

FT I – Exercícios

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Conteúdo

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Questão 7 – 3

Um permutador de calor de envólucro e tubos (com 10 tubos que realizam 8 passagens pelo envólucro) está dimensionado para aquecer 2.5 kg s^{-1} de água de 15°C a 85°C . O aquecimento é conseguido graças à passagem de um óleo de processo, que se encontra disponível a 160°C . O coeficiente de filme do lado do óleo assume o valor de $400 \text{ W m}^{-2} \text{ K}^{-1}$. A água circula pelo interior dos tubos. Os tubos possuem um diâmetro externo de 25 mm e um diâmetro interno de 23 mm. Sabendo que o óleo sai do permutador de calor a 100°C , calcule:

- Fator de Correlação de θ_m : $y = 0.87$
- Condutividade da parede do tubo: $k_W = 45 \text{ W m}^{-1} \text{ K}^{-1}$
- $C_{p,oleo} = 2350 \text{ J kg}^{-1} \text{ K}^{-1}$
- $C_{p,agua} = 4181 \text{ J kg}^{-1} \text{ K}^{-1}$
- $k_{agua} = 0.643 \text{ W m}^{-1} \text{ K}^{-1}$
- $\mu_{agua} = 548 * 10^{-6} \text{ kg m}^{-1} \text{ s}^{-1}$
- $\rho_{agua} = 1000 \text{ kg m}^{-3}$

Q7 – 3 a)

O caudal mássico de óleo necessário para realizar a operação desejada.

$$\begin{aligned}
 G_{m,oleo,1} &= \frac{Q_{oleo}}{C_{m,p,oleo} \Delta T_{oleo}} = \frac{-Q_{agua}}{C_{m,p,oleo} \Delta T_{oleo}} = \\
 &= -\frac{G_{m,agua} C_{p,agua} \Delta T_{agua}}{C_{m,p,oleo} \Delta T_{oleo}} = -\frac{2.5 * 4181 * (85 - 15)}{2350 * (100 - 160)} \cong 5.19
 \end{aligned}$$

Q7 – 3 b)

O comprimento que deverá ter cada tubo do permutador.

$$\begin{aligned}
 L &= \frac{A_e}{2 \pi r_e} = \frac{A_i}{2 \pi r_i}; \quad (\bar{h}_i A_i)^{-1} = \\
 &= \frac{y \Delta(\Delta T)_{\ln}}{Q_{agua}} = \frac{y \left(\frac{\Delta T_1 - \Delta T_0}{\ln(\Delta T_1 / \Delta T_0)} \right)}{(G_{m,agua} C_{p,agua} \Delta T_{agua})} = \\
 &= \frac{y(\Delta T_1 - \Delta T_0)}{(G_{m,agua} C_{p,agua} \Delta T_{agua}) \ln(\Delta T_1 / \Delta T_0)} = \\
 &= (h_i A_i)^{-1} + (h_e A_e)^{-1} + \frac{x_w}{k_w A_w} = \\
 &= \left(\left(\left(\frac{k_{agua} 0.023}{D_i} \left(\frac{\rho D_i u}{\mu_{agua}} \right)^{0.8} \left(\frac{C_{p,agua} \mu_{agua}}{k} \right)^{0.4} \right) (2 \pi (D_i/2) L) \right)^{-1} + \right. \\
 &\quad \left. + (h_e 2 \pi (D_e/2) L)^{-1} \right. \\
 &\quad \left. + \frac{(D_e - D_i)/2}{k_w} \left(\frac{A_e - A_i}{\ln(A_e/A_i)} \right)^{-1} \right. \\
 &= \left(\frac{\mu_{agua}^{0.4}}{k_{agua}^{0.6} 0.023 \rho_{agua}^{0.8} u^{0.8} C_{p,agua}^{0.4} D_i^{0.8}} (\pi L)^{-1} + \right. \\
 &\quad \left. + (h_e D_e)^{-1} (\pi L)^{-1} \right. \\
 &\quad \left. + \frac{(D_e - D_i)/2}{k_w} \left(\frac{\ln(D_e/D_i)}{D_e - D_i} \right) (\pi L)^{-1} \right. \\
 &= \left(\frac{\mu_{agua}^{0.4}}{k_{agua}^{0.6} 0.023 \rho_{agua}^{0.8} C_{p,agua}^{0.4} D_i^{0.8}} \left(\frac{G_{m,agua}}{n_{tubos} \rho_{agua} (\pi (D_i/2)^2)} \right)^{-0.8} + \right. \\
 &\quad \left. + (h_e D_e)^{-1} \right. \\
 &\quad \left. + \frac{\ln(D_e/D_i)}{(2 k_w)} \right) (\pi L)^{-1} = \\
 &= \left(\frac{\mu_{agua}^{0.4} n_{tubos}^{0.8} \pi^{0.8} D_i^{0.8}}{k_{agua}^{0.6} 0.023 C_{p,agua}^{0.4} G_{m,agua}^{0.8} 2^{1.6}} + \right. \\
 &\quad \left. + (h_e D_e)^{-1} \right. \\
 &\quad \left. + \frac{\ln(D_e/D_i)}{(2 k_w)} \right) (\pi L)^{-1} \Rightarrow
 \end{aligned}$$

