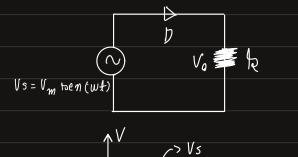
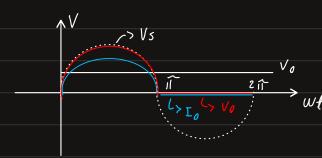
· Com canga nessistiva:

$$V_0 = \frac{\sqrt{m}}{2\pi} \cdot \left( -cgs(\omega t) \right)^{\pi}$$

$$V_g = V_{\frac{M}{211}}$$
,  $(1+1) = V_{\frac{M}{211}}$ 





$$Vo_{hms} = \frac{Vm^2}{z\tilde{n}} \int_0^{\tilde{n}} \left( \frac{1}{z} - \frac{1}{z} \cos(zwt) \right) d(wt)$$

Vanns = 
$$\sqrt{\frac{vm^2}{z\tilde{n}}} \cdot \left( \left( \frac{1}{2} wt \right)^{\tilde{n}} \right) - \frac{1}{z} \cdot \frac{\sin(zwt)}{z} \right)^{\tilde{n}}$$

$$Vo_{nms} = \sqrt{\frac{Vm^2}{z \hat{I}}} \cdot \sqrt{\frac{\hat{I}}{z}} - \frac{1}{4}(0-0)$$
  $\Longrightarrow Vo_{nms} = Vm$ 

· Com canga AL

=> 
$$i_{9H}$$
:  $\frac{dio + kio = 0}{dt} = 0 \Rightarrow \frac{dio}{io} = -\frac{k}{L} dt \Rightarrow lnio = -\frac{k}{L} t + c$ 

=> iop: io) + k io = 
$$\underline{Vm}$$
 benwt =  $\underline{Vm}$  cos( $Wt - 90^9$ )

$$\int W I_0 + k I_0 = \underline{Um} \left[ -90^\circ \right] = \sum I_0 = \frac{\sqrt{m/L} \left[ -90^\circ \right]}{\int W + k/L} = \frac{\sqrt{m} \left[ -90^\circ \right]}{\int W L + k}$$

$$T_0 = \frac{Vm L^{-900}}{|Z| L^{8}}$$
,  $|Z| = \sqrt{R^2 + (WL)^2}$  e  $x = tan^{-1}(WL/R)$ 

$$\overline{L_0} = \frac{\sqrt{m} \left[ -90^{\circ} - \alpha^{\circ} \right]}{|Z|} \Rightarrow \overline{I_0(A)} = \frac{\sqrt{m} \cos(\omega t - \alpha^{\circ} - 9a^{\circ})}{|Z|}$$

$$\frac{io_{b}(t) = vm}{121}$$
 ben(wt-8)

Logo, 
$$i_0(t) = ce^{-\frac{k}{L}t} + \underbrace{Vm}_{1 \ge 1} \text{ ben}(wt - \alpha)$$
; Sabe-se que em

Assim, 
$$Q = C + \frac{vm}{|z|} \text{ ben } (-a) = c = \frac{vm}{|z|} \text{ ben } (a)$$

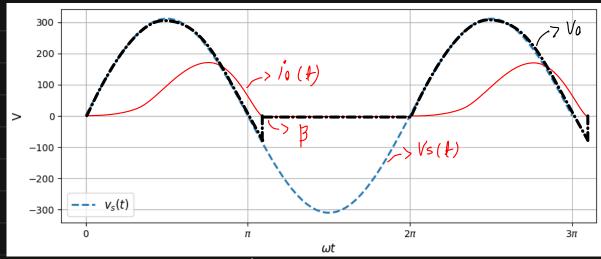
$$lo(t) = Vm \left[ ben(Wt-0) + benge^{-b/Lt} \right]$$

$$|z|$$

$$lo(wt) = Vm \left[ hen(wt-\alpha) + hence^{-\frac{k}{w_L} \cdot wt} \right]; g \leq wt \leq \beta$$

$$|z|$$

# B -> Ângulo de extinção



Idealmente, o diodo para de conduzir quando io(t)=0.

