

Radiometry, Reflectance, Lights

Computer Vision I
CSE 252A
Lecture 6

CS252A, Fall 2018

Computer Vision I

A question from Piazza

Homography Color & Lightening

Hi!

In Homography, we get the projection of the object to another image plane given its projection on one image plane. However, it is just a change of positions of points, but does not consider the colors and lightening problems. Would simply copying the RGB values of points violate the Physics of lightening, i.e. would this cause the image to be unrealistic?

Thanks!

logistics

edit

· good question | 0

Updated 3 days ago by Yinglong Miao

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Announcements

- HW1 posted
- HWO graded, will be returned today
- If anyone has any registration issues, talk to me.

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Appearance: lighting, surface reflectance, transmission, camera



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Computer Vision I

Radiometry

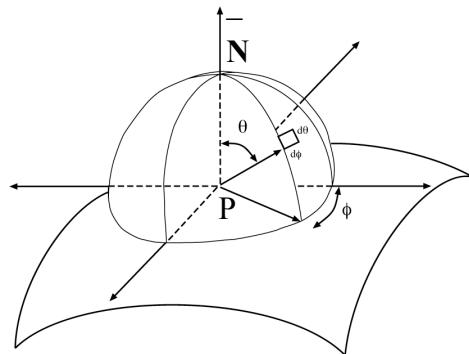
- Read Chapter 4 of Ponce & Forsyth
- Szeliski Sec. 2.2, 2.3
- Solid Angle
- Irradiance
- Radiance
- BRDF
- Lambertian/Phong BRDF

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A local coordinate system on a surface

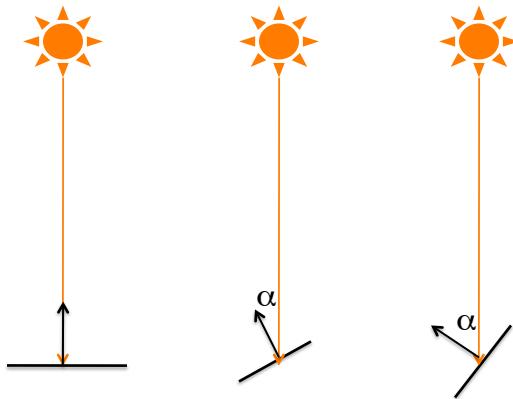
- Consider a point **P** on a surface
- Light arrives at **P** from a hemisphere of directions defined by the surface normal **N**
- We can define a local coordinate system whose origin is **P** and with one axis aligned with **N**
- Convenient to represent in spherical angles.
- θ is well-defined, ϕ isn't



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Foreshortening

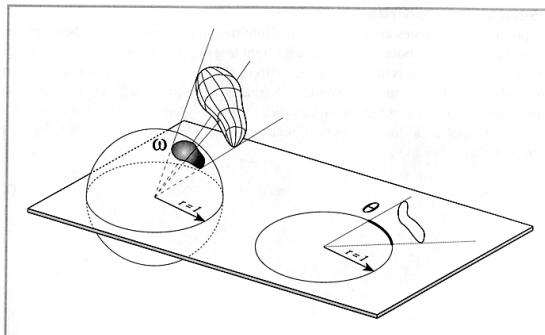


The surface is “foreshortened” by the cosine of the angle α between the normal and direction to a point (e.g., the light).

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Measuring Angle



- The **solid angle** subtended by an object from a point P is the area of the projection of the object onto the unit sphere centered at P
- Definition is analogous to projected angle in 2D
- Measured in *steradians*, sr
- If I'm at P, and I look out, solid angle tells me how much of my view is filled with an object

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Computer Vision I

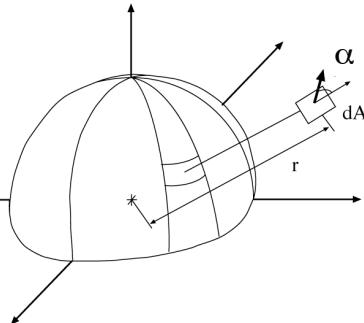
Solid Angle of a patch

- The solid angle subtended by a patch area dA without any foreshortening is

$$d\omega = \frac{dA}{r^2}$$

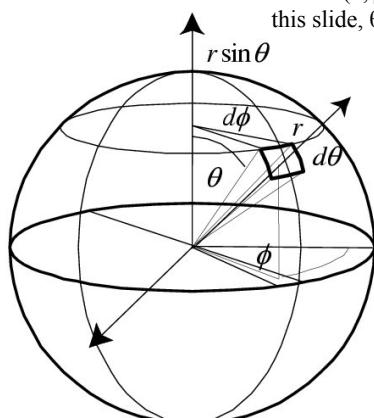
- The solid angle subtended by a patch area dA tilted (foreshortened) at angle α is:

$$d\omega = \frac{dA \cos \alpha}{r^2}$$



Differential Solid Angles

Note: (θ, ϕ) are spherical angles in this slide, θ is not foreshortening.



$$dA = (r d\theta)(r \sin \theta d\phi)$$

$$= r^2 \sin \theta d\theta d\phi$$

-Differential solid angle when representing point on sphere in spherical coordinates

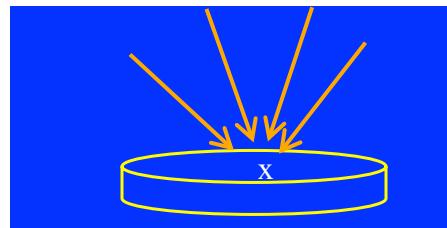
$$d\omega = \frac{dA}{r^2} = \sin \theta d\theta d\phi$$

$$S = \int_0^{\pi} \int_0^{2\pi} \sin \theta d\theta d\phi = 4\pi$$

With foreshortening by α

$$d\omega = \frac{dA}{r^2} \cos \alpha = \sin \theta \cos \alpha d\theta d\phi$$

Irradiance

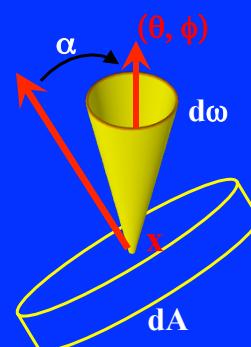


- How much light is arriving at a point x on surface? $E(x)$
- Units of irradiance: Watts/m²
- Recall that power is energy per time, and is measured in Watts (Joules/sec)

