I – Bioreactor Kinetics

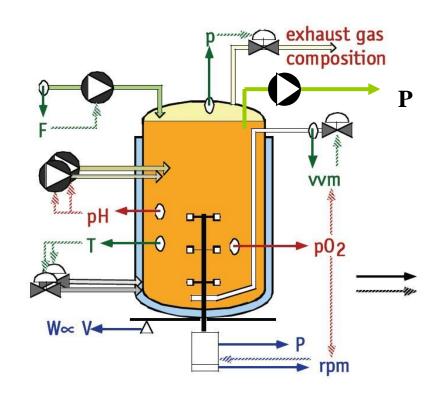


Introduction

- 1 Batch Reactor (BSTR)
- 2 Continuous Reactor (CSTR)
 - 2.1 Mass balance to the cell concentration
 - 2.2 Mass balance to the substrate
 - 2.3 Relationship between substrate concentration and cell concentration with dilution rate
 - 2.4 Cell Productivity
 - 2.5 Effect of the maintenance coefficient
 - 2.6 Product production
 - 2.7 Cell recirculation reactors

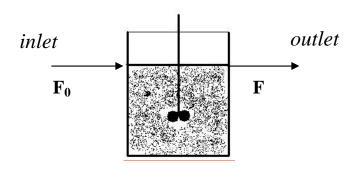


Continuous Stirred Tank Reactor - CSTR

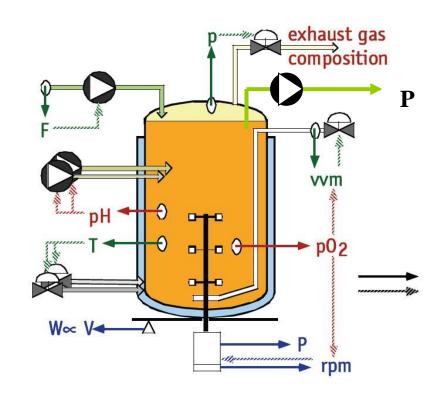




Continuous Stirred Tank Reactor - CSTR

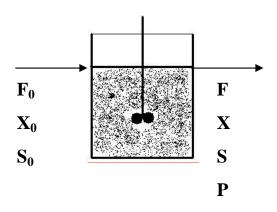


F – flow rate (1/h)





Continuous Stirred Tank Reactor - CSTR

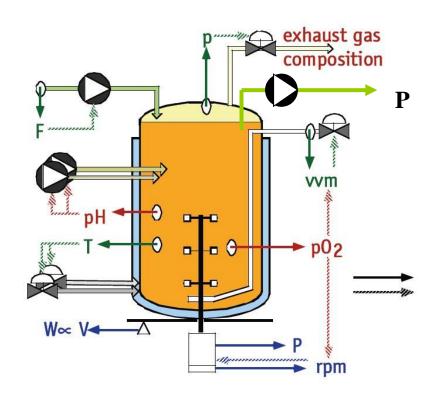


F – flow rate (1/h)

x – cell concentration (gX/l)

S – substrate concentration (gS/l)

P – product concentration (gP/l)



$$\frac{dx}{dt} = \frac{F_0}{V} x_0 - \frac{F}{V} x + \mu x - k_d x$$

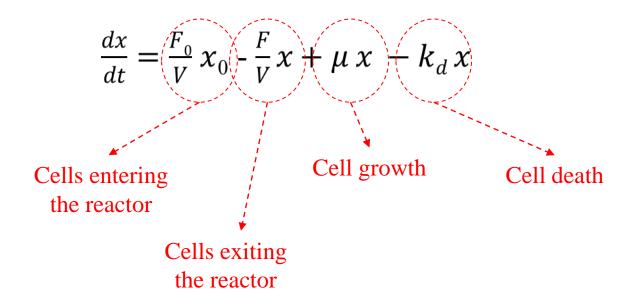
 F_0 – inlet flow rate (l/h)

V - volume of the reactor (1)

k_d – specific cell death rate (h⁻¹)

 x_0 - inlet cell concentration (gX/l)

with $F_0 = F$



$$\frac{dx}{dt} = \frac{F_0}{V} x_0 - \frac{F}{V} x + \mu x - k_d x$$

 F_0 – inlet flow rate (1/h)