Nesse caso;  

$$i_0(\beta) = \frac{Vm}{|z|} \left( hen(\beta - \beta) + hen(\beta) e^{-\frac{he}{hw}\beta} \right) = 0$$

ben(
$$\beta - \beta$$
) + ben( $\delta$ ) e  $\frac{k}{LW}$  = 0 (Equação transcendental)

$$V_0 = \frac{1}{z \hat{n}} \int_0^{\beta} v_m \ker(w + i) d(w + i) = \frac{v_m}{z \hat{n}} (-\cos(w + i) f_0^{\beta})$$

$$V_0 = \frac{v_m}{z \hat{n}} (1 - \cos(\beta))$$

$$V_{0,1m5} = \frac{1}{z_{11}} \int_{0}^{\beta} (Vm ben(wt))^{2} d(wt)$$

$$V_{0,\text{HMS}} = \frac{V_{m}^{2}}{z_{11}} \int_{0}^{\beta} \left( \frac{1}{z} - \frac{1}{z} \cos(z_{11} \omega t) \right) d(\omega t)$$

$$V_{o,hms} = \sqrt{\frac{Vm^2}{z\pi}} \left\{ \frac{1}{z} Wt \right\}_{o}^{B} - \frac{1}{z} \frac{ben(zwt)}{z} \right\}_{o}^{B}$$

$$V_{0 \text{ hms}} = \frac{Vm^2 \left\{ \frac{B}{2} - \frac{1}{4} \text{ ben}(2B) \right\}}{2\pi}$$

$$V_{ohms} = V_{m} - \frac{1}{2\Pi} \cdot \frac{2B - ben(2B)}{4}$$

$$V_{0}_{hms} = V_{m} - \frac{ZB - ben(ZB)}{8\pi}$$

Considerando o circuito do retificador mostrado na Fig. 6.2(a), onde a fonte  $v_s$  possui amplitude  $V_m=220\sqrt{2}$  V e frequência 60 Hz, e a carga RL é formado por  $R=45~\Omega$  e L=100 mH. Determine: (a) o ângulo de extinção  $\beta$ , (b) a tensão média  $V_o$  sobre a carga, (c) a corrente média na carga, (d) a corrente eficaz na carga e (e) a potência dissipada pelo resistor R.

a) 
$$S = tan^{-1}(z^{560.0}, 1/45) \stackrel{\sim}{=} 2z, 43^{\circ} = 0,394 \text{ had}$$

$$bin(\beta - 0,4) + ben(0,4) e^{-1,19\beta} = 0$$

$$\beta \stackrel{\sim}{=} 220^{\circ}$$

c) 
$$i_9(wt) = \frac{Vm}{|Z|} \left( \text{hen}(wt - \alpha) + \text{hen}\alpha e^{-\frac{k}{Lw}} \cdot wt \right), \alpha = 0,4 \text{ had}$$

$$|Z| = 45 \Omega$$

$$I_0 = \frac{1}{2\pi} \int_0^{\beta} (6,91) \sin(\omega t - 0,4) + 2,69e^{-1,19\omega t} d(\omega t)$$

$$\frac{1}{2\pi} \cdot \left\{ -6,91\cos(\omega t - 0,4) \right\}_{0}^{\beta} + 2,69 \cdot \frac{e^{-1,19}\omega t}{-1,19} \right\}_{0}^{\beta} ; \beta = 3,84$$

d) 
$$I_{0_{\text{nm5}}} = \sqrt{\frac{1}{2\pi}} \int_{0}^{\beta} (6,91) \sin(wt-0,4) + 2,69e^{-1,19wt} \int_{0}^{z} d(wt)$$

$$To_{hms} = \begin{cases} \frac{1}{2\pi} \int_{0}^{3\pi} \left(44, 45 \sin^{2}(wt - 0,4) + 34, 14 \sin(wt - 0,4) e^{-1,19wt} + 4,24 e^{-2,38wt}\right) d(wt) \end{cases}$$

