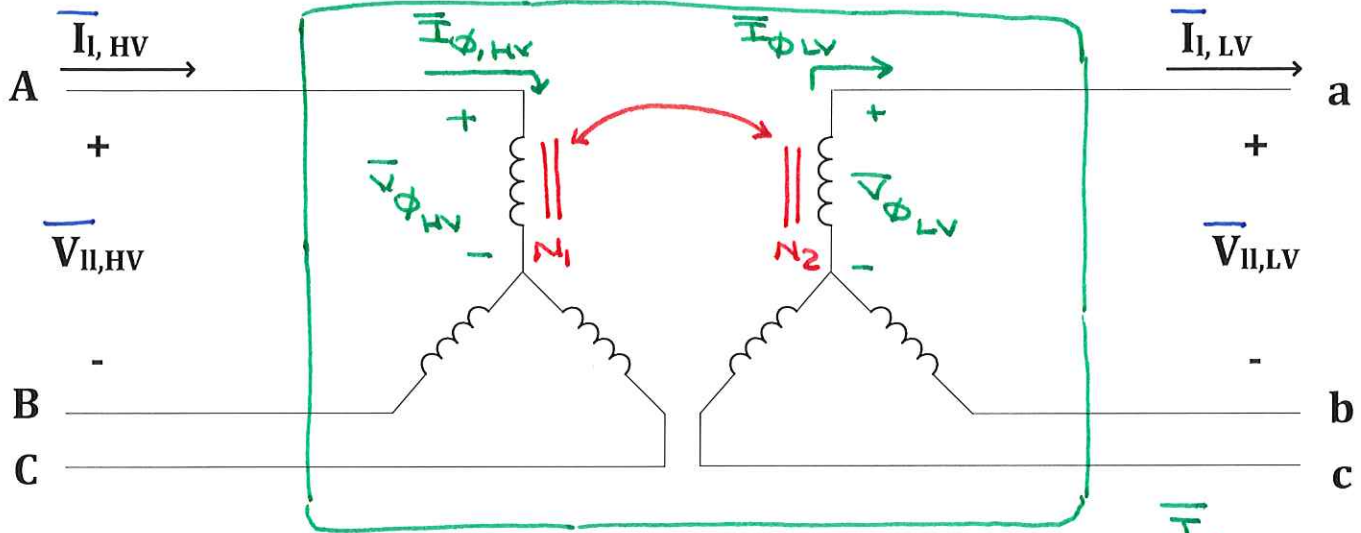


Voltage and current relationships for three phase transformers

Relationships between line-to-line voltage on either side of the transformer and line current on either side of the transformer are dependent on the winding connection type.

1) Y-Y connection



Magnetic coupling between the two winding gives:

$$\frac{\bar{V}_{\phi,HV}}{\bar{V}_{\phi,LV}} = \frac{N_1}{N_2}$$

$$\& \quad \frac{\bar{I}_{\phi,HV}}{\bar{I}_{\phi,LV}} = \frac{N_2}{N_1}$$

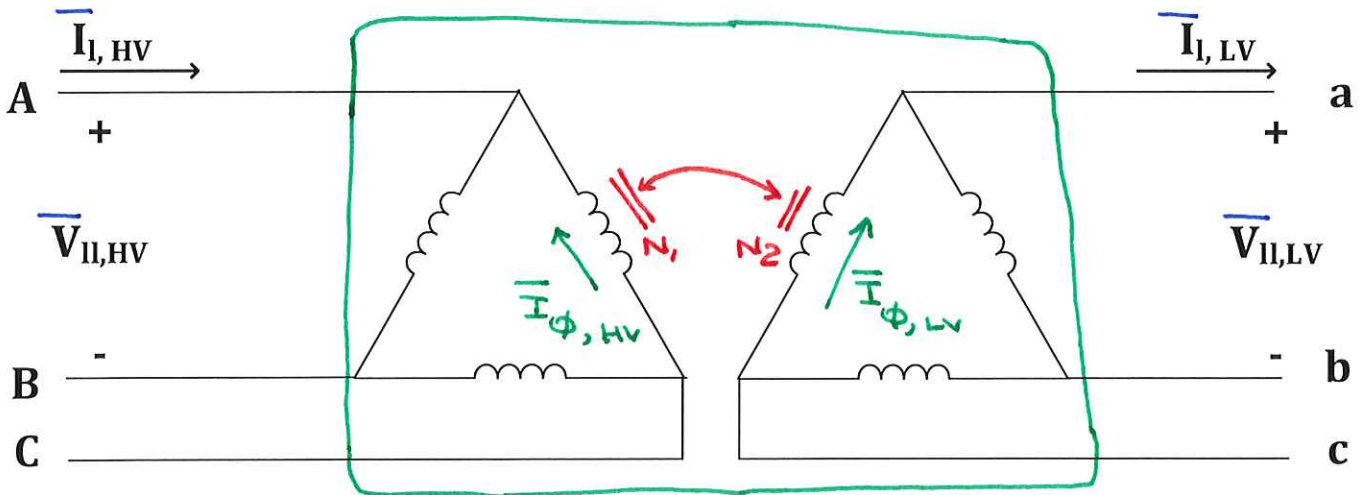
$$= \frac{\bar{I}_{e,HV}}{\bar{I}_{e,LV}}$$

