Infinite impulse response filters Leakey Integrator filter

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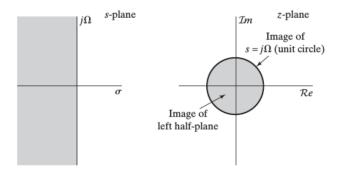
Classification of discrete filters

Table: Classification of discrete filters

	Finite impulse response (FIR)	Infinite impulse response (IIR)
Filtering in time domain	Moving average	Leaky Integrator
Filtering in frequency domain	Windowed Filters Equiripple Minimax	Bilinear z-transform ZOH method

IIR filtering in frequency domain

- The main idea is to transform an analog filter to the discrete domain.
- From s domain to z domain.
- This way, all the theory behind analog filter can be reused to implement a filter in a computer.



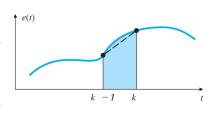
Bilinear transform (Tustin's Method)

Suppose the following integrator,

$$\frac{U(s)}{E(s)} = D_c(s) = \frac{1}{s}. \tag{1}$$

The area under e(t) over $k \times T$ periods is,

$$u(k) = \int_0^{k-1} e(t)dt + \int_{k-1}^k e(t)dt.$$
 (2)



Tustin's method uses the trapezoidal integration, to approximate e(t) by a straight line between two samples. The technique is an algebraic transformation between variables s and z.

$$u(k) = u(k-1) + \frac{T}{2} \left[e(k-1) + e(k) \right], \quad (3)$$

$$U(z) = z^{-1}U(z) + \frac{T}{2}\left[z^{-1}E(z) + E(z)\right], \quad (4)$$

$$U(z)(1-z^{-1}) = \frac{T}{2} \left[E(z)(1+z^{-1}) \right], \quad (5)$$

$$\implies \frac{U(z)}{E(z)} = \frac{T}{2} \left(\frac{1 + z^{-1}}{1 - z^{-1}} \right) = \frac{1}{\frac{2}{T} \frac{1 - z^{-1}}{1 + z^{-1}}}.$$
(6)

Comparing Eq. 1 and 6,

$$s \approx \frac{2}{T} \left(\frac{1 - z^{-1}}{1 + z^{-1}} \right)$$
 (7)

Relationship between analog and digital frequencies

- Ω is the analog frequency, $-\infty, <\Omega<\infty.$
- ω , the "digital" frequency, $-\pi$, $<\omega<\pi$, i.e., $-2\pi f_s/2$, $<\omega<2\pi f_s/2$.
- What is the relationship between Ω and ω .

Doing $s=j\Omega$, z should be evaluated in the unity circle, so, $z=r\cdot e^{j\omega}=\cdot e^{j\omega}$, with r=1.

$$s = \frac{2}{T} \left(\frac{1 - e^{-j\omega}}{1 + e^{-j\omega}} \right) = \frac{2}{T} \left[\frac{2e^{-j\omega/2}(j\sin\omega/2)}{2e^{-j\omega/2}(\cos\omega/2)} \right] = j\frac{2}{T} \tan(\omega/2).$$
 (8)

Real and imaginary parts on both sides of Eq. 8 are,

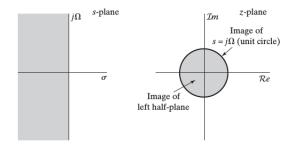
Since $s = \sigma + j\Omega$,

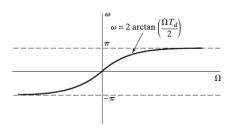
$$\sigma = 0, (9)$$

$$\Omega = \frac{2}{T} \tan(\omega/2) \,, \tag{10}$$

$$\implies \omega = \arctan(\Omega T/2)$$
. (11)

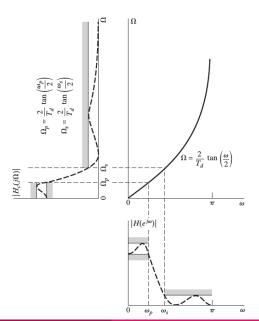
Map from s to z





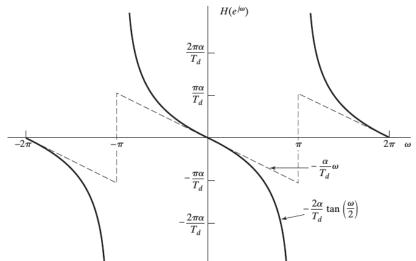
Bilinear transform, Frequency Warping

- Non-linear compression of the frequency axis.
- The design of discrete-time filters using the bilinear transformation is useful only when this compression can be tolerated or compensated for.



Bilinear transform, Phase response

Suppose a continuous-time filter with linear phase response. The nonlinear warping of the frequency axis introduced by the bilinear transformation will not preserve linearity in phase response.