Resolvendo cada integnal:

(a) i 
$$\alpha = \int_{0}^{\beta} 4^{4}, 45 \sin^{2}(w t - 0, 4) ol(w t)$$
;  $w t - 0, 4 = x \frac{dx}{dwt} = 1$ 
 $\alpha = \int_{-0,4}^{\beta - 0,4} 4^{4}, 45 \sin^{2}(x) dx = 4^{4}, 45 \int_{-0,4}^{\beta - 0,4} \left(\frac{1}{2} - \frac{1}{2}\cos(2x)\right) dx$ 
 $\alpha = 4^{4}, 45 \left(\frac{1}{2} \cdot \left[\beta - 0, 4 + 0, 4\right] - \frac{1}{4} \left[\sin(2\beta - 0, 8) - \sin(-0, 8)\right]\right)^{\beta = \frac{1}{3,81}}$ 
 $\alpha = 4^{6}, 2^{9}$ 

b) i  $b = \int_{0}^{\beta} 3^{4}, 1^{4} \sin(w t - 0, 4) e^{-\frac{1}{2}i^{9}w^{4}} d(w t)$ ;  $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^{\beta} u v = u v - \int v du$ 
 $\int_{0}^$ 

 $\frac{x \cdot u = \cos(\omega t - 0, A)}{du = -\sin(\omega t - 0, A)} \qquad \frac{dv = e^{-1, 19\omega t} d(\omega t)}{u = e^{-1, 19\omega t}}$   $\frac{dut}{dut} = -1, 19\omega t$ 

$$= \frac{3\frac{1}{1}, \frac{14}{1}}{-1, \frac{14}{1}} \left\{ \text{ bin } (\beta - 0, 4) e^{-1, \frac{14}{1}\beta} + \text{ bin } (0, 4) - \left( \frac{\cos(\omega \pm - 0, 4) \cdot e^{-1, \frac{14}{14}\beta}}{-1, \frac{14}{14}} \right)^{\beta} - \frac{e^{-1, \frac{14}{14}\beta}}{-1, \frac{14}{14}} \left\{ \text{ bin } (\beta - 0, 4) e^{-1, \frac{14}{14}\beta} + \text{ bin } (0, 4) - \left( -\frac{\cos(\beta - 0, 4) \cdot e^{-1, \frac{14}{14}\beta}}{1, \frac{14}{14}} + \frac{\cos(\beta, 4)}{1, \frac{14}{14}} \right)^{\beta} - \frac{1}{1, \frac{14}{14}} \left\{ \text{ bin } (\beta - 0, 4) e^{-1, \frac{14}{14}\beta} + \text{ bin } (0, 4) + \frac{\cos(\beta - 0, 4) \cdot e^{-1, \frac{14}{14}\beta}}{1, \frac{14}{14}} - \frac{\cos(\beta, 4)}{1, \frac{14}{14}} - \frac{1}{1, \frac{14}{14}} \left\{ \text{ bin } (\beta - 0, 4) e^{-1, \frac{14}{14}\beta} + \text{ bin } (0, 4) + \frac{\cos(\beta - 0, 4) \cdot e^{-1, \frac{14}{14}\beta}}{1, \frac{14}{14}} - \frac{\cos(\beta, 4)}{1, \frac{14}{14}} - \frac{1}{1, \frac{14}{14}} \right\} - \frac{3\frac{1}{14}}{1, \frac{14}{14}} \left\{ \text{ bin } (\beta - 0, 4) e^{-1, \frac{14}{14}\beta} + \text{ bin } (0, 4) + \frac{\cos(\beta - 0, 4) \cdot e^{-1, \frac{14}{14}\beta}}{1, \frac{14}{14}} - \frac{\cos(\beta, 4)}{1, \frac{14}{14}} - \frac{\cos(\beta, 4)}{1, \frac{14}{14}} \right\}$$

