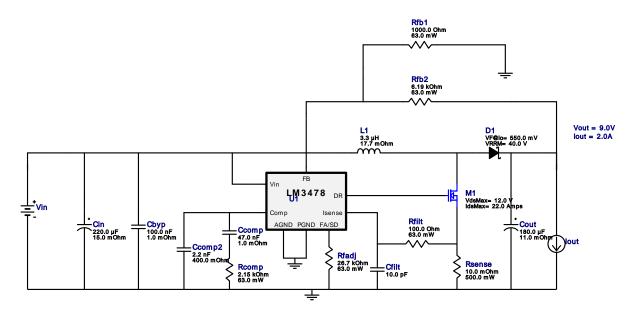
VinMin = 3.5V VinMax = 4.2V Vout = 9.0V lout = 2.0A Device = LM3478MM/NOPB Topology = Boost Created = 2022-08-25 10:14:14.945 BOM Cost = \$2.92 BOM Count = 16 Total Pd = 2.14W

WEBENCH® Design Report

Design: 5 LM3478MM/NOPB LM3478MM/NOPB 3.5V-4.2V to 9.00V @ 2A



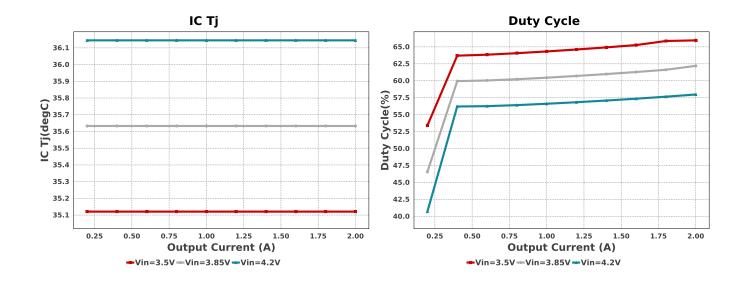
1. With the low turn of voltage of the LM34x8 your power supply may current limit before you reach your working input voltage. If this happens, or to preempt this from happening, you can include a low pass RC filter from input voltage to Vin on the IC. Make sure the rise time on the RC network is slower than your supply's rise time.