Radiance

- **Radiance:** Power traveling at some point in a specified direction, per unit area perpendicular to the direction of travel, per unit solid angle
- Symbol: $L(x, \theta, \phi)$

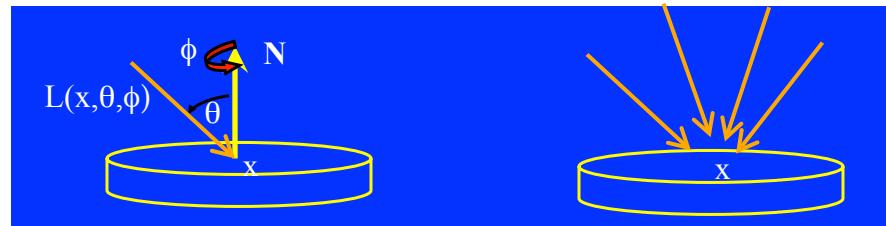
- Units: watts per square meter per steradian : $w/(m^2 sr^1)$



$$L = \frac{P}{(dA \cos \alpha) d\omega}$$

Power emitted from patch, but radiance in direction different from surface normal

Irradiance due to Radiance



A surface experiencing radiance $L(x, \theta, \phi)$ coming in from solid angle $d\omega$ experiences **irradiance**:

$$E(x) = L(x, \theta, \phi) \cos \theta d\omega$$

- Total **Irradiance** arriving at the surface is given by integrating incident irradiances over all incoming angles.

- Total irradiance is

$$\int_{\text{hemisphere}} L(x, \theta, \phi) \cos \theta d\omega = \int_{\text{hemisphere}} L(x, \theta, \phi) \cos \theta \sin \theta d\theta d\phi$$

Radiance transfer

What is the power received by a small area dA_2 at distance r from a small area dA_1 emitting radiance L ?

From definition of radiance

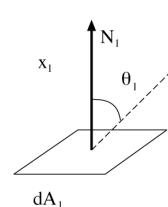
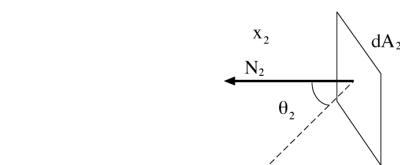
$$L = \frac{P}{(dA \cos \theta) d\omega}$$

From definition of solid angle

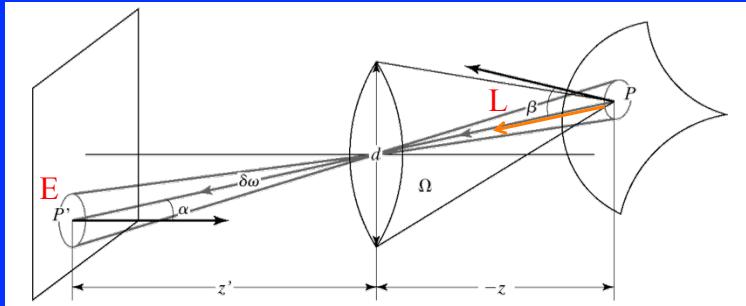
$$d\omega = \frac{dA \cos \theta}{r^2}$$

$$P = L dA_1 \cos \theta_1 d\omega_{1 \rightarrow 2}$$

$$= \frac{L}{r^2} dA_1 dA_2 \cos \theta_1 \cos \theta_2$$



Radiometry of thin lenses

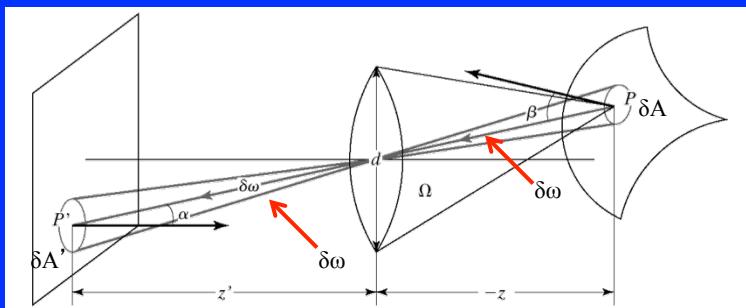


What is image irradiance E for a radiance L emitted from a point P?

Solution is a substantial example problem.

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Radiometry of thin lenses



A small patch on the surface δA projects to a small patch on the image $\delta A'$.

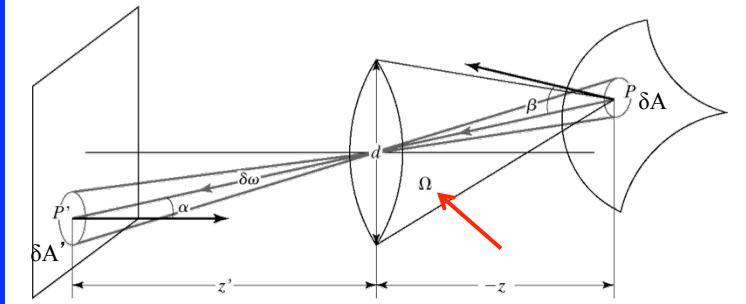
Let $\delta\omega$ be the solid angle subtended by δA (also $\delta A'$) from the center of the lens

$$d\omega = \frac{\delta A' \cos \alpha}{r^2} = \frac{\delta A' \cos \alpha}{(z' / \cos \alpha)^2} = \frac{\delta A \cos \beta}{(z / \cos \alpha)^2} \quad \text{From solid angle equation}$$

$$\frac{\delta A}{\delta A'} = \frac{\cos \alpha}{\cos \beta} \left(\frac{z}{z'} \right)^2 \quad \text{We'll use this later.}$$

