



## Annex 13

### Methodological “Tool to determine project emissions from flaring gases containing methane”

## I. DEFINITIONS, SCOPE, APPLICABILITY AND PARAMETERS

### Definitions

For the purpose of this tool, the following definitions apply:

- **Residual gas stream.** Gas stream containing methane that is to be flared in hour  $h$  as part of the project activity.
- **Flare efficiency.** Methane destruction efficiency of the flare in hour  $h$ , defined as the ratio between the mass flow rate of methane in the exhaust gas of the flare and the mass flow rate of methane in residual gas stream that is flared (both referred to in dry basis<sup>1</sup> and normal (NTP) conditions).
- **Enclosed flare.** Enclosed flares are defined as devices where the residual gas is burned in a cylindrical or rectilinear enclosure that includes a burning system and a damper where air for the combustion reaction is admitted.
- **Open flare.** Open flares are defined as devices where the residual gas is burned in an open air tip with or without any auxiliary fluid assistance.

### Scope and applicability

This tool provides procedures to calculate project emissions from flaring of a residual gas stream (RG) containing methane.

This tool is applicable under the following conditions:

- The residual gas stream to be flared contains no other combustible gases than methane, carbon monoxide and hydrogen;
- The residual gas stream to be flared shall be obtained from decomposition of organic material (through landfills, bio-digesters or anaerobic lagoons, among others) or from gases vented in coal mines (coal mine methane and coal bed methane).

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<sup>1</sup> Dry basis refers to dry gas conditions (moisture must be discounted from flow rate and composition).



## Parameters

This tool provides procedures to determine the following parameters :

Parameter	SI Unit	Description
PE <sub>flare,y</sub>	tCO <sub>2e</sub>	Project emissions from flaring of the residual gas stream in year <i>y</i>
η <sub>flare,h</sub>	-	Flare efficiency in hour <i>h</i> based on measurements or default values.

The following data are required by this tool:

Parameter	SI Unit	Description
f <sub>v,i,h</sub>	-	Volumetric fraction of component <i>i</i> in the residual gas in the hour <i>h</i> where <i>i</i> = CH <sub>4</sub> , CO, CO <sub>2</sub> , O <sub>2</sub> , H <sub>2</sub> , N <sub>2</sub>
FV <sub>RG,h</sub>	m <sup>3</sup> /h	Volumetric flow rate of the residual gas in dry basis at normal (NTP) conditions <sup>2</sup> in the hour <i>h</i>
t <sub>O<sub>2,h</sub></sub>	-	Volumetric fraction of O <sub>2</sub> in the exhaust gas of the flare in the hour <i>h</i> (only in case the flare efficiency is continuously monitored)
f <sub>v,CH<sub>4,FG,h</sub></sub>	mg/m <sup>3</sup>	Concentration of methane in the exhaust gas of the flare in dry basis at normal conditions in the hour <i>h</i> (only in the case the flare efficiency is continuously monitored)
T <sub>flare</sub>	°C	Temperature in the exhaust gas of the enclosed flare
		Any other parameters required to monitor proper operation of the flare according to the manufacturer's specification (only in the case of use of a default value for the flare efficiency of enclosed and open flares)

## II. BASELINE METHODOLOGY PROCEDURE

Project emissions from flaring of the residual gas stream are calculated based on the flare efficiency and the mass flow rate of methane in the residual gas stream that is flared. The flare efficiency depends on both the actual efficiency of combustion in the flare and the time that the flare is operating. The efficiency of combustion in the flare is calculated from the methane content in the exhaust gas of the flare, corrected for the air used in the combustion process, and the methane content in the residual gas.

In case of open flares, the flare efficiency cannot be measured in a reliable manner (i.e. external air will be mixed and will dilute the remaining methane) and a default value of 50%<sup>3</sup> is to be used provided that it can be demonstrated that the flare is operational (e.g. through a flame detection system reporting electronically on continuous basis)). If the flare is not operational the default value to be adopted for flare efficiency is 0%.

<sup>2</sup> Normal (NTP) conditions are 101.325 kPa and 273.15 K.

<sup>3</sup> Whenever the default value for the flare efficiency (either open flare or enclosed flare) is to be used for calculation of project emissions in equation 15 below, the value should be converted into fraction (e.g. 50/100= 0.5) before use in the equation.



For enclosed flares, the temperature in the exhaust gas of the flare is measured to determine whether the flare is operating or not.

