Tunnel Strength

Filippo Gatti, Ph.D. filippo.gatti@centralesupelec.fr Lab.MSSMat UMR CNRS 8579 CentraleSupélec 27 septembre 2020

CentraleSupélec

Outline



• Algebra Recap

• Recap Lecture 4 Linear Elasticity

Hands on session4.2 Tunnel strength

Algebra Recap

Some algebra



Tensor/Vector product

• Scalar product:

$$\underline{\underline{a}}, \underline{\underline{b}} \in \mathbb{R}^a \qquad \langle \underline{\underline{a}}, \underline{\underline{b}} \rangle = \sum_{m=1}^a a_m b_m$$

· Tensors and tensor product:

$$\underline{\underline{A}} \in \mathbb{R}^a \to \mathbb{R}^b$$
 $\underline{\underline{A}} = \underline{\underline{a}} \otimes \underline{\underline{b}}, \underline{\underline{a}} \in \mathbb{R}^a, \underline{\underline{b}} \in \mathbb{R}^b$

• Tensor application to vector:

$$\underline{\underline{A}} = \underline{a} \otimes \underline{b} \in \mathbb{R}^a \to \mathbb{R}^b, \underline{c} \in \mathbb{R}^b \qquad \underline{\underline{A}}.\underline{c} = \underline{a} \langle \underline{b},\underline{c} \rangle$$

Tensor/Tensor product :

$$\underline{\underline{A}} = \underline{a} \otimes \underline{b} \in \mathbb{R}^a \to \mathbb{R}^b, \underline{\underline{B}} = \underline{c} \otimes \underline{d} \in \mathbb{R}^b \otimes \mathbb{R}^c \qquad \underline{\underline{A}} \cdot \underline{\underline{B}} = \underline{a} \otimes \underline{d} \langle \underline{b}, \underline{c} \rangle$$

Some algebra (cont'd)



Tensor/Vector product

Vector gradient :

$$\underline{\underline{a}} \in \mathbb{R}^a \quad \underline{\underline{\mathbb{D}}_{\underline{x}}\underline{a}} = \sum_{m=1}^a \frac{\partial \underline{\underline{a}}}{\partial x_m} \otimes \underline{\underline{e}}_m$$

· Vector divergence:

$$\underline{\boldsymbol{a}} \in \mathbb{R}^{a} \quad div_{x} \left(\underline{\boldsymbol{a}}\right) = Tr\left(\underline{\mathbb{D}_{x}\boldsymbol{a}}\right) = \left\langle \underline{\boldsymbol{\nabla}}_{x}, \underline{\boldsymbol{a}} \right\rangle = \sum_{m=1}^{a} \frac{\partial a_{m}}{\partial x_{m}}$$

· Tensor divergence :

$$\underline{\underline{A}} \in \mathbb{R}^a \to \mathbb{R}^b \quad div_X \left(\underline{\underline{A}}\right) = \sum_{m=1}^b \frac{\partial \underline{\underline{A}}}{\partial x_m} \underline{\underline{e}}_m$$



Tensor/Vector product in cylindrical coordinates

• Vector gradient :

$$\underline{\underline{a}} \in \mathbb{R}^{3} \quad \underline{\underline{\mathbb{D}}_{\underline{x}}\underline{a}} = \frac{\partial \underline{a}}{\partial r} \otimes \underline{i}_{r} (\theta) + \frac{\partial \underline{a}}{\partial \theta} \otimes \frac{\underline{i}_{\theta}}{r} (\theta) + \frac{\partial \underline{a}}{\partial z} \otimes \underline{i}_{z}$$

Vector divergence :

$$\underline{\boldsymbol{a}} \in \mathbb{R}^{3} \quad div_{x} \left(\underline{\boldsymbol{a}}\right) = Tr\left(\underline{\underline{\mathbb{D}_{x}\boldsymbol{a}}}\right) = \left\langle \underline{\boldsymbol{\nabla}}_{x},\underline{\boldsymbol{a}}\right\rangle = \left\langle \frac{\partial\underline{\boldsymbol{a}}}{\partial r},\underline{\boldsymbol{i}}_{r}\right\rangle + \left\langle \frac{\partial\underline{\boldsymbol{a}}}{\partial \theta},\frac{\underline{\boldsymbol{i}}_{\theta}}{r}\right\rangle + \left\langle \frac{\partial\underline{\boldsymbol{a}}}{\partial z},\underline{\boldsymbol{i}}_{z}\right\rangle$$

