



Applied Electronics

C2 – Transmission Line Models

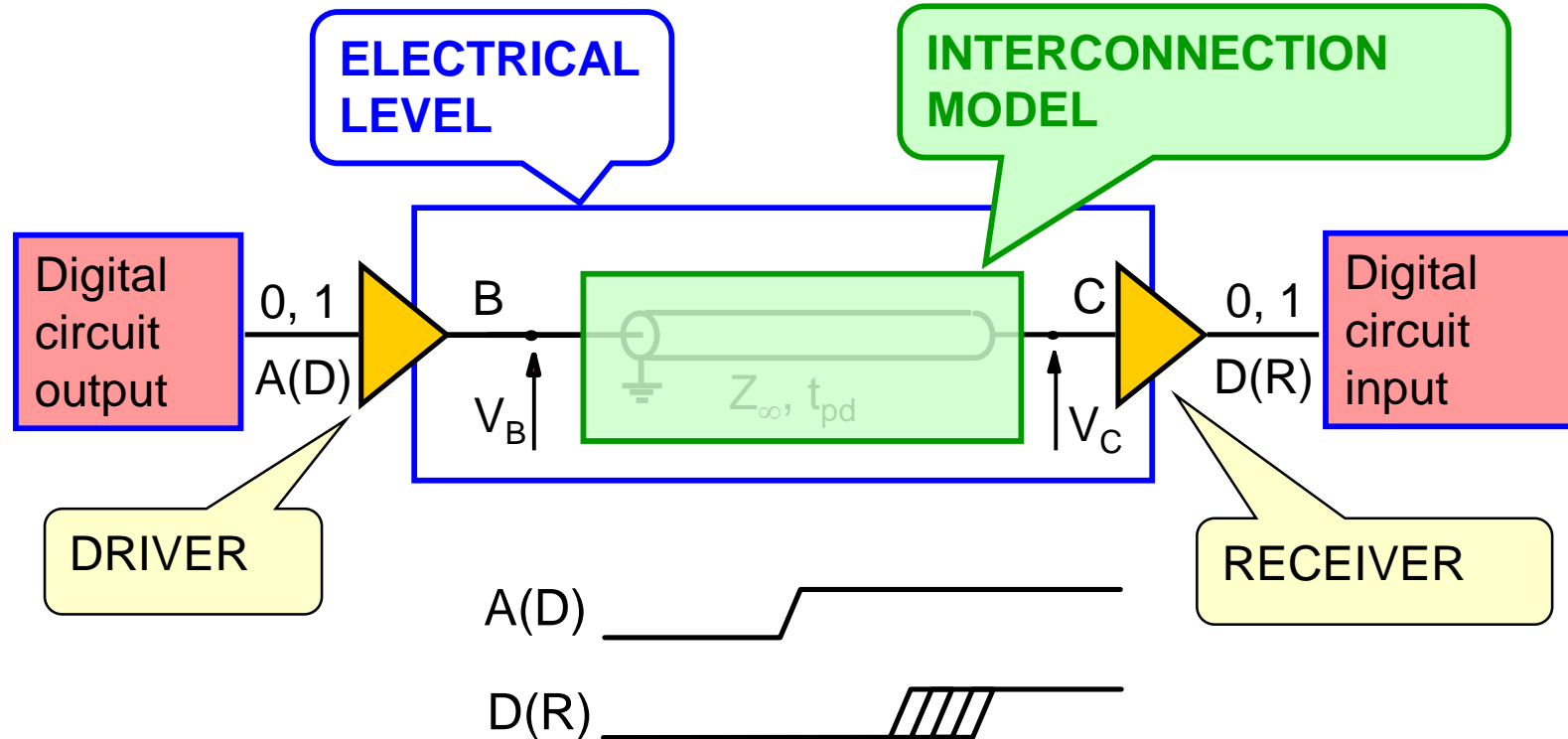
- Transmission lines
- Propagation and reflections
- Evaluation transmission time and skew



Lecture C2: Transmission Line Models

- Transmission lines
- Propagation of digital signals
- Reflections
- Driving conditions
- Transmission time, t_{TX} , and skew, t_K
- References
 - ◆ D. Del Corso: Interconnections for high-speed...
lectures 1, 2

Interconnection system



From B to C (**voltages**): additive noise, variable delay, ...

Effects from A to D (**logical variables**): delay, delay variations (skew).

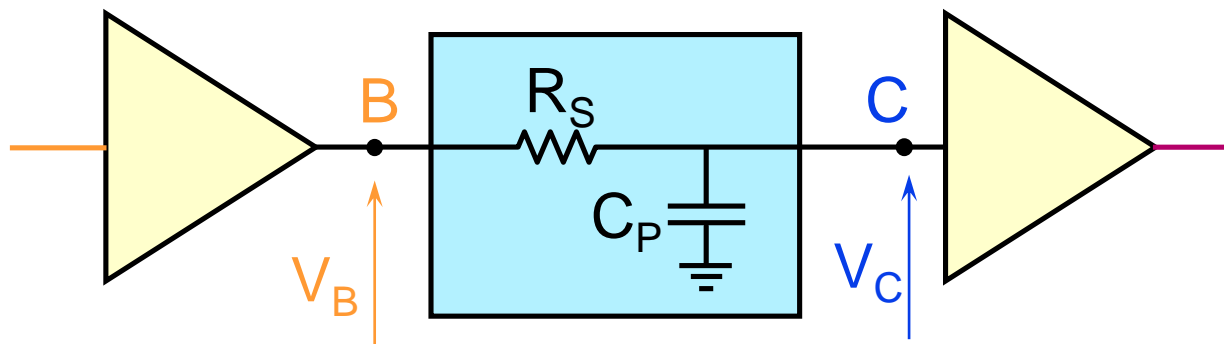


Recall the parameters

- **Transmission time, t_{TX}**
 - ◆ Delay after which is detected the change in the logic state
- With an RC model, t_{TX} depends on
 - ◆ Driver start and end levels (V_H , V_L)
 - ◆ Receiver threshold, V_T , which is between V_{IH} and V_{IL}
 - ◆ Driver output resistance (R_O)
 - ◆ Equivalent receiver input capacitance (C_I)
- **Skew time, t_K**
 - ◆ Variations of t_{TX}
 - ◆ Linked to the variations of the parameters that determine t_{TX}

RC model of interconnection

- Interconnection modeled with an RC cell
 - ◆ Same models for drivers and receivers, with R_O , R_I , C_I
 - ◆ Interconnection with R series, R_S , and C parallel, C_P



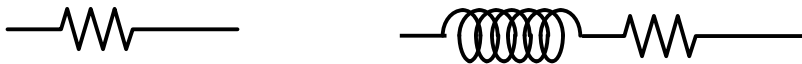
- Behavior
 - ◆ First order low pass cell
 - ◆ Exponential step response
- Objective: determine the evolution in time of V_B and V_C

Lumped parameter models

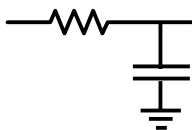
- DC analysis: equipotential conductors



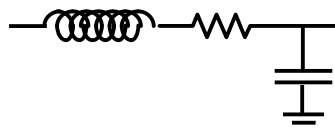
- Real conductors have resistance and inductance



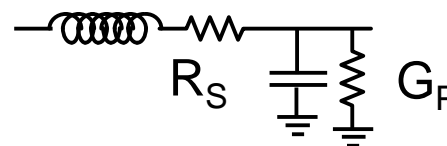
- There are parasitic capacitances and leakage resistances towards ground



