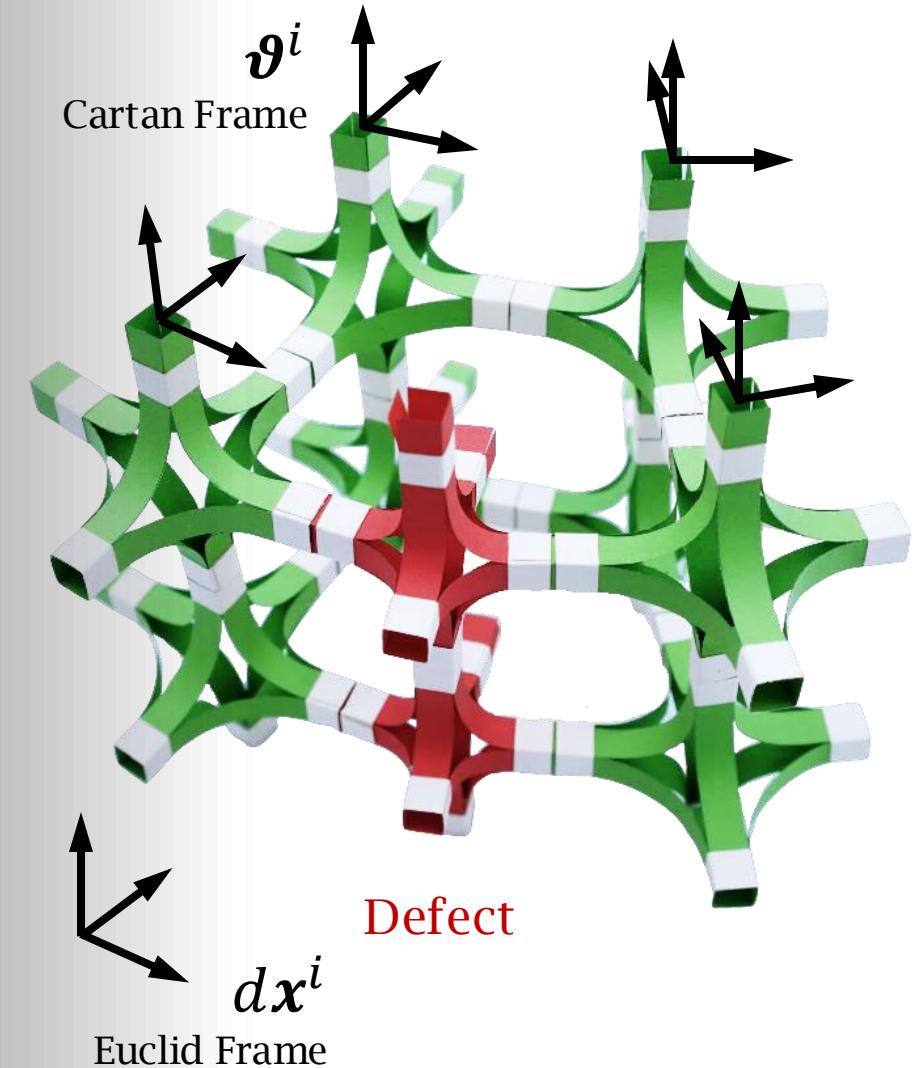


# Materials Science on Riemann-Cartan manifold

## - Reformulation of Volterra Defects -

Nonlinear Mechanics Division, Osaka University  
Ryuichi Tarumi and Shunsuke Kobayashi



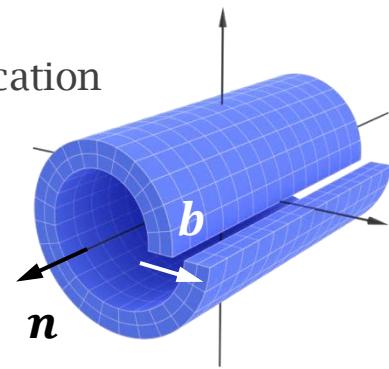
# Introduction

Volterra defects: classification of dislocations and disclinations

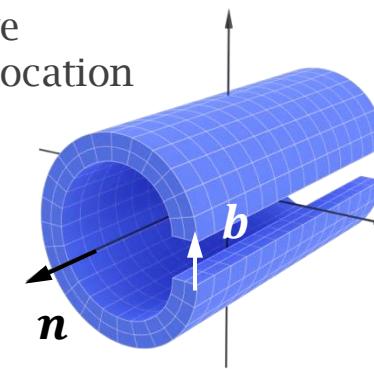


Vito Volterra  
(1860 - 1940)

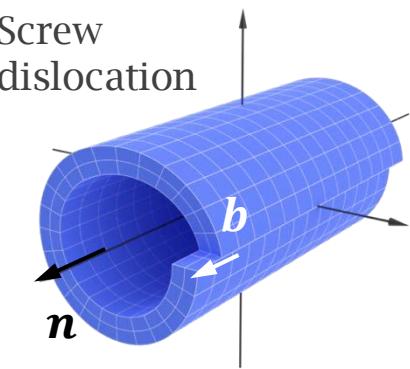
Edge  
dislocation



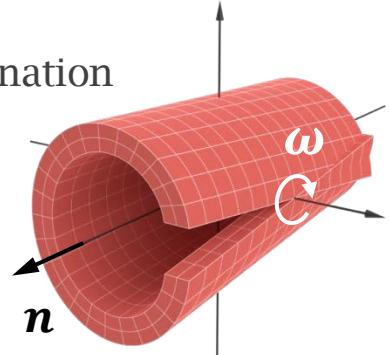
Edge  
dislocation



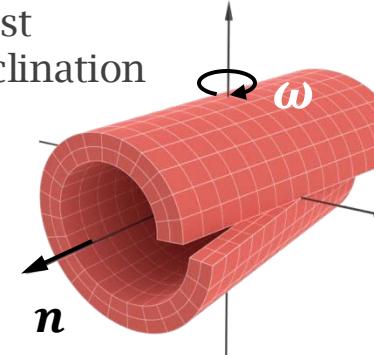
Screw  
dislocation



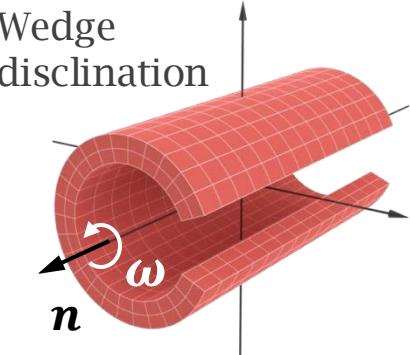
Twist  
disclination



Twist  
disclination



Wedge  
disclination



# Introduction

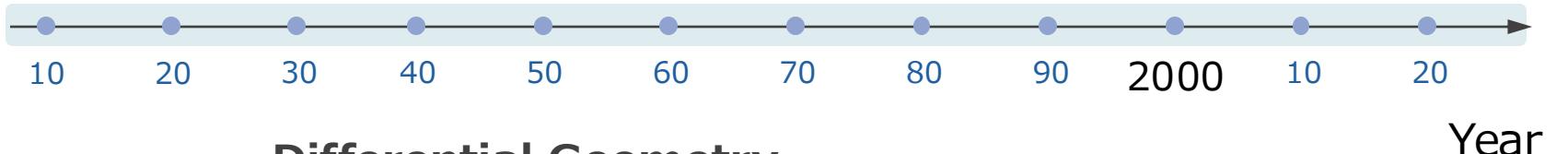
## A brief history of the theory of dislocation



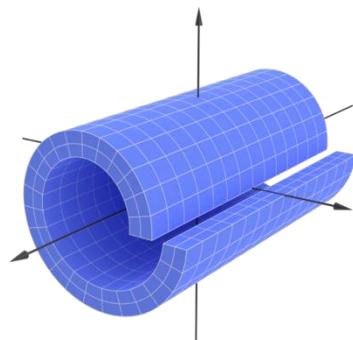
Vito Volterra  
(1860 - 1940)

### Euclidean Space

- V. Volterra (1907)
- G.I. Taylor (1934)
- E. Orowan (1934)
- R. Peierls (1940)
- F.R.N. Nabarro (1947)
- T. Mura (1964)
- W. Noll (1967)
- A.C. Eringen (1983)
- D.G.B. Edelen (1988)
- M.O. Katanaev (1992)
- L.M. Zubov (1997)
- M. Lazar (2000-)
- Acharya (2010-)



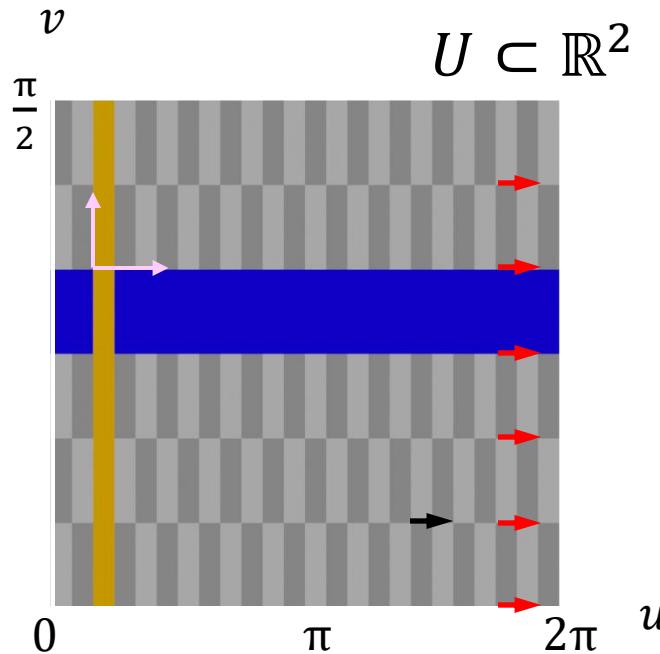
### Differential Geometry



- K. Kondo (1955)
- B.A. Bilby (1955)
- E. Kroner (1959)
- S. Amari (1962)
- R. de Wit (1981)
- J. Wenzelburger (1998)
- Yavari & Goriely (2012)
- Kobayashi & Tarumi (2024) 3

# Introduction

A map  $\phi$  from 2D Euclidean space to a semi-spherical surface

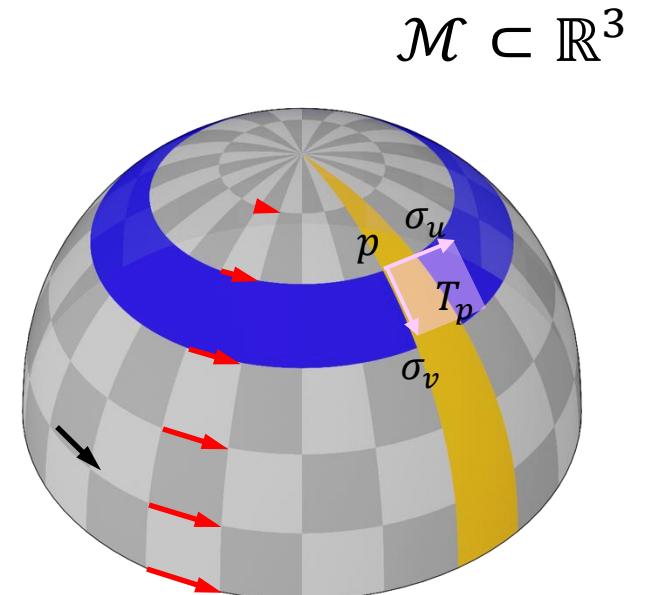


$$\phi : U \rightarrow \mathcal{M}$$

$$\phi(u, v) = \begin{cases} x = r \sin u \cos v \\ y = r \sin u \sin v \\ z = r \cos u \end{cases}$$

$$N = (\sin u \cos v, \sin u \sin v, \cos u)$$

Plane (coordinate)



Riemannian manifold

# Introduction

The first and second fundamental forms of a curved surface

$$\mathcal{F}_1 = Edu^2 + 2Fdudv + Gdv^2$$

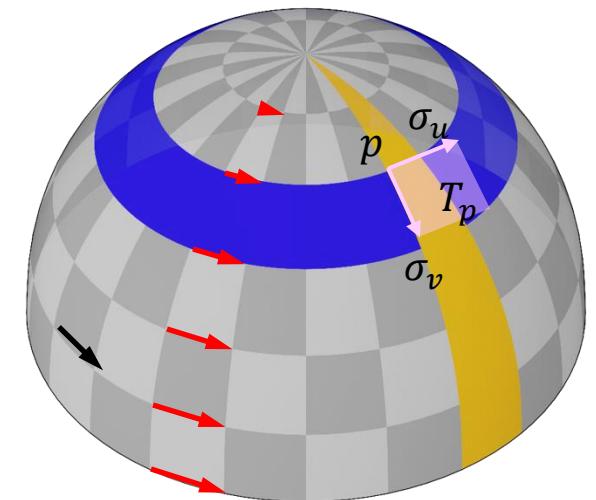
$$\begin{cases} E = \langle \phi_u, \phi_u \rangle = r^2 \sin^2 v \\ F = \langle \phi_u, \phi_v \rangle = 0 \\ G = \langle \phi_v, \phi_v \rangle = r^2 \end{cases} \quad \Rightarrow \quad g_{ij} = \begin{pmatrix} E & F \\ F & G \end{pmatrix} = \begin{pmatrix} r^2 \sin^2 v & 0 \\ 0 & r^2 \end{pmatrix}$$

Riemannian metric

$$\mathcal{F}_2 = edu^2 + 2fdudv + gdv^2$$

$$\begin{cases} e = \langle \phi_{uu}, N \rangle = -r \sin^2 v \\ f = \langle \phi_{uv}, N \rangle = 0 \\ g = \langle \phi_{vv}, N \rangle = -r \end{cases} \quad \Rightarrow \quad W = \frac{1}{EG - F^2} \begin{pmatrix} eG - fF & fG - gF \\ fE - eF & gE - fF \end{pmatrix}$$

