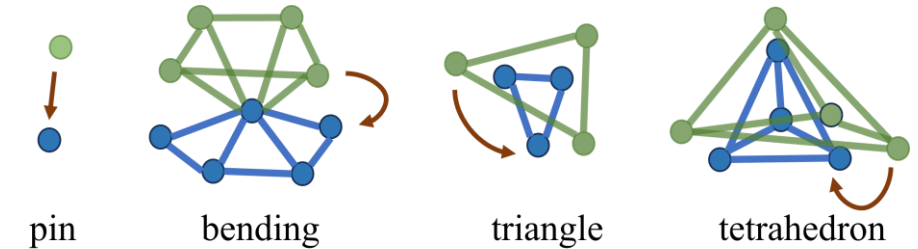
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#m independent problems  
Solved in parallel

3. Frictional contact projection  $\mathbf{p}^{l+1} \leftarrow \arg \min_{\mathbf{p}} L_3$

$$L_3 = I_{K_\mu}(\mathbf{p}) + \frac{1}{2} \left| \mathbf{W}_c^{\frac{1}{2}} (\mathbf{x} - h\mathbf{p}^l - \mathbf{x}_t + \boldsymbol{\lambda}_c^l) \right|^2$$



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$$\boldsymbol{\lambda}_e^{l+1} = \boldsymbol{\lambda}_e^l + \mathbf{D}\mathbf{x}^{l+1} - \mathbf{z}^{l+1}$$

$$\boldsymbol{\lambda}_c^{l+1} = \boldsymbol{\lambda}_c^l + \mathbf{x}^{l+1} - h\mathbf{p}^{l+1} - \mathbf{x}_t$$

Simple vector addition

# ADMM Solver

- Step 1: Global Strain Propagation: Solving a linear system

$$\mathbf{x}^{l+1} \leftarrow \arg \min_{\mathbf{x}} L_1 = \arg \min_{\mathbf{x}} \frac{1}{2h^2} (\mathbf{x} - \tilde{\mathbf{x}})^T \mathbf{M} (\mathbf{x} - \tilde{\mathbf{x}}) + \frac{1}{2} \left| \mathbf{W}_e^{\frac{1}{2}} (\mathbf{D}\mathbf{x} - \mathbf{z}^l + \boldsymbol{\lambda}_e^l) \right|^2 + \frac{1}{2} \left| \mathbf{W}_c^{\frac{1}{2}} (\mathbf{x} - \mathbf{h}\mathbf{p}^l - \mathbf{x}_t + \boldsymbol{\lambda}_c^l) \right|^2$$

First order optimal condition  $\mathbf{A}\mathbf{x} = \mathbf{b}$

$$(\mathbf{M} + h^2 \mathbf{D}^T \mathbf{W}_e \mathbf{D} + h^2 \mathbf{W}_c) \mathbf{x} = \mathbf{M}\hat{\mathbf{x}} + h^2 \mathbf{D}^T \mathbf{W}_e (\mathbf{z}^l - \boldsymbol{\lambda}_e^l) + h^2 \mathbf{W}_c (\mathbf{p}^l - \boldsymbol{\lambda}_c^l)$$

- Constant  $\mathbf{A}$ , **pre-factorization** can be applied
- Rayleigh damping
  - Our formulation  $\mathbf{f}_d = -k_d \mathbf{D}^T \mathbf{W}_e \mathbf{D} \mathbf{v}_{t+1}$
  - Final system

$$(\mathbf{M} + h^2 \mathbf{D}^T \mathbf{W}_e \mathbf{D} + h^2 \mathbf{W}_c + h k_d \mathbf{D}^T \mathbf{W}_e \mathbf{D}) \mathbf{x} = \mathbf{M}\hat{\mathbf{x}} + h^2 \mathbf{D}^T \mathbf{W}_e (\mathbf{z}^l - \boldsymbol{\lambda}_e^l) + h^2 \mathbf{W}_c (\mathbf{p}^l - \boldsymbol{\lambda}_c^l) + \mathbf{f}_d$$

# ADMM Solver


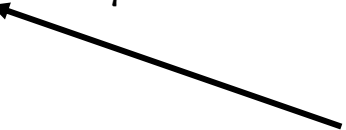
- Step3: Friction Contact Projection
  - First order optimal condition of  $L_3$  + Schur Complement

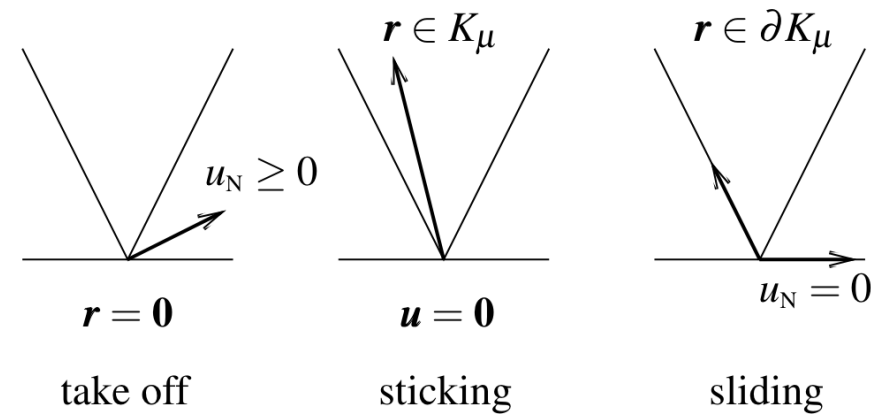
$$L_3 = I_{K_\mu}(\mathbf{p}) + \frac{1}{2} \left| \mathbf{W}_c^{\frac{1}{2}} (\mathbf{x} - \mathbf{h}\mathbf{p}^l - \mathbf{x}_t + \boldsymbol{\lambda}_c^l) \right|^2$$



