

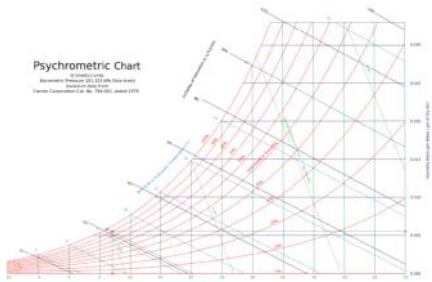
Task 1 Use a weather forecast website, and utilize the psychrometric chart and the formula we went through in the class to determine the absolute humidity, the wet-bulb temperature and the mass of water vapour in the air in Classroom A (Aula A) of Piacenza campus in the moment that you are solving this exercise (provide the inputs that you utilized)

[Weather Forecast Website example](#)

Umidità: Relative humidity, Pressione atmosferica: Air total pressure (1 hPa: 0.1 kPa), Temperatura effettiva: temperature to be utilized.

Il tempo oggi in Piacenza Lunedì, 02 Dicembre 2019							
	13:00	14:00	16:00	18:00	20:00	21:00	22:00
Temperatura effettiva	10°C	10°C	9°C	6°C	7°C	7°C	8°C
Temperatura percepita	10°C	10°C	8°C	5°C	7°C	6°C	7°C
Precipitazioni	0 mm	0 mm	0 mm	0 mm	0 mm	0 mm	0 mm
Umidità	79 %	77 %	89 %	90 %	90 %	92 %	91 %
Pressione atmosferica	1016 hPa	1018 hPa	1016 hPa	1017 hPa	1019 hPa	1019 hPa	1020 hPa

The time now is 8 pm from the data given in the website :
relative humidity is +90%
Total air pressure = 101.9 kPa
Temperture in kelvin scale T= 230 K



absolulte humidity $w = 0.0055$
bulb temperature $T_{wb} = 6^{\circ}\text{C}$
$$w = \frac{0.622 P_v}{P_a} = \frac{0.622 P_v}{P - P_v} = 0.0055$$

introduce $P = 101.9 \text{ kPa}$
 $P_v \approx 0.893 \text{ kPa}$
aurem $\phi = \frac{m_v}{m_g} = 90\%$
for any Ideal gas \Rightarrow water vapour, $R_{sp} = 0.4615$
 $P_v = 0.893 \text{ kPa}$
 $m_v = \frac{0.893 \text{ V}}{0.4615 \times 230} \approx 8.41 \times 10^{-3}$
 $m_g = \frac{m_v}{90\%} \approx 9.34 \times 10^{-3}$

Task 2 Utilize the same methodology we went through in the class and determine the sensible and latent load corresponding to internal gains, the ventilation, and the infiltration in a house with a good construction quality and with the same geometry as that of the example which is located in Brindisi, Italy

BRINDISI, Italy													WMO# 102020	
Lat: 40.63N		Long: 17.95E		Elev: 10		SeaP: 161.2		Time Zone: 1.00 (E/UTC)		Period: 06-10		HDD: 99999		
Climate Analysis and Meteorological Design Conditions														
Calendar Month	Heating DB				Cooling DB				Cooling DB				MICROSPOND in 50-65-75-85	
	DB	WB	WBP	WBS	DB	WB	WBP	WBS	DB	WB	WBP	WBS	DB	WB
(A)	18.2	14.2	12.7	12.1	27.2	24.2	22.7	22.1	11.1	10.1	9.1	8.1	1.0	1.0
(B)	2	2.0	4.1	-5.1	-2.5	7.2	-3.0	3.0	7.4	13.4	10.2	12.4	10.6	3.4
(C)	2	2.0	4.1	-5.1	-2.5	7.2	-3.0	3.0	7.4	13.4	10.2	12.4	10.6	3.4
Annual Climate, Solar Radiation, and Energy Design Conditions														
Calendar Month	Heating DB				Cooling DB				Cooling DB				MICROSPOND in 50-65-75-85	
	DB	WB	WBP	WBS	DB	WB	WBP	WBS	DB	WB	WBP	WBS	DB	WB
(A)	18.2	14.2	12.7	12.1	27.2	24.2	22.7	22.1	11.1	10.1	9.1	8.1	1.0	1.0
(B)	7	7.1	22.8	25.8	31.1	24.3	29.9	24.3	27.2	29.7	26.3	29.0	25.6	4.2
(C)	7	7.1	22.8	25.8	31.1	24.3	29.9	24.3	27.2	29.7	26.3	29.0	25.6	4.2
Extreme Annual Design Conditions														
Calendar Month	Heating DB				Cooling DB				Cooling DB				MICROSPOND in 50-65-75-85	
	DB	WB	WBP	WBS	DB	WB	WBP	WBS	DB	WB	WBP	WBS	DB	WB
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Extreme Annual Design Conditions														
Calendar Month	Heating													