Weingarten matrix



# Introduction

The first and second fundamental forms of a curved surface

$$\mathcal{F}_1 = Edu^2 + 2Fdudv + Gdv^2$$

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Riemannian metric

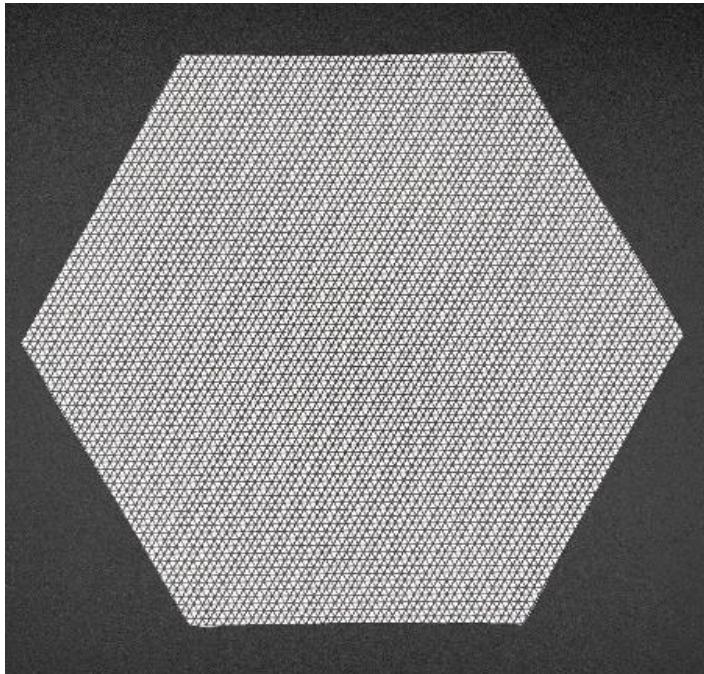
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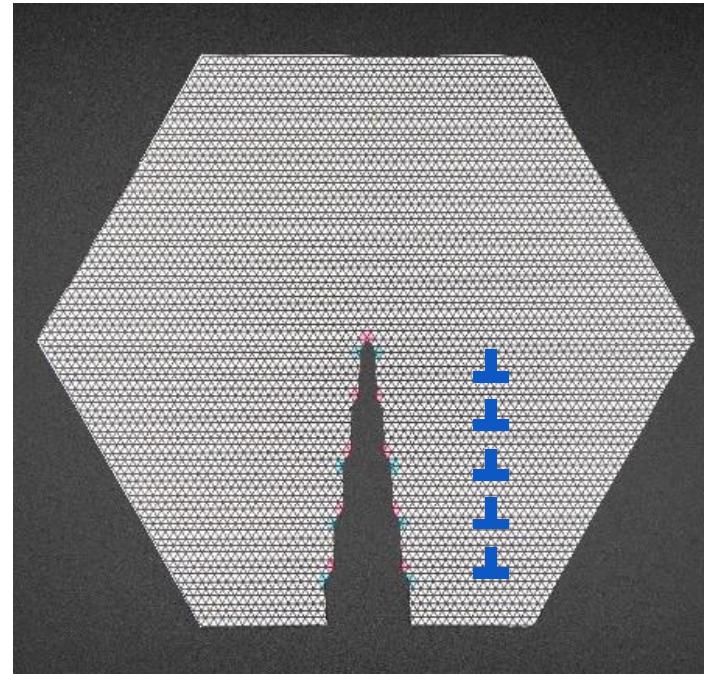
Weingarten matrix

# Introduction

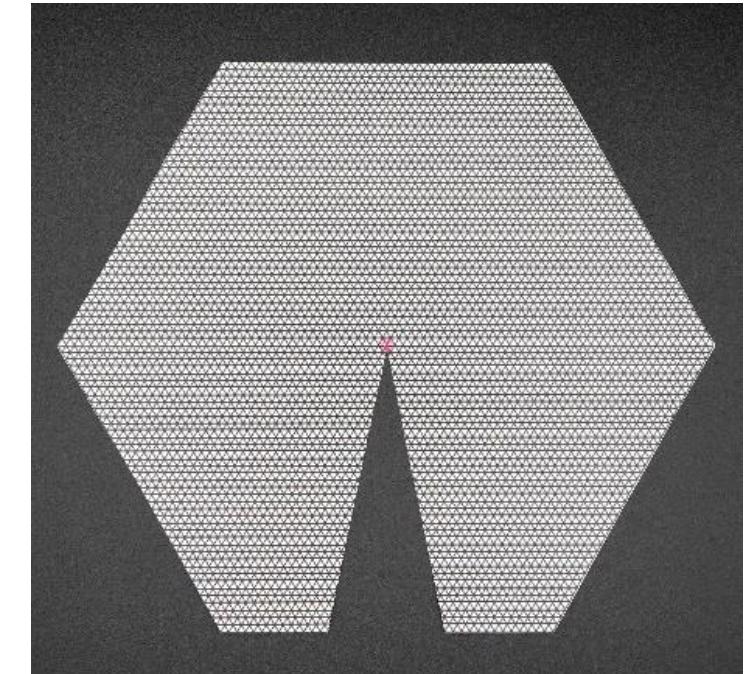
Volterra defects made by ‘Kirigami’ lattice



Perfect crystal

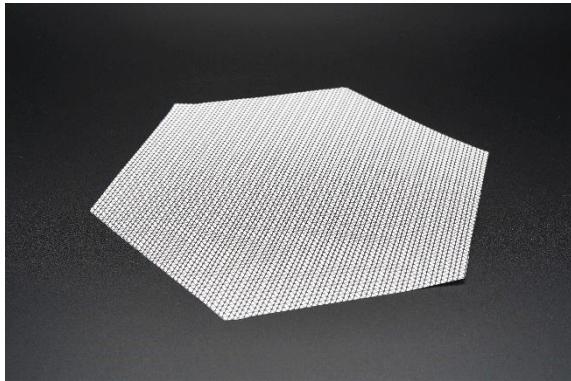


Edge dislocation array



Wedge disclination

# Introduction



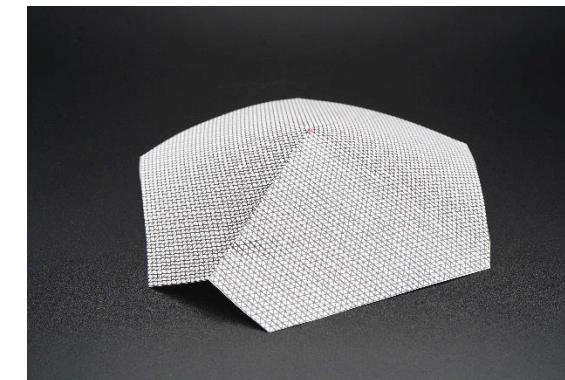
Perfect crystal



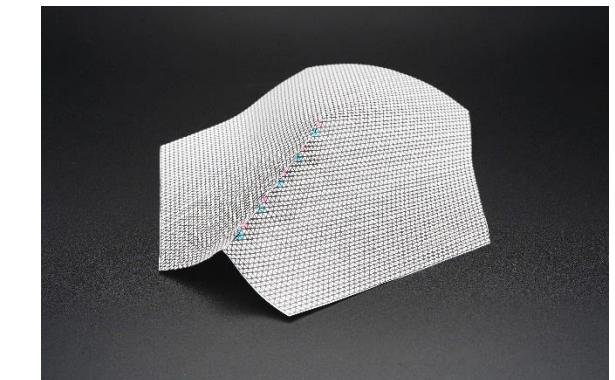
Grain boundary



Dislocation pair



Disclination



Dislocation array

Curvature represents the plastic deformation due to Volterra defects

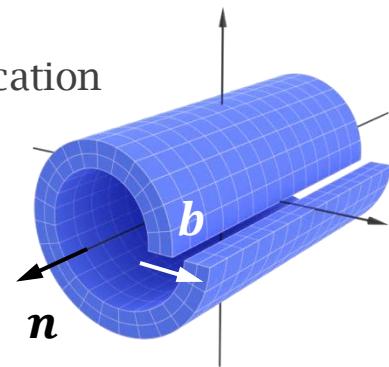
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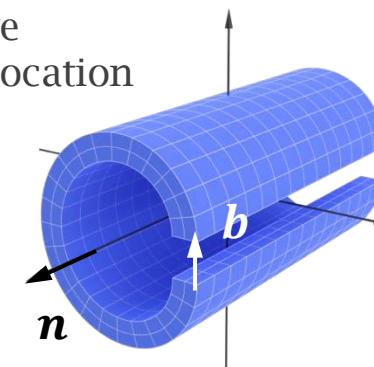


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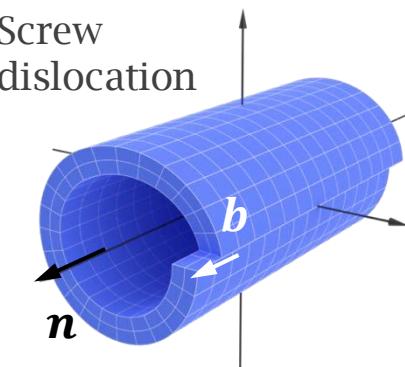
Edge  
dislocation



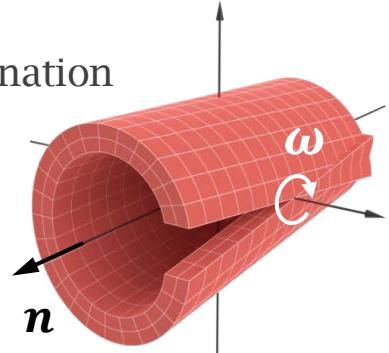
Edge  
dislocation



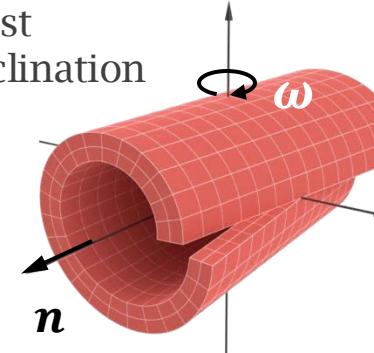
Screw  
dislocation



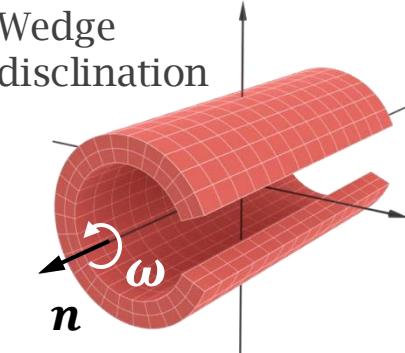
Twist  
disclination



Twist  
disclination



Wedge  
disclination



# Table of contents

## 1. Geometrical frustration

- What is the origin of stress in crystalline solids?
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## 4. Materials Geometry & Information Geometry

- Statistical analysis for materials science

# 1. Geometrical frustration

## Riemann-Cartan Manifold

- Cartan structure equations for Riemann-Cartan manifold

$$\tau^i = d\vartheta^i + \omega_j^i \wedge \vartheta^j$$

$$\Omega_j^i = d\omega_j^i + \omega_k^i \wedge \omega_j^k$$

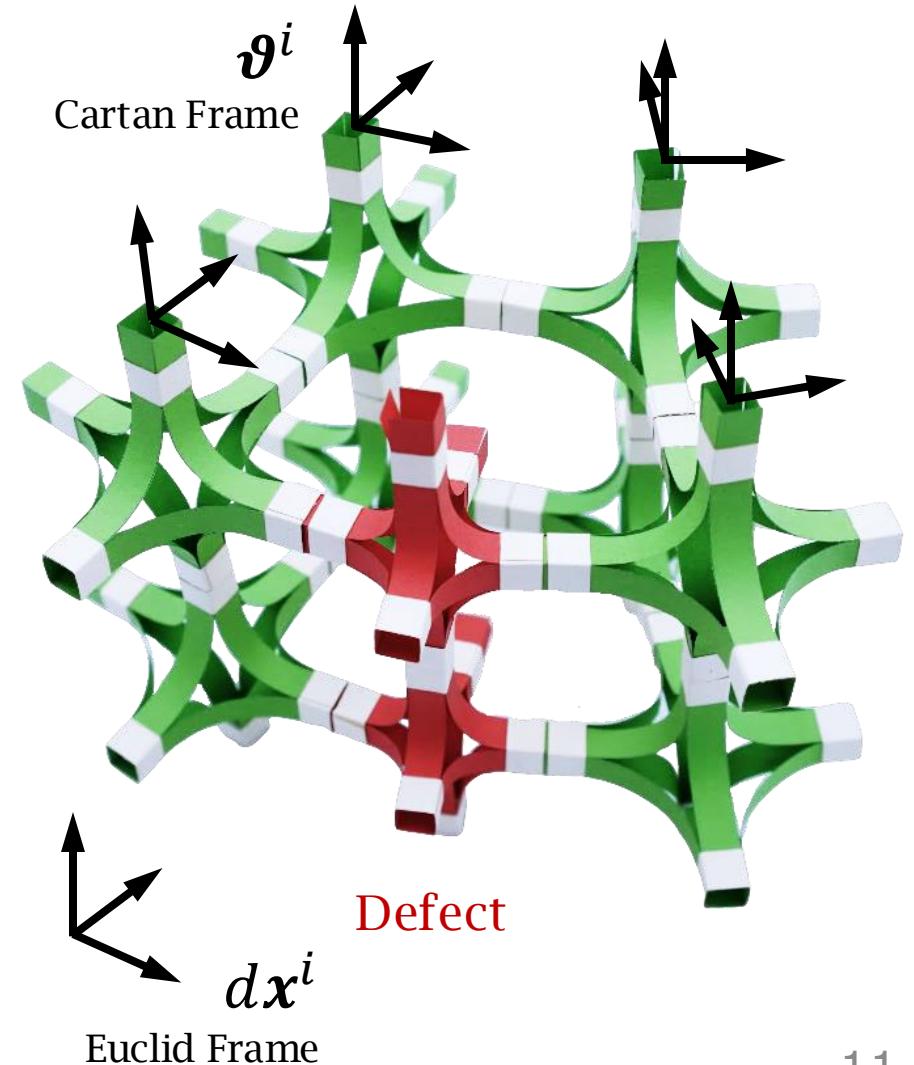
- $\vartheta^i: TM \rightarrow M \times \mathbb{R}^3$ : Cartan moving frame  $\vartheta^i$  for dislocations

$$\vartheta^i = (d\psi^i + \Theta^i) dx^j \otimes E_i$$

Helmholtz decomposition

- Dislocation density and torsions 2-form

$$\tau^i = * \alpha^i = f b^i n_l \epsilon_{ljk} dx^j \wedge dx^k \otimes E_i$$



# 1. Geometrical frustration

## Kinematics on Riemannian manifold

- Three different configurations: reference, intermediate and current configurations.

$$(\mathcal{M}, g, \nabla) \xrightarrow{F_p} (\mathcal{M}, g_B, \nabla_B) \xrightarrow{F_e} (\mathcal{M}, g_C, \nabla_C)$$

