



Improved logistic models of crown fire probability in Canadian conifer forests

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ABSTRACT

Background. Crown fires are an ecologically necessary but hazardous process in conifer forests. Prediction of their behaviour in Canada has largely depended on the Canadian Forest Fire Behaviour Prediction System, in which fire weather indices drive primarily fixed fuel type models. The Crown Fire Initiation and Spread (CFIS) system presents a more flexible approach to predicting crown fire occurrence than fixed fuel type models. **Aims.** Using a multi-decadal database of experimental fires carried out in conifer plots (1960–2019, $n = 113$), our aim was to develop updated models based on the CFIS system approach, fitting crown fire occurrence models to fire environment variables using logistic regression. **Methods.** We tested alternative fuel moisture estimates and compared various model forms using repeated cross-validation. In two-storeyed stands, crown fire occurrence was defined as the involvement of lower canopy stratum fuels. **Key results.** Final models based on wind speed, fuel strata gap, litter moisture and surface fuel consumption predicted crowning events correctly in up to 92% of cases in training data (89% in cross-validation). **Conclusions and implications.** These new models offer improved accuracy and flexibility that will help users assess how competing environmental factors interact under different fuel treatments and wildfire scenarios.

Keywords: Canadian Forest Fire Behaviour Prediction (FBP) System, Canadian Forest Fire Weather Index (FWI) System, Crown Fire Initiation and Spread (CFIS) system, crown fire occurrence, experimental burning, modelling, wildfire management, wildland fire behaviour.

Introduction

Crown fires have long been recognised as important ecological phenomena in conifer forests of boreal and temperate regions, including Canada (Bell 1889; Van Wagner 1983; Coogan *et al.* 2021). As a spreading flame front moves from surface fuels into the forest canopy and accesses crown fuels, it is exposed to higher winds resulting in a 2- to 10-fold increase in rate of spread (ROS) and fireline intensity (Alexander and Cruz 2016). Because most conifer forests will support crown fire under extreme fire weather conditions (Beverly *et al.* 2020; Cruz *et al.* 2022), it is critical to understand the necessary conditions for predicting the occurrence of crown fires. Such information has many practical fire and fuel management applications, including wildfire preparedness, response tactics and firefighter safety, as well as planning fuel treatments to mitigate crown fire behaviour potential (Perrakis *et al.* 2020).

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Canadian empirical and semi-empirical crown fire models

Since the late twentieth century, Canadian fire management personnel and fire researchers have primarily used the Canadian Forest Fire Behaviour Prediction (FBP) System (Forestry Canada Fire Danger Group 1992) to forecast quantitative measures of wildfire behaviour. The FBP and Canadian Forest Fire Weather Index (FWI; Van Wagner 1987) Systems are both part of the larger Canadian Forest Fire Danger Rating System (CFFDRS; Stocks *et al.* 1989; Taylor and Alexander 2006). The present-day CFFDRS is being

renewed, with many proposed changes and improvements anticipated (CFS Fire Danger Group 2021). The current FBP System depends on discrete fuel types representing various fire-prone Canadian vegetation complexes. Each of the seven conifer fuel types has empirical functions for predicting ROS and surface fuel consumption (SFC) based on components of the FWI System, along with mostly fixed values for live crown base height (LCBH) and other fuel attributes (Forestry Canada Fire Danger Group 1992). At the time of its release, the fixed-fuel type concept was well-suited to the needs of operational users, who generally lacked detailed forest structure data (Van Wagner 1990).

The Van Wagner (1977) crown initiation model provides a physical and conceptual framework for crown fire in the FBP System and is used to predict the overall type of fire (i.e. surface or crown) and trigger further calculations of fuel consumption and fireline intensity (Forestry Canada Fire Danger Group 1992). According to Van Wagner's (1977) model, crown fire initiation is deemed to occur when a critical surface fire intensity threshold is exceeded based on the LCBH and foliar moisture content (FMC). In this scheme, LCBH is the critical forest structure variable influencing crown fire occurrence, a readily defined measure in single-storeyed stands. Although researchers have long used Van Wagner's (1977) equation to study how fuel structure can affect crown fire occurrence (Alexander 1988; Agee et al. 2000), it did not address questions related to more complex canopy structure or the influence of ladder fuels (Keane 2015). It also demanded a separate surface fire model, which was available for the FBP System fuel types but otherwise required a separate means of estimation.

Seeking empirical model solutions

Earlier statistical analyses of the influence of LCBH, weather, fuel moisture and selected FWI System components on crown fire occurrence in the Canadian experimental fire database (Cruz et al. 2003, 2004) are incorporated into the Crown Fire Initiation and Spread (CFIS) system and software package (Alexander et al. 2006). Here, we introduce additional data and several novel analytical procedures and modelling methods that have emerged in the intervening years.

The present analysis involves: (1) a larger dataset than previously considered; (2) a stand-adjusted model of surface litter moisture content (MC_{SA}); (3) a new approach to modelling the probability of crown fire occurrence in complex conifer stands; and (4) a more robust statistical testing framework for comparing different model forms than previously used. We also sought to clarify data flow from forest surveys through to crown fuel characteristics, an often-skipped over step (Affleck et al. 2012). The overall goal of the present study was to harness the findings from six decades of experimental burning research in Canada (Fig. 1) in order to improve the operational capability of crown fire occurrence models.

For convenience, a summary list of abbreviations used throughout the paper is provided in Appendix 1 (Table A1).

Material and methods

Experimental fire database: 60 years of experimental burning in Canada

The experimental fire data (Alexander and Quintilio 1990) behind the FBP System (Fig. 1) have been summarised in part in previous publications (e.g. Cruz 1999; de Groot et al. 2022). Our present database (Table 1) includes the majority of conifer experimental fire data between 1960 and 1986, along with 21 more recent observations (the latest being 2019), for a total of 42 more fires than were used in the development of previous crown fire occurrence models (Cruz et al. 2004). The database remains heavily weighted to natural stands of boreal and sub-boreal forest types, particularly jack pine (*Pinus banksiana* Lamb.) and black spruce (*Picea mariana* (Mill.) B. S. P.), and to a lesser extent white pine (*Pinus strobus* L.)–red pine (*Pinus resinosa* Ait.), lodgepole pine (*Pinus contorta* var. *latifolia* Engelm. Dougl. ex Loud.) and red pine plantations. Not included in this study's database were experimental fires and wildfires in dead insect-killed stands (Stocks 1987b; Perrakis et al. 2014), nor sparsely documented fires in dry forest types of southern interior British Columbia (i.e. FBP System fuel type C-7; Forestry Canada Fire Danger Group 1992). It is also noteworthy that we did not include wildfire observations from the FBP System database, other than two well-documented exceptions, as described below.

Most of the experimental fires were carried out in varying sizes of square (Fig. 1g) or rectangular (Fig. 1h) shaped plots (~0.05–5.0 ha) on flat terrain; the fires were generally lit from an ignition line (Fig. 1b, i) along the windward edge of cleared fireguards using hand-held drip torches or pressurised fuel dispensers (Fig. 1b, j). Alternate ignition techniques were used on a small number of plots. These included: ignition as a backing fire, which then became a headfire following a change in wind direction (Van Wagner 1964); paired experiments where one plot's flame front ignited an adjacent area, as part of a fuel treatment effectiveness trial (Fig. 1h; Thompson et al. 2020) and an escaped experimental fire, monitored independently (Plot 5a in Alexander et al. 1991); point source ignition with allowance for acceleration to equilibrium conditions (Kil 1975); and cases where single plots were split into two parts due to significant changes in weather conditions, principally wind speed (Plots 4a and 4b in Quintilio et al. 1977; Plots 11a and 11b in Stocks 1987a; and Plots 8a and 8b in Stocks et al. 2004). Finally, two wildfires have long been included among the experimental observations due to their connections with experimental stands: the Porter Lake CR-6-1982 wildfire resulting from the escaped experimental fire (Alexander et al. 1991) and two observations related to distinct fuel patches in the 1964



Fig. 1. Photographs of experimental fires in Canadian conifer forests, 1960s–2019. (a) Vigorous surface fire near the crown fire threshold in a red pine plantation at the Petawawa National Forestry Institute, Ontario. (b and c) Line source ignition in overstocked immature jack pine at Sharpsand Creek, Ontario, showing high stem density and rapid crowning. (d) Surface fire in jack pine at Darwin Lake, Alberta. (e) Active crown fire in boreal lowland black spruce at Big Fish Lake, Alberta. (f) Mid-storey black spruce under mature jack pine overstorey at Kenshoe Lake, Ontario. (g) Active crown fire in jack pine–black spruce at the International Crown Fire Modelling Experiment site, Northwest Territories. (h) Active crown fire in thinned and unthinned black spruce, Pelican Mountain, Alberta. (i) Line source ignition and surface fire spread in mature lodgepole pine at Summit Lake (near Prince George), British Columbia. (j) Transition to torching and crowning following ignition in semi-mature jack pine, Sharpsand Creek. All photos from Canadian Forest Service fire research archives. For additional photographs, see Alexander and de Groot (1988), Alexander and Lanoville (1989), Stocks and Hartley (1995), and Hirsch et al. (2000).

Gwatkin Lake wildfire (Van Wagner 1965, 1977), based on a detailed wildfire reconstruction within <1.0 km of a pre-existing experimental study area (Hummel 1979). In all cases, we treated these as independent observations following the advice of the original investigators.

Canopy fuel structure: live crown base height, fuel strata gap, and two-storeyed stands

Previous analyses used LCBH or the related fuel strata gap (FSG; Cruz et al. 2004) as the measure of vertical fuel

separation, based on field measurements or alternate means of estimation (Table 1). Due to variable sampling methods and limited descriptions in some studies, we made a considerable effort to locate and reanalyse original stand data wherever possible. The LCBH was calculated as the mean value of a single species canopy stratum sampled directly from plots or estimated using models or measurements of crown ratio. See Supplementary Material for details on the various means used to estimate LCBH. Most stands had a simple one-layer canopy (as per Van Wagner 1977), and we assumed that the FSG was simply the LCBH, with two exceptions: multi-layered stands,

Table I. Summary of the database of experimental observations; see Appendix I for list of abbreviations.

Site & overstorey species	Years	Number: SF/CF	WS₁₀ km h⁻¹	FFMC	DMC	FMC^A%	SFC kg m⁻²	
I. PNFI (WRP)	1960–1964	8/0	10.9 (5.0–23.0)	90.8 (87.8–92.8)	58.8 (42–76)	113.7 (100.5–120.0)	2.1 (0.9–3.1)	
2. PNFI (JP)	1962–1965	5/2	12.6 (5.0–23.0)	90.6 (88.5–92.8)	55.6 (28–77)	107.3 (100.0–118.0)	1.5 (0.4–2.7)	
3. PNFI (RP)	1962–1971	8/4	13.3 (5.0–23.0)	90.9 (88.5–92.9)	47.6 (21–89)	98.1 (91.0–108.0)	1.3 (0.6–2.1)	
4. Prince George (LP): PG	1970	8/0	8.2 (6.4–12.9)	91.6 (90.5–93.0)	61.0 (33–77)	102.8 (90.5–116.6)	0.6 (0.2–1.2)	
5. Big Fish Lake and others (BS): BFL	1972–1986	3/9	11.6 (5.0–18.7)	87.7 (80.0–91.2)	21.0 (9–44)	102.3 (79.0–120.0)	1.5 (0.8–2.3)	
6. Kenshoe Lake (JP/BS): KL	1973–1983	6/6	12.3 (3.0–29.0)	89.6 (87.2–91.4)	31.8 (19–42)	89.4 (85.0–106.1)	0.9 (0.4–1.5)	
7. Darwin Lake (JP): DL	1974	5/2	10.3 (6.3–16.9)	91 (88.7–93.7)	30.3 (15–43)	116.3 (109.7–120.0)	2.0 (1.0–3.2)	
8. Sharpsand Thinned (JP): SC-TH	1974–1981	2/3	12.4 (8.0–15.0)	92 (89.0–94.1)	39.2 (29–45)	107.9 (99.8–115.2)	1.1 (0.8–1.5)	
9. Sharpsand Immature (JP): SC-IM	1975–1981	3/11	12.4 (6.0–21.0)	90.5 (87.9–93.3)	43.0 (25–57)	108.0 (85.7–117.8)	1.4 (0.7–2.4)	
10. Porter Lake (BS): PL	1982	0/7	23.5 (14.5–34.6)	91.5 (89.4–92.8)	58.7 (51–66)	86.0 (85.1–86.5)	1.3 (1.1–1.6)	
11. Sharpsand Semi-mature (JP): SC-SM	1988–1991	4/4	12 (9.0–19.0)	90.8 (88.6–93.4)	47.9 (32–70)	86.8 (85.1–92.6)	2.5 (1.4–3.6) ^B	
12. ICFME (JP/BS)	1997–2000	0/11	14.2 (7.9–25.0)	91.8 (89.4–94.2)	53.8 (35–84)	82.2 (74.2–92.1)	2.6 (1.5–3.8)	
13. Pelican Mountain (BS): PM	2019	0/2	12.0	93.6	46	79.0	1.6 (1.4–1.7)	
Overall	1960–2019	52/61	12.7 (3.0–34.6)	90.6 (80.0–94.2)	44.6 (9–89)	99.0 (74.2–120.0)	1.57 (0.2–3.8)	
Site	MC_{FFMC}%	MC_{SA}%	MC_{SA}: stand	MC_{SA}: season	MC_{SA}: density	LCBH^A M	FSG adjust.	Primary sources
1.	10.0 (7.9–13.2)	9.5 (6.9–11.7)	Pine	0/0/8	2/6/0	11.7 (7.4–13.3)	–	Van Wagner (1963), unpublished files
2.	10.2 (7.9–12.4)	9.3 (7.2–11.9)	Pine	1/2/4	1/6/0	8.4 (6.0–12.0)	–	Van Wagner (1977), Hummel (1979), Weber et al. (1987)
3.	9.9 (7.8–12.4)	10.8 (7.4–17.2)	Pine	2/2/8	0/0/12	7.5 (6.0–9.0)	–	Van Wagner (1968), Van Wagner (1986), unpublished files

(Continued on next page)

Table I. (Continued)

Site	MC _{FFMC} %	MC _{SA} %	MC _{SA} : stand	MC _{SA} : season	MC _{SA} : density	LCBH ^A M	FSG adjust.	Primary sources
4.	9.1 (7.7–10.3)	8.2 (7.3–9.7)	Pine	0/0/8	4/4/0	8.2 (6.7–9.8)	–	Lawson (1972)
5.	13.4 (9.6–22.2)	13.9 (10.9–19.8)	Spruce	0/0/12	9/3/0	1.1 (0.4–1.9)	–	Kiil (1975), Newstead and Alexander (1983), Cruz (1999), unpublished files
6.	11.2 (9.4–13.8)	12 (10.9–14.1)	Pi/Sp	7/1/4	0/0/12	2.0	–	Stocks (1989), unpublished files
7.	9.8 (7.0–12.2)	10.3 (7.0–14.5)	Pine	0/0/7	4/3/0	5.6 (4.8–6.3)	–	Quintilio et al. (1977)
8.	8.7 (6.6–11.9)	9.3 (7.3–12.2)	Pine	0/0/5	0/5/0	4.4 (4.3–4.8)	–	Stocks (1987a), de Groot et al. (2022), unpublished files
9.	10.3 (7.4–13.1)	11.6 (7.9–15.0)	Pine	0/1/13	0/3/11	4.4 (4.1–4.9)	LCBH-2.0	Stocks (1987a), unpublished files
10.	9.3 (7.9–11.5)	8 (6.9–9.7)	Spruce	0/0/7	7/0/0	0.9 (0.8–1.1)	–	Alexander et al. (1991)
11.	10 (7.3–12.3)	9.8 (7.3–11.7)	Pine	2/5/1	0/1/7	5.3	LCBH-1.0	McRae et al. (2017)
12.	9 (6.5–11.5)	9.8 (6.3–13.5)	Pi/Sp	0/0/11	0/3/8	2.6 (0.7–8.2)	LCBH-1.0 ^C	Alexander et al. (2004), Stocks et al. (2004)
13.	7.1	6.6 (6.3–6.9)	Spruce	2/0/0	1/1/0	3.1 (2.1–4.2)	–	Thompson et al. (2020)
Overall	10.2 (6.5–22.2)	10.5 (6.3–19.8)	–	14/11/88	28/35/50	4.9 (0.4–13.3)	–	–

^ASee Supplementary Material for sources of FMC and LCBH estimates.^BEstimated using reported total fuel consumption values, with crown fuel consumption values from SC-IM and SC-TH plots; see Supplementary Material for details.^CFSG Adjustment at ICFME only applied to plots with LCBH >2.0 m. See text for details.

