

# Linearly Stratified Flow Past Rotating 2D Ellipses

## Hilbert and DMD

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# Motivation

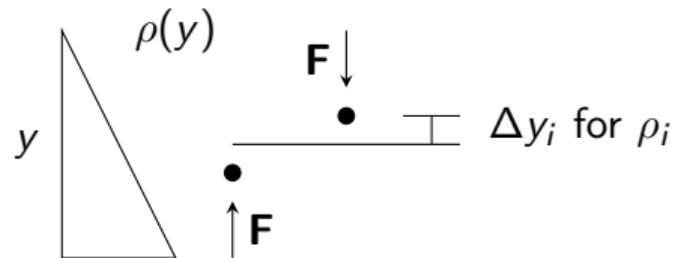


Figure: Restoring force and equilibrium on particle  $i$ .

- In nature, there exist innumerable flows with varying density, known as stratified flows, such as the ocean.
- The density variation is caused by salt content or temperature variation.
- Stratified mediums exhibit a restoring force due to particles being in the lowest potential energy position when at the same depth as particles of similar density.
- This force creates *internal gravity waves*.
  - Flow past a bluff body creates steady gravity waves known as *lee waves*.
  - Bluff body oscillation forms unsteady waves.

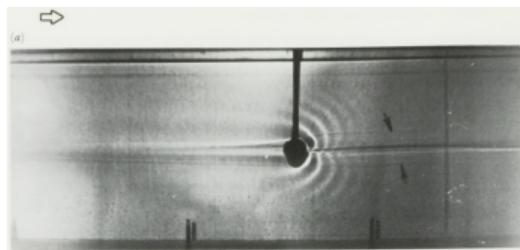


Figure: Lee waves from flow past a cylinder Boyer et al. (1989).

# Motivation

- Internal gravity waves and other effects from stratification affect the flow structures and forces on bodies.
- Stratification is defined by the Densimetric Froude number.
  - Lower Froude number means higher stratification.
- Submersible bodies are approximated by slender bodies, and nonspherical bodies have been neglected in past studies.
- Ortiz-Tarin *et al.* (2019) look at static slender bodies; we introduce rotation.
- We want to better understand the dynamics of spheroidal bodies in stratified flows for design in submersible vehicles.

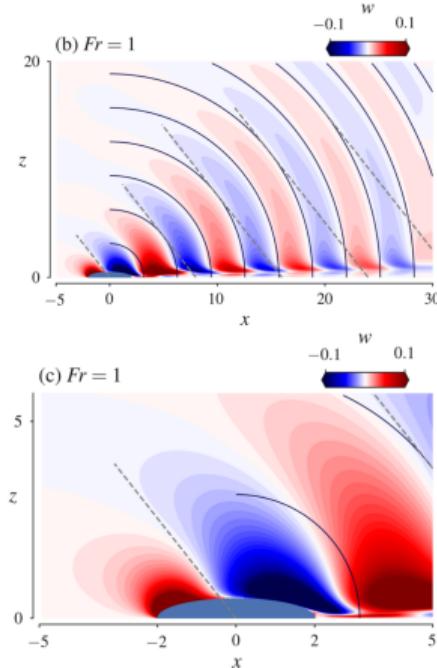


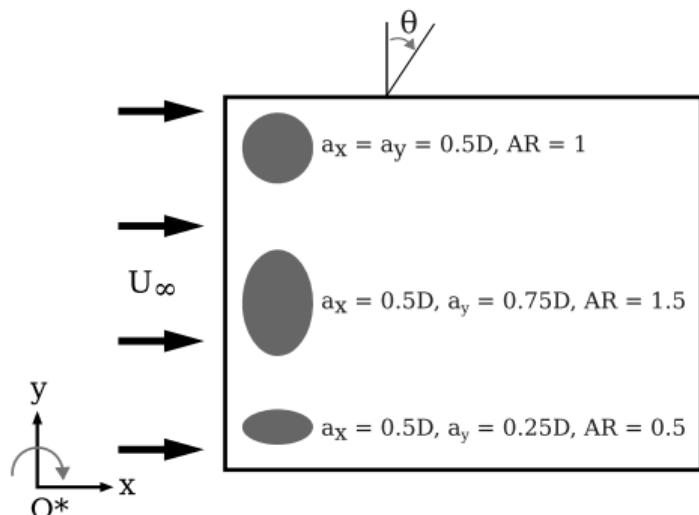
Figure: Internal gravity waves shown in the  $y$ -velocity fields Ortiz-Tarin *et al.* (2019).