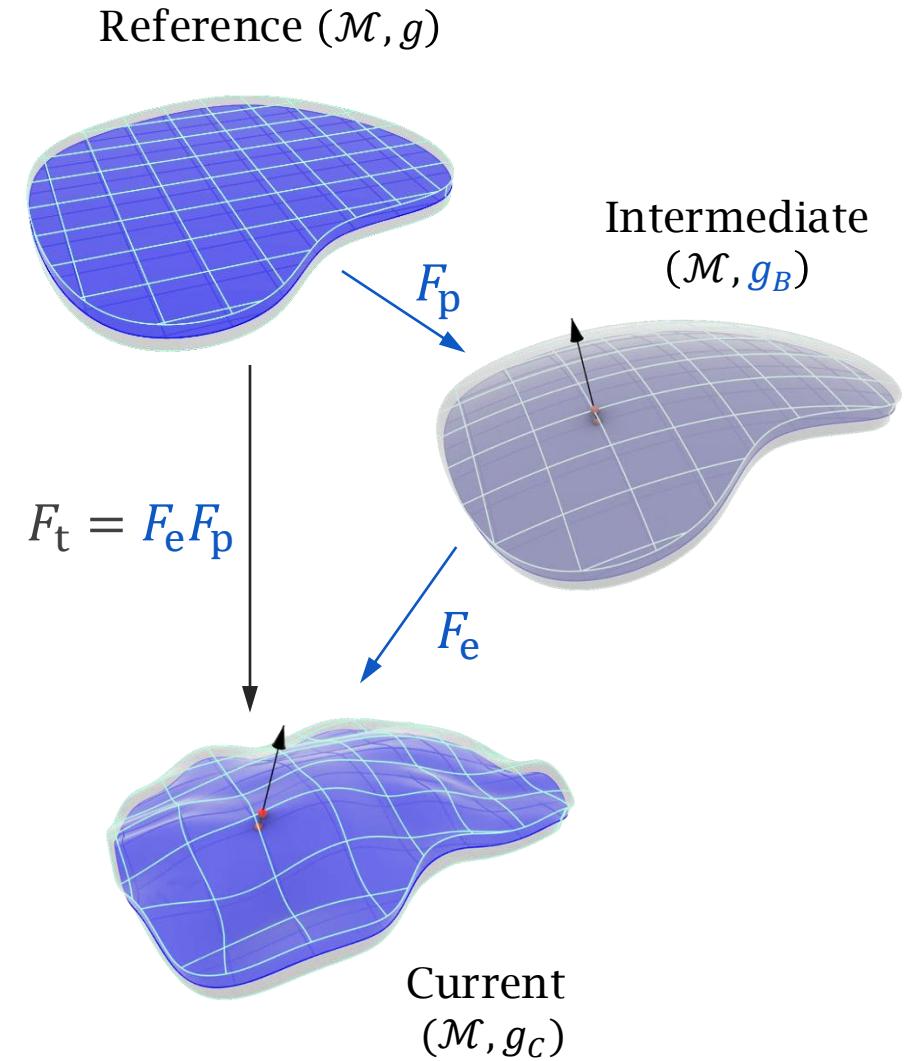
Reference ( $\mathbb{R}^3$ )      Intermediate      Current ( $\mathbb{R}^3$ )

- Kinematics is described by the two deformation gradients:  $F_p$  and  $F_e$ .

$$F_t = F_e F_p \quad \text{Multiplicative decomposition}$$

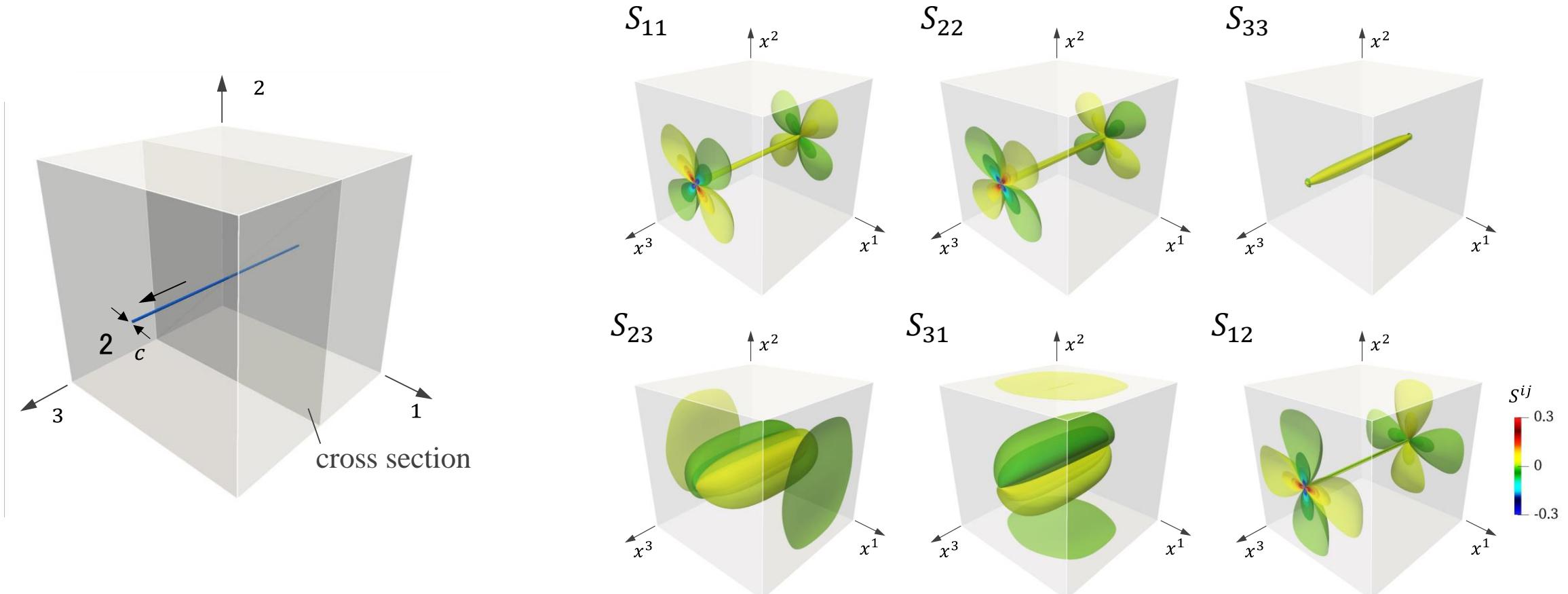
- Elastic embedding from the intermediate to the current configuration

$$W[y] = \int_{\mathcal{M}} C^{ijkl} \frac{(g_C - g_B)_{ij}}{2} \frac{(g_C - g_B)_{kl}}{2} dV$$



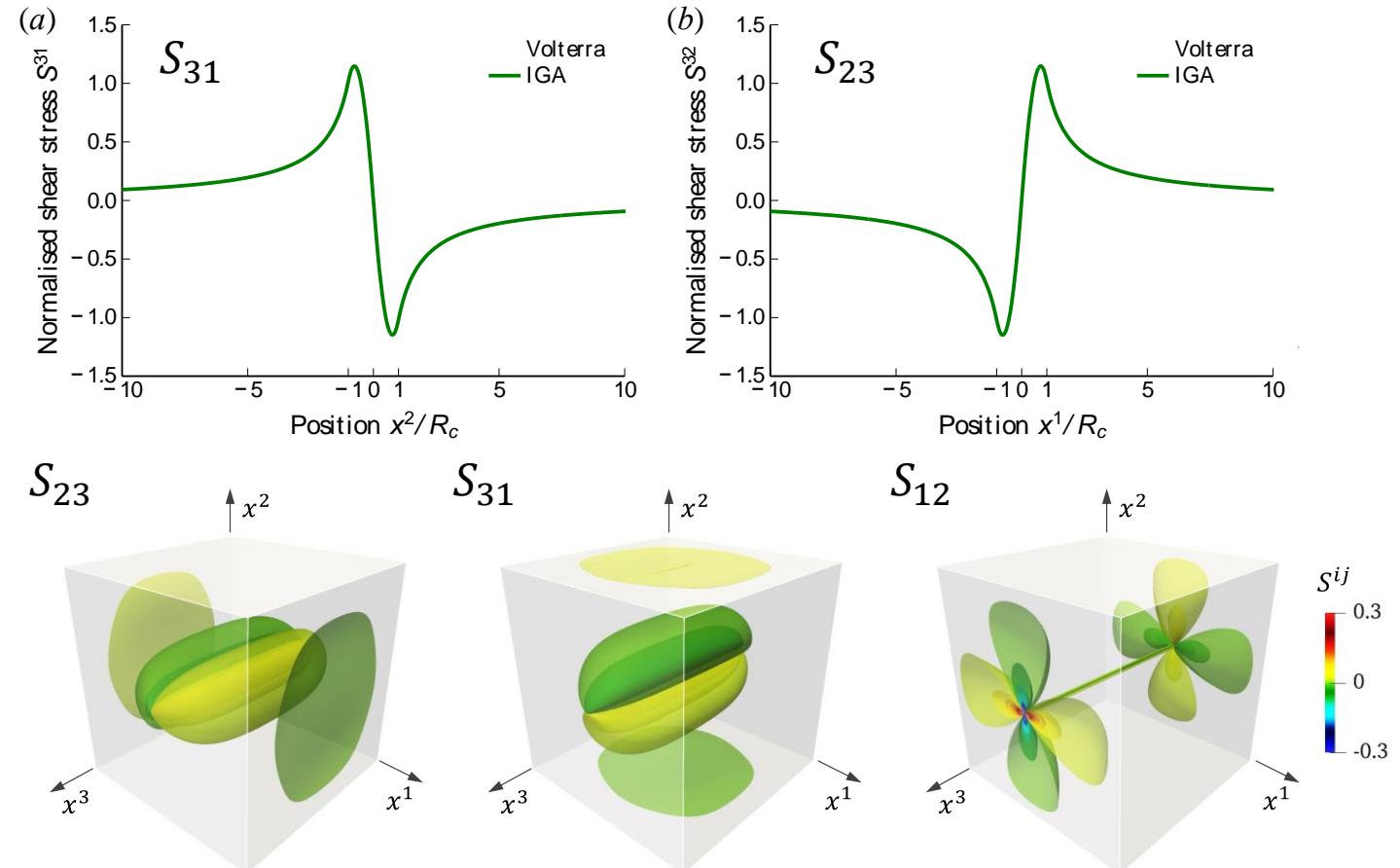
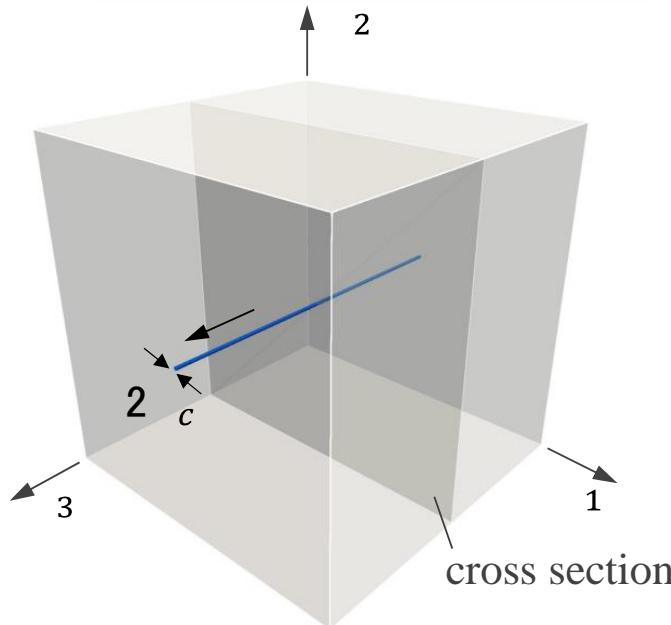
# 1. Geometrical frustration

Internal stress fields of screw dislocation (2<sup>nd</sup>-Piola-Kirchhoff stress)



# 1. Geometrical frustration

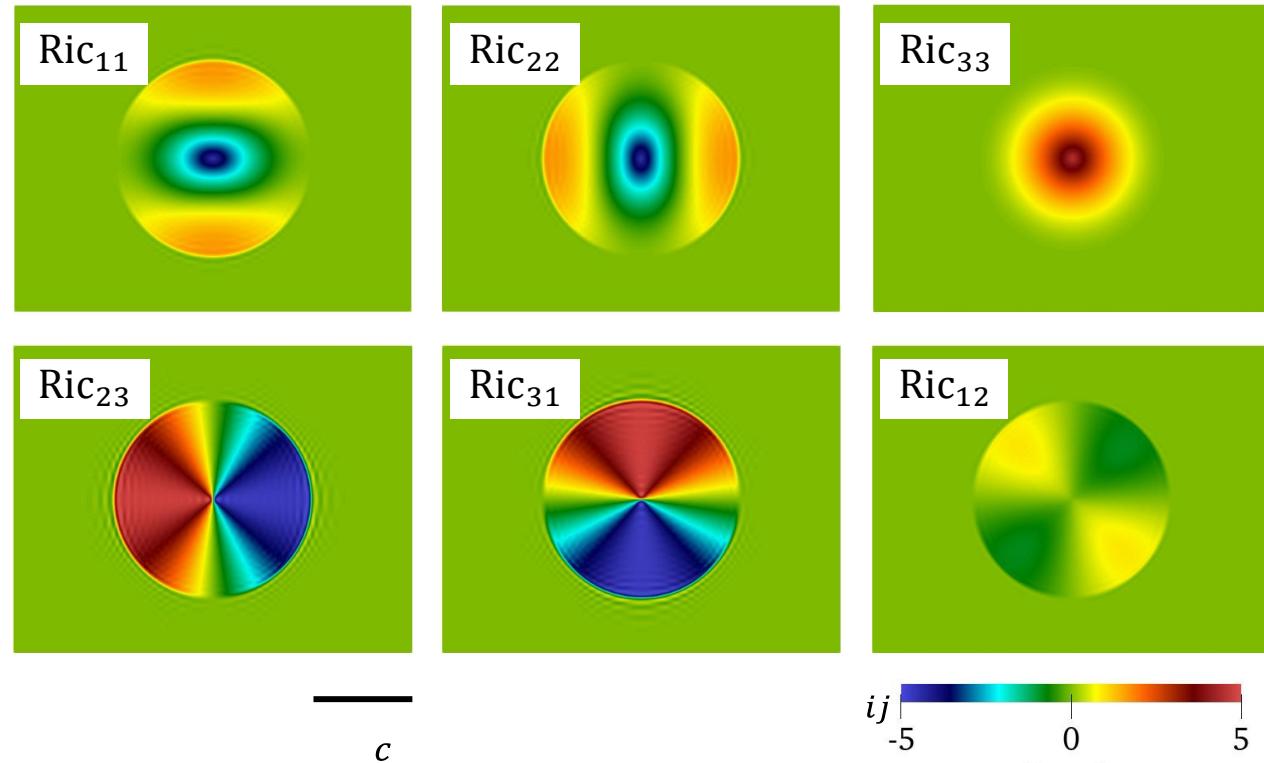
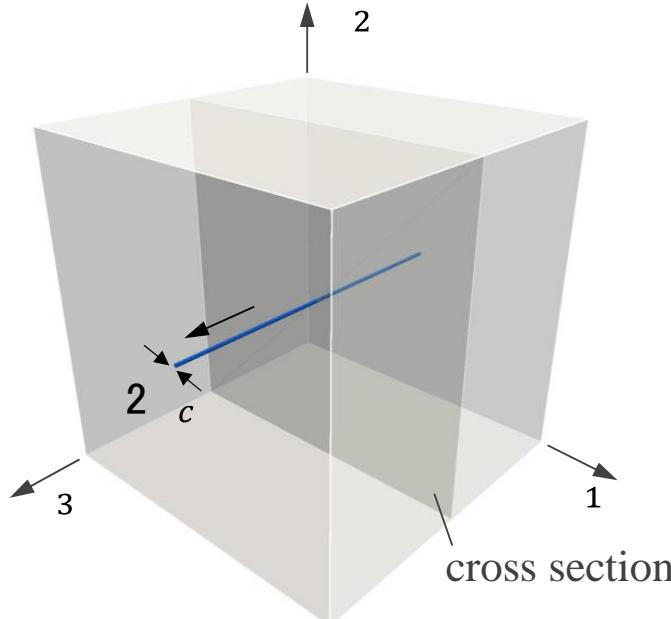
Internal stress fields of screw dislocation (2<sup>nd</sup>-Piola-Kirchhoff stress)



