

# Fluid Dynamics

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# 1 Kinematics

## 1.1 Streamlines and pathlines

There are two natural ways to think of flow.

- (i) A stationary observer watching flow go past. This is the Eulerian perspective. This is the approach used through this course. We define a velocity field (continuum field)  $\mathbf{u}(\mathbf{x}, t)$ .
- (ii) A moving observing, travelling along with the flow. This is the Lagrangian perspective.

**Definition.** (Streamlines) These are curves that are everywhere parallel to the flow at a given instant.

*Remark.* The streamline that goes through  $\mathbf{x}_0$  at time  $t_0$  is given parametrically as  $\mathbf{x} = \mathbf{x}(s, \mathbf{x}_0, t_0)$  and

$$\frac{d\mathbf{x}}{ds} = \mathbf{u}(\mathbf{x}, t_0)$$

(with  $\mathbf{x} = \mathbf{x}_0$  at  $s = 0$ ).

The set of streamlines shows the direction of flow a *given* instant a time (all fluid particle at one given time). Take the example  $\mathbf{u} = (1, t)$ . So at  $t = 0$  we have  $\mathbf{u} = (1, 0)$  so the streamlines are horizontal lines. At  $t = 1$  we have  $\mathbf{u} = (1, 1)$ , so the streamlines are diagonal.

**Definition.** (Pathlines) A *pathline* is the trajectory of a fluid particle (a very small bit of fluid). The pathline  $\mathbf{x} = \mathbf{x}(t, \mathbf{x}_0)$  of a fluid which is at  $\mathbf{x}_0$  at  $t = 0$  is such that

$$\frac{d\mathbf{x}}{dt} = \mathbf{u}(\mathbf{x}, t)$$

with  $\mathbf{x}(0, \mathbf{x}_0) = \mathbf{x}_0$ .

Again if we take  $\mathbf{u} = (1, t)$  we get

$$\begin{cases} \frac{dx}{dt} = 1 \\ \frac{dy}{dt} = t \end{cases} \rightarrow \begin{cases} x = x_0 + t \\ y = y_0 + \frac{t^2}{2} \end{cases}$$

which describes the path  $y - y_0 = \frac{1}{2}(x - x_0)^2$ .

*Remark.* Pathlines are often called "Lagrangian trajectories". The applications are very useful to characterise transport (infectious diseases and pollution simulations).

If the flow is *steady* (so  $\mathbf{u}$  does not depend on time). Then pathlines and streamlines are the same.

## 1.2 The material derivative

We will characterise the rate of change of "stuff" moving with a fluid. Consider a quantity  $F(\mathbf{x}, t)$  in a fluid flow (intuition is  $F$  is temperature). We want to measure how the temperature changes as we move through the field  $F$  along the flow. Let compute the rate of change of (in time) seen

by a moving observer. We will call this  $\frac{DF}{Dt}$ . Take a small time interval  $\delta t$ . Then

$$\begin{aligned}\delta F &= F(\mathbf{x} + \delta \mathbf{x}, t + \delta t) - F(\mathbf{x}, t) \\ &= \delta t \frac{\partial F}{\partial t} + (\delta \mathbf{x} \cdot \nabla) F + (\text{higher order terms}).\end{aligned}$$

We have that  $\delta \mathbf{x} = \mathbf{u} \delta t$ , so

$$\frac{\delta F}{\delta t} = \frac{DF}{Dt} = \frac{\partial F}{\partial t} + (\mathbf{u} \cdot \nabla) F.$$

We have the derivative and the convected derivative. This should be thought of as moving along gradients of a field.

### 1.3 Conservation of mass

Consider the flow through a straight rigid pipe with constant cross section. Suppose we have a  $\mathbf{u}_{\text{in}}$  and a  $\mathbf{u}_{\text{out}}$ . Can we have  $\mathbf{u}_{\text{in}} \neq \mathbf{u}_{\text{out}}$ ? For a gas, yes we can since they can be compressed. For a fluid, we cannot, since they are incompressible.

Define  $\rho(\mathbf{x}, t)$  as the mass density with  $[\rho] = \frac{M}{L^3}$ . We want a relation between  $\rho$  and  $\mathbf{u}$ . Consider a fixed volume  $V$  and compute the rate of change of its mass,  $M$ .

$$M = \int_V \rho dV$$

Assume that mass can only change due to the flow of mass across the boundary surface  $\partial V$ . Take a small surface element  $\delta A$  with normal  $\mathbf{n}$ . The volume out of  $V$  during  $\delta t$  is  $(\mathbf{u} \cdot \mathbf{n}) \delta A \delta t$ . Hence the mass out is  $\rho(\mathbf{u} \cdot \mathbf{n}) \delta A \delta t$ , so we get that

$$\frac{dM}{dt} = - \int_{\partial V} \rho(\mathbf{u} \cdot \mathbf{n}) dA.$$

The divergence theorem will allow us to rewrite this as

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{u}) = 0.$$

We know from IA Vector Calculus that  $\nabla \cdot (\rho \mathbf{u}) = \rho \nabla \cdot \mathbf{u} + \mathbf{u} \cdot \nabla \rho$ , so we can write that

$$\frac{D\rho}{Dt} = -\rho \nabla \cdot \mathbf{u}.$$

**Definition.** (Incompressible) A fluid flow is *incompressible* if  $\frac{D\rho}{Dt} = 0$ .

This is then equivalent to  $\nabla \cdot \mathbf{u} = 0$  which is the equivalent condition we'll use for the course.

