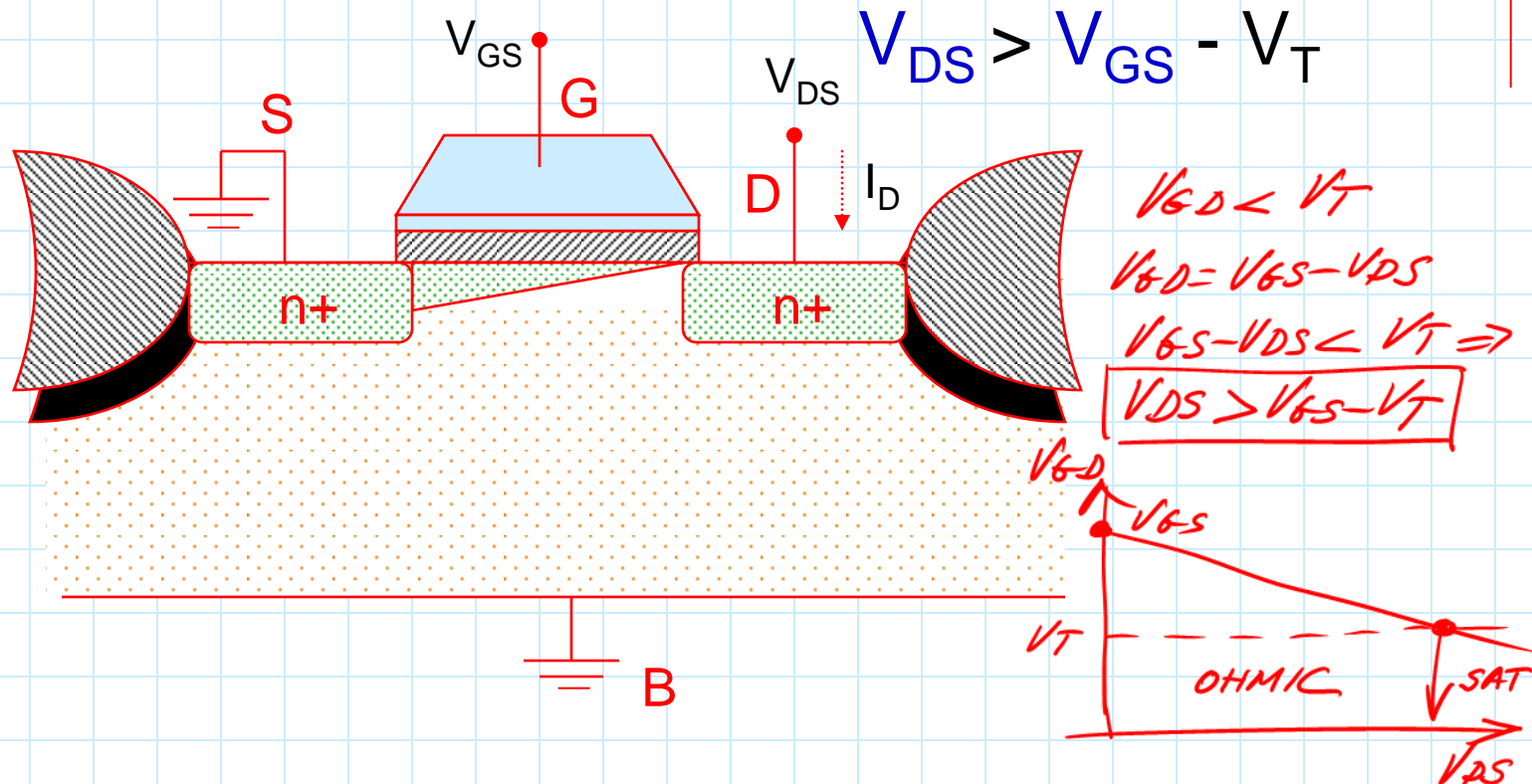


# Operating regions: saturation region

Assuming  $V_{GS} > V_T$



The channel is pinched-off (small channel near D), and the current remains constant

