

1. $\epsilon_r = 9$
 $\sigma = 0$
 $\mu_r = 1$

$$\vec{H}(y,t) = 33 \cos(\omega t - 20y) \vec{a}_z$$

a) $v_p = \omega / \beta$
 $= \frac{\omega}{\omega \sqrt{\mu_r \mu_0 \epsilon_r \epsilon_0}}$
 $= \frac{1}{\sqrt{9 \mu_0 \epsilon_0}}$
 $= \frac{3e^8}{3}$

$$v_p = 1e^8 \text{ m/s}$$

b) $f = ?$

$$\beta = \omega \sqrt{\mu_r \mu_0 \epsilon_r \epsilon_0}$$

$$20 = 2\pi f \frac{\beta}{3e^8}$$

$$\frac{20e^8}{2\pi} = f$$

$$f = \frac{1e^9}{\pi}$$

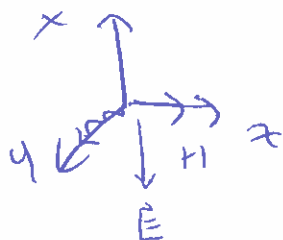
$$f = 3.2 \times 10^8 \text{ Hz}$$

$$f = 0.32 \text{ GHz}$$

c) $n = \sqrt{\frac{\mu_r \mu_0}{\epsilon_r \epsilon_0}}$
 $= \sqrt{\frac{\mu_0}{9 \epsilon_0}}$
 $= 40\pi$

$$\vec{E}(y,t) = (33)(40\pi) \cos(2 \times 10^9 t - 20y) \vec{a}_x$$

$$\vec{E}(y,t) = -1320\pi \cos(2 \times 10^9 t - 20y) \vec{a}_x$$



$E \times H \rightarrow \text{dir'n of prop}$

2. $\vec{E}(x,t) = 10 e^{-250z} \cos(2\pi \times 10^9 t - 250z) \vec{a}_y \text{ mV/m}$

$\rightarrow \mu_r = 1$

$\rightarrow \alpha = 250$
 $\beta = 250$ } good conductor assumption

(check: $\gamma = \frac{2\pi}{\lambda} \rightarrow \lambda = 2.51 \text{ cm} + \delta = \frac{1}{\alpha} \rightarrow \delta = 4 \text{ mm}$)

2. cont'd

(2)

→ ∴ wave attenuated by ~ 33% over 4mm & $l = 2.51\text{cm}$
 ⇒ rapid attenuation & good conductor approx. ok

$$n = \sqrt{\frac{\omega\mu}{\sigma}} \angle 45^\circ$$

$$\rightarrow \sigma = ?$$

$$|n| = \sqrt{\frac{(2\pi \times 10^9)(4\pi \times 10^{-7})}{15.8}}$$

$$= 22.35$$

$$\alpha = \beta = \sqrt{\pi f \mu \sigma}$$

$$250 = \sqrt{(1\pi)(10^9)(4\pi \times 10^{-7})\sigma}$$

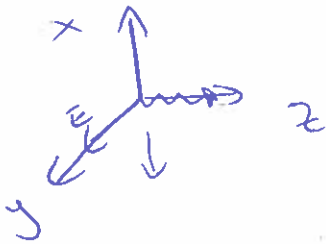
$$250 = \sqrt{(4\pi^2)(100)\sigma}$$

$$250 = 20\pi \sqrt{\sigma}$$

$$\boxed{\sigma = 15.8 \text{ S/m}}$$

$$\vec{H}(z,t) = -\frac{10}{22.35} e^{-250z} \cos(2\pi \times 10^9 t - 250z - \frac{\pi}{4}) \hat{a}_x$$

$$= -0.45 e^{-250z} \cos(2\pi \times 10^9 t - 250z - \frac{\pi}{4}) \hat{a}_x \text{ mA/m}$$



3. $f = 800\text{MHz}$
 $\epsilon_r = 2.5$
 $\mu_r = 1$
 $\sigma = 0$
- $|\vec{E}| = 1.0\text{V/m}$ @ inner surface of slab
 & oriented in y , propagates in z .

