

Fig. 1. Schematic diagram of the CSTR process.

## 1 Interpretable Incipient Fault Detection and Isolation with Cauchy-Schwarz Divergence

In the following, we perform experiments on the continuous stirred-tank heater (CSTH) process to demonstrate the interpretability of conditional CS divergence based fault isolation.

## 1.1 Application to CSTR Process

This section discusses the effectiveness of the proposed method in a closed-loop continuous stirred-tank reactor (CSTR) process, which is a common chemical system that designed especially for simulating incipient faults [1], [2], [3], [4]. The dynamic characteristics of CSTR process is described by mass balance and energy conservation,

$$\frac{dC}{dt} = \frac{Q}{V}(C_i - C) - akC + v_1,\tag{1}$$

$$\frac{dT}{dt} = \frac{Q}{V}(T_i - T) - a\frac{(\Delta H_r)kC}{\rho C_p} - b\frac{UA}{\rho C_p V}(T_i - T) + v_2,$$
(2)

$$\frac{dT_c}{dt} = \frac{Q_c}{V_c} (T_{ci} - T_c) + b \frac{UA}{\rho_c C_{pc} V_c} (T_c - T) + v_3,$$
(3)

where the input is  $\mathbf{u} = [C_i, T_i, T_{ci}]^T$ , the output is  $\mathbf{y} = [C, T, T_c, Q_c]^T$ ,  $v_i$  is process noise, and k is an Arrhenius-type rate constant with  $k = k_0 e^{(\frac{-E}{RT})}$ . It is worth noting that, input disturbances can bring out system dynamics, such that measurements are temporally correlated, non-Gaussian-distributed and noisy due to the process non-linearity.

TABLE 1
Parameter description in CSTR process.

Parameter	Description	Value			
Q	Inlet flow rate	$100.0\ L/min$			
V	Tank volume	150.0 L			
$V_c$	Jacket volume	$10.0 \; L$			
$\Delta H_r$	Chemical reaction heat	$-2.0 \times 10^5 \ cal/mol$			
UA	Heat transfer coefficient	$7.0 \times 10^5 \ cal/min/K$			
$k_0$	Pre-exponential factor to $k$	$7.2 \times 10^{10} \ min^{-1}$			
E/R	Activation energy and gas constant	$1.0 \times 10^4 \ K$			
$\rho, \rho_c$	Fluid density	$1000 \; g/L$			
$C_p, C_{pc}$	Fluid heat capacity	$1.0 \ cal/g/K$			
$v_1, v_2, v_3$	Gaussian noise	N(0, 0.01)			

The CSTR schematic in Fig. 1 shows the measurement locations and the control strategy: reactor temperature T is maintained by manipulating the coolant flow rate  $Q_c$ . In this application, we use the Simulink model developed by Pilario [2], available at https://www.mathworks.com/matlabcentral/fileexchange/66189-feedback-controlled-cstr-process-for-fault-simulation, details of parameters are described in Table. 1. The sampling interval is 1 min, 2000 points under normal conditions are collected as training data. Six variables are measure,  $\mathbf{x} = [C, T, T_c, Q, C_i, T_i]^T$ .

To evaluate the statistical power of CS divergence, 100 faulty data sets are generated from each scenario as Table. 2 shown, differing in the random seeds for process noise, measurement noise, and input disturbances. All testing sets have 1600 samples, with faults imposed since sample 201. Performance metrics for monitoring are averaged across all trials, the detailed results of FDR, FAR, and FDD are shown in Table. 3. As can be seen, most of methods have the FAR of 0 but not too early times of FDD, which suggests that an efficient way to reduce FDD deserves more investigations. Our proposed method obtains stable performance on all data sets in the sense that it has no failing cases, and even achieves compelling performance among others methods, demonstrating the effectiveness of CS divergence in distinguishing faulty

TABLE 2 Incipient fault scenarios in CSTR process.

