

Consider the D/A Converter:

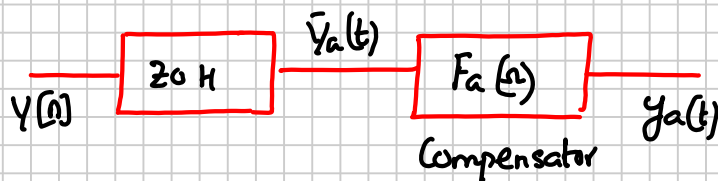


① Ideal D/A Converter:

$$y_a(t) = \sum_{n=-\infty}^{\infty} y[n] g_a(t - nT)$$

$$g_a(t) = \text{Sinc} \frac{\pi t}{T} \rightarrow \text{Pulse in frequency domain}$$

② Zero-order Hold (ZOH):

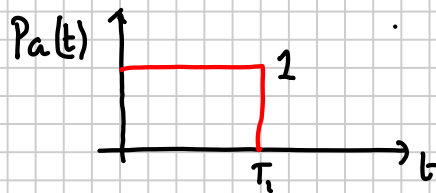


$\bar{y}_a(t)$  = Step approximation for  $y_a(t)$

Compensator  $F_a(z)$  takes  $\bar{y}_a(t)$  and gives  $y_a(t)$

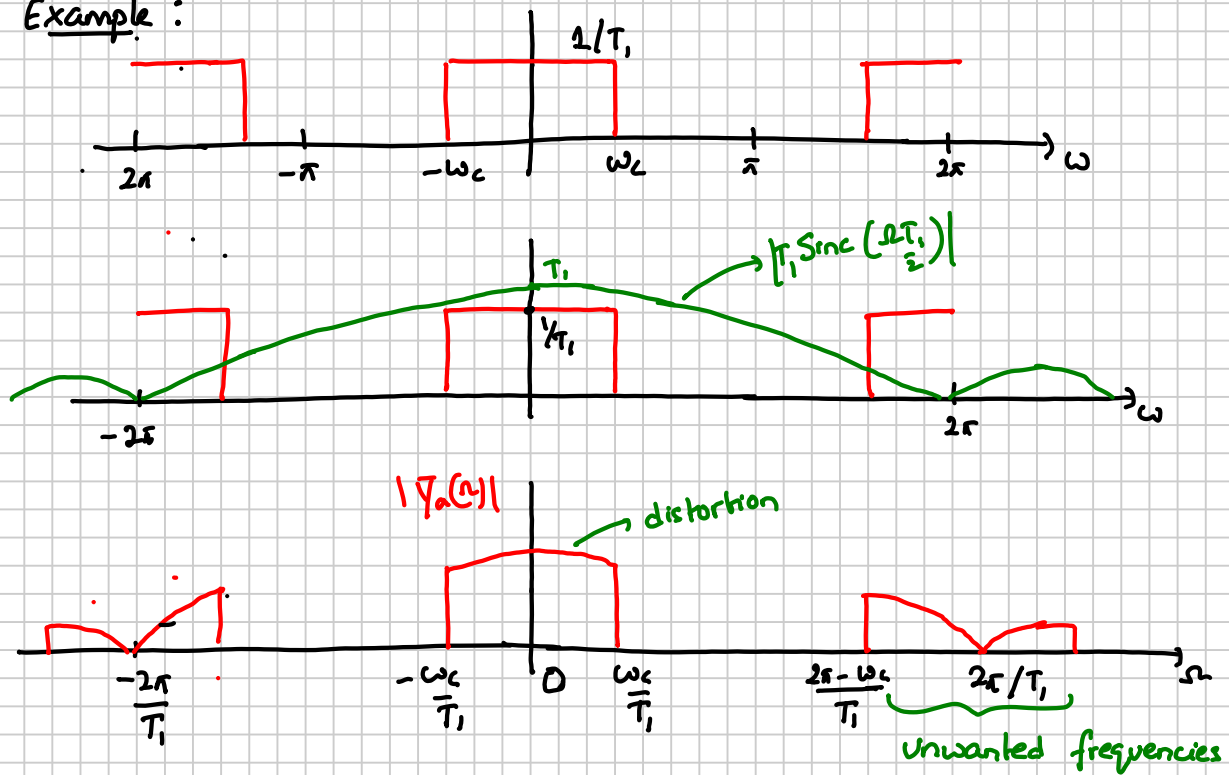
ZOH: D/A converter using rectangular pulses