· Tensor divergence:

$$\underline{\underline{A}} \in \mathbb{R}^{3} \to \mathbb{R}^{3} \quad div_{x} \left(\underline{\underline{A}}\right) = \frac{\partial \underline{\underline{A}}}{\partial r} \underline{i}_{r} \left(\theta\right) + \frac{\partial \underline{\underline{A}}}{\partial \theta} \cdot \frac{\underline{i}_{\theta}}{r} + \frac{\partial \underline{\underline{A}}}{\partial z} \underline{i}_{z}$$

Linear Elasticity



$$\underline{\underline{\sigma}}\left(\underline{\boldsymbol{x}};t\right) = \mathcal{F}\left(\underline{\underline{\varepsilon}}^{el}\left(\underline{\boldsymbol{x}};t\right)\right)$$



(2)

$$\underline{\underline{\sigma}}\left(\underline{\boldsymbol{x}};t\right) = \mathcal{F}\left(\underline{\underline{\varepsilon}}^{el}\left(\underline{\boldsymbol{x}};t\right)\right)$$

- Linearity $\to g\left(\alpha\underline{\underline{\varepsilon}}_1^{el} + \beta\underline{\underline{\varepsilon}}_2^{el}\right) = \alpha\mathcal{F}\left(\underline{\underline{\varepsilon}}_1^{el}\right) + \beta\mathcal{F}\left(\underline{\underline{\varepsilon}}_2^{el}\right)$:
 - Stiffness:

$$\underline{\underline{\sigma}}(\underline{x};t) = \mathbf{D}^{el}(\underline{x}) : \underline{\underline{\varepsilon}}^{el}(\underline{x};t)$$
 (1)

Compliance :

 $\varepsilon^{el} = \mathbf{C}^{el}(x) : \sigma(x;t)$

$$\mathbf{A}: 4^{th}$$
-order tensor (real symmetric)

$$\mathbf{A} = \underline{\underline{A}}_l \otimes \underline{\underline{A}}_r, \quad \mathbf{A} : \underline{\underline{B}} = \underline{\underline{A}}_l Tr \left(\underline{\underline{A}}_r^T \underline{\underline{B}}\right)$$

$$\underline{\underline{\sigma}}\left(\underline{x};t\right) = \mathcal{F}\left(\underline{\underline{\varepsilon}}^{el}\left(\underline{x};t\right)\right)$$

- Isotropic $\{\mathbf{I}, \underline{\underline{I}} \otimes \underline{\underline{I}}\}$:
 - Stiffness:

$$\underline{\underline{\sigma}}\left(\underline{\boldsymbol{x}};t\right) = \lambda\left(\underline{\boldsymbol{x}}\right) Tr\left(\underline{\underline{\varepsilon}}^{el}\left(\underline{\boldsymbol{x}};t\right)\right) \underline{\underline{\boldsymbol{I}}} + 2\mu\left(\underline{\boldsymbol{x}}\right) \underline{\underline{\varepsilon}}^{el}\left(\underline{\boldsymbol{x}};t\right)$$

$$\mathbf{D}^{el}(x) = \lambda(x) \underline{I} \otimes \underline{I} + 2\mu(x) \underline{I}$$

 $\mathbf{I} = \sum_{i=1}^{3} \underline{\boldsymbol{e}}_{i} \otimes \underline{\boldsymbol{e}}_{i} \otimes \underline{\boldsymbol{e}}_{i} \otimes \underline{\boldsymbol{e}}_{i}$

Filippo Gatti

$$\underline{\underline{\varepsilon}}^{el}\left(\underline{\boldsymbol{x}};t\right) = \frac{1+\nu\left(\underline{\boldsymbol{x}}\right)}{F\left(\boldsymbol{x}\right)}Tr\left(\underline{\underline{\sigma}}\left(\underline{\boldsymbol{x}};t\right)\right)\underline{\boldsymbol{I}} - \frac{\nu\left(\underline{\boldsymbol{x}}\right)}{F\left(\boldsymbol{x}\right)}\underline{\underline{\sigma}}\left(\underline{\boldsymbol{x}};t\right)$$

$$\mathbf{C}^{el}(\underline{x}) = \frac{1 + \nu(\underline{x})}{F(x)} \underline{\underline{I}} \otimes \underline{\underline{I}} - \frac{\nu(\underline{x})}{F(x)} \mathbf{I}$$

$$\frac{\mathbf{x}}{\mathbf{x}} = \frac{\mathbf{x}}{\mathbf{x}} = \frac{\mathbf{x}}{\mathbf{x}$$

$$v\left(\underline{x}\right)$$

$$(\underline{x};t)$$
 (5)

CentraleSupélec

(3)