# Equations and Setup

Incompressible Navier-Stokes Equations (1), with Boussinesq approximation and transport equation (2).

$$\frac{\partial \mathbf{u}}{\partial t} + \mathbf{u} \cdot \nabla \mathbf{u} = -\nabla p + \frac{1}{Re} \nabla^2 \mathbf{u} - \frac{1}{Fr^2} (\rho' - \rho_0) \hat{y}, \quad \nabla \cdot \mathbf{u} = 0 \quad (1)$$

$$\frac{\partial \rho'}{\partial t} + \mathbf{u} \cdot \nabla \rho' = \frac{1}{Pr Re} \nabla^2 \rho' \quad (2)$$



- Density perturbation  $\rho'$  from background density  $\rho_0$ .
- Thermal diffusivity  $\kappa$ , kinematic viscosity  $\nu$
- Aspect ratio  $AR = a_y/a_x$ , with  $\Omega^* = \frac{\Omega D}{2U_\infty}$
- Brunt–Väisälä frequency  $N_{BV} = \left( \frac{g}{\rho_0} \rho'_{y,0} \right)^{1/2}$

$$Re = \rho_0 \frac{UD}{\mu}, \quad Pr = \rho_0 \frac{\kappa}{\mu}, \quad Fr^{-2} = \frac{gD^2}{\rho_0 U^2} |\rho'_{y,0}|$$

# Numerical Methodology - Temporal Discretization

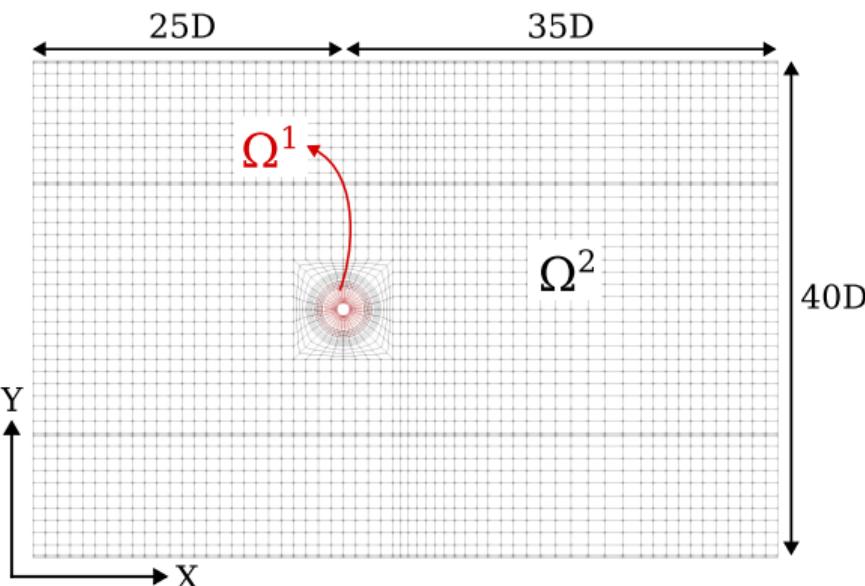
- Semi-implicit BDF-3/EXT-3 timestepping
  - Time derivative - BDF-3
  - Nonlinear terms - EXT-3
  - Pressure and viscous terms - implicit
- Spatially interpolated boundary conditions at interdomain boundaries (Mittal *et al.*, 2019).
  - Picard iterations
  - M-order temporal extrapolation at boundaries for accuracy
  - Q corrector iterations for stability
- Arbitrary Lagrangian-Eulerian (ALE) formulation to track spinning inner mesh.
- Method allows better shape adaptation.
- Spectral accuracy retained

# Numerical Methodology - Spatial Discretization

- Spectrally accurate overset grid method
  - Inner mesh ( $\Omega^1$  : 512 elements)
  - Outer mesh ( $\Omega^2$  : 3200 elements)
- Schwarz-Spectral Element Method (Schwarz-SEM)
- Hexahedral elements
- Symmetric top and bottom boundaries
- Lagrange polynomials