R-C



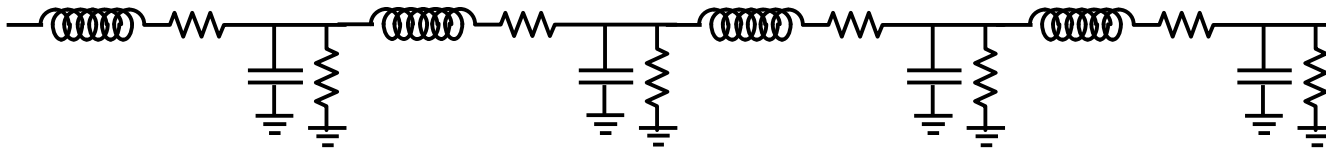
R-L-C



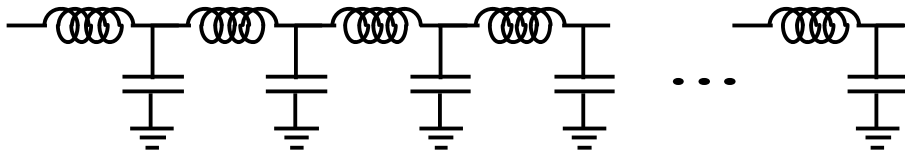
G_P - R_S -L-C

Other lumped parameter models

- R, L, and C are **distributed** along the entire conductor



- If R_S and G_P are zero \rightarrow connection **without losses**

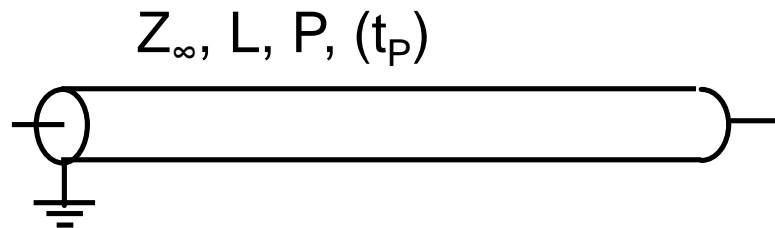


- Increasing the number of cells, we obtain a **transmission line** (without losses)

Transmission line

- Parameters of a transmission line

- ◆ Z_{∞} : characteristic impedance
- ◆ L : length
- ◆ P : propagation speed
- ◆ t_p : propagation time



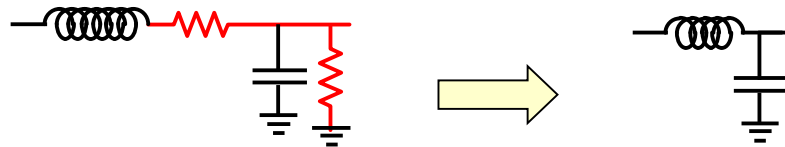
- In steady state (**dc**) it is a **direct link** (single node) for a lossless line

Examples of transmission lines

- Transmission lines **without losses**

- ◆ R series are null → perfect conductor
- ◆ Parallel G are null → perfect insulator

- ◆ Base cell



- Can be considered lossless lines

- ◆ Printed circuit (PCB) tracks
- ◆ Cables (coaxial, flat cables, twisted pair, ...)

- Are considered lines **with losses** (not covered here)

- ◆ Connections within the integrated circuits
 R_S, G_P not zero → losses!



Lossless line parameters

- Physical parameters (dimensions and materials)

- ◆ L_U : unitary inductance
- ◆ C_U : unitary capacitance
- ◆ L : length

- Electrical parameters

- ◆ Z_∞ : characteristic impedance
(typical range: 10 Ω ... 1000 Ω)
- ◆ P : propagation speed
(0.6–0.8 $c \rightarrow$ 18–24 cm/ns)
- ◆ Propagation time $t_p = L / P$
 - Time needed by the electrical signal to move along the conductor

$$Z_\infty = \sqrt{\frac{L_U}{C_U}}$$
$$P = \frac{1}{\sqrt{L_U C_U}}$$



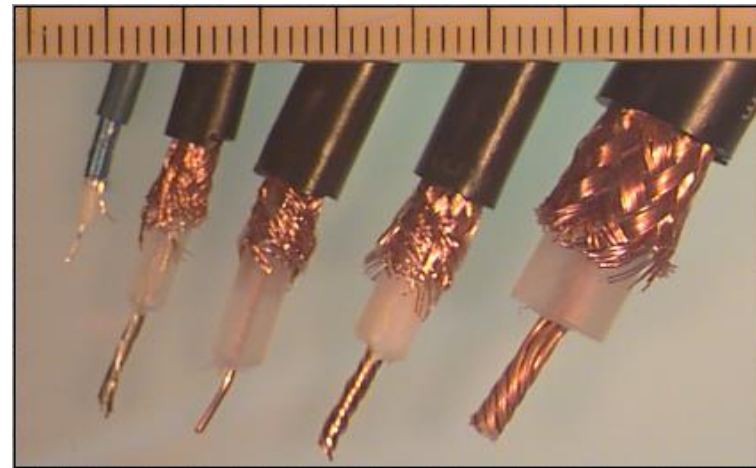
Transmission line models

- The transmission line model is **more accurate** than R L C models
- Use the line model when the conductor **cannot** be considered **equipotential**, i.e.
 - ◆ Transition times (rise/fall, t_R/t_F) are much smaller than the propagation time, t_p
 - Typical $P = 18\text{--}24$ cm/ns, hence for $L = 10$ cm $\rightarrow t_p = 0.4\text{--}0.6$ ns
 - ◆ **Long links** & **signals** with **fast** transitions
 - Matters the **steepness of the fronts**, not the frequency
- In the following we use only **simplified models** (no losses)

Various types of cables/lines

Coaxial cables

- $Z_{\infty} \rightarrow 47 \dots 100 \Omega$



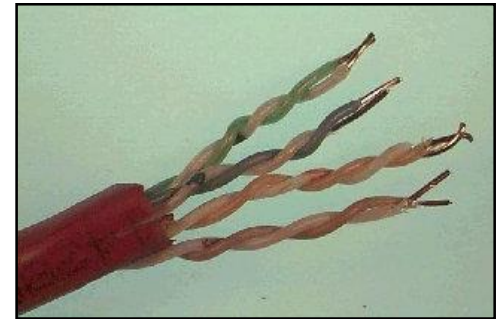
Flat cables

- $Z_{\infty} \rightarrow 100 \dots 1000 \Omega$



Twisted pair

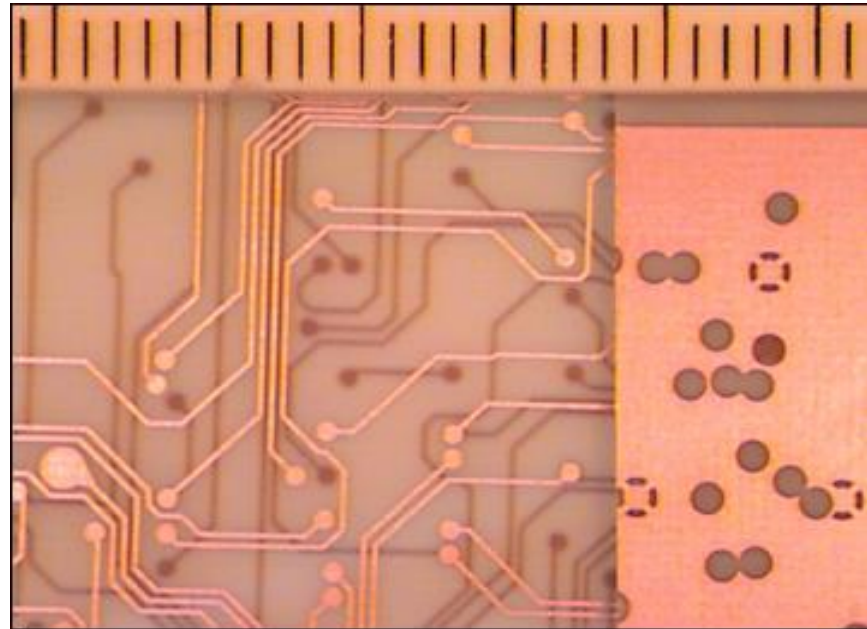
- $Z_{\infty} \rightarrow 100 \dots 600 \Omega$