internal gains:

calculate the sensible cooling load from internal gains:

$$Q_{igs} = 136 + 2.2 A_{cf} + 22 N_{oc} = 136 + 2.2 \times 22 \times 200 + 22 \times 2 = 620 \text{ W}$$

calculate cooling of int gains.

$$Q_{igl} = 20 + 0.22 A_{cf} + 12 N_{oc} = 20 + 0.22 \times 200 + 12 \times 2 = 88 \text{ W}$$

infiltration:

$$A_{ul} = 1.4 \text{ cm}^2/\text{m}^2$$

$$A_{eg} = A_{wall} + A_{roof} = 200 + 144 = 344 \text{ m}^2$$

$$\text{thus, } A_L = A_{eg} \times A_{ul} = 344 \times 1.4 = 481.6 \text{ cm}^2$$

$$T_{cooling} = 24^\circ\text{C} \quad T_{heating} = 20^\circ\text{C}$$

$$\Delta T_{cooling} = 31.1^\circ\text{C} - 24^\circ\text{C} = 7.1^\circ\text{C} = 7.1 \text{ K}$$

$$\Delta T_{heating} = 20^\circ\text{C} - (-4.1^\circ\text{C}) = 24.1^\circ\text{C} = 24.1 \text{ K}$$

$$DR = 7.1^\circ\text{C} = 7.1 \text{ K}$$

$$IDF_{heating} = 0.1073 \frac{\text{L}}{\text{s} \times \text{cm}^2}$$

$$IDF_{cooling} = 0.033 \frac{\text{L}}{\text{s} \times \text{cm}^2}$$

air flow rate:

$$Q_{i,heating} = A_L \times IDF_{heating} = 481.6 \times 0.1073 \approx 35.157 \frac{\text{L}}{\text{s}}$$

$$Q_{i,cooling} = A_L \times IDF_{cooling} = 481.6 \times 0.033 \approx 15.893 \frac{\text{L}}{\text{s}}$$

min whole building ventilation:

$$Q_v = 0.05 A_{cf} + 3.5 (N_{br} + 1) = 0.05 \times 200 + 3.5 \times (1+1) = 17 \frac{\text{L}}{\text{s}}$$

$$Q_{i-v,heating} = Q_{i,heating} + Q_v \approx 35.157 + 17 = 52.157 \frac{\text{L}}{\text{s}}$$

$$Q_{i-v,cooling} = Q_{i,cooling} + Q_v \approx 15.893 + 17 = 32.893 \frac{\text{L}}{\text{s}}$$

Given that $C_{sensible} = 1.23$, $C_{latent} = 3010$, $\Delta W_{cooling} = 0.0039$

$$Q_{inf-v,es} = C_s Q_{i-v} \Delta T_c \approx 1.23 \times 32.893 \times 7.1 = 287.25 \text{ W}$$

$$Q_{inf-v,cf} = C_L Q_{i-v} \Delta W_c \approx 3010 \times 32.893 \times 0.0039 = 386.13 \text{ W}$$

$$Q_{inh-vhs} = C_s Q_{i-vh} \Delta T_{heating} = 1,23 \times 52,157 \times 24,1 = 1546,09 W$$