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Radiometry of thin lenses



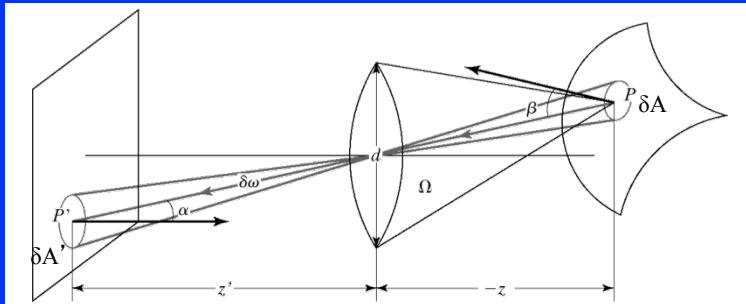
$$d\omega = \frac{\delta A' \cos \alpha}{(z'/\cos \alpha)^2} = \frac{\delta A \cos \beta}{(z'/\cos \alpha)^2} \quad \frac{\delta A}{\delta A'} = \frac{\cos \alpha}{\cos \beta} \left(\frac{z}{z'}\right)^2$$

Let Ω be the solid angle subtended by the lens from P.

$$\Omega = \frac{\pi}{4} \frac{d^2 \cos \alpha}{(z/\cos \alpha)^2} = \frac{\pi}{4} \left(\frac{d}{z}\right)^2 \cos^3 \alpha$$

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Radiometry of thin lenses



$$d\omega = \frac{dA' \cos \alpha}{(z'/\cos \alpha)^2} = \frac{dA \cos \beta}{(z'/\cos \alpha)^2} \quad \frac{\delta A}{\delta A'} = \frac{\cos \alpha}{\cos \beta} \left(\frac{z}{z'}\right)^2$$

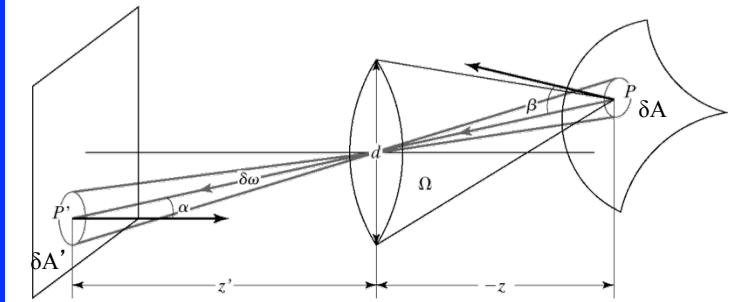
$$\Omega = \frac{\pi}{4} \frac{d^2 \cos \alpha}{(z/\cos \alpha)^2} = \frac{\pi}{4} \left(\frac{d}{z}\right)^2 \cos^3 \alpha$$

The power δP emitted from the patch δA with radiance L and falling on the lens is:

$$\delta P = L \Omega \delta A \cos \beta = \frac{\pi}{4} \left(\frac{d}{z}\right)^2 L \delta A \cos^3 \alpha \cos \beta \quad \delta P \text{ ultimately strikes } \delta A', \text{ and the irradiance } \delta P / \delta A'$$

-CSE 252A, Winter 2007

Radiometry of thin lenses



$$d\omega = \frac{dA' \cos \alpha}{(z'/\cos \alpha)^2} = \frac{dA \cos \beta}{(z'/\cos \alpha)^2} \quad \frac{\delta A}{\delta A'} = \frac{\cos \alpha}{\cos \beta} \left(\frac{z}{z'}\right)^2$$

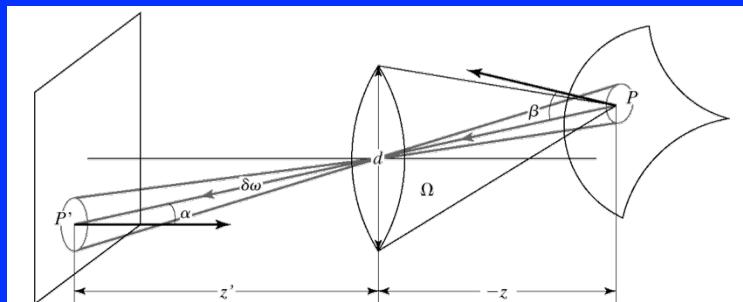
$$\Omega = \frac{\pi}{4} \frac{d^2 \cos \alpha}{(z/\cos \alpha)^2} = \frac{\pi}{4} \left(\frac{d}{z}\right)^2 \cos^3 \alpha$$

$$\delta p = L \Omega \delta A \cos \beta = \frac{\pi}{4} \left(\frac{d}{z}\right)^2 L \delta A \cos^3 \alpha \cos \beta$$

$$E = \frac{\delta P}{\delta A'} = \frac{\pi}{4} \left(\frac{d}{z}\right)^2 L \frac{\delta A}{\delta A'} \cos^3 \alpha \cos \beta = \left[\frac{\pi}{4} \left(\frac{d}{z'}\right)^2 \cos^4 \alpha \right] L$$

Image Irradiance:
Substitute in for $\delta A/\delta A'$

Image Irradiance Equation



E: Image irradiance

L: emitted radiance

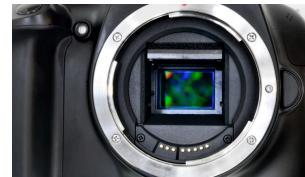
d : Lens diameter

z' : depth of image plane

α : Angle of patch from optical axis

Camera sensor

- Measured pixel intensity is a function of irradiance integrated over
 - Pixel's area
 - over a range of wavelengths
 - for some period of time



$$I = \int_t \int_{\lambda} \int_x \int_y E(x, y, \lambda, t) s(x, y) q(\lambda) dx dy d\lambda dt$$

- Ideally, it's linear to the radiance, but the camera response $C(\cdot)$ may not be linear

$$I = R \left(\int_t \int_{\lambda} \int_x \int_y E(x, y, \lambda, t) s(x, y) q(\lambda) dx dy d\lambda dt \right)$$