in Y, $\bar{I}_{\phi} = \bar{I}_e$

Also know that, in both sides, $\bar{V}_{ll} = \sqrt{3} \angle 30^\circ \bar{V}_{ln}$ therefore,

$$\frac{\bar{V}_{ll,HV}}{\bar{V}_{ll,LV}} = \frac{N_1}{N_2}$$

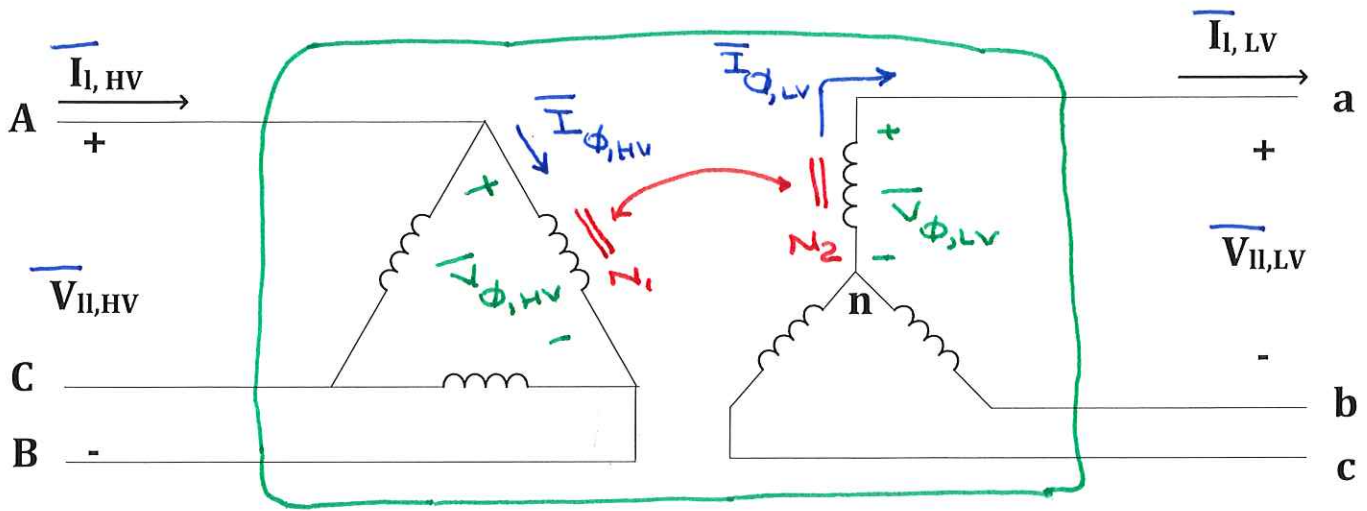
2) Δ-Δ connection



Similar to Y-Y, $\frac{\bar{V}_{ll,HV}}{\bar{V}_{ll,LV}} = \frac{N_1}{N_2}$

$$\& \quad \frac{\bar{I}_{l,HV}}{\bar{I}_{l,LV}} = \frac{N_2}{N_1}$$

3) Δ-Y Connection



Magnetic coupling between the two winding gives: $\frac{\bar{V}_{\phi,HV}}{\bar{V}_{\phi,LV}} = \frac{N_1}{N_2}$ & $\frac{\bar{I}_{\phi,HV}}{\bar{I}_{\phi,LV}} = \frac{N_2}{N_1}$

