

# ERQ II – Exercises

Felipe B. Pinto 61387 – MIEQB

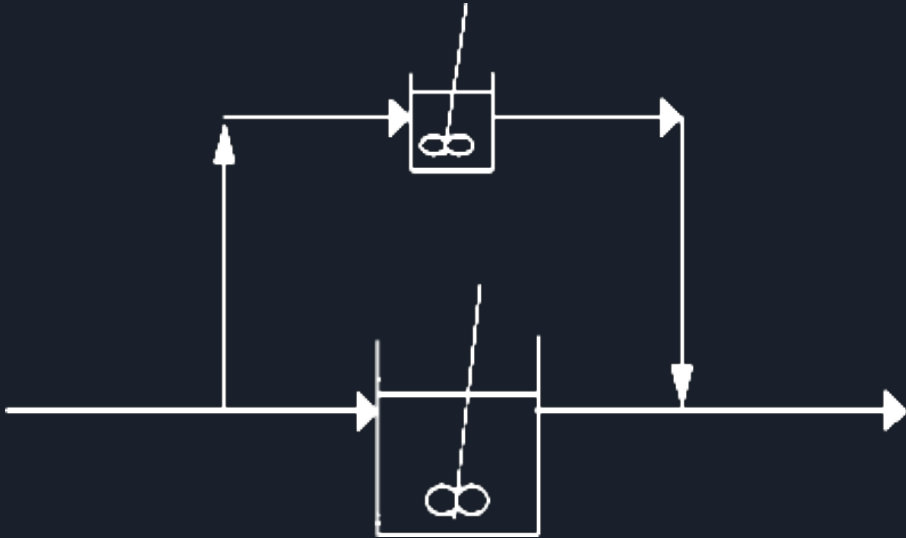
24 de maio de 2024

## Conteúdo

Questão 2	. . . . .	2	Questão 13	. . . . .	12
Questão 4	. . . . .	7			

## Questão 2

Considere um reactor CSTR cujo comportamento não ideal pode ser modelado pela associação de reactores ideais em “by-pass”, esquematizada na figura.



Transformadas de Laplace:

$f(s)$	$F(t)$
$\frac{1}{s-a}$	$e^{at}$

Q2 a.

Escreva as equações do modelo que representa o escoamento no reactor.

Resposta

Reator	Volume	Caldal In	Caldal Out
1	$(1 - \alpha) V$	$(1 - \beta) \nu$	$(1 - \beta) \nu$
2	$\alpha V$	$\beta \nu$	$\beta \nu$

$R_1 :$

$$(1 - \beta) \nu C_{in,1} = (1 - \beta) \nu C_{in} = \\ = (1 - \beta) \nu C_{out,1} + (1 - \alpha) V \frac{dC_{out,1}}{dt};$$

$R_2 :$

$$\beta \nu C_{in,2} = \beta \nu C_{in} = \beta \nu C_{out,2} + \alpha V \frac{dC_{out,2}}{dt};$$

Nó:

$$\nu C_{out} = \beta \nu C_{out,2} + (1 - \beta) \nu C_{out,1}$$

## Q2 b.

Deduza a expressão da distribuição de tempos de residência.

Resposta

$$E(t) = \mathcal{L} g(s);$$

$g(s)$  :

$$g(s) = \bar{C}_{out}/\bar{C}_{in} = \mathcal{L} C_{out}/\mathcal{L} C_{in};$$

$$\nu C_{out} = \beta \nu C_{out,2} + (1 - \beta) \nu C_{out,1} \implies$$

$$\implies C_{out} = \beta C_{out,2} + (1 - \beta) C_{out,1} \implies$$

$$\implies \mathcal{L} C_{out} = \bar{C}_{out} = \beta \bar{C}_{out,2} + (1 - \beta) \bar{C}_{out,1} \implies$$

$$\implies g(s) = \frac{\bar{C}_{out}}{\bar{C}_{in}} = \beta \frac{\bar{C}_{out,2}}{\bar{C}_{in}} + (1 - \beta) \frac{\bar{C}_{out,1}}{\bar{C}_{in}};$$