# Operating regions: saturation region(2)

Condition:  $V_{DS} > V_{GS} - V_T$

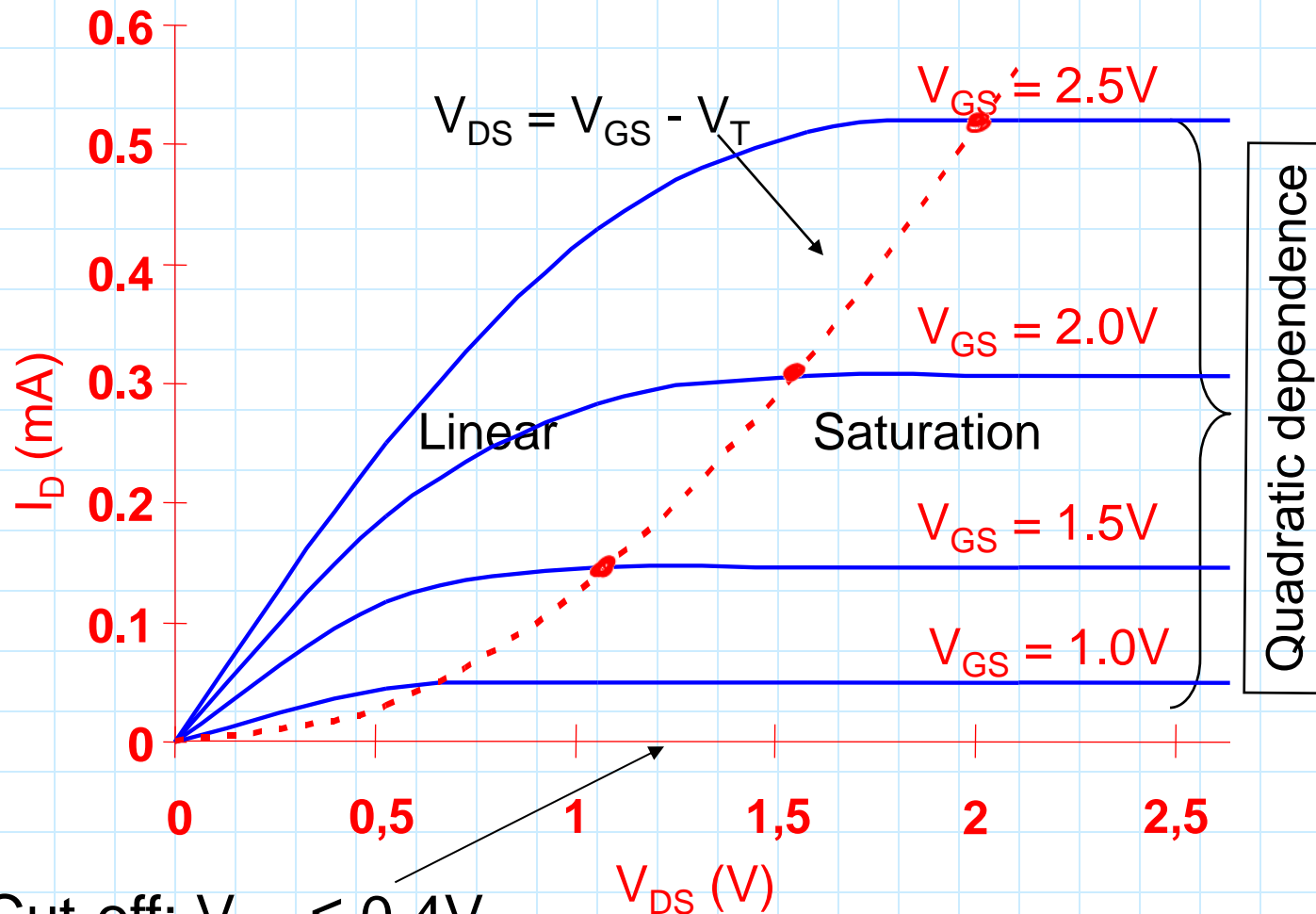
V/I function:  $I_{DS} = K (V_{GS} - V_T)^2$  (Saturation parable)

The channel is *pinched-off* →

For a fixed  $V_{GS}$ , the current  $I_{DS} \approx \text{constant}$ , and  
indep. of  $V_{DS}$

The Mosfet is equivalent to a current source ( $I_{DS}$ )  
controlled by voltage ( $V_{GS}$ )

