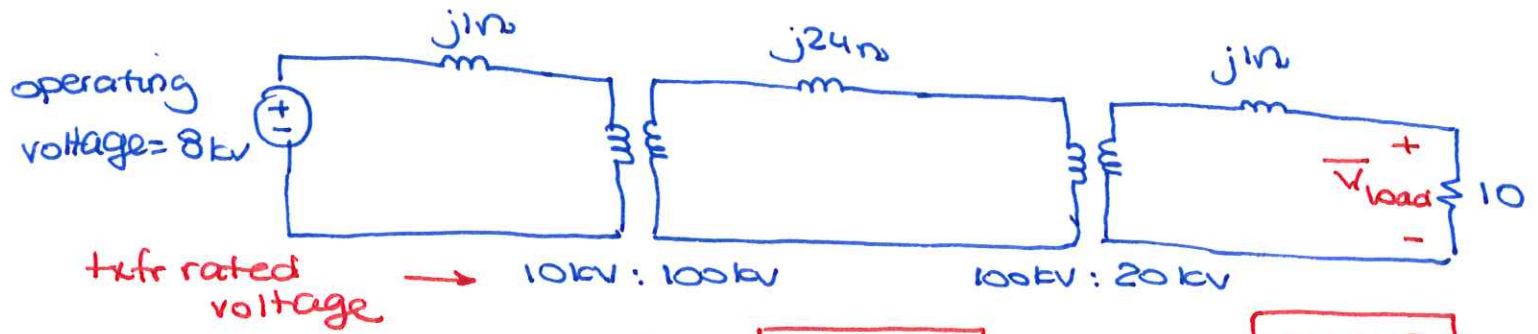


Ex: Calculate load voltage, current, power. Use $S_{base} = 100 \text{ MVA}$
 & $V_{base} = 8 \text{ kV}$ in gen zone.



$$V_{base_1} = 8 \text{ kV} \quad (\text{given})$$

$$Z_{base_1} = \frac{(V_{base_1})^2}{S_{base}} = 0.64 \, \Omega$$

zone 1

$$V_{base_2} = V_{base_1} \times \frac{100 \text{ kV}}{10 \text{ kV}} = 80 \text{ kV}$$

$$Z_{base_2} = \frac{(V_{base_2})^2}{S_{base}} = 64 \, \Omega$$

zone 2

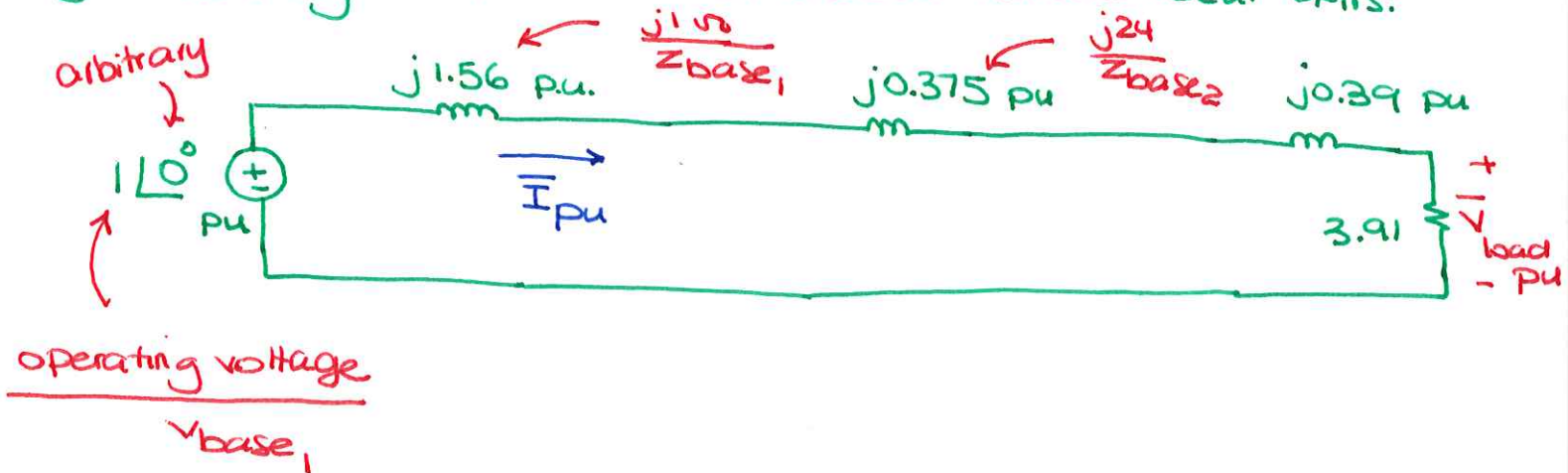
$$V_{base_3} = V_{base_2} \times \frac{20 \text{ kV}}{100 \text{ kV}} = 16 \text{ kV}$$