For enclosed flares, either of the following two options can be used to determine the flare efficiency:

- (a) To use a 90% default value. Continuous monitoring of compliance with manufacturer's specification of flare (temperature, flow rate of residual gas at the inlet of the flare) must be performed. If in a specific hour any of the parameters are out of the limit of manufacturer's specifications, a 50% default value for the flare efficiency should be used for the calculations for this specific hour.
- (b) Continuous monitoring of the methane destruction efficiency of the flare (flare efficiency).

In both cases, if there is no record of the temperature of the exhaust gas of the flare or if the recorded temperature is less than 500 °C for any particular hour, it shall be assumed that during that hour the flare efficiency is zero.

Project participants should document in the CDM-PDD, which type of flare and which approach to determine the flare efficiency is used. In case of use of the default value for the methane destruction efficiency, the manufacturer's specifications for the operation of the flare and the required data and procedures to monitor these specifications should be documented in the CDM-PDD.

This tool involves the following seven steps:

- STEP 1: Determination of the mass flow rate of the residual gas that is flared
- STEP 2: Determination of the mass fraction of carbon, hydrogen, oxygen and nitrogen in the residual gas
- STEP 3: Determination of the volumetric flow rate of the exhaust gas on a dry basis
- STEP 4: Determination of methane mass flow rate of the exhaust gas on a dry basis
- STEP 5: Determination of methane mass flow rate of the residual gas on a dry basis
- STEP 6: Determination of the hourly flare efficiency
- STEP 7: Calculation of annual project emissions from flaring based on measured hourly values or based on default flare efficiencies.

Project participants shall apply these steps to calculate project emissions from flaring ( $PE_{flare,y}$ ) based on the measured hourly flare efficiency or based on the default values for the flare efficiency ( $\eta_{flare,h}$ ). Note that steps 3 and 4 are only applicable in case of enclosed flares and continuous monitoring of the flare efficiency.

The calculation procedure in this tool determines the flow rate of methane before and after the destruction in the flare, taking into account the amount of air supplied to the combustion reaction and the exhaust gas composition (oxygen and methane). The flare efficiency is calculated for each hour of a year based either on measurements or default values plus operational parameters. Project emissions are determined by multiplying the methane flow rate in the residual gas with the flare efficiency for each hour of the year.



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**STEP 1. Determination of the mass flow rate of the residual gas that is flared**

This step calculates the residual gas mass flow rate in each hour  $h$ , based on the volumetric flow rate and the density of the residual gas. The density of the residual gas is determined based on the volumetric fraction of all components in the gas.

$$FM_{RG,h} = \rho_{RG,n,h} \times FV_{RG,h} \quad (1)$$

Where:

Variable	SI Unit	Description
$FM_{RG,h}$	kg/h	Mass flow rate of the residual gas in hour $h$
$\rho_{RG,n,h}$	kg/m <sup>3</sup>	Density of the residual gas at normal conditions in hour $h$
$FV_{RG,h}$	m <sup>3</sup> /h	Volumetric flow rate of the residual gas in dry basis at normal conditions in the hour $h$

and:

$$\rho_{RG,n,h} = \frac{P_n}{\frac{R_u}{MM_{RG,h}} \times T_n} \quad (2)$$

Where:

Variable	SI Unit	Description
$\rho_{RG,n,h}$	kg/m <sup>3</sup>	Density of the residual gas at normal conditions in hour $h$
$P_n$	Pa	Atmospheric pressure at normal conditions (101 325)
$R_u$	Pa.m <sup>3</sup> /kmol.K	Universal ideal gas constant (8 314)
$MM_{RG,h}$	kg/kmol	Molecular mass of the residual gas in hour $h$
$T_n$	K	Temperature at normal conditions (273.15)

and:

$$MM_{RG,h} = \sum_i (fv_{i,h} * MM_i) \quad (3)$$

Where:

Variable	SI Unit	Description
$MM_{RG,h}$	kg/kmol	Molecular mass of the residual gas in hour $h$
$fv_{i,h}$	-	Volumetric fraction of component $i$ in the residual gas in the hour $h$
$MM_i$	kg/kmol	Molecular mass of residual gas component $i$
I		The components CH <sub>4</sub> , CO, CO <sub>2</sub> , O <sub>2</sub> , H <sub>2</sub> , N <sub>2</sub>

As a simplified approach, project participants may only measure the volumetric fraction of methane and consider the difference to 100% as being nitrogen (N<sub>2</sub>).



