

Modeling and control of multi-rotor UAVs

Presentation

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External Wrench Estimation in Multi-rotor UAVs

Simulation and experiments results



SAPIENZA

Outline

- Introduction
- Contact Detection
- Modeling and Control
- External Wrench Estimation
- Experiments
- Conclusions
- References



Motivations



Related Work

Physical modelling

Blade flapping model and propeller induced drag

Data driven modelling

Learn a Regressor from data

Wind tunnel measurements integration

Aerodynamic model estimation based on Blade-flapping(Physical modelling)

Data-driven wind speed estimation



Contact Detection

Aerodynamic Wrench

A learned Aerodynamic Matrix is used to describe the Aerodynamic Wrench $\mathbf{m}_d(\mathbf{f}_e)$

Experiments on a wind tunnel are used to build the aerodynamic model

Residuals based approach $\boldsymbol{\tau}_e = \boldsymbol{\tau}_d + \boldsymbol{\tau}_i + \boldsymbol{\tau}_f$

An accurate aerodynamic model allows a residuals computation as : $\tilde{\mathbf{m}}_d = \mathbf{m}_d(\mathbf{f}_e) - \mathbf{m}_e$

If only the wind effect is acting $\mathbf{m}_d(\mathbf{f}_e) = \mathbf{m}_e$ hence $\tilde{\mathbf{m}}_d = \mathbf{m}_d(\mathbf{f}_e) - \mathbf{m}_e = \mathbf{0}$

Threshold

Uncertainty: both **aerodynamic** and **external wrench** are estimated

Tuning the **threshold** by experiments

$$\|\tilde{\mathbf{m}}_d\| > CD_{threshold} \quad \tilde{\mathbf{m}}_d = \underline{\mathbf{m}_d(\mathbf{f}_e)} - \mathbf{m}_e = \mathbf{0}$$



Modeling

Newton-Euler formalism

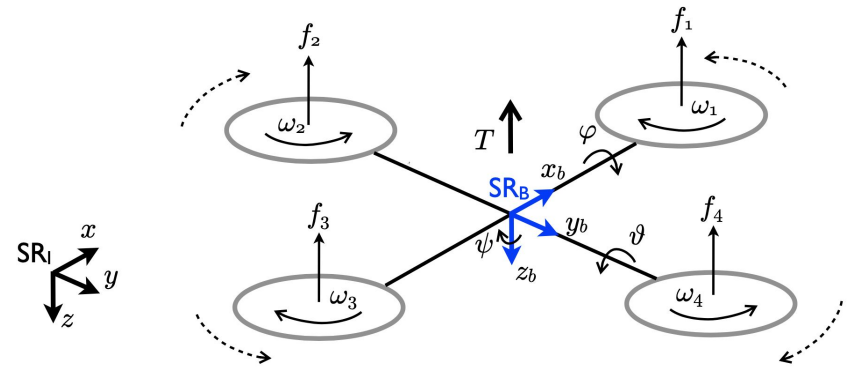
Convenient for control algorithm

Translational and Rotational Dynamics

Expressed in the inertial RF_I and body RF_B frames

Equation of motion

Rbi rpy rotation matrix from body to inertial frame



$$\sum \mathbf{f}_I = \mathcal{M} \ddot{\mathbf{r}}$$

$$\sum \mathbf{m}_B = \mathbf{I} \dot{\boldsymbol{\omega}} + (\mathbf{I} \boldsymbol{\omega}) \times \boldsymbol{\omega}$$

$$\mathcal{M} \ddot{\mathbf{r}} = \mathcal{M} g \mathbf{e}_3 + \mathbf{R}_b^i \mathbf{f} + \mathbf{R}_b^i \mathbf{f}_e$$

$$\mathbf{I} \dot{\boldsymbol{\omega}} = -(\mathbf{I} \boldsymbol{\omega}) \times \boldsymbol{\omega} + \mathbf{m} + \mathbf{m}_e$$