$$a) \vec{E}(z,t) = 1 \cos(\omega t - \beta z) \hat{a}_y$$

$$\omega = (2\pi)(8 \times 10^8)$$

$$= 1.6\pi \times 10^9$$

$$\beta = \omega \sqrt{\mu_r \mu_0 \epsilon_r \epsilon_0}$$

$$= \frac{1.6\pi \times 10^9}{3 \times 10^8} \sqrt{2.5}$$

$$= 26.5 \text{ rad/m}$$

3 a) $\vec{E}(z,t) = \cos(1.6\pi \times 10^9 t - 26.5z) \vec{a}_y$ V/m (3)

b) $n = \sqrt{\frac{\mu_0}{2.5\epsilon_0}}$
 $= 238.4$



$\vec{H}(z,t) = -4.2 \cos(1.6\pi \times 10^9 t - 26.5z) \vec{a}_x$ mA/m

c) $\vec{P}_{AV}(z) = \frac{|\vec{E}_m|^2}{2n} \vec{a}_z$
 $= \frac{1}{2(238.4)} \vec{a}_z$

$\vec{P}_{AV}(z) = 0.1 \vec{a}_z$ mW/m²

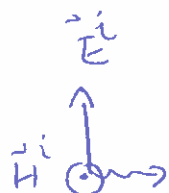
Alt

$\vec{P}_{AV} = \frac{1}{2} \text{Re} \{ \vec{E}_s \times \vec{H}_s^* \}$
 $= \frac{1}{2} \text{Re} \{ e^{-j26.5z} \vec{a}_y \times -4.2e^{j26.5z} \vec{a}_x \}$
 $\uparrow \times 10^{-3}$

$= \frac{1}{2} \text{Re} \{ -4.2 \times 10^{-3} \vec{a}_y \times \vec{a}_x \}$
 $= 0.1 \times 10^{-3} \vec{a}_z \times$

4. $\vec{E}(z,t) = 8\pi \cos(2\pi \times 10^8 t - \beta_1 z) \vec{a}_x$

$\epsilon_r = 4$
 $\mu_r = 1$
 $\sigma = 0$



$\epsilon_r = 16$
 $\mu_r = 3$
 $\sigma = 0.05$

$\frac{\sigma}{\omega\epsilon} = \frac{0.05}{(2\pi \times 10^8)(16)(8.85 \times 10^{-12})}$
 $= 0.562 \Rightarrow$ full formulas

$\alpha_2 = 3.94$ Np/m

$\beta_2 = 15.04$ rad/m

$m = 158.35 \pm 0.256$ rad

$n_i = \sqrt{\frac{\mu_0}{4\epsilon_0}}$
 $= 60\pi$
 $\beta_1 = \omega \sqrt{\mu_0 \epsilon_r \epsilon_0}$
 $= \frac{2\pi \times 10^8}{3 \times 10^8} \sqrt{4}$
 $= \frac{4\pi}{3}$

$\vec{H}^i(z,t) = 0.13 \cos(2\pi \times 10^8 t - \frac{4\pi}{3} z) \vec{a}_y$

(4)

4. cont'd

$$\hookrightarrow \phi = \frac{n_2 - n_1}{n_2 + n_1}$$

$$= 0.167 \text{ \& } 2.27 \text{ rad}$$

$$\hookrightarrow T = \frac{2n_2}{n_1 + n_2}$$

$$= 0.902 \text{ \& } 0.14 \text{ rad}$$

$$b) \quad \vec{E}^r(z, t) = \overset{|r|}{(0.167)(8\pi)} \cos(\overset{\phi}{2\pi \times 10^8 t + \frac{4\pi}{3}z + 2.27}) \vec{a}_x$$

$$= 4.2 \cos(2\pi \times 10^8 t + \frac{4\pi}{3}z + 2.27) \vec{a}_x$$

$$c) \quad \vec{H}^r(z, t) = 0.022 \cos(2\pi \times 10^8 t + \frac{4\pi}{3}z + 2.27) \vec{a}_y$$

$$d) \quad \vec{E}^t(z, t) = \overset{|T|}{(0.902)(8\pi)} e^{-3.94z} \cos(2\pi \times 10^8 t - 15.04z + 0.14) \vec{a}_x$$

$$\vec{E}^t(z, t) = 22.67 e^{-3.94z} \cos(2\pi \times 10^8 t - 15.04z + 0.14) \vec{a}_x$$

$$e) \quad \vec{H}^t(z, t) = \frac{22.67}{152.35} e^{-3.94z} \cos(2\pi \times 10^8 t - 15.04z + 0.14 - 0.256) \vec{a}_y$$

$$\vec{H}^t(z, t) = 0.149 e^{-3.94z} \cos(2\pi \times 10^8 t - 15.04z - 0.116) \vec{a}_y$$