- Speed $P = 0.6 - 0.8 c$ (18–24 cm/ns)

Tracks / lines on printed circuit

- PCB tracks, with ground planes
- Characteristic impedance
 $Z_{\infty} \rightarrow 10 \dots 300 \, \Omega$
- Propagation speed
 $P = 0.6 - 0.8 \, c$
(18–24 cm/ns)



What influences the parameters

- Z_{∞} and P depend on C and L
- C and L depend on physical characteristics (dimensions, materials, ...)
- Narrow tracks (small W)
 - ◆ L increases ($L_U \propto \ln(1 / W)$)
 - ◆ C decreases ($C_U \propto 1 / \ln(1 / W)$)
 - Z_{∞} increases
- Wide tracks (large W)
 - ◆ L decreases, C increases
 - Z_{∞} decreases
 - ◆ Same effect if adding capacitance to inputs/outputs

$$Z_{\infty} = \sqrt{\frac{L_U}{C_U}}$$
$$P = \frac{1}{\sqrt{L_U C_U}}$$



Lecture C2: Transmission Line Models

- Propagation of digital signals
- Transmission line models
- Reflections
- Driving conditions
- Transmission time t_{TX}
- Skew t_K

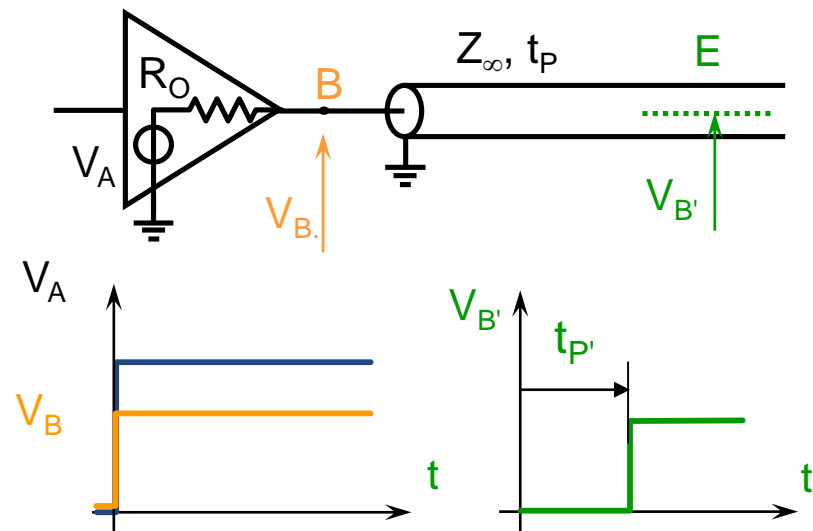
Line driven with voltage step

- Digital signal ($0 \rightarrow 1$): voltage step $0 \text{ V} \rightarrow V_A$
- Linear model for driver, lossless line
 - ◆ The step $V_B(0)$ on the beginning of the line is given by the partition of V_A on R_O and Z_∞

$$V_B(0) = \frac{Z_\infty}{R_O + Z_\infty} V_A$$

- The **first step**

- ◆ Moves along the conductor without distortions
- ◆ Needs $t = t_p$, to move between two points of the line



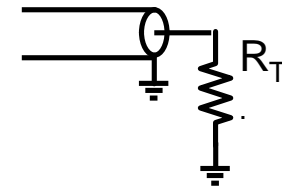


Incident wave and reflected wave

- The step propagates along the line, from the generator to the load, from left to right:
 - ◆ wave **PROGRESSIVE or INCIDENT** (V_{P1})
- At any point on the line
 - ◆ $V(t) / I(t) = Z_{\infty} \rightarrow$ if Z_{∞} is constant, V and I do not change
- Conductor discontinuity and loads
 - ◆ If Z_{∞} varies ($Z_{\infty 1} \rightarrow Z_{\infty 2}$), V and I change to match $V / I = Z_{\infty 2}$
 - ◆ The variations generate a **reflected (regressive)** wave, which travels back, from right to left
 - ◆ The reflected wave behaves like the incident wave (can have further reflections, ...)

At termination

- Line **terminated on R_T** (remote side)
 - ◆ At the ends of R_T , $V / I = R_T$
- The step reaches the termination at t_p
 - ◆ t_p is the propagation time or flight time
 - ◆ It depends on P (speed) and L (length)
- If $R_T = Z_\infty$, V / I does not change (no discontinuity)
 - ◆ The termination absorbs all the progressive wave energy
 - ◆ No reflected waves
- If **$R_T \neq Z_\infty$** , V / I **must change**
 - ◆ R_T **does not absorb** all the progressive wave energy
 - ◆ Generates a reflected wave moving towards the driver



Reflection coefficient (Γ)

- Is defined the reflection coefficient Γ_T

$$\Gamma_T = \frac{R_T - Z_\infty}{R_T + Z_\infty}$$

- An incident (progressive) wave V_P determines at the termination R_T a reflected wave V_R of amplitude
 - $V_R = \Gamma_T V_P$
- In general, the wave reflected by an impedance discontinuity from Z_∞ to Z_1 has an amplitude V_R :
 - $V_R = \Gamma_1 V_P$, with $\Gamma_1 = (Z_1 - Z_\infty) / (Z_1 + Z_\infty)$
- The total voltage at any point on the line is
 - Algebraic sum of the incident wave and the reflected wave



Values of the reflection coefficient

- Closed line on $R_T = Z_\infty$ ($\Gamma_T = 0$)

- ◆ No discontinuity, hence no reflected waves

- ◆ All incident energy is dissipated on the termination resistor

$$\Gamma_T = \frac{R_T - Z_\infty}{R_T + Z_\infty}$$

- Line open: $R_T \rightarrow \infty$ ($\Gamma_T = 1$)

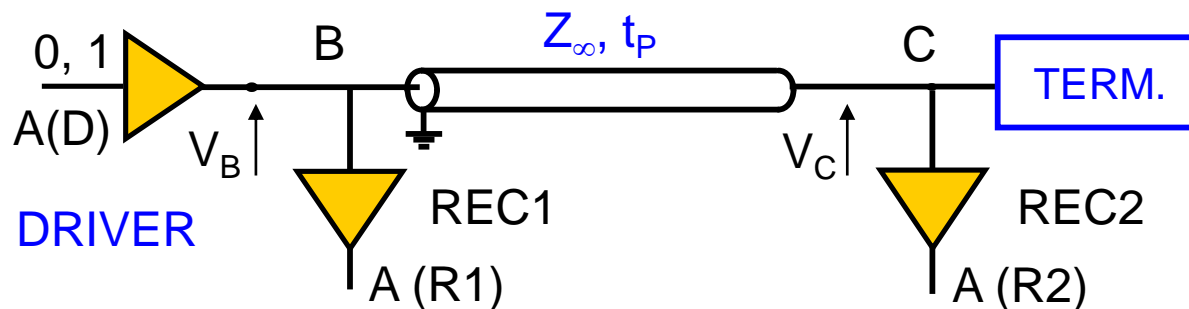
- ◆ Null total current, hence reflected wave with $I_R = -I_I$
- ◆ Voltage of reflected wave equal to the incident one
- ◆ Total voltage at termination doubles

- Line shorted: $R_T = 0 \Omega$ ($\Gamma_T = -1$)