Table 2. Crown fire initiation model comparison, based on four-fold Monte Carlo cross-validation (1000 iterations).

Model	Predictors	Accuracy	MCC	AIC	FSG	MCC Rank	AIC Rank
A	WS ₁₀ + FSG	0.815	0.628	71.7	Base	14	14
B	WS ₁₀ + FSG + MC _{FFMC}	0.841	0.680	56.0	Base	12	13
1.	WS ₁₀ + FSG + SFC + MC _{FFMC}	0.863	0.724	50.8	Base	8	10
2.	WS ₁₀ + FSG + SFC + MC _{SA}	0.839	0.676	54.7	Base	13	12
3.	WS ₁₀ + FSG ^{1.5} + SFC + MC _{FFMC}	0.868	0.733	49.7	Base	6	7
4.	WS ₁₀ + FSG ^{1.5} + SFC + MC _{SA}	0.849	0.696	52.4	Base	11	11
5.	WS ₁₀ + FSG ^{1.5} + SFC + MC _{FFMC} × WS ₁₀	0.873	0.744	46.5	Base	5	5
6.	WS ₁₀ + FSG ^{1.5} + SFC + MC _{SA} × WS ₁₀	0.856	0.710	50.3	Base	9	9
7.	WS ₁₀ + FSG ^{1.5} + ln(SFC) + MC _{FFMC} × WS ₁₀	0.878	0.755	46.0	Base	3	4
8.	WS ₁₀ + FSG ^{1.5} + ln(SFC) + MC _{SA} × WS ₁₀	0.865	0.727	50.3	Base	7	8
9.	WS ₁₀ + FSG ^{1.5} + SFC.CLS + MC _{FFMC} × WS ₁₀	0.853	0.705	47.2	FSG Adj.	10	6
10.	WS ₁₀ + FSG ^{1.5} + ln(SFC) + MC _{FFMC} × WS ₁₀	0.887	0.772	42.8	FSG Adj.	2	2
11.	WS ₁₀ + FSG ^{1.5} + ln(SFC) + MC _{SA} × WS ₁₀	0.890	0.779	42.5	FSG Adj.	1	1
12.	WS ₁₀ + FSG ² + ln(SFC) + MC _{SA} × WS ₁₀	0.876	0.751	44.8	FSG Adj.	4	3

MCC and AIC represent the Matthews Correlation Coefficient and Akaike's Information Criterion, respectively. 'FSG' refers to the form of the fuel strata gap: the Base live crown base height, or adjusted value reflecting standing dead ladder fuels (see Table 1). Model 9 includes a categorical term for SFC; all other inputs are continuous. See Appendix 1 for abbreviation descriptions.

and stands with a large number of small dead stems that visibly contributed to crowning.

Most plots at the Kenshoe Lake (KL) and International Crown Fire Modelling Experiment (ICFME) sites had two canopy layers, a mid-storey black spruce layer underneath an upper canopy of jack pine (Fig. 1f; Stocks 1989; Alexander et al. 2004). Rather than using a combined LCBH value, we assumed these distinct strata involve separate conditional crowning processes: vertical flame propagation into the mid-canopy spruce component is first required before testing the much higher overstorey pine canopy (Van Wagner 1993). Aside from the species mix and two-storeyed structure, the stands at these two sites, KL and ICFME, differ in terms of age class and vertical structure. However, it is apparent that they are otherwise similar, with black spruce comprising about 11% of live basal area and 30–35% of live tree density at both sites (Walker and Stocks 1975; Alexander et al. 2004, Table 2).

A number of plots at Sharpsand Creek (SC) and at ICFME contained significant quantities of ladder fuels in the form of small (< 5.0 cm diameter at breast height (DBH)) dead trees that were observed to be influential in the crowning process (Stocks 1987a; Stocks and Hartley 1995). The abundance of dead ladder fuels evident in the immature jack pine stands at SC (SC-IM: Fig. 1b, c; SC-SM: Fig. 1j) was a result of the stem mortality associated with natural stand development. A separate set of plots at the site had been hand-thinned 15 years prior to their burning (SC-TH) and had much

lower overstorey tree density (Stocks 1987a; de Groot et al. 2022). Earlier studies have treated these experimental plots as separate fuel types (Forestry Canada Fire Danger Group 1992; de Groot et al. 2022),¹ or estimated that the standing dead trees at SC-IM reduced the FMC (Van Wagner 1993).

For the present analysis, we expanded on the FSG concept introduced by Cruz et al. (2004, 2006) and estimated FSG for the SC-IM (~10 000 dead stems ha⁻¹) and SC-SM (~3800 dead stems ha⁻¹) plots as LCBH-2.0 and LCBH-1.0 m, respectively. For the SC-TH plots, no adjustment was made (i.e. FSG = LCBH), due to the lower dead tree density (< 1200 ha⁻¹). At the ICFME site, 31% of the total stem density consisted of small diameter dead jack pine (Alexander et al. 2004); however, there was substantial variation in the amount of black spruce understorey and LCBH. For those plots with LCBH values > 2.0 m, we adjusted FSG (FSG = LCBH - 1.0). No adjustment was made (FSG = LCBH) for plots with low LCBH (LCBH < 2.0 m) because we judged that dead stems would not add significantly to the ladder fuel effect. Although these adjustments were subjective, we analysed our database using both (unadjusted) LCBH and (adjusted) FSG to reveal whether use of the FSG adjustments could be justified. No other site descriptions suggested the presence of standing dead trees in comparable amounts, but lower densities were often noted, such as 0–60 dead stems ha⁻¹ at Darwin Lake

¹Although it is not explained in detail in the report on the FBP System (Forestry Canada Fire Danger Group 1992), the C-3 fuel type models included the SC-TH plots, whereas the C-4 fuel type models included the SC-IM plots.

(DL; Quintilio *et al.* 1977) and 109–250 ha⁻¹ at Prince George (PG; Lawson 1972).

Fine fuel moisture content estimates

To incorporate the influence of fine dead fuel moisture content (MC), we tested two approaches. The first used the Fine Fuel Moisture Code (FFMC) component of the FWI System (MC_{FFMC}). This code is calibrated to predict MC broadly across conifer forests for a ‘generalised pine stand’ (Van Wagner 1974a). The second approach used a stand-adjusted moisture content estimate (MC_{SA} ; Wotton and Beverly 2007) incorporating several stand structure and condition influences on MC in addition to the FFMC and Duff Moisture Code (DMC) components of the FWI System. Calculating the MC_{SA} for the fires assembled in our database required assigning several necessary input variables: FFMC; DMC; and categorical variables for stand type, stand density class and season (Wotton and Beverly 2007).

Although the MC_{SA} model includes five stand type options (Wotton and Beverly 2007), all of our observations were classed as either ‘pine’ or ‘spruce’ (or the mean of both), based on overstorey composition (Table 1). Density class and season variables required some interpretation and judgement. For example, the density class variable has three levels (i.e. ‘light’, ‘moderate’, ‘dense’) based on site descriptions, canopy closure and photographic evidence. We assumed that density affected MC primarily due to variable solar radiation at the forest floor level and the influence of in-stand wind (Whitehead *et al.* 2008; Ma *et al.* 2010; Moon *et al.* 2016). Moderately closed pine stands (~50–60% canopy closure) were assigned to the ‘moderate’ density class, in parallel with the dominant class found in the litter moisture data (Wotton and Beverly 2007). The ‘dense’ class was assigned to sites with estimated canopy closure of >60% or particularly high crown fuel loading values (Forestry Canada Fire Danger Group 1992; Cruz 1999; de Groot *et al.* 2022). ‘Light’ density class was assigned to sites with obvious low-density structure (Alexander *et al.* 1991), as well as to individual plots at other sites with <45% canopy closure (Table 1). The ‘dense’ class experimental fires with $FFMC \geq 93.0$ were reclassified to ‘moderate’ due to some illogical behaviour of the MC_{SA} model at high FFMC levels; see Supplemental Material for details.

Based on the guidance in Wotton and Beverly (2007), we used simple calendar dates to assign the season factor to each observation. Fires taking place before June were assigned to Spring (SP) and fires from 16 June through 1 September were regarded as summer (SU) fires. To avoid an artificially abrupt transition and to approximate the green up process (Chrosiewicz 1986), we added a ‘transition’ (TR) season for dates from 1 to 15 June, calculated as the mean of spring and summer MC_{SA} estimates (Table 1).

Surface fuel consumption

Recognised as a key influence on surface fire intensity and therefore crown fire initiation (Van Wagner 1977; Agee *et al.* 2000), SFC was measured or estimated for all experimental fire plots. We used the sum of all consumed forest floor and fine woody fuels (i.e. roundwood diameters <7.0 cm) as the SFC value in our analysis; most studies did not report separate measures for litter and duff, and some did not separate fuels into forest floor and woody fuel portions. In most experimental fires (e.g. Stocks 1989; Alexander *et al.* 1991), SFC values were dominated by forest floor consumption, with lower contributions (i.e. 1/3 or less of the SFC) from woody fuels. Several fires had particularly high SFC levels (>3.0 kg m⁻²) caused by the consumption of dense, compact duff layers. To reduce the influence of these observations on regression equations, we tested log-transformations of SFC values during the model-building phase.

Model fitting and evaluation

All final records for each fire in the database included measurements or estimates of fuel structure (i.e. LCBH and FSG), FMC, SFC, 10-m open wind speed (WS_{10}), FWI System components (FFMC, DMC) calculated from an onsite or nearby representative station, fine fuel moisture (MC_{FFMC} and MC_{SA}) and finally, a fire behaviour description including the type of fire – i.e. surface (Fig. 1a, d, i) or crown (Fig. 1c, e, g, h, j). Crown fire was considered to have occurred when crowning-type fire behaviour (i.e. passive or active, as per Van Wagner 1977; or intermittent, as per Forestry Canada Fire Danger Group 1992) was described or could be inferred from the original source publications or file photographs. At the two sites with two-layered canopy fuels (i.e. KL and ICFME), only crown involvement of the mid-storey spruce was tested in our main analysis. Following Cruz *et al.* (2003, 2004), crown fire occurrence was modelled as the response variable in a generalised linear model (logistic regression). Predicted probability values above and below 0.5 were interpreted as crown fire and surface fire, respectively.

The initial explanatory variables were suggested from previous modelling results (Cruz *et al.* 2004; Perrakis *et al.* 2020). A backwards stepwise regression approach was used starting with all interaction effects between predictor variables: WS_{10} , SFC, FSG, FMC and MC_{FFMC} or MC_{SA} , with terms tested at the $\alpha = 0.05$ level. For WS_{10} , linear and squared terms were tested. For LCBH and FSG variables, linear, squared and 3/2 exponents were tested, the latter following Van Wagner’s (1977) crown fire initiation model. For the SFC, linear, log-transformed and categorical terms as per Cruz *et al.* (2004) were tested.

Various model forms were then compared using a Monte Carlo implementation of *k*-fold cross-validation, with four folds. This analysis, considered highly efficient for

comparing alternative model forms with small datasets (Zhang 1993; Lantz 2019), involves splitting the data into four equal but randomly selected ‘folds’, fitting the models to three of them, and evaluating the ensuing models using the fourth (unused) portion of observations. Cross-validation was performed in R v.4.2.2, using the ‘vtreat’ data package (Mount and Zumel 2018), with 1000 repeated iterations of training and testing for each model form. Model ranking was based on comparing mean values of Akaike’s Information Criterion (AIC) and Matthews Correlation Coefficient (MCC) values from the iterations. The MCC is an evaluation method based on calculation of the Pearson correlation coefficient between values of a binary confusion matrix. It has been shown to be less biased than more common evaluation measures (Powers 2011) and particularly effective for unbalanced datasets (Chicco and Jurman 2020), as might occur in random selections of surface and crown fire observations. Initial model tests used the unmodified LCBH. We then retested the best performers using the adjusted FSG values for some sites as previously described.

Following cross-validation, the best models were fitted to the complete dataset and evaluated based on accuracy, AIC and Nagelkerke R^2 (Mangiafico 2015). We also tested the dataset on previously published CFIS system models (i.e. LOGIT 1 and 2 models from Cruz et al. 2003) for comparative purposes.

Results

Our final experimental fire database contained 113 observations, consisting of 52 surface fires and 61 crown fires (Table 1). Individual relationships between predictors and crown fire occurrence were generally as expected. Crown fire was clearly associated with low LCBH (and FSG), MC_{FFMC} and FMC values, and high WS₁₀ and SFC values (Fig. 2). Estimated FMC had the only bivariate correlation >0.3 (positive with FSG). We then tested the FMC between low FSG (<4.0 m, 90.8%) and high FSG (≥ 4.0 , 103.6%) and found them significantly different (Welch’s t -test: $P < 0.001$). This appeared to be caused by a disproportionate number of experimental fires in black spruce stands (with low LCBH) during ‘spring dip’ conditions (Van Wagner 1974b) in June and early July, compared with more evenly timed fires in higher-LCBH pine stands.

During model building, complex interaction terms were first dropped due to non-significance. Some models with multiple two-way interaction terms initially appeared significant, but further testing revealed illogical behaviour, thereby suggesting overfitting. The next-best model forms involved dropping the FMC term, it being non-significant ($P > 0.1$) in any tests at this level once insignificant interaction terms were removed. For the fine fuel moisture terms (MC_{SA} or MC_{FFMC}), either the main effect or the interaction term with WS₁₀ (i.e. WS₁₀ \times MC_{SA} or WS₁₀ \times MC_{FFMC}) was significant when included, but not both; in these cases, the

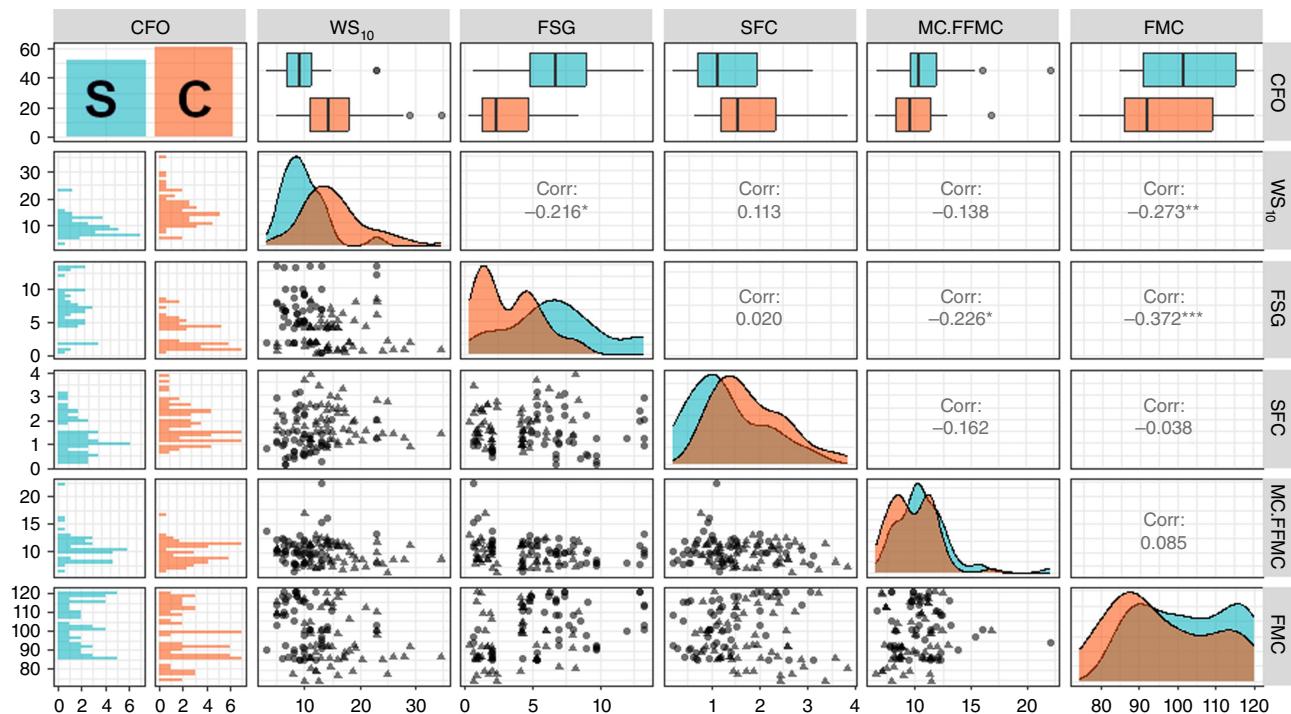


Fig. 2. Pairwise plots and correlations for surface (S, blue, circles) and crown fire (C, red, triangles) observations. See Table A1 for abbreviation details. Lines in diagonal cells indicate frequency distributions of environmental variables, bivariate scatter diagrams show the actual variable values, and ‘Corr.’ indicates Spearman’s Correlation, at the specified significance level: 0.1 (.), 0.05 (*), 0.01 (**), 0.001 (***).

interaction terms all produced better results (i.e. greater accuracy, lower AIC) than the main effects alone. Two simple main effects model forms that excluded the SFC term also showed promise (termed A and B): one used only WS₁₀ and LCBH, with MC_{FFMC} added for the second.

