

Vortex ring models for studying the fuel injection and computations with FreeFem++

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Third Workshop on Freefem++, Paris, December 5-7, 2011.

Outline

- 1 Vortex Rings in Automotive Engines
 - Experimental Investigation of Vortex Rings
 - Mathematical Problem
- 2 Mathematical Modeling
 - Modeling as an Optimal Control Type Problem
 - Variational Problems & Discretization
 - Algorithm
- 3 Numerical Tests
- 4 Conclusion and Future Work

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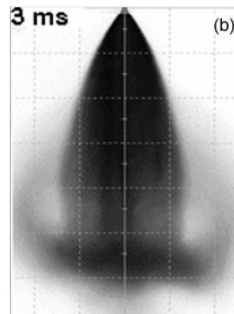
Vortex structures in internal combustion engines

A vortex ring forms ahead of the injected fuel spray.

- New types of gasoline injectors
- Diesel injectors



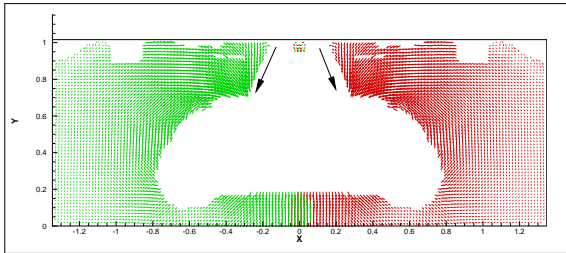
(courtesy of Continental Automotive)



(courtesy of IFP)

Measurements in An Automotive Engine

- Experimental measurements of spray flows by **PIV (Particle Image Velocimetry)** offer a low resolution in the vortex ring region because of high fuel droplet concentration.
- The missing information needs to be reconstructed.



(courtesy of Continental Automotive)

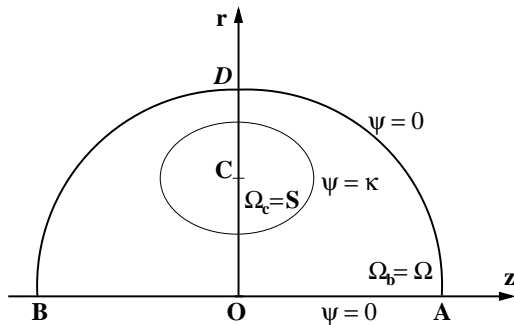
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Mathematical Description of the Problem

- Vortex rings in an elliptic domain $\Omega (\supset \Omega_c = \{x : \psi(x) \geq \kappa\})$

$$\mathcal{L}\psi = - \left(\frac{\partial}{\partial z} \left(\frac{1}{r} \frac{\partial \psi}{\partial z} \right) + \frac{\partial}{\partial r} \left(\frac{1}{r} \frac{\partial \psi}{\partial r} \right) \right) = \begin{cases} rf(\psi), & \text{if } \psi \geq \kappa \\ 0, & \text{otherwise} \end{cases}$$



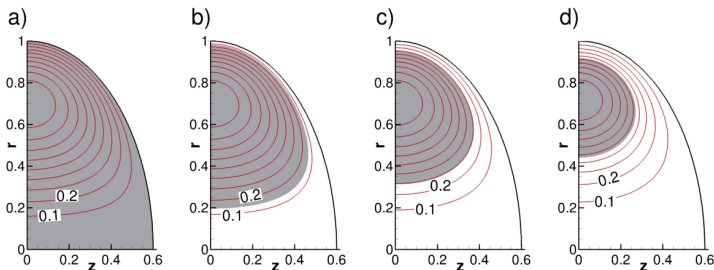
ψ stream function,
 κ constant,
 $f(\psi)$ arbitrary function
 $rf(\psi)$ vorticity
 distribution.

Vortex ring models

Formulations for $rf(\psi)$ (vorticity distribution) :

- Discontinuous form: $f(\psi) := C\chi_{\Omega_c} = C\{\psi \geq k\}$.
- Parameterized 2D Gaussian form: $F(x, \psi, \Theta, X)$
(Θ = magnitude, X = undetermined parameter set).

Multiple solutions for discontinuous vorticity (different C and k)



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Optimal Control Problem (1)

- Minimization problem in the (reconstruction) domain Ω_R

$$\text{Min}_X J(\psi) = \int_{\partial\Omega_R} \left| \frac{1}{r} \left(\frac{\partial\psi}{\partial\vec{n}} - \frac{\partial\psi_{\text{exp}}}{\partial\vec{n}} \right) \right|^2 dS \quad (1)$$

subject to

$$\begin{cases} \mathcal{L}\psi = F(x, \psi, \Theta, X), & \text{in } \Omega_R, \\ \psi = \psi_{\text{exp}}, & \text{on } \partial\Omega_R. \end{cases} \quad (2)$$

\vec{n} is the unit outer normal vector of $\partial\Omega_R$,
 ψ_{exp} is provided by experimental results.