# 1. Geometrical frustration

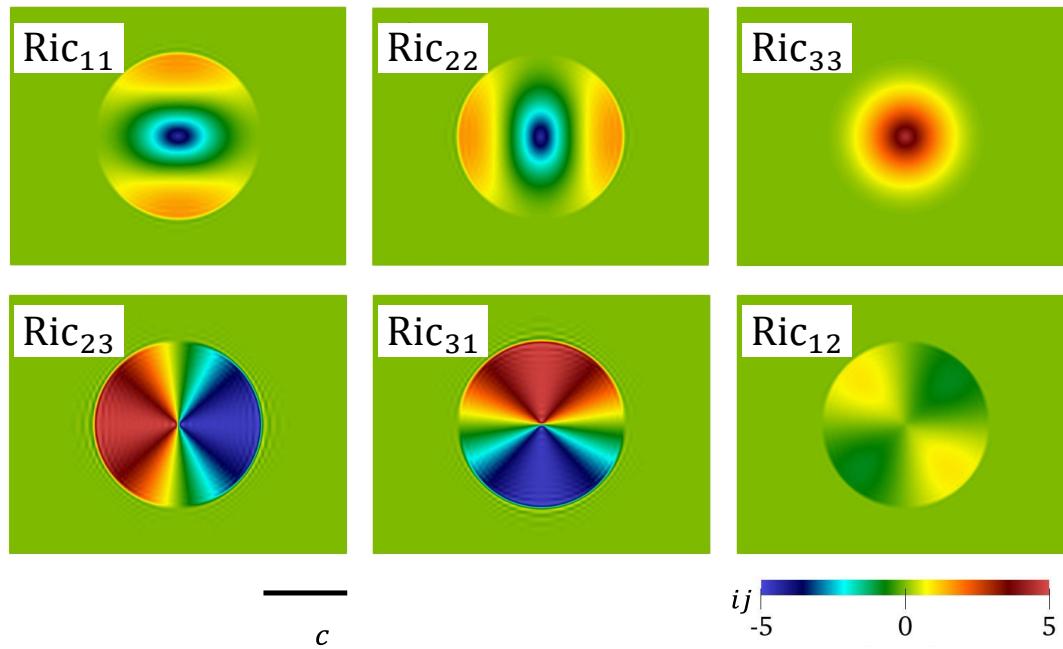
Geometrical frustration of screw dislocation inside the dislocation core

$$\text{Ric}[\vartheta] = R_{ikj}^k [dx^i \otimes dx^j]$$

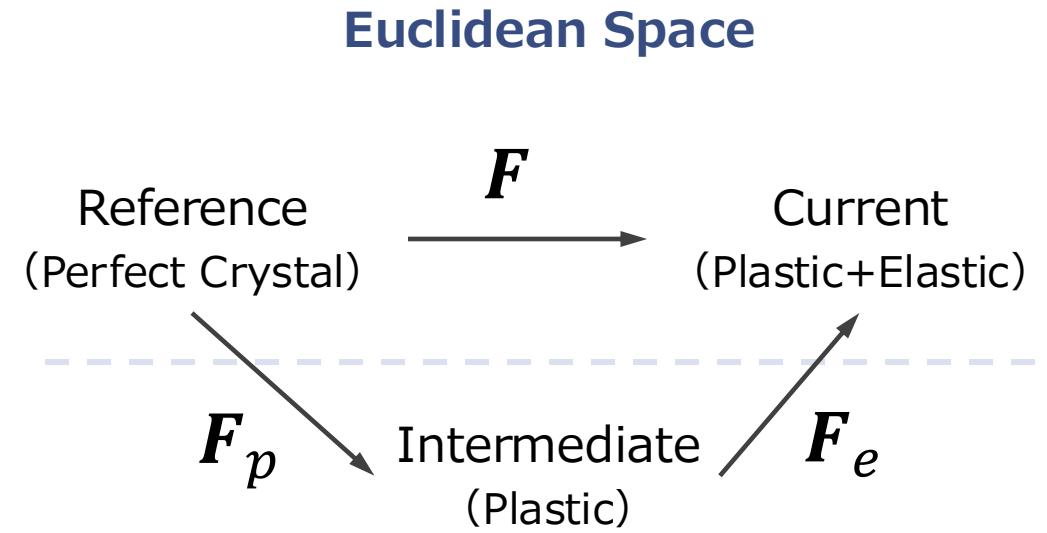


# 1. Geometrical frustration

Duality between the stress and Ricci curvature



$$\text{Ric}[\vartheta] = R^k_{ikj} [dx^i \otimes dx^j]$$



**Differential Geometry**

Remove geometrical frustration

$$\underline{\underline{F}_e = F F_p^{-1}}$$

Stress equilibrium equation  
(Minimize strain energy)

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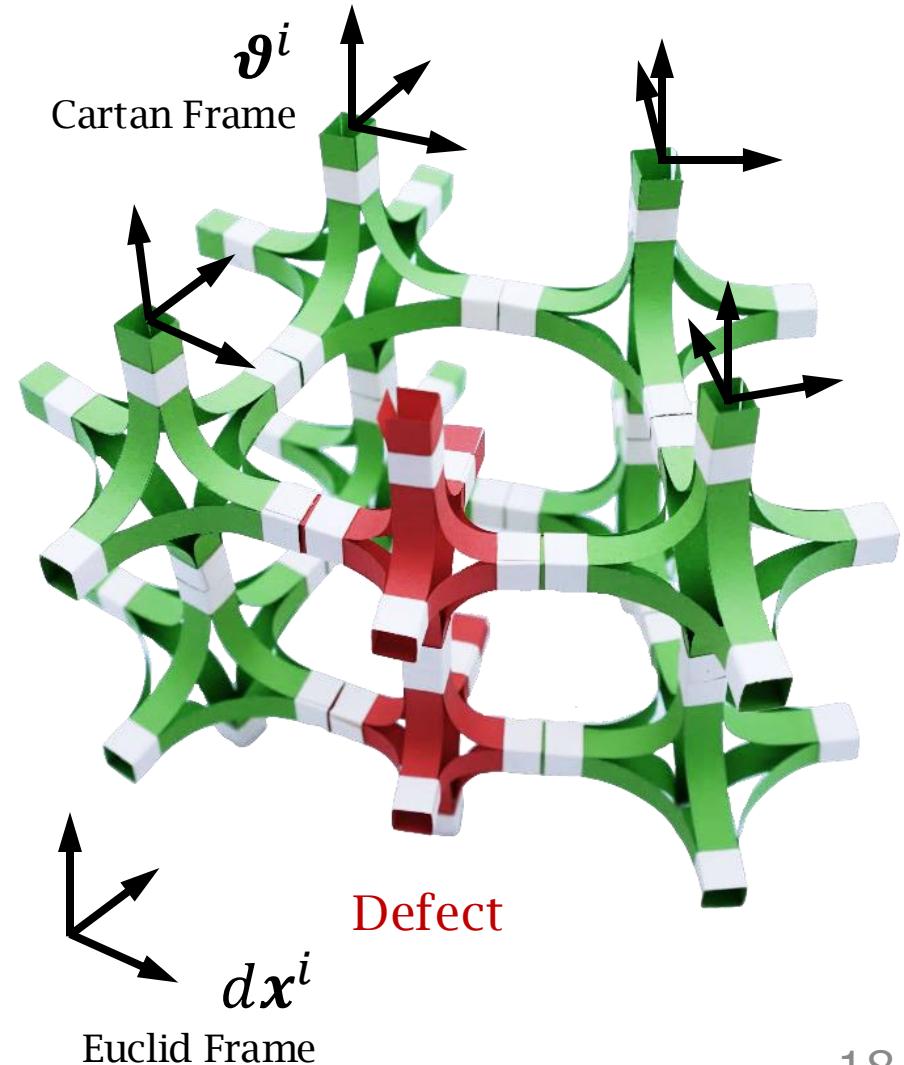
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## 2. Biot-Savart law for dislocations

### Cartan First Structure Equations

- Cartan first structure equation and Helmholtz decomposition

$$\tau^i = d\vartheta^i + \omega_j^i \wedge \vartheta^j$$

$$\vartheta^i = (d\psi^i + \Theta^i) dx^j \otimes E_i$$

**Dislocation Plasticity**  
(Plastic deformation of dislocation)

$$\nabla \times \Theta^i = \tau^i$$

$$\nabla \cdot \Theta^i = 0$$

電磁気学  
(Ampere & Gauss Law)

$$\partial_y \Theta_1^i - \partial_x \Theta_2^i = 0$$

$$\partial_x \Theta_1^i + \partial_y \Theta_2^i = 0$$

複素関数論  
(Cauchy-Riemann Equations)

### Theorem : Biot-Savart Law for Dislocation

Let  $\alpha^i$  be a dislocation density given in an infinite medium. Then, analytical integration of the dual exact form, i.e., plastic displacement gradient of the dislocation, is given by the following form:

$$\Theta^i(x) = \frac{1}{4\pi} \int \frac{* \tau^i(\xi) \times (x - \xi)}{\|x - \xi\|^3} dV$$

## 2. Biot-Savart law for dislocations

### Cartan First Structure Equations

- Cartan first structure equation and Helmholtz decomposition

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**Dislocation Plasticity**  
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**Electromagnetics**  
(Ampere & Gauss Law)

$$\partial_y \Theta_1^i - \partial_x \Theta_2^i = 0$$

$$\partial_x \Theta_1^i + \partial_y \Theta_2^i = 0$$

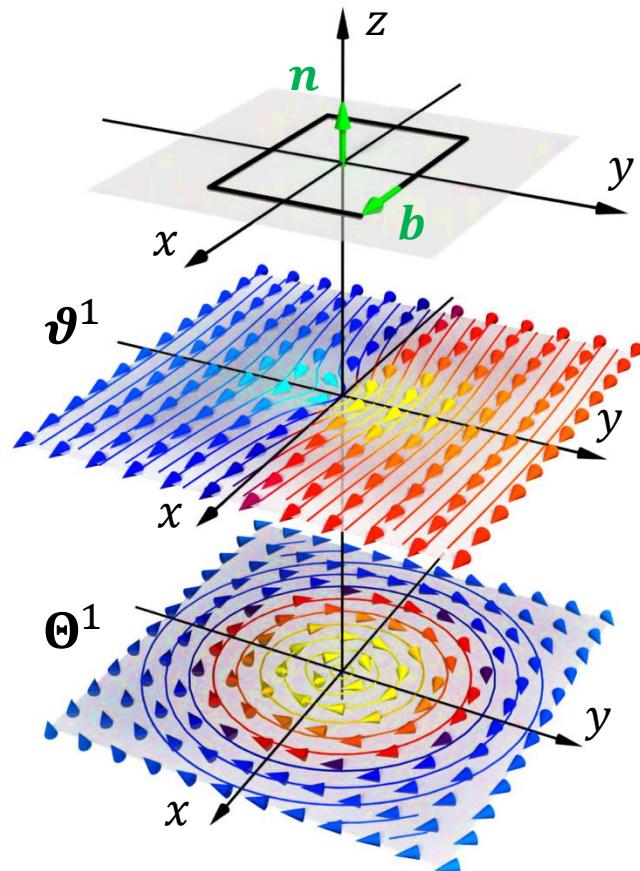
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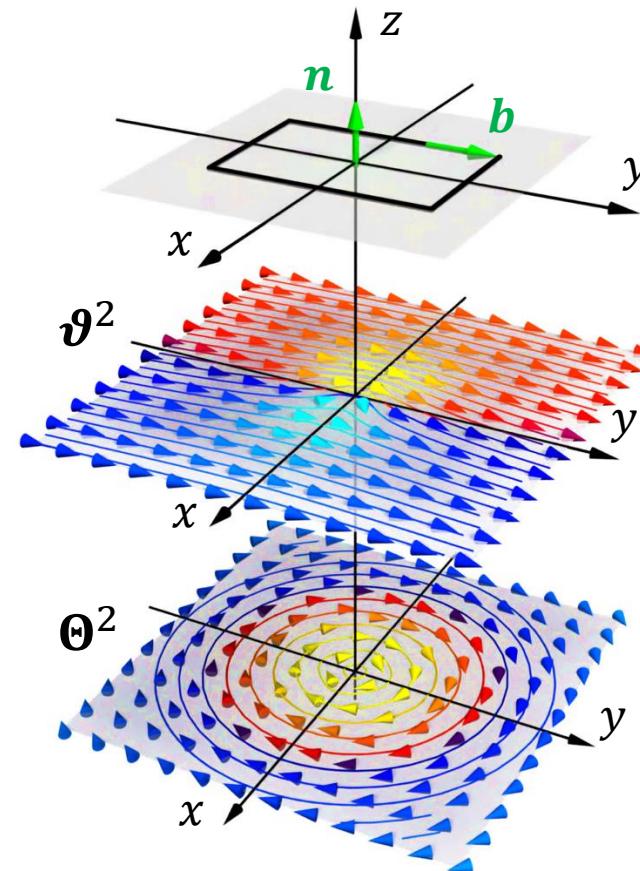
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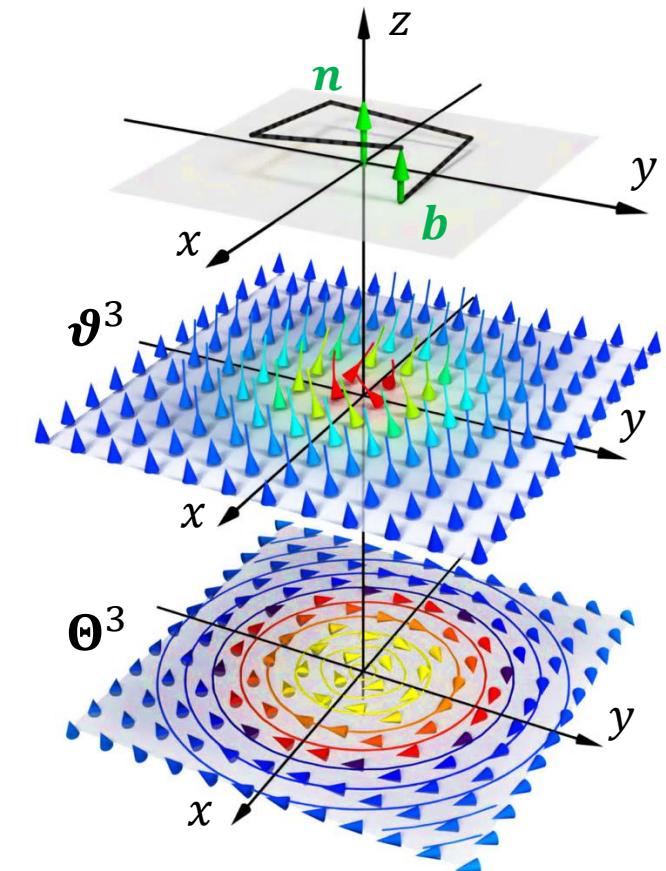
## 2. Biot-Savart law for dislocations