$$\dot{\mathbf{R}}_b^i = \mathbf{R}_b^i(\boldsymbol{\omega}) \times$$

Control

System model

Affine system linear in the input u

Position and attitude control

Output a control thrust T and torque \mathbf{m}

Cascaded control scheme

Efficient for basic maneuvers

state

$$\xi = (x, y, z, v_x, v_y, v_z, \varphi, \vartheta, \psi, p, q, r)'$$

inputs

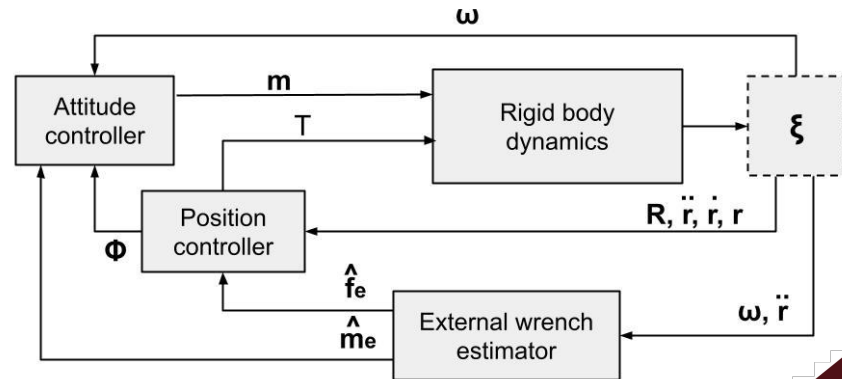
$$u = (T, \mathbf{m})$$

control

$$\mathbf{f}_i = \mathbf{R}_{di}\mathbf{f} = M(\dot{\mathbf{r}}_d - K_{fd} \mathbf{e}_{\dot{\mathbf{r}}} - K_{fp} \mathbf{e}_{\mathbf{r}}) - M\mathbf{g}\mathbf{e}_3 - \mathbf{f}_e$$

$$\mathbf{m} = \mathbf{I}(K_{mp} \mathbf{e}_{\mathbf{R}} - K_{md} \boldsymbol{\omega}) + (\mathbf{I}\boldsymbol{\omega}) \times \boldsymbol{\omega} - \mathbf{m}_e$$

scheme



Lagrangian Formalism

$$\mathbf{M}\dot{\boldsymbol{\nu}} + \mathbf{C}(\boldsymbol{\nu})\boldsymbol{\nu} + \mathbf{D}(\boldsymbol{\nu})\boldsymbol{\nu} + \mathbf{g} = \mathbf{J}^T \boldsymbol{\tau} + \boldsymbol{\tau}_e$$

twist \swarrow
control wrench \swarrow

aerodynamic drag forces \nearrow
external wrench \nearrow

where $\mathbf{g} = [-\mathcal{M}g\mathbf{e}_3 \ 0]^T$, $\boldsymbol{\nu} = [\dot{\mathbf{r}} \ \boldsymbol{\omega}]^T$ is the twist, $\mathbf{J} = \text{blockdiag} \{ \mathbf{R}_b^i, \mathbf{I}_{3 \times 3} \}$ and

$$\mathbf{M} = \begin{bmatrix} \mathcal{M}\mathbf{I}_{3 \times 3} & \mathbf{0}_{3 \times 3} \\ \mathbf{0}_{3 \times 3} & \mathbf{I} \end{bmatrix}, \mathbf{C}(\boldsymbol{\nu}) = \begin{bmatrix} \mathbf{0}_{3 \times 3} & \mathbf{0}_{3 \times 3} \\ \mathbf{0}_{3 \times 3} & -(\mathbf{I}\boldsymbol{\omega}) \times \end{bmatrix}$$



Momentum-based External Wrench Estimation

Generalized momentum

Differentiation according to Lagrangian form

$$\mathbf{p} = \mathbf{M}\mathbf{v}$$

$$\dot{\mathbf{p}} = \mathbf{M}\dot{\mathbf{v}} = \mathbf{J}^T \boldsymbol{\tau} + \boldsymbol{\tau}_e - \mathbf{N}$$

Residual vector

Definition following [De Luca et al.]

Requires a direct measure of the twist

$$\boldsymbol{\rho} = K_I \left[\mathbf{p} - \int \left(\mathbf{J}\boldsymbol{\tau} + \boldsymbol{\tau}_e - \mathbf{N} + \boldsymbol{\rho} \right) dt \right]$$

Residual dynamics

Linear exponentially stable system

$$\dot{\boldsymbol{\rho}} = K_I \boldsymbol{\tau}_e - K_I \boldsymbol{\rho}$$



Acceleration-based External Wrench Estimation

Rearranging the Lagrangian form

Needs a direct measure of acceleration

$$\hat{\boldsymbol{\tau}}_e = \mathbf{M}\dot{\boldsymbol{\nu}} + \mathbf{C}(\boldsymbol{\nu})\boldsymbol{\nu} + \mathbf{D}(\boldsymbol{\nu})\boldsymbol{\nu} + \mathbf{g} - \boldsymbol{\tau}$$