- ◆ Null total voltage at termination
- ◆ Reflected wave voltage $V_R = -V_I$

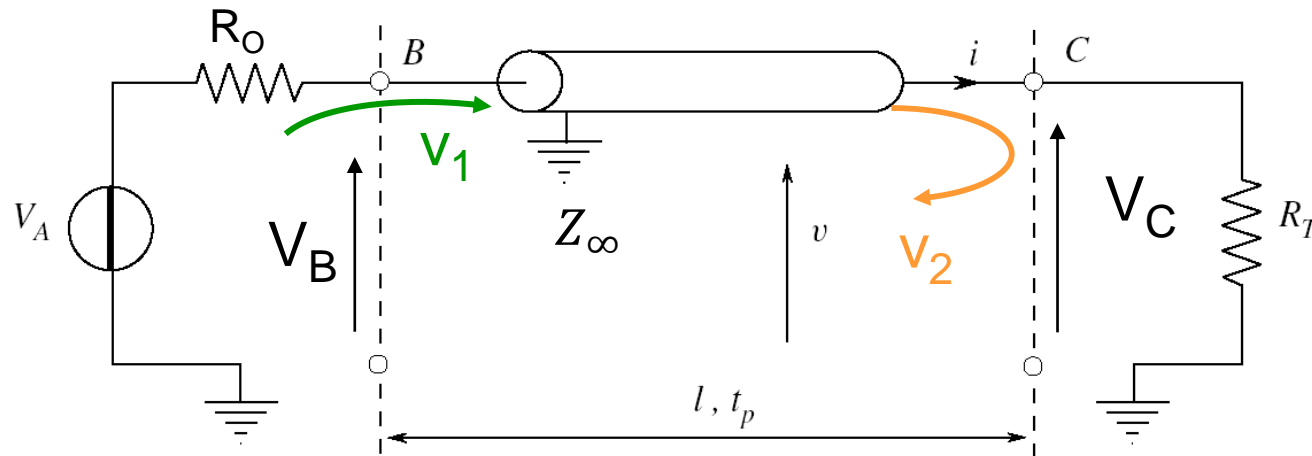
Reference structure

- Driver circuit at far left (near-end)
- Line transmission with parameters Z_{∞} , t_p
- A termination on far right (far-end)
- Receivers in any position
 - ◆ at the driver (near end)
 - ◆ at the termination (far end)
 - ◆ in-between



Complete equivalent circuit

- The voltage step $V_B(0)$ on the line is the partition of V_A on R_O and Z_∞ , and creates the incident wave, v_1
- At the termination R_T , is generated a reflected wave, v_2



$$V_B(0) = \frac{Z_\infty}{R_O + Z_\infty} V_A = v_1$$

$$v_2 = \frac{R_T - Z_\infty}{R_T + Z_\infty} v_1 = \Gamma_T v_1$$

$$V_C = v_1 + v_2$$

First step and first reflection

- The voltage step $V_B(0)$ propagates along the line as **incident wave v_1**
- v_1 arrives at termination R_T after the propagation time t_p
- At the termination R_T , v_1 generates a **reflected wave**, v_2
- The **reflected wave amplitude**, v_2 , depends on Γ_T

$$v_2 = \frac{R_T - Z_\infty}{R_T + Z_\infty} v_1 = \Gamma_T v_1$$

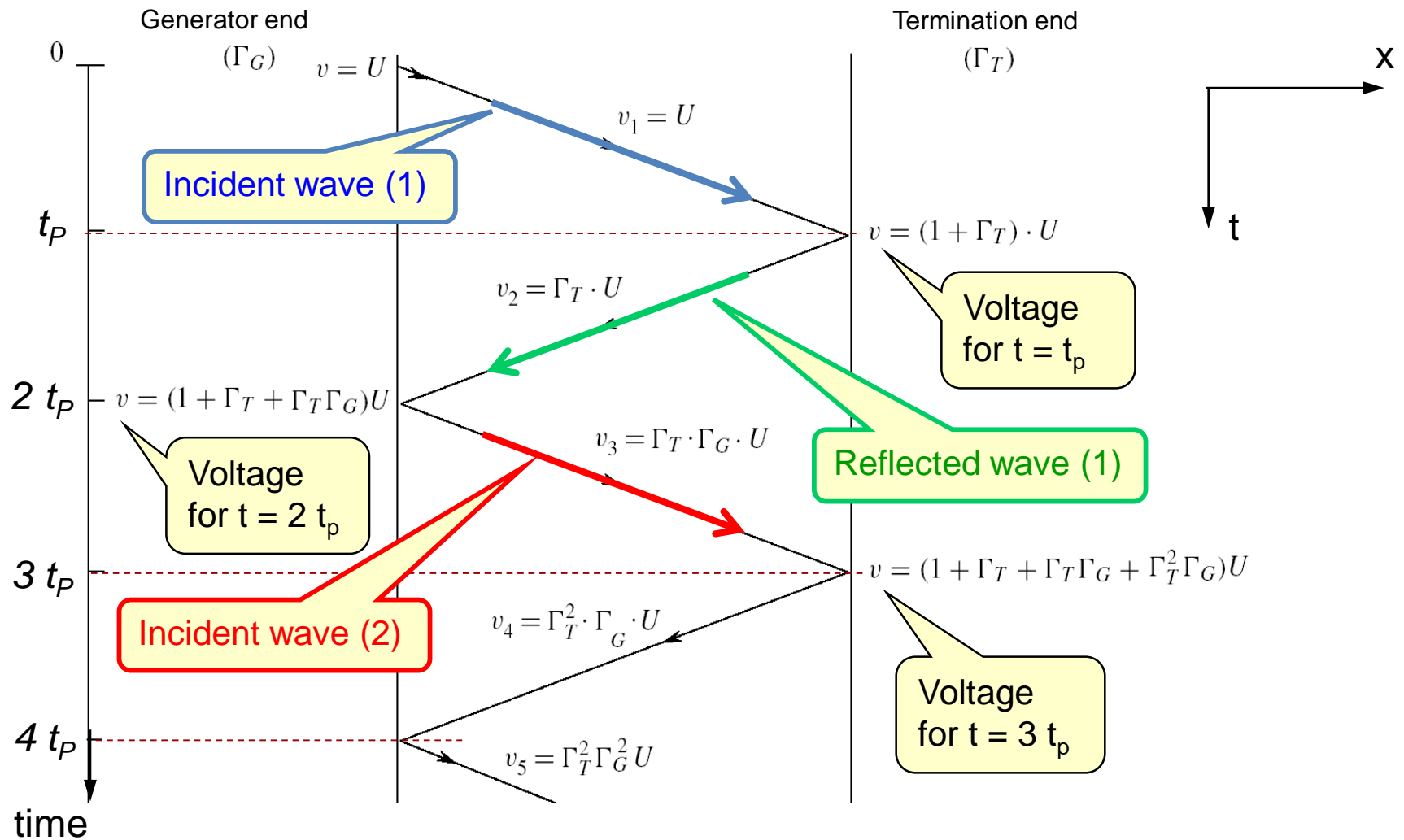
- The reflected wave v_2 propagates towards the driver
- The termination voltage, V_C , is the algebraic sum $v_1 + v_2$
 - ◆ For $t < t_p \rightarrow V_C = 0$
 - ◆ For $t > t_p \rightarrow V_C = v_1 + v_2$