Fault ID	Description	Value of $f$	Type	
$f_1$	$Q = Q_0 + \delta$	5	Additive bias	
$f_2$	$a = a_0 exp(-\delta t)$	0.0005	Multiplicative	
$f_3$	$b = b_0 exp(-\delta t)$	0.001	Multiplicative	
$f_4$	$f_1$ , $f_2$ simultaneous		Multiplicative	
$f_5$	$C_i = C_{i,0} + \delta t$	0.001	Additive	
$f_6$	$T_{ci} = T_{ci,0} + \delta t$	0.05	Additive	
$f_7$	$C = C_0 + \delta t$	0.001	Additive	
$f_8$	$T = T_0 + \delta t$	0.05	Additive	
$f_9$	$T_i = T_{i,0} + \delta t$	0.05	Additive	
$f_{10}$	$Q_c = Q_{c,0} + \delta t$	-0.1	Additive	

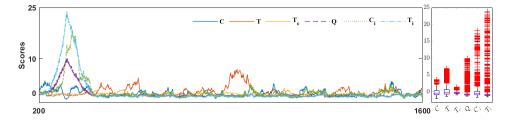


Fig. 2. Fault isolation results of  $f_1$  for CSTR process.

states from normal distribution. Compared with classical SMD, our method has no false alarms for  $f_1$  and  $f_2$ ; and has a good detectability of 92.64% for  $f_9$ , whereas SMD failed to detect it.

For fairness, we have incorporated the projection of PCA to both SMD and our algorithm, aligning with the Wasserstein distance method. After subspace projection, there is a significant improvement in shortening the detection delay of our proposed method. The bias fault  $f_1$  is identified at sample No.203, significantly earlier than the monitoring statistics of SMD (No.228) and Wasserstein distance (No.220). The average FDDs of our approach are 130, 133 and 60, especially the residual space can detect faults earlier than the SMD and WD based methods, highlighting its potential in incipient fault detection. In actual chemical engineering, timely detection of incipient faults can eliminate dangers at an early stage and maintain process safety.

For interpretability verification, we first evaluate the proposed fault isolation method on  $f_1$ , a sensor bias fault of 5 L/min is introduced to Q, corresponding to 201-th sample.  $f_1$  is an incipient fault since the bias 5L is small compared with the initial value 330.9L. If we look deeper, the conditional CS divergence is shown in Fig. 2. It presents the online sample-by-sample isolation result, we can observe that dimensions of Q,  $C_i$ ,  $T_i$  are most related to the fault. This makes sense, because the dependence between Q and  $\{C_i, T_i\}$  are shown in Eq. (1) and Eq. (2). It can be confirmed from the box-plot on the right that a large number of outliers appeared in these variables, and are concentrated on larger values, making the distribution right skewed.

Then we plot the result of monitoring based on conditional CS divergence in Fig. 3. From Fig. 3(a), the alarm points forming 8 phased stages. Their dependencies remain roughly the same in time period [200,303] (ascending) and [302,524] (descending), corresponding to Fig. 3(b). The 2-th dimension, controlled object T, contributes significantly to the 3-th stage due to the changes of its dependence structure Q. Therefore, our method provides more interpretability for dynamic monitoring.

## **ACKNOWLEDGMENT**

This work was supported by the National Natural Science Foundation of China under Grant 62003004.

## **REFERENCES**

- [1] D. Zhou, Y. Y, Modern Fault Diagnosis and Fault Tolerant Control, Tsing Hua University Publishing House: Beijing, 2000.
- [2] K. E. S. Pilario, Y. Cao, Canonical variate dissimilarity analysis for process incipient fault detection, IEEE Transactions on Industrial Informatics 14 (12) (2018) 5308–5315.
- [3] K. E. S. Pilario, Y. Cao, M. Shafiee, Mixed kernel canonical variate dissimilarity analysis for incipient fault monitoring in nonlinear dynamic processes, Computers & Chemical Engineering 123 (2019) 143–154.
- [4] Q. Jiang, D. S. X, Y. Wang, X. Yan, Data-driven distributed local fault detection for large-scale processes based on the ga-regularized canonical correlation analysis, IEEE Transactions on Industrial Electronics 64 (10) (2017) 8148–8157.

TABLE 3 The fault detection performance (%) for CSTR process.