Hybrid External Wrench Estimation

Only momentum-based

Requires more sensors and fusion algorithm

$$\overline{\hat{\boldsymbol{\tau}}_e} = K_I \left[\mathbf{p} - \int \left(\mathbf{J}\boldsymbol{\tau} + \boldsymbol{\tau}_e - \mathbf{N} + \boldsymbol{\rho} \right) dt \right]$$

Only acceleration-based

Requires numerical differentiation

$$\hat{\boldsymbol{\tau}}_e = \mathbf{M}\dot{\boldsymbol{\nu}} + \mathbf{C}(\boldsymbol{\nu})\boldsymbol{\nu} + \mathbf{D}(\boldsymbol{\nu})\boldsymbol{\nu} + \mathbf{g} - \boldsymbol{\tau}$$

Combining the two methods

Requires only accelerometer

$$\hat{\boldsymbol{\tau}}_e = \begin{bmatrix} \hat{\mathbf{f}} \\ \hat{\mathbf{m}}_e \end{bmatrix} = \begin{cases} \int K_f \left(\mathcal{M}\mathbf{a} - \mathbf{f} - \hat{\mathbf{f}}_e \right) dt \\ K_m \left(\mathbf{I}\boldsymbol{\omega} + \int \left((\mathbf{I}\boldsymbol{\omega}) \times \boldsymbol{\omega} - \mathbf{m} - \hat{\mathbf{m}}_e \right) dt \right) \end{cases}$$



Discrimination

Data-driven approach

Train a perceptron over the wind-tunnel dataset

Physical modeling approach

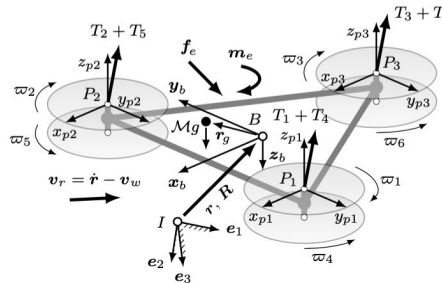
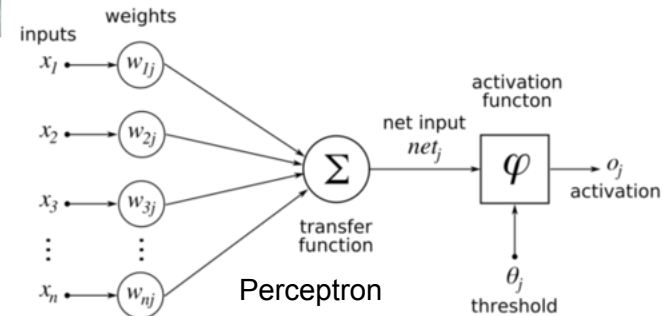
Exploiting propeller aerodynamics

Attempts

- Using a linear model $\mathbf{v}_r = \mathbf{u}$
- Guessing propeller physical characteristics



wind-tunnel
experiment



$$\mathbf{f}_d = \mathbf{A}_d \mathbf{v}_r c_T \sum_i \omega_i$$

Blade flapping model
[Omari et al.]

$$\mathbf{v}_{\infty,k} = \mathbf{R}_{bp,k}^T (\mathbf{R}_{bt}^T \mathbf{v}_r + \boldsymbol{\omega} \times \mathbf{r}_k)$$



Simulation Environment

Applications and Tools

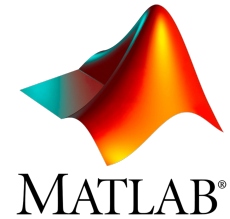
The project is developed using Matlab and CoppeliaSim framework

Matlab

Matlab is a computational framework optimized for iterative analysis and design processes

CoppeliaSim

CoppeliaSim is a robot simulator used in industry, education and research



Implementation

System Architecture

The project consists of two main modules:

- the **Matlab client application**, implementing the **core logic** of the system
- the **Coppelia simulation scene**, providing the **experimental environment** and simulation settings

Matlab Client Structure

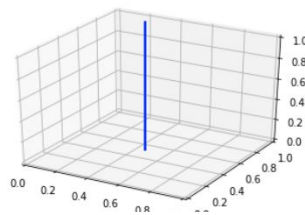
The Matlab application is made up of three main classes:

- **Quadrotor** : implements the system dynamics and provides the control design for tracking task
- **Aerodynamics** : contains the wrench estimation algorithm and the contact detection procedure
- **QuadrotorSim** : acts as an interface between Matlab logic and Coppelia simulation environment

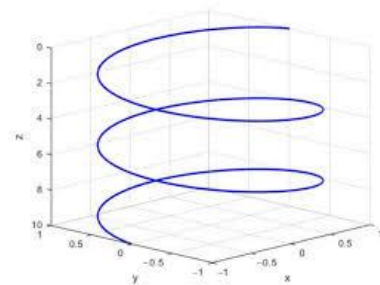
Problem Settings

Task Trajectories

Two task trajectories are considered: a **hovering** and an **elicoidal trajectory**



Hovering



Elicoidal trajecotry

Hovering

We tested the external wrench estimation and contact detection, in the following cases:

- in **presence** of **wind action only**
- in **presence** of a **continuous** contact action but in **absence** of **wind action**
- in **presence** of a **continuous contact** action and of **wind action**
- in **presence** of **wind action** and **not uniformly distributed load** mass

Spiral

We tested this task in **presence of wind action only**.

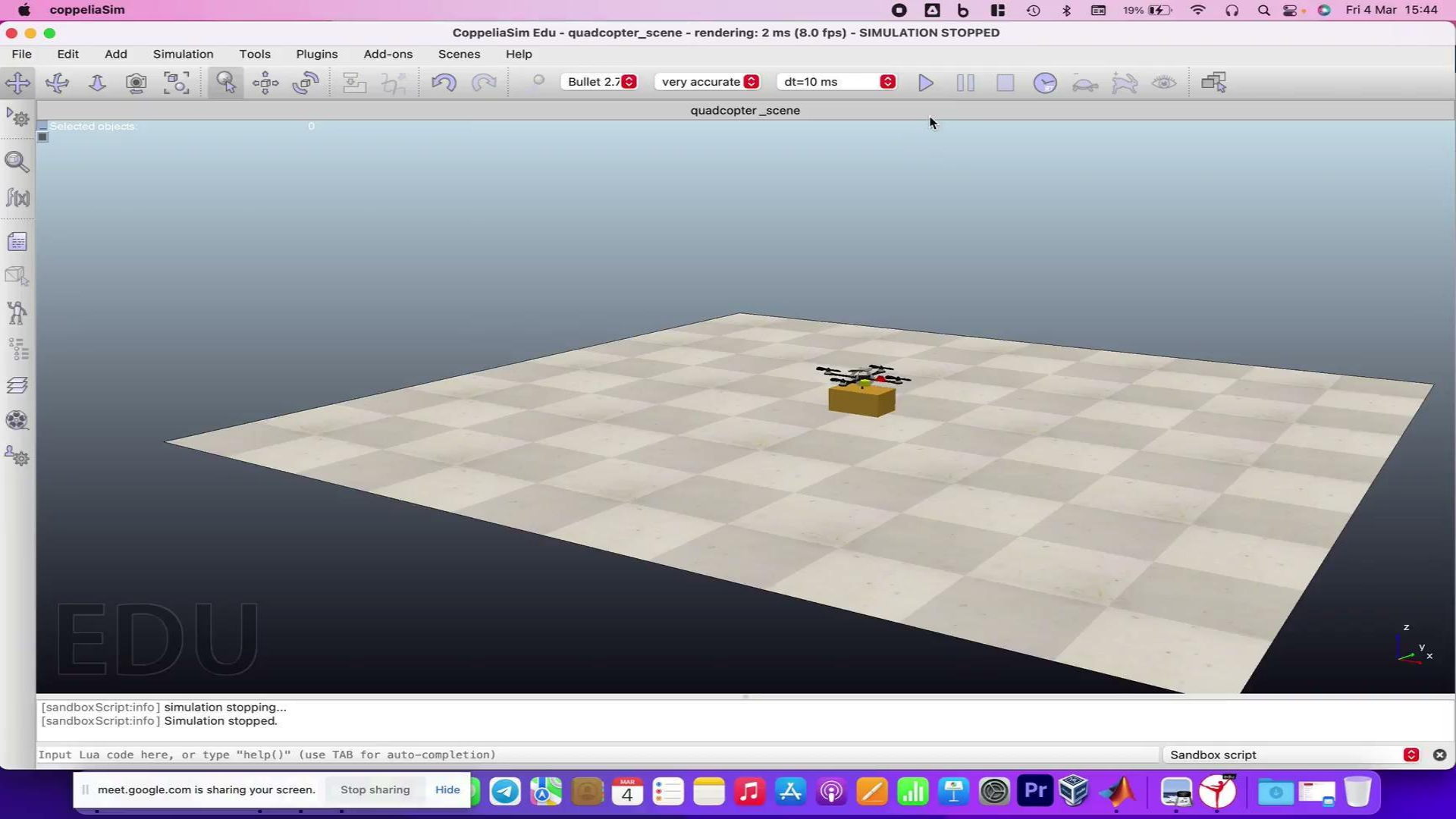


Results

Experiment 1

Hovering with wind action only (aerodynamic external wrench)