Optimal Control Problem (2)

- Explanation of the cost function $J(\psi)$:
 Minimizing $J(\psi)$ indicates that the first order derivatives of ψ and ψ_{exp} should match (with a fixed error bound) on the boundary $\partial\Omega_R$.
- Supplementary constraint: conserve the circulation Γ_{exp}

$$\Gamma_{\text{exp}} = \int_{\partial\Omega_R} \frac{1}{r} \frac{\partial\psi_{\text{exp}}}{\partial\vec{n}} dS, \quad (3)$$

This allows to compute the magnitude Θ from

$$\Gamma_{\text{exp}} = \int_{\partial\Omega_R} F(x, \psi, \Theta, X) dx = \Theta \int_{\partial\Omega_R} F'(x, \psi, X) dx. \quad (4)$$

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Variational Problems

- Functional space

$$H_0(\Omega) = \left\{ u \in L^2(\Omega) : \frac{1}{r} |\nabla u|^2 \in L^1(\Omega) \mid u = 0 \text{ on } \Gamma = \partial\Omega \right\}. \quad (5)$$

- Inner product ($\forall u \in H_0(\Omega), v \in H_0(\Omega)$)

$$\langle u, v \rangle = \int_{\Omega} \frac{1}{r} \nabla u \nabla v \, dx = \int_{\Omega} v \mathcal{L} u \, dx. \quad (6)$$

- Variational form

$$\begin{cases} \text{Find: } \psi \in H_0(\Omega) \text{ such that} \\ \langle \psi, \phi \rangle = (F(x, \psi, \Theta, X), \phi), \quad \forall \phi \in H_0(\Omega). \end{cases} \quad (7)$$

Discretization

- Variational derivatives of $J(\cdot)$ ($X_i \in X$)

$$\frac{\delta J}{\delta X_i} = \frac{\delta J}{\delta \psi} \frac{\delta \psi}{\delta X_i} = 2 \int_{\partial \Omega_R} \frac{1}{r^2} \left(\frac{\partial \psi}{\partial \vec{n}} - \frac{\partial \psi_{\text{exp}}}{\partial \vec{n}} \right) \frac{\partial}{\partial \vec{n}} \left(\frac{\delta \psi}{\delta X_i} \right) dS \quad (8)$$

- Calculations of $\delta \psi / \delta X_i$

$$\begin{cases} \mathcal{L} \left(\frac{\delta \psi}{\delta X_i} \right) = \frac{\delta F(x, \psi, \Theta, X)}{\delta X_i}, & \text{in } \Omega_R, \\ \frac{\delta \psi}{\delta X_i} = 0, & \text{on } \partial \Omega_R. \end{cases} \quad (9)$$

The vanishing of $\delta \psi / \delta X_i$ on $\partial \Omega_R$ is natural for $\Omega_R \supset \Omega_c$.

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Particular formulation of the reconstruction problem

Gaussian vorticity distribution

- Minimization problem

$$\text{Min}_{\alpha, Rc, Zc} J(\psi) = \int_{\partial\Omega_R} \left| \frac{1}{r} \left(\frac{\partial\psi}{\partial\vec{n}} - \frac{\partial\psi_{\text{exp}}}{\partial\vec{n}} \right) \right|^2 dS \quad (10)$$

subject to:

$$\begin{cases} \mathcal{L}\psi = f(\Theta, X), & \text{in } \Omega_R, \\ \psi = \psi_{\text{exp}}, & \text{on } \partial\Omega_R. \end{cases} \quad (11)$$

where $f(\Theta, X) = \Theta \cdot \exp \left[-\alpha^2 \left((r - Rc)^2 + (z - Zc)^2 \right) \right]$.

Algorithm based on the quasi-Newton BFGS method

- 1 Set the initial guess $X^{(0)} = \{\alpha^{(0)}, R_c^{(0)}, Z_c^{(0)}\}$.
 Initialize tolerances eps_J , eps_X and the max iteration steps N .
- 2 Using the experimental data on $\partial\Omega_R$, calculate Γ_{exp} and get $\Theta^{(n)}$ by the following formula

$$\Gamma = \Gamma_{\text{exp}}$$

$$\Gamma = \int_{\Omega_R} \Theta^{(n)} \cdot \text{exp} \left[-\alpha^2 \left((r - R_c^{(n)})^2 + (z - Z_c^{(n)})^2 \right) \right] dz dr.$$

$$\Gamma_{\text{exp}} = \int_{\partial\Omega_R} \frac{1}{r} \nabla \psi_{\text{exp}} \cdot \vec{n} dS.$$

- 3 Solve $\mathcal{L}\psi = f(\Theta, X)$ and obtain $\psi^{(n)}$.