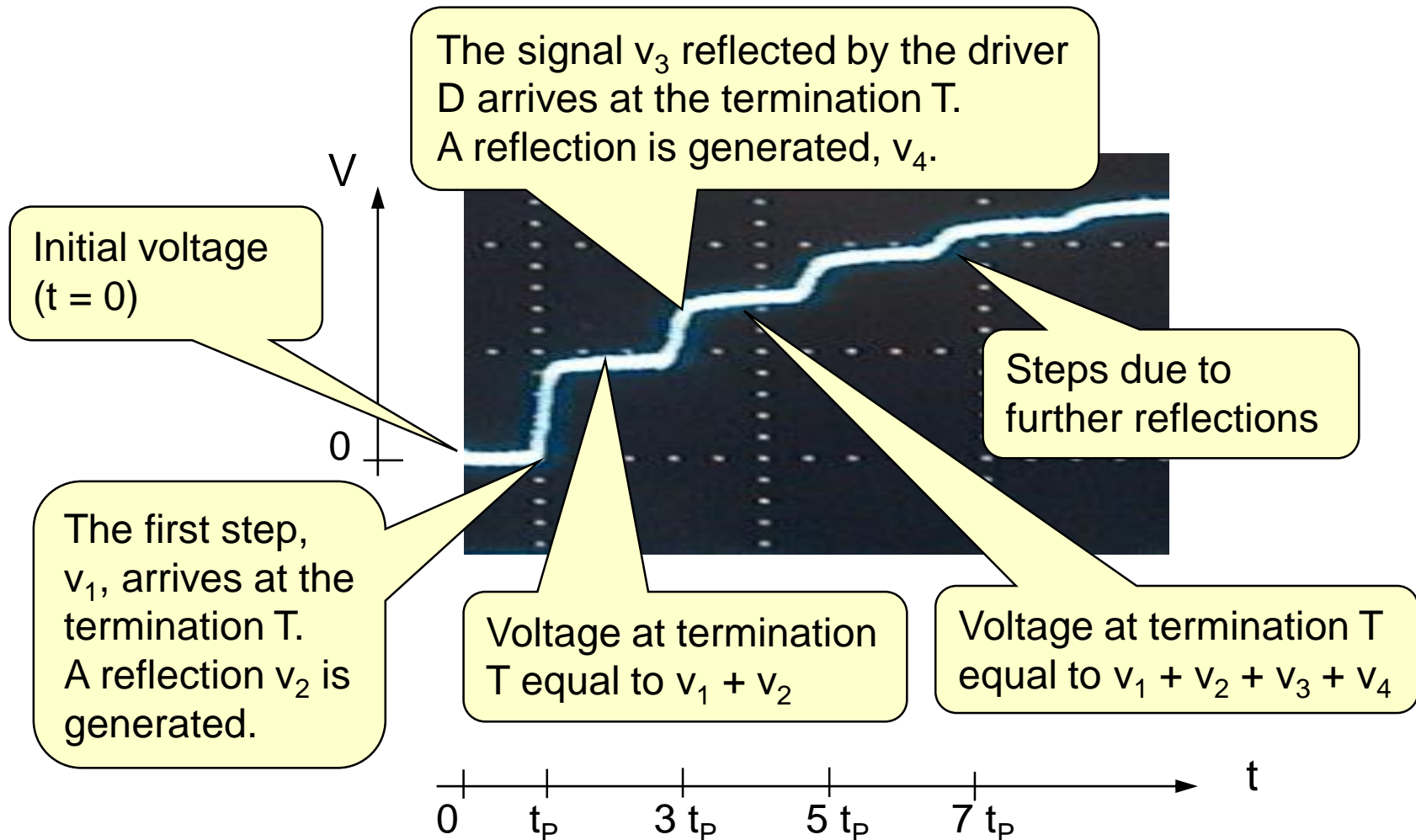
How to represent $V(x, t)$ on the line

- **Time evolution** of the signal $V(t)$ for $x = x_0$
 - ◆ The voltage varies when the initial step and subsequent reflections pass through the observation point
 - ◆ **Lattice diagram**
- Distribution of $V(x)$ along the line at $t = t_0$
(\approx still picture of the voltage along the line)
 - ◆ The incident wave moves from generator to termination
 - ◆ Any reflected wave moves in the opposite direction
 - ◆ Few information, scarcely used
- Time distribution of $V(x)$ along the line
 - ◆ **$V(x, t)$ diagrams** three-dimensional axes: V, x, t

V(t) in various x on the line: lattice diagram



$V(t)$ at the termination T



x/t view of the signal on a line

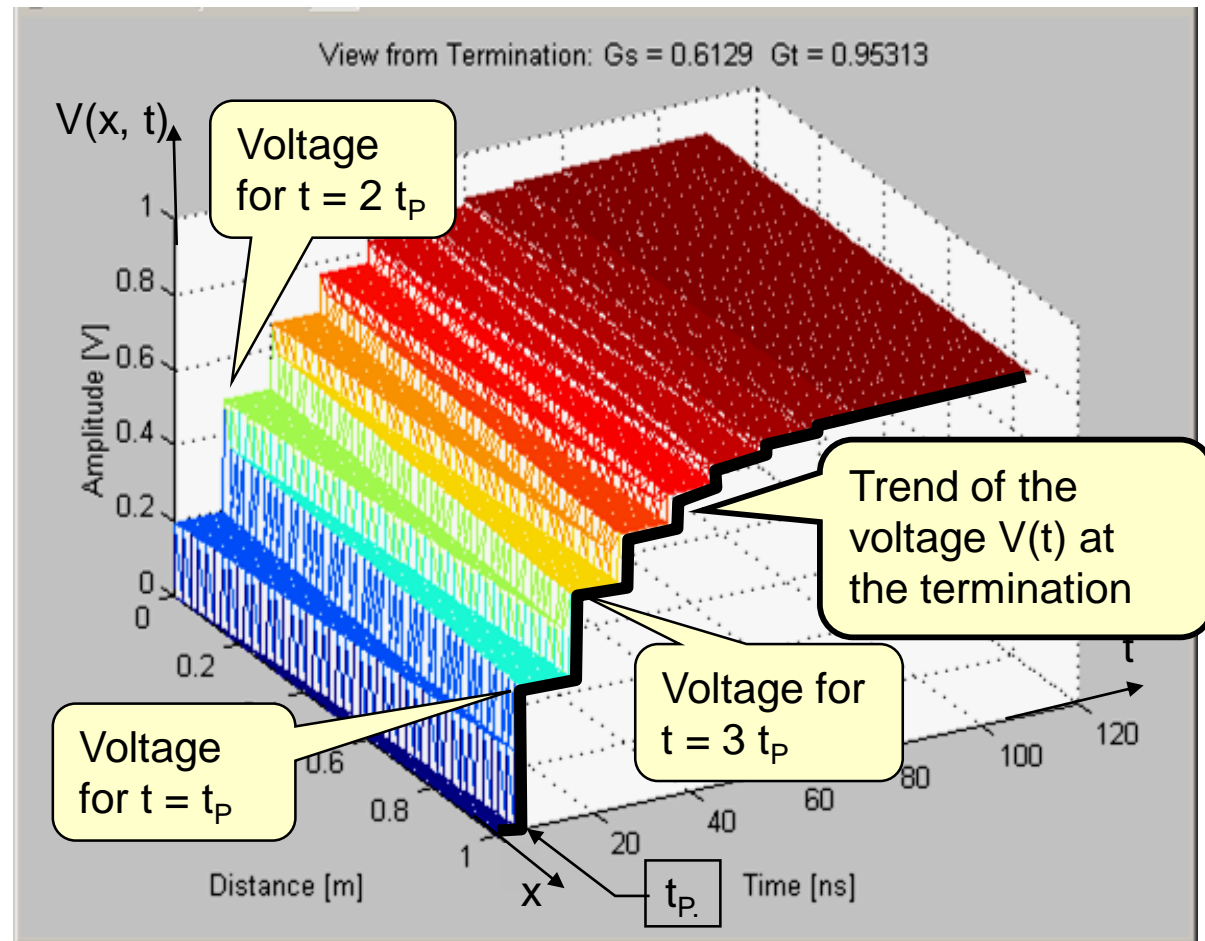
$V(t, x)$ on a transmission line driven by a voltage step:

$$\Gamma_T > 0$$

$$\Gamma_G > 0$$

All steps (direct and reflected) have the same polarity.