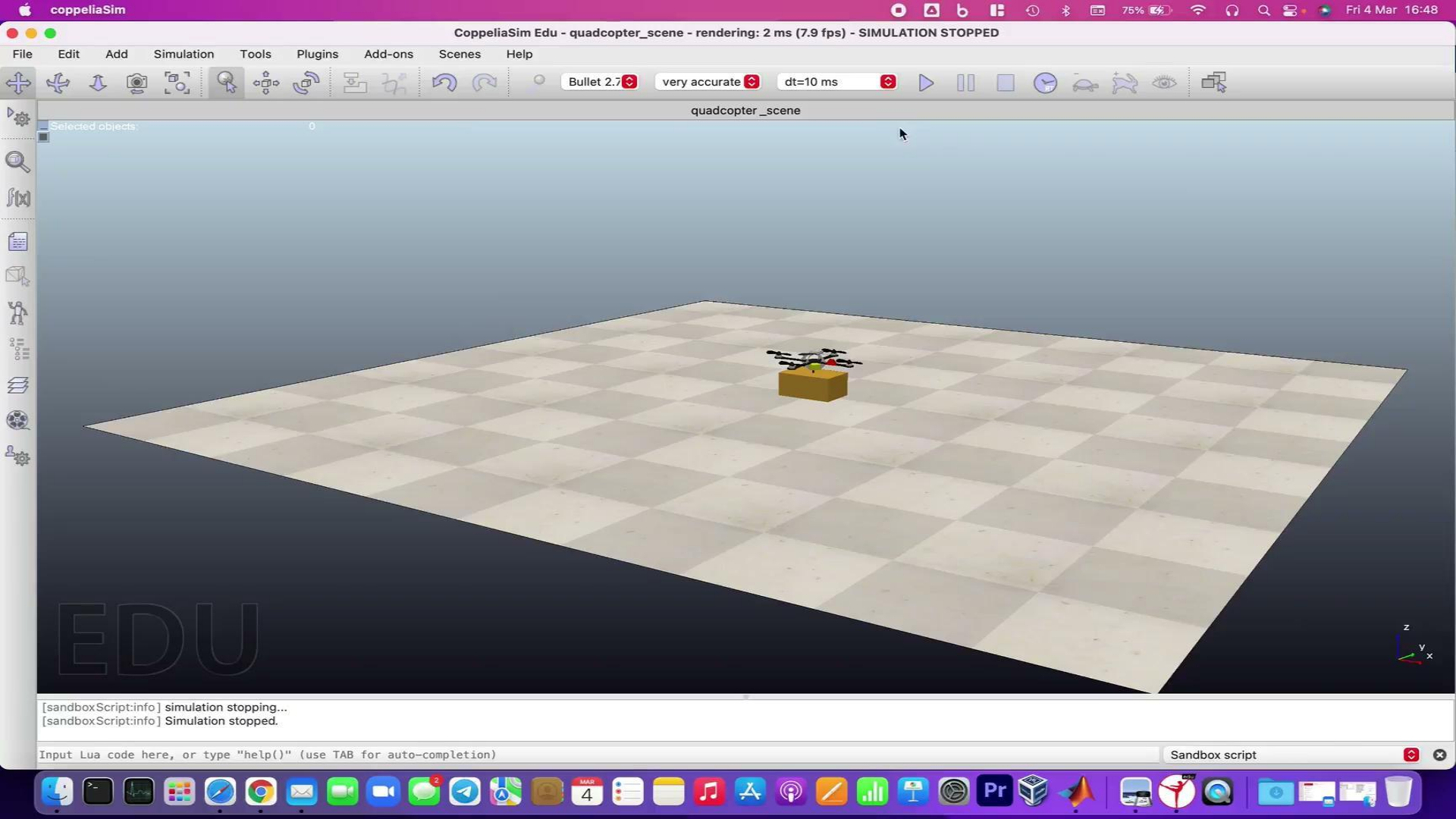


Results

Experiment 2

Hovering with continuous external contact force



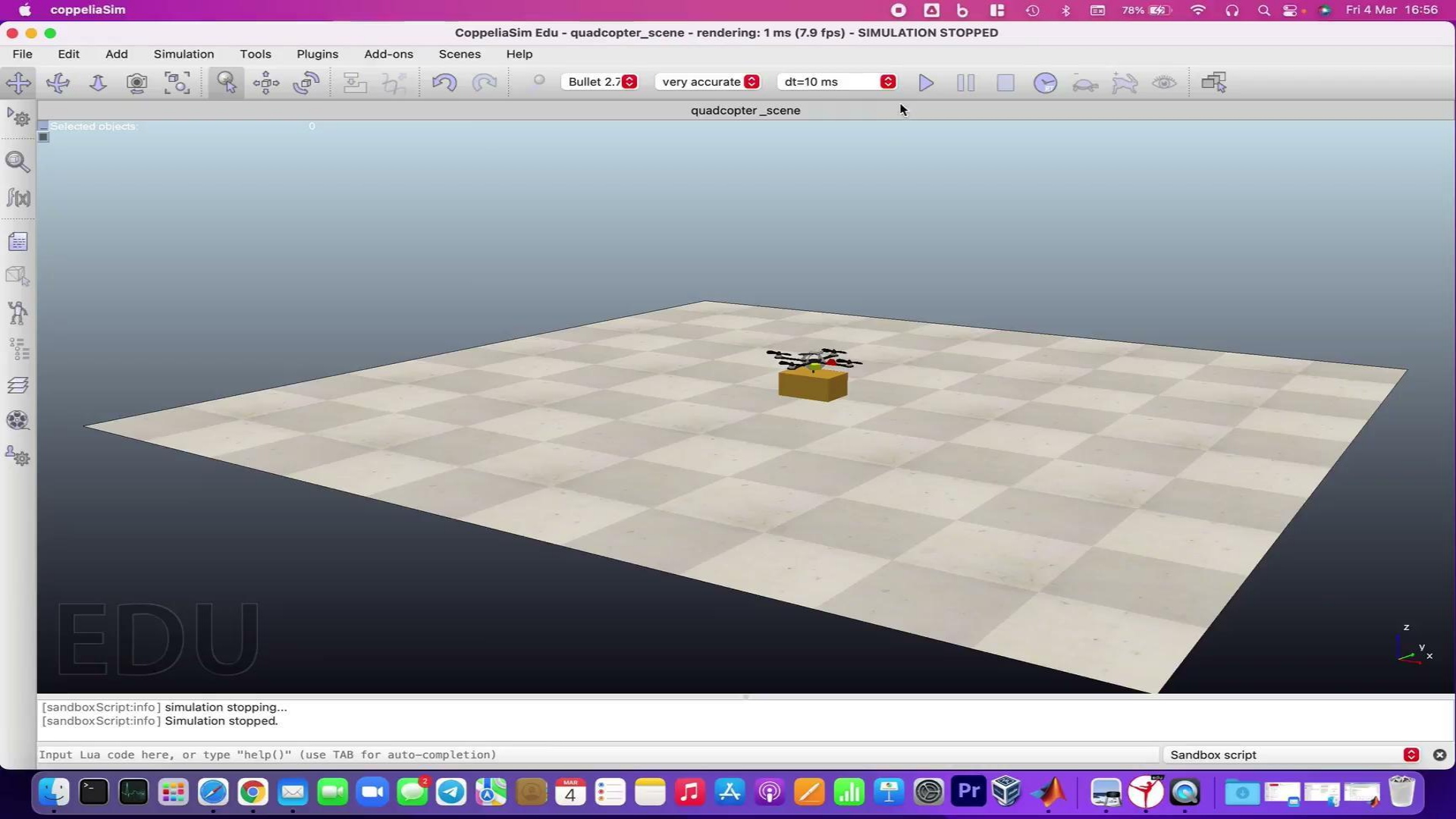


Results

Experiment 3

Hovering with both wind and contact force actions



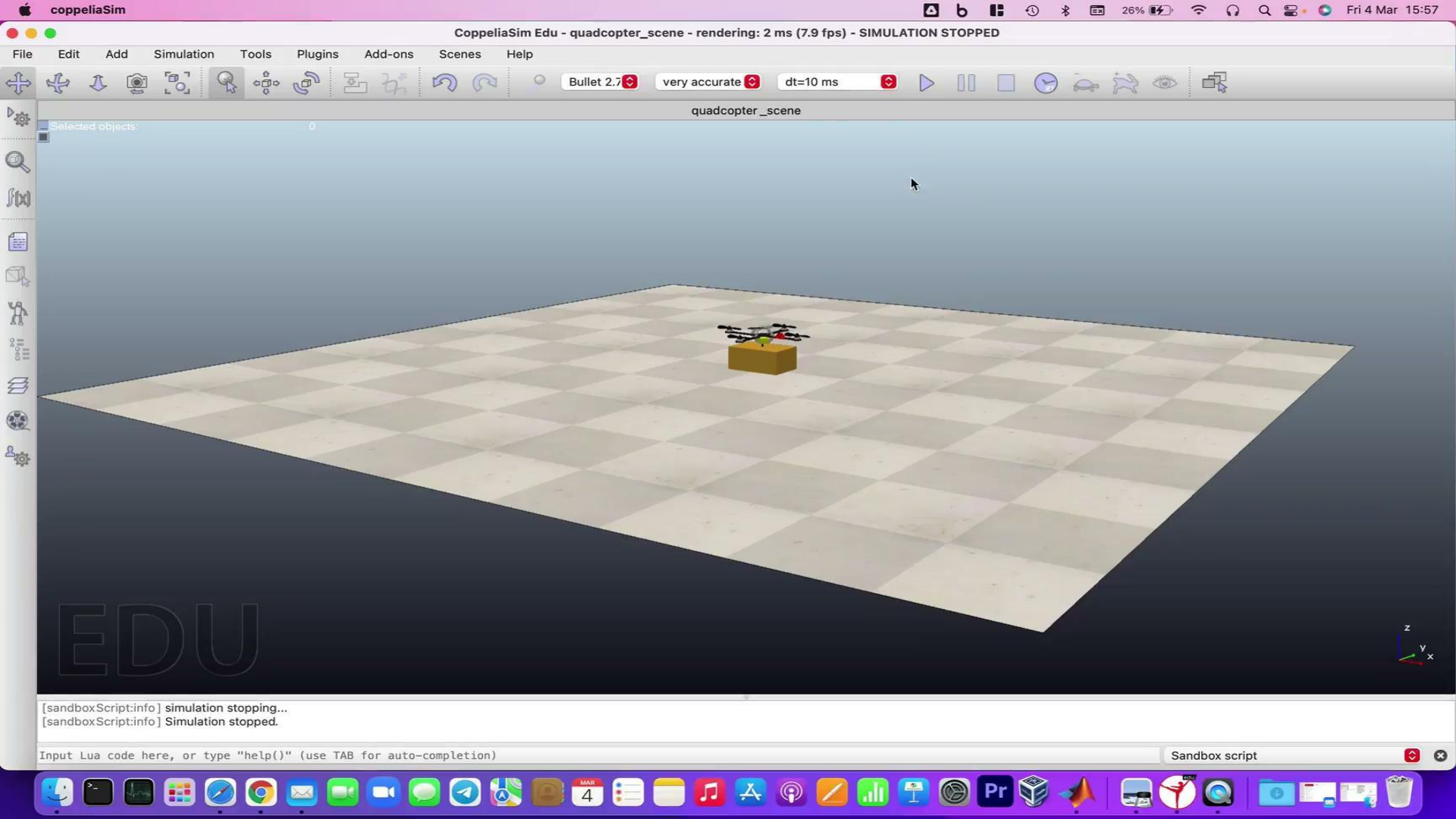


Results

Experiment 4

Elicoidal trajectory with wind action only