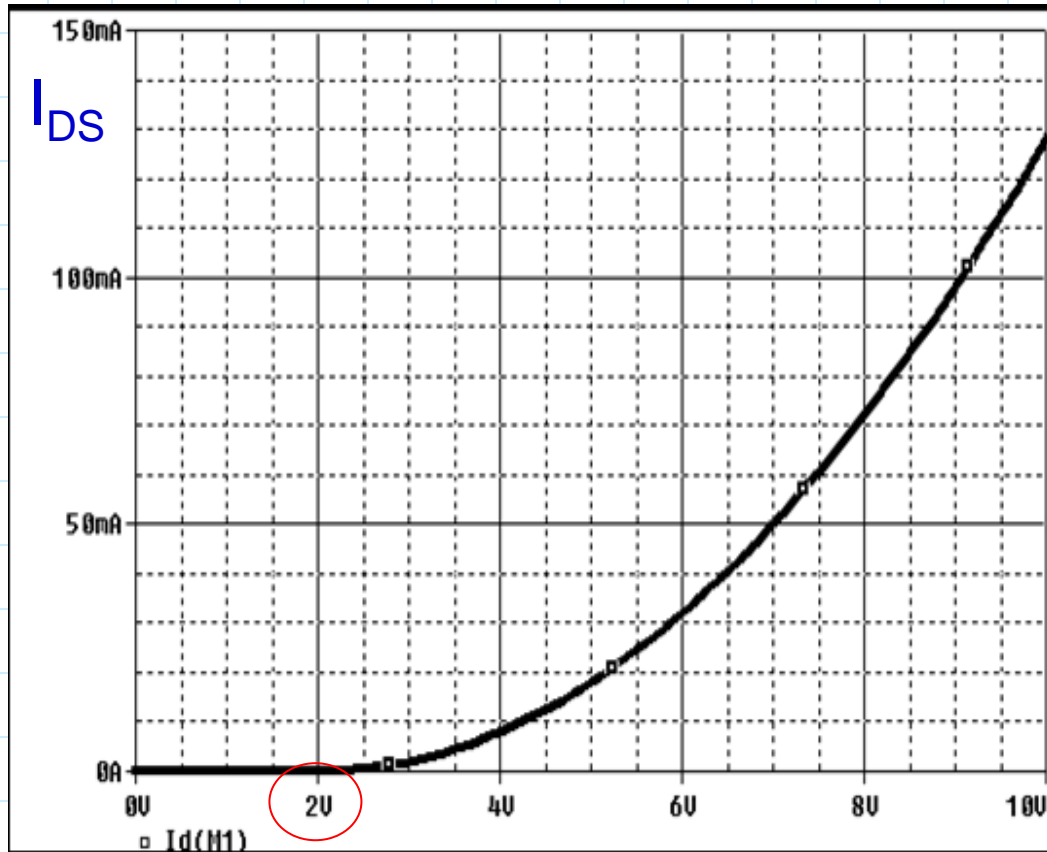
# I-V curves of the NMOS



Cut-off:  $V_{GS} \leq 0.4V$

Example: NMOS Transistor:  $V_T = 0.4V$   $K = 0.12mA/V^2$

# $I_{DS}$ versus $V_{GS}$ in saturation region



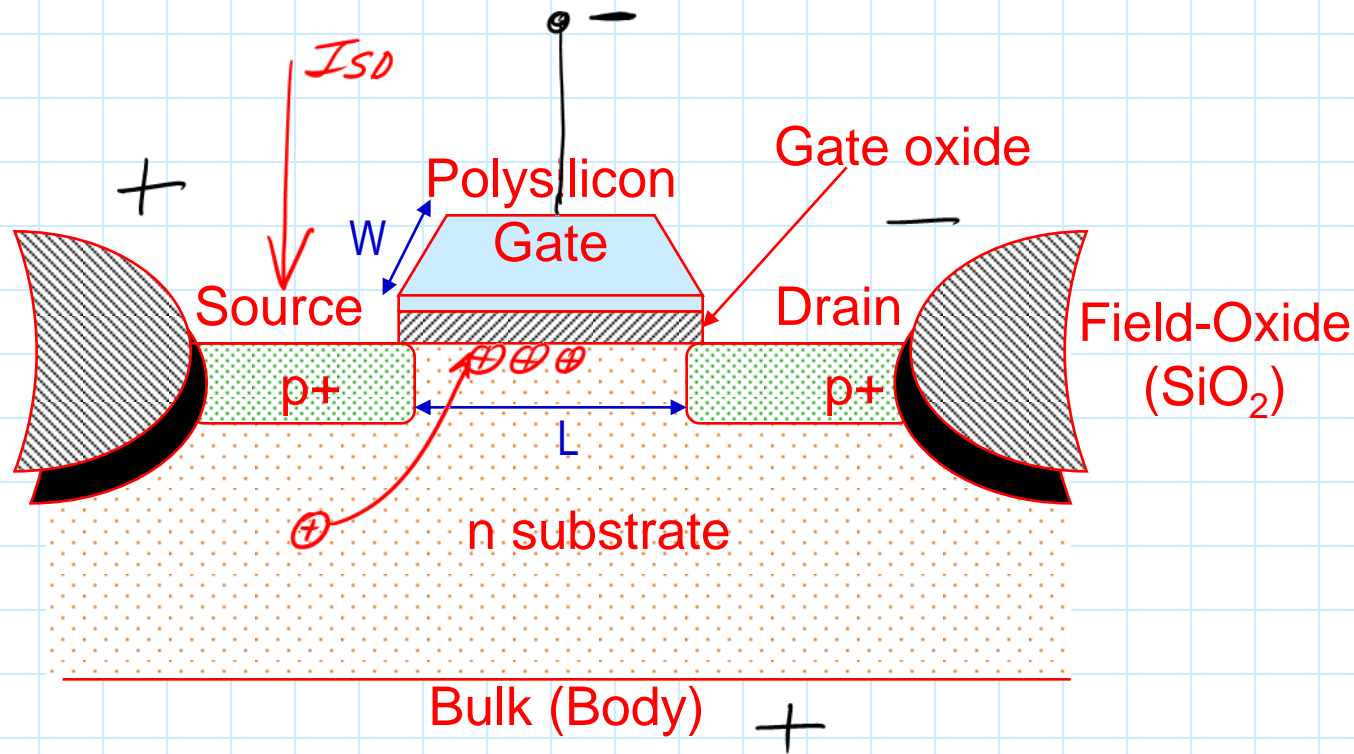
Saturation parable:

$$I_{DS} = K (V_{GS} - V_T)^2$$

$$V_T = 2V$$

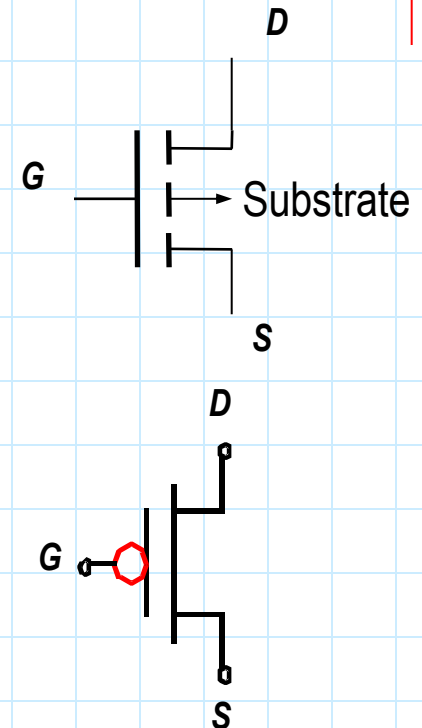
$$V_{GS} \leq V_T \rightarrow I_D = 0$$

# PMOS Transistor: cross section

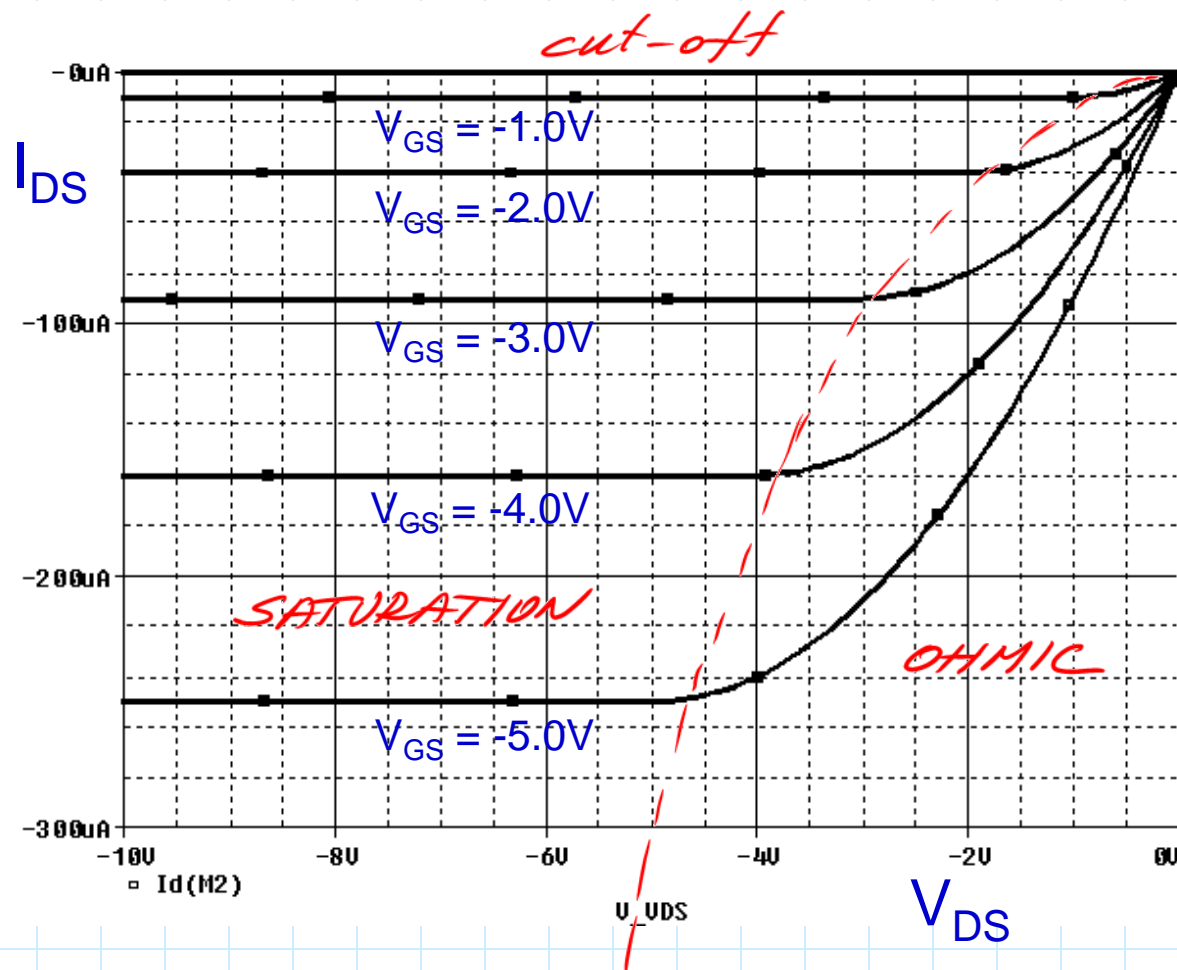


$$V_{GS} < -V_T \Rightarrow T_{ON}$$

Symbols



# PMOS. Characteristic curves



All variables are negative!

$$V_{GS} < 0, V_{DS} < 0,$$

$$I_{DS} < 0 \rightarrow I_{SD} > 0$$

Conduction:  $V_{GS} < -V_T$

# The PMOS transistor: summary

- Cut-off:  $V_{GS} \geq -V_T$

- Saturation:

$$V_{DS} < V_{GS} + V_T$$

$$I_{SD} = K (V_{GS} + V_T)^2$$

- Ohmic:

$$R_{ON} \approx \left| \frac{1}{2 \cdot K (V_{GS} + V_T)} \right|$$

$$\begin{aligned} V_{DS} &\geq V_{GS} + V_T \\ I_{SD} &= K [2(V_{GS} + V_T)V_{DS} - V_{DS}^2] \\ V_{DS} \ll V_{GS} + V_T &\Rightarrow I_{SD} = 2K(V_{GS} + V_T)V_{DS} \end{aligned}$$

(considering  $K$  and  $V_T$  as absolute values,  $V_{GS} < 0$ ,  $V_{DS} < 0$ )

- Less use than N-channel MOSFETS, as holes mobility is smaller than electrons mobility:

- ◆ Slower than the NMOS  $\rightarrow (K_p)_p = \mu_p C_{ox} \frac{W}{L}$ ;  $\mu_p < \mu_n$ ;  $(K_p)_p < (K_p)_n$
- ◆ They need more  $W/L \rightarrow$  bigger than NMOS (more space occupied)