Also, from Δ and Y connection properties: $\bar{V}_{LL,LV} = \sqrt{3} \angle 30^\circ \cdot \bar{V}_{\phi,LV}$ & $\bar{V}_{LL,HV} = \bar{V}_{\phi,HV}$

Therefore, $\frac{\bar{V}_{LL,HV}}{\bar{V}_{LL,LV}} = \frac{\bar{V}_{\phi,HV}}{\sqrt{3} \angle 30^\circ \cdot \bar{V}_{\phi,LV}} = \frac{N_1}{N_2 \cdot \sqrt{3}} \angle -30^\circ$

- The ratio of line-to-line voltage magnitudes is $\frac{N_1}{N_2 \cdot \sqrt{3}}$
- Line-to-line voltage on the Δ side lags line-to-line voltage on the Y side by 30°

Similarly, $\frac{\bar{I}_{L,HV}}{\bar{I}_{L,LV}} = \frac{N_2 \cdot \sqrt{3}}{N_1} \angle -30^\circ$

4) Y-Δ Connection

We can show that:

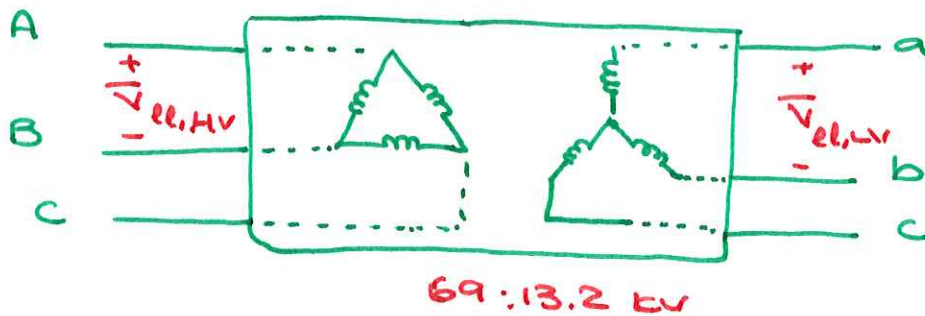
$$\frac{\bar{V}_{LL,HV}}{\bar{V}_{LL,LV}} = \frac{\sqrt{3} \cdot N_1}{N_2} \angle 30^\circ$$

$$\frac{\bar{I}_{L,HV}}{\bar{I}_{L,LV}} = \frac{N_2}{\sqrt{3} \cdot N_1} \angle 30^\circ$$

- Instead of dealing with turns ratios, we will only use the line-to-line voltage ratios for txfrs:

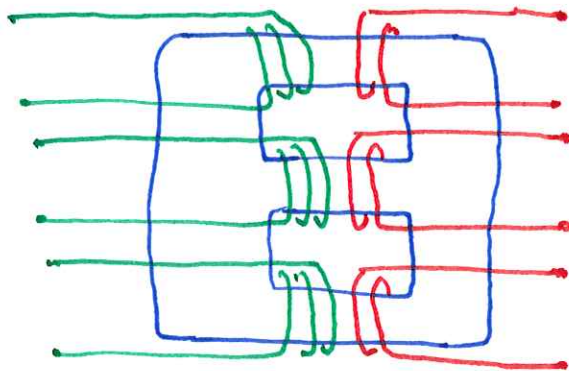
e.g: 69:13.2 kV Δ Y \leftarrow

- rated voltage of txfr
- ratio of line-line voltages



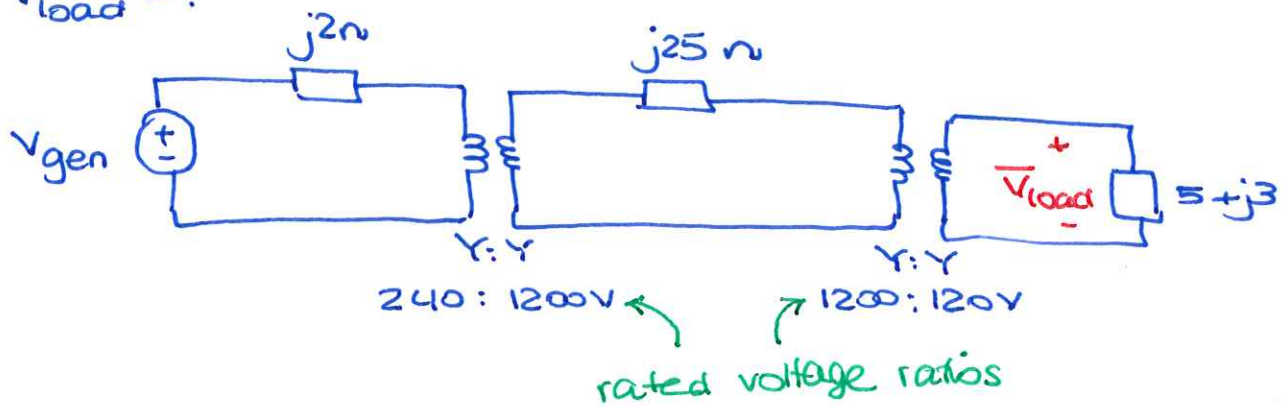
if operating voltage on HV side $\sqrt{3} V_{ll, HV} = 72$ kV,
 then operating voltage on LV side, $\sqrt{3} V_{ll, LV} = 72 \times \frac{13.2}{69} = 13.8$ kV

- Typically, 3 ϕ transformers are constructed such that all windings share a common core:



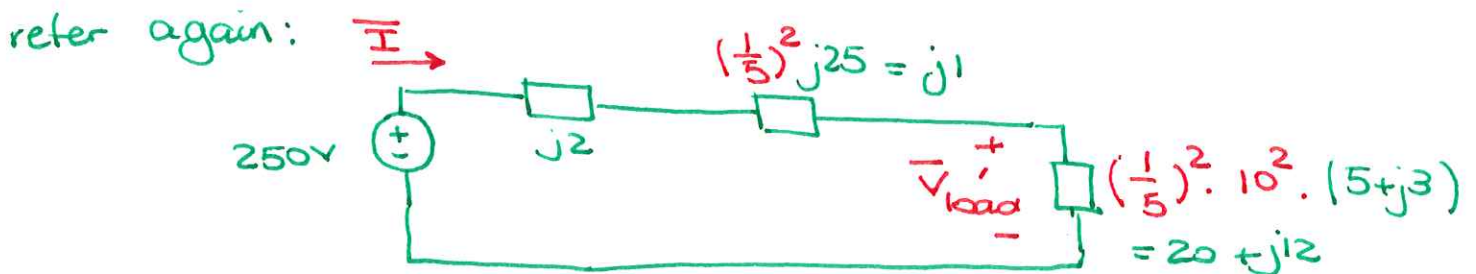
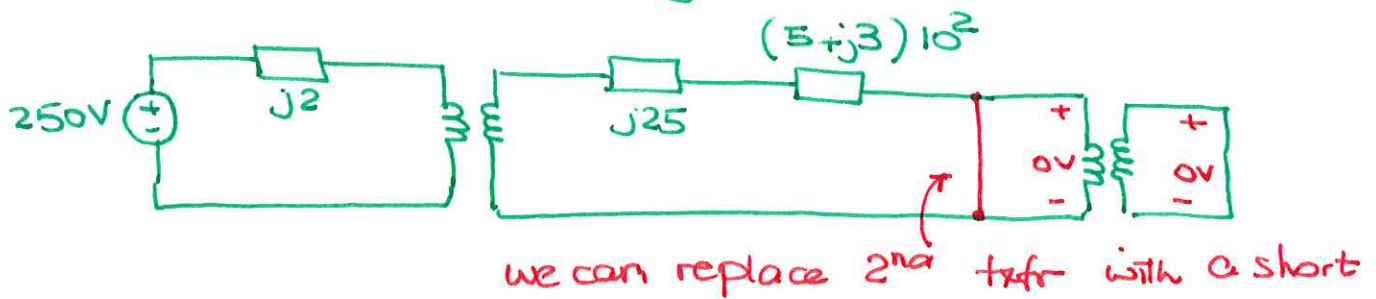
Example: Single ϕ circuit for a 3ϕ system; i.e. Source & load already converted to equivalent Y . If $V_{gen} = 250V$, $\bar{S}_{load} = ?$

$$\bar{V}_{load} = ?$$



Strategy:

- refer all impedances to one side
- Solve circuit
- Go back to orig circuit



$$\bar{I} = \frac{250}{j2 + j1 + (20 + j12)} = 10 \angle -37^\circ \text{ A}$$

$$\bar{V}'_{load} = \bar{I} (20 + j12) = 233.2 \angle -6^\circ \text{ V}$$

$$\bar{S}_{load} = \bar{V}'_{load} \cdot \bar{I}^* = 2332 \angle 3^\circ \text{ VA}$$

• To find \overline{V}_{load} in the orig circuit:

$$\overline{V}_{load} = \overline{V}'_{load} \times \frac{1200}{240} \times \frac{120}{1200} = 116.6 \angle -6^\circ \text{ V}$$

this is V_{e-n} since this is a 1 ϕ analysis

$$V_{e-e} = \sqrt{3} V_{e-n}$$

• \overline{S}_{load} is the same in the orig circuit

(\overline{V}_{load} is $\frac{\overline{V}'_{load}}{2}$ but \overline{I}_{load} is $\overline{I} \times 2$)

this is 1 ϕ power. $\overline{S}_{load, 3\phi} = 3 \times \overline{S}_{load, 1\phi}$

• Yikes! There is too much work dealing with multiple voltage levels (and 1 ϕ vs. 3 ϕ quantities).

Help is on the way: Topic 4.

Topic 4: Per Unit Analysis

- Idea: Normalize / scale magnitudes of all variables (voltage, current, power, impedance) in the power system based on the txfr ratios so we can remove idea: txfr from the analysis.

$$\text{Quantity in per unit} = \frac{\text{actual value}}{\text{base value}}$$

- or, multiply by 100% to express as %

- the base quantities are related to each other by standard power equations:

For single phase systems:

$$I_{\text{base}} = \frac{S_{\text{base}, 1\phi}}{V_{\text{base}, \text{LN}}}$$

← from $S_{1\phi} = I \cdot V_{\text{LN}}$

$$Z_{\text{base}} = \frac{V_{\text{base}, \text{LN}}}{I_{\text{base}}}$$

← all voltages are LN in 1 ϕ

← from $V_{\text{LN}} = I \cdot Z$

$$= \frac{V_{\text{base}, \text{LN}}^2}{S_{\text{base}}}$$

$$R_{\text{base}} = X_{\text{base}} = Z_{\text{base}}$$

$$Y_{\text{base}} = \frac{1}{Z_{\text{base}}}$$

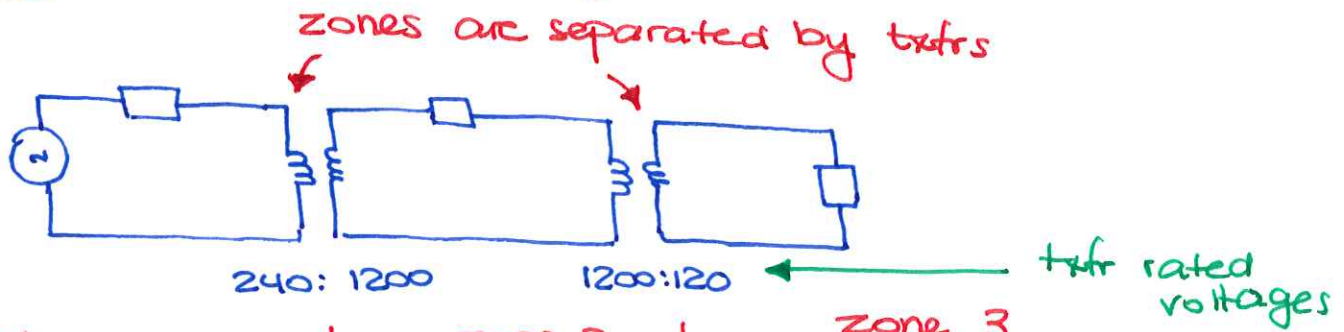
$$S_{\text{base}, 1\phi} = P_{\text{base}, 1\phi} = Q_{\text{base}, 1\phi}$$

Conversion Procedure (To analyze a 1 ϕ system using P.u.)