For this course we will assume that  $\rho$  is constant. This means as a consequence that  $\nabla \cdot \mathbf{u} = 0$ .

### 1.4 Kinematic boundary condition

Consider the material boundary, with unit norm  $\mathbf{n}$ , of a body of fluid has a given velocity  $\mathbf{U}(\mathbf{x}, t)$ . At a point  $\mathbf{x}$  on the boundary, the fluid velocity relative to the surface is  $\mathbf{u} - \mathbf{U}$ . Applying mass conservation on the interface over a small surface element  $\delta A$  in time  $\delta t$ . So

$$\rho(\mathbf{u} - \mathbf{U}) \cdot \mathbf{n} \delta A \delta t = 0.$$

Hence we require  $\mathbf{u} \cdot \mathbf{n} = \mathbf{U} \cdot \mathbf{n}$  at the interface. This is the kinematic boundary condition.

*Remark.*  $\mathbf{n}$  occurs on both sides, hence we don't need  $\mathbf{n}$  to be a unit vector.

We have some consequences of this condition.

- (i) If the boundary is fixed,  $\mathbf{U} = 0$  implies that  $\mathbf{u} \cdot \mathbf{n} = 0$ . This is called the no penetration condition.
- (ii) Consider an air/water interface (free surface). Suppose the surface is defined by  $z = \xi(x, y, t)$ . Then can think of the free space as  $F(x, y, z, t) = 0$  where  $F(x, y, z, t) = z - \xi(x, y, t)$ . So  $\mathbf{n}$  is perp to  $\nabla F = (-\xi_x, -\xi_y, 1)$ . Then if  $\mathbf{u} = (u, v, w)$  so  $\mathbf{U} = (0, 0, \xi_t)$ . Then the kinematic boundary condition becomes  $-u\xi_x - v\xi_y + w = \xi_t$ , so  $w = \xi_t + u\xi_x + v\xi_y = \frac{DF}{Dt}$ . This is equivalent to  $\frac{DF}{Dt} = 0$ .

## 1.5 Streamfunction for 2D incompressible flow

We know that  $\nabla \cdot \mathbf{u} = 0$  which is equivalent to there existing a vector potential  $\mathbf{A}$  such that  $\mathbf{u} = \nabla \times \mathbf{A}$ . In 2D if  $\mathbf{u} = (u, v, 0)$  then  $\mathbf{A} = (0, 0, \psi(x, y))$ . So

$$u = \frac{\partial \psi}{\partial y}, \quad v = -\frac{\partial \psi}{\partial x}.$$

We call  $\psi$  a *streamfunction*. Looking at dimensions we have that  $[\psi] = \text{L}^2 \text{T}^{-1}$ . Now we'll see an example.

Let  $\mathbf{u} = (y, x)$  (which we can see is incompressible) so

$$\frac{\partial \psi}{\partial y} = u = y$$

, hence  $\psi = \frac{1}{2}y^2 + f(x)$ . We also have that  $-\frac{\partial \psi}{\partial x} = -f'(x) = x$ , so  $\psi = \frac{1}{2}(y^2 - x^2) + C$ .

We have some properties about the streamfunction,

- (i) Streamlines are given by  $\psi = \text{constant}$ .
- (ii)  $|\mathbf{u}| = |\nabla \psi|$ , so the flow is faster if the streamlines are closer together.
- (iii) If we take two points  $\mathbf{x}_0, \mathbf{x}_1$ , then then the volume flux crossing the line between  $\mathbf{x}_0$  and  $\mathbf{x}_1$  is

$$\int_{\mathbf{x}_0}^{\mathbf{x}_1} \mathbf{u} \cdot \mathbf{n} d\ell = \psi(\mathbf{x}_1) - \psi(\mathbf{x}_0).$$

- (iv)  $\psi$  is constant at rigid boundaries.

We can do the same in polar coordinates. So  $\mathbf{u} = (u_r(r, \theta), u_\theta(r, \theta), 0)$ . We have that

$$\mathbf{u} = \nabla \times \mathbf{A} = \left( \frac{1}{r} \frac{\partial \psi}{\partial \theta}, -\frac{\partial \psi}{\partial r}, 0 \right),$$

so we can check that  $\nabla \cdot \mathbf{u} = \frac{1}{r} \frac{\partial}{\partial r}(ru_r) + \frac{1}{r} \frac{\partial}{\partial \theta} = 0$

## 2 Dynamics of inviscid flow

### 2.1 Surface and volume forces

There are two types of forces exerted on a fluid.

- (i) Forces proportional to the volume (gravity);
- (ii) Forces proportional to the surface area (pressure, viscous stresses).

We'll first look at the first type, called volume forces. We'll denote  $F(\mathbf{x}, t)\delta V$  as the force acting on a small volume element  $\delta V$ . Let's take gravity as an example, so  $\mathbf{F} = \rho\mathbf{g}$ . Often we have that  $\mathbf{F}$  is conservative, so  $\mathbf{F} = -\nabla\chi$  for some function  $\chi$  (we know gravity is  $\chi = \rho gz$ ).