## Complementary Problem

$$\begin{cases} \mathbf{u} = \mathbf{Q}\boldsymbol{\gamma}^l + \frac{1}{h} \mathbf{J}(\mathbf{x}^{l+1} - \mathbf{x}_t + \boldsymbol{\lambda}_c^l) \\ (\mathbf{u}, \boldsymbol{\gamma}) \in K_\mu \end{cases}$$

 Relative velocity    
  Contact force



Coulomb friction model

# ADMM Solver

- Step3: Friction Contact Projection
  - First order optimal condition of  $L_3$  + Schur Complement

$$L_3 = I_{K_\mu}(\mathbf{p}) + \frac{1}{2} \left| \mathbf{W}_c^{\frac{1}{2}} (\mathbf{x} - \mathbf{h}\mathbf{p}^l - \mathbf{x}_t + \boldsymbol{\lambda}_c^l) \right|^2$$




## Complementary Problem

$$\begin{cases} \mathbf{u} = \mathbf{Q}\boldsymbol{\gamma}^l + \frac{1}{h} \mathbf{J}(\mathbf{x}^{l+1} - \mathbf{x}_t + \boldsymbol{\lambda}_c^l) \\ (\mathbf{u}, \boldsymbol{\gamma}) \in K_\mu \end{cases}$$

Relative velocity

Contact force

**Delassus Operator**

$$\mathbf{Q} = \mathbf{J}\mathbf{W}_c^{-1}\mathbf{J}^T$$


sparse

$\mathbf{W}_c^{-1}$  is a diagonal matrix

# Solve the Complementary Problem

$$\begin{cases} \mathbf{u} = \mathbf{Q}\boldsymbol{\gamma}^l + \frac{1}{h}\mathbf{J}(\mathbf{x}^{l+1} - \mathbf{x}_t + \boldsymbol{\lambda}_c^l) \\ (\mathbf{u}, \boldsymbol{\gamma}) \in K_\mu \end{cases}$$

- Projected Gauss-Seidel
  - **Enumerate Method**: for Contact projection [Daviet, 2020]
    - Coulomb friction law
    - Signorini's condition
  - **Kaczmarz method**: avoid explicitly calculate Delassus operator  $\mathbf{Q}$ 
    - track  $\mathbf{p} = \mathbf{J}^T \mathbf{u}$  in time
  - **Contact stabilization**
    - Constraint Force Mixing (CFM)

PGS initialization

$$\mathbf{u}_g^{k+1} = \begin{cases} q_{g,d}\boldsymbol{\gamma}_g^k + \Sigma_o q_{g,o}\boldsymbol{\gamma}_o^l + \mathbf{b}^{l+1} & \text{if } k > 0, \\ \mathbf{J}\mathbf{p} & \text{if } k = 0. \end{cases}$$

$$\mathbf{u}_g^* = \mathbf{u}_g^{k+1} - q_{g,d}\boldsymbol{\gamma}_g^k = \mathbf{J}\mathbf{p}^k - q_{g,d}\boldsymbol{\gamma}_g^k$$

Classify the contact case (Enumerate Method)

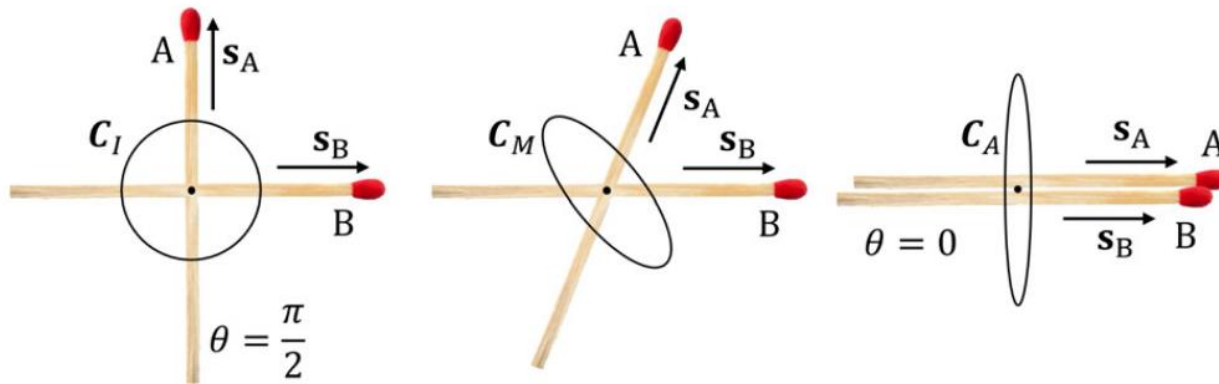
1. Separate:  $\mathbf{u}_g^* \cdot \mathbf{n} > 0 \rightarrow \mathbf{u}_g^{k+1} = \mathbf{u}_g^*$
2. Slide:  $\mathbf{u}_g^* \in K_\mu \rightarrow \mathbf{u}_g^{k+1} = \mathbf{0}$
3. Stick: not 1, 2 then  $\mathbf{u}_g^{k+1} = u_{g,T}^* + \frac{\mu |u_{g,N}^*| u_{g,T}^*}{|u_{g,T}^*|}$