We then proceeded to the cross-validation step comparing model forms. Results comparing predictor sets using various interactions and transformations are shown in Table 2. The two simplest models, A and B, were the weakest performers, but still achieved mean accuracy >80%. Other models used WS₁₀, FSG (initially based on a linear LCBH value), MC (MC_{FFMC} or MC_{SA}) and estimated SFC, starting with simple main-effect predictors (Models 1 and 2) followed by the successive substitution of LCBH^{3/2}, WS₁₀ × MC interaction and log-transformed SFC for their respective linear and main effect terms. The adjusted FSG with ladder fuel influence was used in lieu of LCBH for the later tests, as shown in Table 2. More complex inputs improved model performance, in the form of higher accuracy and MCC, and lower AIC, although overall gains were small among top performers. The best-performing models approached 90% accuracy (Model 10: 88.7%; Model 11; 89.0%). Model 12 had a squared FSG term but was otherwise identical to Model 11, with slightly inferior performance. Models with a squared WS₁₀ term were inferior to all comparable forms with a linear WS₁₀ predictor (not shown). Tests of additional categorical terms for stand type (pine, spruce or a mix) or stand density were non-significant ($P > 0.1$). Based on these results, we moved ahead with the final analysis using model forms 7–11, these appearing to be the most accurate and practically useful forms to consider.

Table 3 shows the fitted coefficients and performance of the final models based on the full dataset. Model 9, with

categorical SFC, predicted crowning occurrence correctly for 99 of 113 observations, as shown. As with the cross-validation results, Models 10 and 11 had the best performance. Model 11 (using MC_{SA}) was slightly more accurate (104/113) than Model 10 (using MC_{FFMC}; 103/113). Model 11 also had better AIC and Nagelkerke pseudo- R^2 scores, indicative of lower residual deviance and better overall data representation, respectively. There was a relatively even split between classification errors for both models. Out of 113 possible classifications, Models 11 and 10 miscategorized four and five, and six and four surface and crown fires, respectively. The full list of fitted coefficients for all models in Table 2 is given in the Supplementary Table S1.

The CFIS LOGIT 1 and 2 models (Cruz *et al.* 2003), which were fitted from approximately half of the observations in our dataset and based on a slightly different definition of crown fire, both produced mean accuracy values of 81% based on the full dataset (92 of 113 correct observations). Further inspection of the results revealed a bias associated with classification errors, with the LOGIT 1 model producing 15 false negatives, or failure to detect crown fires, compared with six false positives (i.e. prediction of crown fires on actual surface fires). For the LOGIT 2 model, the results were 16 and 5 for missed crown and surface fires, respectively.

Model 11 was selected for further display. The probability distributions of crown fire at different WS₁₀ and FSG values are shown in Fig. 3, based on constant SFC and MC values. Fire observations are shown as either surface or crown, with crown fires further indicated as passive or active (Van Wagner 1977). Predictions from Cruz *et al.*'s (2003) LOGIT 1 model are also shown for comparative purposes. A more extensive comparison between models 9–11 with Cruz *et al.*'s (2003)

Table 3. Fitted coefficients and performance metrics of final crown fire occurrence models.

Predictor:	Input Type									
	-	WS ₁₀	FSG ^{3/2}	WS ₁₀ × MC	In(SFC)	Acc.	AIC	N.R ²	MC	FSG
7	-3.0923*	1.2611***	-0.39518***	-0.06588***	2.8324**	0.903	60.1	0.813	MC _{FFMC}	LCBH
8	-2.4341*	1.0449***	-0.37591***	-0.04869***	2.1943***	0.876	65.0	0.789	MC _{SA}	LCBH
10	-4.0204**	1.3514***	-0.43355***	-0.06881**	2.8906**	0.912	56.3	0.830	MC _{FFMC}	Adjusted
11	-3.5550**	1.4407***	-0.53211***	-0.07019***	2.4897*	0.920	55.2	0.835	MC _{SA}	Adjusted
SFC.CLS 2 SFC.CLS 3										
	β ₀	β ₁	β ₂	β ₃	β ₄	β ₅				
9	-4.6830**	1.3156***	-0.41448***	-0.06632**	1.6792 [†]	3.2814*	0.876	61.6	0.815	MC _{FFMC}
										Adjusted

Symbols β₀–β₅ represent intercept and coefficients for predictor terms as indicated (see Appendix I for abbreviations). FSG term refers to either live crown base height (LCBH) or adjusted fuel strata gap, as indicated. Residual degrees of freedom was 108 for all models except 107 for Model 9. Acc. is Accuracy (number correct out of total); AIC is Akaike's Information Criterion; and N.R² is Nagelkerke's R². Input type indicates the type of MC estimate and type of FSG used, either simple LCBH or adjusted (see Table 1).

*Models are in the form $p(\text{CFO}) = \frac{1}{1 + e^{-(\beta_0 + \beta_1 x_1 + \dots + \beta_n x_n)}}$ where p(CFO) is probability of crown fire occurrence (0–1), β₀–β_n are coefficients as shown in the table,

n = 4 (Models 7–11) or n = 5 (Model 9), and x₁–x_n represent estimated values of predictors WS₁₀, FSG^{3/2}, WS₁₀ × MC and In(SFC), respectively (models 7–11). For Model 9, x₄ and x₅ are dummy variables used for representing SFC classes 2 (SFC.CLS 2) and 3 (SFC.CLS 3) as follows: SFC class 1: x₄ = 0, x₅ = 0; class 2: x₄ = 1, x₅ = 0; class 3: x₄ = 0, x₅ = 1.

Asterisks represent significance levels: <0.001 (***)<0.01 (**); <0.05 (*); <0.1 (†).

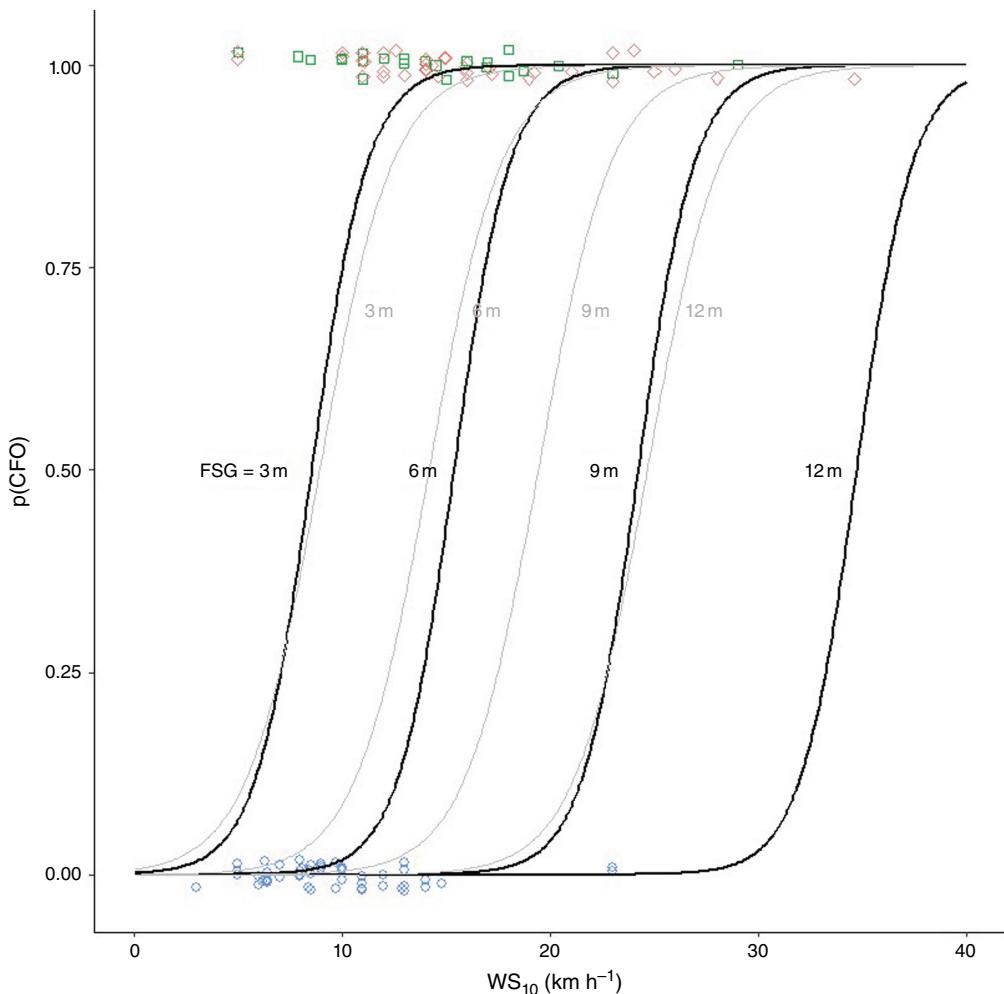


Fig. 3. Probability of crown fire occurrence using Model 11 ($p(\text{CFO})$, black lines) under varying open wind speed (WS_{10}) and Fuel Strata Gap (FSG) values. Calculation constants are surface fuel consumption = 1 kg m^{-2} and stand-adjusted moisture content = 10.0%. Fire observations (vertically jittered for clarity) are shown by type of fire: surface (blue circles); passive crown (green squares); or active crown (red diamonds). Grey lines show predicted probability values from previously published CFIS system LOGIT 1 model (Cruz et al. 2003; calculated using constant Fine Fuel Moisture Code of 90.8 and Drought Code of 200).

LOGIT 1 and 2 models across input levels is shown in the Supplementary Table S2. The distribution of observations is further illustrated in Fig. 4, in which all fire environment variables are displayed. Iso-lines representing the 50% probability level using Model 11 are shown for MC values of 6.0–15.0%, as indicated; these were calculated at SFC of 1.5 kg m^{-2} , close to the median and mean SFC values from all observations (1.42 and 1.57 kg m^{-2} , respectively).

Discussion

Updated and improved probability of crown fire occurrence models

Empirical and quasi-empirical fire behaviour models have typically been simple, aimed at operational use but

constrained by small sample sizes (Sullivan 2009). In attempting to improve the flexibility of crown fire occurrence models, we followed the successful approaches taken in the development of the FBP and CFIS system, using physical principles to guide modelling logic while respecting empirically fitted model terms and forms.

Based on our analysis, crown fires in live boreal and sub-boreal conifer forests can be correctly predicted about eight to nine times out of 10 using WS_{10} , MC, FSG and estimated SFC, at least within our described data range (Fig. 4) and assuming the inputs can be reliably estimated. Our final models used two to four of these predictors with various transformations and are applicable to level or gently undulating terrain. The full-featured Model 11 showed the best combination of performance and flexibility, using log-transformed SFC and incorporating ladder fuel influence

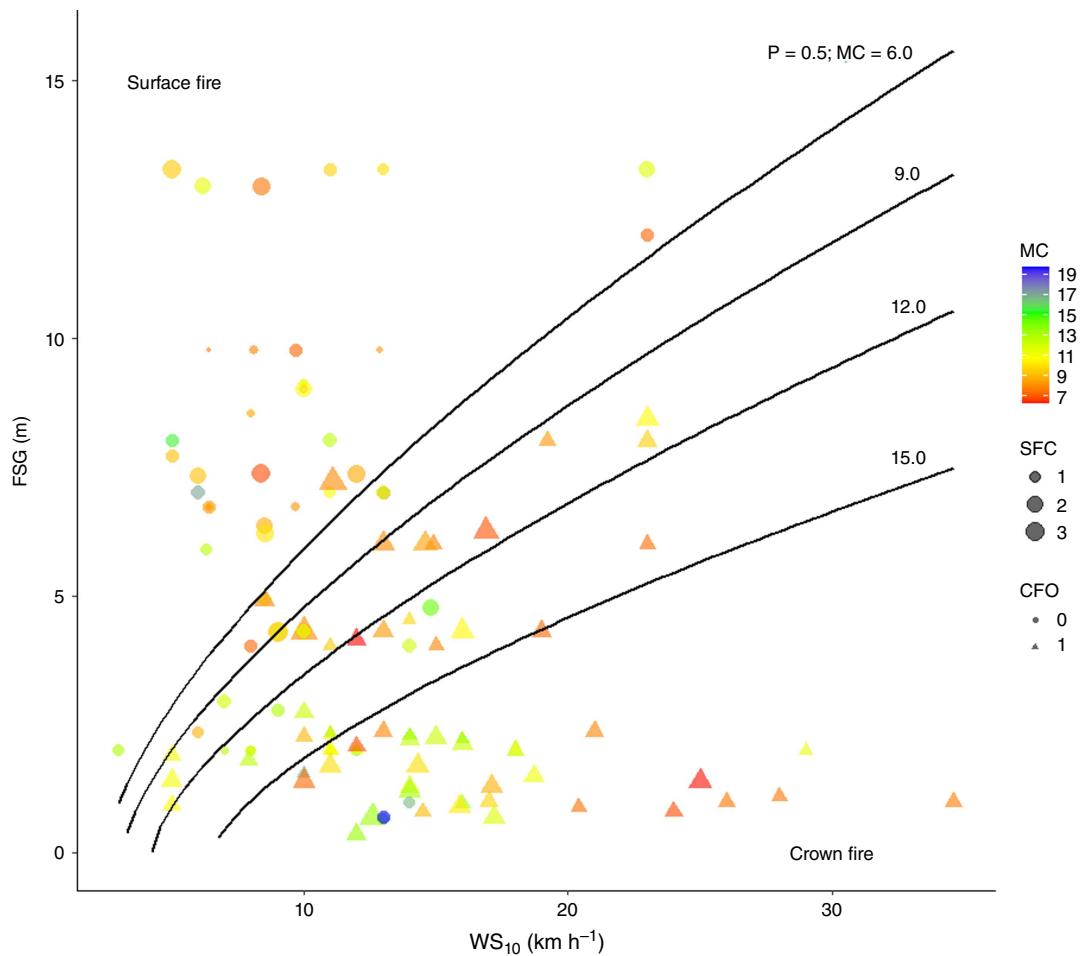


Fig. 4. Scatter plot of 113 fire observations by 10 m open wind speed (WS_{10}) and fuel strata gap (FSG, shown unadjusted). As indicated, symbol sizes represent values of surface fuel consumption (SFC, $kg\ m^{-2}$), colours indicate estimated dead fine fuel moisture content (MC, %) and shapes depict crown fire occurrence (1, triangles) or absence (i.e. surface fire; 0, circles). Iso-lines represent $P = 0.5$ for crown fire initiation based on Model 11 at various indicated stand-adjusted MC values (6–15%), calculated at $SFC = 1.5\ kg\ m^{-2}$. Observation space below and right of isolines represents crown fire behaviour, and observation space above and to the left of the lines represents surface fire behaviour.

on the onset of crowning via the logical (albeit subjective) adjustments on FSG values. Model 11 retains the 3/2 power function associated with FSG as originally conceived by Van Wagner (1977), based on physical principles related to flame height (Lee and Emmons 1961; Thomas 1963). It was encouraging to see how the empirical results from our study confirm this relationship despite its simplicity.

