2.1 (a)
$$\overline{A}_1 = 6 \angle 30^\circ = 6 \left[\cos 30^\circ + j \sin 30^\circ\right] = 5.20 + j 3$$

(b)
$$\overline{A}_2 = -4 + j5 = \sqrt{16 + 25} \angle \tan^{-1} \frac{5}{-4} = 6.40 \angle 128.66^\circ = 6.40 e^{j128.66^\circ}$$

(c)
$$\overline{A}_3 = (5.20 + j3) + (-4 + j5) = 1.20 + j8 = 8.01 \angle 81.50^\circ$$

(d)
$$\overline{A}_4 = (6 \angle 30^\circ)(6.40 \angle 128.66^\circ) = 38.414 \angle 158.658^\circ = -35.78 + j13.98$$

(e)
$$\overline{A}_5 = (6 \angle 30^\circ) / (6.40 \angle -128.66^\circ) = 0.94 \angle 158.66^\circ = 0.94 e^{j158.66^\circ}$$

2.2 (a)
$$\overline{I} = 500 \angle -30^{\circ} = 433.01 - j250$$

(b)
$$i(t) = 4\sin(\omega t + 30^\circ) = 4\cos(\omega t + 30^\circ - 90^\circ) = 4\cos(\omega t - 60^\circ)$$

 $\overline{I} = (4) \angle -60^\circ = 2.83 \angle -60^\circ = 1.42 - j2.45$

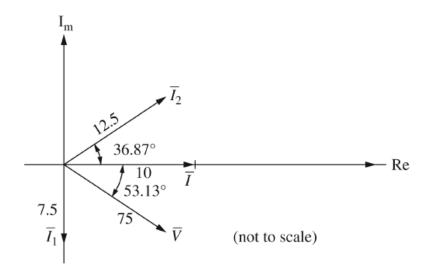
(c)
$$\overline{I} = (5/\sqrt{2}) \angle -15^{\circ} + 4 \angle -60^{\circ} = (3.42 - j0.92) + (2 - j3.46)$$

= 5.42 - j4.38=6.964\angle -38.94\circ

2.4 (a)
$$\overline{I}_1 = 10 \angle 0^{\circ} \frac{-j6}{8 + j6 - j6} = 10 \frac{6 \angle -90^{\circ}}{8} = 7.5 \angle -90^{\circ} \text{ A}$$

 $\overline{I}_2 = \overline{I} - \overline{I}_1 = 10 \angle 0^{\circ} - 7.3 \angle -90^{\circ} = 10 + j7.5 = 12.5 \angle 36.87^{\circ} \text{ A}$
 $\overline{V} = \overline{I}_2 (-j6) = (12.5 \angle 36.87^{\circ}) (6 \angle -90^{\circ}) = 75 \angle -53.13^{\circ} \text{ V}$

(b)



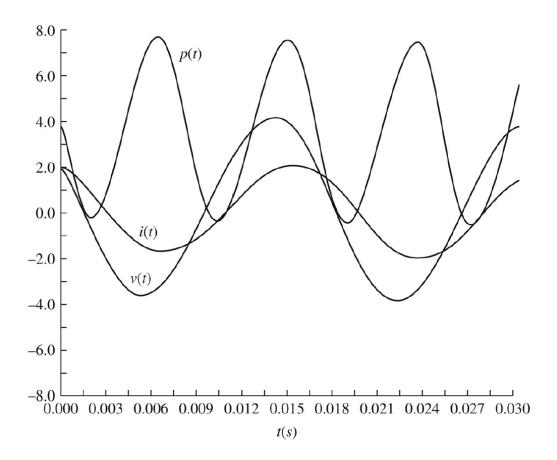
2.15 (a)
$$\overline{I} = \left[\left(\frac{4}{\sqrt{2}} \right) \angle 60^{\circ} \right] / \left(2\angle 30^{\circ} \right) = \sqrt{2} \angle 30^{\circ} \text{ A}$$

$$i(t) = 2\cos(\omega t + 30^{\circ}) \text{ A with } \omega = 377 \text{ rad/s}$$

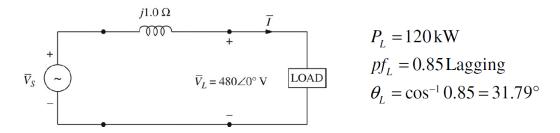
$$p(t) = v(t)i(t) = 4 \left[\cos 30^{\circ} + \cos(2\omega t + 90^{\circ}) \right]$$

$$= 3.46 + 4\cos(2\omega t + 90^{\circ}) \text{ W}$$

- (b) v(t), i(t), and p(t) are plotted below: (See next page)
- (c) The instantaneous power has an average value of 3.46 W, and the frequency is <u>twice</u> that of the voltage or current.