At each point of the line there is a monotonous staircase.



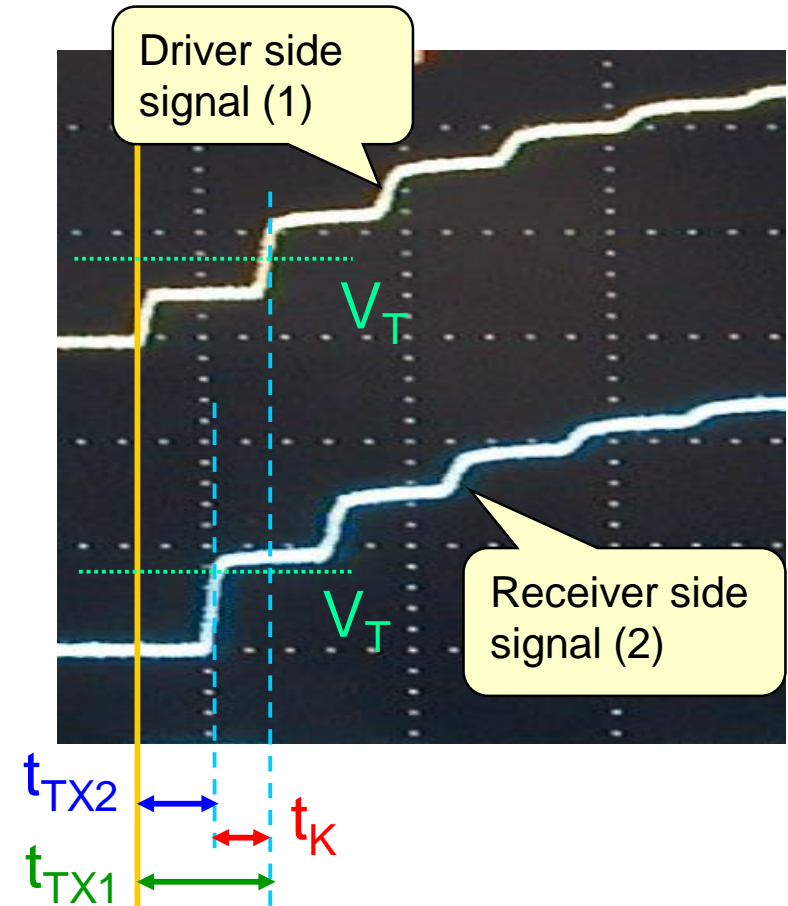


Signal at extremes $V(t)$

- The signal is obtained by incrementally adding the contributions of the incident and the reflected waves
 - ◆ Driver side: discontinuity at $0, 2 t_p, 4 t_p, \dots$
 - Step propagation
 - Arrival of the waves as they are reflected (right \rightarrow left)
 - ◆ Termination side: discontinuity at $t_p, 3 t_p, 5 t_p, \dots$
 - Arrival of the step
 - Arrival of the subsequent incident waves (left \rightarrow right)
 - ◆ Intermediate points: double the number of discontinuities
 - Incident and reflected waves transit at different times
- Steady state: equipotential line (if without losses)

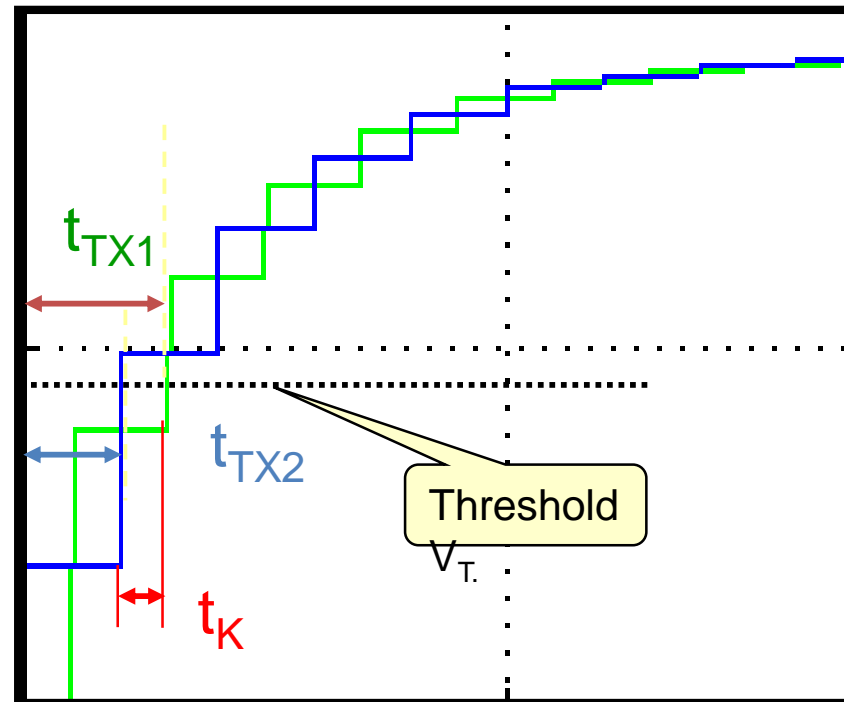
Transmission time and skew

- Same parameters t_{TX} and t_K of the RC model
- **Delay** for crossing the **threshold V_T** is the **transmission time, t_{TX}**
- t_{TX} depends on
 - ◆ Driver and receiver parameters
 - ◆ Parameters of the interconnexion
 - ◆ Operating conditions (reflexions)
 - ◆ **Position**
- t_{TX} variations cause **skew, t_K**



Overall trend of V_B and V_C

- Example of voltage trend on the driver side and on the termination side
 - ◆ Γ is positive at both ends
 - ◆ All reflected waves have the same sign
 - ◆ Monotonous interlaced voltage steps
 - ◆ Different voltages at line ends
 - ◆ Voltages equal in the steady state ($t \rightarrow \infty$, dc)





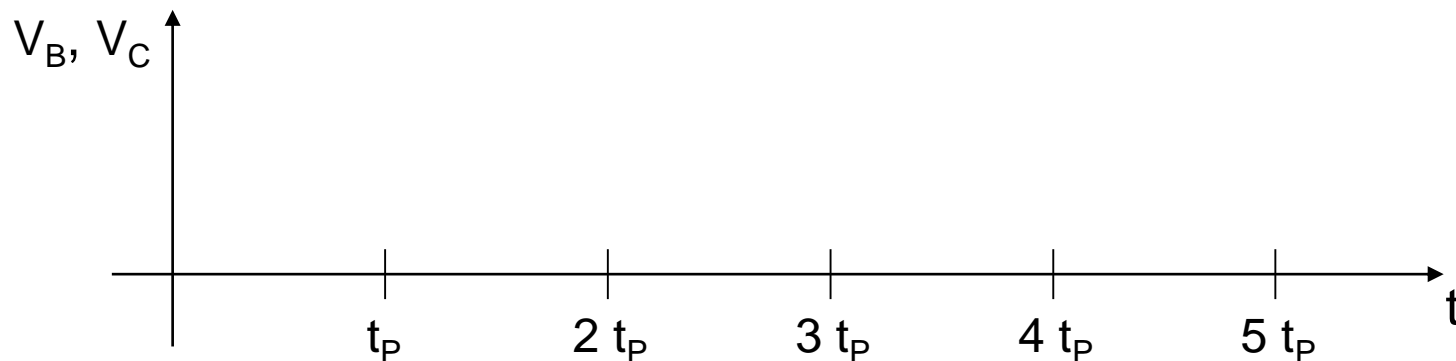
Exercise C2.1: reflections

- A step signal is applied to a line terminated on an open circuit with:
 - ◆ Driver: $R_O = 160 \, \Omega$, 5 V power supply
 - ◆ Line: $Z_\infty = 80 \, \Omega$, $t_p = 10 \, \text{ns}$
- Plot the time evolution of the signals on the driver and termination ends.