Update p

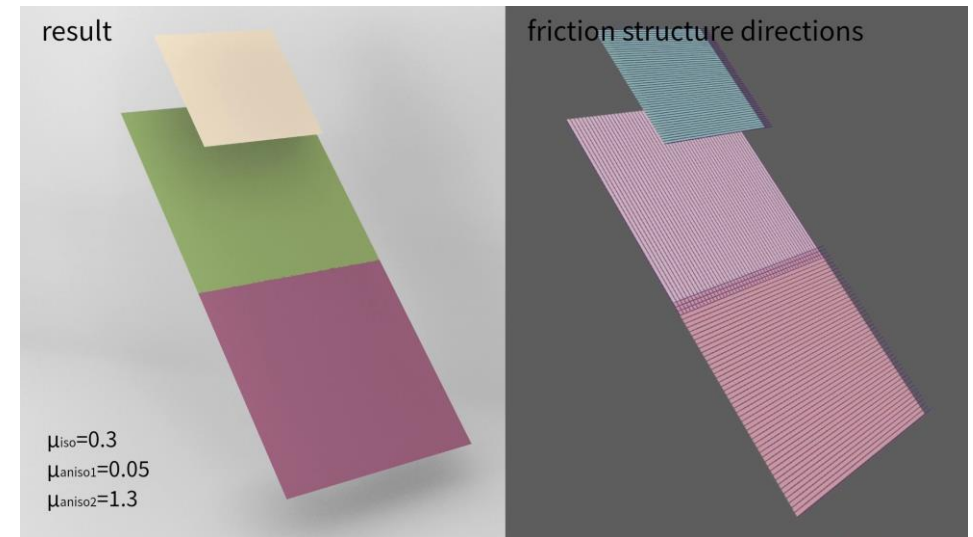
$$\mathbf{p}_i^{k+1} = \mathbf{p}_i + \frac{J_{g,i}}{w_i}(\boldsymbol{\gamma}_g^{k+1} - \boldsymbol{\gamma}_g).$$

# Anisotropic Friction

- Match Stick Model
  - Friction Cone: Conic  $K_\mu \rightarrow$  Elliptic cone  $K_{\mu_t, \mu_b}$

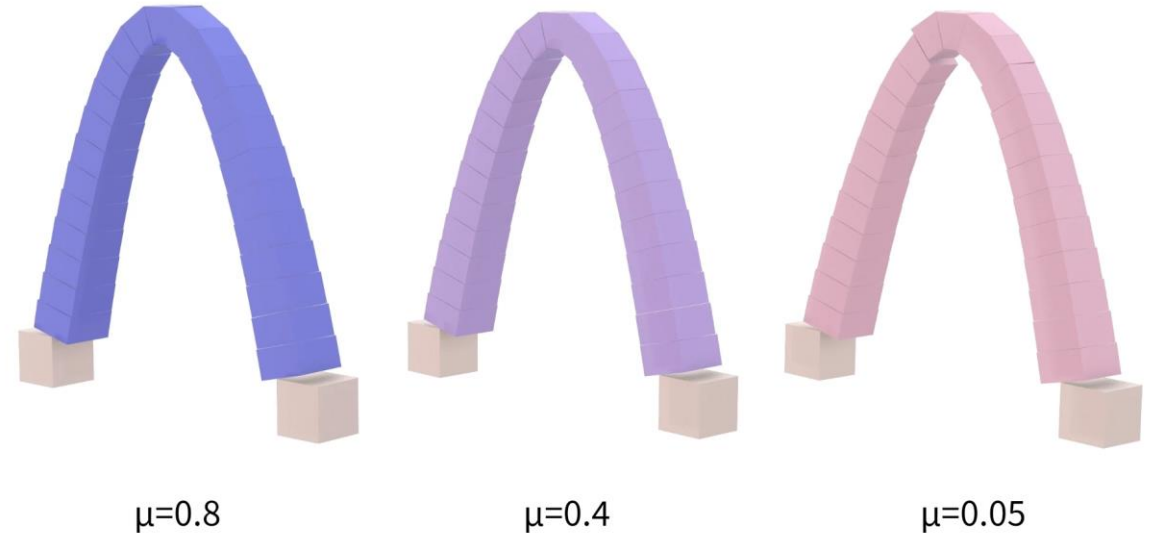
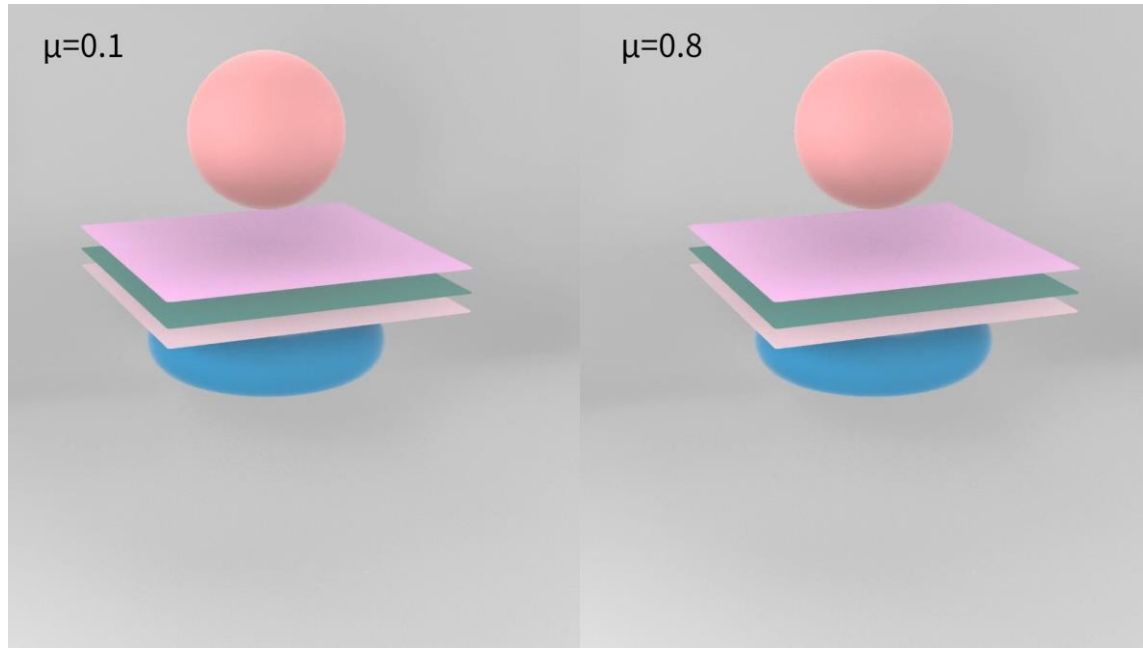