$$Z_{base_3} = \frac{(V_{base_3})^2}{S_{base}} = 2.56 \, \Omega$$

zone 3

$$I_{base_3} = \frac{S_{base}}{V_{base_3}} = 6.25 \text{ kA}$$

We can now come up with a p.u. circuit (impedance diagram) by calculating all p.u. values. We can remove ideal txfrs:



$$\overline{I}_{pu} = \frac{1 \angle 0^\circ}{j1.56 + j0.375 + j0.39 + 3.91} = 0.22 \angle -30.8^\circ \text{ pu}$$

$$\overline{V}_{load,pu} = \overline{I}_{pu} \times 3.91 = 0.859 \angle -30.8^\circ \text{ pu}$$

$$\overline{S}_{load,pu} = \overline{V}_{load,pu} \times \overline{I}_{pu}^* = 0.189 \text{ pu}$$

To get the actual values, multiply P.u. values with their corresponding base values:

phase angles not changed in P.u.

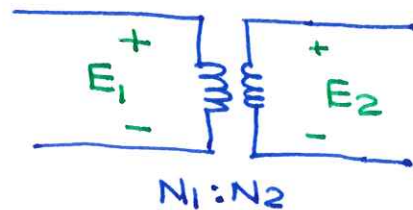
$$\overline{V}_{load} = \overline{V}_{load,pu} \times V_{base_3} = 13.7 \angle -30.8^\circ \text{ kv}$$

$$\overline{I}_{load} = \overline{I}_{pu} \times I_{base_3} = 1375 \angle -30.8^\circ \text{ A}$$

$$\overline{S}_{load} = \overline{S}_{load,pu} \times S_{base} = 18.9 \text{ mw}$$

Transformers in PU

• Ideal txfr model:



zone 1

zone 2

• Suppose we selected \$V_{base_1}\$

$$\therefore E_{1,pu} = \frac{E_1}{V_{base_1}}$$

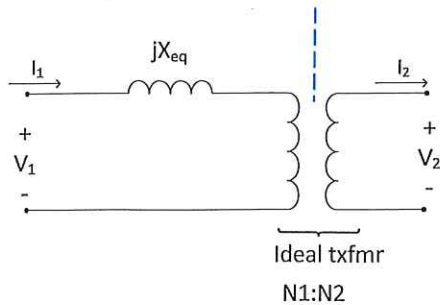
$$V_{base_2} = V_{base_1} \times \frac{N_2}{N_1}$$

$$E_{2,pu} = \frac{E_2}{V_{base_2}} = \frac{\frac{N_2}{N_1} \cdot E_1}{\frac{N_2}{N_1} \cdot V_{base_1}} = E_{1,pu}$$

i.e.: PU voltages (and currents) are identical on either side of ideal txfr \$\therefore\$ we can remove ideal txfrs from pu analysis (as we did in prev. example)

Non-ideal transformers in Per Unit

Let's start with the simplest non-ideal transformer model.