When predictors have conflicting influences on fire behaviour, outcomes become more uncertain, such as in the case of high WS_{10} –MC conditions. The interaction term ($WS_{10} \times MC_{SA}$ or $WS_{10} \times MC_{FFMC}$) in Models 5–12 helps avoid overprediction of crown fire occurrence in such cases. For instance, under WS_{10} of 30–40 $km\ h^{-1}$ and high fine fuel moisture content ($MC_{SA} = 20$ –25%, or FFMC

78–82), a main effects-only model such as Model 3 from this study or the LOGIT 1 model of Cruz *et al.* (2003) would predict a very high probability of crowning (Model 3: $P = 0.9981$; LOGIT 1: $P = 0.9978$ for an FFMC of 82, WS_{10} of 35 $km\ h^{-1}$ and FWI System Drought Code (DC) component of 100) with mid-range values for other predictors ($LCBH/FSG = 4.0$, $SFC = 1.0\ kg\ m^{-2}$).² Using these same predictors with Models 10 or 11 suggests a very low chance of crowning ($P < 0.005$ for both), a consequence of the interaction factor suppressing the crowning probability as MC values approach extinction levels. Although experimental fire data under such conditions are lacking, the closest comparable fires in our database suggest marginal conditions for ignition and negligible crown fire risk. The

²The standard FFMC model predicts litter moisture of 19.8% for an FFMC of 82. A nearly identical MC_{SA} would be predicted to occur under the following conditions (as per Wotton and Beverly 2007): FFMC 82, DMC 38, pine stand type, moderate stand density, and SU season.

highest MC observation in our database (BFL, plot 6: FFMC of 80, $MC_{SA} = 19.8\%$) was associated with a surface fire with a WS_{10} of 13 km h^{-1} , FSG of 0.7 m and SFC of 1.2 kg m^{-2} (M. E. Alexander, unpubl. data). Ignition attempts under high moisture conditions failed at several other experimental study sites (e.g. FFMC 84, $MC_{SA} = 15.3\%$ at DL; Quintilio *et al.* 1977; see also Stocks 1987a; Stocks 1989).

Wind speed and canopy influence

The role of wind in fire behaviour is complex, with various interactions and feedbacks between wind and other fire environment elements occurring at multiple scales (Finney *et al.* 2021). Wind speed has long been known to control ROS (Potter 2012) in surface fire (Rothermel 1972; Nelson and Adkins 1988) and crown fire behaviour models (Rothermel 1991; Alexander and Cruz 2016; Cruz and Alexander 2019). Wind speed remains the most significant variable in our modelling of crown fire occurrence. Our simplest model form (Model A), based only on WS_{10} and LCBH, correctly predicted crown fire occurrence in over 80% of cases during our cross-validation analysis, along with nearly all cases of upper canopy fuel involvement in two-layered stands (see Appendix 2).

Wind speed in experimental fires was measured with anemometers in a cleared opening at a standard 10-m height (Lawson and Armitage 2008). The windward-exposed edges of experimental plots may have had drier and windier conditions compared with plot interiors (Chen *et al.* 1999). The line ignition protocol ensured that after the initial 20–30 m, fires were spreading through the plot at a pseudo-equilibrium with environmental conditions. This ensured that the natural fire acceleration process (McAlpine and Wakimoto 1991), where point-source fires have documented delays of 10–90 min or longer to reach equilibrium conditions (Lawson 1972; Kii 1975; Alexander *et al.* 1991; McRae *et al.* 2017), was bypassed. The suggested interpretation is that the present models (as with the FBP or CFIS systems) will therefore be most accurate for predicting the probability of crown fire occurrence from an established equilibrium surface or crown fire ignition source exposed to ambient conditions. These models do not predict crowning during fire acceleration and are not intended for point-source ignition fires in sheltered locations.

Foliar moisture content

FMC was not a significant predictor of crown fire occurrence in our final models, matching the previous findings of Cruz *et al.* (2004, 2006) and Stocks *et al.* (2004). FMC appears influential in the ignition of conifer foliage in a physical sense (Fazeli *et al.* 2022; Melnik *et al.* 2022; but see Alexander and Cruz 2013). However, in our analysis, FMC was significantly correlated to other variables in our dataset (e.g. WS_{10} , FSG), and as such had minimal explanatory

power. Experimental measurement of FMC was also absent in many studies, requiring the use of imprecise regional interpolation curves (Chrosiewicz 1986) or the model in the FBP System for estimating FMC on the basis of calendar date, latitude/longitude and elevation (Forestry Canada Fire Danger Group 1992). Although Van Wagner's (1977) crown fire initiation model suggests that realistic FMC differences could affect critical FSG values by 2.0 m or more (Keyes 2006), recent studies have noted differences in the seasonality of live conifer tissue flammability compared with FBP System predictions (Melnik *et al.* 2022) and have called for improved methods of estimation.

Despite the convenience of a pan-specific 'spring dip' in foliar moisture causing heightened crown fire hazard (Van Wagner 1974b), the flammability of conifer foliage appears related to multiple physiological variables, including moisture, particle density and phenology (Jolly *et al.* 2016), as well as species (Russell and Turner 1975; Keyes 2006). The effects of severe drought (Peng *et al.* 2011) are also not well captured in our dataset and may affect the FMC levels. Although FMC minima in conifers are generally associated with phenology rather than moisture availability (Kozlowski and Clausen 1965; Chrosiewicz 1986; Jolly *et al.* 2016), severe drought may also impact the timing and amplitude of seasonal FMC variation in unforeseen ways.

Aside from flammability, other factors could affect the FMC signal on the ignition of the foliage above a surface fire. Factors such as the surface fire's upward heat flux or the contribution of bark fuels (for some species) might confound the FMC effect on crowning. Cruz *et al.* (2006) found through explicit heat transfer modelling that the increase in time to foliar ignition due to elevated FMC was small compared with the surface fire residence time (Alexander 1998). Therefore, although heightened FMC could delay ignition, canopy fuels will still tend to ignite when high-intensity surface fire passes under them. The binary, in contrast to continuous, response of the process being studied makes it difficult to observe and isolate the effect.

Stand-adjusted fine dead moisture content

The MC of fine forest floor litter has long been known to be a key variable influencing fire behaviour (Van Wagner 1968; Dimitrakopoulos and Papaioannou 2001). Our results showed that the FFMC, an index based on weather conditions alone, remains a significant predictor of crown fire initiation in a variety of conifer forests. Given the large dataset behind the MC_{SA} model (Wotton and Beverly 2007) and that previous studies identified significant over-storey influence on MC and fire behaviour (Rothermel *et al.* 1986; Tanskanen *et al.* 2005), we expected that models using the MC_{SA} might perform better than those using FFMC alone. Final results were generally supportive: the best overall performance was Model 11, which used the MC_{SA} along with the adjusted FSG. However, FFMC-based

models performed nearly as well, and Model 7 was superior to the MC_{SA}-based Model 8 using the unadjusted LCBH (Table 2). It is logical that an FFMC-based model should outperform one using MC_{SA} at sites using a base LCBH. In dense stands such as SC-IM, incorporating stand density influence on crown fire occurrence (by using the MC_{SA}) but not the effect of ladder fuels creates a bias, where moisture is assumed to be higher due to stand structure but potential ladder fuel effects are ignored. This reduced the accuracy of certain marginal predictions compared with the approach of combining both stand density (via MC_{SA}) and ladder fuel (via adjusted FSG) influences in Model 11. Thus, Wotton and Beverly's (2007) model for estimating MC_{SA} appears to have some skill in the right context, though a stand-adjusted model with more quantitatively defined predictors would be superior and less subjective to apply. See also Supplementary Material for additional cautions and suggestions for future use of the MC_{SA} model.

Surface fuel consumption

SFC, including contributions from all fine surface fuel load (SFL) elements, is a required input with the present equations. This adds an element of uncertainty, because actual consumption values are never available prior to burning; even the relevant inputs to fuel consumption models, such as SFL, will rarely be on hand in wildfire situations, for instance. A number of tools presently exist for estimating SFC. The simplest of these are probably the FBP System equations that require only the BUI and (or) FFMC and fuel type as inputs, with fixed SFL values (ranging from 1.5 to 5 kg m⁻²) hard-coded into the fuel consumption equations (Forestry Canada Fire Danger Group 1992). The more comprehensive studies from the FBP System era include site-specific SFC models based on selected FWI System components and SFL (Van Wagner 1972; Stocks 1987a, 1989; Alexander et al. 1991). The forest floor consumption models of de Groot et al. (2009), including data from several sites in the present study (based on the SFL and various FWI System components), offer additional practical and logically consistent options.

It bears mentioning that SFC models will be most accurate when surface fuel conditions match the input data, those being surface fuels characteristic of unmanaged or thinned boreal and sub-boreal conifer forests, featuring moderately compact needle litter, compact duff layers and relatively smaller contributions of dead-down woody fuels. Higher SFC values in our dataset ($>\sim 2.5 \text{ kg m}^{-2}$) were typically associated with thicker forest floor loads as well as drier conditions due to elevated BUI levels. Although this fuel consumption likely contributes to surface fire intensity, and thereby crowning (Van Wagner 1977), the relationship between SFC and CFO may not be linear. In our analysis, log-transformed SFC models were slightly more accurate than comparable linear SFC models (e.g. models 5 or 6 vs

models 7 or 8; Table 2), effectively muting the influence of a high SFC in certain situations. Significantly different fuelbed types, including those with higher woody debris loads (Agee and Huff 1987) or masticated fuels (Moore et al. 2020) would likely require calibration to produce credible results.

Canopy structure

Van Wagner's (1977) concept of the canopy fuel layer consisted of 'a layer of uniform bulk density and height above ground' (p. 23) and noted in his field experiments that the critical surface intensity for onset of crowning occurred when the surface fire produced a flame front 'whose tip is just reaching into the crown layer' (p. 25). Further studies have suggested that flame tips do not need to actually contact the crown base for crown fire initiation to occur (Alexander and Cruz 2012), with time-temperature curves and net energy release being more representative of the canopy ignition process (Xanthopoulos and Wakimoto 1993; Cruz et al. 2006; Melnik et al. 2022). The image of a surface fire flame height reaching the vicinity of the lower live canopy remains useful for visualising crown fire initiation (Alexander and Cruz 2016), although it may exaggerate the critical surface fire intensity needed for crown fire to occur.

For conifer stands with multi-layered canopy fuel structure, our models more explicitly defined the onset of crowning; further vertical propagation may be inferred but is not assured. The biggest difference between the present analysis and previous empirically based crown fire occurrence models (Cruz et al. 2003, 2004) is the use of the 3/2 exponent for the FSG/LCBH term, which leads to higher crowning thresholds as the FSG increases (Fig. 3). This aligns with the findings of McCaffrey (1979), who found the relationship between temperature change and height (z) above a pulsing flame in laboratory studies varied from z^{-1} to $z^{-5/3}$ depending on the plume region in question. In all cases, models with the 3/2 exponent performed better than comparable model forms with either linear or squared FSG terms (Table 2). Values of LCBH or FSG used in our analysis represented the mean stratum values at the stand or plot level. Variability in LCBH is clearly important in crown fire initiation and defining crown fire thresholds (Parsons et al. 2011), but the varied nature of the LCBH data precluded studying the effects of LCBH variability in our analyses. Previous studies that combined alternative LCBH definitions with Van Wagner's (1977) model resulted in significant underprediction bias (Cruz and Alexander 2010).

Ladder fuels remain a significant challenge in the development of accurate crown fire occurrence models. Our use of an adjusted FSG based on dead ladder fuels appears to have improved model performance slightly but still offers uncertain guidance. Users of these models are advised to estimate the FSG as lower than the LCBH when dense fine-textured biomass exists in the sub-canopy space that visibly contributes to vertical fuel connectivity. Future analyses are

anticipated to provide additional methods to quantify this process more directly.

Management considerations and conclusion

After six decades of progress, the experimental fire database contains a sufficient number and range of observations to support relatively sophisticated statistical models of crown fire occurrence. Users can select from the various models presented (Table 3) depending on the level of detail of their input data. For instance, for general use in a typical moderately closed conifer stand, FFMC-based models may be adequate, whereas MC_{SA}-based models may be more flexible when considering different stand conditions, such as very open stands or comparisons across seasons. For further details, see Supplementary Table S2 for a comparison of crown fire probability predictions among models under a range of input conditions.

Despite the range of our database (FSG 0.4–13.3 m; MC 6.3–19.8%; SFC 0.2–3.8 kg m⁻²; WS₁₀ 3.0–34.6 km h⁻¹), certain conditions have yet to be captured within the four-dimensional variable space (Fig. 4). Obvious data gaps include fires in high-FSG stands (>6.0 m) under high to extreme fire danger conditions (e.g. WS₁₀ > 15 km h⁻¹, FFMC > 90), observations that will also be relevant to planning effective hazard reduction treatments (Agee and Skinner 2005; Beverly et al. 2020). Fire behaviour observations in extreme conditions will likely only be obtained from detailed wildfire monitoring (Hart et al. 2021), typically through collaboration with fire management organisations. Although there is potential to recover fuel structure for wildfires in areas with LIDAR coverage, obtaining high-quality wind speed and fuel consumption data will continue to be problematic, suggesting that field-scale fire behaviour experiments will still be required.

Changes in fine fuel moisture dynamics and in-stand microclimate caused by fuel treatments (Ma et al. 2010) have often been ignored (Varner and Keyes 2009). This is only partially addressed in our models thanks to the MC_{SA} model. Along with FMC, the influence of conifer species is also unresolved. Although pine and spruce forests comprise most of the Canadian boreal biome, additional tests and evaluation seem warranted in other temperate forests in Canada and worldwide, where other conifer genera are often dominant.

Compared with previous studies using Canadian experimental fire behaviour data (Forestry Canada Fire Danger Group 1992; Cruz et al. 2003, 2004), the present analysis used a greater number of continuous predictors. This may have improved the overall predictive accuracy but requires users to have more detailed inputs. The present models also defined crowning differently from previous studies, at least for multi-layered stands, where crowning is only properly considered for the lowest LCBH or FSG layer. The original CFIS system models (Alexander et al. 2006) will remain useful for more general predictions of crown fire occurrence encompassing full canopy involvement and combined LCBH

values in multi-layered stands. As discussed in Appendix 2, the present models and approach may also prove useful for predicting transitions between canopy strata in two-layered stands, but further studies and testing will be required. Our results show continued improvement in crown fire occurrence modelling using experimental data. Such models can be expected to be further refined with time.

Supplemental material

Supplementary material is available online.

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Data availability. The data that support this study will be shared upon reasonable request to the corresponding author. Plans are in place to store all experimental burning data conducted by the Canadian Forest Service in a public data repository by 2025.

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Appendix I. List of abbreviations and acronyms.

Table A1. Summary of abbreviations used in the main text, tables and figures.

Abbreviation	Units or levels	Definition	Source ^A
BFL	—	Big Fish Lake (experiment site, Ontario)	1
BS	—	Black Spruce (<i>Picea mariana</i>)	1, 17
BUI	—	Buildup Index (Fire Weather Index System)	2
CF	—	Crown Fire	This study, 8
CFIS	—	Crown Fire Initiation and Spread (system)	3, 4
CFO	0 or 1	Crown Fire Occurrence	This study, 4
DBH	cm	Diameter at Breast Height	
DC	—	Drought Code (Fire Weather Index System)	2
DL	—	Darwin Lake (experiment site, Alberta)	5
DMC	—	Duff Moisture Code (Fire Weather Index System)	2
FBP	—	Fire Behaviour Prediction (System)	1
FFMC	—	Fine Fuel Moisture Code (Fire Weather Index System)	2
FMC	%	Foliar Moisture Content (live conifer)	1, 8
FSG	m	Fuel Strata Gap	4
FWI	—	Fire Weather Index (index or System)	2
ICFME	—	International Crown Fire Modelling Experiment (exp. site, Northwest Territories)	6
JP	—	Jack Pine (<i>Pinus banksiana</i>)	7, 13
KL	—	Kenshoe Lake (experiment site, Ontario)	7
LCBH	m	Live Crown (or canopy) Base Height	8
LP	—	Lodgepole Pine (<i>Pinus contorta</i>)	1, 12
MC	%	Moisture Content, fine dead litter	9, 10
MCC	—	Matthews Correlation Coefficient	11
MC _{FFMC}	%	Moisture Content estimate, fine dead litter, from the FFMC; also MC.FFMC	9

(Continued on next page)

Table A1. (Continued)

Abbreviation	Units or levels	Definition	Source ^A
MC _{SA}	%	Stand-Adjusted Moisture Content estimate, fine dead litter	10
PG	—	Prince George (or Summit Lake; experiment site, British Columbia)	12
PL	—	Porter Lake (experiment site, Northwest Territories)	16
PM	—	Pelican Mountain (experiment site, Alberta)	17
PNFI	—	Petawawa National Forestry Institute (experiment site, Ontario)	1
ROS	m/min	Rate of Spread	1
RP	—	Red Pine (<i>Pinus resinosa</i>)	1, 18
SC-IM	—	Sharpsand Creek (experiment site, Ontario), Immature plots	13
SC-SM	—	Sharpsand Creek (experiment site, Ontario), Semi-Mature plots	14
SC-TH	—	Sharpsand Creek (experiment site, Ontario), Thinned plots	13
SF	—	Surface Fire	This study, 8
SFC	kg/m ²	Surface Fuel Consumption	1, 8
SFC.CLS	1, 2, or 3	Surface Fuel Consumption Class; classes are 0–0.99, 1.0–2.0, >2.0 kg m ⁻²	This study, 4
SFL	kg m ⁻²	Surface Fuel Load	1
WWRP	—	White (<i>Pinus strobus</i>) and Red Pine (<i>P. resinosa</i>) species mix	1
WS ₁₀	km h ⁻¹	10 m open wind speed	15

^ASources: 1: Forestry Canada Fire Danger Group (1992); 2: Van Wagner (1987); 3: Cruz et al. (2003); 4: Cruz et al. (2004); 5: Quintilio et al. (1977); 6: Alexander et al. (2004), Stocks et al. (2004); 7: Stocks 1989; 8: Van Wagner (1977); 9: Van Wagner (1974a); 10: Wotton and Beverly (2007); 11: Chicco and Jurman (2020); 12: Lawson (1972); 13: Stocks (1987a); 14: McRae et al. (2017); 15: Lawson and Armitage (2008); 16: Alexander et al. (1991); 17: Thompson et al. (2020); 18: Van Wagner (1968). See main text for full references.