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Computer Vision I

Color Cameras



We consider 3 concepts:

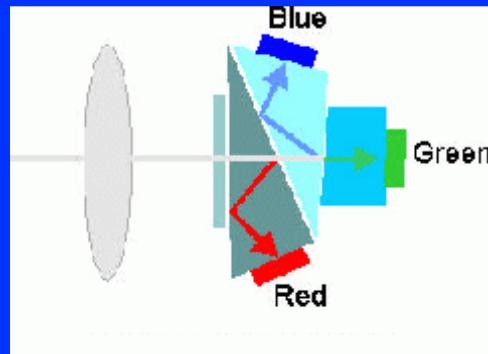
1. Prism (with 3 sensors)
2. Filter mosaic
3. Filter wheel

... and X3

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Prism color camera

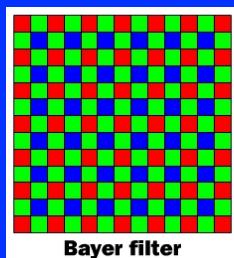
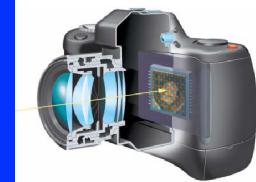
Separate light in 3 beams using dichroic prism
Requires 3 sensors & precise alignment
Good color separation



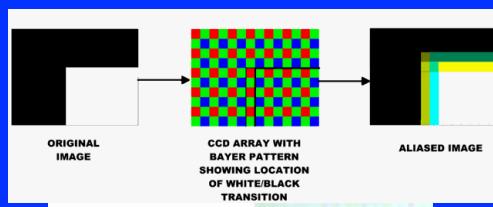
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Filter mosaic

Coat filter directly on sensor



Demosaicing (obtain full colour & full resolution image)

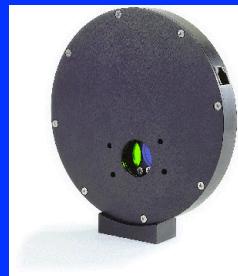


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Filter wheel

Rotate multiple filters in front of lens

Allows more than 3 colour bands



Only suitable for static scenes

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Prism vs. mosaic vs. wheel

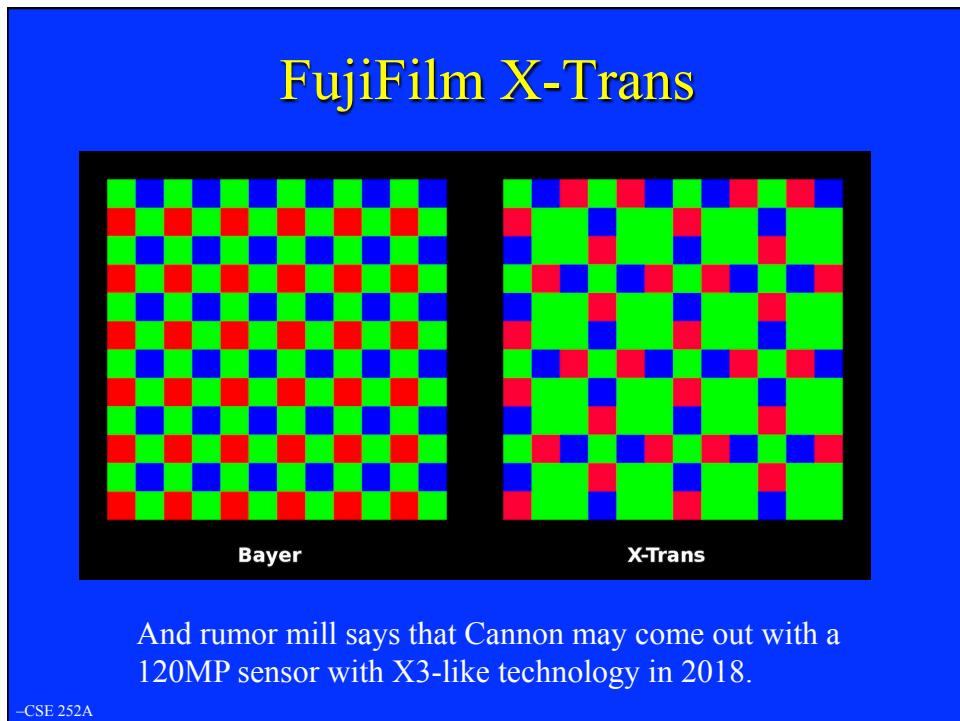
<u>approach</u>	<u>Prism</u>	<u>Mosaic</u>	<u>Wheel</u>
# sensors	3	1	1
Separation	High	Average	Good
Cost	High	Low	Average
Framerate	High	High	Low
Artefacts	Low	Aliasing	Motion
Bands	3	3	3 or more

High-end
cameras

Low-end
cameras

Scientific
applications

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Light at surfaces

Many effects when light strikes a surface -- could be:

- transmitted
 - Skin, glass
- reflected
 - mirror
- scattered
 - milk
- travel along the surface and leave at some other point
- absorbed
 - sweaty skin

Assume that

- surfaces don't fluoresce
 - e.g. scorpions, detergents
- surfaces don't emit light (i.e. are cool)
- all the light leaving a point is due to that arriving at that point

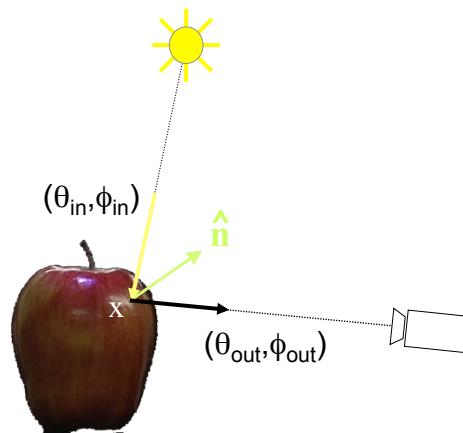
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BRDF

