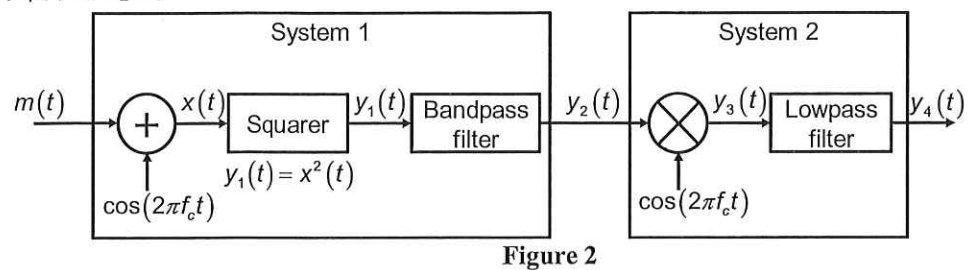
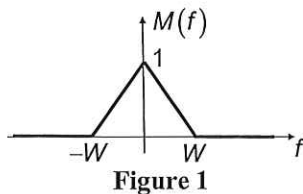


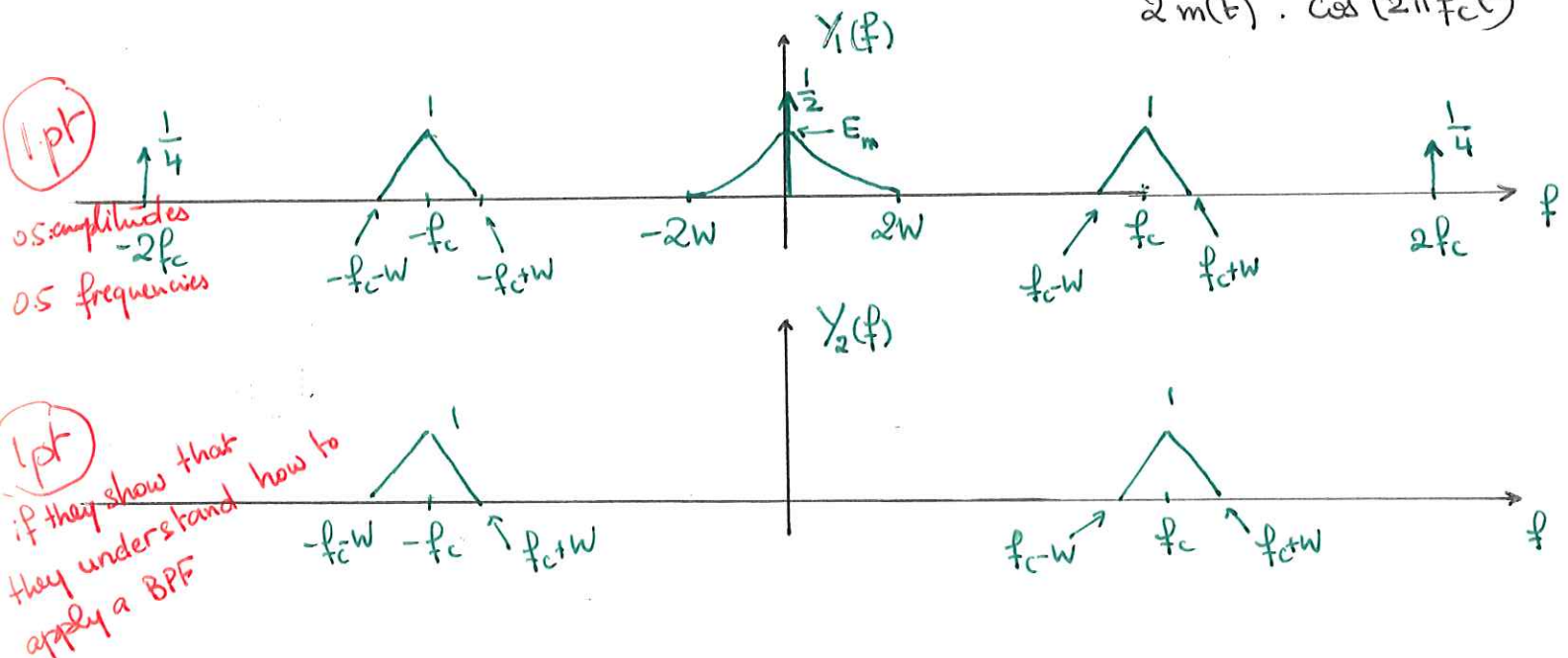
Question 1 [8 pts]