- 1) Pick an S_{base} for entire system. e.g. $S_{base} = 100 \text{ mVA}$
 - all base values are real numbers
 - P.u. only affects magnitudes, not phase angles.

- 2) Pick a V_{base} for one voltage level/zone.

V_{base} values are related by ~~txfr~~ voltage ratios



we can select $V_{base_1} = 240 \text{ V}$

good idea/practice to choose V_{base} to be the same as nominal/rated voltage.

$$\begin{aligned} V_{base_2} &= V_{base_1} \times \underbrace{\frac{1200}{240}}_{\text{txfr ratio}} \\ &= 1200 \text{ V} \end{aligned}$$

$$\begin{aligned} V_{base_3} &= V_{base_2} \times \frac{120}{1200} \\ &= 120 \text{ V} \end{aligned}$$

- 3) Calculate Z_{base} for each zone.

$$Z_{base} = \frac{V_{base}^2}{S_{base}}$$

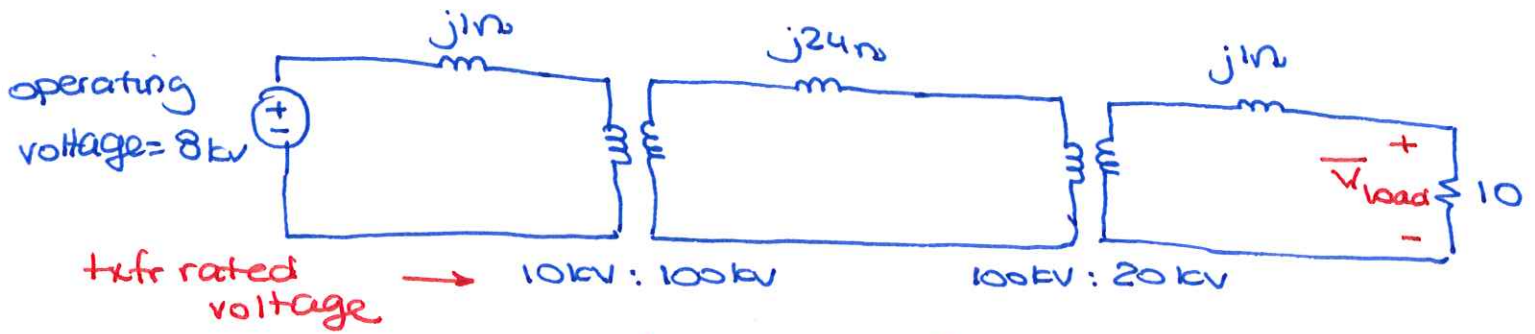
- 4) Calculate I_{base} for each zone.

$$I_{base} = \frac{S_{base}}{V_{base}}$$

- 5) Convert actual values to P.u.

- After conversion,
 - Solve the P.u. circuit. Obtain P.u. voltage, current, power
 - Convert to actual quantity by multiplying P.u. values by S_{base} , V_{base} , I_{base}

Ex: Calculate load voltage, current, power. Use $S_{base} = 100 \text{ MVA}$
 & $V_{base} = 8 \text{ kV}$ in gen zone.



$$V_{base_1} = 8 \text{ kV} \quad (\text{given})$$

$$Z_{base_1} = \frac{(V_{base_1})^2}{S_{base}} = 0.64 \, \Omega$$

zone 1

zone 2

$$V_{base_2} = V_{base_1} \times \frac{100 \text{ kV}}{10 \text{ kV}} = 80 \text{ kV}$$

$$Z_{base_2} = \frac{(V_{base_2})^2}{S_{base}} = 64 \, \Omega$$

$$V_{base_3} = V_{base_2} \times \frac{20 \text{ kV}}{100 \text{ kV}} = 16 \text{ kV}$$

$$Z_{base_3} = \frac{(V_{base_3})^2}{S_{base}} = 2.56 \, \Omega$$

$$I_{base_3} = \frac{S_{base}}{V_{base_3}} = 6.25 \text{ kA}$$