$\bar{C}_{out,1}$  :

$$(1 - \beta) \nu C_{in} = (1 - \beta) \nu C_{out,1} + (1 - \alpha) V \frac{dC_{out,1}}{dt} \implies$$

$$\implies (1 - \beta) C_{in} = (1 - \beta) C_{out,1} + (1 - \alpha) \tau \frac{dC_{out,1}}{dt} \implies$$

$$\implies \mathcal{L} ((1 - \beta) C_{in}) = (1 - \beta) \bar{C}_{in} =$$

$$= \mathcal{L} ((1 - \beta) C_{out,1}) + \mathcal{L} \left( (1 - \alpha) \tau \frac{dC_{out,1}}{dt} \right) =$$

$$= (1 - \beta) \bar{C}_{out,1} + (1 - \alpha) \tau s \bar{C}_{out,1} \implies$$

$$\implies \frac{\bar{C}_{out,1}}{\bar{C}_{in}} = \frac{1 - \beta}{1 - \beta + (1 - \alpha) \tau s};$$

$\bar{C}_{out,2}$  :

$$\beta \nu C_{in} = \beta \nu C_{out,2} + \alpha V \frac{dC_{out,2}}{dt} \implies$$

$$\implies \beta C_{in} = \beta C_{out,2} + \alpha \tau \frac{dC_{out,2}}{dt} \implies$$

$$\implies \mathcal{L} (\beta C_{in}) = \beta \bar{C}_{in} =$$

$$= \mathcal{L} (\beta C_{out,2}) + \mathcal{L} \left( \alpha \tau \frac{dC_{out,2}}{dt} \right) =$$

$$= \beta \bar{C}_{out,2} + \alpha \tau s \bar{C}_{out,2} \implies$$

$$\implies \frac{\bar{C}_{out,2}}{\bar{C}_{in}} = \frac{\beta}{\beta + \alpha \tau s};$$

$$\implies g(s) = \beta \frac{\beta}{\beta + \alpha \tau s} + (1 - \beta) \frac{1 - \beta}{1 - \beta + (1 - \alpha) \tau s} =$$

$$= \frac{\beta^2}{\alpha \tau} \left( \frac{1}{\frac{\beta}{\alpha \tau} + s} \right) + \frac{(1 - \beta)^2}{(1 - \alpha) \tau} \left( \frac{1}{\frac{1 - \beta}{(1 - \alpha) \tau} + s} \right) \implies$$

$$\implies \mathcal{L} g(s) = \frac{\beta^2}{\alpha \tau} \exp \left( -\frac{\beta}{\alpha \tau} t \right) + \frac{(1 - \beta)^2}{(1 - \alpha) \tau} \exp \left( -\frac{1 - \beta}{(1 - \alpha) \tau} t \right)$$

Q2 c.

Deduza a expressão da função cumulativa.

---

---

Resposta

Função culmulativa:

$$\begin{aligned} F(t) &= \int_0^t E(t) \, dt = \\ &= \int_0^t \left( \frac{\beta^2}{\alpha \tau} \exp \left( -\frac{\beta}{\alpha \tau} t \right) + \frac{(1-\beta)^2}{(1-\alpha)\tau} \exp \left( -\frac{1-\beta}{(1-\alpha)\tau} t \right) \right) dt = \\ &= \frac{\beta^2}{\alpha \tau} \int_0^t \exp \left( -\frac{\beta}{\alpha \tau} t \right) dt + \\ &+ \frac{(1-\beta)^2}{(1-\alpha)\tau} \int_0^t \exp \left( -\frac{1-\beta}{(1-\alpha)\tau} t \right) dt = \\ &= \frac{\beta^2}{\alpha \tau} \frac{\alpha \tau}{\beta} \Delta - \exp \left( -\frac{\beta}{\alpha \tau} t \right) \Big|_0^t + \\ &+ \frac{(1-\beta)^2}{(1-\alpha)\tau} \frac{(1-\alpha)\tau}{1-\beta} \Delta - \exp \left( -\frac{1-\beta}{(1-\alpha)\tau} t \right) \Big|_0^t = \\ &= (\beta) \left( -\exp \left( -\frac{\beta}{\alpha \tau} t \right) + \exp 0 \right) + \\ &+ (1-\beta) \left( -\exp \left( -\frac{1-\beta}{(1-\alpha)\tau} t \right) + \exp 0 \right) = \\ &= \beta \left( -\exp \left( -\frac{\beta}{\alpha \tau} t \right) + 1 \right) + \\ &+ (1-\beta) \left( -\exp \left( -\frac{1-\beta}{(1-\alpha)\tau} t \right) + 1 \right) \end{aligned}$$

Q2 d.

Sabendo que no reactor é introduzido um traçador, por degrau, com uma concentração à entrada do reactor  $C_0 = 0.1 \text{ M}$ , a um caudal volumétrico  $10 \text{ dm}^3/\text{min}$ , calcule o tempo ao fim do qual a concentração de traçador à saída é 95% da concentração à entrada.