The message signal $m(t)$, whose spectrum is shown in Figure 1 below, is passed through the system in Figure 2 below, where $f_c = 100 \text{ kHz}$, $W = 1 \text{ kHz}$, $A_m = \max|m(t)| = 0.5$, the bandpass filter is ideal and has a bandwidth of $2W$ centered around f_c , the lowpass filter is ideal with a bandwidth of W

- Sketch the frequency spectra of the signals $y_1(t)$ and $y_2(t)$. **Indicate all the center frequencies, bandwidths, and amplitudes of interest for all the components of these signals.** [2 pts]
- What type of modulation is obtained at the output of System 1? Indicate the modulation index of this modulation. [2 pts]
- Sketch the frequency spectra of the signals $y_3(t)$ and $y_4(t)$. **Indicate all the center frequencies, bandwidths, and amplitudes of interest for all the components of these signals.** [2 pts]
- Propose an alternative for System 2 that does not require a coherent carrier to obtain the message signal $m(t)$ at the output $y_4(t)$. [2 pts]



$$a) \quad y_1(t) = x^2(t) = (m(t) + \cos(2\pi f_c t))^2 = m^2(t) + \frac{1}{2} + \frac{1}{2} \cos(4\pi f_c t) + 2m(t) \cdot \cos(2\pi f_c t)$$



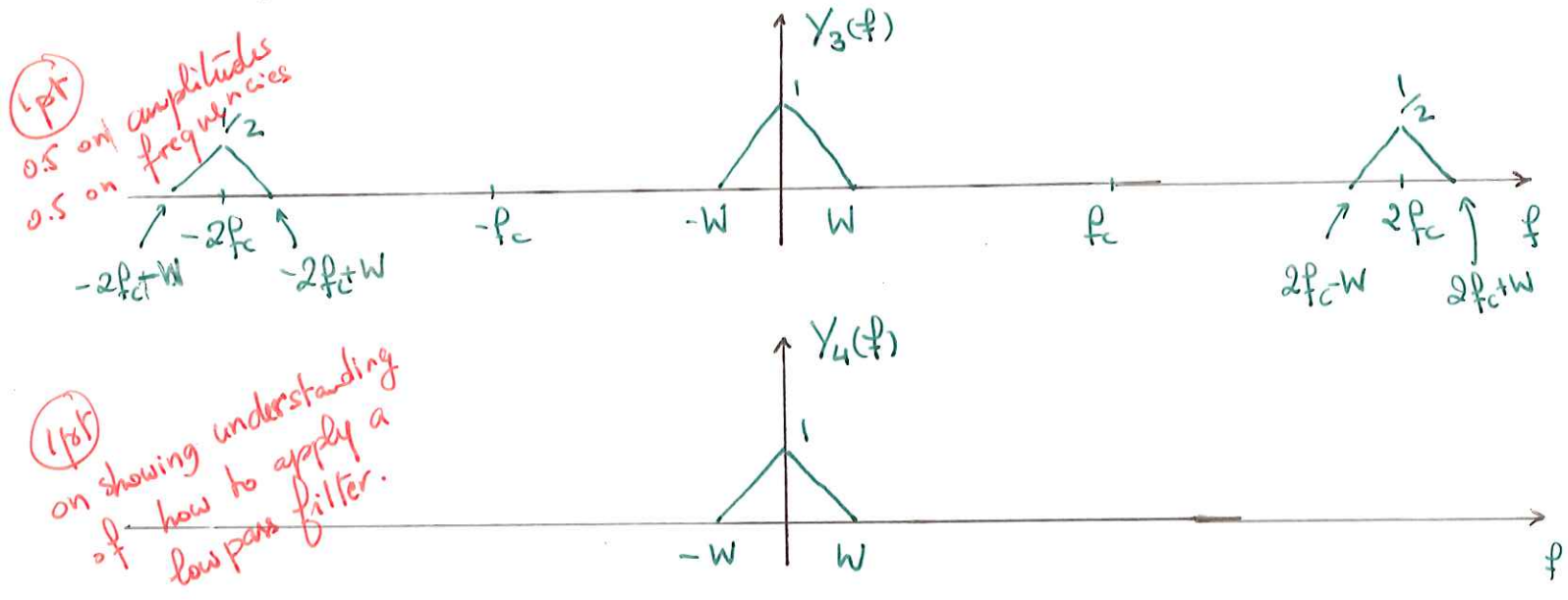
b) Modulation: DSB or DSB-SC

Modulation index: $\mu = 1$

← 2pts (circled)