# MOSFET: Summary of some formulas

NMOS		PMOS
$V_{GS} > V_T$	CONDUCTS	$V_{GS} < -V_T$
$V_{DS} > V_{GS} - V_T$	SATURATION condition	$V_{DS} < V_{GS} + V_T$
$I_{DS} = K (V_{GS} - V_T)^2$	SATURATION	$I_{SD} = K (V_{GS} + V_T)^2$
$I_{DS} = K [2(V_{GS} - V_T)V_{DS} - V_{DS}^2]$ $V_{DS} \leq V_{GS} - V_T$ $R_{ON} \approx \frac{1}{2 \cdot K(V_{GS} - V_T)}$	OHMIC or LINEAR	$I_{SD} = K [2(V_{GS} + V_T)V_{DS} - V_{DS}^2]$ $V_{DS} \geq V_{GS} + V_T$ $R_{ON} \approx \left  \frac{1}{2 \cdot K(V_{GS} + V_T)} \right $

(Taking the absolute value of  $V_T$  and  $K$  in all formulas)



# Equivalences and differences between Mosfet-BJTs

## Terminals

MOSFET	BJT
DRAIN	COLLECTOR
SOURCE	EMITTER
GATE	BASE

BJT:  $I_B > 0$  for conducting

Mosfet:  $I_G = 0$  always!

## Working regions

MOSFET	BJT
CUT-OFF REGION	CUT-OFF REGION
SATURATION REGION	ACTIVE REGION
OHMIC \ LINEAR REGIN	SATURATION REGION

Mosfet's Saturation : maximum  $I_{DS}$  for a given  $V_{GS}$

BJT's saturation: maximum  $I_C$  for a given biass circuit

# Enhancement MOSFET Biassing (1)

Equations to analyze the Mosfets biassing circuits

1.- Input loop: **G-S** → loop equation with  $V_{GS}$

2.- **Assuming** saturation → saturation equation

$$\text{NMOS: } I_{DS} = K (V_{GS} - V_T)^2 \quad \text{PMOS: } I_{SD} = K (V_{GS} + V_T)^2$$

*(With  $V_{GS}$ , checkout if MOSFET is conducting)*

3.- Output loop **D-S** → loop equation with  $V_{DS}$

4.- **Checkout** of saturation

$$\text{NMOS: } V_{DS} > V_{GS} - V_T$$

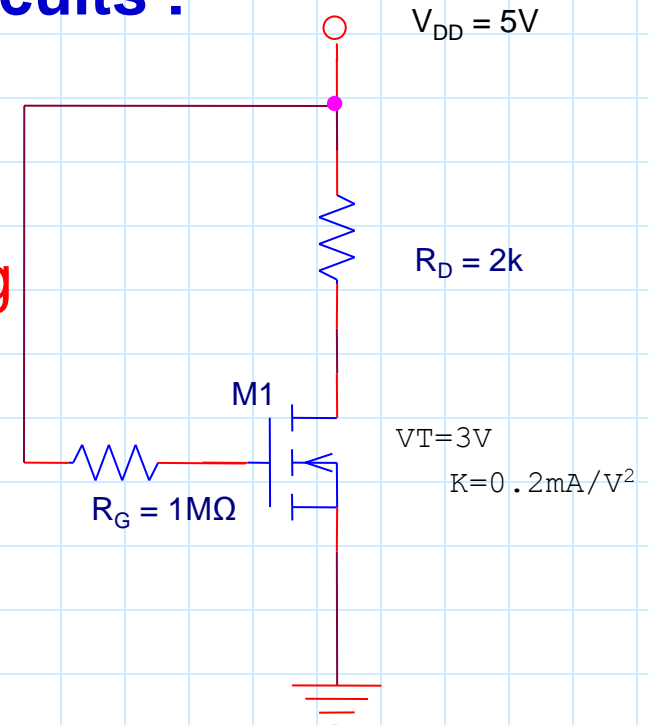
$$\text{PMOS: } V_{DS} < V_{GS} + V_T$$

*(If not satisfied, return to step 2, using the equation of the linear region, and redo the calculations)*