- Volume do reactor:  $1 \text{ m}^3$ ;
- caudal de by-pass: 10% do caudal volumétrico à entrada;
- volume do by-pass: 20% do volume do reactor.

---

---

Resposta

$$t : C(t) = 0.95 C_0;$$

**Tracador em Degrau:**  $F(t) = \frac{C(t)}{C_0};$

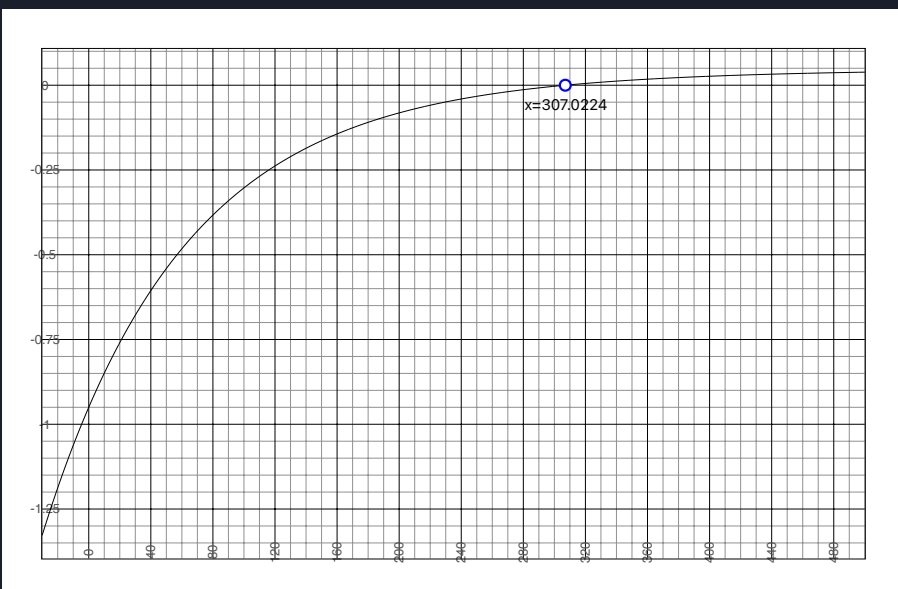
**Normalização da curva  $C$ :**

$$\begin{cases} \alpha = 20\% \\ \beta = 10\% \end{cases}$$

$$F(t) = \frac{C(t)}{C_0} = \frac{0.95 C_0}{C_0} = 0.95 =$$

$$\begin{aligned} &= \beta \left( -\exp \left( -\frac{\beta}{\alpha \tau} t \right) + 1 \right) + \\ &+ (1 - \beta) \left( -\exp \left( -\frac{1 - \beta}{(1 - \alpha)\tau} t \right) + 1 \right) \\ &= 0.1 \left( -\exp \left( -\frac{0.1}{0.2 \frac{1000}{10}} t \right) + 1 \right) + \\ &+ (1 - 0.1) \left( -\exp \left( -\frac{1 - 0.1}{(1 - 0.2) \frac{1000}{10}} t \right) + 1 \right) \cong \\ &\cong -\exp \left( -\frac{t}{200} \right) - \exp \left( -\frac{9t}{800} \right) + 1 \Rightarrow \end{aligned}$$

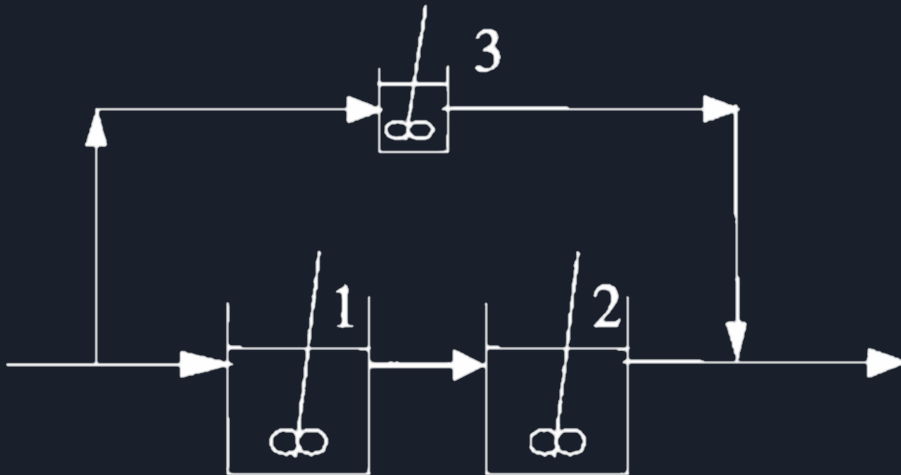
$$\Rightarrow f(t) = -\exp \left( -\frac{t}{200} \right) - \exp \left( -\frac{9t}{800} \right) + 0.05$$



$$t \cong 307.022 \text{ min}$$

## Questão 4

Considere um reator contínuo cujo comportamento não ideal pode ser modelado pela associação de reactores ideais esquematizada na figura.