## STEP 2. Determination of the mass fraction of carbon, hydrogen, oxygen and nitrogen in the residual gas

Determine the mass fractions of carbon, hydrogen, oxygen and nitrogen in the residual gas, calculated from the volumetric fraction of each component  $i$  in the residual gas, as follows:

$$fm_{j,h} = \frac{\sum_i fv_{i,h} \cdot AM_j \cdot NA_{j,i}}{MM_{RG,h}} \quad (4)$$

Where:

Variable	SI Unit	Description
$fm_{j,h}$	-	Mass fraction of element $j$ in the residual gas in hour $h$
$fv_{i,h}$	-	Volumetric fraction of component $i$ in the residual gas in the hour $h$
$AM_j$	kg/kmol	Atomic mass of element $j$
$NA_{j,i}$	-	Number of atoms of element $j$ in component $i$
$MM_{RG,h}$	kg/kmol	Molecular mass of the residual gas in hour $h$
$j$		The elements carbon, hydrogen, oxygen and nitrogen
$i$		The components $CH_4, CO, CO_2, O_2, H_2, N_2$

## STEP 3. Determination of the volumetric flow rate of the exhaust gas on a dry basis

This step is only applicable if the methane combustion efficiency of the flare is continuously monitored.

Determine the average volumetric flow rate of the exhaust gas in each hour  $h$  based on a stoichiometric calculation of the combustion process, which depends on the chemical composition of the residual gas, the amount of air supplied to combust it and the composition of the exhaust gas, as follows:

$$TV_{n,FG,h} = V_{n,FG,h} \times FM_{RG,h} \quad (5)$$

Where:

Variable	SI Unit	Description
$TV_{n,FG,h}$	$m^3/h$	Volumetric flow rate of the exhaust gas in dry basis at normal conditions in hour $h$
$V_{n,FG,h}$	$m^3/kg$ residual gas	Volume of the exhaust gas of the flare in dry basis at normal conditions per kg of residual gas in hour $h$
$FM_{RG,h}$	kg residual gas/h	Mass flow rate of the residual gas in the hour $h$



$$V_{n,FG,h} = V_{n,CO_2,h} + V_{n,O_2,h} + V_{n,N_2,h} \quad (6)$$

Where:

Variable	SI Unit	Description
$V_{n,FG,h}$	$\text{m}^3/\text{kg residual gas}$	Volume of the exhaust gas of the flare in dry basis at normal conditions per kg of residual gas in the hour $h$
$V_{n,CO_2,h}$	$\text{m}^3/\text{kg residual gas}$	Quantity of $\text{CO}_2$ volume free in the exhaust gas of the flare at normal conditions per kg of residual gas in the hour $h$
$V_{n,N_2,h}$	$\text{m}^3/\text{kg residual gas}$	Quantity of $\text{N}_2$ volume free in the exhaust gas of the flare at normal conditions per kg of residual gas in the hour $h$
$V_{n,O_2,h}$	$\text{m}^3/\text{kg residual gas}$	Quantity of $\text{O}_2$ volume free in the exhaust gas of the flare at normal conditions per kg of residual gas in the hour $h$

$$V_{n,O_2,h} = n_{O_2,h} \times MV_n \quad (7)$$

Where:

Variable	SI Unit	Description
$V_{n,O_2,h}$	$\text{m}^3/\text{kg residual gas}$	Quantity of $\text{O}_2$ volume free in the exhaust gas of the flare at normal conditions per kg of residual gas in the hour $h$
$n_{O_2,h}$	$\text{kmol/kg residual gas}$	Quantity of moles $\text{O}_2$ in the exhaust gas of the flare per kg residual gas flared in hour $h$
$MV_n$	$\text{m}^3/\text{kmol}$	Volume of one mole of any ideal gas at normal temperature and pressure (22.4 L/mol)

$$V_{n,N_2,h} = MV_n * \left\{ \frac{fm_{N,h}}{200AM_N} + \left( \frac{1 - MF_{O_2}}{MF_{O_2}} \right) * [F_h + n_{O_2,h}] \right\} \quad (8)$$

Where:

Variable	SI Unit	Description
$V_{n,N_2,h}$	$\text{m}^3/\text{kg residual gas}$	Quantity of $\text{N}_2$ volume free in the exhaust gas of the flare at normal conditions per kg of residual gas in the hour $h$
$MV_n$	$\text{m}^3/\text{kmol}$	Volume of one mole of any ideal gas at normal temperature and pressure (22.4 $\text{m}^3/\text{Kmol}$ )
$fm_{N,h}$	-	Mass fraction of nitrogen in the residual gas in the hour $h$
$AM_n$	$\text{kg/kmol}$	Atomic mass of nitrogen
$MF_{O_2}$	-	$\text{O}_2$ volumetric fraction of air
$F_h$	$\text{kmol/kg residual gas}$	Stoichiometric quantity of moles of $\text{O}_2$ required for a complete oxidation of one kg residual gas in hour $h$
$n_{O_2,h}$	$\text{kmol/kg residual gas}$	Quantity of moles $\text{O}_2$ in the exhaust gas of the flare per kg residual gas flared in hour $h$



$$V_{n,CO_2,h} = \frac{fm_{C,h}}{AM_C} * MV_n \quad (9)$$

Where:

Variable	SI Unit	Description
V <sub>n,CO<sub>2</sub>,h</sub>	m <sup>3</sup> /kg residual gas	Quantity of CO <sub>2</sub> volume free in the exhaust gas of the flare at normal conditions per kg of residual gas in the hour h
fm <sub>C,h</sub>	-	Mass fraction of carbon in the residual gas in the hour h
AM <sub>C</sub>	kg/kmol	Atomic mass of carbon
MV <sub>n</sub>	m <sup>3</sup> /kmol	Volume of one mole of any ideal gas at normal temperature and pressure (22.4 m <sup>3</sup> /Kmol)

$$n_{O_2,h} = \frac{t_{O_2,h}}{(1 - (t_{O_2,h} / MF_{O_2}))} \times \left[ \frac{fm_{C,h}}{AM_C} + \frac{fm_{N,h}}{2AM_N} + \left( \frac{1 - MF_{O_2}}{MF_{O_2}} \right) \times F_h \right] \quad (10)$$

Where:

Variable	SI Unit	Description
n <sub>O<sub>2</sub>,h</sub>	kmol/kg residual gas	Quantity of moles O <sub>2</sub> in the exhaust gas of the flare per kg residual gas flared in hour h
t <sub>O<sub>2</sub>,h</sub>	-	Volumetric fraction of O <sub>2</sub> in the exhaust gas in the hour h
MF <sub>O<sub>2</sub></sub>	-	Volumetric fraction of O <sub>2</sub> in the air (0.21)
F <sub>h</sub>	kmol/kg residual gas	Stoichiometric quantity of moles of O <sub>2</sub> required for a complete oxidation of one kg residual gas in hour h
fm <sub>j,h</sub>	-	Mass fraction of element j in the residual gas in hour h (from equation 4)
AM <sub>j</sub>	kg/kmol	Atomic mass of element j
j		The elements carbon (index C) and nitrogen (index N)

$$F_h = \frac{fm_{C,h}}{AM_C} + \frac{fm_{H,h}}{4AM_H} - \frac{fm_{O,h}}{2AM_O} \quad (11)$$

Where:

Variable	SI Unit	Description
F <sub>h</sub>	kmol O <sub>2</sub> /kg residual gas	Stoichiometric quantity of moles of O <sub>2</sub> required for a complete oxidation of one kg residual gas in hour h
fm <sub>j,h</sub>	-	Mass fraction of element j in the residual gas in hour h (from equation 4)
AM <sub>j</sub>	kg/kmol	Atomic mass of element j
j		The elements carbon (index C), hydrogen (index H) and oxygen (index O)

**STEP 4. Determination of methane mass flow rate in the exhaust gas on a dry basis**

This step is only applicable if the methane combustion efficiency of the flare is continuously monitored.