Example of IIR design using bilinear transform

1 Choose the analog filter that complains with the desired performance.

For example, second-order Butterworth low-pass filter.

$$G(s) = rac{\Omega_c^2}{s^2 + s\sqrt{2}\Omega_c + \Omega_c^2}$$

2 Cut-off digital frequency is normalized.

$$f_{dc} = 100 \; \mathrm{Hz}, \, f_s = 1000 \; \mathrm{Hz}, \, T = 0.001 \; \mathrm{s}.$$

$$\omega_c = 2 \pi \, 100/1000 = 0.628 \, \text{rad/s}.$$

3 Pre-warp the analog frequencies.

$$\Omega_c = \frac{2}{T} \tan(\omega_c/2) = \frac{2}{0.001} \tan\left(\frac{0.628}{2}\right) = 649.839 \text{ rad/s}.$$
 $f_{ac} = 103.42 \text{ Hz}.$

Example of IIR design using bilinear transform

4 Replace *s* by the bilinear transform, $s \approx \frac{2}{T} \left(\frac{1-z^{-1}}{1+z^{-1}} \right)$.

$$\begin{split} H(s) &= \frac{\Omega_c^2}{s^2 + s\sqrt{2}\Omega_c + \Omega_c^2} \\ H(z) &= \frac{(649.84)^2}{\left(\frac{2}{T}\right)^2 \left(\frac{1-z^{-1}}{1+z^{-1}}\right)^2 + \frac{2}{T} \left(\frac{1-z^{-1}}{1+z^{-1}}\right) \sqrt{2} (649.84) + (649.84)^2} \\ H(z) &= \frac{0.067 + 0.135z^{-1} + 0.067z^{-2}}{1 - 1.143z^{-1} + 0.413z^{-2}} \end{split}$$

5 Invert the Z-transform to find the difference equation.

$$y[n] = 0.067 x[n] + 0.135 x[n-1] + 0.067 x[n-2] + 1.143 y[n-1] - 0.413 y[n-2]$$

Direct form I IIR implementation

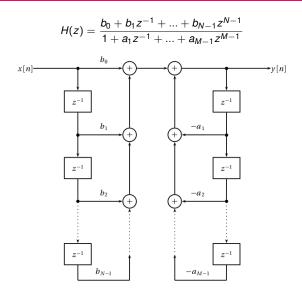


Figure 7.24 Direct Form implementation of an IIR filter.

Direct form I IIR implementation inverted

$$H(z) = \frac{b_0 + b_1 z^{-1} + b_2 z^{-2}}{1 + a_1 z^{-1} + a_2 z^{-2}}$$

By the commutative properties of the z-transform, we can invert the order of computation to turn the Direct Form I structure into a new structure.

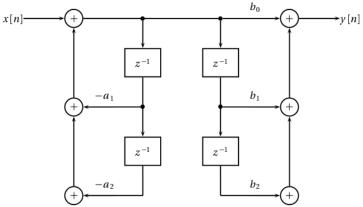


Figure 7.25 Direct form I with inverted order.

Direct form II IIR implementation

$$H(z) = \frac{b_0 + b_1 z^{-1} + b_2 z^{-2}}{1 + a_1 z^{-1} + a_2 z^{-2}}$$

We can then combine the parallel delays together. This implementation is called Direct Form II; its obvious advantage is the reduced number of the required delay elements (hence of memory storage).

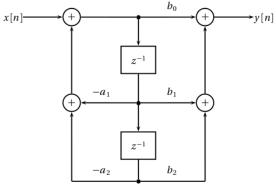


Figure 7.26 Direct Form II implementation of a second-order section.

IIR cascade implementation

The cascade structure of N second-order sections is much less sensitive to quantization errors than the previous Direct form II of order $2 \cdot N$.

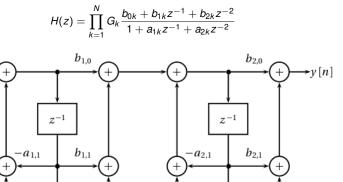


Figure 7.27 4th order IIR: cascade implementation.

 $b_{1,2}$

 $b_{2,2}$

 $-a_{2,2}$

FIR vs IIR

FIR, pros:

- Unconditional stability (no poles).
- Precise control of the phase response and, in particular, exact linear phase.
- Robustness with respect to finite numerical precision hardware.

FIR, cons:

- Longer input-output delay.
- Higher computational cost with respect to IIR solutions.

IIR, pros:

- Lower computational cost with respect to an FIR with similar behavior.
- Shorter input-output delay.
- Compact representation.

IIR, cons:

- Stability is not guaranteed.
- Phase response is difficult to control.
- Design is complex in the general case.
- Sensitive to numerical precision.

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