ERQ I – Slide: Chemical Reactors

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- Ideal reactors dimensioning

- Isothermic and non-isothermic operations

• Catalysts preparation and characterization

1 General equaltion of molar balance

$$aA + bB + ... \longrightarrow dD + eE + ...$$

$$F_{i\,0}-F_{i\,1}+F_{i\,P}=rac{\mathrm{d}N_i}{\mathrm{d}t}$$

Molar balance to the limitant reagent A

$$F_{A\,0}/\mathrm{mol}\,(\mathrm{A})/\mathrm{L}\,(0)\,\mathrm{h}\,\,\mathrm{input}$$
 $F_{A\,P}/\mathrm{mol}\,(\mathrm{A})/\mathrm{L}\,\mathrm{h}\,\,\mathrm{produced}$ $F_{A\,1}/\mathrm{mol}\,(\mathrm{A})/\mathrm{L}\,(1)\,\mathrm{h}\,\,\mathrm{output}$ $\frac{\mathrm{d}N_A}{\mathrm{d}t}/\mathrm{mol}\,(\mathrm{A})/\mathrm{L}\,\mathrm{h}\,\,\mathrm{Acumulated}$

2 Reaction rate

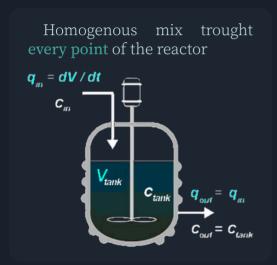
$$r_A = V^{-1}rac{\mathrm{d}N_A}{\mathrm{d}t} \hspace{0.5cm} r_A' = W^{-1}rac{\mathrm{d}N_A}{\mathrm{d}t} \hspace{0.5cm} r"_A = S^{-1}rac{\mathrm{d}N_A}{\mathrm{d}t}$$

$$\overline{t}$$

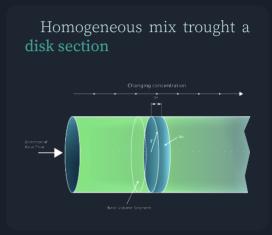
 $F_{AP} = \int_V r_A \; \mathrm{d}V$

3 Ideal reactors

CSTR: Continuous stirred-tank reactor



PFR: Plug flow reactor model



Batch: Similar to CSTR but descontinous (no input/output)

4 How to balance each reactor

General equation

$$F_{i\,0}-F_{i\,1}+F_{i\,P}=rac{\mathrm{d}N_i}{\mathrm{d}t}$$

X: Conversion

$$X = 1 - N_{i\,1}/N_{i\,0} = 1 - F_{i\,1}/F_{i\,0}$$

4.1 Continuous reactors

Steady State: Maintaining constant all functioning conditions (input current, temperature, pressure, ...), after a certain time the reactor reaches a steady state where all the output parameters (caudal, concentration, temperature, ...) become constant in time.

Spatial time:

$$au = rac{V ext{ (reactor volume)}}{v ext{ (volumetric caudal)}}$$

4.2 Batch balance



$$r_i\,V = rac{\mathrm{d}N_i}{\mathrm{d}t} \iff t = C_{i\,0}\,\int_0^X rac{\mathrm{d}X}{-r_A};$$
 $\left(egin{array}{c} F_{i\,0} = F_{i\,1} = 0 ext{ (No input/output)} \ \int_{\Gamma} r_i \,\mathrm{d}V = r_i\,V ext{ (Continously agitated)} \end{array}
ight)$

$$F_{i0} + F_{i1} + F_{iP} = F_{iP} = \int_{V} r_i \, dV = r_i \int_{V} dV = r_i V = \frac{dN_i}{dt};$$

$$X = 1 - N_{i1}/N_{i0} \implies N_{i1} = N_{i0}(1 - X) \implies$$

$$\implies \frac{\mathrm{d}N_i}{\mathrm{d}t} = \frac{\mathrm{d}N_{i0}(1-X)}{\mathrm{d}t} = -N_{i0}\frac{\mathrm{d}X}{\mathrm{d}t}r_iV \implies$$

$$\implies \int_0^t \mathrm{d}t = t = \int_0^X \frac{-N_{i0}}{r_iV} \,\mathrm{d}X = \frac{N_{i0}}{V} \int_0^X \frac{\mathrm{d}X}{-r_i} = C_{i0} \int_0^X \frac{\mathrm{d}X}{-r_i}$$

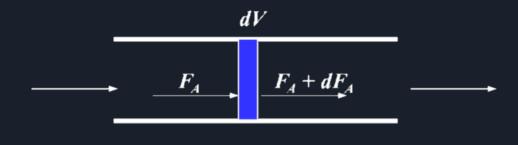
4.3 CSTR balance

$$egin{aligned} F_{A heta} & C_{A heta} \ X_{ heta} &= egin{aligned} F_A & C_A \ X & X & X \end{aligned}$$
 $au = C_{i\,0}\,rac{X}{-r_i};$ $au = C_{i\,0}\,rac{X}{-r_i};$ $au = 0 ext{ (Steady state)}$ $au = \int_V r_A \; \mathrm{d}V = r_A \, V ext{ (Continously agitated)} \end{aligned}$

$$F_{i0} - F_{i1} + F_{iP} = F_{i0} - (F_{i0}(1 - X)) + (r_i V) = F_{i0} X + r_i V = (v_0 C_{i0}) X + r_i V =$$

$$= \frac{dN_A}{dt} = 0 \implies \frac{V}{v_0} = \tau = C_{i0} \frac{X}{-r_i}$$

4.4 PFR Balance



$$au = C_{i\,0} \int_0^X rac{\mathrm{d} X}{-r_A};$$

(steady state elementar disk)

$$\begin{split} F_{ij} - F_{i(j+1)} + F_i &= F_{ij} - (F_{ij} + \mathrm{d}F_{ij}) + (r_i \, \mathrm{d}V) = -\, \mathrm{d}F_{ij} + r_i \, \mathrm{d}V = \\ &= -\, \mathrm{d}F_{i0}(1-X) + r_i \, \mathrm{d}V = F_{i0} \, \mathrm{d}X + r_i \, \mathrm{d}V = (C_{i0} \, v_0) \, \mathrm{d}X + r_i \, \mathrm{d}V = \\ &= \frac{\mathrm{d}N_i}{\mathrm{d}t} = 0 \implies \\ &\implies \frac{1}{v_0} \int_0^V \mathrm{d}V \frac{V}{v_0} = \tau = \int_0^X C_{i0} \frac{\mathrm{d}X}{-r_i} = C_{i0} \int_0^X \frac{\mathrm{d}X}{-r_i} \end{split}$$