Zone 1

Suppose we selected $V_{base 1}$

$$Z_{base 1} = \frac{(V_{base 1})^2}{S_{base}}$$

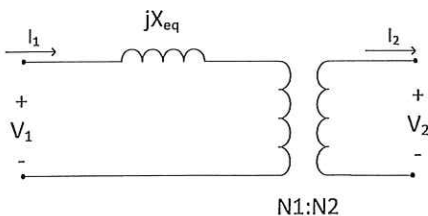
Zone 2

$$V_{base 2} = V_{base 1} \frac{N_2}{N_1}$$

$$Z_{base 2} = \frac{(V_{base 2})^2}{S_{base}} = \frac{\left(V_{base 1} \frac{N_2}{N_1}\right)^2}{S_{base}} = \left(\frac{N_2}{N_1}\right)^2 Z_{base 1}$$

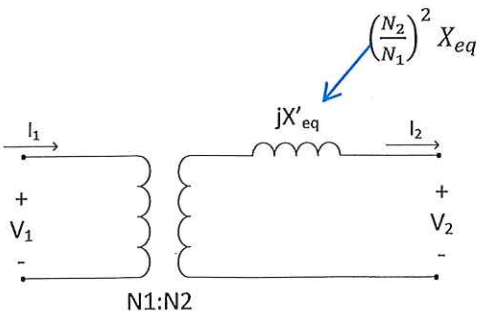
We already established that the ideal transformer portion can be removed in per unit analysis. The transformer impedance is the only thing left! The impedance should be divided by the correct Z_{base} in the per unit analysis.

1) With transformer impedance referred to winding 1 side:



$$X_{eq,pu} = \frac{X_{eq}}{Z_{base 1}}$$

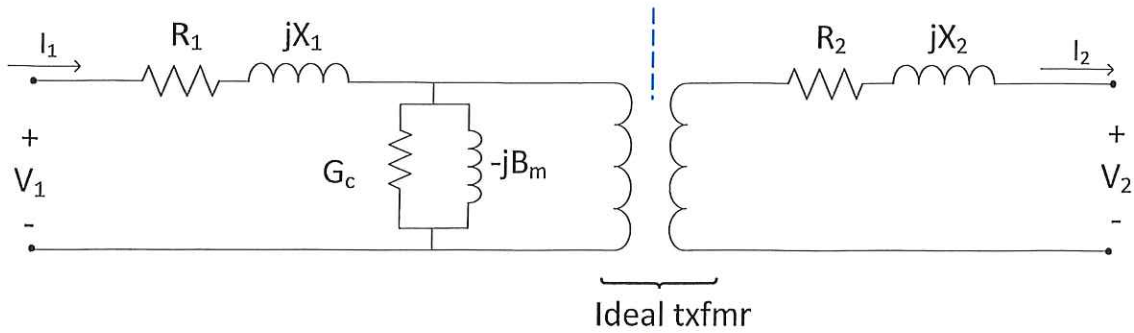
2) With transformer impedance referred to winding 2 side:



$$X'_{eq,pu} = \frac{X'_{eq}}{Z_{base 2}} = \frac{\left(\frac{N_2}{N_1}\right)^2 X_{eq}}{\left(\frac{N_2}{N_1}\right)^2 Z_{base 1}} = \frac{X_{eq}}{Z_{base 1}} = X_{eq,pu}$$

Conclusion: Transformer impedance in PU is the same regardless of which side it is referred to.

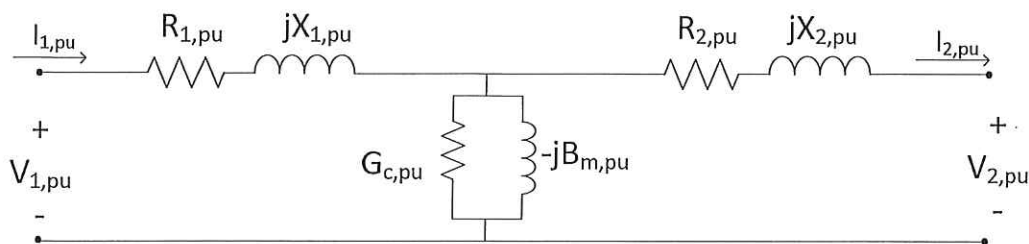
We can extend this out to the complete non-ideal transformer model:



Zone 1 with $V_{base\ 1}$ and $Z_{base\ 1}$ as defined before

Zone 2 with $V_{base\ 2}$ and $Z_{base\ 2}$ as defined before

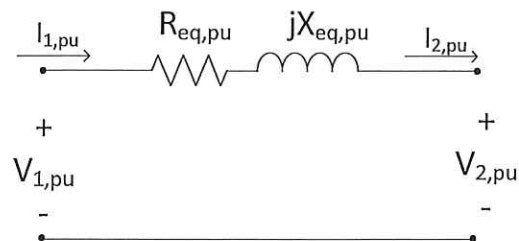
In per Unit, this transformer model becomes:



$$X_{1,pu} = \frac{X_1}{Z_{base\ 1}} \quad R_{1,pu} = \frac{R_1}{Z_{base\ 1}} \quad G_{c,pu} = \frac{G_c}{Y_{base\ 1}} \quad B_{m,pu} = \frac{B_m}{Y_{base\ 1}} \quad X_{2,pu} = \frac{X_2}{Z_{base\ 2}} \quad R_{2,pu} = \frac{R_2}{Z_{base\ 2}}$$

base admittance $Y_{base} = \frac{1}{Z_{base}}$

With the excitation branch omitted, the per unit representation of a non-ideal transformer becomes:



This is just the model from the previous page with winding resistance added.

The other conclusion: In PU analysis, non-ideal transformer becomes just another impedance in the circuit.

3 ϕ Per Unit Analysis

2 options:

- 1) Convert 3 ϕ system to per phase (i.e. convert everything to Y)

Carry per-phase P.u. analysis using 1 ϕ base values as in previous example. When converting to actual 3 ϕ quantities, remember $S_{3\phi} = 3 \times S_{1\phi}$, $V_{LL} = \sqrt{3} V_{LN}$

- This seems like more work than necessary! see Lab 1

- 2) Go directly from 3 ϕ system (e.g. single line diagram) to per unit system (impedance diagram)

• Analysis is similar to 1 ϕ P.u. circuit except base values are 3 ϕ :

- use a 3 ϕ S_{base}
- V_{base} is line-to-line voltage
- I_{base} is line current

Procedure:

- Pick a 3 ϕ power base for entire system, $S_{base, 3\phi}$
- Pick $V_{base, LL}$ for each voltage zone

(aside: $V_{base, LL} = \sqrt{3} V_{base, LN}$)

- Calculate Z_{base} :

$$Z_{base} = \frac{V_{base, LL}^2}{S_{base, 3\phi}}$$

we can use this for all Z in the system except Δ -connected load

- Calculate I_{base} :

$$I_{base} = \frac{S_{base, 3\phi}}{\sqrt{3} V_{base, LL}}$$

reminder:

in 3 ϕ systems

$$S_{3\phi} = \sqrt{3} V_{ll} \cdot I_l$$

v) Convert actual values to P.u. & draw P.u. circuit (impedance diagram)

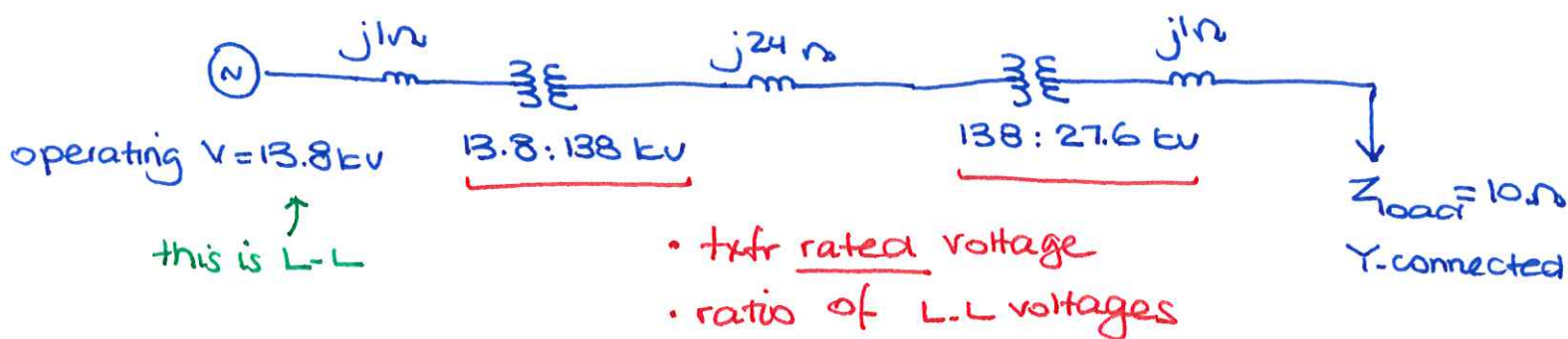
vi) Analyze P.u. circuit. Multiply P.u. quantities by corresponding base values to obtain 3 ϕ quantities.