Assim:
$$b = 3\frac{1}{1} \cdot \frac{14}{14} \left\{ \text{ bin } (\beta - 0, 4) e^{-1, \frac{14}{14}\beta} + \text{ bin } (0, 4) + \frac{\cos(\beta - 0, 4) \cdot e^{-1, \frac{14}{14}\beta}}{1, \frac{14}{14}} - \frac{\cos(\beta, 4)}{1, \frac{14}{14}} - \frac{\cos(\beta, 4)}{1, \frac{14}{14}} - \frac{\cos(\beta, 4)}{1, \frac{14}{14}} \right\}$$

$$\frac{3\frac{1}{14}}{14} \left\{ \text{ bin } (\beta - 0, 4) e^{-1, \frac{14}{14}\beta} + \text{ bin } (0, 4) + \frac{\cos(\beta - 0, 4) \cdot e^{-1, \frac{14}{14}\beta}}{1, \frac{14}{14}} - \frac{\cos(\beta, 4)}{1, \frac{14}{14}} - \frac{\cos($$

$$\frac{37,14}{-1,19} \begin{cases} bin(\beta-0,4)e^{-1,19\beta} + bin(0,4) + cos(\beta-0,4).e^{-1,19\beta} - cos(0,4) \\ 1,19 \end{cases} \begin{cases} -\frac{34,14}{1,19} \end{cases}$$

$$34,14 \int_{0}^{\beta} hoin(\omega t - 0,4) e^{-1,19} wt d(\omega t) + \underbrace{34,14}_{1,19} \int_{0}^{\beta} e^{-1,19} wt hoin(\omega t) d(\omega t)$$

$$= \underbrace{34,14}_{-1,19} \int_{0}^{\beta} hoin(\beta - 0,4) e^{-1,19} + hoin(0,4) + \underbrace{\cos(\beta - 0,4) \cdot e^{-1,19}}_{1,19} - \underbrace{\cos(\beta,4)}_{1,19} \int_{0}^{\beta} hoin(\omega t) d(\omega t)$$

$$63,41 \int_{0}^{B} bin(wt-0,4)e^{-1,19wt} d(wt) = \frac{34,14}{-1,19} \begin{cases} bin(\beta-0,4)e^{-1,19\beta} + bin(0,4) + \frac{\cos(\beta-0,4)\cdot e^{-1,19\beta}}{1,19} - \frac{\cos(0,4)}{1,19} \end{cases}$$

$$34,14.1,406$$
 bin  $(wt-0,4)e^{-1,19}$  d $(wt) = \frac{34,14}{-1,19}$  bin  $(\beta-0,4)e^{-1,19\beta}$  + bin  $(0,4)$  +  $\frac{\cos(\beta-0,4).e^{-1,19\beta}}{1,19}$  -  $\frac{\cos(0,4)}{1,19}$ 

$$b = 34,14 \int_{0}^{B} bin(\omega t - 0,4) e^{-1,19} d(\omega t) =$$

$$34,14 \int_{0}^{B} bin(\beta - 0,4) e^{-1,19} + bin(0,4) + cos(\beta - 0,4) e^{-1,19} - cos(0,4)$$

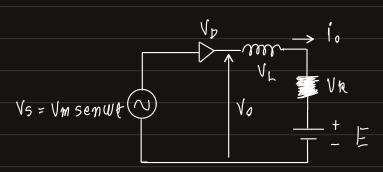
$$\frac{37,14}{-1,19} \begin{cases} bin(\beta-0,4)e^{-1,19\beta} + bin(0,4) + \frac{\cos(\beta-0,4).e^{-1,19\beta}}{1,19} - \frac{\cos(0,4)}{1,19} \end{cases}$$