(4)

(6)

$$\underline{\underline{\sigma}}\left(\underline{x};t\right) = \mathcal{F}\left(\underline{\underline{\varepsilon}}^{el}\left(\underline{x};t\right)\right)$$

- Spherical and deviatoric decomposition :
 - Spherical component (pression) σ_m :

$$\sigma_{m}\left(\underline{\boldsymbol{x}};t\right) = \frac{Tr\left(\underline{\boldsymbol{\varphi}}\right)}{3} = \frac{\left(3\lambda\left(\underline{\boldsymbol{x}}\right) + 2\mu\left(\underline{\boldsymbol{x}}\right)\right)}{3}Tr\left(\underline{\boldsymbol{\varepsilon}}^{el}\left(\underline{\boldsymbol{x}};t\right)\right) = K\left(\underline{\boldsymbol{x}}\right)\boldsymbol{\varepsilon}_{vol}^{el}\left(\underline{\boldsymbol{x}};t\right)$$

Deviatoric component \underline{s}^{σ} :

 $\underline{\underline{\mathbf{x}}}^{\sigma}\left(\underline{\mathbf{x}};t\right) = \underline{\underline{\sigma}} - \sigma_{m}\underline{\underline{\mathbf{I}}} = 2\mu\left(\underline{\mathbf{x}}\right)\underline{\underline{\varepsilon}}^{el} - \frac{2}{3}\mu\left(\underline{\mathbf{x}}\right)\varepsilon_{vol}^{el}\left(\underline{\mathbf{x}};t\right) = 2\mu\left(\underline{\mathbf{x}}\right)\underline{\underline{\mathbf{e}}}^{el}\left(\underline{\mathbf{x}};t\right)$ (8)

Direct relationship spherical/deviatoric
$$\varepsilon^{el}$$
 : volumetric strain

 ε_{vol}^{el} : volumetric strain \underline{e}^{el} : deviatoric strains

$$\bar{e} = \sqrt{\frac{4}{3}J_2\left(\underline{\underline{\varepsilon}}\right)}$$
: equivalent deviatoric strain

Filippo Gatti CentraleSupélec



$$\underline{\underline{\sigma}}\left(\underline{\boldsymbol{x}};t\right) = \mathcal{F}\left(\underline{\underline{\varepsilon}}^{el}\left(\underline{\boldsymbol{x}};t\right)\right)$$

Homogeneity :

$$\mathbf{D}^{el}(\underline{x}) = \mathbf{D}^{el}, \quad \mathbf{C}^{el}(\underline{x}) = \mathbf{C}^{el}$$
 (9)

- (λ, μ) : Lamé parameters (stiffness)
- (E, v): Young's modulus and Poisson's coefficient (compliance)
- $E > 0, \mu > 0, 3\lambda + 2\mu > 0, -1 < \nu < 0.5$

$$\lambda = \frac{vE}{(1+v)(1-2v)}, \quad \mu = \frac{E}{2(1+v)}$$
 (10)



$$\underline{\underline{\sigma}}\left(\underline{\boldsymbol{x}};t\right) = \mathcal{F}\left(\underline{\underline{\varepsilon}}^{el}\left(\underline{\boldsymbol{x}};t\right)\right)$$

$$\mathbf{D}^{el} = \frac{\mathcal{E}}{(1+
u)} egin{bmatrix} rac{1-
u}{(1-2
u)} & rac{
u}{1-2
u} & rac{
u}{1-2
u} & 0 & 0 & 0 \\ rac{
u}{1-2
u} & rac{1-
u}{(1-2
u)} & rac{
u}{1-2
u} & 0 & 0 & 0 \\ rac{
u}{1-2
u} & rac{
u}{1-2
u} & rac{1-
u}{(1-2
u)} & 0 & 0 & 0 \\
rac{
u}{1-2
u} & rac{
u}{1-2
u} & rac{1-
u}{(1-2
u)} & 0 & 0 & 0 \\
0 & 0 & 0 & 1 & 0 & 0 \\
0 & 0 & 0 & 0 & 0 & 1 & 0 \\
0 & 0 & 0 & 0 & 0 & 1 & 0 \\
\end{pmatrix}$$

$$\mathbf{C}^{el} = \ rac{1}{E} egin{bmatrix} 1 & -
u & -
u & 0 & 0 & 0 & 0 \ -
u & 1 & -
u & 0 & 0 & 0 & 0 \ -
u & -
u & 1 & 0 & 0 & 0 & 0 \ 0 & 0 & 0 & 2(1+
u) & 0 & 0 & 0 \ 0 & 0 & 0 & 0 & 2(1+
u) & 0 & 0 \ 0 & 0 & 0 & 0 & 0 & 2(1+
u) \end{bmatrix}$$

Figure – Elastic tensors with (E, ν) .