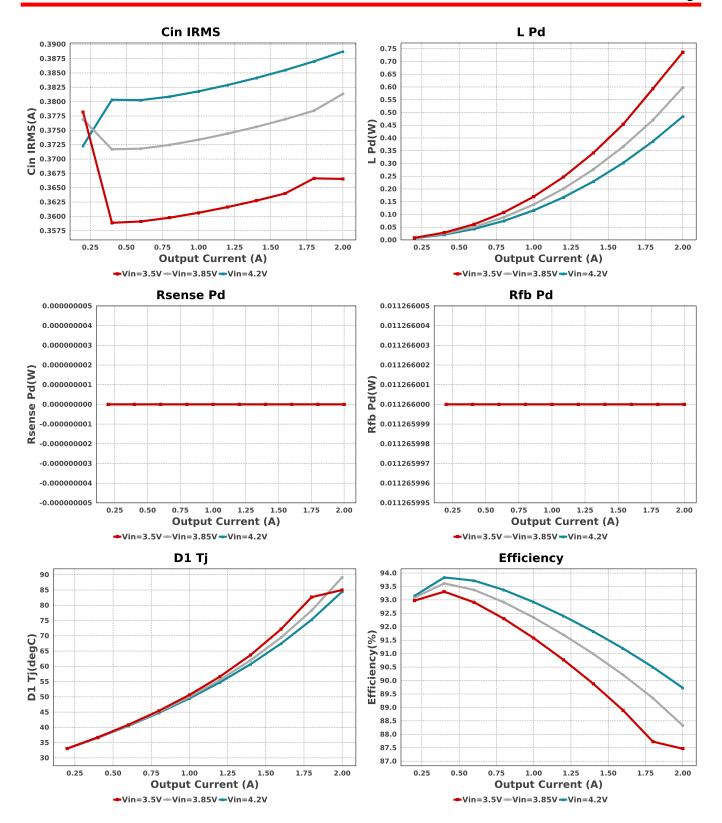
Electrical BOM

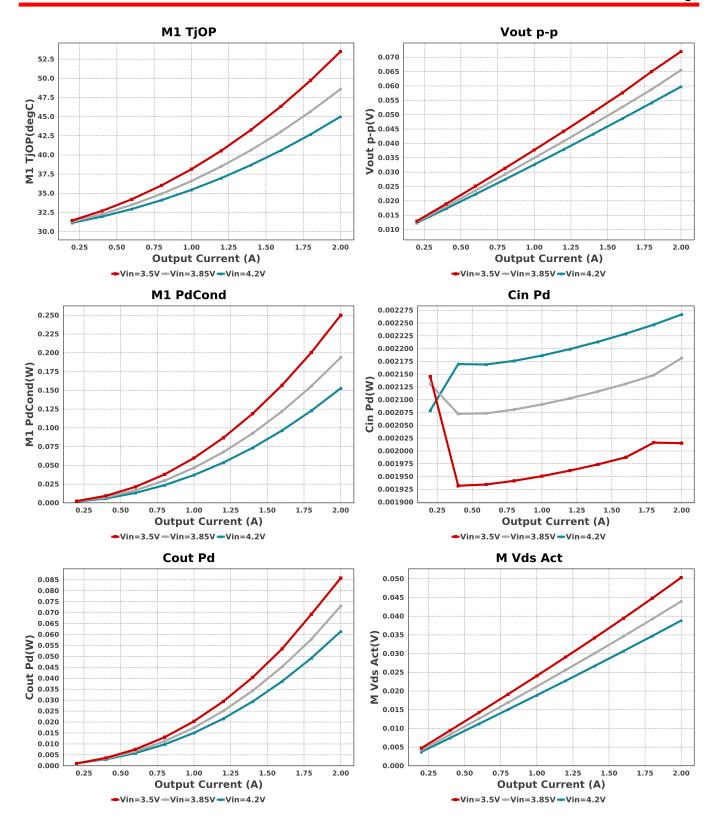
Name	Manufacturer	Part Number	Properties	Qty	Price	Footprint
Cbyp	MuRata	GRM155R70J104KA01D Series= X7R	Cap= 100.0 nF ESR= 1.0 mOhm VDC= 6.3 V IRMS= 0.0 A	1	\$0.01	0402 3 mm ²
Ccomp	MuRata	GRM155R71C473KA01D Series= X7R	Cap= 47.0 nF ESR= 1.0 mOhm VDC= 16.0 V IRMS= 0.0 A	1	\$0.01	0402 3 mm ²
Ccomp2	Kemet	C0805C222K5RACTU Series= X7R	Cap= 2.2 nF ESR= 400.0 mOhm VDC= 50.0 V IRMS= 251.0 mA	1	\$0.01	0805 7 mm ²
Cfilt	Samsung Electro- Mechanics	CL21C100JBANNNC Series= C0G/NP0	Cap= 10.0 pF VDC= 50.0 V IRMS= 0.0 A	1	\$0.01	0805 7 mm ²
Cin	Panasonic	6SVPE220MW Series= SVPE	Cap= 220.0 uF ESR= 15.0 mOhm VDC= 6.3 V IRMS= 3.15 A	1	\$0.20	CAPSMT_62_E61 53 mm²
Cout	Panasonic	16SVPE180M Series= SVPE	Cap= 180.0 uF ESR= 11.0 mOhm VDC= 16.0 V IRMS= 4.46 A	1	\$0.50	CAPSMT_62_C10 74 mm ²
D1	Diodes Inc.	B540C-13-F	VF@Io= 550.0 mV VRRM= 40.0 V	1	\$0.17	SMC 83 mm ²