[Erleben et al. 19]



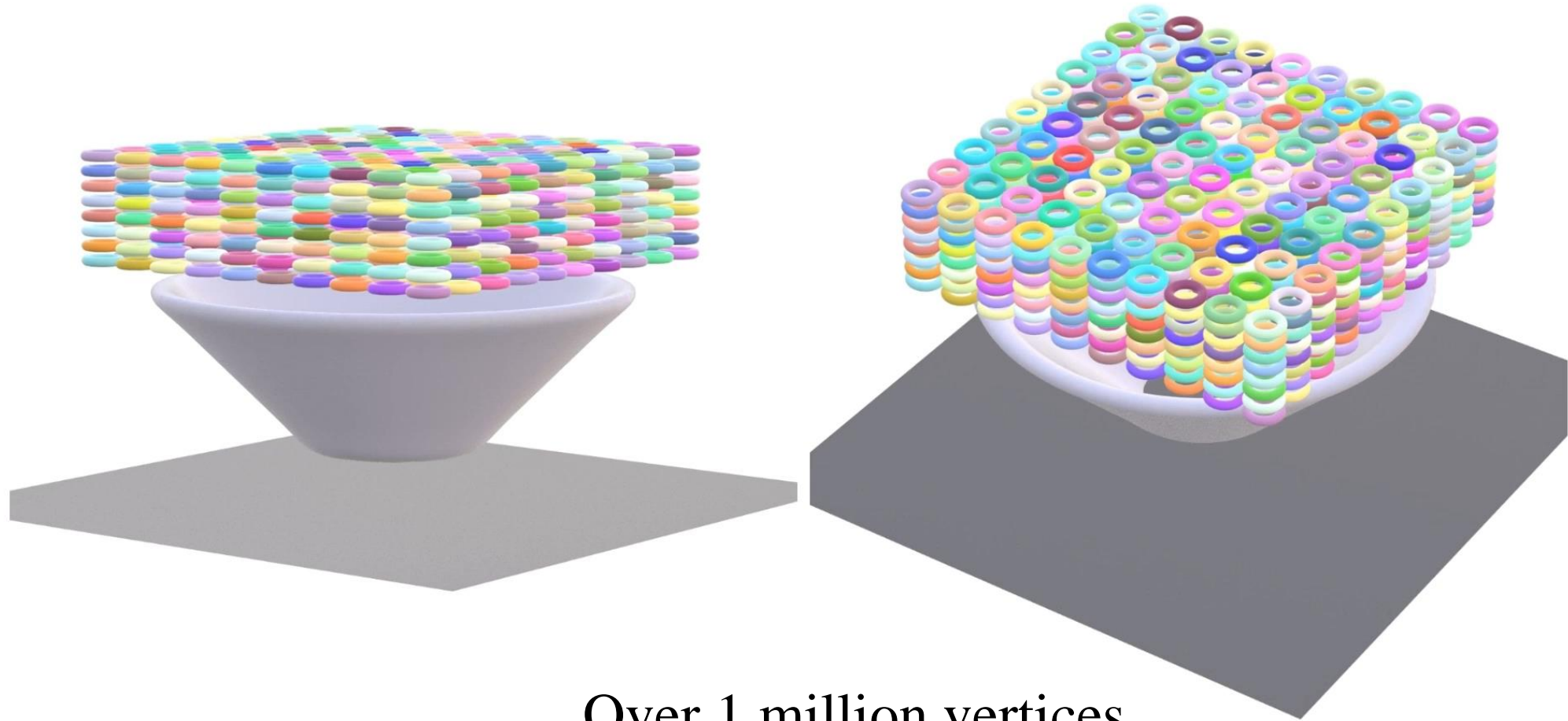
Our method with Anisotropic Friction

# Result *different friction coefficients*





# Result *large scale*



Over 1 million vertices