The mass flow of methane in the exhaust gas is based on the volumetric flow of the exhaust gas and the measured concentration of methane in the exhaust gas, as follows:

(12)

$$TM_{FG,h} = \frac{TV_{n,FG,h} * fv_{CH4,FG,h}}{1000000}$$

Where:

Variable	SI Unit	Description
TM <sub>FG,h</sub>	kg/h	Mass flow rate of methane in the exhaust gas of the flare in dry basis at normal conditions in the hour <i>h</i>
TV <sub>n,FG,h</sub>	m <sup>3</sup> /h exhaust gas	Volumetric flow rate of the exhaust gas in dry basis at normal conditions in hour <i>h</i>
fv <sub>CH4,FG,h</sub>	mg/m <sup>3</sup>	Concentration of methane in the exhaust gas of the flare in dry basis at normal conditions in hour <i>h</i>

**STEP 5. Determination of methane mass flow rate in the residual gas on a dry basis**

The quantity of methane in the residual gas flowing into the flare is the product of the volumetric flow rate of the residual gas ( $FV_{RG,h}$ ), the volumetric fraction of methane in the residual gas ( $fv_{CH4,RG,h}$ ) and the density of methane ( $\rho_{CH4,n,h}$ ) in the same reference conditions (normal conditions and dry or wet basis).

It is necessary to refer both measurements (flow rate of the residual gas and volumetric fraction of methane in the residual gas) to the same reference condition that may be dry or wet basis. If the residual gas moisture is significant (temperature greater than 60°C), the measured flow rate of the residual gas that is usually referred to wet basis should be corrected to dry basis due to the fact that the measurement of methane is usually undertaken on a dry basis (i.e. water is removed before sample analysis).

$$TM_{RG,h} = FV_{RG,h} \times fv_{CH4,RG,h} \times \rho_{CH4,n} \quad (13)$$

Where:

Variable	SI Unit	Description
TM <sub>RG,h</sub>	kg/h	Mass flow rate of methane in the residual gas in the hour <i>h</i>
FV <sub>RG,h</sub>	m <sup>3</sup> /h	Volumetric flow rate of the residual gas in dry basis at normal conditions in hour <i>h</i>
fv <sub>CH4,RG,h</sub>	-	Volumetric fraction of methane in the residual gas on dry basis in hour <i>h</i> (NB: this corresponds to fv <sub>i,RG,h</sub> where <i>i</i> refers to methane).
$\rho_{CH4,n}$	kg/m <sup>3</sup>	Density of methane at normal conditions (0.716)



## STEP 6. Determination of the hourly flare efficiency

The determination of the hourly flare efficiency depends on the operation of flare (e.g. temperature), the type of flare used (open or enclosed) and, in case of enclosed flares, the approach selected by project participants to determine the flare efficiency (default value or continuous monitoring).

In case of **enclosed flares and continuous monitoring** of the flare efficiency, the flare efficiency in the hour  $h$  ( $\eta_{flare,h}$ ) is

- 0% if the temperature of the exhaust gas of the flare ( $T_{flare}$ ) is below 500 °C during more than 20 minutes during the hour  $h$ .
- determined as follows in cases where the temperature of the exhaust gas of the flare ( $T_{flare}$ ) is above 500 °C for more than 40 minutes during the hour  $h$  :

$$\eta_{flare,h} = 1 - \frac{TM_{FG,h}}{TM_{RG,h}} \quad (14)$$

Where:

Variable	SI Unit	Description
$\eta_{flare,h}$	-	Flare efficiency in the hour $h$
$TM_{FG,h}$	kg/h	Methane mass flow rate in exhaust gas averaged in a period of time $t$ (hour, two months or year)
$TM_{RG,h}$	kg/h	Mass flow rate of methane in the residual gas in the hour $h$

In case of **enclosed flares and use of the default value** for the flare efficiency, the flare efficiency in the hour  $h$  ( $\eta_{flare,h}$ ) is:

- 0% if the temperature in the exhaust gas of the flare ( $T_{flare}$ ) is below 500 °C for more than 20 minutes during the hour  $h$ .
- 50%, if the temperature in the exhaust gas of the flare ( $T_{flare}$ ) is above 500 °C for more than 40 minutes during the hour  $h$ , but the manufacturer's specifications on proper operation of the flare are not met at any point in time during the hour  $h$ .
- 90%, if the temperature in the exhaust gas of the flare ( $T_{flare}$ ) is above 500 °C for more than 40 minutes during the hour  $h$  and the manufacturer's specifications on proper operation of the flare are met continuously during the hour  $h$ .

In case of **open flares**, the flare efficiency in the hour  $h$  ( $\eta_{flare,h}$ ) is

- 0% if the flame is not detected for more than 20 minutes during the hour  $h$ .
- 50%, if the flare is detected for more than 20 minutes during the hour  $h$ .