Edge dislocation



Edge dislocation



Screw dislocation

## 2. Biot-Savart law for dislocations

### Cartan First Structure Equations

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$$\partial_y \Theta_1^i - \partial_x \Theta_2^i = 0$$

$$\partial_x \Theta_1^i + \partial_y \Theta_2^i = 0$$

**Complex Function**  
(Cauchy-Riemann Equations)

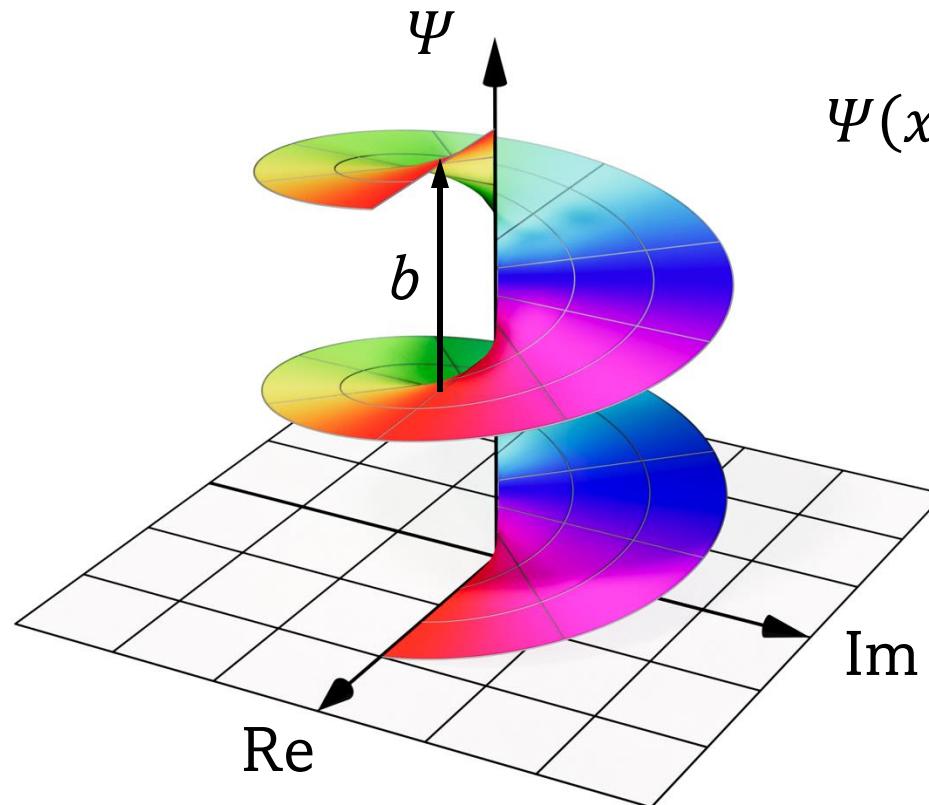
### Theorem : Complex Potential for Dislocations

Plastic displacement gradients  $\Theta^i$  of a dislocation can be obtained from the complex potential of plastic deformation in such a way that

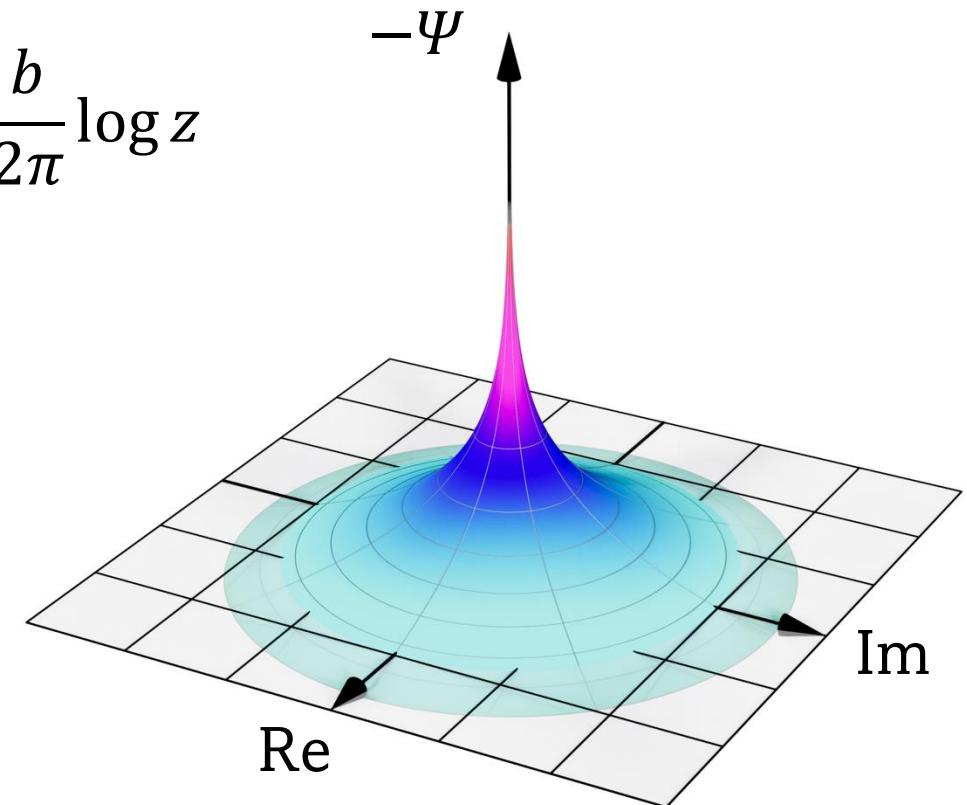
$$\Psi(x, y) = -\frac{b}{2\pi} \log z, \quad \Theta_1^i = \operatorname{Re} \left( \frac{d\Psi}{dz} \right), \quad \Theta_2^i = \operatorname{Im} \left( \frac{d\Psi}{dz} \right)$$

## 2. Biot-Savart law for dislocations

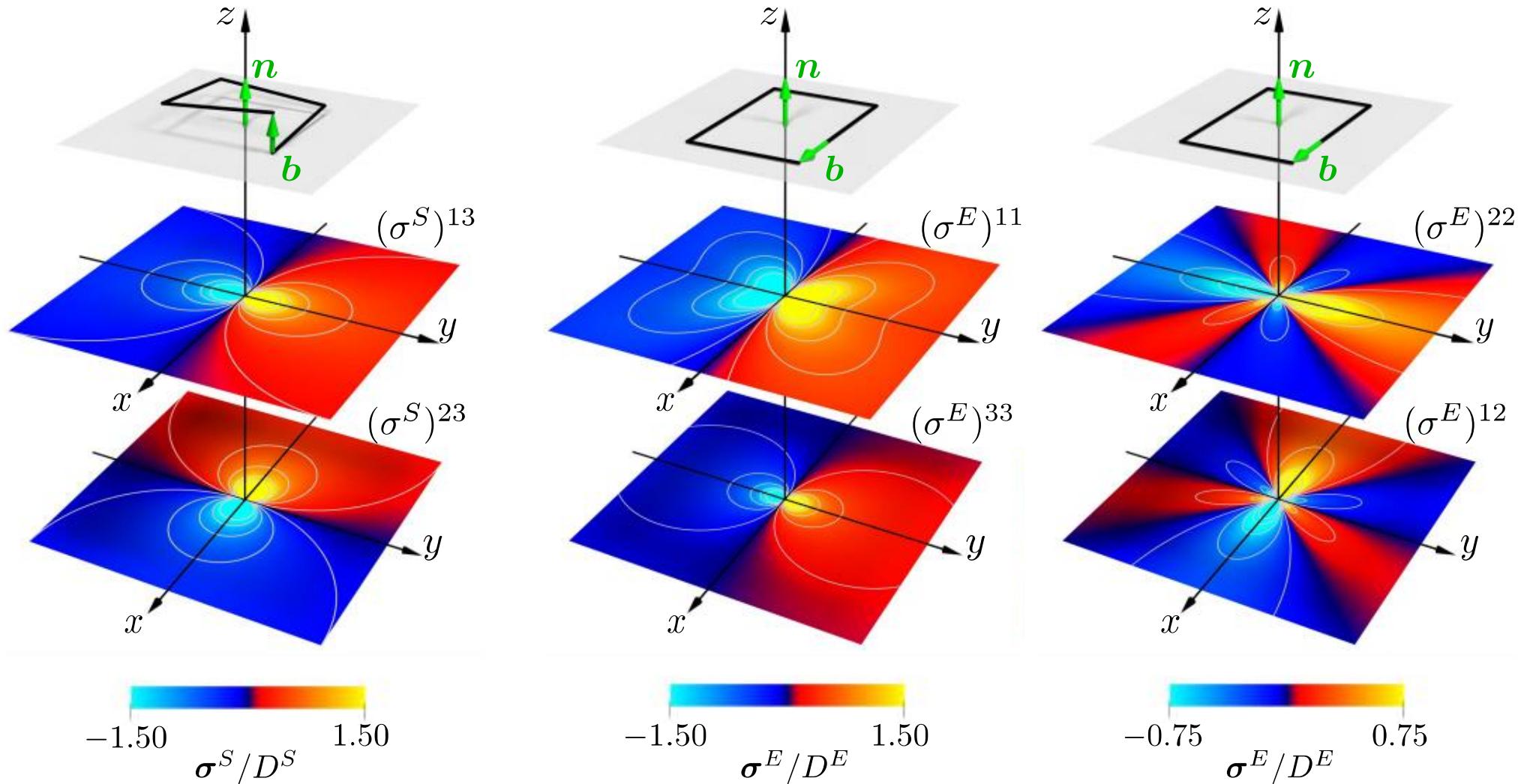
Polar representations of plastic deformation potential  $\psi$



$$\Psi(x, y) = -\frac{b}{2\pi} \log z$$



## 2. Biot-Savart law for dislocations



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# 3. Reconsideration of Volterra defects

Classification of 1-D topological defects by Volterra

Volterra Process for defect

$$\psi(x) = \mathcal{R}(x)x + \mathcal{T}(x)$$

Deformation    Rotation    Translation



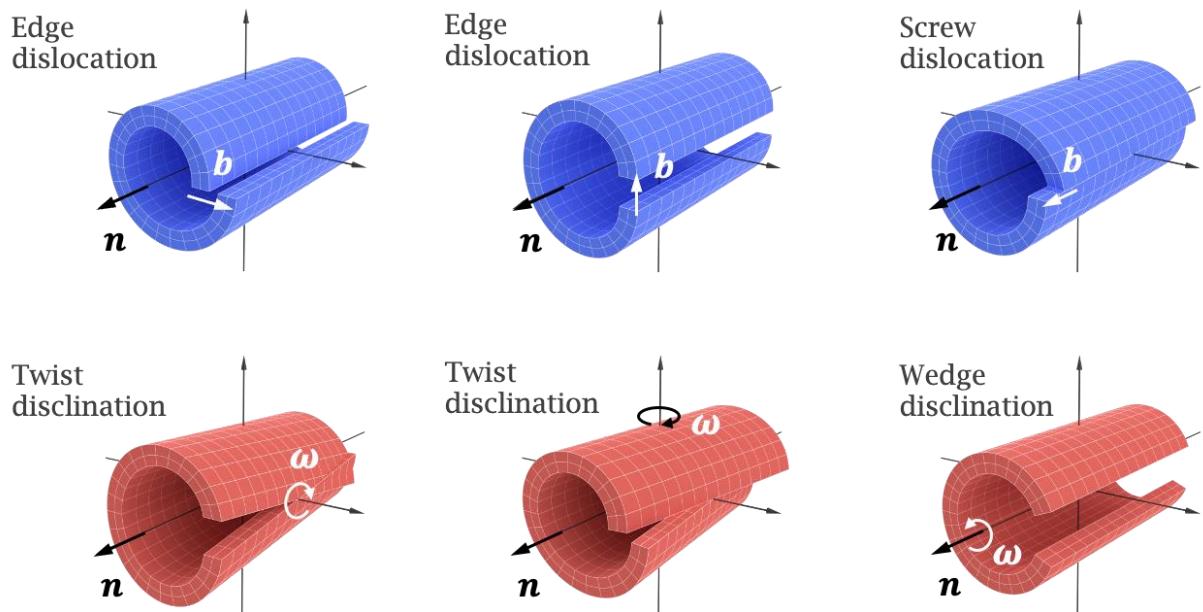
Mathematical issues

- Geometrical definition of disclinations
- Dislocations and disclinations relation



Objective

Clarify the relation between Volterra defects based on the differential geometry



# 3. Reconsideration of Volterra defects

Classification of 1-D topological defects by Volterra

Volterra Process for defect

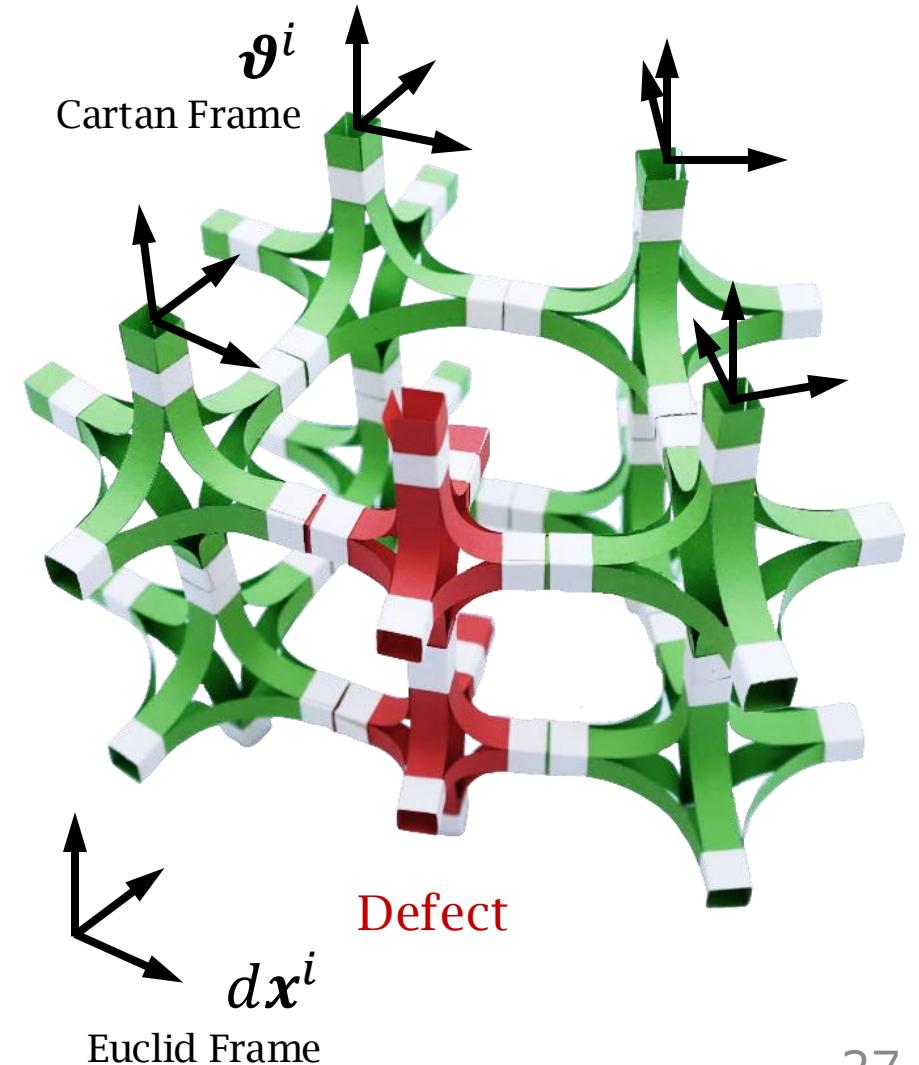
$$\psi(x) = \mathcal{R}(x)x + \mathcal{T}(x)$$