# Result *compare with IPC*

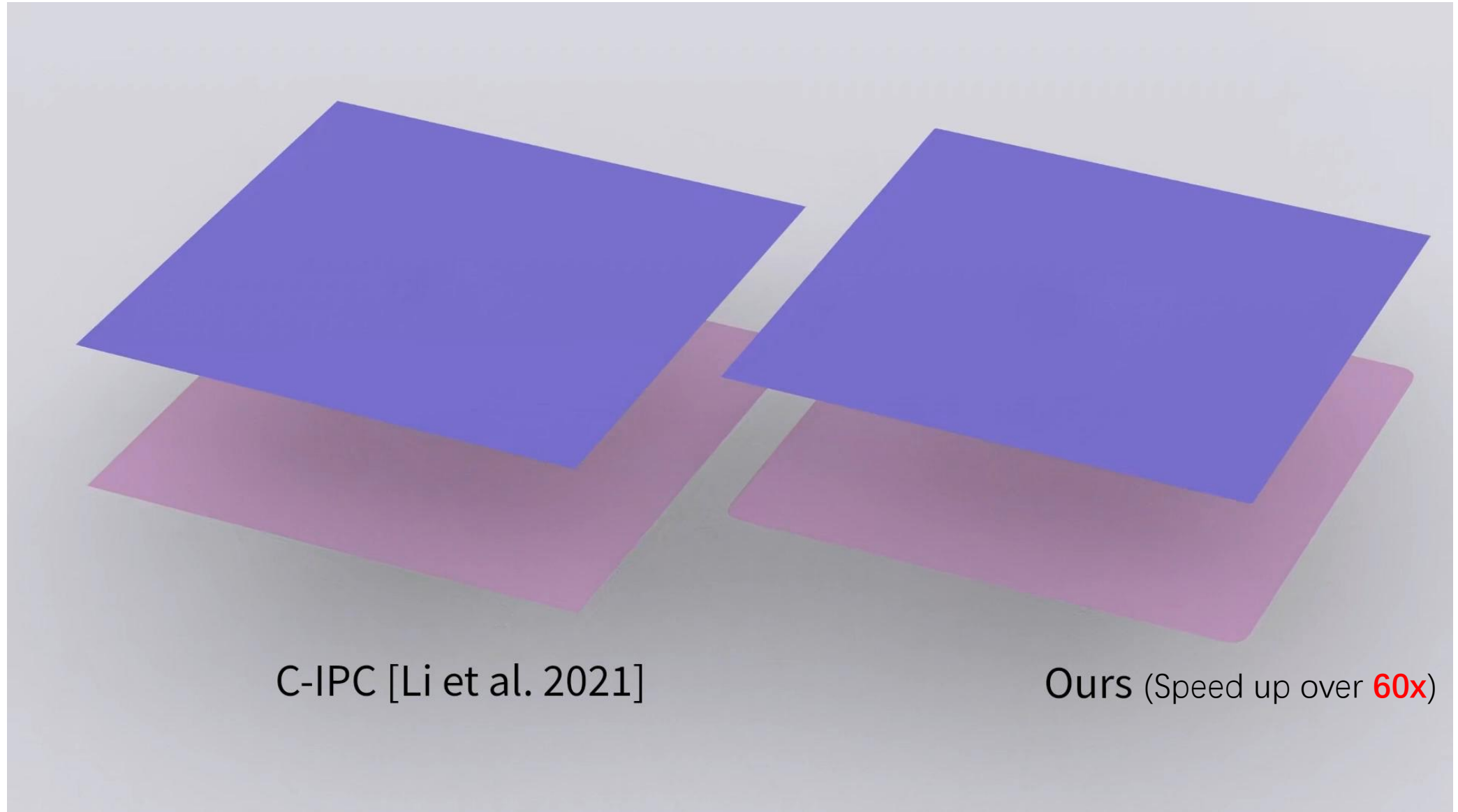


IPC[Li et al. 2020]

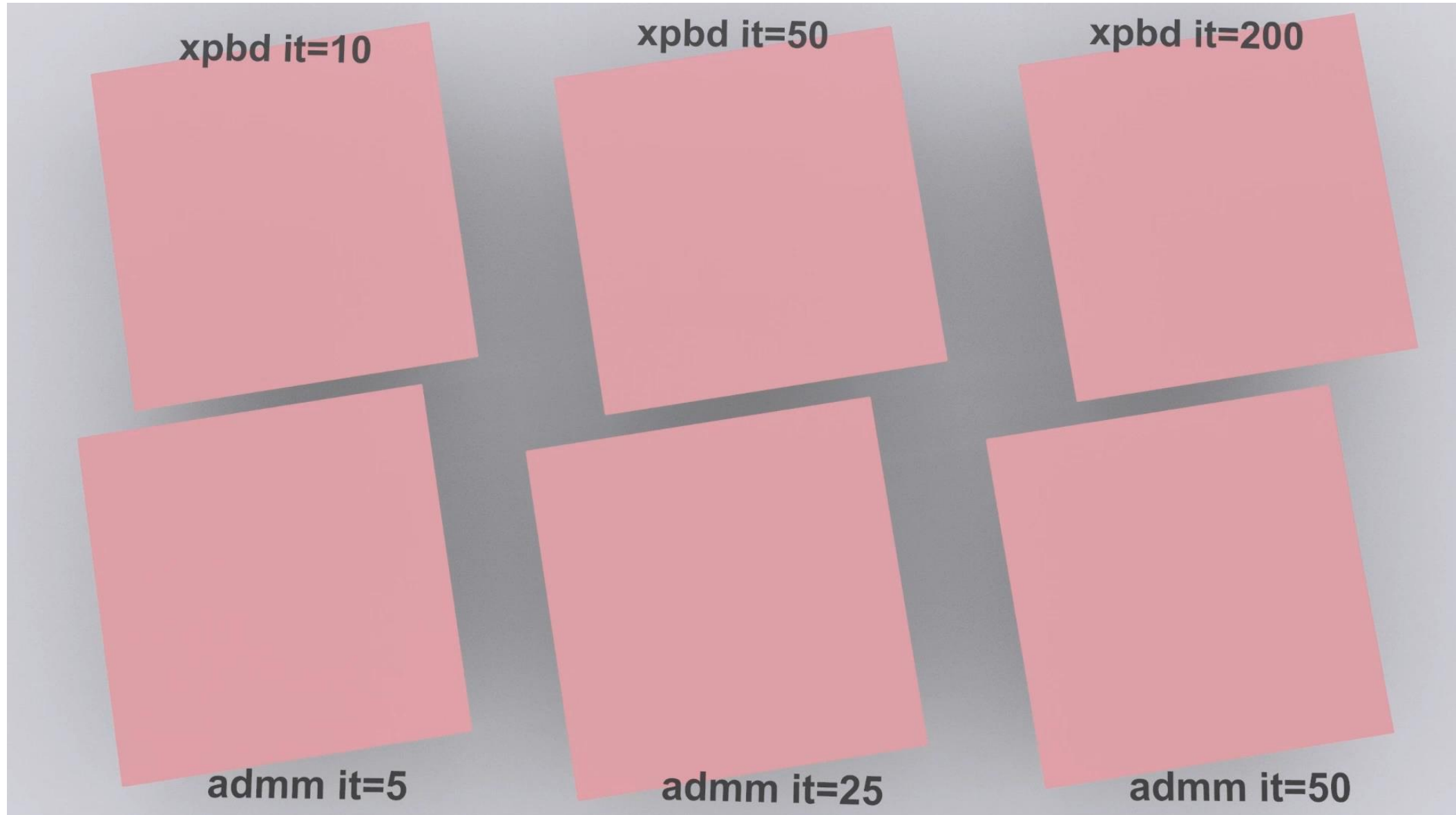


Ours (Speed up **10x**)