V - volume of the reactor (l)

k_d – specific cell death rate (h⁻¹)

 x_0 - inlet cell concentration (gX/l)

with $F_0 = F$

In most fermentations ($x_0 = 0$) and ($\mu \gg k_d$):

$$\frac{dx}{dt} = -\frac{F}{V}x + \mu x$$

$$\frac{F}{V} = D = \frac{1}{TRH}$$

D - dilution rate (h⁻¹) TRH - hydraulic retention time (h)

$$\frac{dx}{dt} = -\frac{F}{V}x + \mu x \qquad \longrightarrow \qquad \frac{dx}{dt} = \mu x - Dx$$

$$\frac{F}{V} = D$$



$$\frac{dx}{dt} = -\frac{F}{V}x + \mu x \qquad \longrightarrow \qquad \frac{dx}{dt} = \mu x - Dx$$

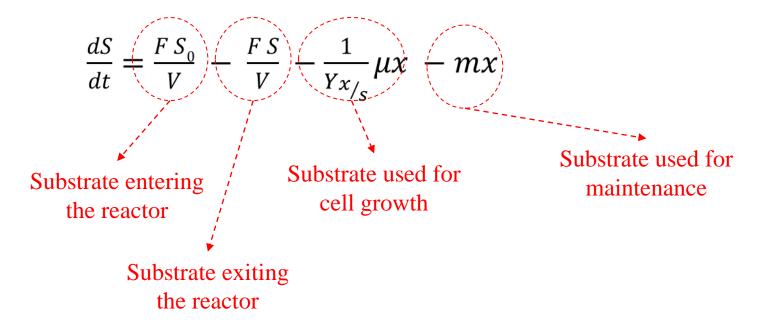
In steady state:
$$\frac{dx}{dt} = 0$$

$$D x = \mu x$$
 \longrightarrow $\mu = D$

In steady state, without cell death and sterile feeding:

$$\mu=D$$

$$\frac{dS}{dt} = \frac{FS_0}{V} - \frac{FS}{V} - \frac{1}{Yx_{/s}}\mu x - mx$$



$$\frac{dS}{dt} = \frac{FS_0}{V} - \frac{FS}{V} - \frac{1}{Yx_{/s}}\mu x - mx$$

$$\frac{F}{V} = D$$

$$\frac{dS}{dt} = D S_0 - D S - \frac{1}{Y_{x/s}} \mu x - mx$$

if m is negligible ($mx \ll \mu x$):

$$\frac{dS}{dt} = D \left(S_0 - S \right) - \frac{1}{Y_{x/s}} \mu x$$

In steady state

$$\frac{dS}{dt} = 0$$

$$D(S_0 - S) = \frac{1}{Y_{x/s}} \mu x$$

$$\mu = D$$

$$D(S_0 - S) = \frac{1}{Y_{x/s}} Dx$$

$$Y_{x/s} (S_0 - S) = x$$

$$\mu = \frac{\mu_{\text{max}} S}{K_s + S}$$

In a continuous reactor under steady state

$$D = \frac{\mu_{\text{max}} S}{K_s + S}$$

Rearranging for S

$$S = \frac{K_s D}{\mu_{max} - D}$$

$$S = \frac{K_s D}{\mu_{max} - D}$$

$$Y_{x/s} (S_0 - S) = x$$

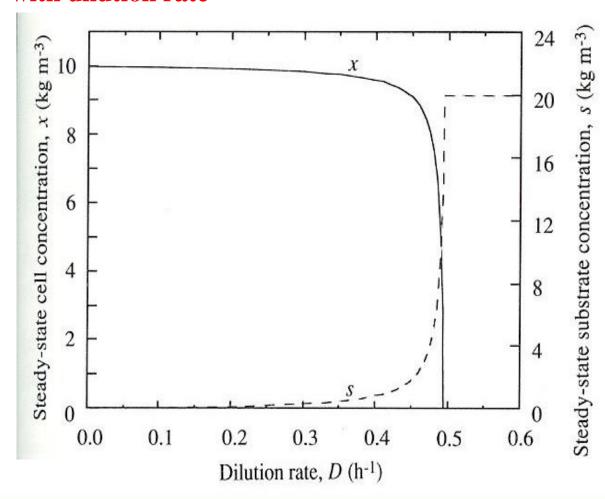
$$x = Y_{x/s} \left(S_0 - \frac{K_s D}{\mu_{max} - D} \right)$$

when
$$D \rightarrow 0$$

 $S \rightarrow 0$

$$x=Y_{x/s}\;S_0$$





For high dilution rates:

- X decreases sharply
- S is not consumed $\rightarrow S_0$



The value at which x=0 and D ~ μ_{max} is named the critical washout rate D_c

At this D value we have an "washout" of the reactor

$$D_c = \frac{\mu_{\text{max}} S_0}{K_s + S_0}$$

If
$$S_0 \gg K_s$$
 then $D_c = \mu_{max}$

This point is very sensitive: a small variation of D gives a large variation of X or S





$$DX = Y_{x/s} D \left(S_0 - \frac{K_s D}{\mu_{max} - D} \right)$$

Maximum productivity is obtained for:

$$\frac{dDx}{dD} = 0$$

Then:

$$D_{\text{max}} = \mu_{\text{max}} \left[1 - \left(\frac{K_s}{K_s + S_0} \right)^{1/2} \right]$$

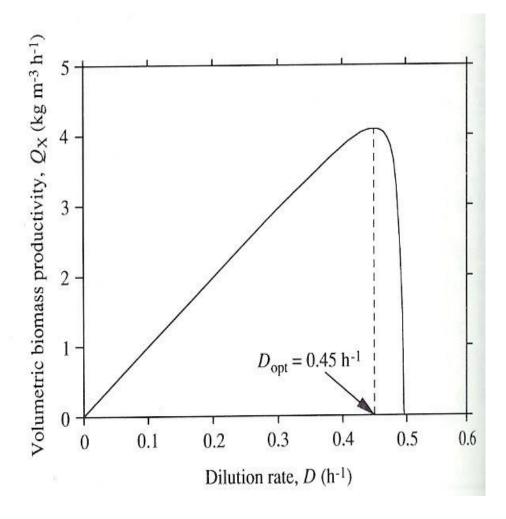
When $S_0 > Ks \rightarrow \mu = \mu_{max}$, near washout.

The cell concentration corresponding to the point of maximum productivity is given by:

$$X_{m} = Y_{x/s} (S_{0} + K_{s} - [K_{s} (S_{0} + K_{s})]^{1/2})$$

For
$$S_0 \gg K_s$$
 $D_{max} X_m = D_{max} Y_{x/s} S_0$

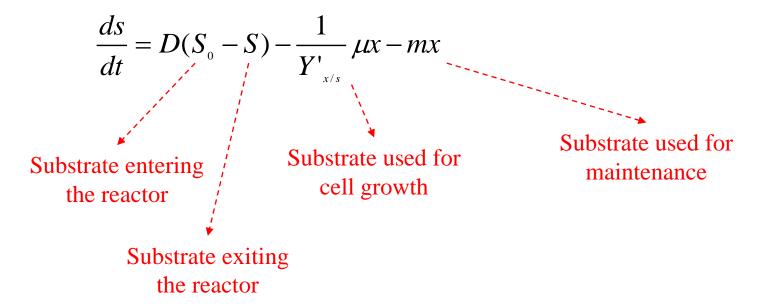




The productivity:

- Increases with the dilution rate until D_{opt}
- Decreases sharply after D_{opt}
 → zero

2.5 – Effect of the maintenance coefficient



2.5 – Effect of the maintenance coefficient

$$\frac{ds}{dt} = D(S_0 - S) - \frac{1}{Y'_{x/s}} \mu x - mx$$

In steady state:
$$\frac{ds}{dt} = 0 \implies D(S_0 - S) = \frac{1}{Y'_{x/s}} Dx + mx$$

$$x = \frac{D(S_0 - S)}{\frac{1}{Y'_{x/s}}D + m}$$

or
$$x = \frac{S_0 - S}{\frac{1}{Y'_{x/s}} + \frac{m}{D}}$$

2 – Continuous Reactor



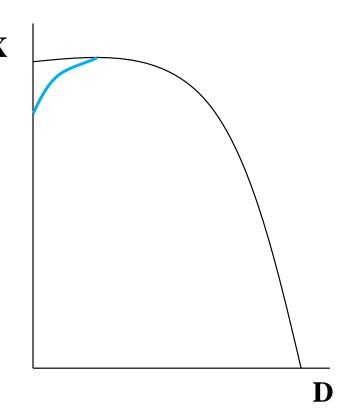
2.5 – Effect of the maintenance coefficient