2.26 (a) The problem is modeled as shown in figure below:



Power triangle for the load:

$$\overline{S}_L = P_L + jQ_L = 141.18 \angle 31.79^\circ \text{ kVA}$$

$$I = S_L / V = 141,180 / 480 = 294.13 \text{ A}$$

$$Q_L = P_L \tan(31.79^\circ)$$

$$= 74.364 \text{ kVAR}$$

Real power loss in the line is zero.

Reactive power loss in the line is
$$Q_{LINE} = I^2 X_{LINE} = (294.13)^2 1$$

= 86.512 kVAR

$$\vec{S}_S = P_S + jQ_S = 120 + j(74.364 + 86.512) = 200.7 \angle 53.28^{\circ} \text{ kVA}$$

The input voltage is given by $V_S = S_S / I = 682.4 \text{ V (rms)}$

The power factor at the input is $\cos 53.28^{\circ} = 0.6$ Lagging

(b) Applying KVL,
$$\overline{V}_S = 480 \angle 0^\circ + j1.0 (294.13 \angle -31.79^\circ)$$

= $635 + j250 = 682.4 \angle 21.5^\circ \text{V (rms)}$
 $(pf)_S = \cos(21.5^\circ + 31.79^\circ) = 0.6 \text{ Lagging}$
Pf = $\cos(\text{voltage angle} - \text{current angle})$

2.30 (a) For load 1:
$$\theta_1 = \cos^{-1}(0.28) = 73.74^{\circ}$$
 Lagging
$$\overline{S}_1 = 125 \angle 73.74^{\circ} = 35 + j120$$

$$\overline{S}_2 = 10 - j40$$

$$\overline{S}_3 = 15 + j0$$

$$\overline{S}_{TOTAL} = \overline{S}_1 + \overline{S}_2 + \overline{S}_3 = 60 + j80 = 100 \angle 53.13^{\circ} \text{ kVA} = P + jQ$$

$$\therefore P_{TOTAL} = 60 \text{ kW}; Q_{TOTAL} = 80 \text{ kVAR}; \text{ kVA}_{TOTAL} = S_{TOTAL} = 100 \text{ kVA}. \leftarrow$$
Supply $pf = \cos(53.13^{\circ}) = 0.6$ Lagging \leftarrow

(b)
$$\overline{I}_{TOTAL} = \frac{\overline{S}^*}{\overline{V}^*} = \frac{100 \times 10^3 \angle -53.13^\circ}{1000 \angle 0^\circ} = 100 \angle -53.13^\circ A$$

At the new pf of 0.8 lagging, $P_{\tiny TOTAL}$ of 60kW results in the new reactive power Q', such that

$$\theta' = \cos^{-1}(0.8) = 36.87^{\circ}$$

and
$$Q' = 60 \tan (36.87^{\circ}) = 45 \text{ kVAR}$$

∴ The required capacitor's kVAR is $Q_C = 80 - 45 = 35 \text{ kVAR}$ \leftarrow

It follows then
$$X_C = \frac{V^2}{\overline{S}_C^*} = \frac{(1000)^2}{j35000} = -j28.57 \,\Omega$$

and

$$C = \frac{10^6}{2\pi (60)(28.57)} = 92.85 \mu \text{ F} \leftarrow$$

The new current is
$$I' = \frac{\overline{S}'^*}{\overline{V}^*} = \frac{60,000 - j45,000}{1000 \angle 0^\circ} = 60 - j45 = 75 \angle -36.87^\circ \text{A}$$

The supply current, in magnitude, is reduced from 100A to $75A \leftarrow$

Addition of capacitor bank and "correction of power factor" closer to unity resulted in lower current throught thetransmission lines, which translates to lower losses in the lines.

