



**POLITECNICO**  
MILANO 1863

# Esercitazione 06 - Cicli a gas

*Esercizio 05* ([link registrazione](#))

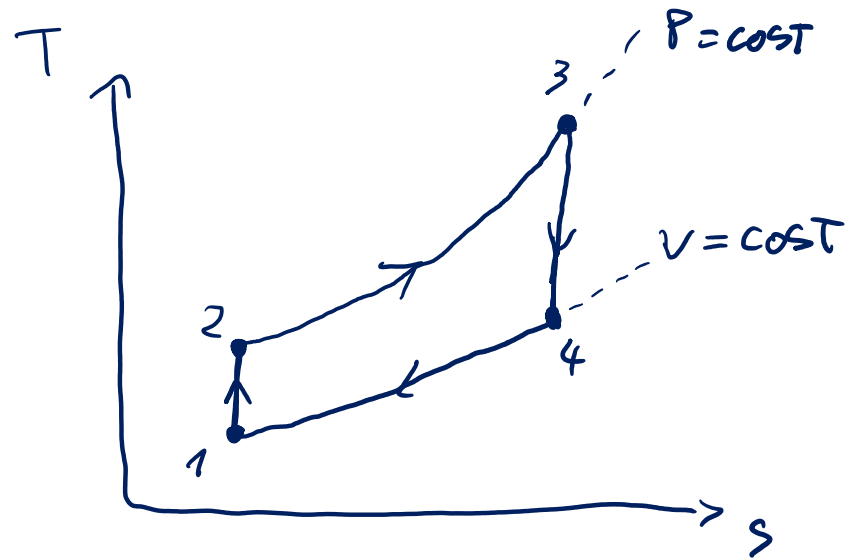
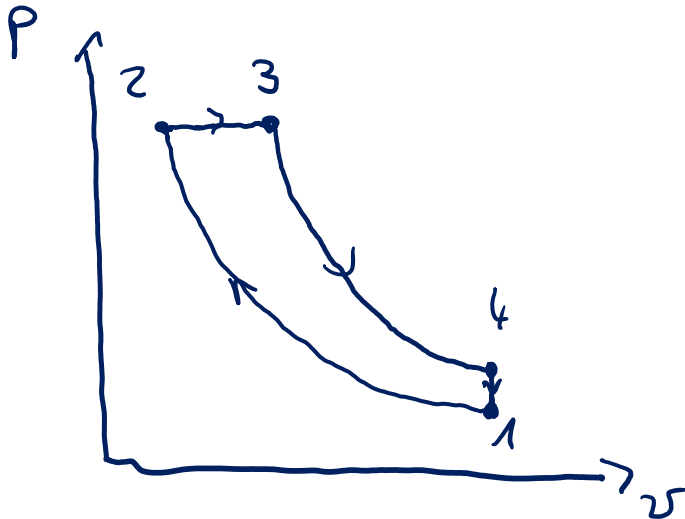
**Corso di Fisica Tecnica**  
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## Esercizio 05

6.5. [intermedio] Un motore a ciclo Diesel ideale a quattro cilindri ha cilindrata  $V = 1600 \text{ cm}^3$ . Il rapporto di compressione volumetrico è  $r = 15$ . La miscela aspirata all'inizio della fase di compressione ha pressione  $P_1 = 1 \text{ atm}$  e temperatura  $T_1 = 50^\circ \text{C}$ . Il rapporto di combustione è pari a  $z = 2,1$ . Ipotizzando di considerare la miscela aria-gasolio un gas ideale biatomico con massa molare  $M_m = 29 \text{ kg/kmol}$ , si chiede di caratterizzare il ciclo (determinando  $P$ ,  $T$ ,  $V$  per tutti gli stati del fluido, il lavoro specifico prodotto, il rendimento).

$$[l_N^+ = 631.8 \text{ kJ/kg}; \eta_I = 0.6]$$



## Esercizio 05

DATI:

$$V = 1600 \text{ cm}^3 = 0,0016 \text{ m}^3$$

$$\Omega = 15$$

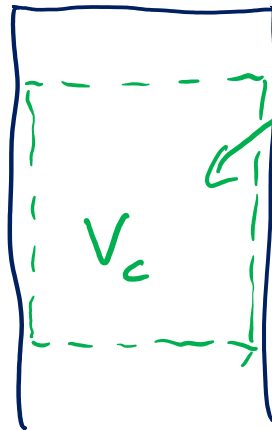
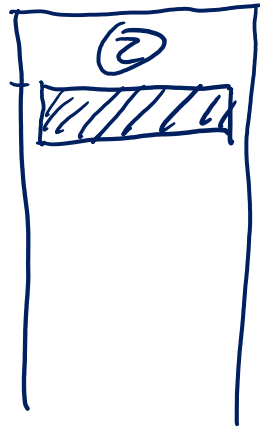
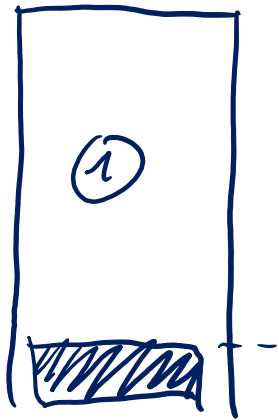
$$P_1 = 1 \text{ atm} = 101325 \text{ Pa}$$

$$T_1 = 50^\circ\text{C} = 323,15 \text{ K}$$

$$z = 2,1$$

$$M_m = 29 \text{ kg/kmol}$$

STATO	P (Pa)	T (K)	V (m <sup>3</sup> )
1	101325	323	0,0004286
2	4490273	954,7	0,0000286
3	4490273	2004,9	0,0000601
4	286320	913	0,0004286