### STEP 7. Calculation of annual project emissions from flaring

Project emissions from flaring are calculated as the sum of emissions from each hour  $h$ , based on the methane flow rate in the residual gas ( $TM_{RG,h}$ ) and the flare efficiency during each hour  $h$  ( $\eta_{flare,h}$ ), as follows:

$$PE_{flare,y} = \sum_{h=1}^{8760} TM_{RG,h} \times (1 - \eta_{flare,h}) \times \frac{GWP_{CH4}}{1000} \quad (15)$$

Where:

Variable	SI Unit	Description
PE <sub>flare,y</sub>	tCO <sub>2</sub> e	Project emissions from flaring of the residual gas stream in year $y$
TM <sub>RG,h</sub>	kg/h	Mass flow rate of methane in the residual gas in the hour $h$
$\eta_{flare,h}$	-	Flare efficiency in hour $h$
GWP <sub>CH4</sub>	tCO <sub>2</sub> e/tCH <sub>4</sub>	Global Warming Potential of methane valid for the commitment period

### Data and parameters not monitored

The only parameters and data that is not monitored are the constants used in equations, as listed in Table 1 below.

**Table 1. Constants used in equations**

Parameter	SI Unit	Description	Value
MM <sub>CH4</sub>	kg/kmol	Molecular mass of methane	16.04
MM <sub>CO</sub>	kg/kmol	Molecular mass of carbon monoxide	28.01
MM <sub>CO2</sub>	kg/kmol	Molecular mass of carbon dioxide	44.01
MM <sub>O2</sub>	kg/kmol	Molecular mass of oxygen	32.00
MM <sub>H2</sub>	kg/kmol	Molecular mass of hydrogen	2.02
MM <sub>N2</sub>	kg/kmol	Molecular mass of nitrogen	28.02
AM <sub>c</sub>	kg/kmol (g/mol)	Atomic mass of carbon	12.00
AM <sub>h</sub>	kg/kmol (g/mol)	Atomic mass of hydrogen	1.01
AM <sub>o</sub>	kg/kmol (g/mol)	Atomic mass of oxygen	16.00
AM <sub>n</sub>	kg/kmol (g/mol)	Atomic mass of nitrogen	14.01
P <sub>n</sub>	Pa	Atmospheric pressure at normal conditions	101 325
R <sub>u</sub>	Pa.m <sup>3</sup> /kmol.K	Universal ideal gas constant	8 314.472
T <sub>n</sub>	K	Temperature at normal conditions	273.15
MF <sub>O2</sub>	Dimensionless	O <sub>2</sub> volumetric fraction of air	0.21
GWP <sub>CH4</sub>	tCO <sub>2</sub> /tCH <sub>4</sub>	Global warming potential of methane	21
MV <sub>n</sub>	m <sup>3</sup> /Kmol	Volume of one mole of any ideal gas at normal	22.414



Parameter	SI Unit	Description	Value
		temperature and pressure	
$\rho_{CH_4,n}$	kg/m <sup>3</sup>	Density of methane gas at normal conditions	0.716
$NA_{ij}$	Dimensionless	Number of atoms of element j in component i, depending on molecular structure	

### III. MONITORING METHODOLOGY PROCEDURE

#### Data and parameters to be monitored

All monitored data must be linked in time, i.e. calculations shall be performed considering only a set of data acquired in the same time interval in case of continuous monitoring. As noted above, project participants may use one hour or a smaller discrete time interval.

<b>Data / Parameter:</b>	$fv_{i,h}$
Data unit:	-
Description:	Volumetric fraction of component $i$ in the residual gas in the hour $h$ where $i = CH_4, CO, CO_2, O_2, H_2, N_2$
Source of data:	Measurements by project participants using a continuous gas analyser
Measurement procedures:	Ensure that the same basis (dry or wet) is considered for this measurement and the measurement of the volumetric flow rate of the residual gas ( $FV_{RG,h}$ ) when the residual gas temperature exceeds 60 °C
Monitoring frequency:	Continuously. Values to be averaged hourly or at a shorter time interval
QA/QC procedures	Analysers must be periodically calibrated according to the manufacturer's recommendation. A zero check and a typical value check should be performed by comparison with a standard certified gas.
Any comment:	As a simplified approach, project participants may only measure the methane content of the residual gas and consider the remaining part as $N_2$ .