$$x = \frac{S_0 - S}{\frac{1}{Y'_{x/s}} + \frac{m}{D}}$$



For high D values: X does not depend on m

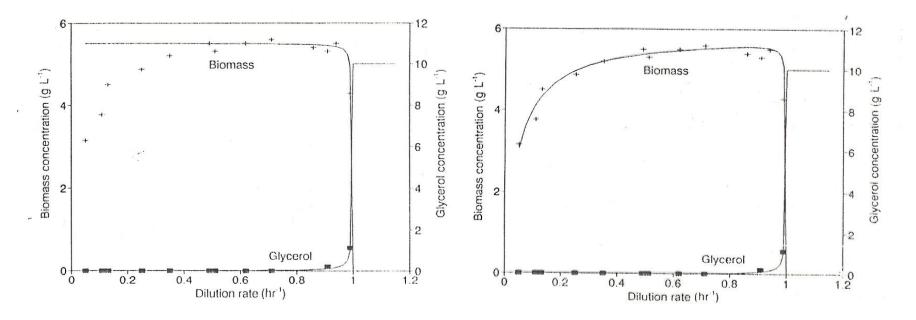
$$x = \frac{S_0 - S}{\frac{1}{Y'_{x/s}} + \frac{m}{D}} \longrightarrow x = \frac{S_0 - S}{\frac{1}{Y'_{x/s}}}$$



2 – Continuous Reactor



2.5 – Effect of the maintenance coefficient



Monod model aplied to CSTR

$$x = Y_{x/s} \left(S_0 - \frac{K_s D}{\mu_{max} - D} \right)$$

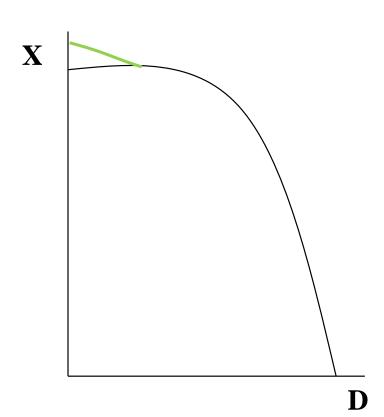
Monod model aplied to CSTR considering the cell maintenance

$$x = \frac{D(S_0 - S)}{\frac{1}{Y'_{x/s}}D + m}$$

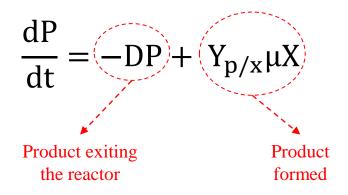


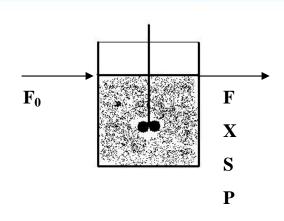
2.5 – Effect of the maintenance coefficient

increase in biomass weight due to the production of intracellular reserves



2.6.1- Product associated to growth



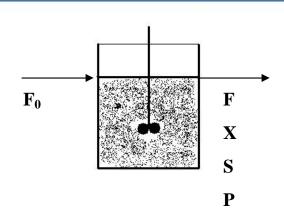


2.6.1- Product associated to growth

$$\frac{dP}{dt} = -DP + Y_{p/x}\mu X$$

At steady-state

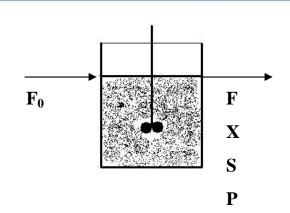
$$\frac{\mathrm{dP}}{\mathrm{dt}} = 0$$



2.6.1- Product associated to growth

$$\frac{\mathrm{dP}}{\mathrm{dt}} = -\mathrm{DP} + \mathrm{Y}_{\mathrm{p/x}} \mu \mathrm{X}$$

 $\Leftrightarrow V_p = Y_{p/x} \mu$



At steady-state

$$\frac{dP}{dt} = 0 \implies DP = Y_{p/x}\mu X \qquad \text{(Volumetric productivity (gP/l.h))}$$

$$\Leftrightarrow \frac{D.P}{X} = Y_{p/x}\mu$$

(Specific productivity (gP/gX.h))