4.2 Tunnel Strength

Set up



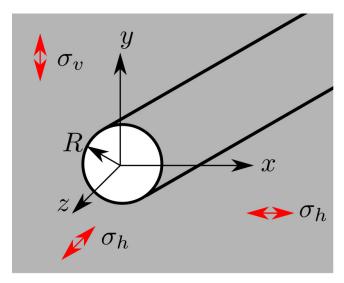


Figure – Set up [Credits : G. Puel]

10/15 Filippo Gatti

Set up



Stress description

•
$$\underline{x} = x\underline{i}_x + y\underline{i}_y + z\underline{i}_z = r\underline{i}_r + z\underline{i}_z$$
, $(r, \theta, z) \in \Omega_t =]0, R[\times]0, 2\pi[\times]0, L[$

- $x = r \cos \theta =$, $y = r \sin \theta$, $r = \sqrt{x^2 + y^2}$
- Initial stress

$$\underline{\underline{\sigma}}_0 = \sigma_h \underline{\underline{I}} + (\sigma_v - \sigma_h) \, \underline{\underline{i}}_y \otimes \underline{\underline{i}}_y, \quad \sigma_v \le \sigma_h < 0$$

•
$$\underline{f}_{v} = 0, \underline{a} = 0$$

Part I: Initial Stress



Question 1 : principal stresses $\sigma_I \ge \sigma_{II} \ge \sigma_{III}$?

$$\sigma_I = \sigma_{II} = \sigma_{xx} = \sigma_{zz} = \sigma_h, \sigma_{III} = \sigma_v$$

Question 2 : n that maximizes $||\tau_{\Sigma}||$?

•
$$\underline{\tau}_{\Sigma} = \underline{\underline{\sigma}} \cdot \underline{\underline{n}} - \sigma_{nn} \underline{\underline{n}} = \sigma_h \underline{\underline{n}} + (\sigma_v - \sigma_h) n_y \underline{\underline{i}}_y - (\sigma_h + (\sigma_v - \sigma_h) n_y^2) \underline{\underline{n}} = (\sigma_v - \sigma_h) n_y (\underline{\underline{i}}_y - n_y \underline{\underline{n}})$$

•
$$\|\underline{\tau}_{\Sigma}\| = |\sigma_v - \sigma_h| \cdot |n_y| \cdot \sqrt{1 - n_y^2} \quad (n_y \in [0, 1])$$

•
$$\tau_{\max} = \|\underline{\tau}_{\Sigma}\|_{n_{\mathcal{V}} = \pm \frac{\sqrt{2}}{2}} = \frac{|\sigma_{\mathcal{V}} - \sigma_{h}|}{2}$$
 Mohr's circle with $\alpha = \arccos n_{\mathcal{V}} = \pm \frac{\pi}{4}$

Question 3: failure criteria?

- Splitting: $\max_{\|\boldsymbol{n}\|=1} \sigma_{nn} = \sigma_I = \sigma_h \le 0 \le \sigma_R$, with $\sigma_R \ge 0$
- Maximum shear (Tresca): $\max_{\|\boldsymbol{n}\|=1} \|\underline{\tau}_{\Sigma}\| = \frac{|\sigma_{V} \sigma_{h}|}{2} \le \tau_{R}$

Part II : Auxiliary Problem



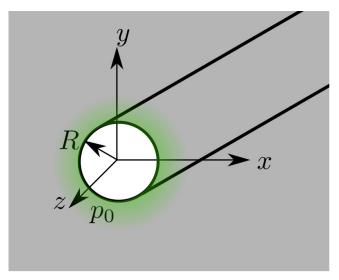


Figure - Set up [Credits : G. Puel]

13/15 Filippo Gatti

Part II: Auxiliary Problem



Auxiliary problem r > R

•
$$\boldsymbol{u}(r,\theta) = \alpha \frac{R^2}{r} \boldsymbol{i}_r(\theta), r > R$$

•
$$f_{S} = -p_0 \underline{n}, r = R$$

•
$$f_{y} = 0, \underline{a} = 0$$

Question 4/5/6/7 : verify auxiliary problem

4 Strain tensor:
$$\underline{\underline{\varepsilon}} = \underline{\underline{\mathbb{D}_{x}^{S} u}} = \frac{\partial \underline{\underline{u}}}{\partial r} \otimes \underline{\underline{i}}_{r} + \frac{\partial \underline{u}}{\partial \theta} \otimes \frac{\underline{i}_{\theta}}{r} = \alpha \left(\frac{\underline{R}}{r}\right)^{2} \left(\underline{\underline{i}}_{\theta} \otimes \underline{\underline{i}}_{\theta} - \underline{\underline{i}}_{r} \otimes \underline{\underline{i}}_{r}\right)$$