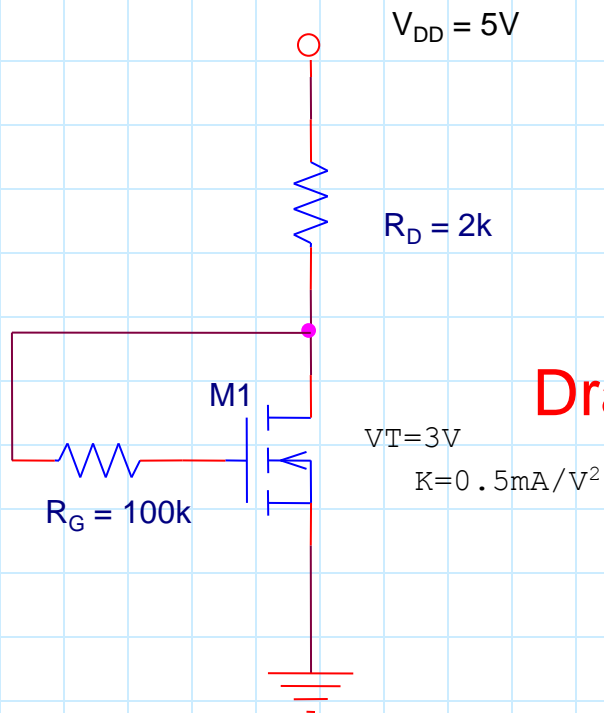
# Enhancement MOSFET. Biassing (2)

Examples of Biassing circuits :

Fixed biassing

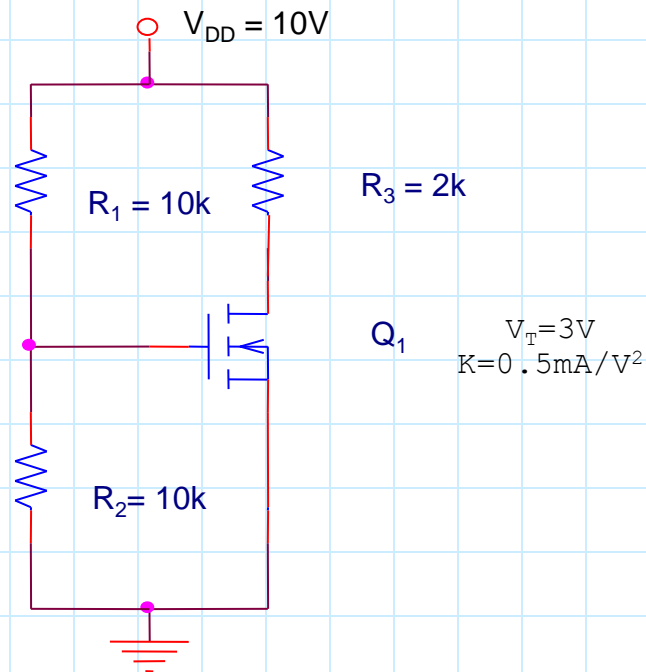


Drain feedback



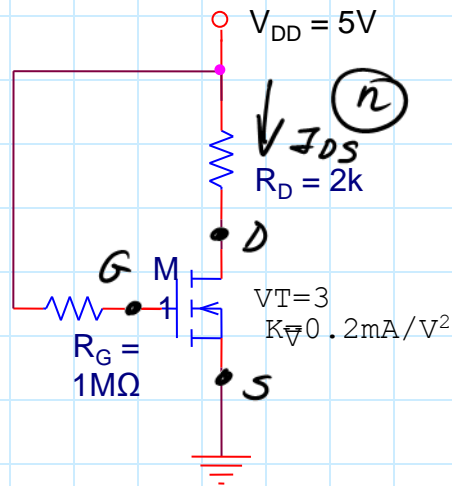
# Enhancement MOSFET. Biassing (3)

Biassing with  
resistor divider



2 solutions for  $I_{DS} \rightarrow$  you choose the one for which  $V_{GS} > V_T$