Parameters	Values
$AR$	0.5, 1.0, 1.5
$Fr^2$	0.01, 0.1, 1.0, 10.0, 100.0, $\infty$
$Re$	120
$Pr$	1
$\Omega^*$	0.0 ( $AR = 1$ only), 1.0

- Polynomial order  $N = 11$
- Gauss-Lobatto-Legendre (GLL) nodes



# Validation

We validate Schwarz-SEM stratification implementation in two ways. First, by validating nonrotating stratified cases against monodomain stratified cases. Second, by comparing rotating unstratified cases with rotating unstratified cases from Lu *et al.* (2018) (two papers) produced with *Ansys<sup>®</sup> Fluent* with *Sliding Mesh*. Drag and lift show similarity.

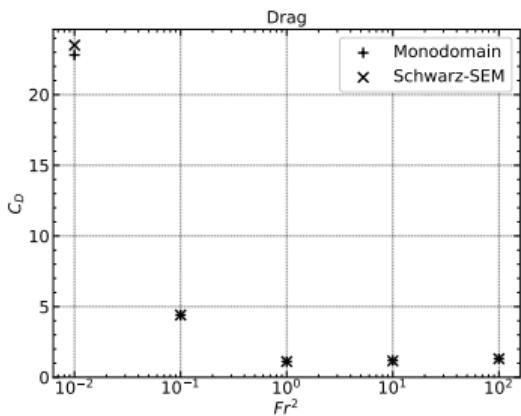


Figure: Comparison of drag against monodomain case.

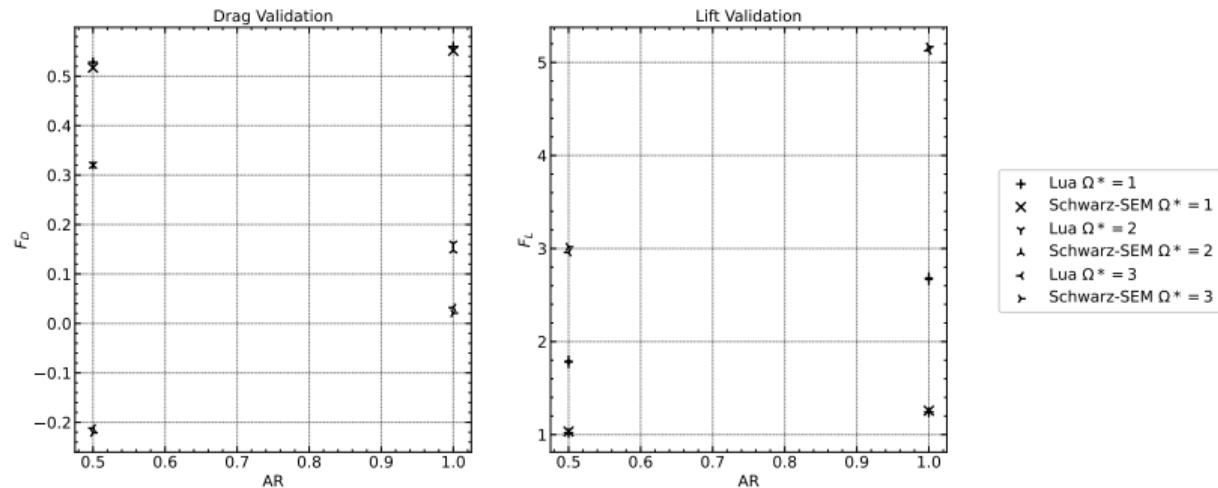
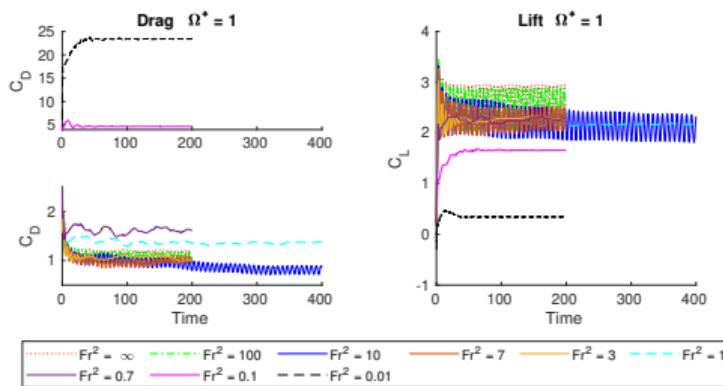
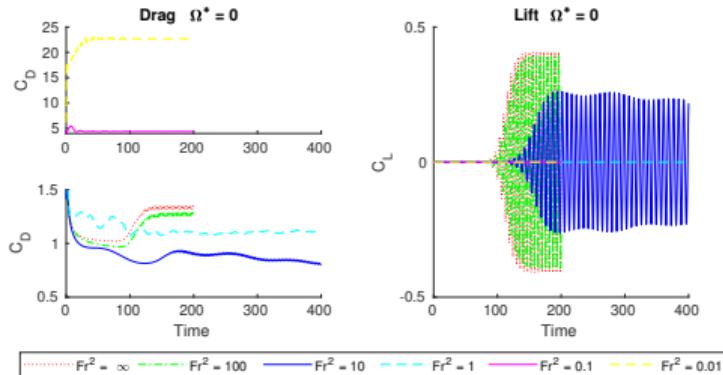