2.6.1- Product associated to growth

$$X = Y_{x/s}(S_0 - S)$$

$$S = \frac{K_s D}{\mu_{max} - D}$$

$$X = Y_{x/s} \left(S_0 - \frac{K_s D}{\mu_{max} - D} \right)$$

$$DP = Y_{p/x} \mu X \Leftrightarrow DP = Y_{p/x} DX$$

At steady-state

$$D = \mu$$



2.6.1- Product associated to growth

$$X = Y_{x/s}(S_0 - S)$$

$$S = \frac{K_s D}{\mu_{max} - D}$$

$$X = Y_{x/s} \left(S_0 - \frac{K_s D}{\mu_{max} - D}\right)$$

$$DP = Y_{p/x}\mu X \Leftrightarrow DP = Y_{p/x}DX$$

$$\Leftrightarrow DP = Y_{p/x}DY_{x/s} \left(S_0 - \frac{K_s D}{\mu_{max} - D} \right)$$



2.6.1- Product associated to growth

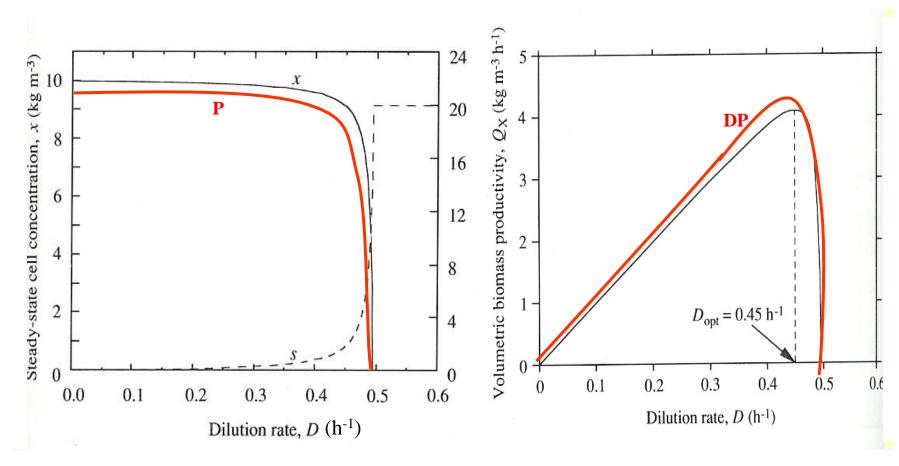
$$DP = Y_{p/x}DY_{x/s} \left(S_0 - \frac{K_s D}{\mu_{max} - D}\right)$$

$$\Leftrightarrow DP = Y_{p/s}D\left(S_0 - \frac{K_s D}{\mu_{max} - D}\right)$$

Product concentration (P) and volumetric productivity (DP) follow the same trend of X and DX as a function of D (see figure below, lines in red).



2.6.1- Product associated to growth





2.6.1- Product associated to growth

$$DP = Y_{p/s}D\left(S_0 - \frac{K_s D}{\mu_{max} - D}\right) \Leftrightarrow P = Y_{p/s}\left(S_0 - \frac{K_s D}{\mu_{max} - D}\right)$$



2.6.1- Product associated to growth

$$DP = Y_{p/s}D\left(S_0 - \frac{K_s D}{\mu_{max} - D}\right) \Leftrightarrow P = Y_{p/s}\left(S_0 - \frac{K_s D}{\mu_{max} - D}\right)$$

The maximum productivity is obtained for D_{max}

max

At this point the product concentration is:

$$D_{\text{max}} = \mu_{\text{max}} \left[1 - \left(\frac{K_s}{K_s + S_0} \right)^{1/2} \right]$$

$$P_{\rm m} = Y_{\rm p/s} (S_0 + K_{\rm s} - (K_{\rm s}(S_0 + K_{\rm s}))^{1/2})$$