<b>Data / Parameter:</b>	$FV_{RG,h}$
Data unit:	m <sup>3</sup> /h
Description:	Volumetric flow rate of the residual gas in dry basis at normal conditions in the hour $h$
Source of data:	Measurements by project participants using a flow meter
Measurement procedures:	Ensure that the same basis (dry or wet) is considered for this measurement and the measurement of volumetric fraction of all components in the residual gas ( $fv_{i,h}$ ) when the residual gas temperature exceeds 60 °C
Monitoring frequency:	Continuously. Values to be averaged hourly or at a shorter time interval
QA/QC procedures	Flow meters are to be periodically calibrated according to the manufacturer's recommendation.
Any comment:	



<b>Data / Parameter:</b>	$t_{O_2,h}$
Data unit:	-
Description:	Volumetric fraction of O <sub>2</sub> in the exhaust gas of the flare in the hour <i>h</i>
Source of data:	Measurements by project participants using a continuous gas analyser
Measurement procedures:	Extractive sampling analysers with water and particulates removal devices or in situ analysers for wet basis determination. The point of measurement (sampling point) shall be in the upper section of the flare (80% of total flare height). Sampling shall be conducted with appropriate sampling probes adequate to high temperatures level (e.g. inconel probes). An excessively high temperature at the sampling point (above 700 °C) may be an indication that the flare is not being adequately operated or that its capacity is not adequate to the actual flow.
Monitoring frequency:	Continuously. Values to be averaged hourly or at a shorter time interval
QA/QC procedures	Analysers must be periodically calibrated according to the manufacturer's recommendation. A zero check and a typical value check should be performed by comparison with a standard gas.
Any comment:	Monitoring of this parameter is only applicable in case of enclosed flares and continuous monitoring of the flare efficiency.

<b>Data / Parameter:</b>	$f_{v,CH_4,FG,h}$
Data unit:	mg/m <sup>3</sup>
Description:	Concentration of methane in the exhaust gas of the flare in dry basis at normal conditions in the hour <i>h</i>
Source of data:	Measurements by project participants using a continuous gas analyser
Measurement procedures:	Extractive sampling analysers with water and particulates removal devices or in situ analyser for wet basis determination. The point of measurement (sampling point) shall be in the upper section of the flare (80% of total flare height). Sampling shall be conducted with appropriate sampling probes adequate to high temperatures level (e.g. inconel probes). An excessively high temperature at the sampling point (above 700 °C) may be an indication that the flare is not being adequately operated or that its capacity is not adequate to the actual flow.
Monitoring frequency:	Continuously. Values to be averaged hourly or at a shorter time interval
QA/QC procedures	Analysers must be periodically calibrated according to manufacturer's recommendation. A zero check and a typical value check should be performed by comparison with a standard gas.
Any comment:	Monitoring of this parameter is only applicable in case of enclosed flares and continuous monitoring of the flare efficiency. Measurement instruments may read ppmv or % values. To convert from ppmv to mg/m <sup>3</sup> simply multiply by 0.716. 1% equals 10 000 ppmv.



<b>Data / Parameter:</b>	T <sub>flare</sub>
Data unit:	°C
Description:	Temperature in the exhaust gas of the flare
Source of data:	Measurements by project participants
Measurement procedures:	Measure the temperature of the exhaust gas stream in the flare by a Type N thermocouple. A temperature above 500 °C indicates that a significant amount of gases are still being burnt and that the flare is operating.
Monitoring frequency:	Continuously.
QA/QC procedures	Thermocouples should be replaced or calibrated every year.
Any comment:	An excessively high temperature at the sampling point (above 700 °C) may be an indication that the flare is not being adequately operated or that its capacity is not adequate to the actual flow.

<b>Data / Parameter:</b>	<b>Other flare operation parameters</b>
Data unit:	-
Description:	This should include all data and parameters that are required to monitor whether the flare operates within the range of operating conditions according to the manufacturer's specifications including a flame detector in case of open flares.
Source of data:	Measurements by project participants
Measurement procedures:	
Monitoring frequency:	Continuously
QA/QC procedures	
Any comment:	Only applicable in case of use of a default value

#### IV. REFERENCES

Fundamentals of Classical Thermodynamics; Gordon J. Van Wylen, Richard E. Sonntag and Claus Borgnakke; 4<sup>o</sup> Edition, 1994, John Wiley & Sons, Inc.