give 1pt if they mention only AM modulation

$$c) \quad y_3(t) = 2 m(t) \cos^2(2\pi f_c t) = m(t) + m(t) \cos(4\pi f_c t)$$



$$y_4(t) = m(t)$$

d) System 2 is used to demodulate a DSB signal. A coherent carrier is required for the demodulation.

One can use a Costas receiver to perform the demodulation.

Question 2 [10 pts]

A conventional AM signal is given by:

$$s(t) = 5 \cos(1800\pi t) + 20 \cos(2000\pi t) + 5 \cos(2200\pi t)$$

a- Determine the modulating signal $m(t)$ and the carrier $c(t)$. [2 pts]

b- Determine the modulation index and the ratio of the power in the sidebands to the power in the carrier. [2 pts]

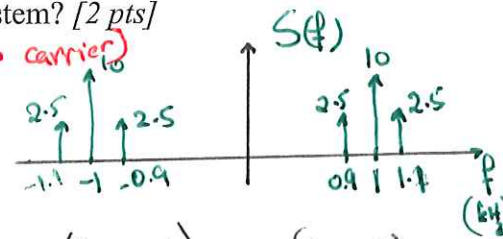
This signal is fed to a conventional AM receiver using an envelope detector. The average noise power per unit bandwidth measured at the input of the receiver front-end is 10^{-3} watt per Hertz.c- Assuming an input resistor of 1Ω , calculate the input signal-to-noise ratio of the system. [2 pts]

d- Determine the output signal-to-noise ratio at the output of the receiver. [2 pts]

e- By how many decibels is this system inferior to a DSB modulation system? [2 pts]

a) $c(t) = 20 \cos(2000\pi t)$ ← 1 pt [identifying the carrier]

$$s(t) = 20 \cos(2000\pi t) [1 + k_a m(t)]$$



$$20 \cos(2000\pi t) k_a m(t) = 5 \cos(1800\pi t) + 5 \cos(2200\pi t) = 10 \cos(2000\pi t) \cdot \cos(200\pi t)$$

$$k_a m(t) = \frac{1}{2} \cos(200\pi t)$$
 ← 1 pt

0.5 on form $\cos(\cdot)$
 0.25 on amplitude
 0.25 on freq.

b) $\mu = 0.5$ or 50% ← 1 pt

$$P_{\text{sidebands}} = 25 \text{ W}$$

$$P_{\text{carrier}} = 200 \text{ W}$$

$$\frac{P_{\text{sideband}}}{P_{\text{carrier}}} = \frac{25}{200} = 0.125 \text{ or } 12.5\%$$

c) $P_{\text{nin}} = 2 \cdot 100 \cdot 10^{-3} = 0.2 \text{ W}$

$$P_{\text{sin}} = 25 + 200 = 225 \text{ W}$$

$$\text{SNR}_{\text{in}} = \frac{P_{\text{sin}}}{P_{\text{nin}}} = \frac{225}{0.2} = 1125 \text{ or } 30.5 \text{ dB}$$

1 pt

0.5 on {signal, noise} power calculation
 0.5 on SNR

d) $\text{SNR}_{\text{out}} = \frac{P_{\text{sout}}}{P_{\text{nout}}} = \frac{50}{0.4} = 125$ ← 2 pts

or $\text{SNR}_{\text{out}} = \frac{\mu^2}{2 + \mu^2} \text{SNR}_{\text{in}} = \frac{0.25}{2.25} \cdot 1125 = 125$

1 pt on formula
 1 pt on calculation

e) this is inferior to DSB modulation system by $10 \log\left(\frac{2.25}{0.25}\right) = 9.5 \text{ dB}$ ← 2 pts

Question 3 [10 pts]