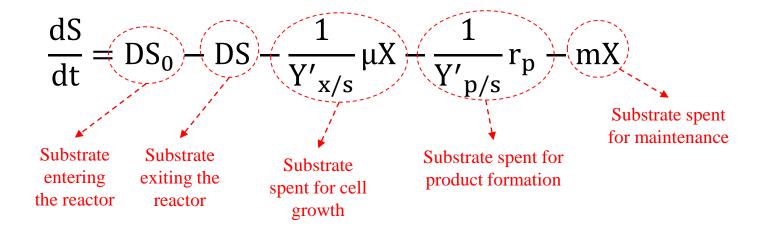
2.6.1- Product partially associated to growth

Mass balance to the substrate:

$$\frac{dS}{dt} = DS_0 - DS - \frac{1}{Y'_{x/s}} \mu X - \frac{1}{Y'_{p/s}} r_p - mX$$

2.6.1- Product partially associated to growth

Mass balance to the substrate:



2.6.1- Product partially associated to growth

Mass balance to the substrate:

$$\frac{dS}{dt} = DS_0 - DS - \frac{1}{Y'_{x/s}} \mu X - \frac{1}{Y'_{p/s}} r_p - mX$$

$$V_{p} = \frac{r_{p}}{X} \Leftrightarrow r_{p} = V_{p} X$$

$$\frac{dS}{dt} = DS_0 - DS - \frac{1}{Y'_{x/s}} \mu X - \frac{1}{Y'_{p/s}} V_p X - mX$$

$$\Leftrightarrow \frac{dS}{dt} = D(S_0 - S) - (\frac{1}{Y'_{x/s}} \mu + \frac{1}{Y'_{p/s}} V_p + m) X$$



2.6.1- Product partially associated to growth

$$\frac{dS}{dt} = D(S_0 - S) - (\frac{1}{Y'_{x/S}} \mu + \frac{1}{Y'_{p/S}} V_p + m) X$$

$$D = \mu$$

$$\frac{dS}{dt} = 0$$

$$D(S_0 - S) = (\frac{1}{Y'_{x/s}}D + \frac{1}{Y'_{p/s}}V_p + m)X$$

$$\Leftrightarrow X = \frac{D(S_0 - S)}{\frac{D}{Y'_{x/s}} + \frac{1}{Y'_{p/s}} V_p + m}$$