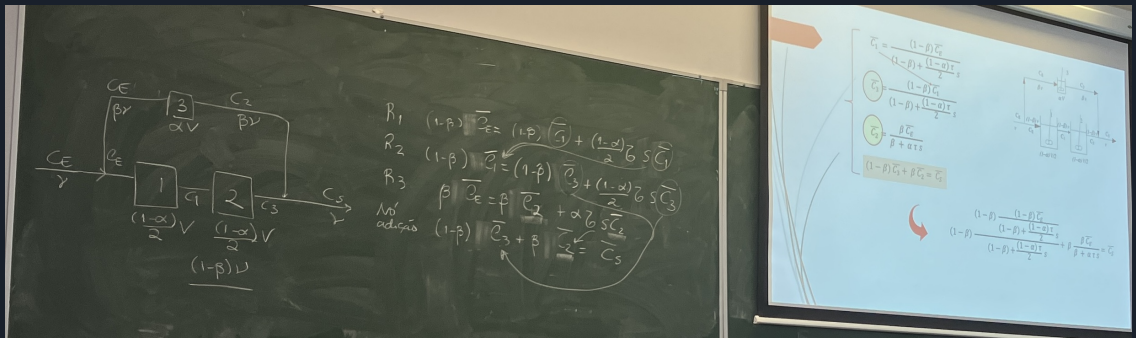
Transformadas de Laplace:

$f(s)$	$F(t)$
$\frac{1}{s-a}$	$e^{at}$
$\frac{1}{(s-a)^2}$	$t e^{at}$

Q4 a.

Escreva as equações do modelo que representa o escoamento no reactor, tendo em conta que os tanques 1 e 2 são iguais.

Resposta



Reator	Volume	Caldal In	Caldal Out
1	$\alpha V$	$\beta \nu$	$\beta \nu$
2	$(1 - \alpha) V / 2$	$(1 - \beta) \nu$	$(1 - \beta) \nu$
3	$(1 - \alpha) V / 2$	$(1 - \beta) \nu$	$(1 - \beta) \nu$

$R_1 :$

$$(1 - \beta) \nu C_{in,1} = (1 - \beta) \nu C_{in} =$$

$$= (1 - \beta) \nu C_{out,1} + (1 - \alpha) \frac{V}{2} \frac{dC_{out,1}}{dt};$$

$R_2 :$

$$(1 - \beta) \nu C_{in,2} = (1 - \beta) \nu C_{out,1} =$$

$$= (1 - \beta) \nu C_{out,2} + (1 - \alpha) \frac{V}{2} \frac{dC_{out,2}}{dt};$$

$R_3 :$

$$\beta \nu C_{in,3} = \beta \nu C_{in} = \beta \nu C_{out,3} + \alpha V \frac{dC_{out,3}}{dt};$$

$Nó :$

$$\nu C_{out} = (1 - \beta) \nu C_{out,2} + \beta \nu C_{out,3}$$



Deduz a expressão da distribuição de tempos de residência.

Resposta

$$E(t) = \mathcal{L} g(s);$$

$g(s)$  :

$$g(s) = \bar{C}_{out}/\bar{C}_{in} = \mathcal{L} C_{out}/\mathcal{L} C_{in};$$

$$\begin{aligned} \nu C_{out} &= (1 - \beta) \nu C_{out,2} + \beta \nu C_{out,3} \implies \\ &\implies C_{out} = (1 - \beta) C_{out,2} + \beta C_{out,3} \implies \\ &\implies \mathcal{L} C_{out} = \bar{C}_{out} = \\ &= \mathcal{L} ((1 - \beta) C_{out,2}) + \mathcal{L} (\beta C_{out,3}) = \\ &= (1 - \beta) \bar{C}_{out,2} + \beta \bar{C}_{out,3} \implies \\ &\implies g(s) = (1 - \beta) \frac{\bar{C}_{out,2}}{\bar{C}_{in}} + \beta \frac{\bar{C}_{out,3}}{\bar{C}_{in}}; \end{aligned}$$