Appendix 2. Upper stratum crowning in two-layered stands

As discussed in the main text, two sites in our dataset had clearly defined dual-layer stands with black spruce in the understorey and mid-storey beneath an upper overstorey of jack pine. These included the KL site (Fig. 1e) and most plots at the ICFME site (Fig. 1g).³ In contrast to previous analyses (e.g. Van Wagner 1993; Cruz et al. 2004), we treated the crowning process separately between these two strata. The main modelling in our study considered only the crown involvement of the mid-canopy black spruce at both sites, the lower layer proximal to the surface fuel layer.

For testing upper canopy fuel involvement, a conditional process was evaluated. Experimental plots at KL and ICFME predicted to involve crowning into the spruce layer were subsequently tested for crowning into the upper pine stratum. This was clearly a different process than that intended by the traditional notion of crown fire initiation models, with a surface fire testing the overall LCBH or FSG (Van Wagner 1977; Scott and Reinhardt 2001). However, we wished to explore whether there might be merit to using empirically based crown fire occurrence models to predict vertical flame transitioning between canopy strata.

To do this, a first assumption was made that the heat flux for upper canopy involvement originated from the crown centroid (C_S) of the mid-storey spruce stratum:

$$C_S = \text{LCBH}_S + (H_S - \text{LCBH}_S)/2 \quad (\text{A1})$$

where H_S and LCBH_S represent the mean spruce stratum height and spruce LCBH, respectively. The stratum gap between fuel layers would then be defined as

$$\text{FSG}_{SP} = \text{LCBH}_P - C_S \quad (\text{A2})$$

where FSG_{SP} is the mean spruce-pine FSG and LCBH_P is the pine live crown base height. The relevant plot-level measures were calculated from stand data for the ICFME (Alexander et al. 2004) and sites (see Supplementary Material). Because most

³ICFME plots 3 and 4 had no mid-storey black spruce layer (Alexander et al. 2004) and are therefore excluded from this discussion.

of the described empirical models also require estimates of SFC, which is undefined in this context, this was only intended as an exploratory analysis at the present. We selected mid-range values of SFC as necessary and used measured or estimated values for other variables (WS_{10} and MC_{SA} or MC_{FFMC}).

Stand calculations gave mean FSG_{SP} values of 5.7 m (range: 4.8–6.5 m) at KL and 4.3 m (range: 2.5–5.8 m) for ICFME plots. Using Model 11 with a mid-range SFC value (1.5 kg m^{-2} ; between median and mean values of 1.42 and 1.57 kg m^{-2} , respectively) along with actual MC_{SA} values (6.3–13.5%), crown fire occurrence was correctly predicted in 14 of 15 observations (i.e. 93% correct). Similar results (14/15 correct) were obtained using Model 9, with SFC class 2 (1.0–1.99 kg m^{-2}) along with actual MC_{FFMC} values (i.e. 6.5–13.5%). The two models requiring no fuel consumption estimates (Models A and B) also gave identical results, using WS_{10} and FSG_{SP} alone (A) or WS , FSG_{SP} and MC_{FFMC} (B). In all cases, the only misclassified fire was ICFME Plot 2, a passive crown fire involving the full canopy spruce and pine layers; this burn was otherwise notable for its relatively low WS_{10} (7.9 km h^{-1}) and FFMC (89.5) values for an intense crown fire involving the full canopy.

This cursory exploration of upper canopy crowning showed that such crown fire occurrence models may have the potential to help predict crown fire transitions in vertically complex stands, by adopting a conditional process of evaluating one stratum at a time. This process involves making several significant assumptions that will require further study and testing. These include vertical fuel continuity and flame propagation through the mid-canopy stratum (in our case, from the LCBHs to the C_S and higher), as well as the assumption that variables such as WS_{10} and MC can be applied unchanged to elevated fuel strata. The greatest uncertainty is probably associated with the arbitrarily assigned SFC value (in Models 10 and 11), which, if it can be applied to upper crowning at all, should properly reflect heat flux contributions from both surface (dead, compact) and lower canopy (live, aerated) fuels. With such a small and unbalanced dataset (15 observations, with only three cases of upper CFI failure), additional observations and studies are clearly warranted to further inform this type of analysis.

Supplementary Material

Improved logistic models of crown fire probability in Canadian conifer forests

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Canadian experimental burn sites: Estimates of live crown base height, foliar moisture content, and other details

This document contains additional background information on the Canadian experimental burning experiments and data used to calculate or estimate live crown base height (LCBH), foliar moisture content (FMC), and other variables for crown fire modelling purposes. Experimental fires were carried out in natural stands of black spruce (*Picea mariana* (Mill.) B.S.P.) and jack pine (*Pinus banksiana* Lamb.), and to a lesser extent red pine (*Pinus resinosa* Ait.)–white pine (*Pinus strobus* L.) and lodgepole pine (*Pinus contorta* var. *latifolia* Engelm. Dougl. ex Loud.), as well as red pine plantations.

Sampling intensity and transparency of LCBH values increased over time in the various fire experiments comprising our database. At the earliest sites, little information was available and crown ratio (CR) modelling based on overall stand metrics appeared to be the only option for estimating LCBH. Starting in the mid-1970's, some measure of variation between plots was typically available, with either individual plot mean LCBH values (mostly previously published), or measures from a small sample (e.g. 10-30 trees) of biomass trees of different sizes produced for estimating diameter at breast height (DBH)–height and CR relationships; these relationships could then be applied to experimental plots. Later experimental burning projects typically featured more detailed fuel sampling (e.g. at the International Crown Fire Modelling Experiment, ICFME; Alexander *et al.* 2004), though not in all cases.

The sites described here with previously-unpublished LCBH estimates are from Sharpsand Creek (immature and thinned plots), Kenshoe Lake (pine stratum and spruce-pine fuel strata gap (FSG_{SP}) only), and the Petawawa National Forest Institute (PNFI: jack pine and red/white pine) in Ontario; and Darwin Lake, Big Fish Lake, and Pelican Mountain sites in

Alberta. Additionally, values at ICFME were calculated differently than in past analyses. At the remaining sites, LCBH values were unchanged from values reported in the original sources.

At the Sharpsand Creek site, raw cruise data were available for immature (SC-IM) and thinning treatment (SC-TH) plots based on earlier sampling (Walker and Stocks 1975), allowing for a fresh analysis of crown fuel structure. Analysis of plot density values revealed one clear outlier among the SC-TH plots, with much higher live (8380 ha^{-1}) and dead (6875 ha^{-1}) density compared with other thinned plots; these values were in the range of the SC-IM plots (live density: $6424\text{--}13\,928 \text{ ha}^{-1}$; dead density: $5032\text{--}13\,164 \text{ ha}^{-1}$). This plot (number 16) was therefore suspected to have been only partially or incompletely thinned and was assigned to the SC-IM treatment for analysis purposes. Overall, immature plots had mean values of 9213 and 9971 live and dead stems ha^{-1} , respectively, while the comparable values for SC-TH plots were 4725 live and 1175 dead stems ha^{-1} ; both differences were highly significant between treatments (Welch's t-test, $p < 0.001$ for both live and dead stems). The biomass trees from the same study (Walker and Stocks 1975) were also reanalyzed to examine CR values. CR varied slightly by DBH, and was modelled as a linear function as follows:

$$\text{CR} = 0.3705 + 0.009196 \cdot \text{DBH} \quad (\text{S1}),$$

and deemed marginally significant ($p=0.0747$); this gave estimated CR values of 0.39-0.48 for trees with DBH values from 2-12 cm.

We then calibrated an Ontario-based mixed-effects model (Sharma and Parton 2007) for describing tree heights and CR for jack pine based on density and basal area, with a random effect for site quality. We used this model to produce new height estimates for live and dead cohorts and LCBH for live SC-IM trees. Together with the estimated CR values, this produced

the DBH-LCBH model shown in Figure S1. This was used together with the cruise data to estimate plot-level LCBH estimates for the SC-IM plots.

Unfortunately, raw plot-level data from the SC-SM plots could not be found; consequently, all SC-SM plots were assumed to have the an LCBH value of 5.3 m (McRae *et al.* 2017).

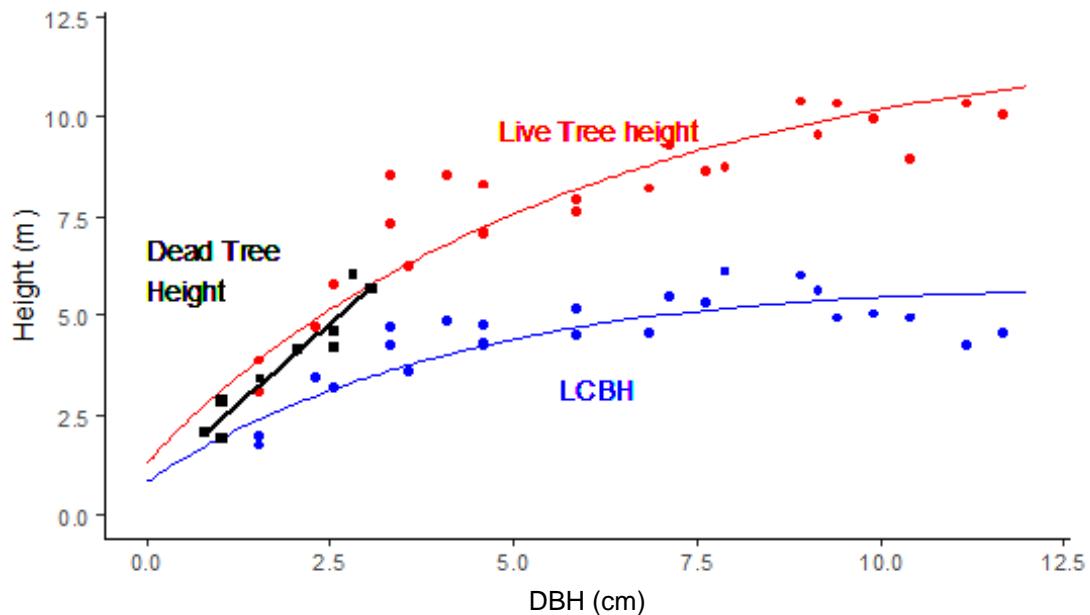


Figure S1. Biomass tree data and models from Sharpsand Creek jack pine: height-DBH data and model (red), LCBH data and model (blue); and dead tree data and linear fit (black). For estimating dead tree height, the linear model was used for DBH < 3 cm and the live tree height model was used for DBH ≥ 3 cm.

For the SC-TH plots, no cruise data (DBH) was located for two of the five plots. Furthermore, the DBH-height (and CR) relationship from the SC-IM biomass trees could not be assumed to hold. Pre-commercial thinning treatments in jack pine are known to cause radial growth compared to controls (Zhang *et al.* 2006) and can also alter crown recession rate and CR

(Morris *et al.* 1994). In the absence of a credible model for LCBH in thinning treatments, we used the mean SC-IM plot value (4.28 m) for SC-TH plots.

One additional adjustment was made to the Sharpsand Creek plot data based on time of burning. The SC-IM and SC-TH plots were burned between 1974-1976 and 1981, while SC-SM plots were burned from 1988-1991. Stand measurements occurred in 1974 (for IM and TH plots), and again in 1984 (for SC-SM). As noted by McRae *et al.* (2017), significant stand changes had occurred over the decade between measurements, with >50% reductions in live and dead stand density and a 1.0 m increase in LCBH (i.e. from 4.28 m to 5.3 m). Therefore, the latest SC-TH and SC-IM burns occurred halfway between measurements. To compensate for this, 0.5 m (half of the mean difference) was added to the estimated LCBH of the four plots burned in 1981 (i.e. 2 each of the SC-IM and SC-TH plots).

Foliar moisture content (FMC) for all Sharpsand Creek plots was estimated using the FBP System equations based on calendar date, elevation and latitude/longitude (Forestry Canada Fire Danger Group 1992; hereafter FCFDG 1992).

Surface fuel consumption (SFC) values were missing for the SC-SM plot files, though total fuel consumption (TFC) and depth of burn values were reported (McRae *et al.* 2017). In order to estimate SFC in line with the remaining observations, we subtracted estimated crown fuel consumption (CFC) values from reported TFC (as per FCFDG 1992). Mean reported CFC values in the SC-IM and SC-TH plots were grouped by type of fire (Stocks 1987; unpublished data files). SC-SM TFC values were therefore reduced by 0.02, 0.39, and 1.14 kg m⁻², for surface, passive crown (or ‘torching’), and active crown fires, respectively. For the two observations with fire behaviour described as ‘some torching’, we estimated CFC as the mean of

the first two categories (surface and passive crown) or in other words 0.20 kg m^{-2} . This gave overall SFC estimates of $1.4\text{--}3.6 \text{ kg m}^{-2}$.

At the Kenshoe Lake site, a similar process was used for LCBH on the jack pine data (used for the upper crowning analysis). The local biomass tree data was used once again to calibrate Sharma and Parton (2007)'s DBH-height model, with parameters and biomass data for black spruce and jack pine calculated separately. For the pine cohorts, CR values were not significantly different across size classes ($p = 0.336$), so a constant CR of 0.34 was assumed. With the DBH-height model and constant CR, new pine LCBH estimates were calculated, which ranged from 10.2-11.0 m. As noted in the main text, the LCBH for spruce layer was not measured, but estimated to be 2.0 m for all plots. Together with new spruce cohort mean height estimates of 5.4-7.8 m, this gave black spruce crown centroid heights estimates of 3.4-5.8 m and FSG_{SP} estimates of 4.8-6.5 m (see main text, Appendix II for additional information). FMC estimates at Kenshoe Lake were based on the FBP System equations (FCFDG 1992).

At the Big Fish Lake site, unpublished plot-level LCBH measurements were made available for 8 of the 9 experimental fires (M. E. Alexander, research coordinator for the experimental burning project). These were based on sampling of trees directly across from the fireguards surrounding each plot; this was done to avoid trampling the sensitive surface fuelbeds inside the plot perimeters. The resulting LCBH plot values ranged from 0.36–1.29 m, based on samples from 55–221 trees per plot. LCBH for the only unsampled plot was estimated as the mean value (i.e. 0.96 m) of the other eight plot averages. FMC estimates at Big Fish Lake were derived from the FBP System equations (FCFDG 1992). LCBH and FMC values at other associated black spruce experimental burning sites were provided or estimated from the original sources (Kiil 1975; Newstead and Alexander 1983).

At the Darwin Lake site, two distinct stand types were described, with similar basal area but differing stand height, age and density (Quintilio *et al.* 1977). Overstory data on tree heights and LCBH were sparse, with a biomass tree sample (later published in Alexander *et al.* 1991) lacking in data from larger trees. We estimated height and DBH values from three additional dominant trees based on photos presented in Alexander and de Groot (1988) to add to the biomass sample; we then fitted a simple log-model to these data to estimate an overall DBH-height relationship (Fig. S2). In the biomass sample, the slope of the DBH–CR relationship was not significantly different from zero ($p > 0.1$), suggesting a constant CR of about 0.54. Using this biomass model with the plot data resulted in new LCBH estimates from 4.75–6.21 m. FMC at Darwin Lake was estimated using the FBP System equations (FCFDG 1992).