Deformation    Rotation    Translation

Cartan moving frame and Helmholtz decomposition

$$\vartheta^i(x) = dx^i + \Theta^i(x)$$

Cartan Frame    Euclid Frame    Plastic Deformation



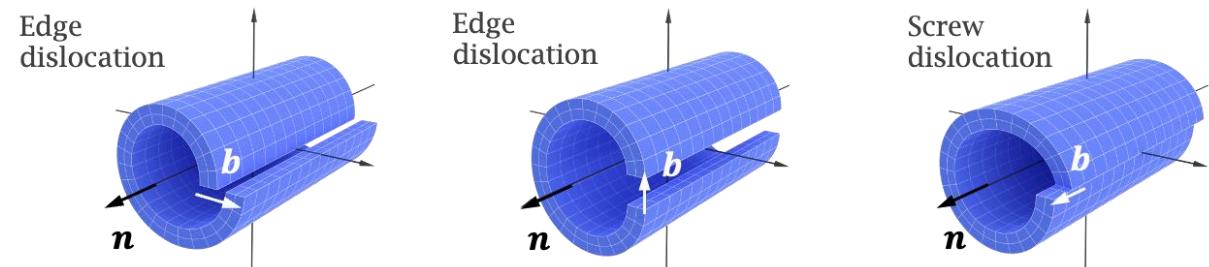
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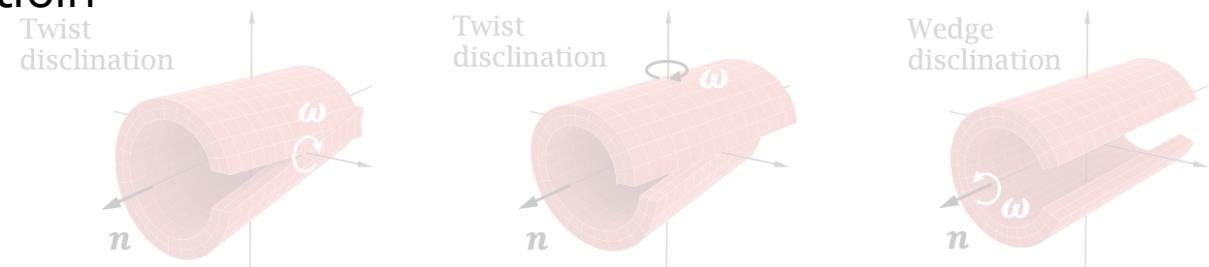
Deformation    Rotation    Translation



Cartan moving frame and Helmholtz decomposition

$$\vartheta^i(x) = dx^i + \Theta^i(x)$$

Cartan Frame    Euclid Frame    Plastic Deformation



Local moving frame

$$\vartheta^i(x) = dx^i + d\mathcal{T}(x)$$

Definition of dislocations by torsions

$$\tau^i = b\delta(x, y)dx \wedge dy$$

$$\Omega = (0, 0, 0)$$

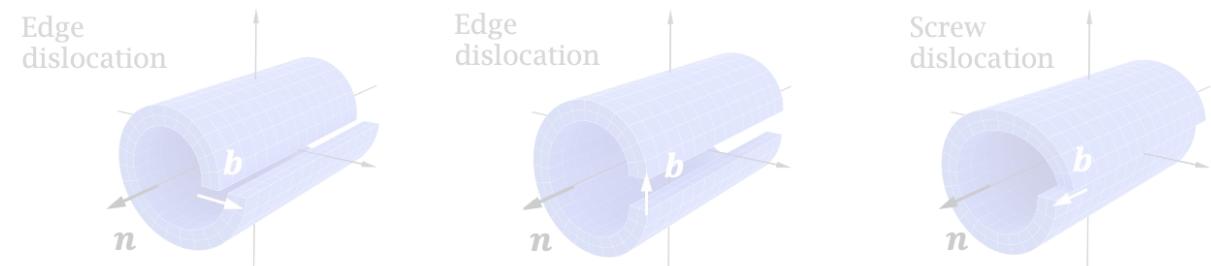
# 3. Reconsideration of Volterra defects

Classification of 1-D topological defects by Volterra

Volterra Process for defect

$$\psi(x) = \mathcal{R}(x)x + \mathcal{T}(x)$$

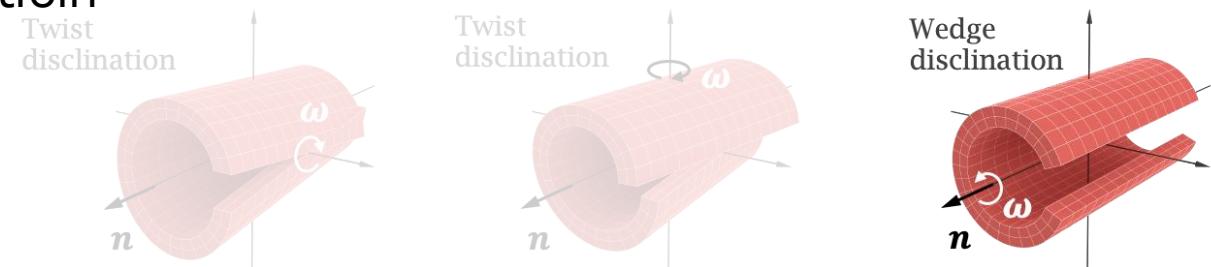
Deformation    Rotation    Translation



Cartan moving frame and Helmholtz decomposition

$$\vartheta^i(x) = dx^i + \Theta^i(x)$$

Cartan Frame    Euclid Frame    Plastic Deformation



Local moving frame

$$\vartheta^i(x) = dx^i + \mathcal{R}^{-1}d\mathcal{R}(x)x \longrightarrow \Omega_2^1 = \phi\delta(x,y)dx \wedge dy$$

$$\tau = (0,0,0)$$

Definition of disclinations by curvature

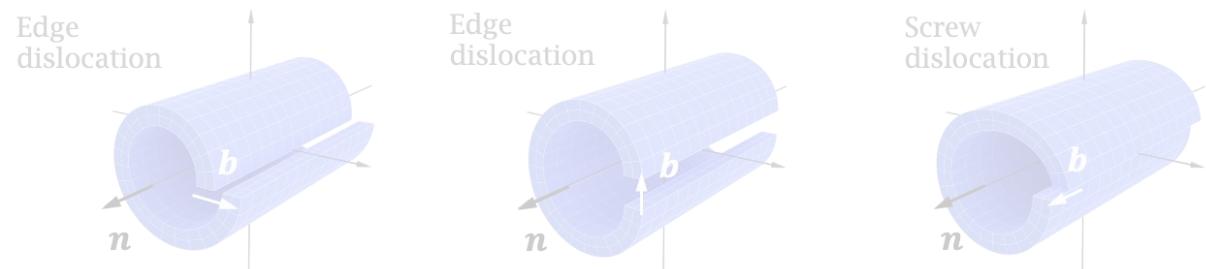
# 3. Reconsideration of Volterra defects

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$$\psi(x) = \mathcal{R}(x)x + \mathcal{T}(x)$$

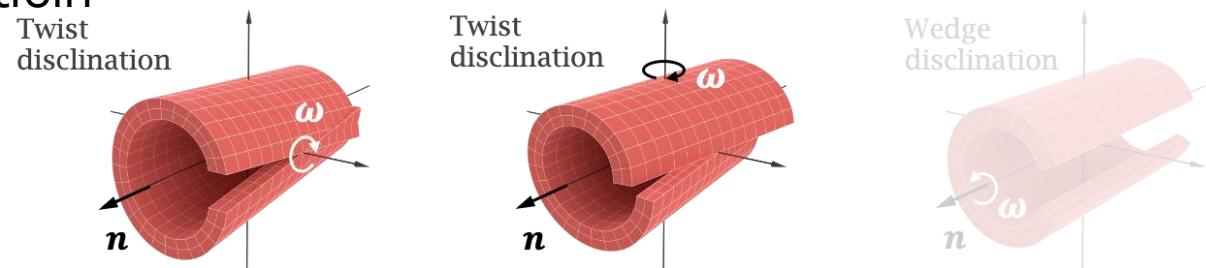
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Twist disclination cannot be defined ...

$$\Omega_3^2 = \omega \delta(x, y) dx \wedge dy$$

$$\tau^1 = \frac{\omega z}{2\pi} \delta(x, y) dx \wedge dy$$

# 3. Reconsideration of Volterra defects

Revision of Volterra Process

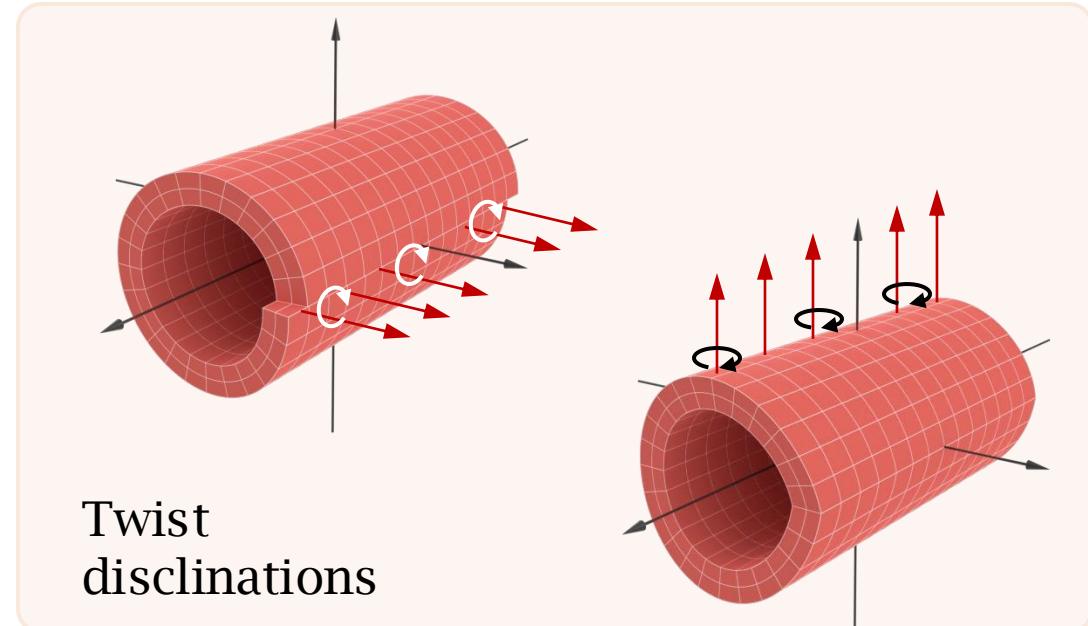
$$\psi(x) = \mathcal{R}(x)(x, y, z)$$

$$\psi(x) = \begin{pmatrix} \cos \frac{\phi}{2\pi} \theta & 0 & \sin \frac{\phi}{2\pi} \theta \\ 0 & 1 & 0 \\ -\sin \frac{\phi}{2\pi} \theta & 0 & \cos \frac{\phi}{2\pi} \theta \end{pmatrix} \begin{pmatrix} x \\ y \\ z \end{pmatrix}$$

 Copy of rotation along z-axis

$$\psi(x) = \mathcal{R}(x)(x, y, 0) + (0, 0, z)$$

$$\psi(x) = \begin{pmatrix} \cos \frac{\phi}{2\pi} \theta & 0 & \sin \frac{\phi}{2\pi} \theta \\ 0 & 1 & 0 \\ -\sin \frac{\phi}{2\pi} \theta & 0 & \cos \frac{\phi}{2\pi} \theta \end{pmatrix} \begin{pmatrix} x \\ y \\ z \end{pmatrix} + \begin{pmatrix} 0 \\ 0 \\ z \end{pmatrix}$$



True definition of twist disclinations by curvature

$$\Omega_3^2 = \phi \delta(x, y) dx \wedge dy$$

$$\boldsymbol{\tau} = (0, 0, 0)$$

### 3. Reconsideration of Volterra defects

Theorem-1 : Wedge disclination dipole at the ends of dislocation array

Weitzenbock cnct.

$$\tau^i = d\vartheta^i + \omega_j^i \wedge \vartheta^j$$

$$\Omega_j^i = d\omega_j^i + \omega_k^i \wedge \omega_j^k$$

Cartan Equations

$$\tau^i = d\vartheta^i + \omega_j^i \wedge \vartheta^j$$

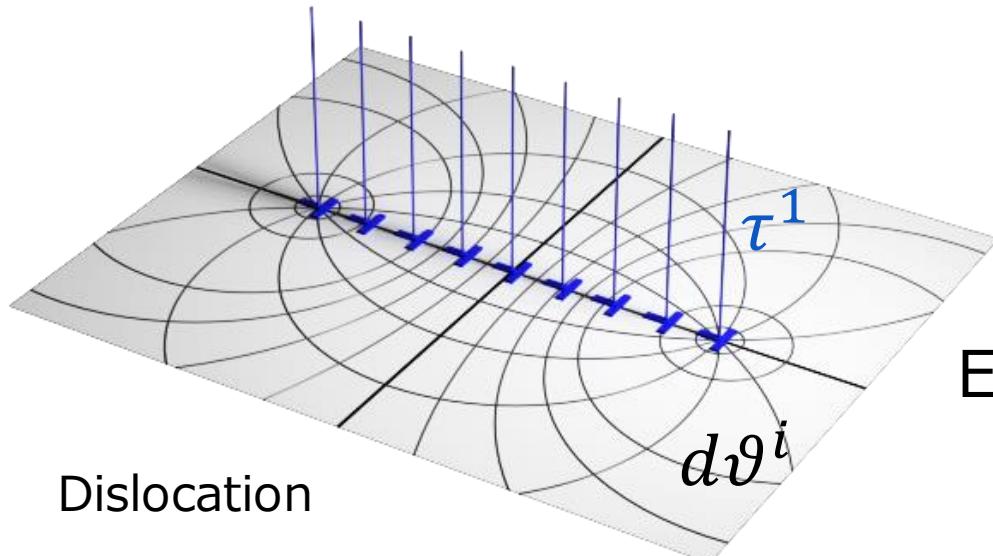
$$\Omega_j^i = d\omega_j^i + \omega_k^i \wedge \omega_j^k$$