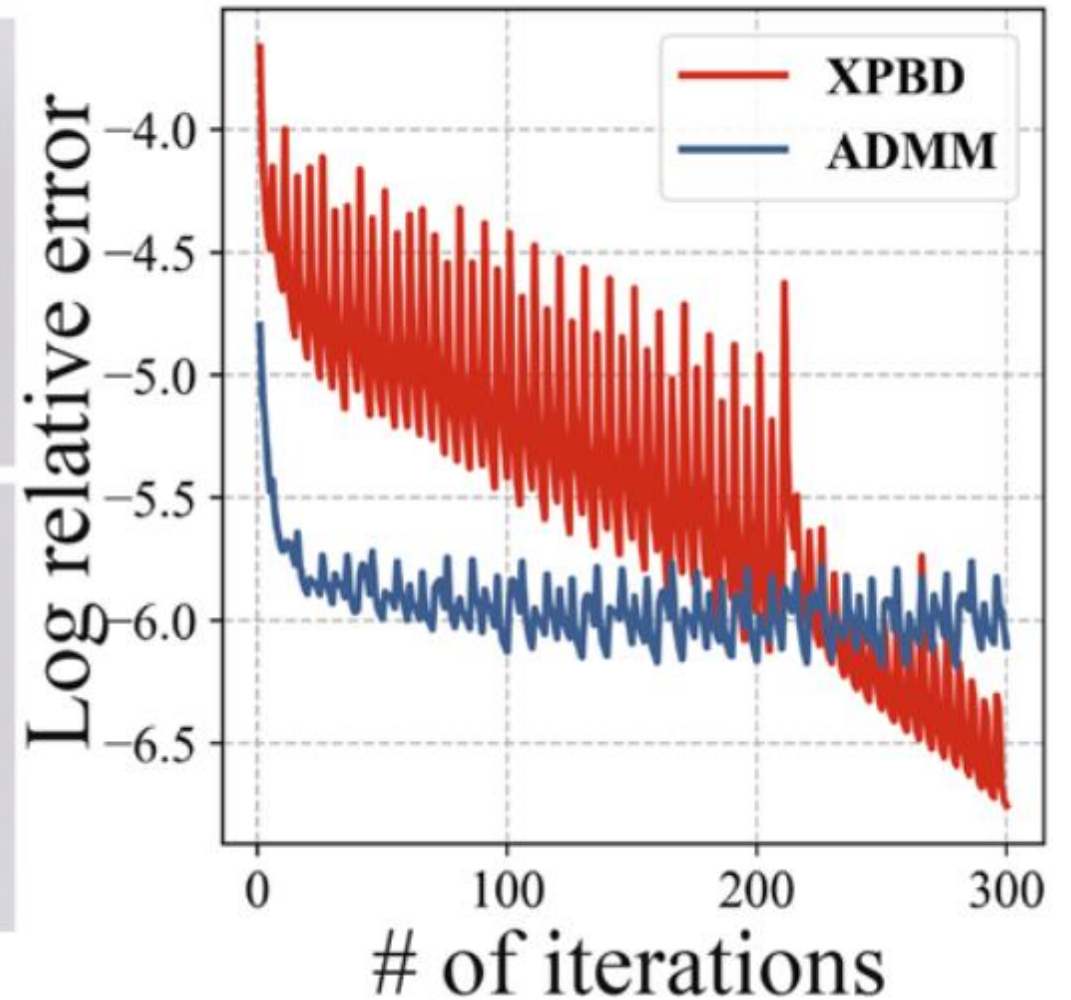
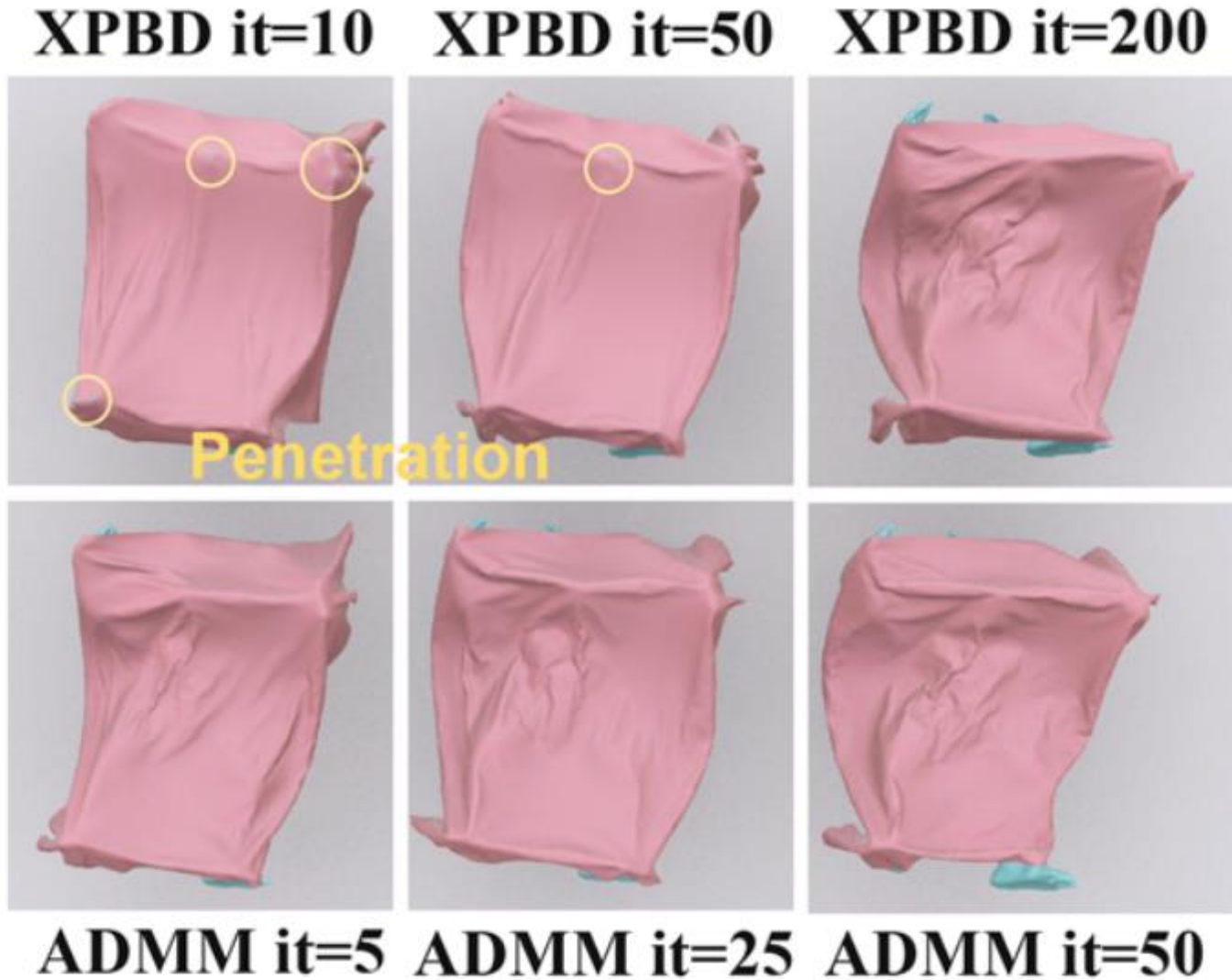
# Result *compare with C-IPC*