# Enhancement MOSFET. Biassing (2)



Fixed biassing

$$V_G = V_{DD} \Rightarrow V_{GS} = V_{DD} = 5V > V_T \Rightarrow \text{TON}$$

assume saturation

$$I_{DS} = K(V_{GS} - V_T)^2 = 0.2(5 - 3)^2 = 0.8 \text{ mA}$$

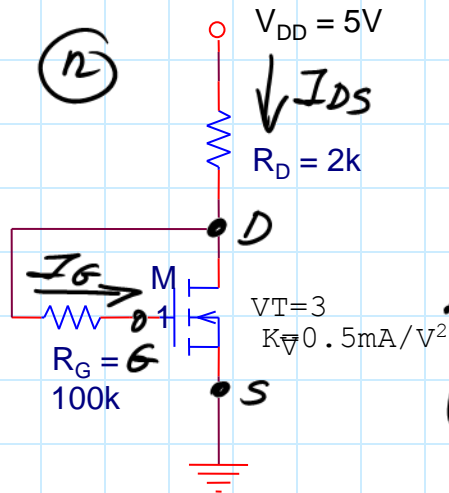
Output loop:

$$V_{DS} = V_{DD} - I_{DS} R_D = 5 - 0.8 \cdot 2 = 3.4V$$

as  $V_{DS} = 3.4V > V_{GS} - V_T = 2V \Rightarrow$  T is saturated  $\Rightarrow$

$$Q(V_{GS} = 5V, I_{DS} = 0.8 \text{ mA}, V_{DS} = 3.4V)$$

# Enhancement MOSFET. Biassing (2)



$$I_G = 0 \Rightarrow V_D = V_G \Rightarrow V_{DS} = V_{GS}$$

$$\text{as } V_{DS} > V_{DS} - V_T = V_{GS} - V_T \Rightarrow \text{TRANSISTOR SATURATED.}$$

$$\left\{ \begin{array}{l} a) I_{DS} = K(V_{GS} - V_T)^2 = K(V_{DS} - V_T)^2 = 0.5(V_{DS} - 3)^2 \\ b) \text{ output loop:} \\ I_{DS} = \frac{V_{DD} - V_{DS}}{R_D} = \frac{5 - V_{DS}}{2} \end{array} \right.$$

**Drain feedback** From a) and b):  $\frac{5 - V_{DS}}{2} = 0.5(V_{DS} - 3)^2$

$$5 - V_{DS} = V_{DS}^2 - 6V_{DS} + 9$$

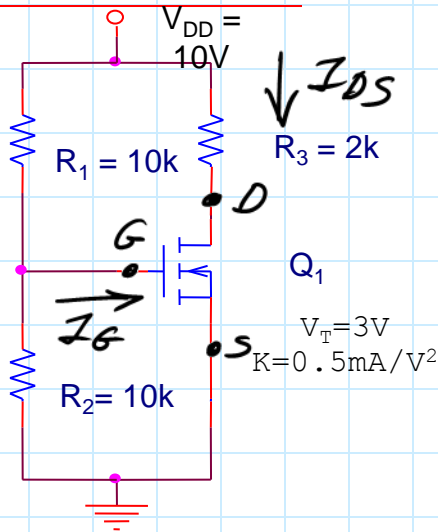
$$V_{DS}^2 - 5V_{DS} + 4 = 0 \Rightarrow \underline{V_{DS} = \frac{5 \pm \sqrt{25 - 16}}{2} = \frac{5 \pm 3}{2}} \rightarrow \begin{array}{l} \nearrow 4 (*) \\ \searrow 1 \end{array}$$

(\*) Correct,  $V_{DS} = V_{GS} > V_T$  (TON)

$$\underline{I_{DS} = \frac{5 - V_{DS}}{2} = \frac{5 - 4}{2} = 0.5mA}$$

$$\boxed{Q(V_{GS} = 4V; I_{DS} = 0.5mA; V_{DS} = 4V)}$$

# Enhancement MOSFET. Biassing (3)



Biassing with  
resistor divider

$$I_G = 0 \Rightarrow V_G = 10 \frac{R_2}{R_1 + R_2} = 5V = V_{GS} > V_T \Rightarrow \text{TON}$$

Assume SAT

$$I_{DS} = K(V_{GS} - V_T)^2 = 0.5(5 - 3)^2 = 2mA$$

$$\text{output loop: } V_{DS} = V_{DD} - I_{DS} R_3 = 10 - 4 = 6V$$

$$V_{DS} > V_{GS} - V_T = 5 - 3 \Rightarrow T \text{ is saturated}$$

$$Q(V_{GS} = 5V, I_{DS} = 2mA, V_{DS} = 6V)$$