2.6.1- Product partially associated to growth

$$\frac{dP}{dt} = -DP + V_pX$$

$$\Leftrightarrow \frac{dP}{dt} = -DP + (Y'_{p/x} \mu + m_p) X$$

$$\Leftrightarrow$$
 DP = $(Y'_{p/x} \mu + m_p) X$

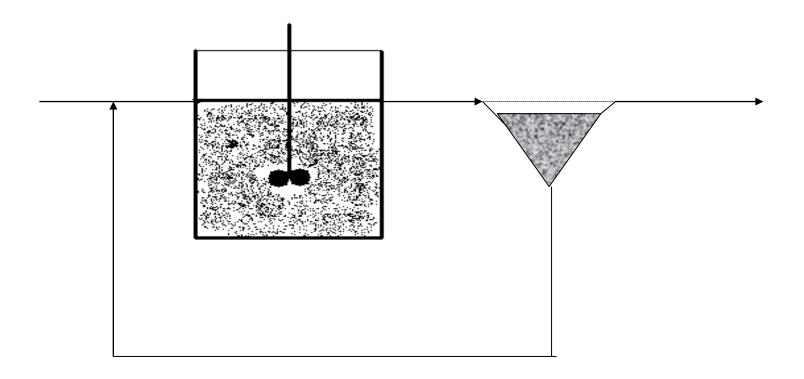
$$V_p = Y'_{p/x} \mu + m_p$$

At steady-state
$$D = \mu$$

$$\frac{\mathrm{dS}}{\mathrm{dt}} = 0$$



With a decanter





Membrane bioreactors

Type of membranes

- Dense
- Microporous

Configurations

- External circuit membrane
- Submerged membrane

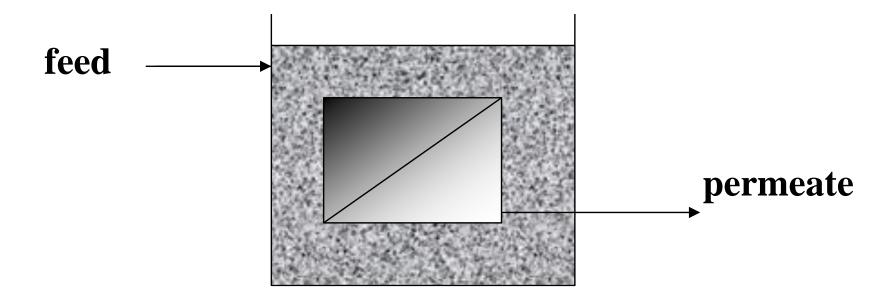
Applications

- Chemicals production
- Treatment of gaseous or liquid effluents



Membrane bioreactors

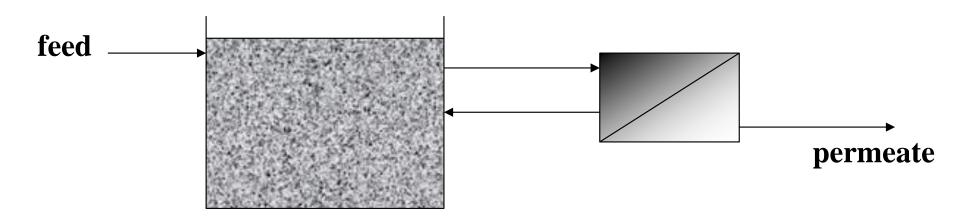
Submerged membrane bioreactor





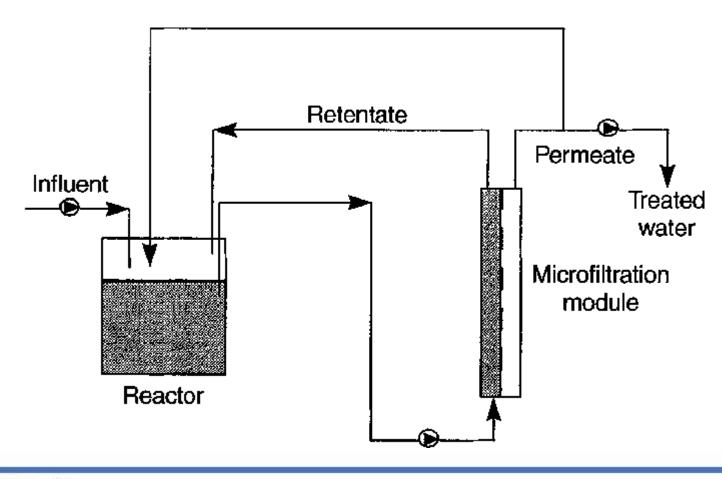
Membrane bioreactors

Membrane bioreactor with cell recirculation



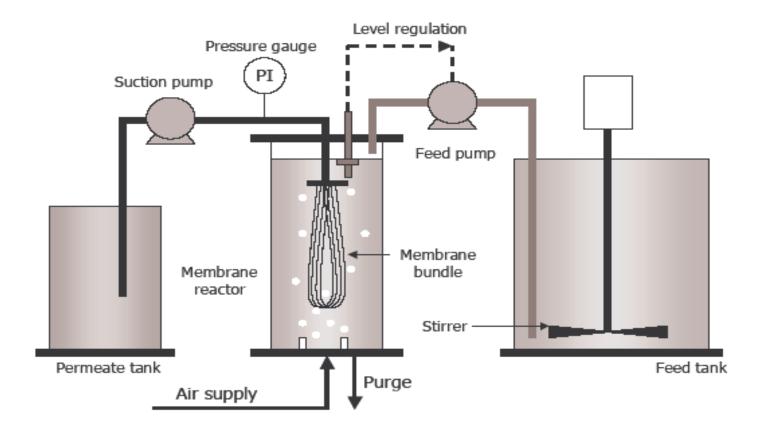


Membrane bioreactors

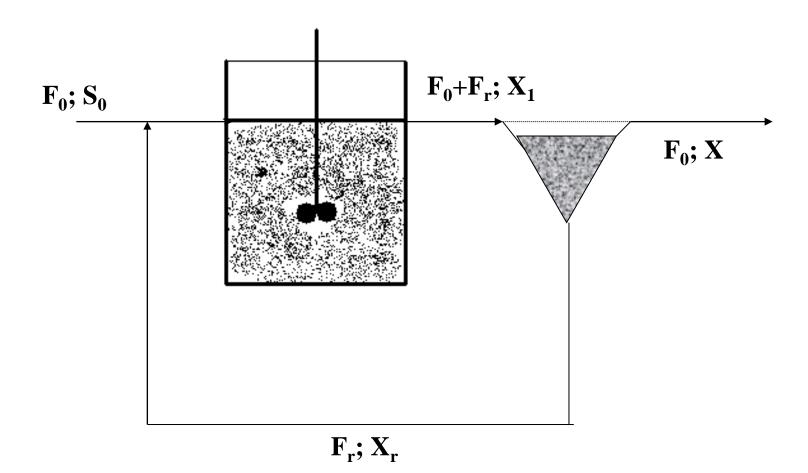




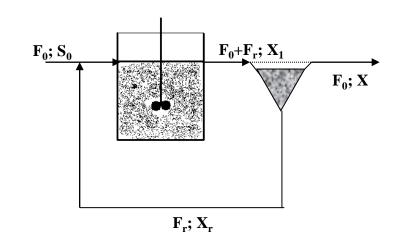
Submerged membrane bioreactors



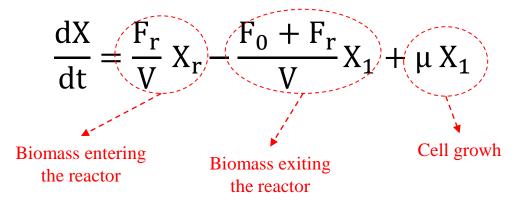