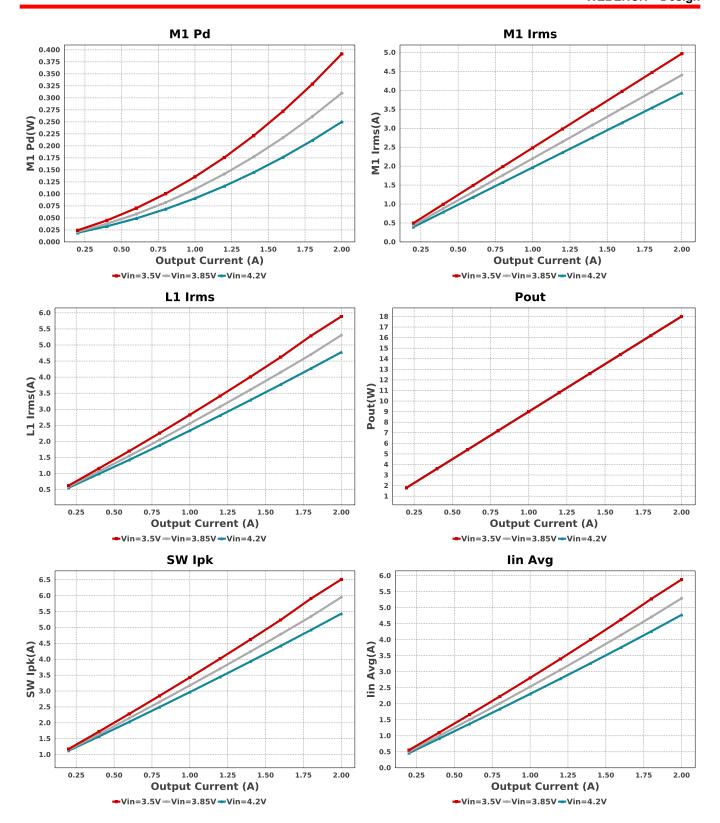
MUA08A 24 mm²

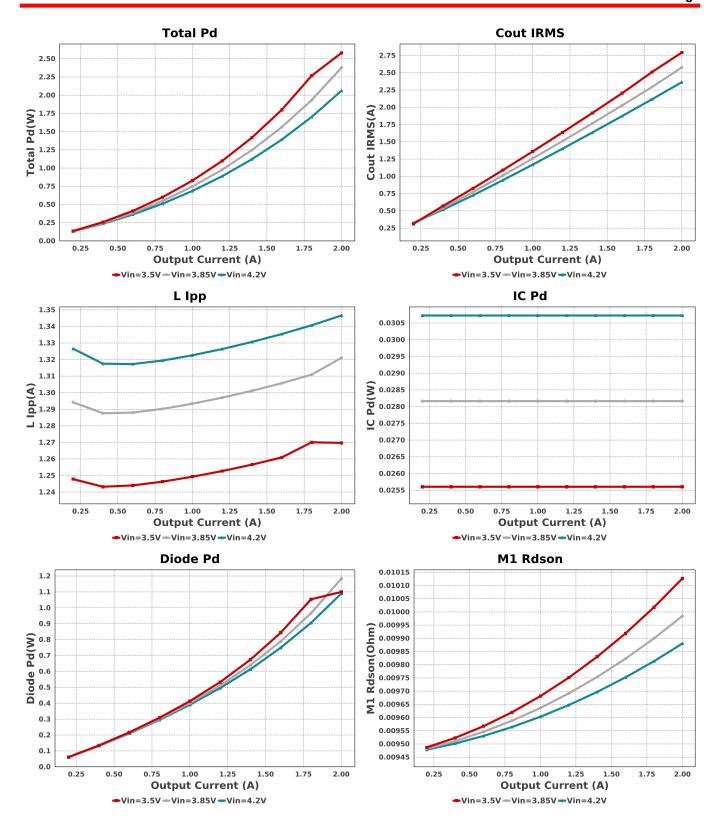
Name	Manufacturer	Part Number	Properties	Qty	Price	Footprint
L1	Vishay-Dale	IHLP3232DZER3R3M01	L= 3.3 μH 17.7 mOhm	1	\$0.66	IHLP-3232DZ 112 mm ²
M1	Texas Instruments	CSD13202Q2	VdsMax= 12.0 V ldsMax= 22.0 Amps	1	\$0.13	DQK0006C 9 mm²
Rcomp	Vishay-Dale	CRCW04022K15FKED Series= CRCWe3	Res= 2.15 kOhm Power= 63.0 mW Tolerance= 1.0%	1	\$0.01	0402 3 mm ²
Rfadj	Vishay-Dale	CRCW040226K7FKED Series= CRCWe3	Res= 26.7 kOhm Power= 63.0 mW Tolerance= 1.0%	1	\$0.01	0402 3 mm ²
Rfb1	Vishay-Dale	CRCW04021K00FKED Series= CRCWe3	Res= 1000.0 Ohm Power= 63.0 mW Tolerance= 1.0%	1	\$0.01	0402 3 mm ²
Rfb2	Vishay-Dale	CRCW04026K19FKED Series= CRCWe3	Res= 6.19 kOhm Power= 63.0 mW Tolerance= 1.0%	1	\$0.01	0402 3 mm ²
Rfilt	Vishay-Dale	CRCW0402100RFKED Series= CRCWe3	Res= 100.0 Ohm Power= 63.0 mW Tolerance= 1.0%	1	\$0.01	0402 3 mm ²
Rsense	Stackpole Electronics Inc	CSR1206FK10L0 Series= ?	Res= 10.0 mOhm Power= 500.0 mW Tolerance= 1.0%	1	\$0.12	1206 11 mm ²
U1	Texas Instruments	LM3478MM/NOPB	Switcher	1	\$1.05	