$\bar{C}_{out,3}/\bar{C}_{in}$  :

$$\begin{aligned} \beta \nu C_{in} &= \beta \nu C_{out,3} + \alpha V \frac{dC_{out,3}}{dt} \implies \\ &\implies \beta C_{in} = \beta C_{out,3} + \alpha \tau \frac{dC_{out,3}}{dt} \implies \\ &\implies \mathcal{L} (\beta C_{in}) = \beta \bar{C}_{in} = \\ &= \mathcal{L} (\beta C_{out,3}) + \mathcal{L} \left( \alpha \tau \frac{dC_{out,3}}{dt} \right) = \beta \bar{C}_{out,3} + \alpha \tau s \bar{C}_{out,3} \implies \\ &\implies \frac{\bar{C}_{out,3}}{\bar{C}_{in}} = \frac{\beta}{\beta + \alpha \tau s}; \end{aligned}$$

$\bar{C}_{out,2}/\bar{C}_{in}$  :

$$\begin{aligned} (1 - \beta) \nu C_{out,1} &= (1 - \beta) \nu C_{out,2} + (1 - \alpha) \frac{V}{2} \frac{dC_{out,2}}{dt} \implies \\ &\implies (1 - \beta) C_{out,1} = (1 - \beta) C_{out,2} + \frac{1 - \alpha}{2} \tau \frac{dC_{out,2}}{dt} \implies \\ &\implies \mathcal{L} ((1 - \beta) C_{out,1}) = (1 - \beta) \bar{C}_{out,1} = \\ &= \mathcal{L} ((1 - \beta) C_{out,2}) + \mathcal{L} \left( \frac{1 - \alpha}{2} \tau \frac{dC_{out,2}}{dt} \right) = \\ &= (1 - \beta) \bar{C}_{out,2} + \frac{1 - \alpha}{2} \tau s \bar{C}_{out,2} \implies \\ &\implies \frac{\bar{C}_{out,2}}{\bar{C}_{in}} = \frac{(1 - \beta)}{(1 - \beta) + \frac{(1 - \alpha)\tau}{2} s} \frac{\bar{C}_{out,1}}{\bar{C}_{in}}; \end{aligned}$$

$\bar{C}_{out,1}/\bar{C}_{in}$  :

$$\begin{aligned} (1 - \beta) \nu C_{in} &= (1 - \beta) \nu C_{out,1} + (1 - \alpha) \frac{V}{2} \frac{dC_{out,1}}{dt} \implies \\ &\implies (1 - \beta) C_{in} = (1 - \beta) C_{out,1} + \frac{1 - \alpha}{2} \tau \frac{dC_{out,1}}{dt} \implies \\ &\implies \mathcal{L} ((1 - \beta) C_{in}) = (1 - \beta) \bar{C}_{in} = \\ &= \mathcal{L} (1 - \beta) C_{out,1} + \mathcal{L} \left( \frac{1 - \alpha}{2} \tau \frac{dC_{out,1}}{dt} \right) = \\ &= (1 - \beta) \bar{C}_{out,1} + \frac{1 - \alpha}{2} \tau s \bar{C}_{out,1} \implies \\ &\implies \frac{\bar{C}_{out,1}}{\bar{C}_{in}} = \frac{(1 - \beta)}{(1 - \beta) + \frac{(1 - \alpha)\tau}{2} s} \implies \\ &\implies \frac{\bar{C}_{out,2}}{\bar{C}_{in}} = \frac{(1 - \beta)}{(1 - \beta) + \frac{(1 - \alpha)\tau}{2} s} \frac{\bar{C}_{out,1}}{\bar{C}_{in}} = \\ &= \left( \frac{(1 - \beta)}{(1 - \beta) + \frac{(1 - \alpha)\tau}{2} s} \right)^2; \\ &\implies g(s) = \\ &= (1 - \beta) \left( \frac{(1 - \beta)}{(1 - \beta) + \frac{(1 - \alpha)\tau}{2} s} \right)^2 + \beta \left( \frac{\beta}{\beta + \alpha \tau s} \right) = \\ &= \frac{(1 - \beta)^3}{\left( \frac{(1 - \alpha)\tau}{2} \right)^2} \frac{1}{\left( \frac{(1 - \beta)^2}{(1 - \alpha)\tau} + s \right)^2} + \frac{\beta^2}{\alpha \tau} \frac{1}{\frac{\beta}{\alpha \tau} + s} \implies \\ &\implies E(t) = \mathcal{L} g(s) = \\ &= \frac{(1 - \beta)^3 4}{(1 - \alpha)^2 \tau^2} t \exp \left( -\frac{(1 - \beta)^2}{(1 - \alpha)\tau} t \right) + \frac{\beta^2}{\alpha \tau} \exp \left( -\frac{\beta}{\alpha \tau} t \right) \end{aligned}$$

Deduza e expressão da função cumulativa.