An angle-modulated signal around a carrier frequency $f_c = 10 \text{ MHz}$, has the form

$$s(t) = 100 \cos(2\pi f_c t + 4 \sin(2000\pi t))$$

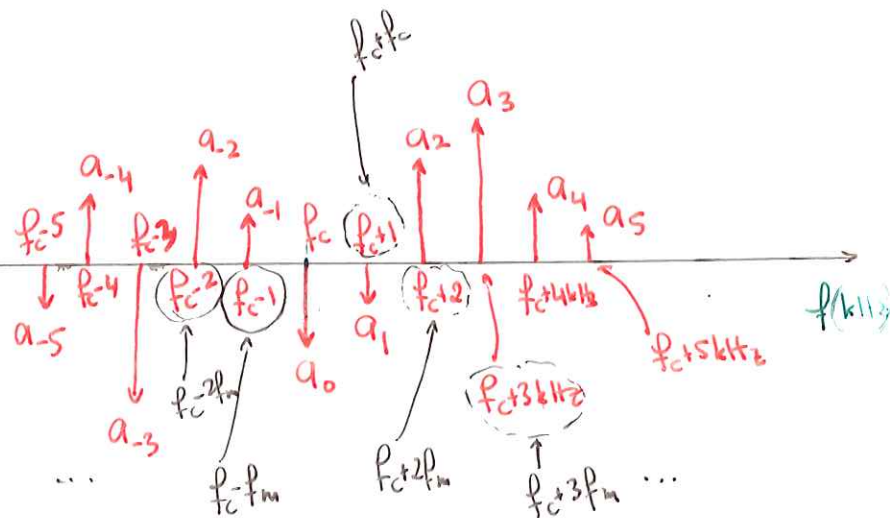
The modulating message has a maximum amplitude $A_m = \max|m(t)| = 1$.

- Determine the peak-phase deviation and peak-frequency deviation of $s(t)$. [2 pts]
- Determine $m(t)$ and k_f if $s(t)$ is an FM signal [2 pts]
- Determine $m(t)$ and k_p if $s(t)$ is a PM signal [2 pts]
- Determine the approximate bandwidth of $s(t)$ using Carson's rule. [2 pts]
- Sketch the spectrum of the modulated signal $s(t)$. **Show only the sidebands within the approximate bandwidth calculated in d-. Indicate all the frequencies and amplitudes of interest.** (Use the table below) [2 pts]

	$\beta = 1$	$\beta = 2$	$\beta = 3$	$\beta = 4$	$\beta = 5$
$n = 0$	0.7652	0.2239	-0.2601	-0.3971	-0.1776
$n = 1$	0.4401	0.5767	0.3391	-0.066	-0.3276
$n = 2$	0.1149	0.3528	0.4861	0.3641	0.04657
$n = 3$	0.0196	0.1289	0.3091	0.4302	0.3648
$n = 4$	0.0025	0.034	0.132	0.2811	0.3912
$n = 5$		0.007	0.043	0.1321	0.2611
$n = 6$		0.0012	0.0114	0.0491	0.131
$n = 7$			0.0025	0.01518	0.05338
$n = 8$				0.004	0.01841
$n = 9$					0.0055

- peak phase deviation: $\beta = 4 \text{ rad}$ ← (1 pt)
 peak frequency deviation: $\Delta f = \beta \cdot f_m = 4 \text{ kHz}$ ← (1 pt)
- if $s(t)$ is an FM signal:
 $k_f = 4 \text{ kHz/V}$ ← (1 pt)
 $m(t) = \cos(2000\pi t)$ ← (1 pt)
- if $s(t)$ is a PM signal:
 $k_p = 4 \text{ rad/V}$ ← (1 pt)
 $m(t) = \sin(2000\pi t)$ ← (1 pt)
- $B_T = (1 + \beta) \cdot 2f_m = 10 \text{ kHz}$ ← (2 pts)

e)



$$a_o = \frac{A_c}{2} J_o(4) = 50 \cdot (-0.3971) = \underline{\underline{-19.8}}$$

$$a_1 = \frac{A_c}{2} J_1(4) = 50 (-0.066) = \underline{\underline{-3.3}} \quad ; \quad a_{-1} = -a_1 = \underline{\underline{3.3}}$$