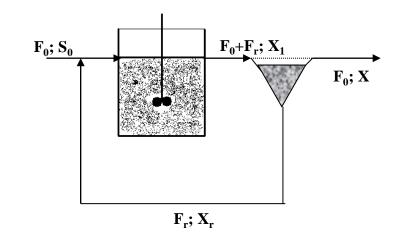


$$\frac{dX}{dt} = \frac{F_r}{V} X_r - \frac{F_0 + F_r}{V} X_1 + \mu X_1$$









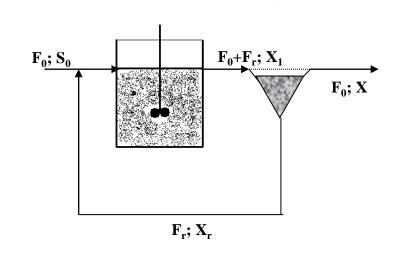


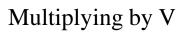
$$\frac{dX}{dt} = \frac{F_r}{V} X_r - \frac{F_0 + F_r}{V} X_1 + \mu X_1$$

At steady-state
$$\frac{dX}{dt} = 0$$

$$0 = \frac{F_r}{V} X_r - \frac{F_0 + F_r}{V} X_1 + \mu X_1$$

$$\Leftrightarrow 0 = F_r X_r - (F_0 + F_r) X_1 + \mu X_1 V$$

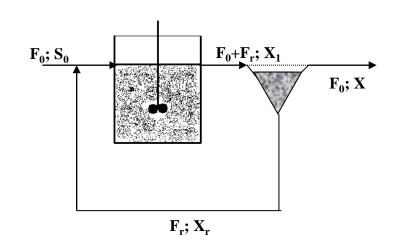




$$0 = F_r X_r - (F_0 + F_r) X_1 + \mu X_1 V$$

If
$$a = \frac{F_r}{F_0}$$
 $b = \frac{x_r}{x_1}$ $D = \frac{F_0}{V}$

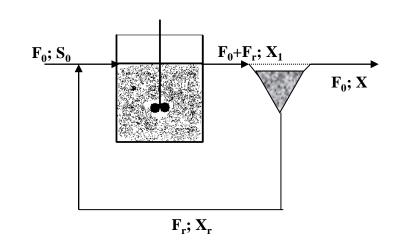
Then:
$$D = \frac{\mu}{1 - a(b-1)}$$





Balance to the substrate:

$$\frac{dS}{dt} = D(S_0 - S) - \frac{\mu X_1}{Y_{x/s}} = 0$$



$$a = \frac{F_r}{F_0}$$
 $b = \frac{x_r}{x_s}$ $D = \frac{F_0}{V}$ $\longrightarrow \mu x_1 = \frac{\mu Y_{x/s}(S_0 - S)}{1 - a(b - 1)}$

The rate of biomass production increases with a factor: $[1-a (b-1)]^{-1}$



Comparison of reactors with and without cell recirculation