# Result *compare with XPBD*



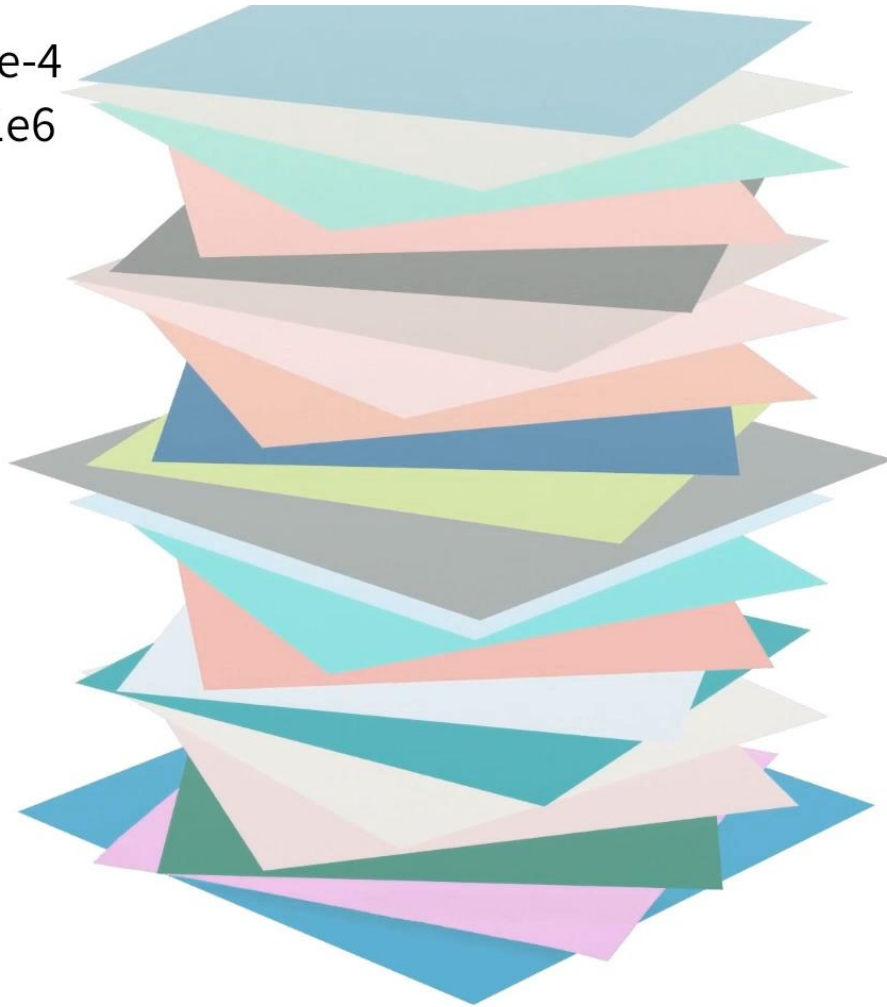
# Result *compare with XPBD*





# Result Ablation: *Contact Stabilization*

$\alpha=1e-4$   
 $k_s=1e6$

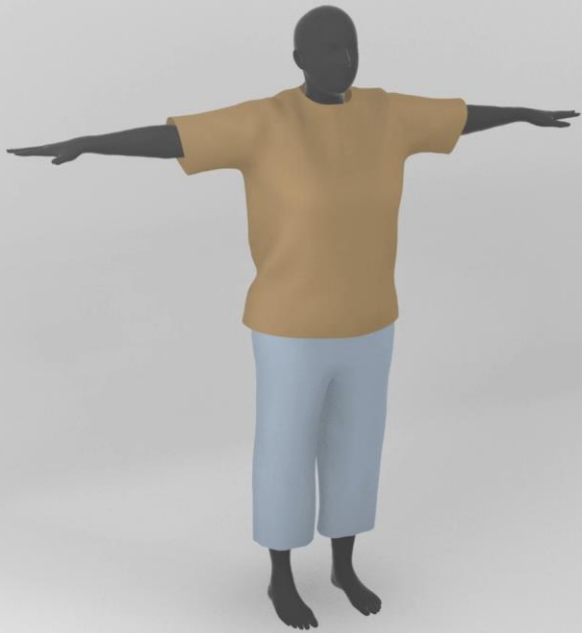


without contact stabilization



with contact stabilization

# Result *complex contact*





# Conclusion

- Introduce a novel **decoupled scheme** for soft body dynamics with frictional contacts, in the framework of ADMM, combining
  - an **efficient elasticity solver** from PD
  - a **lightweight non-Linear PGS** for contact handling
- Integrate techniques to enhance both reliability and realism
  - Matchstick anisotropic friction