$$a_2 = a_{-2} = \frac{A_c}{2} J_2(4) = 50 \cdot (0.3641) = \underline{\underline{18.2}}$$

$$a_3 = \frac{A_c}{2} J_3(4) = 50 \cdot (0.4302) = \underline{\underline{21.5}} \quad ; \quad a_{-3} = a_3 = \underline{\underline{-21.5}}$$

$$a_4 = a_{-4} = \frac{Ac}{2} \quad J_4(4) = \sin(0.2811) = \underline{\underline{14.06}}$$

$$a_5 = \frac{A_c}{2} J_5(4) = 50(0.1321) = \underline{\underline{6.6}} \quad q_{-5} = -a_5 = \underline{\underline{-6.6}}$$

the question is on (2pts) in total:

0.5 pt on the shape (impulses on both sides of f_c stopping at $n=5$)

0.5 pt on spacing between impulses (f_m or 1 kHz)

0.5 pt on amplitudes $\frac{A_c}{2} J_n(\beta)$

0.5 pt on showing $\frac{A_c}{2} J_{-n}(\beta) = (-1)^n \frac{A_c}{2} J_n(\beta)$
[antisymmetric for n odd]
[symmetric for n even]

Question 4 [8 pts]

A FM modulation system has a modulation index $\beta = 4 \text{ rad}$.

- a- The SNR at the input of the FM receiver is equal to 30 dB. What is the SNR at the output of the FM receiver if no pre-emphasis and de-emphasis filters are used. [2 pts]

This FM modulation system uses a pair of pre-emphasis and de-emphasis filters defined by:

$$H_{pe}(f) = 1 + j \frac{f}{f_0} \quad \text{and} \quad H_{de}(f) = \frac{1}{1 + j \frac{f}{f_0}}$$

where $f_0 = 2.1 \text{ kHz}$, the message bandwidth $W = 15 \text{ kHz}$.

- b- What is the value of the improvement factor I in the output signal-to-noise ratio of the FM receiver produced by using this pair of pre-emphasis and de-emphasis filters? [2 pts]
 c- What is the SNR at the output of the FM receiver taking into account the effect of the pre-emphasis and de-emphasis filters. [2 pts]
 d- By how many decibels this FM system is superior to a DSB system? [2 pts]

a) $SNR_{out} = \left(\frac{3}{2} \beta^2\right) \cdot SNR_{in} = \frac{3}{2} (4)^2 \cdot 1000$

or $SNR_{out} = 24000 \text{ or } 43.8 \text{ dB}$

give full mark if this is correct

b) $I = \frac{2W^3}{3 \int_{-W}^W |H_{de}(f)|^2 df} = \frac{2W^3}{3 \int_{-W}^W \frac{f^2}{1 + \frac{f^2}{f_0^2}} df}$

or $I = \frac{(W/f_0)^3}{3 \left[\left(\frac{W}{f_0}\right) - \tan^{-1}\left(\frac{W}{f_0}\right) \right]}$

$I = \frac{(7.14)^3}{3 [7.14 - \tan^{-1}(7.14)]} = 21.25 \text{ or } 13.3 \text{ dB}$

c) $SNR_{out-emphasis} = 43.8 \text{ dB} + 13.3 \text{ dB} = 57.1 \text{ dB}$

or $= 24000 \times 21.25 = 510000$

d) This system is superior to a DSB system by $(13.8 + 13.3) = 27.1 \text{ dB}$

Question 5 [6 pts]

- a. Plot the spectrum of a PAM wave produced by the modulating signal:

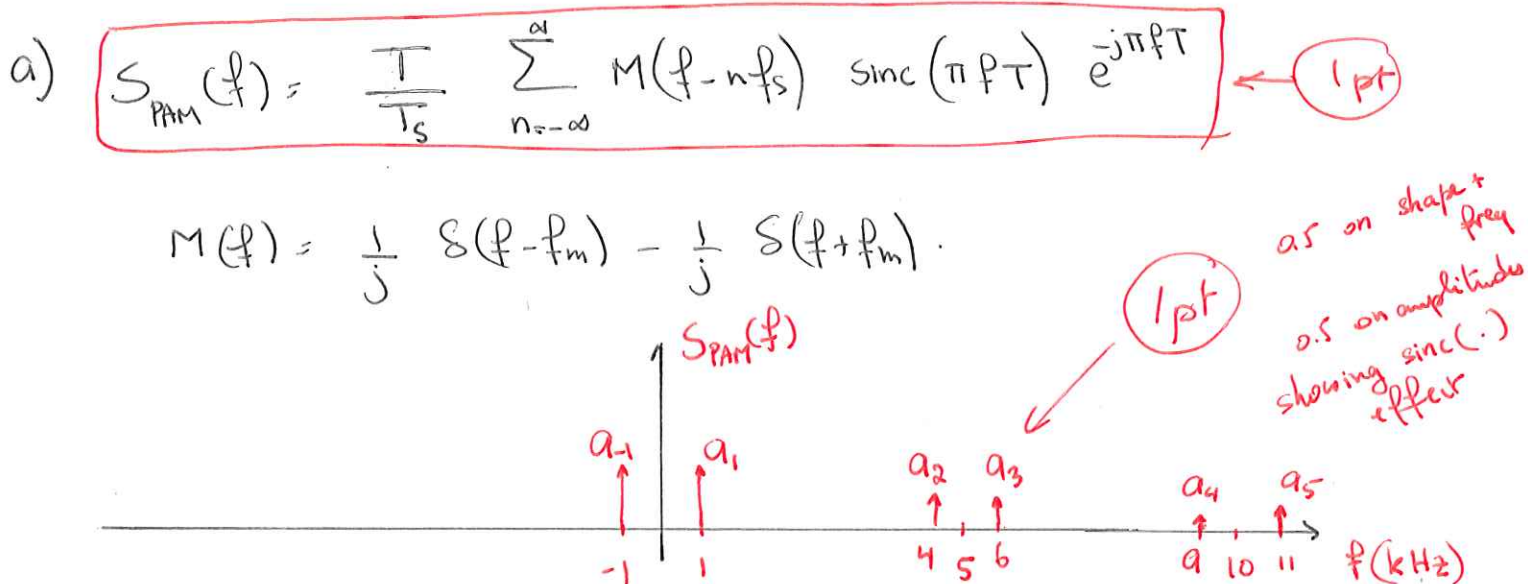
$$m(t) = 2 \sin(2\pi f_m t)$$

Assuming a modulation frequency of $f_m = 1 \text{ kHz}$, sampling period $T_s = 200 \mu\text{s}$ and pulse duration $T = 100 \mu\text{s}$ [2 pts]

- b. Using an ideal reconstruction filter, plot the spectrum of the filter output. [2 pts]

- c. What should be the expression of the amplitude spectrum of the equalizer required to compensate for the aperture effect. [2 pts]

For the spectrum plots, indicate all the frequencies and amplitudes of interest.



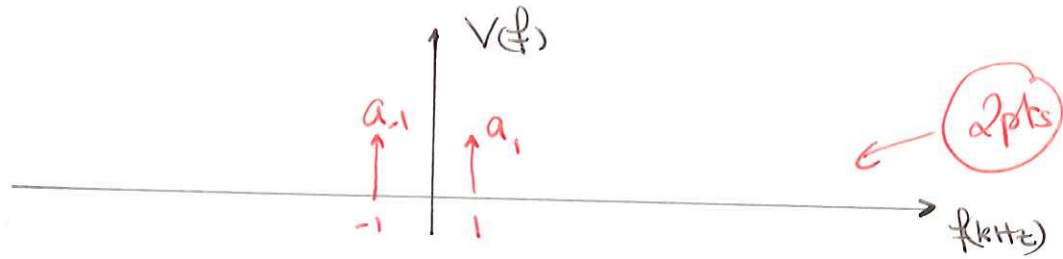
$$a_1 = \frac{1}{j} \cdot \frac{T}{T_s} \text{sinc}(\pi \cdot 1 \text{ kHz} \cdot 0.1 \text{ ms}) e^{-j\pi \cdot 1 \text{ kHz} \cdot 0.1 \text{ ms}} = \frac{1}{2j} \text{sinc}(0.1 \pi) e^{-j0.1\pi}$$

$$a_{-1} = -\frac{1}{j} \cdot \frac{T}{T_s} \text{sinc}(\pi \cdot -1 \text{ kHz} \cdot 0.1 \text{ ms}) e^{-j(-1 \text{ kHz}) \cdot 0.1 \text{ ms}} = -\frac{1}{2j} \text{sinc}(0.1 \pi) e^{j0.1\pi}$$