$$\begin{aligned}
\Rightarrow L &= \left(\frac{\mu_{agua}^{0.4} n_{tubos}^{0.8} \pi^{0.8} D_i^{0.8}}{k_{agua}^{0.6} 0.023 C_{p,agua}^{0.4} G_{m,agua}^{0.8} 2^{1.6}} + \right. \\
&\quad \left. + (h_e D_e)^{-1} \right. \\
&\quad \left. + \frac{\ln(D_e/D_i)}{(2 k_w)} \right) * \\
&\quad * \frac{(G_{m,agua} C_{p,agua} \Delta T_{agua}) \ln(\Delta T_1 / \Delta T_0)}{\pi y(\Delta T_1 - \Delta T_0)} = \\
&= \left(\frac{(548 * 10^{-6})^{0.4} * 10^{0.8} * \pi^{0.8} * (23 * 10^{-3})^{0.8}}{(0.643)^{0.6} * 0.023 * 4181^{0.4} * (2.5)^{0.8} * 2^{1.6}} + \right. \\
&\quad \left. + (400 * 25 * 10^{-3})^{-1} \right. \\
&\quad \left. + \frac{\ln(25/23)}{(2 * 45)} \right) * \\
&\quad * \frac{2.5 * 4181 * (85 - 15) * \ln\left(\frac{100-15}{160-85}\right)}{\pi * 0.87 * ((100 - 15) - (160 - 85))} \cong 379.15
\end{aligned}$$

Q7 – 3 c)

A área total necessária.

$$A_w = \frac{A_e - A_i}{\ln(A_e/A_i)} = \pi L \frac{D_e - D_i}{\ln(D_e/D_i)} \cong \pi 379.15 \frac{(25 - 23) * 10^{-3}}{\ln(25/23)} \cong 28.57$$

Questão 7 – 4

Condensa-se benzeno à temperatura de 353 K no exterior dos tubos dum permutador de calor do tipo caixa/tubos, com tubos verticais de diâmetros interior 22 mm e exterior 25 mm, fazendo passar água pelo interior dos tubos a um caudal de $0.03 \text{ m}^3/\text{s}$. Qual será o comprimento total de tubo necessário, sabendo que a água entra a 290 K e sai a 300 K, e que o coeficiente de transferência de calor do lado da água é $850 \text{ W m}^{-2} \text{ K}^{-1}$?

- Condutividade térmica do material da parede do tubo:

$$k_w = 45 \text{ W m}^{-1} \text{ K}^{-1}$$

- $C_{p,agua} = 4181 \text{ J kg}^{-1} \text{ K}^{-1}$

$$\rho_{agua} = 1000 \text{ kg m}^{-3}$$

- $\mu_{ben} = 0.35 * 10^{-3} \text{ kg m}^{-1} \text{ s}^{-1}$

$$\rho_{ben} = 880 \text{ kg m}^{-3}$$

- $k_{ben} = 0.15 \text{ W m}^{-1} \text{ K}^{-1}$

$$\lambda_{ben} = 394 \text{ kJ kg}^{-1}$$

$$\begin{aligned} L &= \frac{A_e}{\pi D_e} = \frac{A_i}{\pi D_i}; \quad (\bar{h} A)^{-1} = \frac{\Delta(\Delta T)_{\ln}}{Q_{agua}} = \frac{\left(\frac{\Delta T_1 - \Delta T_0}{\ln(\Delta T_1 / \Delta T_0)} \right)}{(G_{m,agua} C_{p,agua} \Delta T_{agua})} = \\ &= (h_i A_i)^{-1} + (h_{ben} A_e)^{-1} + \frac{x_w}{k_w A_w} = \\ &= \left(\begin{aligned} &(h_i (\pi D_i L))^{-1} \\ &+ \left(\left(1.47 \left(\frac{k_{ben}^3 \rho_{ben}^2 g}{4 M_{ben} \mu_{ben}} \right)^{1/3} \right) (\pi D_e L) \right)^{-1} \\ &+ \frac{(D_e - D_i)/2}{k_w} \left(\frac{\ln(A_e/A_i)}{A_e - A_i} \right) \end{aligned} \right)^{-1} = \\ &= \left(\begin{aligned} &(h_i D_i)^{-1} (\pi L)^{-1} \\ &+ \frac{4^{1/3} \mu_{ben}^{1/3}}{1.47 k_{ben}^{3*1/3} \rho_{ben}^{2*1/3} g^{1/3} D_e} \left(\frac{G_{ben}}{A_e/L} \right)^{1/3} (\pi L)^{-1} \\ &+ \frac{(D_e - D_i)/2}{k_w} \left(\frac{\ln(A_e/A_i)}{A_e - A_i} \right) \end{aligned} \right)^{-1} = \end{aligned}$$

$$\begin{aligned}
&= \left(\begin{array}{c} (h_i D_i)^{-1} \\ + \frac{4^{1/3} \mu_{ben}^{1/3}}{1.47 k_{ben} \rho_{ben}^{2/3} g^{1/3} D_e} \left(\frac{(Q_{ben} C_{p,ben}^{-1} \rho_{ben}^{-1}) L}{(\pi D_e L)} \right)^{1/3} \\ + \frac{\ln(D_e/D_i)}{2 k_w} \end{array} \right)^+ (\pi L)^{-1} = \\
&= \left(\begin{array}{c} (h_i D_i)^{-1} \\ + \frac{4^{1/3} \mu_{ben}^{1/3}}{1.47 k_{ben} \rho_{ben} g^{1/3} D_e^{4/3} \pi^{1/3} C_{p,ben}^{1/3}} (-Q_{agua})^{1/3} \\ + \frac{\ln(D_e/D_i)}{2 k_w} \end{array} \right)^+ (\pi L)^{-1} = \\
&= \left(\begin{array}{c} (h_i D_i)^{-1} \\ + \frac{4^{1/3} \mu_{ben}^{1/3} (-G_{m,agua} \rho_{agua} \Delta T_{agua})^{1/3}}{1.47 k_{ben} \rho_{ben} g^{1/3} D_e^{4/3} \pi^{1/3} C_{p,ben}^{1/3}} \\ + \frac{\ln(D_e/D_i)}{2 k_w} \end{array} \right)^+ (\pi L)^{-1} \Rightarrow \\
&\Rightarrow L = \\
&= \left(\begin{array}{c} (h_i D_i)^{-1} \\ + \frac{4^{1/3} \mu_{ben}^{1/3} (-G_{m,agua} \rho_{agua} \Delta T_{agua})^{1/3}}{1.47 k_{ben} \rho_{ben} g^{1/3} D_e^{4/3} \pi^{1/3} C_{p,ben}^{1/3}} \\ + \frac{\ln(D_e/D_i)}{2 k_w} \end{array} \right)^+ * \\
&* \left(\frac{G_{m,agua} C_{p,agua} \Delta T_{agua}}{\pi(\Delta T_1 - \Delta T_0)} \ln \frac{\Delta T_1}{\Delta T_0} \right) = \\
&= \left(\begin{array}{c} (850 * 22 * 10^{-3})^{-1} \\ + \frac{4^{1/3} * (0.35 * 10^{-3})^{1/3} * (-0.03 * 880 * (300 - 290))^{1/3}}{1.47 * 0.15 * 880 * g^{1/3} * D_e^{4/3} * \pi^{1/3} * C_{p,ben}^{1/3}} \\ + \frac{\ln(D_e/D_i)}{2 k_w} \end{array} \right)^+ * \\
&* \left(\frac{G_{m,agua} C_{p,agua} \Delta T_{agua}}{\pi(\Delta T_1 - \Delta T_0)} \ln \frac{\Delta T_1}{\Delta T_0} \right)
\end{aligned}$$