With assumptions in previous slide

- Bi-directional Reflectance Distribution Function
 $\rho(\theta_{in}, \phi_{in}; \theta_{out}, \phi_{out})$
- Ratio of emitted radiance to incident irradiance (units: sr^{-1})
- In local coordinate system at x
 - Incoming light direction:
 θ_{in}, ϕ_{in}
 - Outgoing light direction:
 θ_{out}, ϕ_{out}



$$\rho(x; \theta_{in}, \phi_{in}; \theta_{out}, \phi_{out}) = \frac{L_o(x; \theta_{out}, \phi_{out})}{L_i(x; \theta_{in}, \phi_{in}) \cos \theta_{in} d\omega}$$

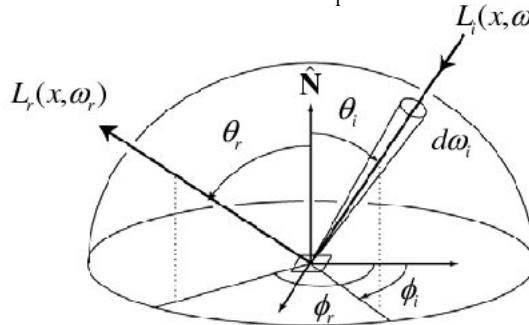
Where ρ is sometimes denoted f_r .

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The Reflection Equation

Emitted radiance in direction f_r for incident radiance L_i .



$$L_r(x, \omega_r) = \int_{H^2} f_r(x, \omega_i \rightarrow \omega_r) L_i(x, \omega_i) \cos \theta_i d\omega_i$$

CS348B Lecture 10

where $\omega_i = (\theta_i, \phi_i)$

Pat Hanrahan, Spring 2002

Computer Vision

Properties of BRDFs

1. Non-negative: $\rho(\theta_{in}, \phi_{in}; \theta_{out}, \phi_{out}) \geq 0$
2. Helmholtz Reciprocity Principle:
$$\rho(\theta_{in}, \phi_{in}; \theta_{out}, \phi_{out}) = \rho(\theta_{out}, \phi_{out}; \theta_{in}, \phi_{in})$$
3. Total energy leaving a surface must be less than total energy arriving at the surface

$$\int_{\Omega_i} L_i(\mathbf{x}, \theta_i, \phi_i) \cos \theta_i d\omega_i \geq \int_{\Omega_o} \left[\int_{\Omega_i} \rho(\theta_i, \phi_i; \theta_o, \phi_o) L_i(\mathbf{x}, \theta_i, \phi_i) \cos \theta_i d\omega_i \right] \cos \theta_o d\omega_o$$

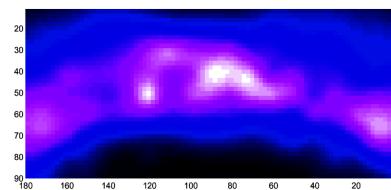
Surface Reflectance Models

Common Models

- Lambertian
- Phong
- Physics-based
 - Specular [Blinn 1977], [Cook-Torrance 1982], [Ward 1992]
 - Diffuse [Hanrahan, Kreuger 1993]
 - Generalized Lambertian [Oren, Nayar 1995]
 - Thoroughly Pitted Surfaces [Koenderink et al 1999]
- Phenomenological
 - [Koenderink, Van Doorn 1996]

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Arbitrary Reflectance



- Non-parametric model
- Anisotropic
- Non-uniform over surface
- BRDF Measurement [Dana et al, 1999], [Marschner]

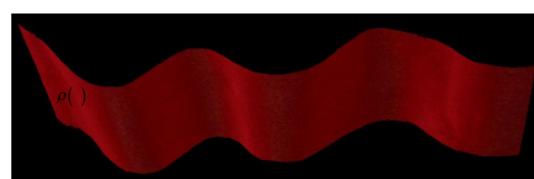
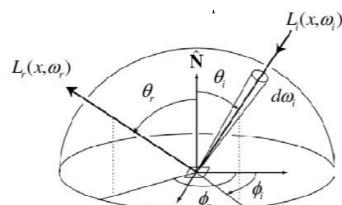
Specialized

- Hair, skin, threads, paper [Jensen et al]
- Fur

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Important class of BRDFs: Isotropic BRDF

$$\rho(\theta_i, \phi_i; \theta_o, \phi_o) = \rho_r(\theta_i, \theta_o, \phi_i - \phi_o)$$

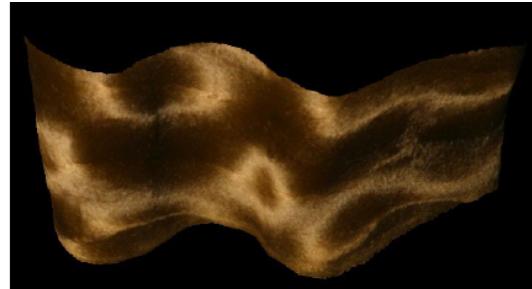
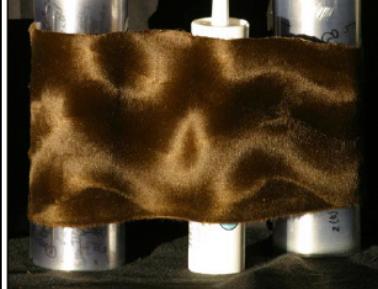


Isotropic BRDF's are symmetric about the surface normal. If the surface is rotated about the normal for the same incident and emitting directions, the value of the BRDF is the same.