$$a_2 = -\frac{1}{2j} \text{sinc}(0.4 \pi) e^{-j0.4\pi}$$

$$a_3 = \frac{1}{2j} \text{sinc}(0.6 \pi) e^{-j0.6\pi}$$

b) if $v(t)$ is the signal at the output of the reconstruction filter:



$$a_1 = \frac{1}{2j} \text{sinc}(0.1\pi) e^{-j0.1\pi}$$

$$a_{-1} = \frac{1}{2j} \text{sinc}(0.1\pi) e^{j0.1\pi}$$

c) The frequency response of the equalizer should satisfy:

$$|E(f)| = \frac{1}{|T \text{sinc}(\pi f T) e^{-j\pi f T}|} = \boxed{\frac{1}{T |\text{sinc}(\pi f T)|}}$$

(0.5) 2pts

Question 6 [8 pts]

For practical considerations, a pulse $g(t)$ in a PAM signal is assumed to have the shape shown in Figure 3. The amplitude is $A = 1$, and the pulse duration is $T = 3 \text{ ms}$.

- Determine the impulse response $h(t)$ of a filter matched to this signal and sketch it. [2 pts]
- What is the peak value of the matched filter output? [2 pts]
- What is the expression of the peak-pulse signal-to-noise ratio if a white noise with double-sided power spectral density of $N_0/2 = 10^{-4} \text{ W/Hz}$ is added to the signal before the matched filter? [2 pts]
- Compare the peak-pulse signal-to-noise ratio in this case to the ideal case where the pulse has zero rising and falling times, the same amplitude ($A = 1$), and the same pulse duration ($T = 3 \text{ ms}$). [2 pts]

$$\frac{3}{4}T - \frac{1}{4}T = \frac{1}{2}T$$

$$\frac{2}{4}T = \frac{1}{2}T$$

$$SNR = \frac{k^2 T^2}{\frac{N_0}{2} k^2 T}$$

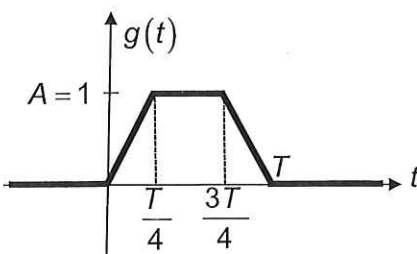
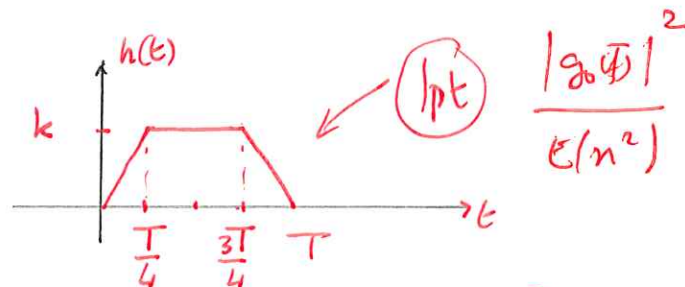


Figure 3

a) $h(t) = k g(T-t)$

1 pt



b) $y(t) = h(t) * g(t) = k \int_0^T g(z) g(T-t+z) dz$

the peak value of $y(t)$ is at $t=T$

1 pt $\rightarrow y(T) = k \int_0^T g^2(t) dt = k \left[2 \cdot \int_0^{T/4} \left(\frac{4}{T}t\right)^2 dt + \frac{T}{2} \right]$

$y(T) = k \left[\frac{32}{T^2} \cdot \frac{1}{3} \cdot \frac{T^3}{64} + \frac{T}{2} \right] = k \left[\frac{T}{6} + \frac{T}{2} \right] = k \cdot \frac{2T}{3} = k \cdot 2.10$

1 pt

c) $\eta = \frac{2E_g}{N_0} = \frac{4T}{3N_0} = \frac{2 \cdot 10^{-3}}{10^{-4}} = 20$

2 pts

d) the peak-pulse SNR in this case is $\frac{2}{3}$ the peak-pulse SNR in the ideal case

2 pts $\rightarrow \frac{2}{3} = 0.66$