Levi-Civita cnct.

$$0 = d\vartheta^i + \omega_j^i \wedge \vartheta^j$$

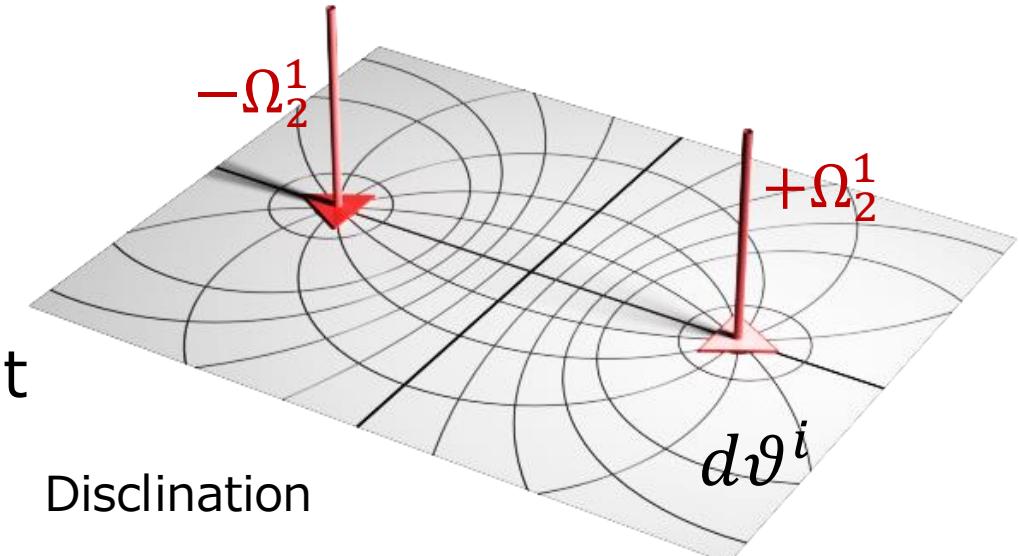
$$\Omega_j^i = d\omega_j^i + \omega_k^i \wedge \omega_j^k$$

$$\tau^1 = b\rho\delta(y)(H(x+L) - H(x-L))dx \wedge dy$$



Equivalent

$$\Omega_2^1 = b\rho(\delta(x-L, y) - \delta(x+L, y))dx \wedge dy$$



### 3. Reconsideration of Volterra defects

Theorem-2 : Edge dislocation is equivalent to wedge disclination dipole

Weitzenbock cnct.

$$\tau^i = d\vartheta^i + \omega_j^i \wedge \vartheta^j$$

$$\Omega_j^i = d\omega_j^i + \omega_k^i \wedge \omega_j^k$$

Cartan Equations

$$\tau^i = d\vartheta^i + \omega_j^i \wedge \vartheta^j$$

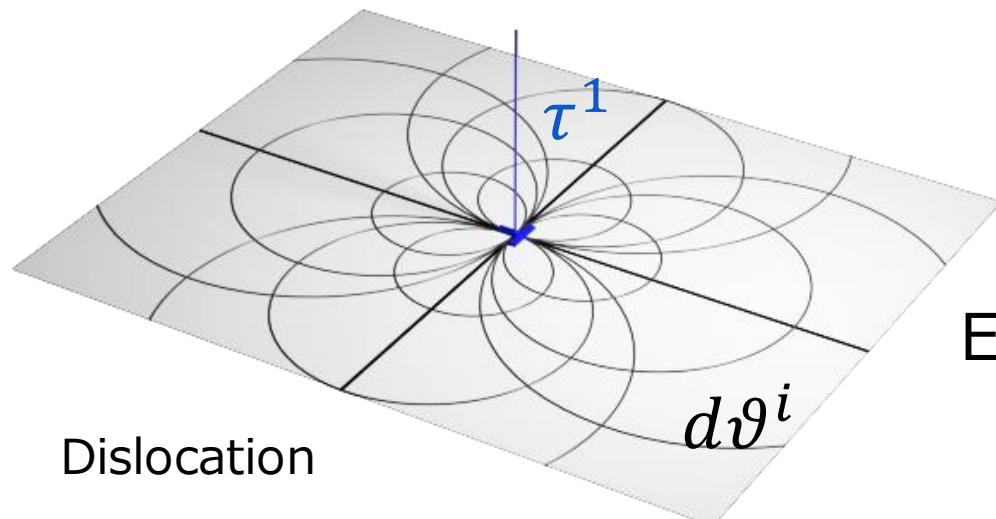
$$\Omega_j^i = d\omega_j^i + \omega_k^i \wedge \omega_j^k$$

Levi-Civita cnct.

$$0 = d\vartheta^i + \omega_j^i \wedge \vartheta^j$$

$$\Omega_j^i = d\omega_j^i + \omega_k^i \wedge \omega_j^k$$

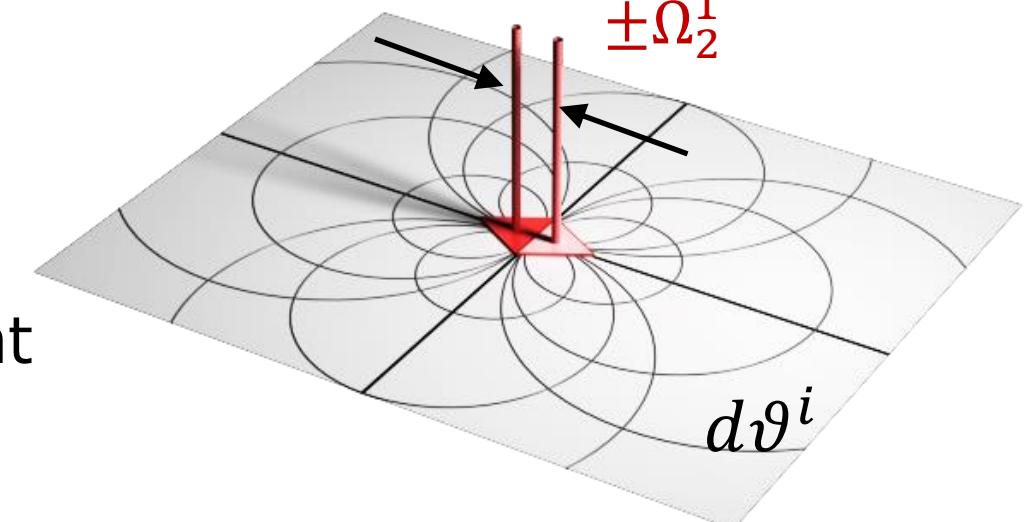
$$\tau^1 = b\delta(x, y) dx \wedge dy$$



Equivalent

$$\lim_{L \rightarrow 0} \Omega_2^1 = \pm\infty$$

$$\pm\Omega_2^1$$



### 3. Reconsideration of Volterra defects

Theorem-3 : Existence of disclination monopole at semi-infinite array of dislocations

Weitzenbock cnct.

$$\tau^i = d\vartheta^i + \omega_j^i \wedge \vartheta^j$$

$$\Omega_j^i = d\omega_j^i + \omega_k^i \wedge \omega_j^k$$

Cartan Equations

$$\tau^i = d\vartheta^i + \omega_j^i \wedge \vartheta^j$$

$$\Omega_j^i = d\omega_j^i + \omega_k^i \wedge \omega_j^k$$

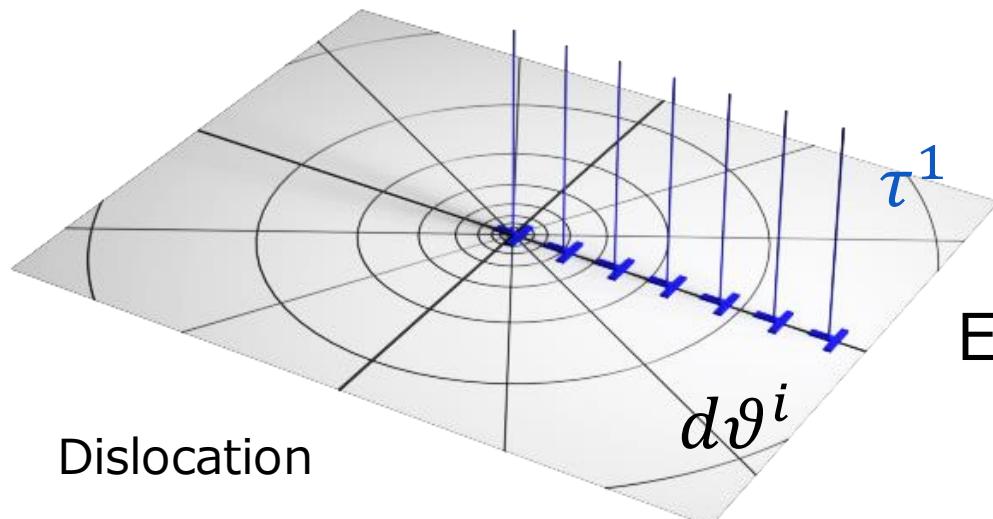
Levi-Civita cnct.

$$0 = d\vartheta^i + \omega_j^i \wedge \vartheta^j$$

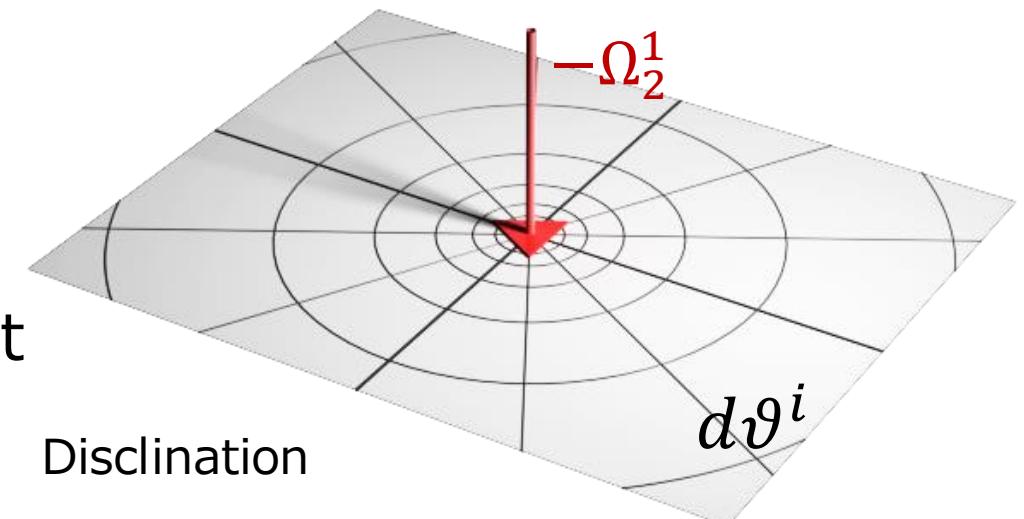
$$\Omega_j^i = d\omega_j^i + \omega_k^i \wedge \omega_j^k$$

$$\tau^1 = b\rho\delta(y)H(x)dx \wedge dy$$

$$\Omega_2^1 = -b\rho\delta(x, y)dx \wedge dy$$

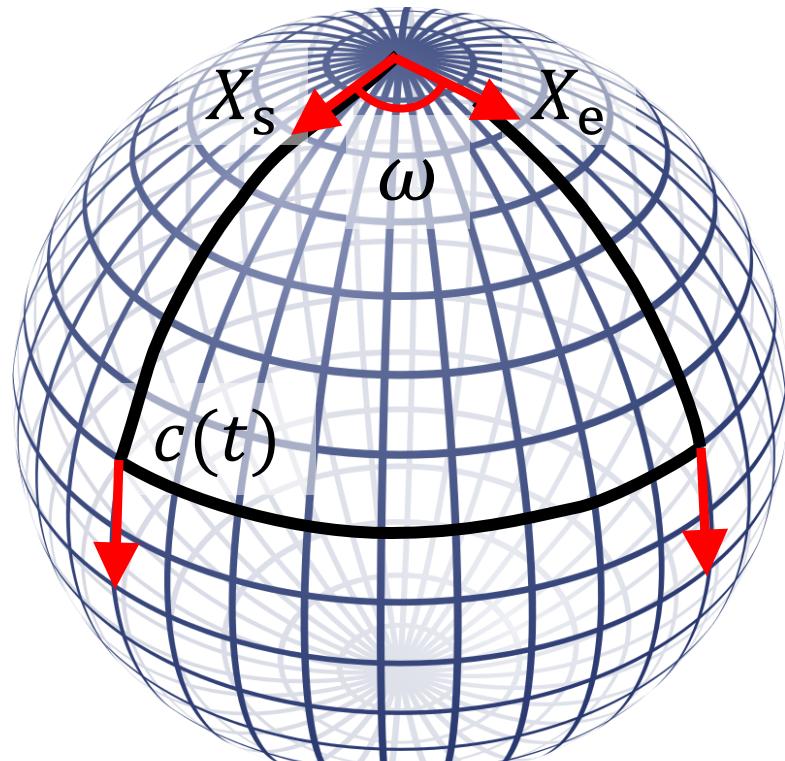


Equivalent



# 3. Reconsideration of Volterra defects

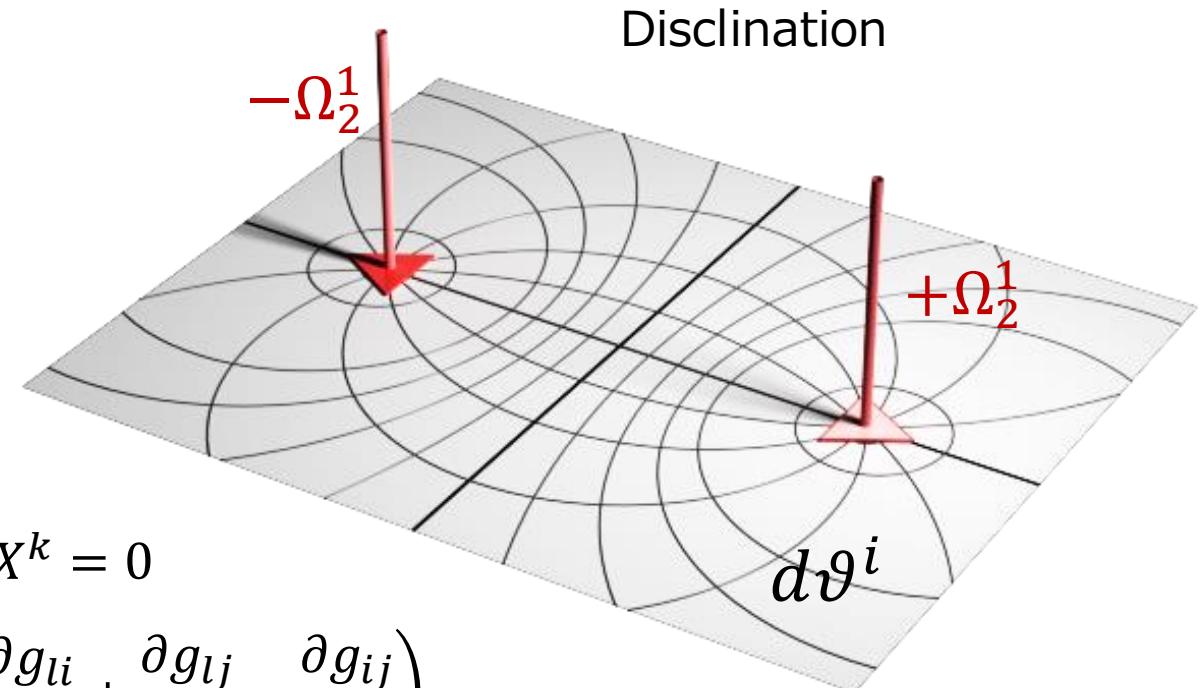
Frank vector of disclination can be measured using holonomy on Riemannian mfd