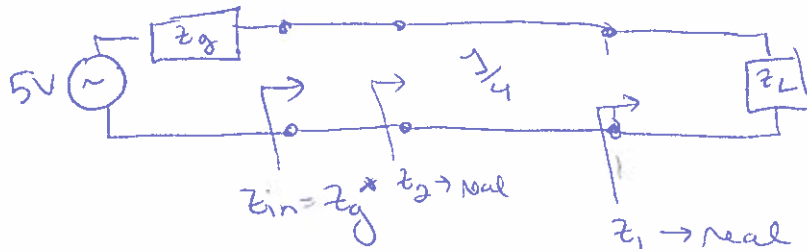
5. $V_g = 5V$

(5)

$$Z_g = 75 - j20 \Omega$$

$$Z_0 = 50 \Omega$$

$$Z_L = 20 + j70 \Omega$$



→ for maximum power transfer, we want

$$Z_{in} = Z_g^*$$

$$\therefore Z_{in} = 75 + j20 \Omega$$

→ We want to use a $\frac{1}{4}$ transformer

\therefore need real values of impedance at each end

\Rightarrow move towards load from Z_{in} to obtain real value (Z_2)

\Rightarrow move towards generator to obtain real value (Z_1)

\Rightarrow use $Z_1 + Z_2$ to design $\frac{1}{4}$ tx.

$$Z_{in} \Rightarrow \frac{75}{50} + j\frac{20}{50}$$

$$Z_{in} = 1.5 + j0.4$$

$$Z_L \Rightarrow \frac{20}{50} + j\frac{70}{50}$$

$$Z_L = 0.4 + j1.4$$

5. cont'd:

(6)

$$Z_{in} \rightarrow 0.6 = Z_2 \Rightarrow \text{rotate from } (0.292 \rightarrow 0.5) \text{ J}$$

$$\text{distance} = (0.5 - 0.292) \text{ J} \\ = 0.208 \text{ J}$$

$$Z_L \rightarrow 7.5 = Z_1 \Rightarrow \text{rotate from } (0.156 \text{ to } 0.25) \text{ J}$$

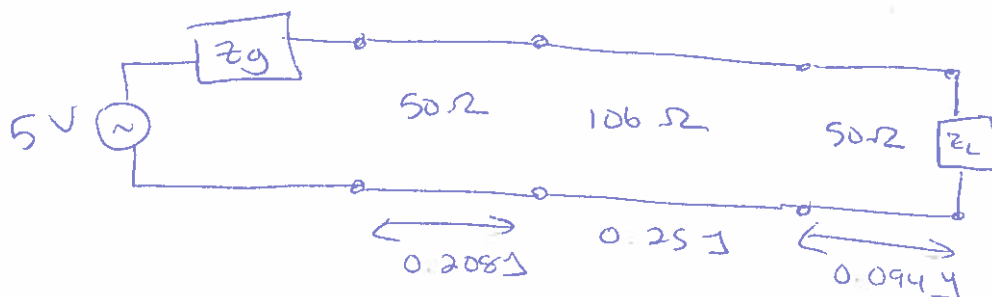
$$\text{distance} = (0.25 - 0.156) \text{ J} \\ = 0.094 \text{ J}$$