2.40 (a)
$$\overline{V}_{AN} = \frac{240}{\sqrt{3}} \angle 0^{\circ} = 138.56 \angle 0^{\circ} \text{V}$$
 (Assumed as Reference) $\overline{V}_{AB} = 240 \angle 30^{\circ} \text{V}; \overline{V}_{BC} = 240 \angle -90^{\circ} \text{V}; \overline{I}_{A} = 15 \angle -90^{\circ} \text{A}$ $\overline{Z}_{Y} = \frac{\overline{V}_{AN}}{\overline{I}_{A}} = \frac{138.56 \angle 0^{\circ}}{15 \angle -90^{\circ}} = 9.24 \angle 90^{\circ} = (0+j9.24) \Omega$ (b) $\overline{I}_{AB} = \frac{\overline{I}_{A}}{\sqrt{3}} \angle 30^{\circ} = \frac{15}{\sqrt{3}} \angle -90^{\circ} + 30^{\circ} = 8.66 \angle -60^{\circ} \text{A}$ $\overline{Z}_{\Delta} = \frac{\overline{V}_{AB}}{\overline{I}_{AB}} = \frac{240 \angle 30^{\circ}}{8.66 \angle -60^{\circ}} = 27.71 \angle 90^{\circ} = (0+j27.71) \Omega$ Note: $\overline{Z}_{Y} = \overline{Z}_{\Delta} / 3$

2.42 (a) With \overline{V}_{ab} as reference

$$\bar{V}_{an} = \frac{208}{\sqrt{3}} \angle -30^{\circ}$$

$$= \frac{208}{\sqrt{3}} = 4 + j3 = 5 \angle 36.87^{\circ} \Omega$$

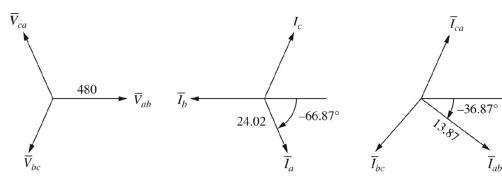
$$\overline{I}_a = \frac{\overline{V}_{an}}{\left(\frac{\overline{Z}_{\Delta}}{3}\right)} = \frac{120.1\angle - 30^{\circ}}{5\angle 36.87^{\circ}} = 24.02\angle - 66.87^{\circ} A$$

$$\overline{S}_{3\phi} = 3\overline{V}_{an}\overline{I}_{a}^{*} = 3(120.1\angle -30^{\circ})(24.02\angle +66.87^{\circ})$$
$$= 8654\angle 36.87^{\circ} = 6923 + j5192$$

 $P_{3\phi} = 6923 \,\mathrm{W}; \, Q_{3\phi} = 5192 \,\mathrm{VAR};$ both absorbed by the load

$$pf = \cos(36.87^{\circ}) = 0.8 \text{ Lagging}; S_{3\phi} = |\overline{S}_{3\phi}| = 8654 \text{ VA}$$

(b)



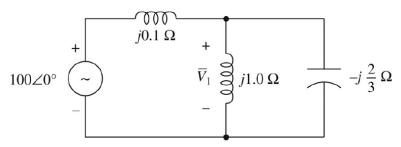
$$V_{ab} = 208 \angle 0^{\circ} V \qquad I_a = 1$$

$$\overline{V}_{ab} = 208 \angle 0^{\circ} \text{V}$$
 $\overline{I}_{a} = 24.02 \angle -66.87^{\circ} \text{A}$

$$13.87 \angle -36.87^{\circ} A$$

2.50 Replace delta by the equivalent WYE: $\frac{\overline{Z}_{y}}{Z_{y}} = -j\frac{2}{3}\Omega$

Per-phase equivalent circuit is shown below:



Noting that $\left(j1.0 \left\| -j\frac{2}{3} \right\| = -j2$, by voltage-divider law,

$$\overline{V}_1 = \frac{-j2}{-j2 + j0.1} (100 \angle 0^\circ) = 105 \angle 0^\circ$$

$$\therefore v_1(t) = 105\sqrt{2}\cos(\omega t + 0^\circ) = 148.5\cos\omega t \text{ V} \leftarrow$$

In order to find $i_2(t)$ in the original circuit, let us calculate $\overline{V}_{A'B'}$

$$\overline{V}_{A'B'} = \overline{V}_{A'N'} - \overline{V}_{B'N'} = \sqrt{3} e^{j30^{\circ}} \overline{V}_{A'N'} = 181.8 \ \angle 30^{\circ}$$
Then
$$\overline{I}_{A'B'} = \frac{181.8 \ \angle 30^{\circ}}{-j2} = 90.9 \ \angle 120^{\circ}$$

$$\therefore i_{2}(t) = 90.9 \ \sqrt{2} \cos(\omega t + 120^{\circ})$$

$$\therefore i_2(t) = 90.9 \sqrt{2} \cos(\omega t + 120^\circ)$$
$$= 128.6 \cos(\omega t + 120^\circ) A \leftarrow$$