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Anisotropic BRDF



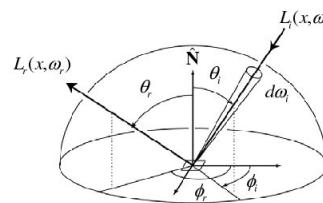
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Lambertian (Diffuse) Surface

- BRDF is a constant called the albedo. $\rho(x; \theta_{in}, \phi_{in}; \theta_{out}, \phi_{out}) = K$
- Emitted radiance is NOT a function of outgoing direction – i.e. constant in all directions.
- For lighting coming in single direction ω_i , emitted radiance is proportional to cosine of the angle between normal and light direction

$$L_r = K \hat{N} \cdot \omega_i$$



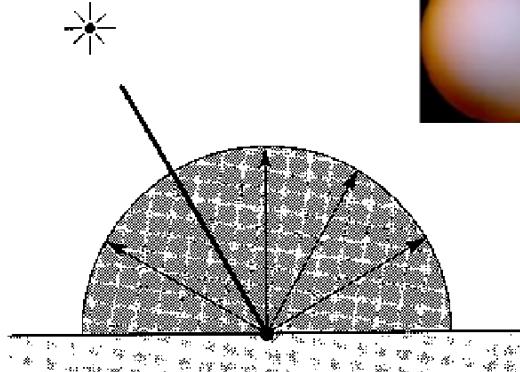
$$L_r(x, \omega_r) = \int_{H^2} f_r(x, \omega_i \rightarrow \omega_r) L_i(x, \omega_i) \cos \theta_i d\omega_i$$

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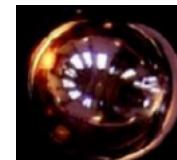
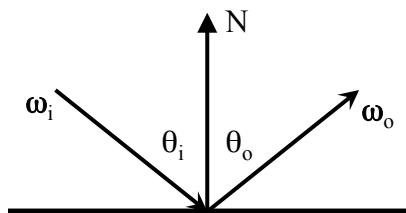
Lambertian reflection

- Lambertian
- Matte
- Diffuse



Light emitted equally in all directions.

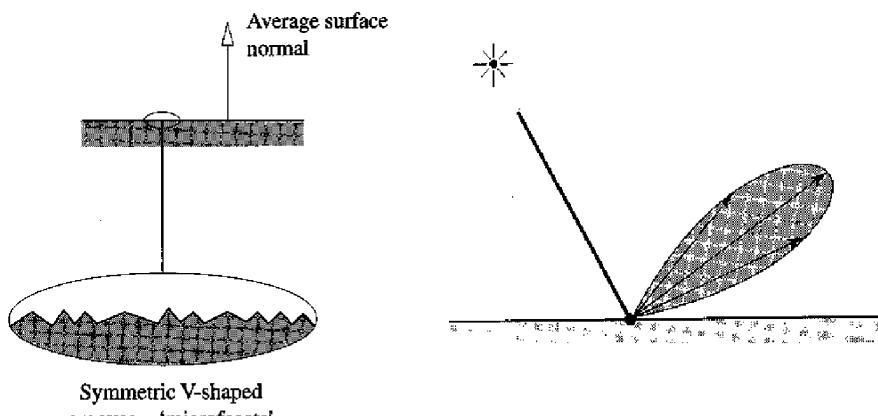
Specular Reflection: Smooth Surface



- N, ω_i, ω_o are coplanar
- $\theta_i = \theta_o$

Speculum – Latin for “Mirror”

Rough Specular Surface



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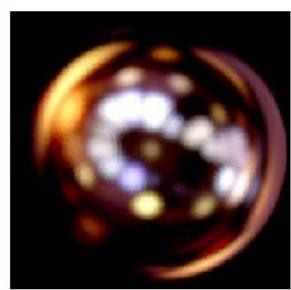
Phong Model



Mirror



Diffuse



CS348B Lecture 10



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Pat Hanrahan, Spring 2002

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Non-Lambertian reflectance



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Computer Vision I

General BRDF: e.g. Velvet



Portrait of Sir Thomas More, Hans Holbein the Younger, 1527

[After Koenderink et al, 1998]

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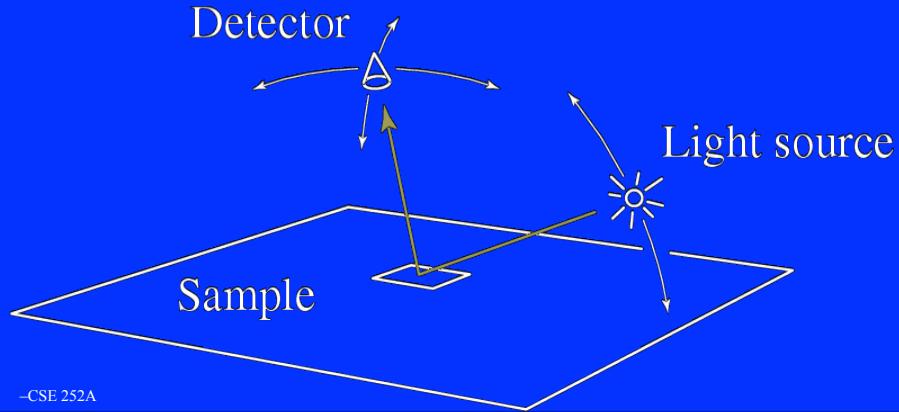
Ways to measure BRDFs

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Gonioreflectometers

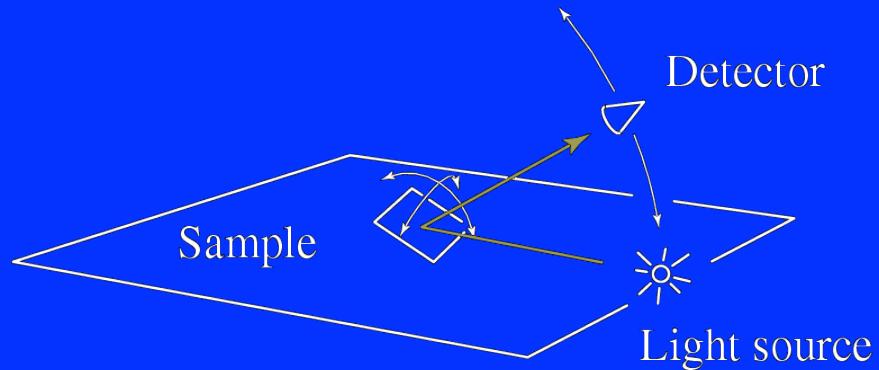
- Three degrees of freedom spread among light source, detector, and/or sample