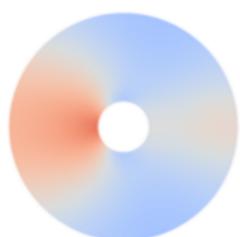
Figure: Comparison of drag and lift in unstratified flow against Lu *et al.* (2018) finite-volume results at  $Re = 200$ .

# Circle Drag and Lift Time Series

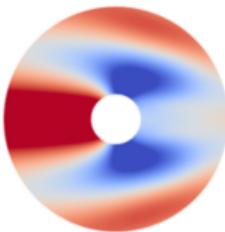


- The plots to the left show time series data for nonspinning and spinning cylinders.
- We observe the presence of different flow regimes
  - A regime in which stratification dominates and there is little oscillation in lift
  - A regime in which vortex-shedding dominates and there is substantial oscillation in lift.
- The increase in drag with stratification increase if a result of upstream blocking.

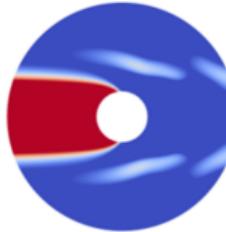
# Circle Drag and Lift



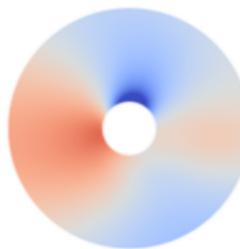
(g)  $Fr^2 = 1, \Omega^* = 0$



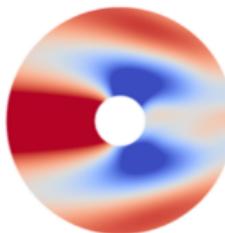
(h)  $Fr^2 = 0.1, \Omega^* = 0$



(i)  $Fr^2 = 0.01, \Omega^* = 0$



(j)  $Fr^2 = 1, \Omega^* = 1$



(k)  $Fr^2 = 0.1, \Omega^* = 1$



(l)  $Fr^2 = 0.01, \Omega^* = 1$

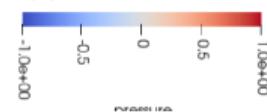


Figure: Pressure distribution around 2D cylinders. High pressure region in front of the body at high stratification is upstream blocking.