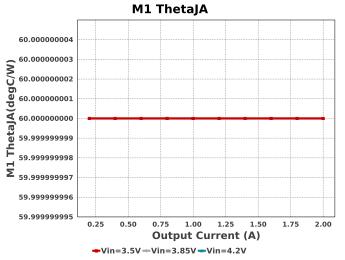


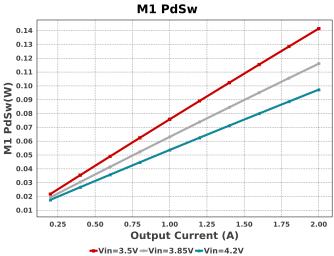


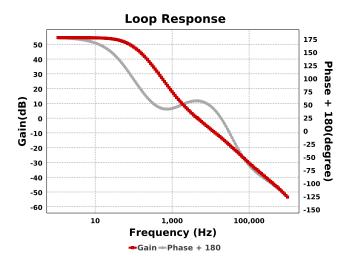












Operating Values

Name	\ / = 1	_	
INAITIC	Value	Category	Description
Cin IRMS	362.6 mA	Capacitor	Input capacitor RMS ripple current
Cin Pd	1.972 mW	Capacitor	Input capacitor power dissipation
Cout IRMS	2.748 A	Capacitor	Output capacitor RMS ripple current
Cout Pd	83.049 mW	Capacitor	Output capacitor power dissipation
D1 Tj	85.0 degC	Diode	D1 junction temperature
Diode Pd	1.1 W	Diode	Diode power dissipation
IC Pd	25.781 mW	IC	IC power dissipation
IC Tj	35.156 degC	IC	IC junction temperature
IC Tolerance	24.3 mV	IC	IC Feedback Tolerance
ICThetaJA	200.0 degC/W	IC	IC junction-to-ambient thermal resistance
lin Avg	5.755 A	IC	Average input current
L lpp	1.256 A	Inductor	Peak-to-peak inductor ripple current
L Pd	705.55 mW	Inductor	Inductor power dissipation
L1 Irms	5.764 A	Inductor	Inductor ripple current
M Vds Act	50.339 mV	Mosfet	M Vds
M1 Irms	4.969 A	Mosfet	M1 MOSFET Irms
M1 Pd	393.79 mW	Mosfet	M1 MOSFET total power dissipation
M1 PdCond	250.13 mW	Mosfet	M1 MOSFET conduction losses
M1 PdSw	143.66 mW	Mosfet	M1 MOSFET switching losses
M1 Rdson	10.131 mOhm	Mosfet	Drain-Source On-resistance
M1 ThetaJA	60.0 degC/W	Mosfet	MOSFET junction-to-ambient thermal resistance
M1 TjOP	53.628 degC	Mosfet	M1 MOSFET junction temperature
Cin Pd	1.972 mW	Power	Input capacitor power dissipation
Cout Pd	83.049 mW	Power	Output capacitor power dissipation
Diode Pd	1.1 W	Power	Diode power dissipation
IC Pd	25.781 mW	Power	IC power dissipation
L Pd	705.55 mW	Power	Inductor power dissipation
M1 Pd	393.79 mW	Power	M1 MOSFET total power dissipation
M1 PdCond	250.13 mW	Power	M1 MOSFET conduction losses
M1 PdSw	143.66 mW	Power	M1 MOSFET switching losses
Rfb Pd	11.266 mW	Power	Rfb Power Dissipation
Rsense Pd	264.49 mW	Power	LED Current Rsns Power Dissipation
	Cin Pd Cout IRMS Cout IRMS Cout Pd D1 Tj Diode Pd C Pd C Tj C Tolerance CThetaJA in Avg Ipp Pd 1 Irms V Vds Act V1 Pd V1 PdCond V1 PdSw V1 Rdson V1 ThetaJA V1 TjOP Cin Pd Cout Pd Cou	Cin Pd 1.972 mW Cout IRMS 2.748 A Cout Pd 83.049 mW D1 Tj 85.0 degC Diode Pd 1.1 W C Pd 25.781 mW C Tj 35.156 degC C Tolerance 24.3 mV C ThetaJA 200.0 degC/W in Avg 5.755 A Ipp 1.256 A Pd 705.55 mW L1 Irms 5.764 A M Vds Act 50.339 mV M1 Irms 4.969 A M1 Pd 393.79 mW M1 PdSw 143.66 mW M1 Rdson 10.131 mOhm M1 TjOP 53.628 degC Cin Pd 1.972 mW Cout Pd 83.049 mW Diode Pd 1.1 W C Pd 25.781 mW L Pd 705.55 mW M1 Pd 393.79 mW M1 Pd 393.79 mW M1 Pd 393.79 mW M1 Pd 393.79 mW M1 PdSw 143.66 mW	Cin Pd 1.972 mW Capacitor Cout IRMS 2.748 A Capacitor Cout Pd 83.049 mW Capacitor Diode Pd 1.1 W Diode Diode Pd 1.1 W Diode C Pd 25.781 mW IC C Tj 35.156 degC IC C Tolerance 24.3 mV IC C Tolerance 24.3 mV IC C ThetaJA 200.0 degC/W IC in Avg 5.755 A IC L Ipp 1.256 A Inductor L Pd 705.55 mW Inductor L Irms 5.764 A Inductor M Vds Act 50.339 mV Mosfet M1 Irms 4.969 A Mosfet M1 Pd 393.79 mW Mosfet M1 Pd 393.79 mW Mosfet M1 PdSw 143.66 mW Mosfet M1 TjOP 53.628 degC Mosfet Cin Pd 1.972 mW Power Diode Pd 1.1 W Power