Resposta

$$\begin{aligned}
 F(t) &= \int_0^t E(t) \, dt = \\
 &= \int_0^t \frac{(1-\beta)^3 4}{(1-\alpha)^2 \tau^2} t \exp\left(-\frac{(1-\beta) 2}{(1-\alpha) \tau} t\right) dt + \\
 &+ \int_0^t \frac{\beta^2}{\alpha \tau} \exp\left(-\frac{\beta}{\alpha \tau} t\right) dt = \\
 &= \frac{(1-\beta)^3 4}{(1-\alpha)^2 \tau^2} \int_0^t t \exp\left(-\frac{(1-\beta) 2}{(1-\alpha) \tau} t\right) dt + \\
 &+ \frac{\beta^2}{\alpha \tau} \frac{\alpha \tau}{\beta} \Delta\left(-\exp\left(-\frac{\beta}{\alpha \tau} t\right)\right) \Big|_0^t = \\
 &= \frac{(1-\beta)^3 4}{(1-\alpha)^2 \tau^2} \int_0^t t \exp\left(-\frac{(1-\beta) 2}{(1-\alpha) \tau} t\right) dt + \\
 &+ \beta \left(-\exp\left(-\frac{\beta}{\alpha \tau} t\right) + \exp 0\right);
 \end{aligned}$$

Primitiva:

$$\begin{aligned}
 d\left(t \exp\left(-\frac{(1-\beta) 2}{(1-\alpha) \tau} t\right)\right) &= \\
 &= \exp\left(-\frac{(1-\beta) 2}{(1-\alpha) \tau} t\right) + \\
 &+ t \left(-\frac{(1-\beta) 2}{(1-\alpha) \tau}\right) \exp\left(-\frac{(1-\beta) 2}{(1-\alpha) \tau} t\right) \implies \\
 \implies \mathcal{P}\left(d\left(t \exp\left(-\frac{(1-\beta) 2}{(1-\alpha) \tau} t\right)\right)\right) &= t \exp\left(-\frac{(1-\beta) 2}{(1-\alpha) \tau} t\right) = \\
 &= \mathcal{P}\left(\exp\left(-\frac{(1-\beta) 2}{(1-\alpha) \tau} t\right)\right) + \\
 &+ \mathcal{P}\left(t \left(-\frac{(1-\beta) 2}{(1-\alpha) \tau}\right) \exp\left(-\frac{(1-\beta) 2}{(1-\alpha) \tau} t\right)\right) = \\
 &= -\frac{(1-\alpha) \tau}{(1-\beta) 2} \exp\left(-\frac{(1-\beta) 2}{(1-\alpha) \tau} t\right) + \\
 &- \frac{(1-\beta) 2}{(1-\alpha) \tau} \mathcal{P}\left(t \exp\left(-\frac{(1-\beta) 2}{(1-\alpha) \tau} t\right)\right) \implies \\
 \implies \mathcal{P}\left(t \exp\left(-\frac{(1-\beta) 2}{(1-\alpha) \tau} t\right)\right) &= \\
 &= -\frac{(1-\alpha) \tau}{(1-\beta) 2} \left(t + \frac{(1-\alpha) \tau}{(1-\beta) 2}\right) \exp\left(-\frac{(1-\beta) 2}{(1-\alpha) \tau} t\right) \implies \\
 \implies F(t) &= \frac{(1-\beta)^3 4}{(1-\alpha)^2 \tau^2} * \\
 * \Delta\left(-\frac{(1-\alpha) \tau}{(1-\beta) 2} \left(t + \frac{(1-\alpha) \tau}{(1-\beta) 2}\right) \exp\left(-\frac{(1-\beta) 2}{(1-\alpha) \tau} t\right)\right) \Big|_0^t &+ \\
 &+ \beta \left(-\exp\left(-\frac{\beta}{\alpha \tau} t\right) + 1\right) = \\
 &= \frac{(1-\beta)^3 4}{(1-\alpha)^2 \tau^2} * \\
 * \left(-\frac{(1-\alpha) \tau}{(1-\beta) 2} \left(t + \frac{(1-\alpha) \tau}{(1-\beta) 2}\right) \exp\left(-\frac{(1-\beta) 2}{(1-\alpha) \tau} t\right) + \right. & \\
 \left. + \left(\frac{(1-\alpha) \tau}{(1-\beta) 2}\right)^2 \exp 0\right) + & \\
 &+ \beta \left(-\exp\left(-\frac{\beta}{\alpha \tau} t\right) + 1\right) = \\
 &= (1-\beta) \left(-\left(t \frac{(1-\beta) 2}{(1-\alpha) \tau} + 1\right) \exp\left(-\frac{(1-\beta) 2}{(1-\alpha) \tau} t\right) + 1\right) + \\
 &+ \beta \left(-\exp\left(-\frac{\beta}{\alpha \tau} t\right) + 1\right)
 \end{aligned}$$

Q4 d.