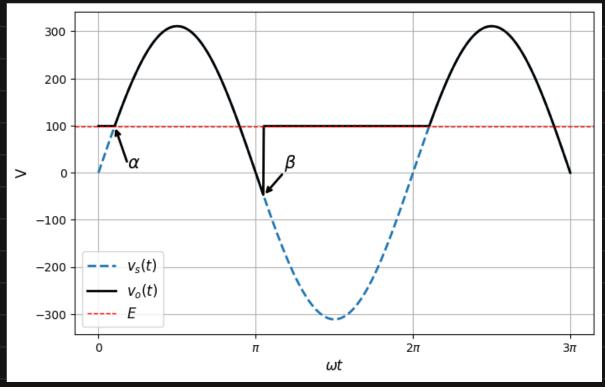
$$C = -3,04.\left(e^{-2,38\beta} - e^{\circ}\right), \beta = 3,81$$

• Assim, 
$$I_{o_{hms}} = \sqrt{\frac{1}{z_{1}}} (a + b + c) = \sqrt{\frac{1}{z_{1}}} (46, 29 + 4, 25 + 3, 04)$$

$$I_{o_{hm}} = 3,414$$

· Com canga RLE





o O diodo bassa a conduzin quando vs >> E.

com isso, vs = Vmsen(wt) = E, wt = \preceq

vm sen(\pi) = E

$$\propto = alncsen\left(\frac{E}{\sqrt{m}}\right)$$

· Com o diodo conduzindo, tem-se as seguintes nelações ole tensão:

$$Vmsen(wt) = Ldi(t) + ki(t) + E$$

$$L_{di}(t) + R_{i}(t) = Vm hen(wt) - E$$

A solução e dada bon: in + ip = i(+)

# Solução hamagénea

$$L di(t) + ki(t) = 0$$

$$dt$$

$$di(t) = -ki(t)$$

$$dt$$

$$\int_{i}^{di} = \int_{L}^{-\frac{1}{2}} dt$$

$$\ln(i) = -\frac{1}{2} t + C$$

-k+

### Solução Particular

$$\frac{dt}{dt}$$

$$\frac{d}{dt}$$

$$\frac{d}{dt}$$

$$\frac{d}{dt}$$

$$\frac{d}{dt}$$

$$T_{\parallel} = \frac{Vm - 90^{\circ}}{R + JWL} = \frac{Vm - 90^{\circ}}{|Z| |\mathcal{B}|}$$

o qual: 
$$|Z| = \sqrt{k^2 + (wL)^2}$$
  
 $\emptyset = \operatorname{anctan}\left(\frac{wL}{k}\right)$ 

$$I_1 = Vm \left[ -9 - 90^{\circ} = \right] ip_1 = Vm \cos(wt - 8 - 90^{\circ})$$

$$|Z| \qquad |Z| \qquad -90^{\circ}$$

$$|\dot{p}| = \sqrt{m} \operatorname{sen}(\omega t - \theta)$$

$$\begin{array}{c} Ldi(t) + ki(t) = -E = > i_{p_2} = -E \\ \hline Assim, \end{array}$$

· pontanto,

assumindo  $|(\alpha)=9$ 

$$Ce^{\frac{h}{L}\omega} + Vm sen(\propto -a) - \frac{E}{R} = 0$$
|Z|

$$C = \left[\frac{E}{R} - \frac{Vm}{IZI} \operatorname{Sen}(\alpha - \alpha)\right] e^{\frac{k}{L}\omega} \alpha$$

$$i(t) = \begin{bmatrix} E - Vm & sen(\alpha - \alpha) \end{bmatrix} e^{\frac{k}{1w}\alpha} e^{-\frac{k}{2}t} + Vm & sen(wt - \alpha) - E \\ k & |z| & |z| & |z| & |z| & |z|$$

Logo, 
$$i(wt) = \left[\frac{E}{k} - \frac{Vm}{121} \operatorname{sen}(\alpha - \alpha)\right] e^{\frac{k}{Lw}(\alpha - \omega t)} + \frac{Vm}{121} \operatorname{sen}(\omega t - \alpha) - \frac{E}{k}$$

· O diodo pana de conduzin
quando i(13) = 0.