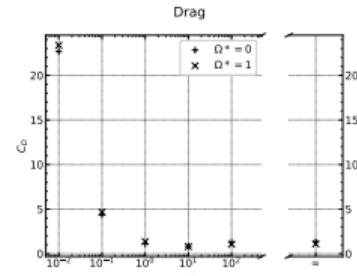


Figure: Mean Drag Coefficients

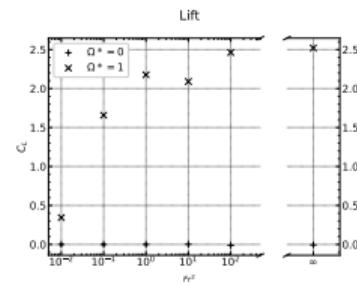
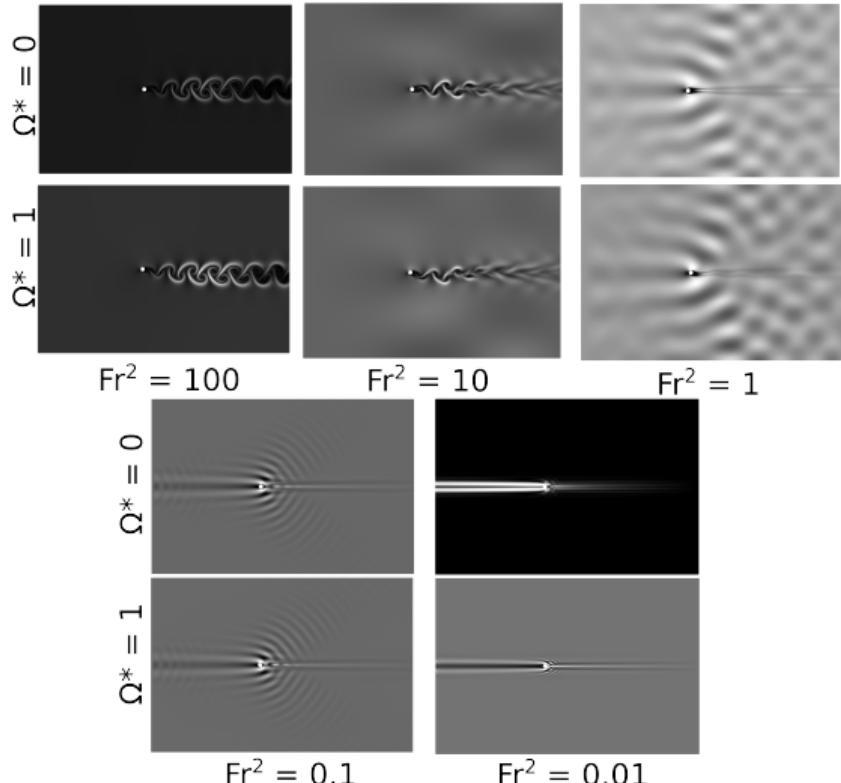


Figure: Mean Lift Coefficients

# Circle Schlieren Plots

- The following plots are Schlieren plots calculated with density gradient  $|\nabla \rho|$
- We observe the presence of different flow regimes
  - A regime in which stratification dominates
  - A regime in which vortex-shedding dominates
- There exists a transitional regime at  $Fr^2 \approx 10$