Parallel transportation of vector

$$\frac{\partial X^i}{\partial t} + \Gamma_{jk}^i \dot{c}^j X^k = 0$$

$$\Gamma_{ij}^k = \frac{g_{kl}^{-1}}{2} \left( \frac{\partial g_{li}}{\partial x_j} + \frac{\partial g_{lj}}{\partial x^i} - \frac{\partial g_{ij}}{\partial x^l} \right)$$



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- What is the origin of stress in crystalline solids?
- Remove stress singularity at the core of dislocation

S. Kobayashi & R. Tarumi, Royal Society Open Science (In Press)

## 2. Biot-Savart law for dislocations

- Cartan structure equation, Maxwell equation and Cauchy-Riemann equation
- Analytical solution of plastic deformation fields

S. Kobayashi & R. Tarumi, Royal Society Open Science (Accepted)

## 3. Reconsideration of Volterra defects

- Geometrical definition of Volterra defects
- Equivalence of edge dislocation and wedge disclination

S. Kobayashi, K. Takemasa & R. Tarumi (to be submitted to RSOS)

## 4. Riemann-Cartan Geometry & Information Geometry

- Unification of materials science using differential geometry

# 4. Riemann-Cartan & Information Geometry

JSPS KAKENHI, Promotion of Innovative Area A (5 years, 1.5 Billion YEN, Deadline: May 2025)

Materials Science



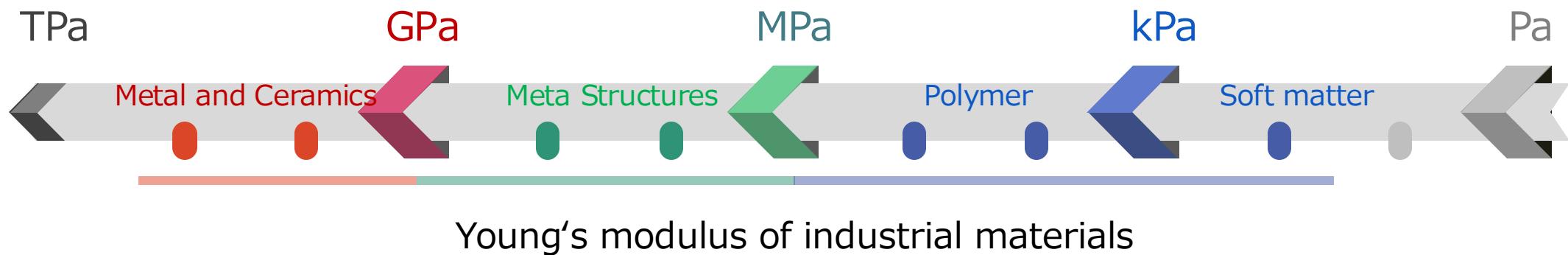
Differential Geometry



In this research field, we will create a new academic discipline called "**Material Geometry**" by integrating "Materials Science" and "Differential Geometry." By establishing a common academic foundation for a wide range of materials, we aim to lead the next generation of materials mechanics research, which will deepen traditional materials science in a more integrated manner.

## 4. Riemann-Cartan & Information Geometry

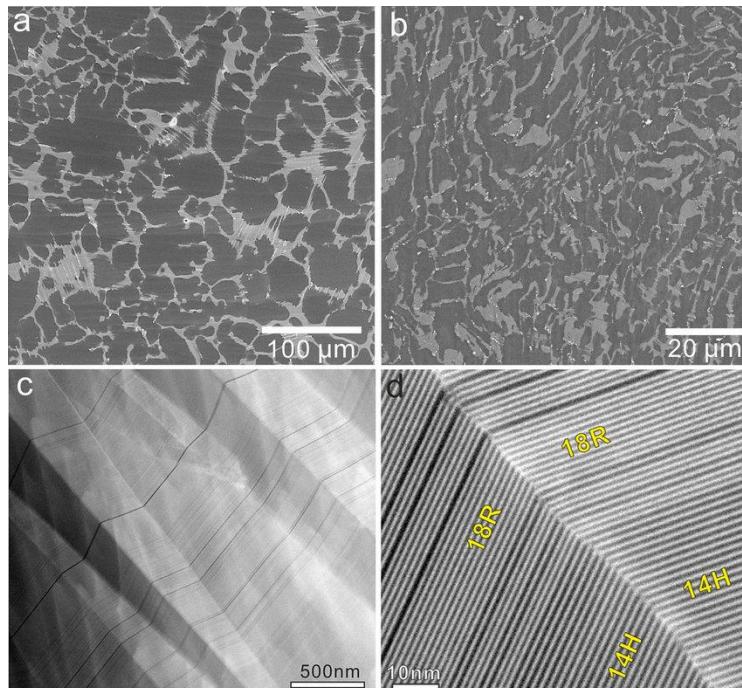
- ✓ 材料科学は高強度化によるCO<sub>2</sub>削減、医療材料、環境保護など産業基盤に直結（材料の国際戦略）
- ✓ 国際的に高い競争力を持つ構造材料や、高機能性材料の研究開発は進むが、基本原理が未解明のものが多く、効率的な応用展開に繋がらない（基本原理の解明・学術の普遍化）
- ✓ 人類が使用する実用材料の剛性比は1,000万倍を超えるため、材料種ごとに専門分野が分かれている。微分幾何学による共通の学術基盤を構築し、イノベーションを促進（学術基盤の共通化）
- ✓ JST「ナノ力学」は、材料の多様性から相乗効果を生み出す革新的な試みで、専門分野を超えた研究者の横の繋がりが生まれ始めている。相乗効果は萌芽的な段階にあるが、この方向性を維持することが重要（多様性の創出）



# 4. Riemann-Cartan & Information Geometry

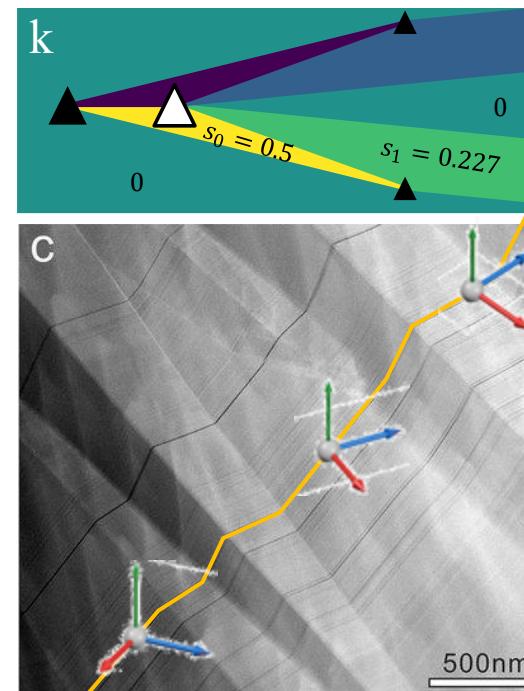
Application of **Riemann-Cartan geometry** for analysis of kink deformation

Kink Analysis



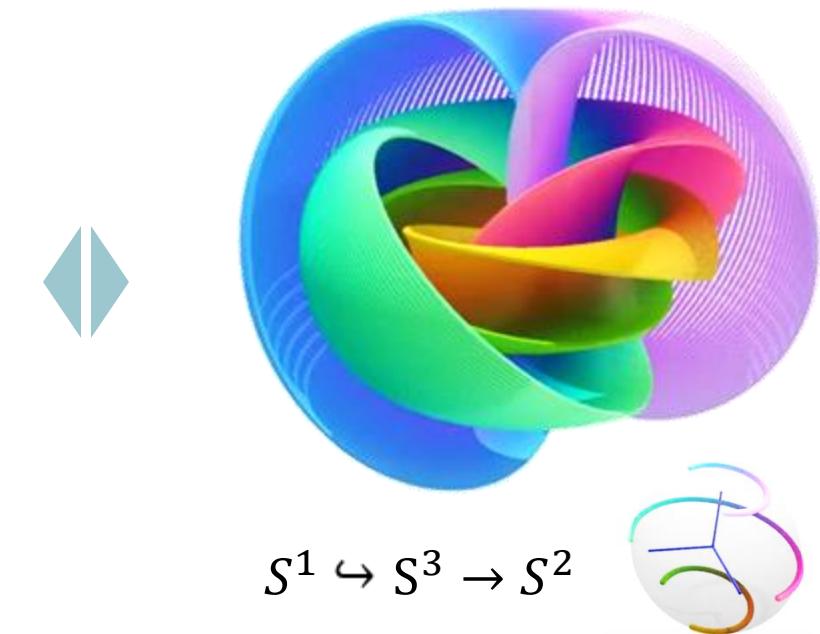
電子顕微鏡によるキンク界面構造の精密解析  
+ 力学特性と構造・組織の関係

Topological Defects



Rank-1接続解析による回位の検出  
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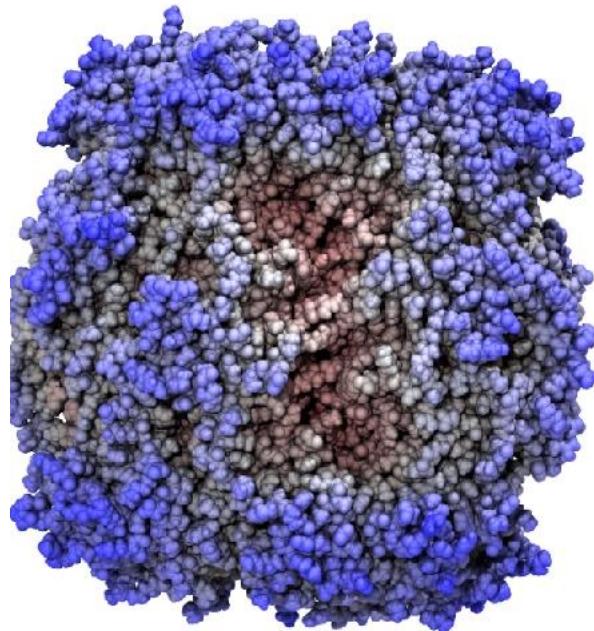


強化原理の普遍化  
(位相微分幾何学によるキンク構造解析)

# 4. Riemann-Cartan & Information Geometry

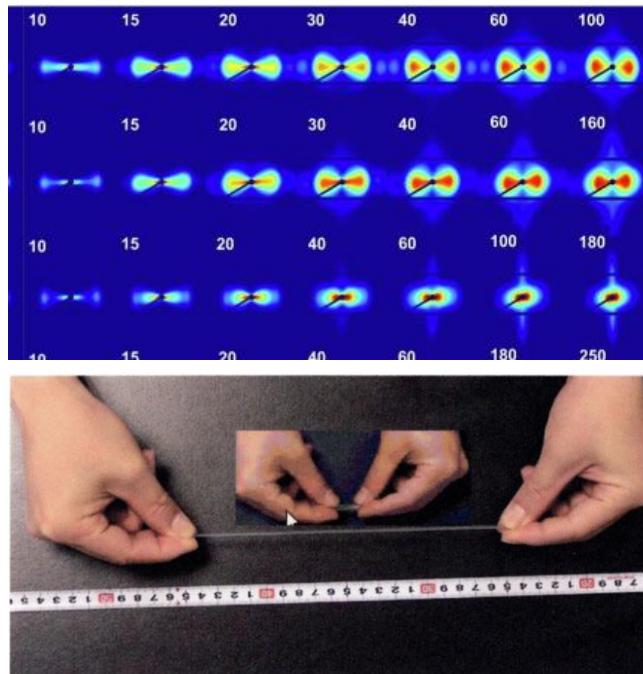
Application of **information geometry** for statistical mechanics of polymers and soft matters

Nonlinear Mechanics



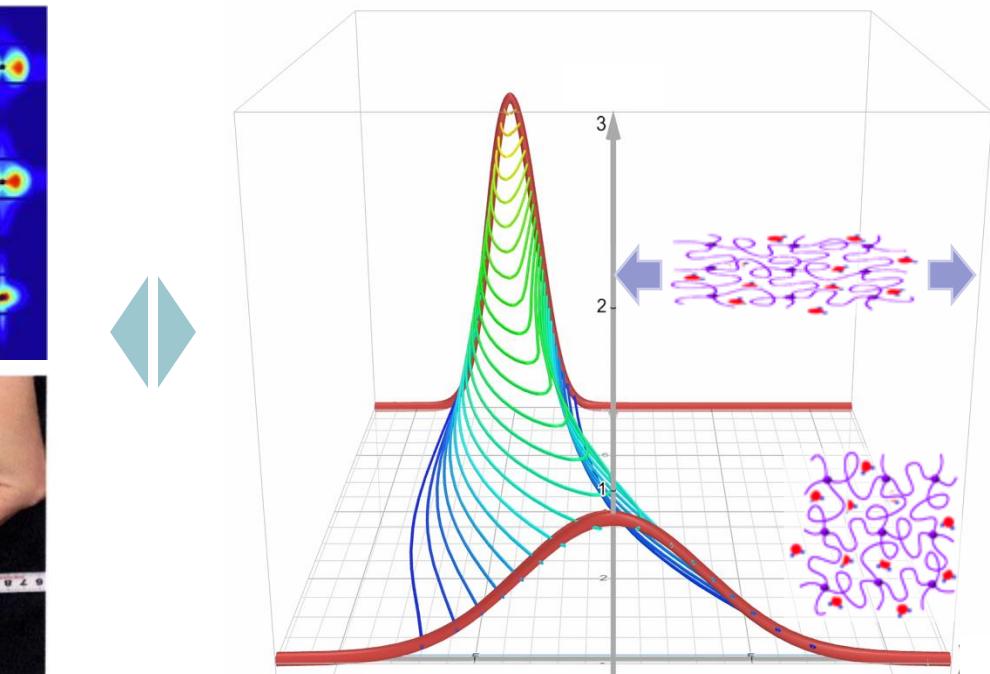
ソフトマテリアルの分子設計と力学特性  
+ 热延伸による高分子の高強度化

X-Ray Scattering and Diffraction



分子鎖ネットワークの配向度・結晶化計測  
+ 分子動力学計算力との比較・検証

Information Geometry



グラフ理論による分子鎖の位相幾何学解析  
+ 確率密度分布の時間発展評価 (情報幾何学)