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#	Name	Value	Category	Description
33.	Total Pd	2.143 W	Power	Total Power Dissipation
34.	Rfb Pd	11.266 mW	Resistor	Rfb Power Dissipation
35.	Rsense Pd	264.49 mW	Resistor	LED Current Rsns Power Dissipation
36.	BOM Count	16	System Information	Total Design BOM count
37.	Cross Freq	3.847 kHz	System Information	Bode plot crossover frequency
38.	Duty Cycle	65.23 %	System Information	Duty cycle
39.	Efficiency	89.359 %	System Information	Steady state efficiency
40.	FootPrint	400.0 mm ²	System Information	Total Foot Print Area of BOM components
41.	Frequency	541.734 kHz	System Information	Switching frequency
42.	Gain Marg	-16.404 dB	System Information	Bode Plot Gain Margin
43.	lout	2.0 A	System Information	lout operating point
44.	Low Freq Gain	52.83 dB	System Information	Gain at 1Hz
45.	Mode	CCM	System Information	Conduction Mode
46.	Phase Marg	55.72 deg	System Information	Bode Plot Phase Margin
47.	Pout	18.0 W	System Information	Total output power
48.	SW lpk	6.38 A	System Information	Peak switch current
49.	Total BOM	\$2.92	System Information	Total BOM Cost
50.	Vin	3.5 V	System Information	Vin operating point
51.	Vout	9.0 V	System Information	Operational Output Voltage
52.	Vout Actual	9.059 V	System Information	Vout Actual calculated based on selected voltage divider resistors
53.	Vout Tolerance	3.701 %	System Information	Vout Tolerance based on IC Tolerance (no load) and voltage divider resistors if applicable
54.	Vout p-p	70.544 mV	System Information	Peak-to-peak output ripple voltage

Design Inputs

Name	Value	Description	
lout	2.0	Maximum Output Current	
VinMax	4.2	Maximum input voltage	
VinMin	3.5	Minimum input voltage	
Vout	9.0	Output Voltage	
base_pn	LM3478	Base Product Number	
source	DC	Input Source Type	
Та	30.0	Ambient temperature	

WEBENCH® Assembly

Component Testing

Some published data on components in datasheets such as Capacitor ESR and Inductor DC resistance is based on conservative values that will guarantee that the components always exceed the specification. For design purposes it is usually better to work with typical values. Since this data is not always available it is a good practice to measure the Capacitance and ESR values of Cin and Cout, and the inductance and DC resistance of L1 before assembly of the board. Any large discrepancies in values should be electrically simulated in WEBENCH to check for instabilities and thermally simulated in WebTHERM to make sure critical temperatures are not exceeded.