(could also rotate $(0.094 + 0.25) \text{ J}$
to $Z_1 = 0.13$)

$$Z_2 = (0.6)(50) \\ = 30 \Omega$$

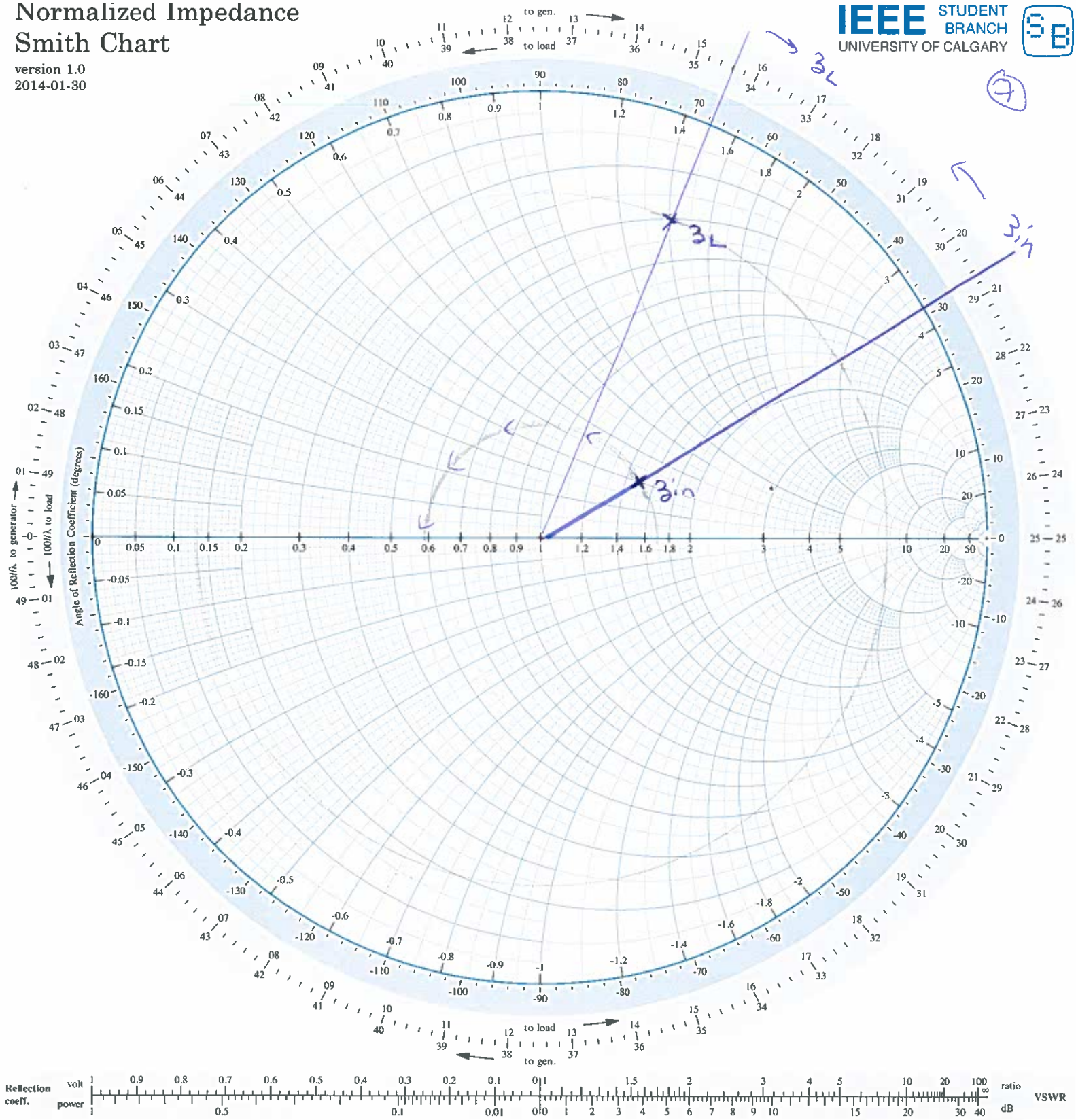
$$Z_1 = 375 \Omega$$

$$\therefore \Gamma_{\text{max}} \rightarrow Z_{\text{max}} = \sqrt{Z_1 Z_2} \\ = 106 \Omega$$



Normalized Impedance Smith Chart

version 1.0
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<http://www.ieee-ucalgary.ca/svn/ece/smithChart/>