# Phase Averaged Drag and Lift

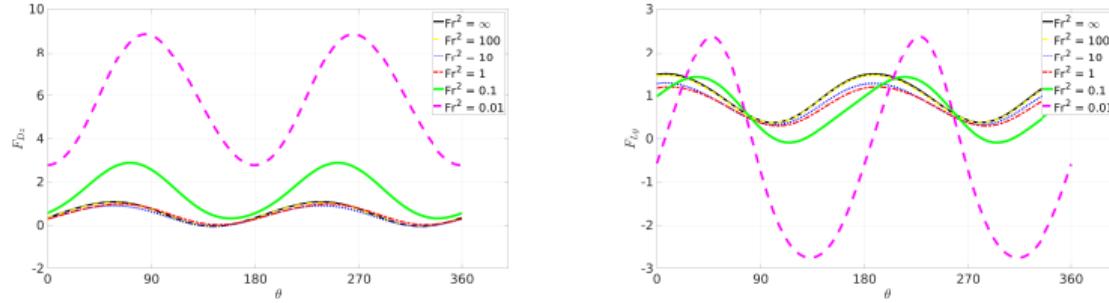


Figure: Phase-averaged drag and lift for  $AR = 0.5$

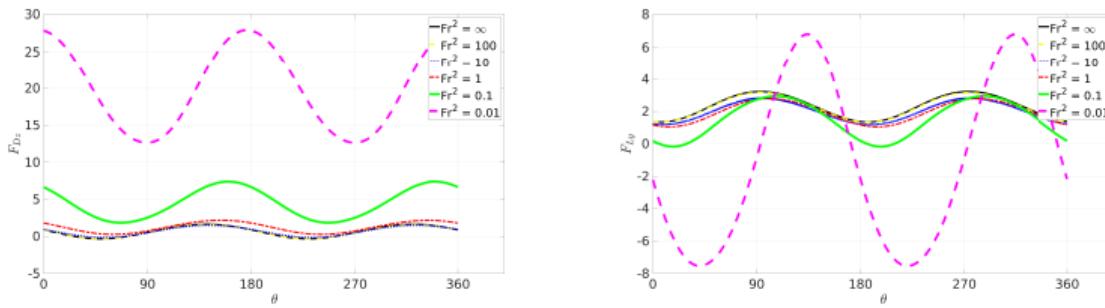
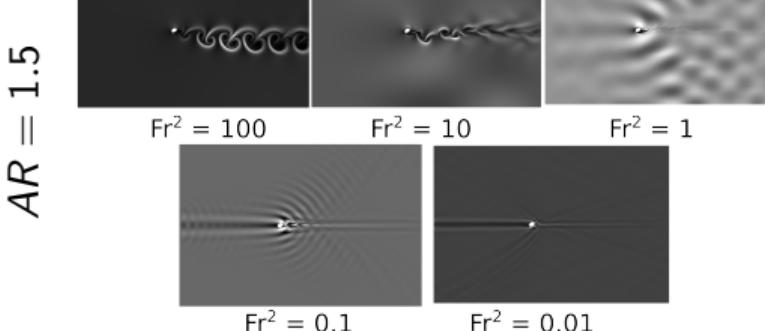
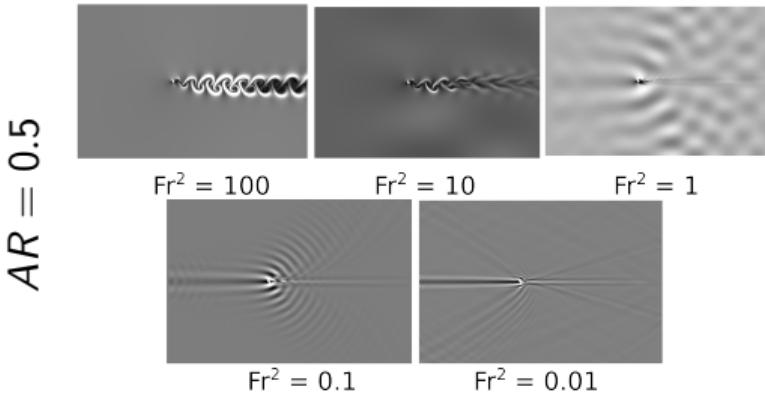


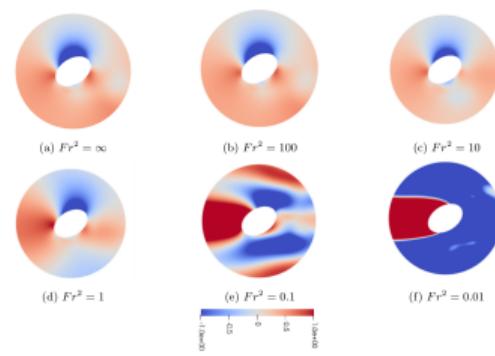
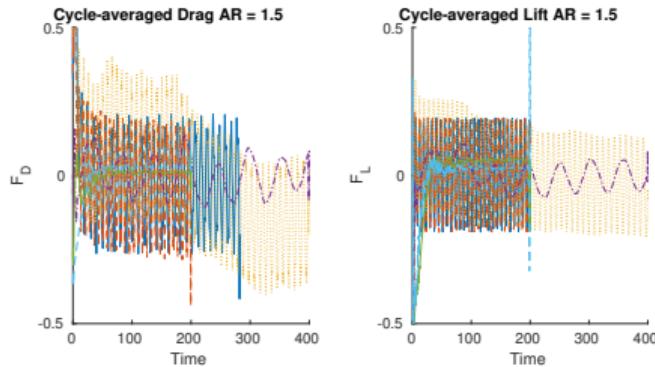
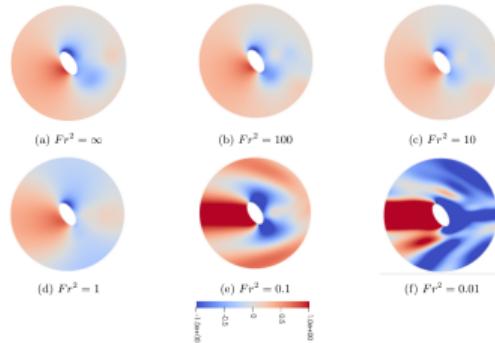
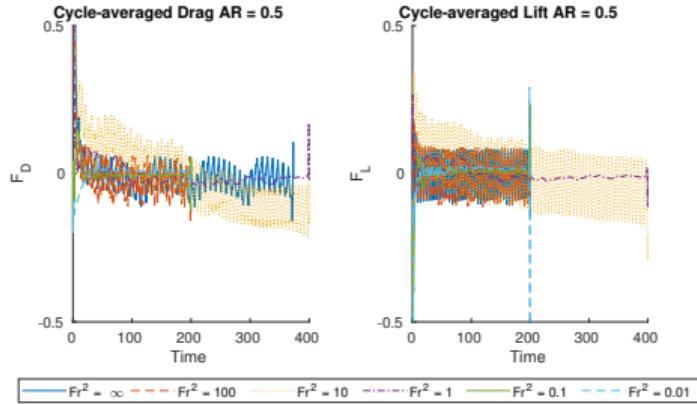
Figure: Phase-averaged drag and lift for  $AR = 1.5$