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Gonioreflectometers

- Three degrees of freedom spread among light source, **detector**, and/or **sample**



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Gonioreflectometers

- Can add fourth degree of freedom to measure anisotropic BRDFs

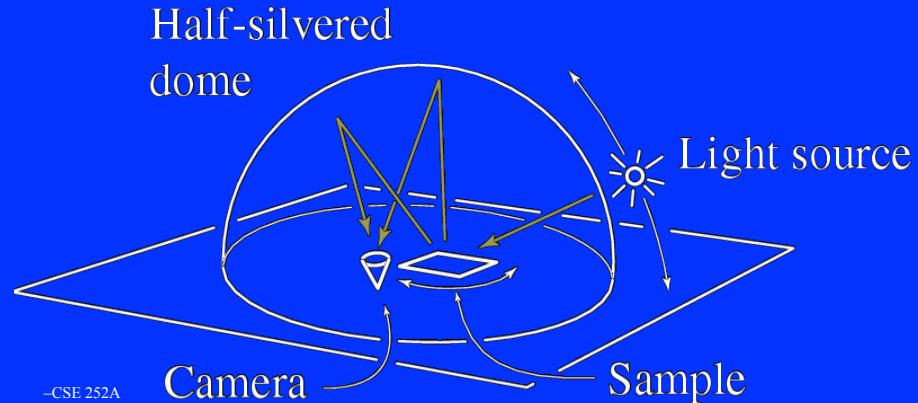


4 degree-of-freedom gantry

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Ward's BRDF Measurement Setup

- Collect reflected light with hemispherical (should be ellipsoidal) mirror [SIGGRAPH 92]



Ward's BRDF Measurement Setup

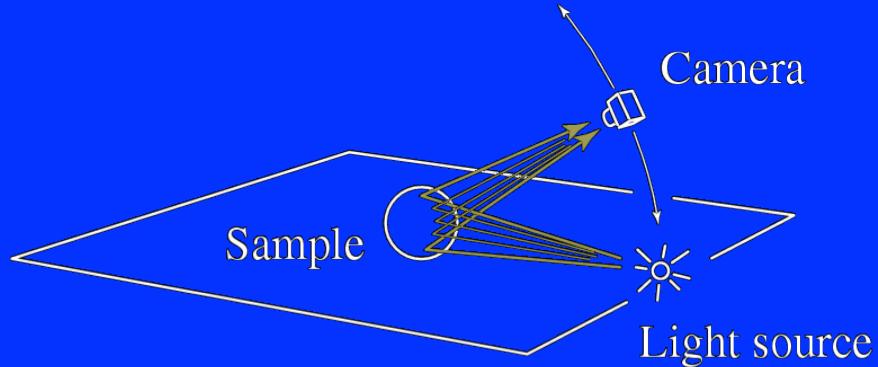
- Result: each image captures light at all exitant angles



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Marschner's Image-Based BRDF Measurement

- For uniform BRDF, capture 2-D slice corresponding to variations in normals



BRDF Not Always Appropriate



BRDF

BSSRDF

<http://graphics.stanford.edu/papers/bssrdf/>
(Jensen, Marschner, Levoy, Hanrahan)

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Light sources and shading

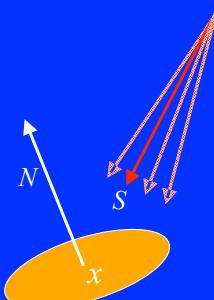
- A light source is a power source that emits light (instead of reflecting it)
- Laser – a single ray
- Point source – like a light bulb
- Line source – fluorescent light bulb
- Area source

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Nearby point source model

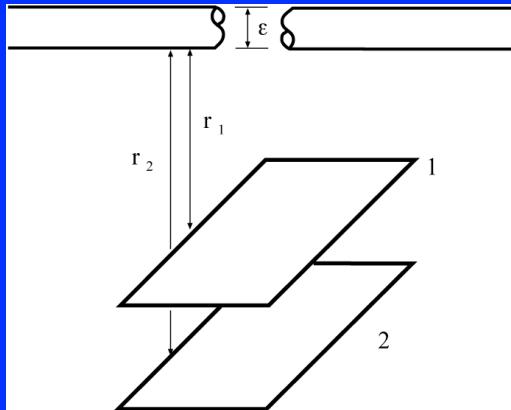
$$L = \rho_d(x) \left(\frac{\hat{N}(x) \cdot S(x)}{r(x)^2} \right)$$

- N is the surface normal
- ρ_d is diffuse (Lambertian) albedo
- S is source vector - a vector from x to the source, whose length is the intensity term



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Nearby Line Source



Intensity due to line source varies with inverse distance,
if the source is long enough

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Distant Point Source Model

- Assume that all points in the model are close to each other with respect to the distance to the source. Then the source vector doesn't vary much, and the distance doesn't vary much either, and we can roll the constants together to get:

$$L = \rho_d(x) N(x) \cdot S(x)$$



- N is the surface normal
- ρ_d is diffuse (Lambertian) albedo
- S is source vector - a vector in source direction, whose length is the intensity term

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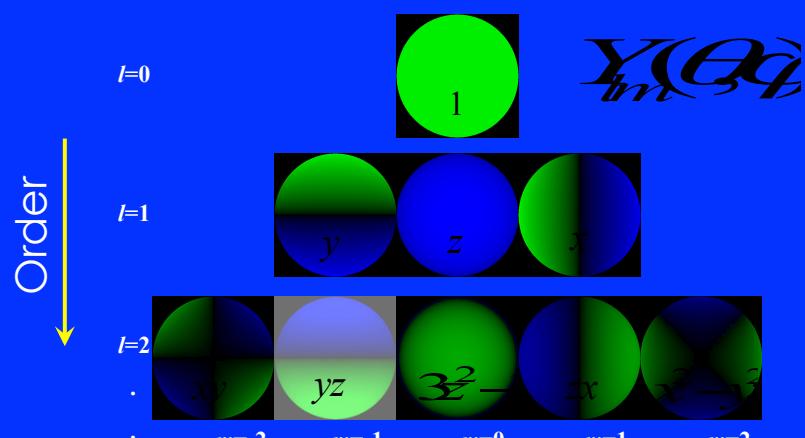
Lighting at infinity