Ex: Suppose our previous example is one phase of a 3 ϕ system

Find \bar{V}_{load} , \bar{S}_{load} , \bar{I}_{load} . Use $S_{base, 3\phi} = 300 \text{ mVA}$

$V_{base, LL} = 13.8 \text{ kV}$ in Gen zone

The single line diagram of the system is:



Zone 1

$$V_{base, 1, LL} = 13.8 \text{ kV (given)}$$

$$Z_{base, 1} = \frac{(13.8 \text{ kV})^2}{300 \text{ mVA}}$$

$S_{base} = 0.64 \Omega$

Zone 2

$$V_{base, 2, LL} = V_{base, 1} \times \frac{138}{13.8}$$

$$= 138 \text{ kV}$$

$$Z_{base, 2} = 64 \Omega$$

Zone 3

$$V_{base, 3, LL} = V_{base, 2} \times \frac{27.6}{138}$$

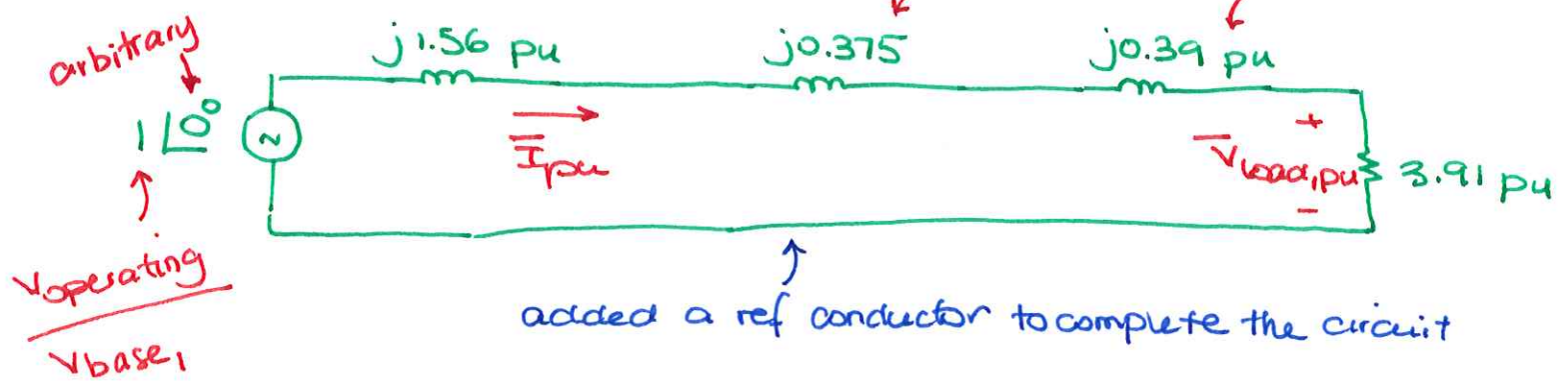
$$= 27.6 \text{ kV}$$

$$Z_{base, 3} = 2.56 \Omega$$

$$I_{base, 3} = \frac{300 \text{ mVA}}{\sqrt{3} \times 27.6}$$

$$= 6275.5 \text{ A}$$

P.u. circuit (impedance diagram):



• Notice the differences between per-phase (single phase) circuits and P.u. (impedance) diagram. While the topology is similar, the information in the circuits are different.