5 Stress tensor (linear elastic homogenenous isotropic):
$$\underline{\underline{\sigma}} = \lambda Tr\left(\underline{\underline{\varepsilon}}\right)\underline{\underline{I}} + 2\mu\underline{\underline{\varepsilon}} = 0 + 2\mu\alpha\left(\frac{R}{r}\right)^2\left(\underline{\underline{i}}_{\theta} \otimes \underline{\underline{i}}_{\theta} - \underline{\underline{i}}_{r} \otimes \underline{\underline{i}}_{r}\right)$$

6
$$div_{x}\left(\underline{\sigma}\right) = \frac{\partial\underline{\sigma}}{\partial r}.\underline{i}_{r} + \frac{\partial\underline{\sigma}}{\partial\theta}.\underline{i}_{r} + \frac{\partial\underline{\sigma}}{\partial\tau}.\underline{i}_{z} = 4\mu\alpha\frac{R^{2}}{\sigma^{3}}\underline{i}_{r} - 4\mu\alpha\frac{R^{2}}{\sigma^{3}}\underline{i}_{r} + 0 = 0$$

7
$$\underline{\sigma} \cdot \underline{n}|_{r=R} = -\underline{\sigma}|_{r=R} \cdot \underline{i}_r = 2\mu\alpha\underline{i}_r = f_s = -p_0\underline{n} = p_0\underline{i}_r \Rightarrow \alpha = \frac{p_0}{2\mu}$$

Part III - Failure criteria (isotropic)



Isotropic stress state

•
$$\sigma_v = \sigma_h = -\rho g H < 0$$
 $\underline{\underline{\sigma}}_0 = \sigma_v \underline{\underline{I}}, \underline{\underline{\sigma}}_t = \underline{\underline{\sigma}}_0 + \underline{\underline{\sigma}}$

Question 8/9/10/11 : failure criteria?

$$\begin{aligned}
8 & div_{X}\left(\underline{\underline{\sigma}}_{t}\right) = div_{X}\left(\underline{\underline{\sigma}}_{0}\right) + div_{X}\left(\underline{\underline{\sigma}}\right) = 0 \\
\underline{\underline{\sigma}}_{x} \underline{\underline{n}}|_{r=R} & -\underline{\underline{\sigma}}_{x}\underline{\underline{i}}_{r} = -\sigma_{v}\underline{\underline{i}}_{r} + p_{0}\underline{\underline{i}}_{r} = 0 \to p_{0} = \sigma_{v} < 0
\end{aligned}$$

$$9 \ \underline{\underline{\sigma}}_{t} = \sigma_{v} \underline{\underline{I}} + \sigma_{v} \left(\frac{R}{r} \right)^{2} \left(\underline{\underline{i}}_{\theta} \otimes \underline{\underline{i}}_{\theta} - \underline{\underline{i}}_{r} \otimes \underline{\underline{i}}_{r} \right) \text{ (diagonal)} \rightarrow \sigma_{I} =$$

$$\sigma_{v}\left(1-\left(\frac{R}{r}\right)^{2}\right); \sigma_{III}=\sigma_{v}\left(1+\left(\frac{R}{r}\right)^{2}\right), \tau_{\max}=\frac{\sigma_{I}-\sigma_{III}}{2}=-\sigma_{v} \leq \tau_{c}$$

10 In plane
$$(\underline{i}_r, \underline{i}_\theta)$$
, tangent to tunnel's cross section, fractures at $\alpha = \pm \frac{\pi}{4}$)

11 $\sigma_I < 0 = \sigma_R$ $\tau_{\text{max}} = -\sigma_v \le \tau_c \to H \le \frac{\tau_c}{\rho g}$

$$\underline{\boldsymbol{u}}_t = \underline{\boldsymbol{u}}_0 + \underline{\boldsymbol{u}} = 0 + \frac{\rho g H}{2\mu} \frac{R^2}{r} \underline{\boldsymbol{i}}_r \to u_{\text{max}} = \left\langle \underline{\boldsymbol{u}}_t, \underline{\boldsymbol{i}}_y \right\rangle \Big|_{r=R} = \frac{\rho g H R}{2\mu} \le \frac{\tau_c R}{2\mu}$$