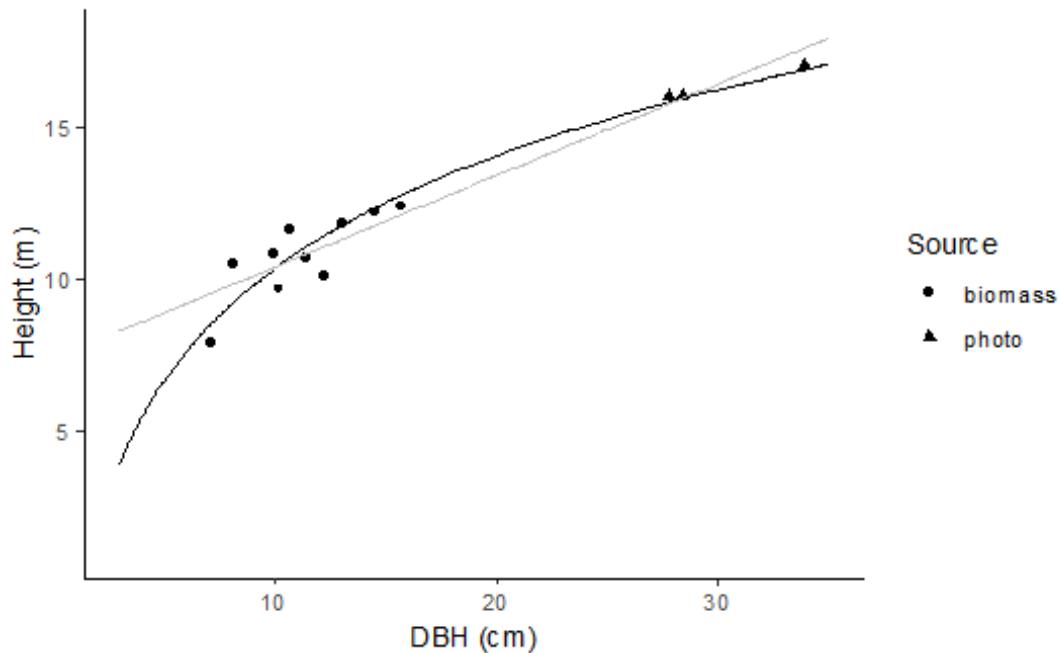


Figure S2. Fitted DBH-height relationship for overstory jack pine trees at Darwin Lake, Alberta, showing observations from the published biomass trees along with three additions based on scaling from photographs. The log-model performed slightly better (black; $R^2=0.931$) and was believed to be more realistic than a linear model (gray; $R^2=0.917$) for representing the DBH-height relationship; consequently the log-model was used to estimate tree heights in experimental fire plots.

The PNFI establishment (formerly the Petawawa Forest Experiment Station), west of Ottawa, Ontario, was the site of the earliest field experiments on fire behaviour in pine stands (e.g., Van Wagner 1963; 1965). The 1960's era jack pine experimental fires conducted by C. E. Van Wagner were later documented by Hummel (1979) and Weber *et al.* (1987) in a related fire effects study. We used Hummel's (1979) stand data and reconstructions with McAlpine and Hobbs' (1994) locally-calibrated model to estimate plot-level LCBH values based on stand density and basal area. This resulted in five new LCBH estimates for PNFI jack pine plots, ranging from 7.33–9.12 m.

For the PNFI red and white pine stands, no previous LCBH measures were ever formally published, though the FBP System documentation suggested a fixed LCBH value of 18 m for the C-5 fuel type (FCFDG 1992). Stand data was published for the various experimental blocks along with the results from earlier experimental fires (Van Wagner 1963). We used Holdaway's (1988) models from Wisconsin, USA to calculate CR values for these stands, providing for admittedly crude estimates. Together with published stand height values (14.6–25.0 m), this resulted in new LCBH estimates for the PNFI red and white pine stands of 7.4 m–13.3 m. FMC values for all PNFI red and white pine stands were interpolated from local species-specific seasonal curves (Van Wagner 1967).

Experimental fires in red pine plantations at PNFI were also conducted and documented by Van Wagner (1968, 1977), with additional insights documented in later reports (e.g. Van Wagner 1986). Field-scale experimental fires carried out between 1962 and 1967 were conducted in late spring through summer conditions. Mean stand attributes, including LCBH values, were provided in these reports, though no sampling details were provided. The described ranges suggest that some stand-wide sampling was conducted. Stem and canopy fuel densities

were high in these stands (FCFDG 1992). FMC values were estimated from locally-derived seasonal FMC curves (Van Wagner 1967).

At the Pelican Mountain experimental burning site, most of the necessary inputs involved in crown fire modelling were documented and reported on by Thompson *et al.* (2020), with the exception of LCBH. Mean overstory (black spruce) LCBH values were obtained for the control (2.08 m) and thinned (4.15 m) plots from G. A. Marshall (personal communication, April 2022). FMC was estimated and reported in the study (Thompson *et al.* 2020) using the FBP System equations (FCFDG 1992).

At the ICFME site, detailed fuel structure surveys were previously published in various tables (Alexander *et al.* 2004). The only difference from previous analyses was the change from using the ‘combined’ black spruce-jack pine LCBH value to using individual values for overstory spruce and pine cohorts (Alexander *et al.* 2004, Table 12).¹ The overstory spruce had LCBH values of 0.7–2.4 m, while pine cohorts (used for estimating upper canopy crowning) had LCBH values of 3.6–8.2 m. Combined with spruce crown depth plot measurements, this gave spruce crown centroid estimates of 2.7–4.3 m and spruce-pine fuel strata gap (FSG_{SP}) estimates of 2.5–5.8 m. Two of the ICFME plots (numbers 3 and 4) had no overstory spruce and were therefore excluded from the dual strata calculations. FMC was measured at the plot level as part of the ICFME burning project (Stocks *et al.* 2004).

At the Porter Lake site, plot-level LCBH as well as FMC values were published in the original primary source report (Alexander *et al.* 1991) and remain unchanged for our analysis.

¹ Note that Table 12 in Alexander *et al.* (2004) contains a previously unreported error in the black spruce overstory LCBH. The value for Plot 5 should be 0.7 m (not 10.0 m as shown); the mean spruce LCBH for all 7 plots with this stratum was 1.49 m and not 2.7 m as shown.

At the Prince George (Summit Lake) site, the LCBH from the two distinct stand types (i.e. ‘Dry pine south’ and ‘Dry pine north’) were published in the original source report (Lawson 1972) and remain unchanged for our analysis. The FMC values were estimated using the FBP System equations (FCFDG 1992).

Use of MC_{SA} model – suggestions and caution at high FFMC levels

With the present published version of Wotton and Beverly’s (2007) stand-adjusted litter moisture content (MC_{SA}) model, it is straightforward, if somewhat uncertain, to apply the five stand parameters to generate MC_{SA} estimates. Applying FFMC, DMC, and stand type inputs follows the application of standard hourly or diurnal Canadian Forest Fire Weather Index (FWI) System components (Van Wagner 1987) and stand survey information. Use of calendar dates for assigning season, as we did in the present study, is a coarse but sometimes necessary simplification. Future users will likely have better success using local greenup dates to define the end of the spring season, as intended by Wotton and Beverly (2007). While not originally part of their model, the ‘spring-summer transition’ season (i.e. June 1-15, or as defined locally) likely remains useful and is simply calculated as the mean value from the two seasons. The density factor can be applied as we did, using estimated canopy closure classes (e.g. from hemispherical photographs; Chianucci and Cutini 2012) roughly as follows: ‘light’ (20-45%), ‘moderate’ (46-60%) and ‘dense’ (>61%). In a physical sense, we expect the crown closure influence to be tied to in-stand solar radiation and potential evapotranspiration (Vezina and Péch 1964; van der Kamp *et al.* 2017); additional testing and validation of this effect are clearly required.

Users should take heed of some illogical behaviour in the MC_{SA} model of Wotton and Beverly (2007) at high FFMC levels, likely caused by limited sampling and statistical interaction terms. Stands classified as ‘dense’ begin to show a reverse density influence on litter moisture content (MC) above an FFMC of approximately 92.93, such that ‘dense’ stands are predicted to have slightly lower MC values than ‘moderate’ stands; similarly illogical differences between ‘light’ and ‘moderate’ categories exist above an FFMC of approximately 96.15, where ‘light’ density stands begin to have higher predicted MC than ‘moderate’ density stands. Below these thresholds, the density classes behave as expected. A similar reversal exists with the season factor: below FFMC 95.16, ‘spring’ produces lower estimated MC than ‘summer’; above that threshold, ‘summer’ MC value is slightly higher than ‘spring’. In this latter instance, however, it is not clear if this is a model error since the cause of the seasonal difference was unknown (Wotton and Beverly 2007). In our analyses, we adjusted the density classes of five high FFMC (> 92.9) fire observations, from ‘dense’ to ‘moderate’, where the FFMC-density combinations were producing illogical behaviour; the maximum change in MC due to this adjustment was 0.37% for FFMC values up to 94.2. For cases with higher FFMC values, differences could be more pronounced. In a practical sense, these differences are small but suggest the need for additional studies or refinements to the MC_{SA} model.

Fitted coefficients for all described models

Table S1. Coefficients for all models tested in the main study, fitted to full database (n=113). Models 7-11 are duplicated here for simplicity (see Table 3 in main text). All coefficients in Models A, B and 1–6 are significant at the $\alpha=0.05$ level. See main text, Appendix I for abbreviations.

Model	Intercept	WS ₁₀	FSG	MC	SFC	SFC.CLS2	SFC.CLS3	Accuracy	AIC	Predictors	FSG
A	-1.1933	0.3250	-0.519	-	-	-	-	0.8142	94.3	WS ₁₀ + FSG	Base

B	6.3281	0.4292	-0.853	-0.688	-	-	0.8407	73.9	WS ₁₀ + FSG + MC _{FFMC}	Base	
1	4.3777	0.4923	-1.081	-0.6928	1.4377	-	0.8761	65.9	WS ₁₀ + FSG + SFC + MC _{FFMC}	Base	
2	3.7926	0.4586	-1.047	-0.5466	1.1419	-	0.8673	71.2	WS ₁₀ + FSG + SFC + MC _{SA}	Base	
3	2.4339	0.5171	-0.345	-0.6579	1.4751	-	0.885	64.7	WS ₁₀ + FSG ^{1.5} + SFC + MC _{FFMC}	Base	
4	2.1617	0.4983	-0.343	-0.5452	1.1888	-	0.8761	68.5	WS ₁₀ + FSG ^{1.5} + SFC + MC _{SA}	Base	
5	-4.8496	1.2658	-0.397	-0.0662	1.7128	-	0.9027	61	WS ₁₀ + FSG ^{1.5} + SFC + MC _{FFMC} x WS ₁₀	Base	
6	-3.8869	1.0597	-0.38	-0.0493	1.3516	-	0.8761	65.5	WS ₁₀ + FSG ^{1.5} + SFC + MC _{SA} x WS ₁₀	Base	
7	-3.0923	1.2611	-0.395	-0.0659	2.8324	-	0.9027	60.1	WS ₁₀ + FSG ^{1.5} + ln(SFC) + MC _{FFMC} x WS ₁₀	Base	
8	-2.4341	1.0449	-0.376	-0.0487	2.1943	-	0.8761	65	WS ₁₀ + FSG ^{1.5} + ln(SFC) + MC _{SA} x WS ₁₀	Base	
9	-4.6830	1.3156	-0.415	-0.0663	-	1.6792	3.2814	0.8761	61.6	WS ₁₀ + FSG ^{1.5} + SFC.CLS + MC _{FFMC} x WS ₁₀	FSG Adj.
10	-4.0204	1.3514	-0.434	-0.0688	2.8906	-	0.9115	56.3	WS ₁₀ + FSG ^{1.5} + ln(SFC) + MC _{FFMC} x WS ₁₀	FSG Adj.	
11	-3.5550	1.4407	-0.532	-0.0702	2.4897	-	0.9204	55.2	WS ₁₀ + FSG ^{1.5} + ln(SFC) + MC _{SA} x WS ₁₀	FSG Adj.	
12	-3.2882	1.0441	-0.125	-0.0476	2.0661	-	0.8938	64.9	WS ₁₀ + FSG ² + ln(SFC) + MC _{SA} x WS ₁₀	FSG Adj.	

Comparison between crown fire occurrence probability models

Table S2. Table of crown fire occurrence probabilities comparing inputs and different model outputs.

Models 9–10 shown are from the present study. Model 11_{d1} and Model 11_{d2} indicate model 11 with low and moderate stand density, respectively, and LOGIT1 and LOGIT2 represent the models of Cruz *et al.* (2003). Required inputs for various models are as indicated. MC_{SA-d1} and MC_{SA-d2} refer to stand-adjusted moisture content estimates using light (d1) and moderate (d2) stand density categories, respectively, assuming a pine stand and summer season (Wotton and Beverly 2007). Green text and background indicate predicted surface fire behaviour ($p < 0.5$) while red text and background indicate predicted crown fire behaviour ($p \geq 0.5$). Same fire type (FT) is true (T) when Model 9, Model 10, Model 11_{d2} and LOGIT1 and LOGIT2 models all predict the same fire type (surface or crown) or false (F) when at least one is different from the others. Drought Code (DC) associated with selected Duff Moisture Code (DMC) values are mean values calculated from British Columbia fire weather database statistics (1970–2016) for DMC 36–45, excluding anomalously high values (i.e. DC < 400, for DMC 40; $n = 104,651$) and DMC 86–95 (DC < 500, for DMC 90; $n = 15,310$). Initial Spread Index (ISI) is calculated from indicated wind speed (WS) and Fine Fuel Moisture Code (FFMC) values, and Buildup (BUI) is calculated from the indicated DMC and DC values as per the Canadian Forest Fire Weather Index System (Van Wagner 1987). SFC for Models 10 and 11, and SFC class for Model 9, were calculated from the FBP System C-3/C-4 fuel type SFC model based on the BUI (FCFDG 1992, Eqn. 11). This gave values of 1.6 kg m⁻² (SFC class 2) and 3.4 kg m⁻² (SFC class 3) for BUI 57 and 111, respectively. Refer to Appendix 1 in the main text for abbreviations and units.