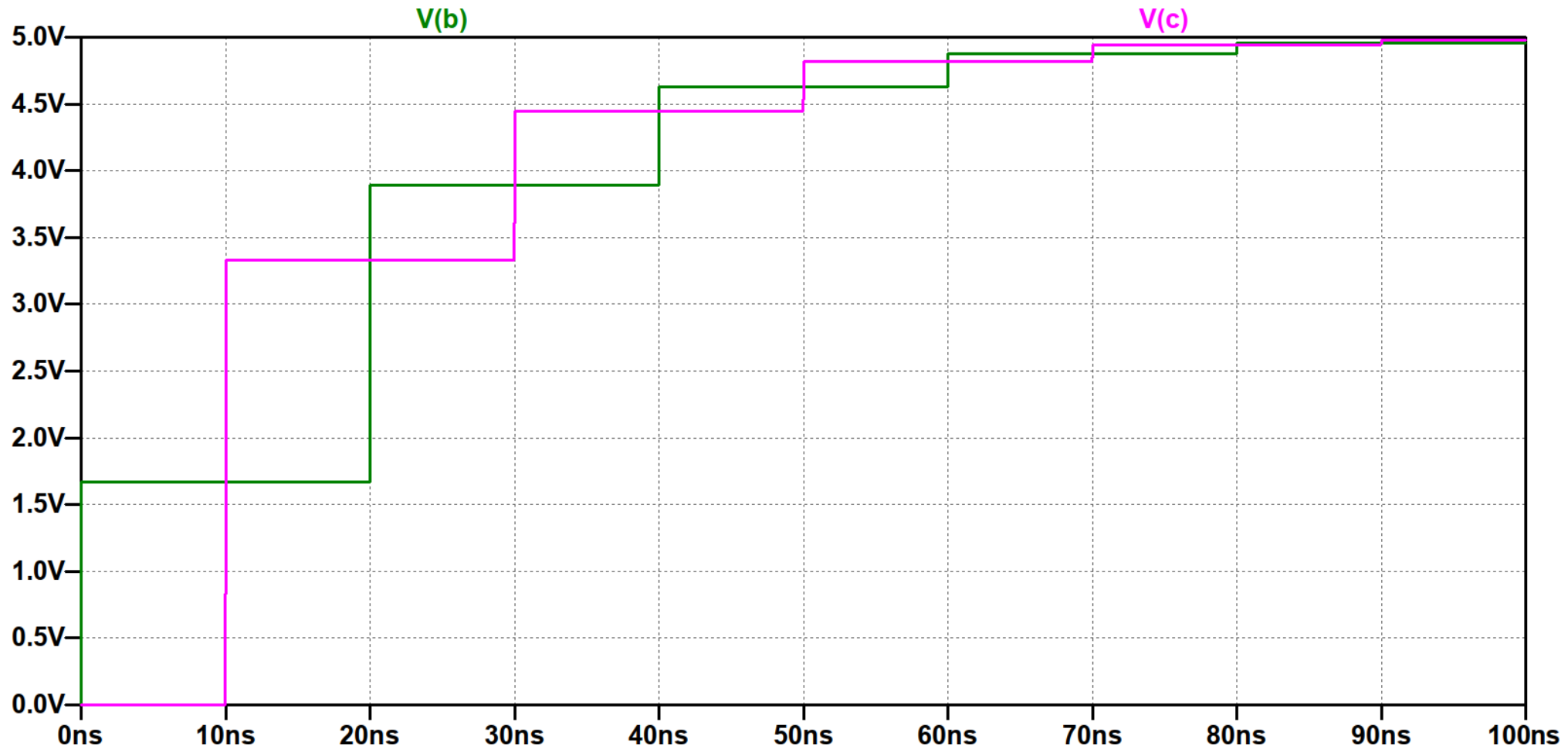


Exercise C2.1a: reflections

- Reflection coefficients:
- First step width:
- Time evolution:



Exercise C2.1a: reflections

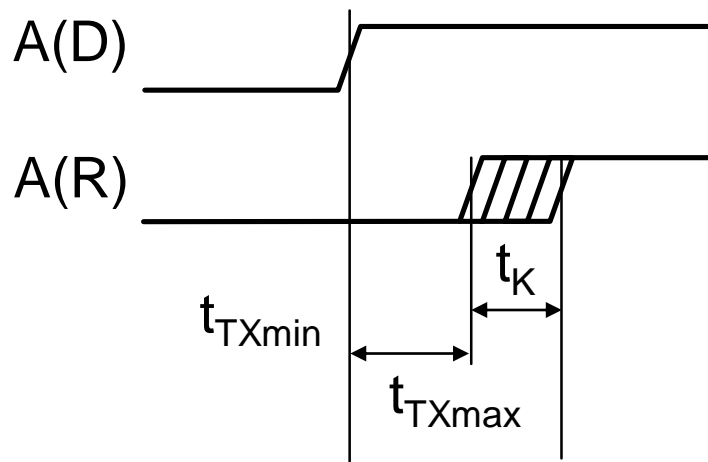
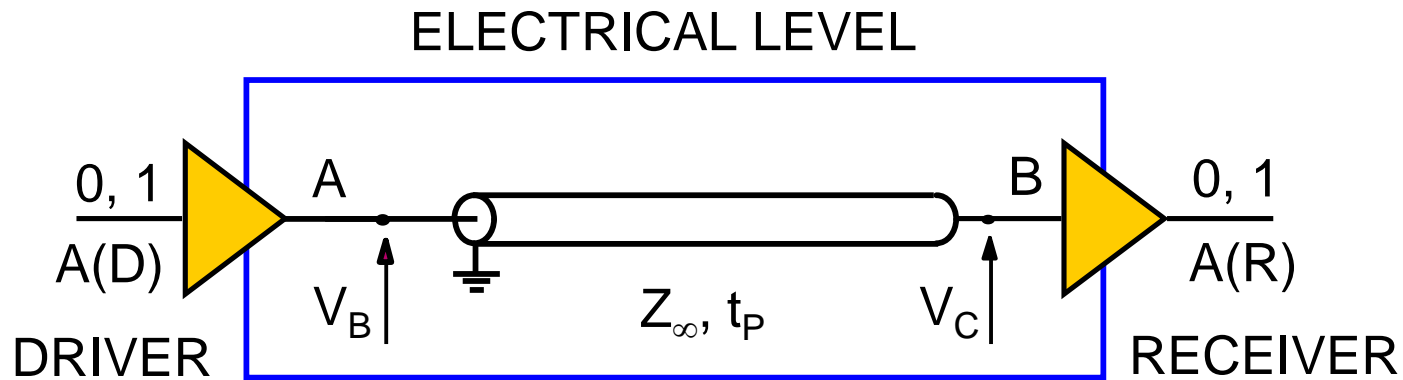




Effects of propagation summary

- The voltage variation propagates from one end to the other in the **propagation time t_p**
- The receiver recognizes logic state changes when the signal crosses its input threshold V_{TH} . May happen after multiple signal reflections, and introduces a **transmission time, t_{TX}** , delay between signal generation and detection at the receiver
- This delay can have a variation **t_K (skew)** due to variations in electrical and physical parameters
- The delays t_{TX} and t_K depend on the electrical (driver, receiver) and physical (line) characteristics