  - Contact stabilization
  - Rayleigh elastic damping (with zero overhead)
- Demonstrating the effectiveness, accuracy, and computational efficiency of our solver

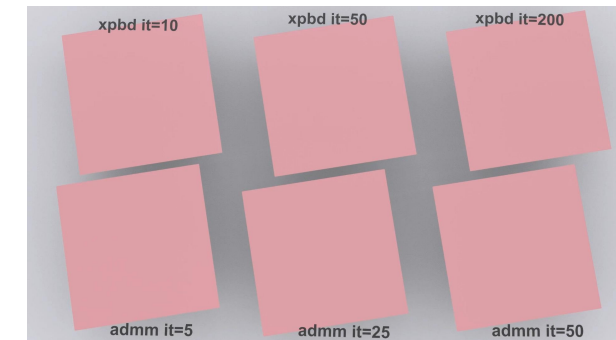
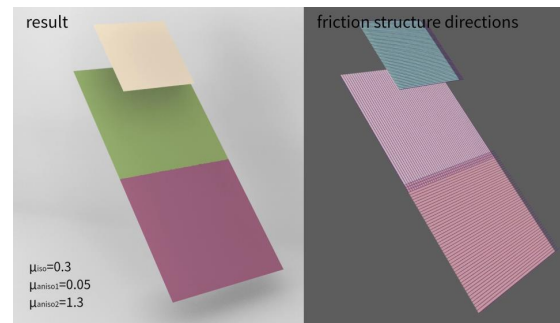
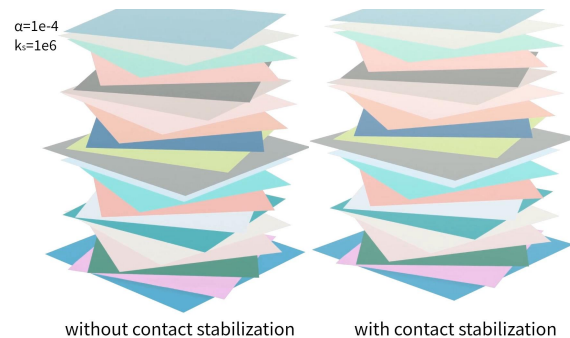
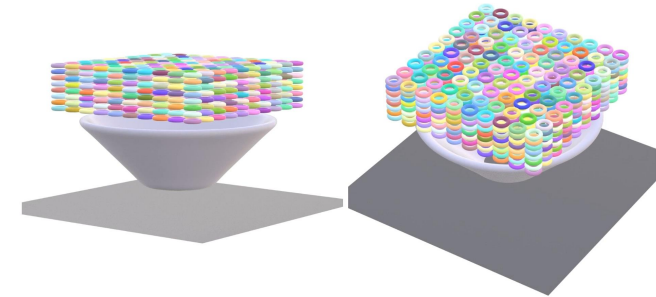
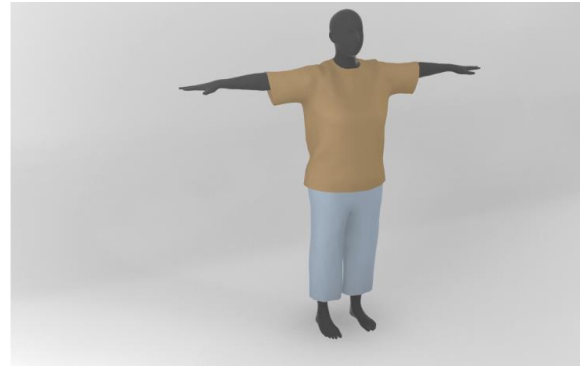
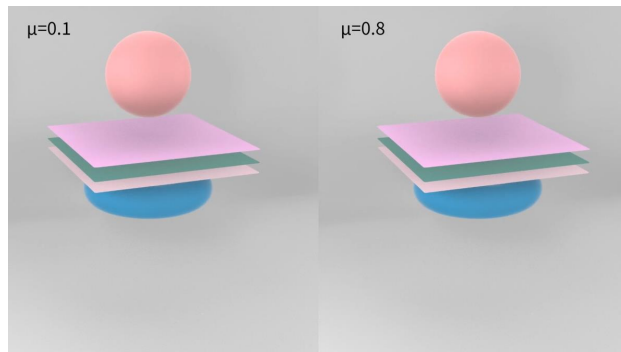
# Efficient frictional contacts for soft body dynamics via ADMM



Siyan Zhu<sup>1</sup>, Cheng Fang<sup>1</sup>, \*Peng Yu<sup>1</sup>, \*Xiao Zhai<sup>2</sup>, Aimin Hao<sup>1</sup>, \*Junjun Pan<sup>1</sup>

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wetaFX