Soldering Component to Board

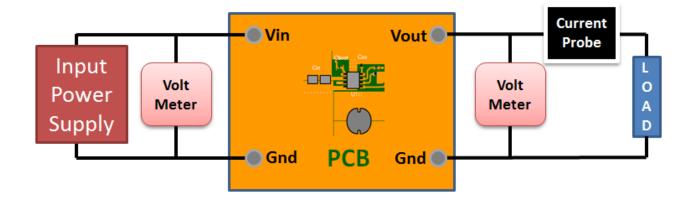
If board assembly is done in house it is best to tack down one terminal of a component on the board then solder the other terminal. For surface mount parts with large tabs, such as the DPAK, the tab on the back of the package should be pre-tinned with solder, then tacked into place by one of the pins. To solder the tab town to the board place the iron down on the board while resting against the tab, heating both surfaces simultaneously. Apply light pressure to the top of the plastic case until the solder flows around the part and the part is flush with the PCB. If the solder is not flowing around the board you may need a higher wattage iron (generally 25W to 30W is enough).

Initial Startup of Circuit

It is best to initially power up the board by setting the input supply voltage to the lowest operating input voltage 3.5V and set the input supply's current limit to zero. With the input supply off connect up the input supply to Vin and GND. Connect a digital volt meter and a load if needed to set the minimum lout of the design from Vout and GND. Turn on the input supply and slowly turn up the current limit on the input supply. If the voltage starts to rise on the input supply continue increasing the input supply current limit while watching the output voltage. If the current increases on the input supply, but the voltage remains near zero, then there may be a short or a component misplaced on the board. Power down the board and visually inspect for solder bridges and recheck the diode and capacitor polarities. Once the power supply circuit is operational then more extensive testing may include full load testing, transient load and line tests to compare with simulation results.

Load Testing

The setup is the same as the initial startup, except that an additional digital voltmeter is connected between Vin and GND, a load is connected between Vout and GND and a current meter is connected in series between Vout and the load. The load must be able to handle at least rated output power + 50% (7.5 watts for this design). Ideally the load is supplied in the form of a variable load test unit. It can also be done in the form of suitably large power resistors. When using an oscilloscope to measure waveforms on the prototype board, the ground leads of the oscilloscope probes should be as short as possible and the area of the loop formed by the ground lead should be kept to a minimum. This will help reduce ground lead inductance and eliminate EMI noise that is not actually present in the circuit.

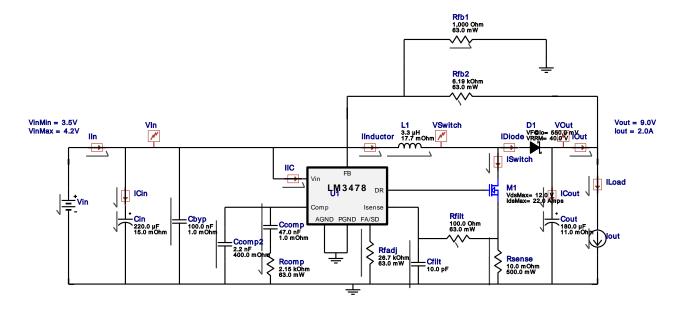


WEBENCH[®] Electrical Simulation Report

Design Id = 5

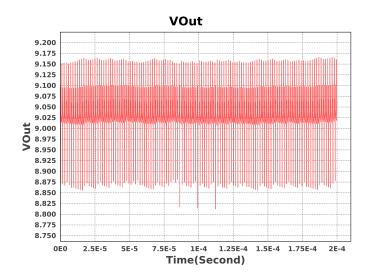
 $sim_id = 4$

Simulation Type = Steady State



Simulation Parameters

# Name	Parameter Name	Description	Values
	1	Load Current	2.0 A



Design Assistance

- 1. Master key: 9852E6C16827247CB7E100346849B713[v1]
- 2. LM3478 Product Folder: http://www.ti.com/product/LM3478: contains the data sheet and other resources.

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