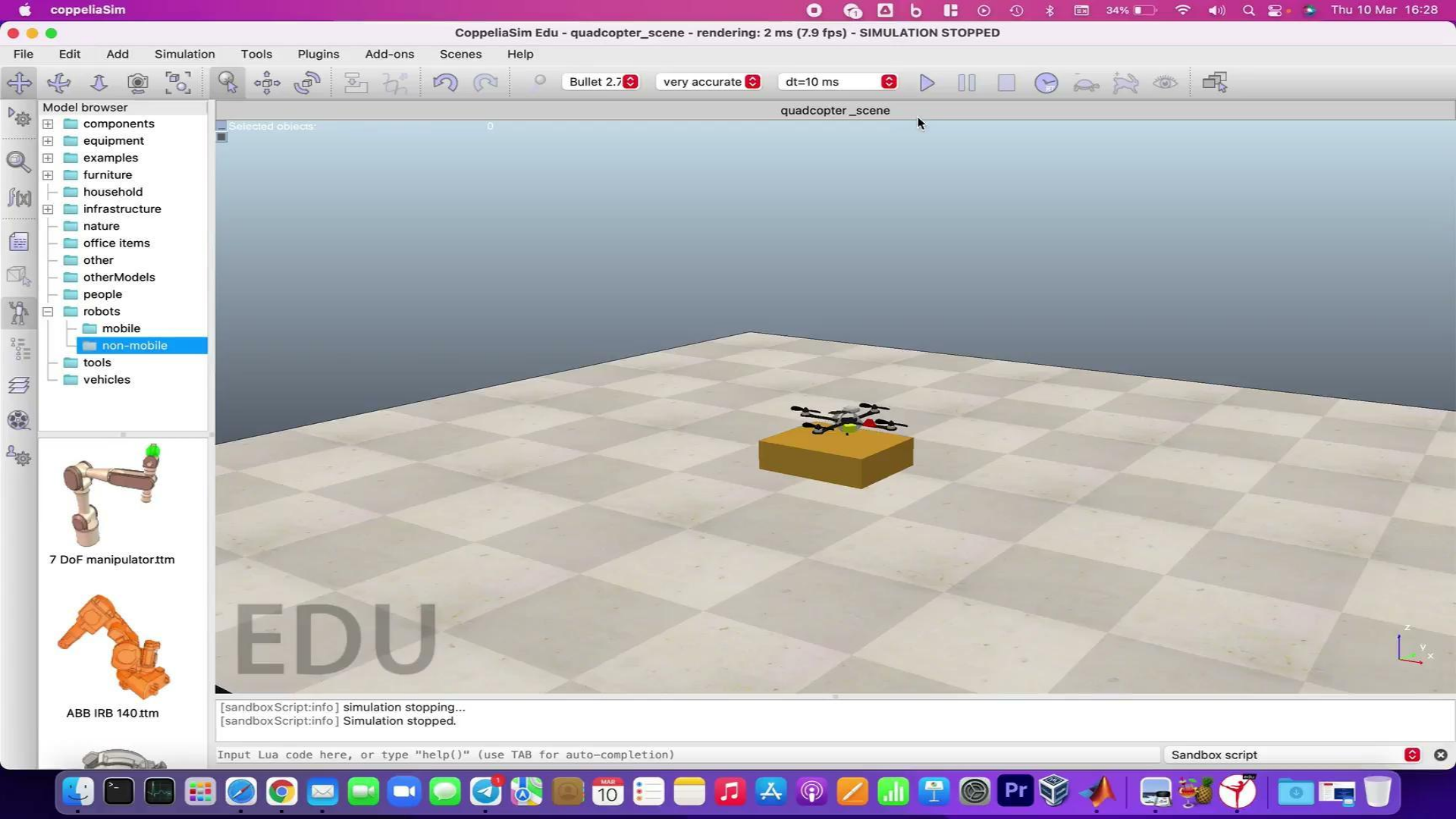




Results

Experiment 5

Hovering with wind action and not uniformly distributed load mass



Conclusions

Achieved Results

In this project, we provided the implementation and evaluation of a simultaneous contact and external wrench estimation system for aerial robots without the need for additional on-board sensors

Weaknesses

As motivated in the section [Discrimination](#), The wrench estimator lacks of the module for discrimination between areodynamics and contact wrenches.

Improvements

A particle filter can be used, as proposed in [\[Tomic et al.\]](#), to directly estimate the contact force position on the robot convex hull



References

Simultaneous Contact and Aerodynamic Force Estimation (s-CAFE) for Aerial Robots

Teodor Tomic, Philipp Lutz, Korbinian Schmid, Andrew Mathers, Sami Haddadin

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Nonlinear Control of VTOLs UAVs incorporating Flapping Dynamics

Sammy Omari, Minh-Duc Hua, Guillaume Ducard, Tarek Hamel

<https://ieeexplore.ieee.org/document/6696696>

Thanks