FFMC	DMC	MC _{SA-d1}	MC _{SA-d2}	WS ₁₀	DC	ISI	BUI	FSG	Model 9 WS ₁₀ , FFMC, FSG, SFC.CLS	Model 10 WS ₁₀ , FFMC, FSG, SFC	Model 11 _{d2} WS ₁₀ , MC _{SA} , FSG, SFC	LOGIT1 WS ₁₀ , FFMC, LCBH, DC	LOGIT2 ISI, LCBH, DC	Same FT?	Model 11 _{d1} WS ₁₀ , MC _{SA} , FSG, SFC
88	40	10.91	13.31	7	241	4.58	57	3	0.122	0.163	0.175	0.096	0.242	T	0.409
91	40	8.91	10.3	7	241	7.04	57	3	0.38	0.475	0.483	0.444	0.625	F	0.649
94	40	6.8	7.31	7	241	10.73	57	3	0.718	0.798	0.802	0.857	0.952	T	0.839

88	90	9.21	11.23	7	366	4.58	111	3	0.409	0.61	0.781	0.503	0.648	F	0.906
91	90	7.52	8.69	7	366	7.04	111	3	0.753	0.879	0.925	0.883	0.906	T	0.957
94	90	5.74	6.17	7	366	10.73	111	3	0.927	0.97	0.977	0.983	0.991	T	0.981
88	40	10.91	13.31	13	241	6.2	57	3	0.681	0.753	0.816	0.763	0.487	F	0.975
91	40	8.91	10.3	13	241	9.52	57	3	0.971	0.981	0.986	0.96	0.899	T	0.996
94	40	6.8	7.31	13	241	14.52	57	3	0.998	0.999	0.999	0.994	0.996	T	0.999
88	90	9.21	11.23	13	366	6.2	111	3	0.914	0.961	0.994	0.968	0.845	T	0.999
91	90	7.52	8.69	13	366	9.52	111	3	0.994	0.998	0.999	0.996	0.981	T	>0.999
94	90	5.74	6.17	13	366	14.52	111	3	>0.999	>0.999	>0.999	0.999	0.999	T	>0.999
88	40	10.91	13.31	19	241	8.38	57	3	0.97	0.979	0.989	0.99	0.805	T	>0.999
91	40	8.91	10.3	19	241	12.88	57	3	0.999	>0.999	>0.999	0.999	0.988	T	>0.999
94	40	6.8	7.31	19	241	19.65	57	3	>0.999	>0.999	>0.999	>0.999	>0.999	T	>0.999
88	90	9.21	11.23	19	366	8.38	111	3	0.994	0.997	>0.999	0.999	0.96	T	>0.999
91	90	7.52	8.69	19	366	12.88	111	3	>0.999	>0.999	>0.999	>0.999	0.998	T	>0.999
94	90	5.74	6.17	19	366	19.65	111	3	>0.999	>0.999	>0.999	>0.999	>0.999	T	>0.999
88	40	10.91	13.31	7	241	4.58	57	8	<0.001	<0.001	<0.001	0.001	0.004	T	<0.001
91	40	8.91	10.3	7	241	7.04	57	8	<0.001	<0.001	<0.001	0.006	0.022	T	<0.001
94	40	6.8	7.31	7	241	10.73	57	8	0.002	0.002	<0.001	0.04	0.212	T	<0.001
88	90	9.21	11.23	7	366	4.58	111	8	0.001	0.001	<0.001	0.007	0.024	T	0.001
91	90	7.52	8.69	7	366	7.04	111	8	0.002	0.004	0.001	0.05	0.114	T	0.002
94	90	5.74	6.17	7	366	10.73	111	8	0.009	0.016	0.004	0.284	0.607	F	0.005
88	40	10.91	13.31	13	241	6.2	57	8	0.002	0.002	<0.001	0.022	0.013	T	0.004
91	40	8.91	10.3	13	241	9.52	57	8	0.024	0.027	0.006	0.144	0.106	T	0.023
94	40	6.8	7.31	13	241	14.52	57	8	0.256	0.301	0.09	0.558	0.774	F	0.137
88	90	9.21	11.23	13	366	6.2	111	8	0.008	0.013	0.016	0.176	0.068	T	0.096
91	90	7.52	8.69	13	366	9.52	111	8	0.108	0.182	0.145	0.615	0.407	F	0.331
94	90	5.74	6.17	13	366	14.52	111	8	0.631	0.776	0.629	0.923	0.952	T	0.715
88	40	10.91	13.31	19	241	8.38	57	8	0.023	0.024	0.009	0.405	0.052	T	0.176
91	40	8.91	10.3	19	241	12.88	57	8	0.572	0.618	0.325	0.836	0.533	F	0.754
94	40	6.8	7.31	19	241	19.65	57	8	0.985	0.989	0.963	0.974	0.991	T	0.981
88	90	9.21	11.23	19	366	8.38	111	8	0.106	0.167	0.456	0.866	0.242	F	0.925
91	90	7.52	8.69	19	366	12.88	111	8	0.869	0.929	0.961	0.98	0.868	T	0.992
94	90	5.74	6.17	19	366	19.65	111	8	0.997	0.999	0.999	0.997	0.998	T	0.999

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Supplementary Material

Improved logistic models of crown fire probability in Canadian conifer forests

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Canadian experimental burn sites: Estimates of live crown base height, foliar moisture content, and other details

This document contains additional background information on the Canadian experimental burning experiments and data used to calculate or estimate live crown base height (LCBH), foliar moisture content (FMC), and other variables for crown fire modelling purposes. Experimental fires were carried out in natural stands of black spruce (*Picea mariana* (Mill.) B.S.P.) and jack pine (*Pinus banksiana* Lamb.), and to a lesser extent red pine (*Pinus resinosa* Ait.)–white pine (*Pinus strobus* L.) and lodgepole pine (*Pinus contorta* var. *latifolia* Engelm. Dougl. ex Loud.), as well as red pine plantations.

Sampling intensity and transparency of LCBH values increased over time in the various fire experiments comprising our database. At the earliest sites, little information was available and crown ratio (CR) modelling based on overall stand metrics appeared to be the only option for estimating LCBH. Starting in the mid-1970's, some measure of variation between plots was typically available, with either individual plot mean LCBH values (mostly previously published), or measures from a small sample (e.g. 10-30 trees) of biomass trees of different sizes produced for estimating diameter at breast height (DBH)–height and CR relationships; these relationships could then be applied to experimental plots. Later experimental burning projects typically featured more detailed fuel sampling (e.g. at the International Crown Fire Modelling Experiment, ICFME; Alexander *et al.* 2004), though not in all cases.

The sites described here with previously-unpublished LCBH estimates are from Sharpsand Creek (immature and thinned plots), Kenshoe Lake (pine stratum and spruce-pine fuel strata gap (FSG_{SP}) only), and the Petawawa National Forest Institute (PNFI: jack pine and red/white pine) in Ontario; and Darwin Lake, Big Fish Lake, and Pelican Mountain sites in

Alberta. Additionally, values at ICFME were calculated differently than in past analyses. At the remaining sites, LCBH values were unchanged from values reported in the original sources.

At the Sharpsand Creek site, raw cruise data were available for immature (SC-IM) and thinning treatment (SC-TH) plots based on earlier sampling (Walker and Stocks 1975), allowing for a fresh analysis of crown fuel structure. Analysis of plot density values revealed one clear outlier among the SC-TH plots, with much higher live (8380 ha^{-1}) and dead (6875 ha^{-1}) density compared with other thinned plots; these values were in the range of the SC-IM plots (live density: $6424\text{--}13\,928 \text{ ha}^{-1}$; dead density: $5032\text{--}13\,164 \text{ ha}^{-1}$). This plot (number 16) was therefore suspected to have been only partially or incompletely thinned and was assigned to the SC-IM treatment for analysis purposes. Overall, immature plots had mean values of 9213 and 9971 live and dead stems ha^{-1} , respectively, while the comparable values for SC-TH plots were 4725 live and 1175 dead stems ha^{-1} ; both differences were highly significant between treatments (Welch's t-test, $p < 0.001$ for both live and dead stems). The biomass trees from the same study (Walker and Stocks 1975) were also reanalyzed to examine CR values. CR varied slightly by DBH, and was modelled as a linear function as follows:

$$\text{CR} = 0.3705 + 0.009196 \cdot \text{DBH} \quad (\text{S1}),$$

and deemed marginally significant ($p=0.0747$); this gave estimated CR values of 0.39-0.48 for trees with DBH values from 2-12 cm.

We then calibrated an Ontario-based mixed-effects model (Sharma and Parton 2007) for describing tree heights and CR for jack pine based on density and basal area, with a random effect for site quality. We used this model to produce new height estimates for live and dead cohorts and LCBH for live SC-IM trees. Together with the estimated CR values, this produced

the DBH-LCBH model shown in Figure S1. This was used together with the cruise data to estimate plot-level LCBH estimates for the SC-IM plots.

Unfortunately, raw plot-level data from the SC-SM plots could not be found; consequently, all SC-SM plots were assumed to have the an LCBH value of 5.3 m (McRae *et al.* 2017).

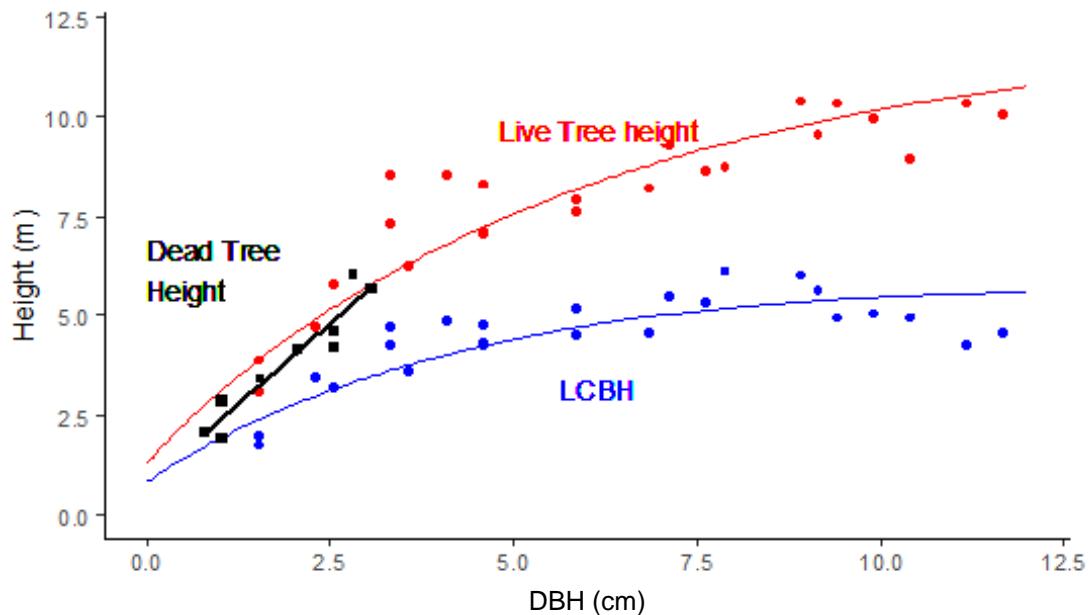


Figure S1. Biomass tree data and models from Sharpsand Creek jack pine: height-DBH data and model (red), LCBH data and model (blue); and dead tree data and linear fit (black). For estimating dead tree height, the linear model was used for DBH < 3 cm and the live tree height model was used for DBH ≥ 3 cm.

For the SC-TH plots, no cruise data (DBH) was located for two of the five plots. Furthermore, the DBH-height (and CR) relationship from the SC-IM biomass trees could not be assumed to hold. Pre-commercial thinning treatments in jack pine are known to cause radial growth compared to controls (Zhang *et al.* 2006) and can also alter crown recession rate and CR

(Morris *et al.* 1994). In the absence of a credible model for LCBH in thinning treatments, we used the mean SC-IM plot value (4.28 m) for SC-TH plots.

One additional adjustment was made to the Sharpsand Creek plot data based on time of burning. The SC-IM and SC-TH plots were burned between 1974-1976 and 1981, while SC-SM plots were burned from 1988-1991. Stand measurements occurred in 1974 (for IM and TH plots), and again in 1984 (for SC-SM). As noted by McRae *et al.* (2017), significant stand changes had occurred over the decade between measurements, with >50% reductions in live and dead stand density and a 1.0 m increase in LCBH (i.e. from 4.28 m to 5.3 m). Therefore, the latest SC-TH and SC-IM burns occurred halfway between measurements. To compensate for this, 0.5 m (half of the mean difference) was added to the estimated LCBH of the four plots burned in 1981 (i.e. 2 each of the SC-IM and SC-TH plots).

Foliar moisture content (FMC) for all Sharpsand Creek plots was estimated using the FBP System equations based on calendar date, elevation and latitude/longitude (Forestry Canada Fire Danger Group 1992; hereafter FCFDG 1992).

Surface fuel consumption (SFC) values were missing for the SC-SM plot files, though total fuel consumption (TFC) and depth of burn values were reported (McRae *et al.* 2017). In order to estimate SFC in line with the remaining observations, we subtracted estimated crown fuel consumption (CFC) values from reported TFC (as per FCFDG 1992). Mean reported CFC values in the SC-IM and SC-TH plots were grouped by type of fire (Stocks 1987; unpublished data files). SC-SM TFC values were therefore reduced by 0.02, 0.39, and 1.14 kg m⁻², for surface, passive crown (or ‘torching’), and active crown fires, respectively. For the two observations with fire behaviour described as ‘some torching’, we estimated CFC as the mean of

the first two categories (surface and passive crown) or in other words 0.20 kg m^{-2} . This gave overall SFC estimates of $1.4\text{--}3.6 \text{ kg m}^{-2}$.

At the Kenshoe Lake site, a similar process was used for LCBH on the jack pine data (used for the upper crowning analysis). The local biomass tree data was used once again to calibrate Sharma and Parton (2007)'s DBH-height model, with parameters and biomass data for black spruce and jack pine calculated separately. For the pine cohorts, CR values were not significantly different across size classes ($p = 0.336$), so a constant CR of 0.34 was assumed. With the DBH-height model and constant CR, new pine LCBH estimates were calculated, which ranged from 10.2-11.0 m. As noted in the main text, the LCBH for spruce layer was not measured, but estimated to be 2.0 m for all plots. Together with new spruce cohort mean height estimates of 5.4-7.8 m, this gave black spruce crown centroid heights estimates of 3.4-5.8 m and FSG_{SP} estimates of 4.8-6.5 m (see main text, Appendix II for additional information). FMC estimates at Kenshoe Lake were based on the FBP System equations (FCFDG 1992).

At the Big Fish Lake site, unpublished plot-level LCBH measurements were made available for 8 of the 9 experimental fires (M. E. Alexander, research coordinator for the experimental burning project). These were based on sampling of trees directly across from the fireguards surrounding each plot; this was done to avoid trampling the sensitive surface fuelbeds inside the plot perimeters. The resulting LCBH plot values ranged from 0.36–1.29 m, based on samples from 55–221 trees per plot. LCBH for the only unsampled plot was estimated as the mean value (i.e. 0.96 m) of the other eight plot averages. FMC estimates at Big Fish Lake were derived from the FBP System equations (FCFDG 1992). LCBH and FMC values at other associated black spruce experimental burning sites were provided or estimated from the original sources (Kiil 1975; Newstead and Alexander 1983).

At the Darwin Lake site, two distinct stand types were described, with similar basal area but differing stand height, age and density (Quintilio *et al.* 1977). Overstory data on tree heights and LCBH were sparse, with a biomass tree sample (later published in Alexander *et al.* 1991) lacking in data from larger trees. We estimated height and DBH values from three additional dominant trees based on photos presented in Alexander and de Groot (1988) to add to the biomass sample; we then fitted a simple log-model to these data to estimate an overall DBH-height relationship (Fig. S2). In the biomass sample, the slope of the DBH–CR relationship was not significantly different from zero ($p > 0.1$), suggesting a constant CR of about 0.54. Using this biomass model with the plot data resulted in new LCBH estimates from 4.75–6.21 m. FMC at Darwin Lake was estimated using the FBP System equations (FCFDG 1992).

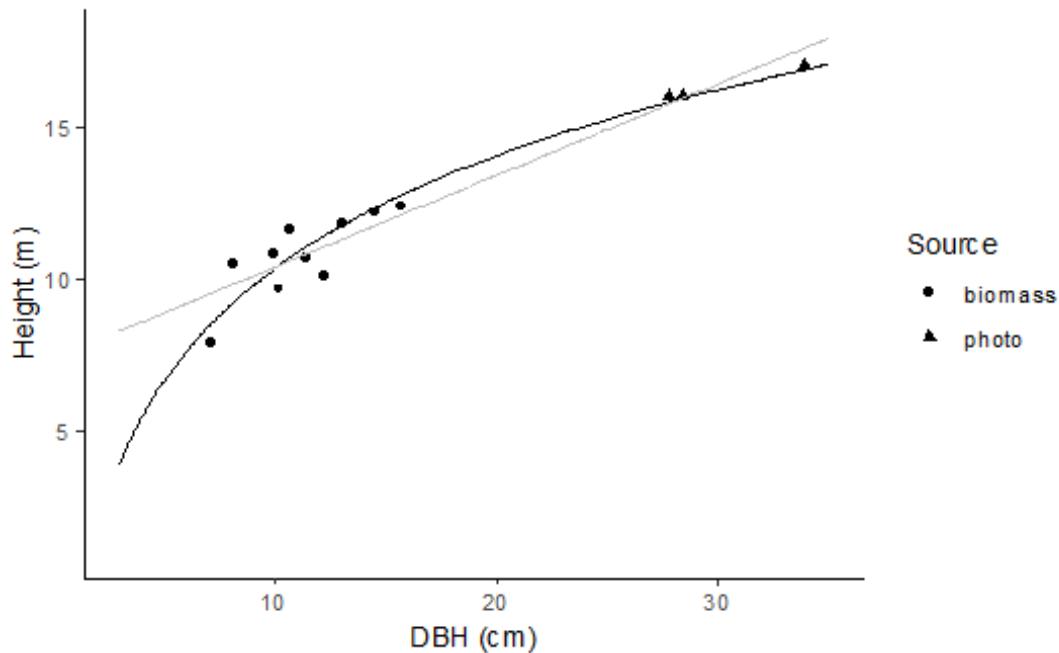


Figure S2. Fitted DBH-height relationship for overstory jack pine trees at Darwin Lake, Alberta, showing observations from the published biomass trees along with three additions based on scaling from photographs. The log-model performed slightly better (black; $R^2=0.931$) and was believed to be more realistic than a linear model (gray; $R^2=0.917$) for representing the DBH-height relationship; consequently the log-model was used to estimate tree heights in experimental fire plots.