Summary of the parameters



t_{TX} → transmission time
 t_{TXmax} → transmission time max
 t_{TXmin} → transmission time min

$$t_K = t_{TXmax} - t_{TXmin} \rightarrow \text{SKEW}$$

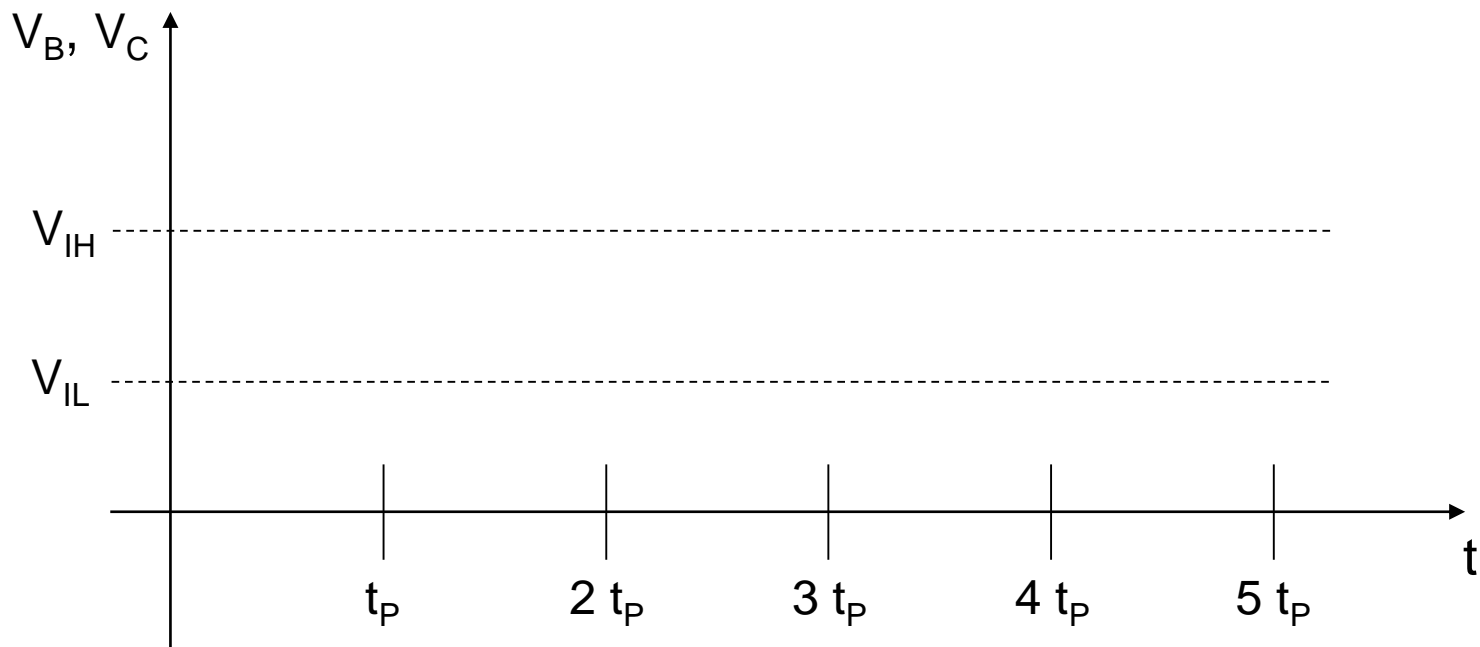


Exercise C2.2: propagation and skew

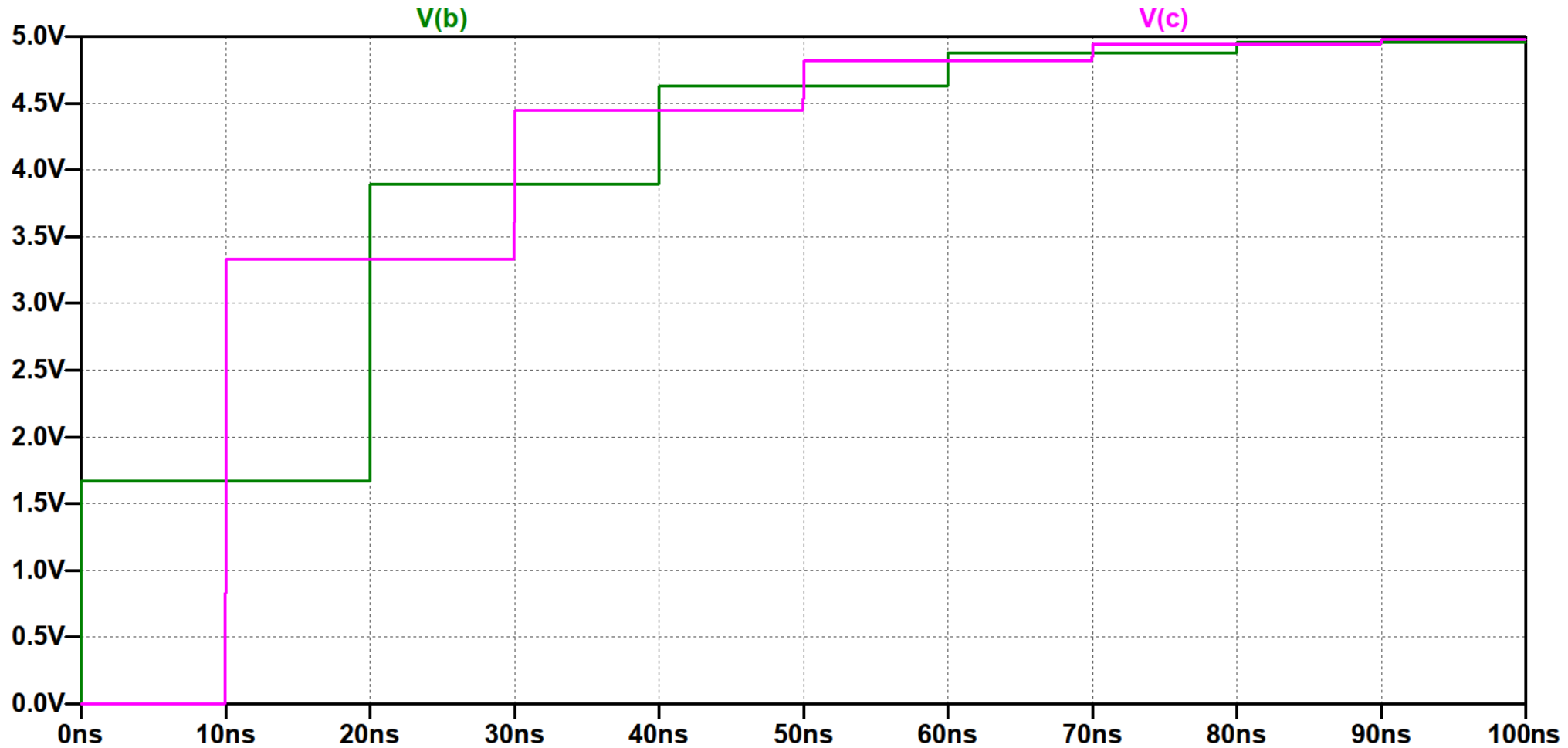
- Connect two receivers to the system of exercise C2.1, one at the output of the driver, and one at the end of the line, with
 - ◆ $V_{IL} = 1 \text{ V}$, $V_{IH} = 3 \text{ V}$
- Evaluate
 - ◆ Transmission time t_{TX}
 - ◆ Skew t_K

Exercise C2.2a: propagation and skew

- Use the time evolution from exercise C2.1
- Mark the crossing of the thresholds



Exercise C2.2a: propagation and skew





Lecture C2 – final check

- Define the transmission time and skew and indicate which parameters they depend on.
- How propagation time, t_p , and transmission time, t_{TX} , differ for an interconnection over a transmission line?
- Value of the reflection coefficient for terminations
 - ◆ Open circuit, short circuit, $R_{T1} = Z_\infty / 2$, $R_{T2} = 2 Z_\infty$
- The steady state voltage on a lossless transmission line depends on Z_∞ ?
- First voltage step on a lossless line depends on R_T ?
- How could we measure the characteristic impedance Z_∞ of a transmission line?