- Direction is a three vector \mathbf{s} , with $|\mathbf{s}| = 1$.
- Described as function on a sphere: radiance as a function of direction $r(\mathbf{s})$
- Single point source is a delta function at some direction
- Multiple point sources: sum of delta functions



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Diffuse lighting at infinity: Spherical Harmonics



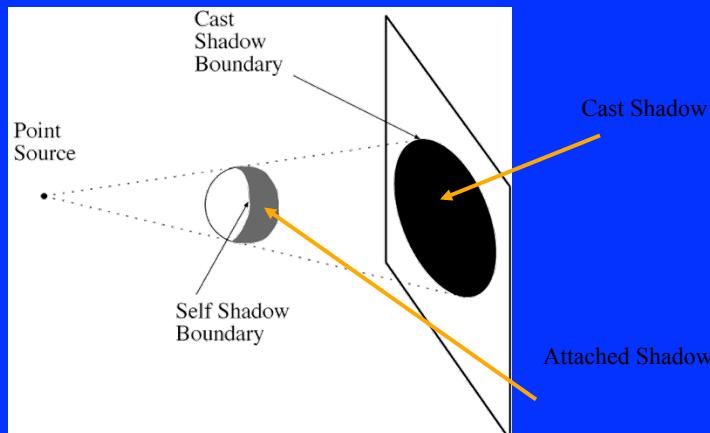
Green: Positive
Blue: Negative

(Borrowed from: Ramamoorthi, Hanrahan, SIGGRAPH'01)

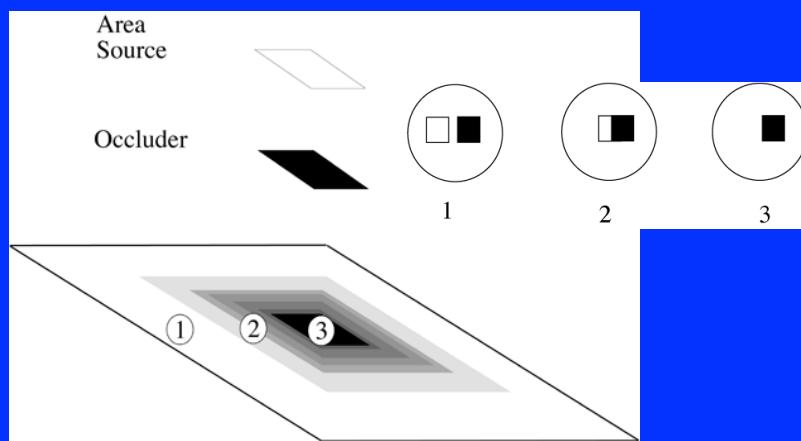
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Shadows cast by a point source

- A point that can't see the source is in shadow
- For point sources, the geometry is simple



Area Source Shadows



Shading models

Local shading model

- Surface has incident radiance due only to sources visible at each point
- Advantages:
 - often easy to manipulate, expressions easy
 - supports quite simple theories of how shape information can be extracted from shading
- Used in vision & real time graphics

Global shading model

- surface radiosity is due to radiance reflected from other surfaces as well as from surfaces
- Advantages:
 - usually very accurate
- Disadvantage:
 - extremely difficult to infer anything from shading values
- Rarely used in vision, often in photorealistic graphics

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Illumination from an infinitely distant point source, in this direction



At the top, geometry of a gutter with triangular cross-section; below, predicted radiosity solutions, scaled to lie on top of each other, for different albedos of the geometry. When albedo is close to zero, shading follows a local model; when it is close to one, there are substantial reflexes.

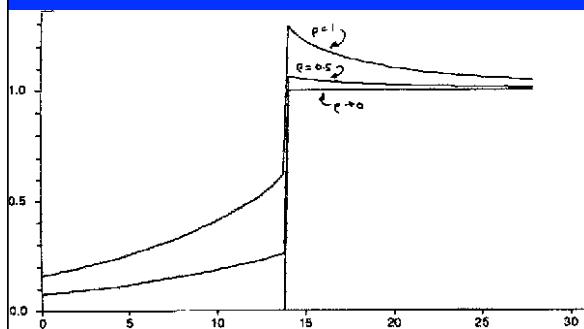


Figure from "Mutual Illumination," by D.A. Forsyth and A.P. Zisserman, Proc. CVPR, 1989, copyright 1989 IEEE
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Irradiance observed in an image of
this geometry for a real white
gutter.

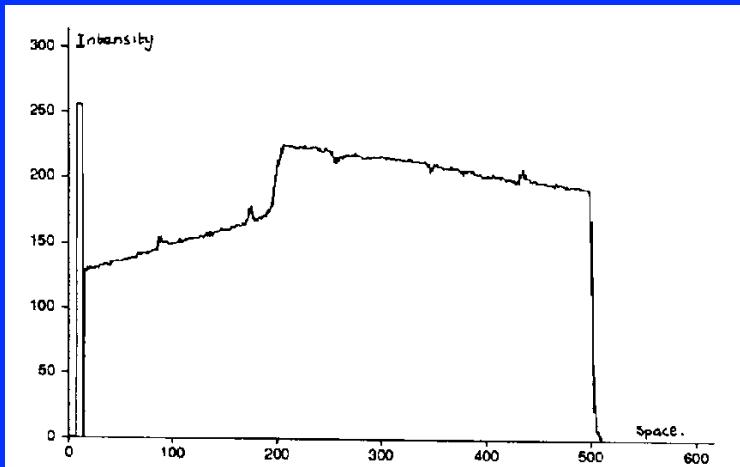


Figure from "Mutual Illumination," by D.A. Forsyth and A.P. Zisserman, Proc. CVPR, 1989, copyright 1989 IEEE
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