- Actual values in per-phase, P.u. values in P.u. diagram
- L-N voltages in per-phase, P.u. voltages in P.u. diagram

we can solve this circuit to get: $\bar{I}_{\text{pu}} = 0.22 \angle -30.8^\circ \text{ pu}$

$$\bar{V}_{\text{load, pu}} = 0.86 \angle -30.8^\circ \text{ pu}$$

$$\bar{S}_{\text{load, pu}} = 0.189 \text{ pu}$$

actual values: $\bar{V}_{\text{load, LL}} = \bar{V}_{\text{load, pu}} \times V_{\text{base}_3, \text{LL}} = 23.8 \angle -30.8^\circ \text{ kV}$

$$\bar{I}_{\text{load}} = \bar{I}_{\text{pu}} \times I_{\text{base}_3} = 1.381 \angle -30.8^\circ \text{ kA}$$

• This is the line current going into the load.

• For Y connections, this is equal to \bar{I}_ϕ

$$\bar{S}_{\text{load, 3}\phi} = \bar{S}_{\text{load}} \times S_{\text{base, 3}\phi} = 57.6 \text{ MW}$$

Z_{base} for Δ -connected load

• For Y-connected loads

$$Z_{base} = \frac{V_{base,LL}^2}{S_{base,3\phi}}$$

also know that $Z_{\Delta} = 3 \cdot Z_Y$

$$\therefore Z_{base,\Delta} = 3 \cdot Z_{base,Y} = 3 \frac{V_{base,LL}^2}{S_{base,3\phi}}$$

↑
use for Δ -connected load
use for all other Z

• regardless of load connection type, we arrive at the same PU value for a given load

Change of base

• Equipment impedances are often given in PU using the rated power & voltage as S_{base} & V_{base} . If these are different from S_{base} & V_{base} used in our analysis, we need to convert them:

$$\begin{aligned} Z_{pu,new} &= \frac{Z_{actual}}{Z_{base,new}} = \frac{Z_{pu,old} \times Z_{base,old}}{Z_{base,new}} \\ &= Z_{pu,old} \times \frac{Z_{base,old}}{Z_{base,new}} \end{aligned}$$

$$\therefore Z_{pu,new} = Z_{pu,old} \times \frac{V_{base,old}^2}{V_{base,new}^2} \times \frac{S_{base,new}}{S_{base,old}}$$

Ex: $\overbrace{400 \text{ mVA}}^{\text{rated power}}, \overbrace{144:245 \text{ kV}}^{\text{rated voltage}}$ transformer has leakage reactance of 13%. What is P.U. impedance on 100 mVA $\overbrace{138 \text{ kV}}^{\text{V}_{\text{base on LV side?}}} \overbrace{S_{\text{base, new}}}$

- Pu value $\times 100\%$.
- based on rated values $\text{V}_{\text{base, new on LV side}}$

$$Z_{\text{pu, new}} = j0.13 \times \left(\frac{144 \text{ kV}}{138 \text{ kV}} \right)^2 \times \frac{100 \text{ mVA}}{400 \text{ mVA}} = j0.035$$

$$\text{or } X_{\text{pu, new}} = 3.5\%$$

• What if we used HV side values?

$$V_{\text{base, new, HV}} = V_{\text{base, new, LV}} \times \frac{245}{144} = 138 \times \frac{245}{144}$$

$$Z_{\text{pu, new}} = j0.13 \times \left(\frac{245 \text{ kV}}{V_{\text{base, new, HV}}} \right)^2 \times \frac{100 \text{ mVA}}{400 \text{ mVA}} = j0.035$$

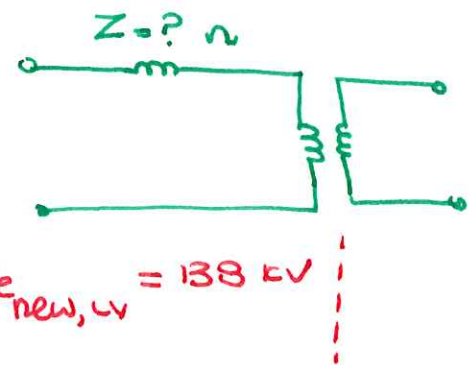
same as before!