$$\Rightarrow \bar{y}_a(t) = \sum_{n=-\infty}^{\infty} y[n] p_a(t - nT)$$

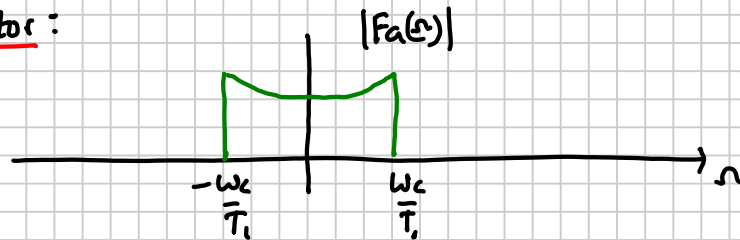


$$\bar{y}_a(z) = T_1 e^{-j\omega T_1/2} \text{Sinc} \left( \frac{\omega T_1}{2} \right) Y_d(\omega T)$$

Example :

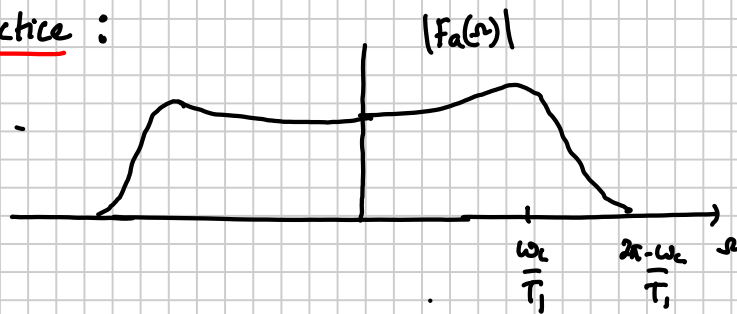


Compensator :



Ideal  $|F_a(\omega)|$  : LPF with  $\frac{1}{\text{Sinc}(\frac{\omega T_1}{2})}$  shape.

In practice :

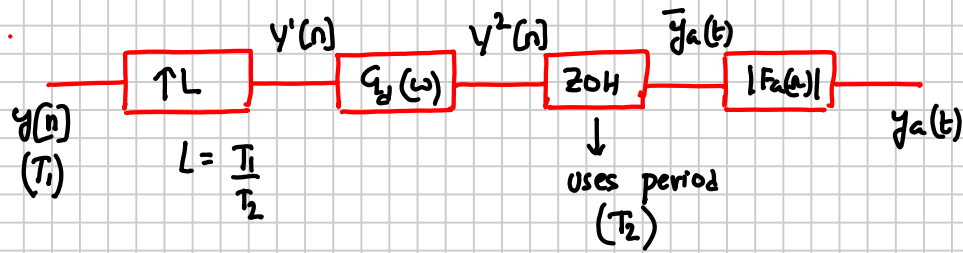


Permitted Transition bandwidth

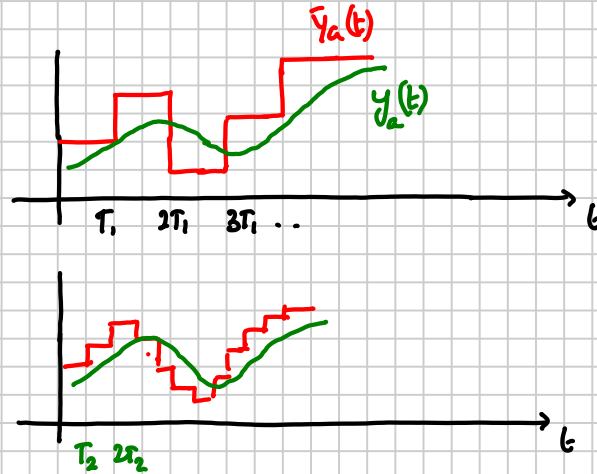
$$B = \frac{2\pi - \omega_c}{T_1} - \frac{\omega_c}{T_1}$$