Esboçan as cunvas da tensões de saída

$$V_0 = \frac{1}{2\pi} \left[ \int_{\alpha}^{\beta} v_s(wt) d(wt) + \int_{\beta}^{2\pi+\alpha} Ed d(wt) \right] = \frac{1}{2\pi} \left[ V_m \cdot (\cos \alpha - \cos \beta) + Ed (z_{11} + \alpha - \beta) \right]$$

$$V_0 = I$$
  $V_m(cos x - cos \beta) + Ed(x - \beta + zît)$ 

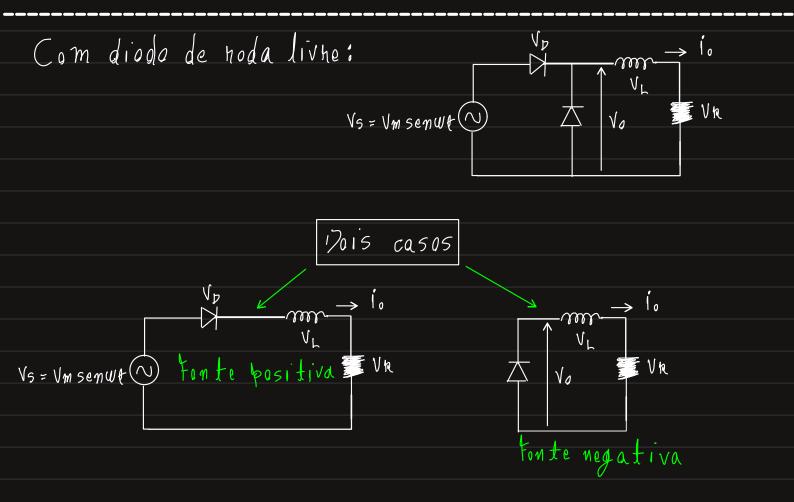
· Poténcia média tonnecida à canga:

$$P_0 = \frac{1}{z_{11}^{n}} \int_0^{z_{11}^{n}} V_0(wt) i_0(wt) d(wt)$$

$$P_0 = \frac{1}{2\pi} \left[ \int_0^{2\pi} (Vk(wt) + VL(wt) + Ed) i_0(wt) d(wt) \right]$$

$$b_0 = \frac{R}{z_1^n} \int_0^{z_1^n} \int_0^{z_1^n$$

L> poténcia ativa média fonnecida pela fonte CA.



· Formas de onda:



Obs.: A cunva de io é considerando o modo de condução contínua, ou seja, L muito grande.

· Ana lise da connente:

$$0 \le W + \le 1$$
:  $\log(W +) = \frac{Vm}{|z|} \left[ \operatorname{ben}(W + - \alpha) + \operatorname{ben} \alpha e^{\frac{-k}{W_L} \cdot W + 1} \right]$ 

$$i(t) = ce^{-\frac{R}{L}t} \Rightarrow i(wt) = ce^{-\frac{R}{L}wt}$$

♥VI: ((î) = io(î) =>

$$Ce^{-\frac{k}{hw}} = \frac{Vm}{[ben(\tilde{1} - \alpha) + ben\alpha e^{\frac{-k}{w_L}}]}$$

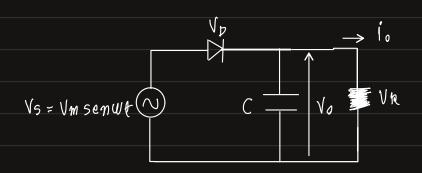
$$C = \frac{Vm}{[Ebe(\tilde{1} - \alpha)e^{-\frac{k}{hw}}]} + ben\alpha$$

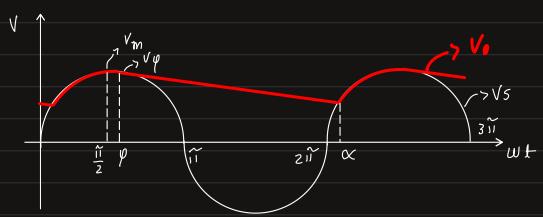
$$|Z|$$

$$|Z|$$

Assim, no semiciclo negativo a conhente decai exponencialmente.