• What is Z in Ohms referred to LV side?

$$Z = \underbrace{j0.035}_{Z_{\text{pu, new}}} \times \underbrace{\frac{(138 \text{ kV})^2}{100 \text{ mVA}}}_{Z_{\text{base, new, LV}}} = j6.7 \Omega$$

or

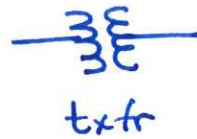
$$Z = \underbrace{j0.13}_{Z_{\text{pu, old}}} \times \underbrace{\frac{(144 \text{ kV})^2}{400 \text{ mVA}}}_{Z_{\text{base, old, LV}}} = j6.7 \Omega$$



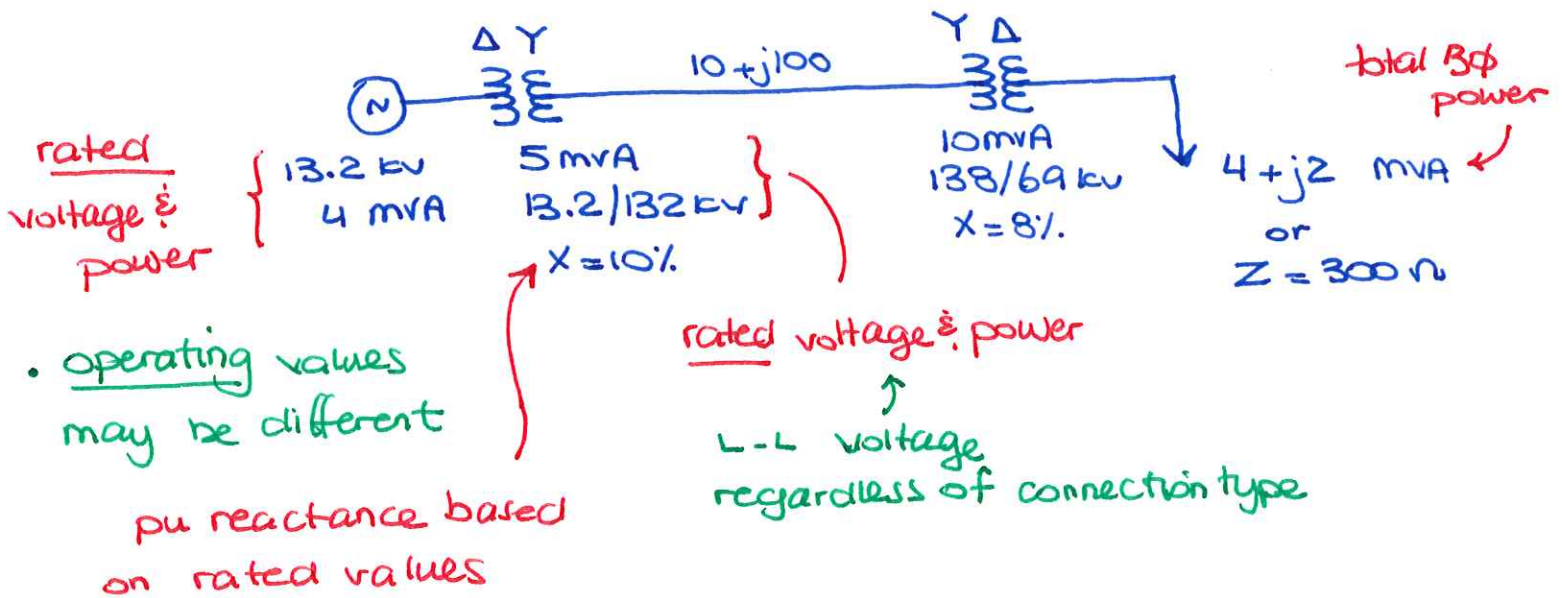
Single Line Diagram (SLD)