$$\Rightarrow B = \frac{2(\pi - \omega_c)}{T_1}$$

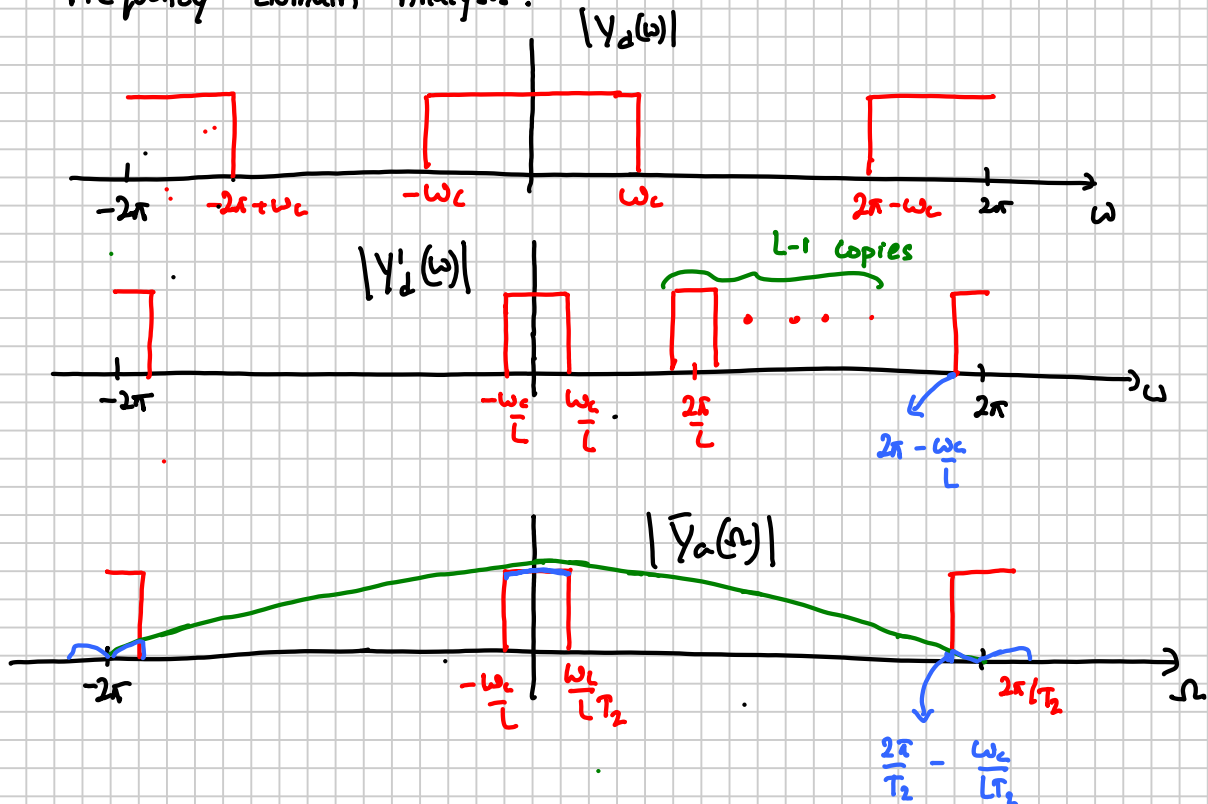
Oversampled D/A:



Due to interpolation, the above 20H puts out finer staircase approximation.



Frequency domain Analysis:



Transition bandwidth of the compensation filter,

$$B = \frac{2\pi}{T_2} - \frac{\omega_c}{LT_2} - \frac{\omega_c}{LT_2}$$

$$\Rightarrow B = \frac{2\pi L}{T_1} - \frac{\omega_c}{T_1} - \frac{\omega_c}{T_1}$$

$$\Rightarrow B = \frac{2(\pi L - \omega_c)}{T_1}$$

Note:  $\frac{2(\pi L - \omega_c)}{T_1} \gg \frac{2\pi(\omega - \omega_c)}{T_1}$

Also Note: ① Center pulse being smaller is almost flat.

② Artifact centered at  $\frac{2\pi}{T_2}$  is nearly zero, so even a fairly crude  $F_a(x)$  will work