#### · Com filtro capacitivo na saida:





- · φ= 17/2 ; Vp= Vm pois Rc>> 1/F.
- · Tensão sobre a carga:

$$(z_{1} + \alpha) \angle wt \angle (z_{1} + \varphi)$$

$$V_{0} = V \text{ m se n } (wt)$$

$$V_{p} \longrightarrow i_{0}$$

$$V_{r} \longrightarrow V_{R}$$

$$Ve + 1e k = 0$$

$$Ve + 1e k = 0$$

$$RC dVe + Ve = 0$$

$$dt$$

$$dVe = -1 : Ve = > dVe = -1 . dt$$

$$dt \quad ke$$

$$Ve \quad ke$$

$$In Ve = -1/ket + ke = > Ve = ke e^{-\frac{1}{Re}} t$$

$$Ve(wt) = ke e^{-\frac{1}{Rew}} wt$$

$$Ve(wt) = ke e^{-\frac{1}{Rew}} wt$$

$$Ve(y) = Ve(y) = Ve(y) = V(y)$$

$$Ve(y) = ke e^{-\frac{1}{Rew}} (y - wt)$$

$$Ve(y) = ke e^{-\frac{1}{Rew}} (y - wt)$$

$$Ve(y) = Ve(y) e^{-\frac{1}{Rew}} (y - wt)$$

$$V_{0}(w +) = \begin{cases} Vmsen(w +) & (z\hat{i} + \alpha) \angle w + \angle (z\hat{i} + \varphi) \\ V(\varphi) e^{\frac{1}{|\alpha + \alpha|}} (\varphi - w +) & (2 + \alpha) \angle w + \angle (z\hat{i} + \alpha) \end{vmatrix}$$

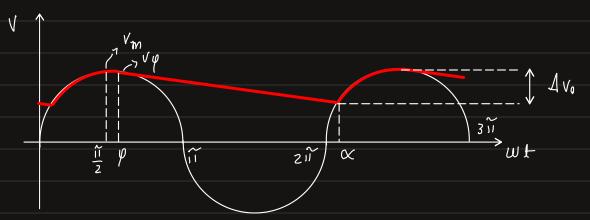
Vomin: (Abhoximando 
$$\alpha = \tilde{1}/2$$
) Logo,  $V(z\tilde{1}+\alpha) = V(y)e^{\frac{1}{kc\omega}}(y-z\tilde{1}-\alpha)$ 

$$V_{omin} = V(y)e^{\frac{1}{kc\omega}}(\tilde{1}/2-z\tilde{1}-\tilde{1}/2) = V(y)e^{\frac{1}{kc\omega}}$$

Assim, 
$$V_{0,min} = V(\varphi) \left( 1 - \frac{2 \hat{1} \hat{1}}{w k c} \right) = V m sen(\hat{1}/z) \left( 1 - \frac{2 \hat{1} \hat{1}}{w k c} \right)$$

$$V_{0,min} = V_{m} \left( 1 - \frac{2 \tilde{I}}{w kc} \right)$$

· Oscilação da tensão de saída: 1 vo = Vomáx - Vomin



$$4 \text{ Vo} = \text{Vm Sen}(\tilde{1}/2) - \text{Vm}\left(1 - \frac{z\tilde{1}}{w kc}\right) = \frac{\text{Vm} z\tilde{1}}{w kc} = \frac{\text{Vm}}{kc}$$

Luiz Felipe

