

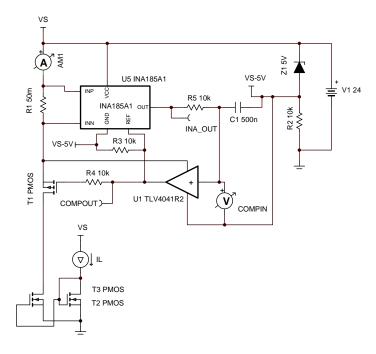
# Precision Over-Current Latch Circuit

### **Design Goals**

LOAD CURRENT (I <sub>L</sub> )	SYSTEM SUPPLY (V <sub>s</sub> )	CURRENT SENSE AMP	COMPARATOR (	OUTPUT STATUS
Over Current (I <sub>OC</sub> )	Typical	Gain	Over Current	Normal Operation
200mA	24 V	20 V/V	$V_{OH} = V_{S}$	V <sub>OL</sub> = V <sub>S</sub> - 5 V

### **Design Description**

This high-side, current sensing solution uses a current sense amplifier, a comparator with an integrated reference, and a P-channel MOSFET to create an over-current latch circuit. When a load current greater than 200 mA is detected, the circuit disconnects the system from its power source. Since the comparator drives the gate of the P-channel MOSFET and feeds the signal back into the reference pin of the current sense amplifier, the comparator output will latch (hold the gate source voltage of the P-channel MOSFET to 0 V) until power to the circuit is cycled.



### **Design Notes**

- 1. Select a precision, current sense amplifier (INA) with an external reference pin so its output voltage can be adjusted.
- 2. Select a comparator with a rail-to-rail input so its output will be valid over the entire operating voltage range of the current sense amplifier.
- 3. Select a comparator with a push-pull output stage that can drive the gate of a MOSFET and an integrated reference to optimize circuit accuracy.
- 4. Create a floating 5V supply that can power the INA and comparator.



### **Design Steps**

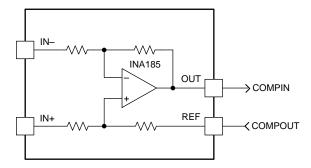
1. Select the value of R<sub>1</sub> so V<sub>SHUNT</sub> is at least 100x greater than the current sense amplifier input offset voltage (V<sub>OS</sub>). Note that making R<sub>6</sub> very large will improve OC detection accuracy but will reduce supply headroom and power disssipation.

$$\begin{split} &V_{SHUNT} = (I_{OC} \times R_1) \ge 100 \times V_{OS} \\ &\text{Set} \ \ R_1 \ge \frac{100 \times V_{OS}}{I_{OC}} = 50 \text{m} \Omega \ \ \text{for} \ \ I_{OC} = 200 \text{mA} \ \ \& \ \ V_{OS} = 100 \mu V_{OS} \end{split}$$

2. Determine the desired gain (A<sub>V</sub>) option for the INA based on the switching threshold of the comparator. When the load current (I<sub>L</sub>) reaches the over-current threshold (I<sub>OC</sub>), the INA output must cross the switching threshold (V<sub>TH</sub>) of the comparator.

$$\begin{split} &V_{TH}\!=(I_{OC}\!\times\!R_1) \times A_V\!=0\,.\,2V\\ &\text{Set}\ A_V\!=\tfrac{V_{TH}}{I_{OC}\!\times\!R_1}\!=\tfrac{0.2}{0.2\!\times\!0.05}\!=20V\,/\,V\ \text{for}\ R_1\!=50\text{m}\Omega \end{split}$$

- 3. Since many INA's and comparators have 5V operating voltage ranges, a 5V supply voltage needs to be derived from the system supply  $V_s$ . In addition, the 5V supply needs to float below  $V_s$  so the comparator output can drive the source-gate voltage of the P-channel MOSFET to 0V when an over-current condition occurs and 5V when the load current is less than  $I_{oc}$ . The method used in this circuit is a 5V zener diode with a  $10k\Omega$  bias resistor ( $R_2$ ). Other options such as shunt regulators can also be utilized as long as proper bias current through the device is maintained.
- 4. A low pass filter is added between the INA output and the comparator input to attenuate any high frequency current spikes. It is more important to trigger the over-current latch with a delay than to falsely disconnect the system from the supply voltage. The low pass filter is derived from R<sub>5</sub> and C<sub>1</sub>. Since the switching threshold of the comparator is 0.2V, the delay is less than 1 time constant (R<sub>5</sub>×C<sub>1</sub>=5ms).
- 5. A current limiting resistor  $R_4$  is inserted between the comparator output and the gate of the P-channel MOSFET. Setting  $R_4$  to  $10k\Omega$  reduces current spikes on the supply when the comparator output needs to charge the MOSFET gate-source capacitance as a compromise to increasing the charge time. Inserting  $R_4$  also serves the purpose of protecting the comparator output from any supply transients that can be present on the supply line.
- 6. The output of the comparator is directly connected to the REF pin of the INA in order to apply an offset to the INA's output voltage. When  $I_L < I_{OC}$ , the comparator output is low (equal to  $V_S$ -5V) and no offset is added to the INA. However, when  $I_L > I_{OC}$ , the comparator output goes high (equal to  $V_S$ ) and a 5V offset is added to the INA. This offset causes the INA output to saturate at a level equal to  $V_S$ . Since an INA output level of  $V_S$  is higher than the  $V_{TH}$  of the comparator, the comparator output will remain high. This condition is referred to as a "latched" output state since the circuit will remain in this state until power to the circuit is cycled.

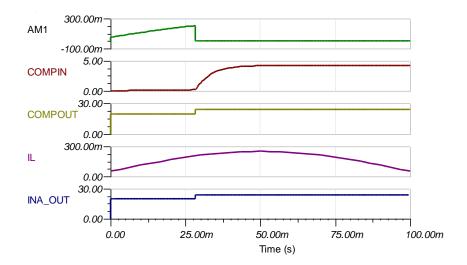


- 7.  $R_3$  is added between the INA reference pin (REF) and GND ( $V_S$ -5V) to ensure a proper ground path as the 5V supply ramps up to the comparator minimum operating voltage.
- 8. If a latching feature is not preferred, the comparator output can be disconnected from the current sense amplifier reference pin and R<sub>3</sub> can be replaced with a short. In this configuration, the circuit will behave as a 200 mA current limiter.



## **Design Simulations**

## **Transient Simulation Results**





## **Design References**

See Circuit SPICE Simulation File SBVM944, http://www.ti.com/lit/zip/SBVM944.

## **Design Featured Comparator**

TLV4041R2			
V <sub>s</sub>	1.6 V to 5.5 V		
V <sub>inCM</sub>	Rail-to-rail		
V <sub>out</sub>	Push-Pull		
Integrated Reference	200 mV ± 3 mV		
lα	2 μΑ		
t <sub>PD</sub>	360 ns		
www.ti.com/pro	duct/TLV4041		

## **Design Featured Current Sense Amplifier**

	INA185
V <sub>s</sub>	2.7 V to 5.5 V
V <sub>inCM</sub>	-0.2 V to 26 V
Gain Options	20 V/V, 50 V/V, 100 V/V, 200 V/V
Gain Error	0.2 %
V <sub>os</sub>	100 μV (Α1), 25 μV (Α2, Α3, Α4)
Ι <sub>Q</sub>	200 μΑ
	www.ti.com/product/INA185

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