Sabendo que o reactor real tem um volume de  $1 \text{ m}^3$  e que são introduzidos, por impulso,  $6 \text{ mol}$  de um tracador, determine o valor da concentração máxima de tracador. à saída do reactor.

- Caudal volumétrico da alimentação:  $20 \text{ dm}^3/\text{min}$ ;
- caudal de by-pass: 5% do caudal volumétrico à entrada;
- volume do reciclo: 8% do volume activo;
- volumes mortos: 12% do volume do reactor.

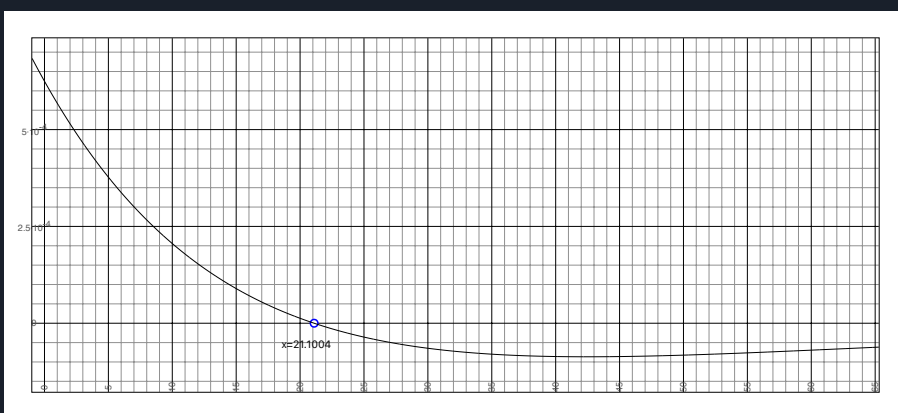
Resposta

Traçador por impulso:

$$\frac{dC}{dt} = \frac{N}{\nu} \frac{dE(t)}{dt};$$

$$\begin{cases} \beta = 0.05; & (1 - \beta) = 0.95 \\ \alpha = 0.08; & (1 - \alpha) = 0.92 \\ V_m = 0.12 * 1000 \text{ dm}^3 = 120 \text{ dm}^3 \\ V = (1000 - 120) \text{ dm}^3 = 880 \text{ dm}^3 \\ \nu = 20 \text{ dm}^3/\text{min} \\ \tau = \frac{880}{20} \text{ min} = 44 \text{ min} \\ N = 6 \text{ mol} \\ t = 21 \text{ min} \end{cases}$$

$$\begin{aligned} \Rightarrow \frac{dC}{dt} &= 0 = \\ &= \frac{N}{\nu} \left( \frac{(1 - \beta)^3 4}{(1 - \alpha)^2 \tau^2} \left( 1 - \frac{(1 - \beta) 2}{(1 - \alpha) \tau} t \right) \exp \left( -\frac{(1 - \beta) 2}{(1 - \alpha) \tau} t \right) \right. \\ &\quad \left. - \frac{\beta^3}{\alpha^2 \tau^2} \exp \left( -\frac{\beta}{\alpha \tau} t \right) \right) = \\ &= \frac{6}{20} \left( \frac{0.95^3 * 4}{0.92^2 * 44^2} \left( 1 - \frac{0.95 * 2}{0.92 * 44} t \right) \exp \left( -\frac{0.95 * 2}{0.92 * 44} t \right) \right. \\ &\quad \left. - \frac{0.05^3}{0.08^2 * 44^2} \exp \left( -\frac{0.05}{0.08 * 44} t \right) \right) = \\ &= (6.279 \text{ E}^{-4} - 2.947 \text{ E}^{-5} t) \exp (-4.694 \text{ E}^{-2} t) \\ &\quad - 3.027 \text{ E}^{-6} \exp (-1.420 \text{ E}^{-2} t) \end{aligned}$$



$$t = 21.100 \text{ min};$$

$$\begin{aligned} C &\cong \frac{N}{\nu} E(21.100) \cong \\ &\cong \frac{6}{20} \left( \frac{0.95^3 * 4}{0.92^2 * 44^2} 21.100 \exp \left( -\frac{0.95 * 2}{0.92 * 44} 21.100 \right) + \right. \\ &\quad \left. + \frac{0.05^2}{0.08 * 44} \exp \left( -\frac{0.05}{0.08 * 44} 21.100 \right) \right) \cong \\ &\cong 8.435 \text{ E}^{-3} \text{ M} \end{aligned}$$