# Ellipse Schlieren Plots

- Same large-scale flow structures as in the circle cases are present
- Unsteady internal gravity waves manifest themselves in the cases of  $Fr^2 = 0.1, 0.01$
- Internal gravity wave reflection off domain boundaries is present in the  $Fr^2 = 0.01$  case

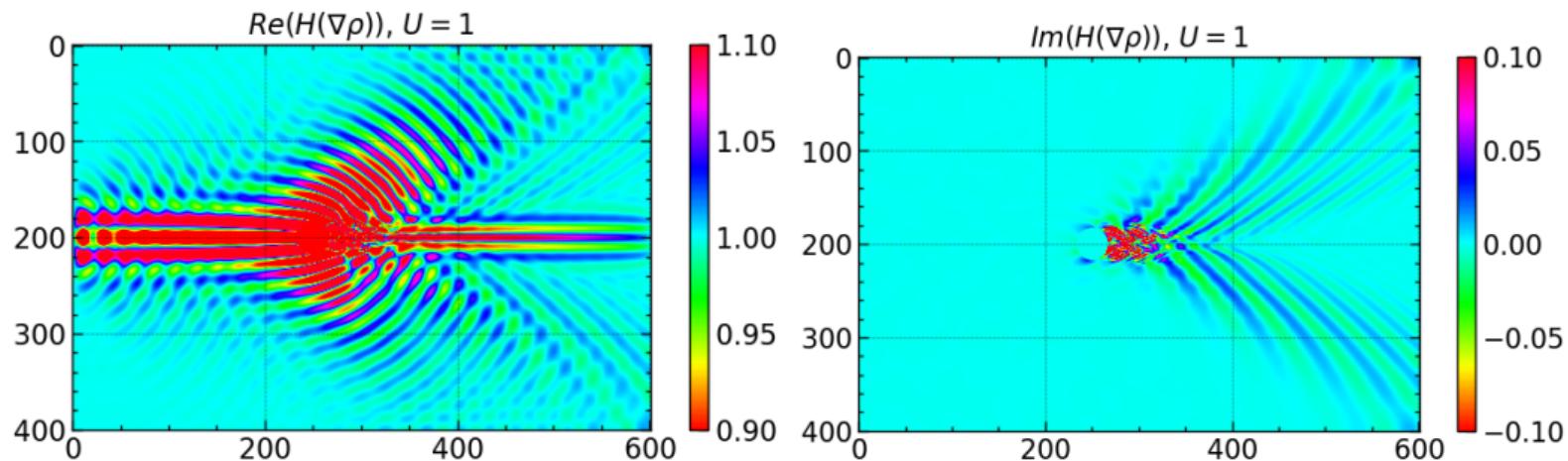


# Cycle-averaged Drag and Lift



# Deeper Analysis

- Applying Hilbert transform to extract analytic signal using FFT
- Follow the procedure outlined by Mercier *et al.* (2008)
- $\mathfrak{H}(|\nabla \rho|) = \mathfrak{F}^{-1}(2H(\mathfrak{F}(|\nabla \rho|)))$
- $Fr^2 = 0.1, AR = 1.5$  case



## Acknowledgements

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## References

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