CILINDRATA  
PER 1 CILINDRO

$$\hookrightarrow V_1 - V_2 = V_c$$

$$r = \frac{V_{\text{MAX}}}{V_{\text{MIN}}}$$

$$\begin{cases} V_c = V_1 - V_2 \\ r = \frac{V_1}{V_2} \end{cases} \Rightarrow V_1 = V_c \left( \frac{r}{r-1} \right)$$

$$V_c = \frac{V}{4} = 400 \text{ cm}^3$$

$$V_1 = 400 \left( \frac{15}{15-1} \right) = 428,6 \text{ cm}^3 = 0,0004286 \text{ m}^3$$

$$V_2 = \frac{V_1}{r}$$

$$V_2 = V_1 - V_c = 28,6 \text{ cm}^3 = 0,0000286 \text{ m}^3$$

$$z = \frac{V_3}{V_2} \Rightarrow V_3 = 2,1 \times 28,6 = 60,06 \text{ cm}^3 = 0,0000601$$

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1-2 ISOENTROPICA  $P V^k = \text{cost}$   $k = \frac{c_p}{c_v} = \frac{7}{5} = 1,4$

$$P_2 = P_1 \left( \frac{V_1}{V_2} \right)^k = 101325 \times 15^k$$

$$P_2 = 4490273 \text{ Pa}$$

$$T_2 \rightarrow \text{EdS G.I.} \quad P_2 V_2 = M R^* T_2$$

$$M = \frac{P_1 V_1}{R^* T_1} = 4,688 \times 10^{-4} \text{ kg}$$

$$T_2 = \frac{P_2 V_2}{M R^*} = 954,7 \text{ K}$$

$$T_3 = \frac{P_3 V_3}{M R^*} = 2004,9 \text{ K}$$

3-4 ISOENTROPICA  $PV^k = \text{cost}$

$$P_4 = P_3 \left( \frac{V_3}{V_4} \right)^k = 286320 \text{ Pa}$$

$$T_4 = \frac{P_4 V_4}{M R^*} = 913 \text{ K}$$

## BILANCI ENERGETICI

1-2) COMPRESSIONE  $\Delta U_{12} = \cancel{Q_{12}^{\leftarrow}} - \overset{\rightarrow}{L_{12}} \quad \overset{\leftarrow}{L_{12}} = M c_v (T_2 - T_1) \quad \text{G.P.}$

2-3) RISC. ISOBARO  $\Delta U_{23} = \overset{\leftarrow}{Q_{23}} - \overset{\rightarrow}{L_{23}} = M c_v (T_3 - T_2) \quad \text{G.P.}$

ISOBARA  $\rightarrow \overset{\leftarrow}{Q_{23}} = \overset{\text{G.P.}}{\Delta H_{23}} = M c_p (T_3 - T_2)$

$\overset{\rightarrow}{L_{23}} = \overset{\leftarrow}{Q_{23}} - \Delta U_{23} = M c_p (T_3 - T_2) - M c_v (T_3 - T_2)$

3-4) ESPANSIONE  $\Delta U_{34} = \cancel{Q_{34}^{\leftarrow}} - \overset{\rightarrow}{L_{34}} \quad \overset{\rightarrow}{L_{34}} = -\Delta U_{34} = M c_v (T_3 - T_4) \quad \text{G.P.}$

4-1) RAFFR. ISOCORO  $\Delta U_{41} = \overset{\leftarrow}{Q_{41}} - \cancel{L_{41}^{\rightarrow}} \quad \overset{\rightarrow}{Q_{41}} = -\Delta U_{41} = M c_v (T_1 - T_4) \quad \text{G.P.}$

$$\eta_{\text{DIESEL}} = \frac{L^{\rightarrow}}{Q_c^{\leftarrow}} = \frac{L_{34}^{\rightarrow} + L_{23}^{\rightarrow} - L_{12}^{\leftarrow}}{Q_{23}^{\leftarrow}} = \frac{Q_c^{\leftarrow} - Q_F^{\rightarrow}}{Q_c^{\leftarrow}} = 1 - \frac{Q_F^{\rightarrow}}{Q_c^{\leftarrow}}$$

$$\eta_{\text{DIESEL}} = 1 - \frac{\cancel{M} c_v (T_1 - T_4)}{\cancel{M} c_p (T_3 - T_2)} = 1 - \frac{1}{k} \frac{(T_1 - T_4)}{(T_3 - T_2)} = \underline{\underline{0,6}}$$

$$L^{\rightarrow} = L_{34}^{\rightarrow} + L_{23}^{\rightarrow} - L_{12}^{\leftarrow} = q_c^{\leftarrow} - q_F^{\rightarrow} = q_{23}^{\leftarrow} - q_{41}^{\rightarrow}$$

$$L^{\rightarrow} = c_p (T_3 - T_2) - c_v (T_1 - T_4) = \underline{\underline{631,8 \text{ kJ/kg}}}$$