## Questão 13

A reacção elementar  $A \longrightarrow B$  é conduzida, na fase gasosa, num reactor multitubular de leito fixo, consistindo em 100 tubos de 2 m de comprimento e 2 cm de diâmetro da secção recta, cheios com um catalisador sólido, poroso, na forma de pellets esféricas de 5 mm de diâmetro. O reagente A é alimentado puro a um caudal de 100 dm<sup>3</sup>/min, à temperatura de 373 K e à pressão de 6 atm

Dados:

- $\rho_P = 1.3 \text{ g/cm}^3$
- Coeficiente de Difusão externo:  $D_A = 2.7 \text{ E}^{-7} \text{ m}^2/\text{s}$
- Viscosidade Cinemática:  $\nu = 4 \text{ E}^{-6} \text{ m}^2/\text{s}$
- $\varepsilon_B = 0.45$
- Difusidade efetiva intraparticular:  $D_e = 1.3 \text{ E}^{-8} \text{ m}^2/\text{s}$
- Constante cinética:  $k' = 0.023 \text{ dm}^3 \text{ g}^{-1} (\text{cat}) \text{ min}^{-1}$
- $R \cong 8.206 \text{ E}^{-2} \text{ dm}^3 \text{ atm mol}^{-1} \text{ K}^{-1}$

Formulas:

$$Sh = 1.0 Re^{1/2} Sc^{1/3} = \frac{k_c d_P}{D_A} \frac{1}{(1/\varepsilon_b) - 1};$$

$$Re = \frac{u d_P}{\nu (1 - \varepsilon_b)}; Sc = \frac{\nu}{D_A};$$

$$\phi = R \sqrt{\frac{k' \rho_P}{D_e}}; \eta = \frac{3}{\phi^2} (\phi \coth \phi - 1)$$

Perfil de concentração de pellet:  $\rho = \frac{\sinh(\phi \lambda)}{\lambda \cosh \phi}$

### Q13 a.

Calcule o valor da constante cinética aparente, que observaria no caso da ausência de limitações difusionais externas.

---

---

Resposta

$$k'_{ap} = \eta k' = \left( \frac{3}{\phi^2} (\phi \coth \phi - 1) \right) k';$$

$$\phi = R \sqrt{\frac{k' \rho_P}{D_e}} \cong$$

$$\cong 8.206 \text{ E}^{-2} \text{ dm}^3 \text{ atm mol}^{-1} \text{ K}^{-1} \sqrt{\frac{0.023 \text{ E}^{-3} \frac{\text{m}^3}{\text{min}} \frac{\text{min}}{60 \text{ s}} * 1.300 \text{ E}^3 \text{ m}^2/\text{s}}{1.300 \text{ E}^{-8} \text{ m}^2/\text{s}}} \cong$$

$$\cong 16.066 \implies$$

$$\implies k'_{ap} = \frac{3}{\phi^2} (\phi \coth \phi - 1) k' \cong$$

$$\cong \frac{3}{(16.066)^2} (16.066 \coth 16.066 - 1) \frac{0.023}{60} \cong 6.712 \text{ E}^{-5} \text{ L/sec g}$$

Q13 b.

Calcule o valor do coeficiente de transferência de massa.

---

Resposta

$$Sh = Re^{1/2} Sc^{1/3} = \left( \frac{u d_P}{\nu (1 - \varepsilon_b)} \right)^{1/2} \left( \frac{\nu}{D_a} \right)^{1/3} ;$$

$$u = \frac{\nu_{tubos}}{A_c} = \frac{(\nu / N_{tubos})}{(\varepsilon_b \pi D^2 / 4)} = \frac{(\nu / 60 * 100)}{(0.45 \pi 0.02^2 / 4)} \cong \\ \cong \nu 1.179 \implies$$

$$\implies Sh = \left( \frac{u d_P}{\nu (1 - \varepsilon_b)} \right)^{1/2} \left( \frac{\nu}{D_a} \right)^{1/3}$$

Q13 c.

Calcule o valor da constante cinética realmente observada.

Q13 d.

Diga, justificando a sua resposta, se o reactor se encontra em regime cinético, difusional interno, difusional externo ou misto.



Q13 e.

Calcule a conversão à saída do reactor.

Q13 f.

Determine o valor da concentração de A no centro das pellets, à saída do reactor.