- Used for analyzing 3 ϕ systems. It shows one phase of a balanced 3 ϕ system. We often use symbols instead of circuit elements. Values indicated on the SLD are often 3 ϕ values e.g: L-L values, 3 ϕ power

- Standard symbols :



- Example :

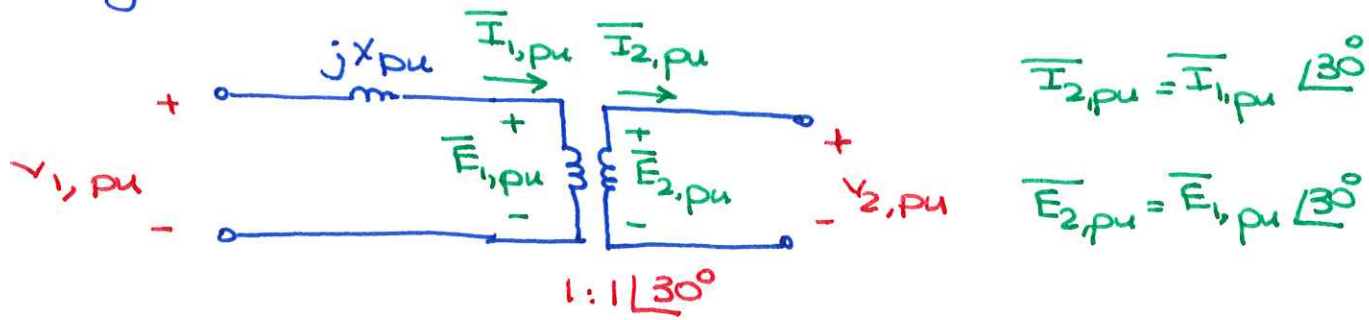


3 ϕ Txfr in PU

- Y-Y or Δ - Δ : line-to-line voltages on either side are in phase with each other so the txfr becomes an impedance in pu :



2) Δ -Y : 30° phase shift between 2 sides. P.u. only deals with magnitudes:



3) Y- Δ : identical to Δ -Y but with a $1:1 \angle -30^\circ$ ideal txfr

• We will ignore the phase shifts for Δ -Y & Y- Δ transformers in this course.

Motors & Generators (Machines)

• on the SLD

Gen



Motor



operating voltage & power
may be different

13.8 kV

10 mVA

$X = 10\%$

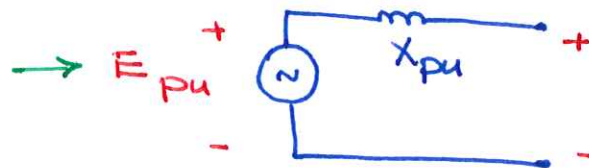
← rated voltage

← rated power

← pu reactance

• In pu circuit (impedance diagram), machines are shown as an EMF behind an impedance:

operating
internal EMF
voltage



operating voltage
at terminals

value in pu
circuit

$$X_{pu} = X_{pu,old}$$

value based on
rated V, S

(10% in our example)

$$\times \frac{V_{rated}^2}{V_{base}^2}$$

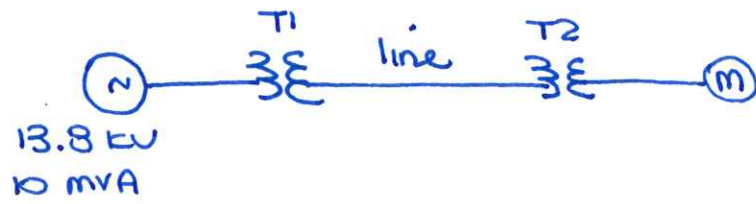
our choice
for V_{base}

$$\times \frac{S_{base}}{S_{rated}}$$

$S_{base,old}$
(10 mVA in our ex.)

$V_{base,old}$ (13.8 kV in our example)

• SLD



• PU Circuit
(Impedance)
Diagram