No.	PCA		SMD		WD		CS			
	$T^2$	SPE		$\mathrm{MD}_z$	$\mathrm{MD}_e$	$W_z$	$W_e$		$CS_z$	$CS_e$
$f_1$	46.86	0.50	97.93	97.43	96.14	95.50	98.64	97.71	94.93	99.86
3.1	22.88	1.99	25.49	0	4.90	0	0	0	0	0
	1	246	28	37	55	64	20	33	71	3
$f_2$	69.50	47.86	76.86	75.21	75.36	71.36	76.64	69.93	69.50	85.71
	23.88	0.50	8.82	23.53	0	0	0	0	0	0
	10	59	10	133	346	382	235	419	33	33
$f_3$	84.14	2.43	94.28	87.28	96.35	69.35	89.57	85.78	70.71	93.93
	19.40	0.49	0	0	0	0	0	0	0	0
	4	79	57	86	<b>52</b>	427	147	200	360	19
$f_4$	80.85	49.07	90.07	90.21	95.93	73.71	87.57	81.21	76.64	90.96
	27.36	0.49	0	0	0	0	0	0	0	0
	8	62	110	137	<b>58</b>	344	175	237	326	129
$f_5$	83.36	89.36	94.85	95.43	85.93	94.91	93.29	94.64	94.93	93.29
	27.86	0.49	0	0.98	0	0	0	0	0	0
	1	64	73	65	198	72	95	76	<b>72</b>	8
$f_6$	80.00	92.78	96.29	97.29	89.50	97.28	89.14	96.71	96.57	89.71
	19.40	1.49	0	0	0	0	0	0	0	0
	3	49	53	<b>39</b>	146	39	151	50	49	145
$f_7$	27.86	48.07	85.93	83.07	29.79	89.43	50.86	92.36	91.71	61.50
	24.87	1.49	0	0	0	0	0	0	0	0
	2	67	64	153	566	124	558	<b>82</b>	83	44
$f_8$	89.93	25.14	94.92	93.21	98.86	88.43	92.79	93.07	89.21	94.71
	23.38	0.99	2.94	0	6.86	0	0	0	0	0
	14	211	71	92	17	163	102	11	147	<b>75</b>
$f_9$	92.57	38.14	3.64	93.64	98.86	89.57	93.86	92.64	89.29	95.29
	27.36	0	0	0	0	20.59	0	0	0	0
	8	130	419	86	17	146	87	104	148	67
$f_{10}$	85.50	11.79	90.42	93.36	95.00	87.79	94.36	93.57	88.50	94.36
	25.87	0	0.98	6.86	36.27	0	0	0	0	0
	2	82	135	93	71	165	<b>78</b>	91	45	<b>78</b>
Ave.FDR	74.06	40.51	82.52	90.61	86.17	85.74	77.67	89.76	86.20	89.93
Ave.FAR	24.23	0.79	3.82	3.14	4.80	2.06	0	0	0	0
Ave.FDD	5	104	102	92	152	192	164	130	133	60

The window lengths are all set as the commonly used 100. The significance level is set as 1%.  $MD_z$ ,  $MD_e$ ,  $W_z$ ,  $W_e$  and  $CS_z$ ,  $CS_e$  denote statistic patterns of principal and residual space in statistics Mahalanobis distance, Wasserstein distance and CS divergence based framework respectively.

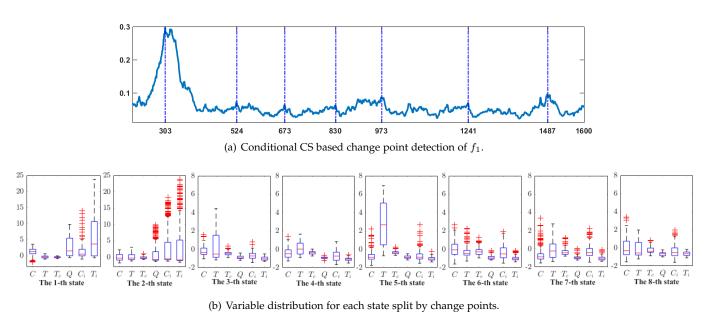


Fig. 3. The results of process monitoring based on change point detection of  $f_1$  for CSTR process.(a) Conditional CS based change point detection of  $f_1$ . The vertical lines indicate the change time of next state. (b) Variable distribution for each state split by change points.