The PNFI establishment (formerly the Petawawa Forest Experiment Station), west of Ottawa, Ontario, was the site of the earliest field experiments on fire behaviour in pine stands (e.g., Van Wagner 1963; 1965). The 1960's era jack pine experimental fires conducted by C. E. Van Wagner were later documented by Hummel (1979) and Weber *et al.* (1987) in a related fire effects study. We used Hummel's (1979) stand data and reconstructions with McAlpine and Hobbs' (1994) locally-calibrated model to estimate plot-level LCBH values based on stand density and basal area. This resulted in five new LCBH estimates for PNFI jack pine plots, ranging from 7.33–9.12 m.

For the PNFI red and white pine stands, no previous LCBH measures were ever formally published, though the FBP System documentation suggested a fixed LCBH value of 18 m for the C-5 fuel type (FCFDG 1992). Stand data was published for the various experimental blocks along with the results from earlier experimental fires (Van Wagner 1963). We used Holdaway's (1988) models from Wisconsin, USA to calculate CR values for these stands, providing for admittedly crude estimates. Together with published stand height values (14.6–25.0 m), this resulted in new LCBH estimates for the PNFI red and white pine stands of 7.4 m–13.3 m. FMC values for all PNFI red and white pine stands were interpolated from local species-specific seasonal curves (Van Wagner 1967).

Experimental fires in red pine plantations at PNFI were also conducted and documented by Van Wagner (1968, 1977), with additional insights documented in later reports (e.g. Van Wagner 1986). Field-scale experimental fires carried out between 1962 and 1967 were conducted in late spring through summer conditions. Mean stand attributes, including LCBH values, were provided in these reports, though no sampling details were provided. The described ranges suggest that some stand-wide sampling was conducted. Stem and canopy fuel densities

were high in these stands (FCFDG 1992). FMC values were estimated from locally-derived seasonal FMC curves (Van Wagner 1967).

At the Pelican Mountain experimental burning site, most of the necessary inputs involved in crown fire modelling were documented and reported on by Thompson *et al.* (2020), with the exception of LCBH. Mean overstory (black spruce) LCBH values were obtained for the control (2.08 m) and thinned (4.15 m) plots from G. A. Marshall (personal communication, April 2022). FMC was estimated and reported in the study (Thompson *et al.* 2020) using the FBP System equations (FCFDG 1992).

At the ICFME site, detailed fuel structure surveys were previously published in various tables (Alexander *et al.* 2004). The only difference from previous analyses was the change from using the ‘combined’ black spruce-jack pine LCBH value to using individual values for overstory spruce and pine cohorts (Alexander *et al.* 2004, Table 12).¹ The overstory spruce had LCBH values of 0.7–2.4 m, while pine cohorts (used for estimating upper canopy crowning) had LCBH values of 3.6–8.2 m. Combined with spruce crown depth plot measurements, this gave spruce crown centroid estimates of 2.7–4.3 m and spruce-pine fuel strata gap (FSG_{SP}) estimates of 2.5–5.8 m. Two of the ICFME plots (numbers 3 and 4) had no overstory spruce and were therefore excluded from the dual strata calculations. FMC was measured at the plot level as part of the ICFME burning project (Stocks *et al.* 2004).

At the Porter Lake site, plot-level LCBH as well as FMC values were published in the original primary source report (Alexander *et al.* 1991) and remain unchanged for our analysis.

¹ Note that Table 12 in Alexander *et al.* (2004) contains a previously unreported error in the black spruce overstory LCBH. The value for Plot 5 should be 0.7 m (not 10.0 m as shown); the mean spruce LCBH for all 7 plots with this stratum was 1.49 m and not 2.7 m as shown.

At the Prince George (Summit Lake) site, the LCBH from the two distinct stand types (i.e. ‘Dry pine south’ and ‘Dry pine north’) were published in the original source report (Lawson 1972) and remain unchanged for our analysis. The FMC values were estimated using the FBP System equations (FCFDG 1992).

Use of MC_{SA} model – suggestions and caution at high FFMC levels

With the present published version of Wotton and Beverly’s (2007) stand-adjusted litter moisture content (MC_{SA}) model, it is straightforward, if somewhat uncertain, to apply the five stand parameters to generate MC_{SA} estimates. Applying FFMC, DMC, and stand type inputs follows the application of standard hourly or diurnal Canadian Forest Fire Weather Index (FWI) System components (Van Wagner 1987) and stand survey information. Use of calendar dates for assigning season, as we did in the present study, is a coarse but sometimes necessary simplification. Future users will likely have better success using local greenup dates to define the end of the spring season, as intended by Wotton and Beverly (2007). While not originally part of their model, the ‘spring-summer transition’ season (i.e. June 1-15, or as defined locally) likely remains useful and is simply calculated as the mean value from the two seasons. The density factor can be applied as we did, using estimated canopy closure classes (e.g. from hemispherical photographs; Chianucci and Cutini 2012) roughly as follows: ‘light’ (20-45%), ‘moderate’ (46-60%) and ‘dense’ (>61%). In a physical sense, we expect the crown closure influence to be tied to in-stand solar radiation and potential evapotranspiration (Vezina and Péch 1964; van der Kamp *et al.* 2017); additional testing and validation of this effect are clearly required.

Users should take heed of some illogical behaviour in the MC_{SA} model of Wotton and Beverly (2007) at high FFMC levels, likely caused by limited sampling and statistical interaction terms. Stands classified as ‘dense’ begin to show a reverse density influence on litter moisture content (MC) above an FFMC of approximately 92.93, such that ‘dense’ stands are predicted to have slightly lower MC values than ‘moderate’ stands; similarly illogical differences between ‘light’ and ‘moderate’ categories exist above an FFMC of approximately 96.15, where ‘light’ density stands begin to have higher predicted MC than ‘moderate’ density stands. Below these thresholds, the density classes behave as expected. A similar reversal exists with the season factor: below FFMC 95.16, ‘spring’ produces lower estimated MC than ‘summer’; above that threshold, ‘summer’ MC value is slightly higher than ‘spring’. In this latter instance, however, it is not clear if this is a model error since the cause of the seasonal difference was unknown (Wotton and Beverly 2007). In our analyses, we adjusted the density classes of five high FFMC (> 92.9) fire observations, from ‘dense’ to ‘moderate’, where the FFMC-density combinations were producing illogical behaviour; the maximum change in MC due to this adjustment was 0.37% for FFMC values up to 94.2. For cases with higher FFMC values, differences could be more pronounced. In a practical sense, these differences are small but suggest the need for additional studies or refinements to the MC_{SA} model.

Fitted coefficients for all described models

Table S1. Coefficients for all models tested in the main study, fitted to full database (n=113). Models 7-11 are duplicated here for simplicity (see Table 3 in main text). All coefficients in Models A, B and 1–6 are significant at the $\alpha=0.05$ level. See main text, Appendix I for abbreviations.

Model	Intercept	WS ₁₀	FSG	MC	SFC	SFC.CLS2	SFC.CLS3	Accuracy	AIC	Predictors	FSG
A	-1.1933	0.3250	-0.519	-	-	-	-	0.8142	94.3	WS ₁₀ + FSG	Base

B	6.3281	0.4292	-0.853	-0.688	-	-	0.8407	73.9	WS ₁₀ + FSG + MC _{FFMC}	Base	
1	4.3777	0.4923	-1.081	-0.6928	1.4377	-	0.8761	65.9	WS ₁₀ + FSG + SFC + MC _{FFMC}	Base	
2	3.7926	0.4586	-1.047	-0.5466	1.1419	-	0.8673	71.2	WS ₁₀ + FSG + SFC + MC _{SA}	Base	
3	2.4339	0.5171	-0.345	-0.6579	1.4751	-	0.885	64.7	WS ₁₀ + FSG ^{1.5} + SFC + MC _{FFMC}	Base	
4	2.1617	0.4983	-0.343	-0.5452	1.1888	-	0.8761	68.5	WS ₁₀ + FSG ^{1.5} + SFC + MC _{SA}	Base	
5	-4.8496	1.2658	-0.397	-0.0662	1.7128	-	0.9027	61	WS ₁₀ + FSG ^{1.5} + SFC + MC _{FFMC} x WS ₁₀	Base	
6	-3.8869	1.0597	-0.38	-0.0493	1.3516	-	0.8761	65.5	WS ₁₀ + FSG ^{1.5} + SFC + MC _{SA} x WS ₁₀	Base	
7	-3.0923	1.2611	-0.395	-0.0659	2.8324	-	0.9027	60.1	WS ₁₀ + FSG ^{1.5} + ln(SFC) + MC _{FFMC} x WS ₁₀	Base	
8	-2.4341	1.0449	-0.376	-0.0487	2.1943	-	0.8761	65	WS ₁₀ + FSG ^{1.5} + ln(SFC) + MC _{SA} x WS ₁₀	Base	
9	-4.6830	1.3156	-0.415	-0.0663	-	1.6792	3.2814	0.8761	61.6	WS ₁₀ + FSG ^{1.5} + SFC.CLS + MC _{FFMC} x WS ₁₀	FSG Adj.
10	-4.0204	1.3514	-0.434	-0.0688	2.8906	-	0.9115	56.3	WS ₁₀ + FSG ^{1.5} + ln(SFC) + MC _{FFMC} x WS ₁₀	FSG Adj.	
11	-3.5550	1.4407	-0.532	-0.0702	2.4897	-	0.9204	55.2	WS ₁₀ + FSG ^{1.5} + ln(SFC) + MC _{SA} x WS ₁₀	FSG Adj.	
12	-3.2882	1.0441	-0.125	-0.0476	2.0661	-	0.8938	64.9	WS ₁₀ + FSG ² + ln(SFC) + MC _{SA} x WS ₁₀	FSG Adj.	

Comparison between crown fire occurrence probability models

Table S2. Table of crown fire occurrence probabilities comparing inputs and different model outputs.

Models 9–10 shown are from the present study. Model 11_{d1} and Model 11_{d2} indicate model 11 with low and moderate stand density, respectively, and LOGIT1 and LOGIT2 represent the models of Cruz *et al.* (2003). Required inputs for various models are as indicated. MC_{SA-d1} and MC_{SA-d2} refer to stand-adjusted moisture content estimates using light (d1) and moderate (d2) stand density categories, respectively, assuming a pine stand and summer season (Wotton and Beverly 2007). Green text and background indicate predicted surface fire behaviour ($p < 0.5$) while red text and background indicate predicted crown fire behaviour ($p \geq 0.5$). Same fire type (FT) is true (T) when Model 9, Model 10, Model 11_{d2} and LOGIT1 and LOGIT2 models all predict the same fire type (surface or crown) or false (F) when at least one is different from the others. Drought Code (DC) associated with selected Duff Moisture Code (DMC) values are mean values calculated from British Columbia fire weather database statistics (1970–2016) for DMC 36–45, excluding anomalously high values (i.e. DC < 400, for DMC 40; $n = 104,651$) and DMC 86–95 (DC < 500, for DMC 90; $n = 15,310$). Initial Spread Index (ISI) is calculated from indicated wind speed (WS) and Fine Fuel Moisture Code (FFMC) values, and Buildup (BUI) is calculated from the indicated DMC and DC values as per the Canadian Forest Fire Weather Index System (Van Wagner 1987). SFC for Models 10 and 11, and SFC class for Model 9, were calculated from the FBP System C-3/C-4 fuel type SFC model based on the BUI (FCFDG 1992, Eqn. 11). This gave values of 1.6 kg m⁻² (SFC class 2) and 3.4 kg m⁻² (SFC class 3) for BUI 57 and 111, respectively. Refer to Appendix 1 in the main text for abbreviations and units.

FFMC	DMC	MC _{SA-d1}	MC _{SA-d2}	WS ₁₀	DC	ISI	BUI	FSG	Model 9 WS ₁₀ , FFMC, FSG, SFC.CLS	Model 10 WS ₁₀ , FFMC, FSG, SFC	Model 11 _{d2} WS ₁₀ , MC _{SA} , FSG, SFC	LOGIT1 WS ₁₀ , FFMC, LCBH, DC	LOGIT2 ISI, LCBH, DC	Same FT?	Model 11 _{d1} WS ₁₀ , MC _{SA} , FSG, SFC
88	40	10.91	13.31	7	241	4.58	57	3	0.122	0.163	0.175	0.096	0.242	T	0.409
91	40	8.91	10.3	7	241	7.04	57	3	0.38	0.475	0.483	0.444	0.625	F	0.649
94	40	6.8	7.31	7	241	10.73	57	3	0.718	0.798	0.802	0.857	0.952	T	0.839

88	90	9.21	11.23	7	366	4.58	111	3	0.409	0.61	0.781	0.503	0.648	F	0.906
91	90	7.52	8.69	7	366	7.04	111	3	0.753	0.879	0.925	0.883	0.906	T	0.957
94	90	5.74	6.17	7	366	10.73	111	3	0.927	0.97	0.977	0.983	0.991	T	0.981
88	40	10.91	13.31	13	241	6.2	57	3	0.681	0.753	0.816	0.763	0.487	F	0.975
91	40	8.91	10.3	13	241	9.52	57	3	0.971	0.981	0.986	0.96	0.899	T	0.996
94	40	6.8	7.31	13	241	14.52	57	3	0.998	0.999	0.999	0.994	0.996	T	0.999
88	90	9.21	11.23	13	366	6.2	111	3	0.914	0.961	0.994	0.968	0.845	T	0.999
91	90	7.52	8.69	13	366	9.52	111	3	0.994	0.998	0.999	0.996	0.981	T	>0.999
94	90	5.74	6.17	13	366	14.52	111	3	>0.999	>0.999	>0.999	0.999	0.999	T	>0.999
88	40	10.91	13.31	19	241	8.38	57	3	0.97	0.979	0.989	0.99	0.805	T	>0.999
91	40	8.91	10.3	19	241	12.88	57	3	0.999	>0.999	>0.999	0.999	0.988	T	>0.999
94	40	6.8	7.31	19	241	19.65	57	3	>0.999	>0.999	>0.999	>0.999	>0.999	T	>0.999
88	90	9.21	11.23	19	366	8.38	111	3	0.994	0.997	>0.999	0.999	0.96	T	>0.999
91	90	7.52	8.69	19	366	12.88	111	3	>0.999	>0.999	>0.999	>0.999	0.998	T	>0.999
94	90	5.74	6.17	19	366	19.65	111	3	>0.999	>0.999	>0.999	>0.999	>0.999	T	>0.999
88	40	10.91	13.31	7	241	4.58	57	8	<0.001	<0.001	<0.001	0.001	0.004	T	<0.001
91	40	8.91	10.3	7	241	7.04	57	8	<0.001	<0.001	<0.001	0.006	0.022	T	<0.001
94	40	6.8	7.31	7	241	10.73	57	8	0.002	0.002	<0.001	0.04	0.212	T	<0.001
88	90	9.21	11.23	7	366	4.58	111	8	0.001	0.001	<0.001	0.007	0.024	T	0.001
91	90	7.52	8.69	7	366	7.04	111	8	0.002	0.004	0.001	0.05	0.114	T	0.002
94	90	5.74	6.17	7	366	10.73	111	8	0.009	0.016	0.004	0.284	0.607	F	0.005
88	40	10.91	13.31	13	241	6.2	57	8	0.002	0.002	<0.001	0.022	0.013	T	0.004
91	40	8.91	10.3	13	241	9.52	57	8	0.024	0.027	0.006	0.144	0.106	T	0.023
94	40	6.8	7.31	13	241	14.52	57	8	0.256	0.301	0.09	0.558	0.774	F	0.137
88	90	9.21	11.23	13	366	6.2	111	8	0.008	0.013	0.016	0.176	0.068	T	0.096
91	90	7.52	8.69	13	366	9.52	111	8	0.108	0.182	0.145	0.615	0.407	F	0.331
94	90	5.74	6.17	13	366	14.52	111	8	0.631	0.776	0.629	0.923	0.952	T	0.715
88	40	10.91	13.31	19	241	8.38	57	8	0.023	0.024	0.009	0.405	0.052	T	0.176
91	40	8.91	10.3	19	241	12.88	57	8	0.572	0.618	0.325	0.836	0.533	F	0.754
94	40	6.8	7.31	19	241	19.65	57	8	0.985	0.989	0.963	0.974	0.991	T	0.981
88	90	9.21	11.23	19	366	8.38	111	8	0.106	0.167	0.456	0.866	0.242	F	0.925
91	90	7.52	8.69	19	366	12.88	111	8	0.869	0.929	0.961	0.98	0.868	T	0.992
94	90	5.74	6.17	19	366	19.65	111	8	0.997	0.999	0.999	0.997	0.998	T	0.999

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