Algorithm based on the quasi-Newton BFGS method

- 4 Get $\nabla J(\psi^{(n)})$ by the following equation

$$\nabla_{\psi} J \cdot \delta\psi^{(n)} = 2 \cdot \int_{\partial\Omega_R} \frac{1}{r^2} \left(\frac{\partial\psi^{(n)}}{\partial \vec{n}} - \frac{\partial\psi_{\text{exp}}}{\partial \vec{n}} \right) \cdot \frac{\partial(\delta\psi^{(n)})}{\partial \vec{n}} dz dr. \quad (12)$$

From Eq. (11), we have

$$\mathcal{L} \left(\frac{\partial\psi^{(n)}}{\partial X_i} \right) = \left. \frac{\partial f(\Omega^{(n)}, X)}{\partial X_i} \right|_{X=X^{(n)}} \cdot \left. \frac{\partial\psi^{(n)}}{\partial X_i} \right|_{\partial\Omega_R} = 0. \quad (13)$$

Then, $\nabla_X J(\psi^{(n)})$ is calculated by Eq. (12)

$$\nabla_X J(\psi^{(n)}) = \left\{ \nabla_{\psi} J \cdot \left(\frac{\partial\psi^{(n)}}{\partial X_i} \right) \right\}_{i=0, \dots, 2}. \quad (14)$$

Algorithm based on the quasi-Newton BFGS method

- 5 Calculate maximum acceptable Euclidean norm of the gradient $\|\nabla_X J(\psi^n)\|$. If $\|\nabla_X J(\psi^n)\| \leq \text{eps}_J$, the iteration is terminated. Otherwise, go to Step 6.
- 6 From Hessian matrix $H(\psi^{(n)})$ obtained by BFGS

$$\nabla_X J(\psi^{(n+1)}) \approx \nabla_X J(\psi^{(n)}) + H(\psi^{(n)}) \cdot \delta X^{(n+1)}. \quad (15)$$

$$\delta X^{*,(n)} = -H^{-1}(\psi^{(n)}) \cdot \nabla_X J(\psi^{(n)}). \quad (16)$$

Update $X^{(n+1)}$ by

$$X^{(n+1)} = X^{(n)} + \beta^{(n)} \delta X^{*,(n)}, \quad (17)$$

where $\beta^{(n)}$ is an acceptable step size in the direction $\delta X^{*,(n)}$.

Algorithm based on the quasi-Newton BFGS method

- 7 If $\|X^{(n+1)} - X^{(n)}\| / \|X^{(n)}\| \leq \text{eps}_X$ or $n + 1 > N$, the iteration is terminated. Otherwise, go to Step 2.

For current computation tests, $\text{eps}_J = \text{eps}_X = 10^{-6}$ and $N = 50$.

Remark on Step 2

The parameter Θ appears as an extra constraint to guarantee the existence of the vortex core and the consistency of the circulation.

Basic quantities

- The reconstruction domain has an elliptic shape.
 R_c and Z_c are initialized by the center coordinates of the computational domain.
 α is set as the half-length inverse of semi-minor axis.

Table: Comparison between the fitting/reconstructed results and the DNS results. K-R: Kaplanski-Rudi.

Methods	Γ	I	E	R_c	Z_c
NSEs	1.17592	1.33698	0.216944	0.66194	3.51000
K-R	1.12217	1.29092	0.224925	0.71384	3.51000
C- κ	1.17488	1.55884	0.217152	0.71384	3.49190
Recon.	1.17592	1.73646	0.175927	0.65307	3.50953

Streamline figures

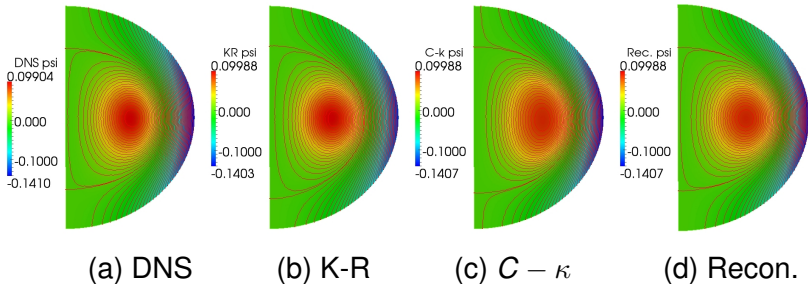


Figure: Stream function contours: comparison between different vortex ring models, the reconstructed method and DNS data.

Streamline profiles along $z = Z_c$

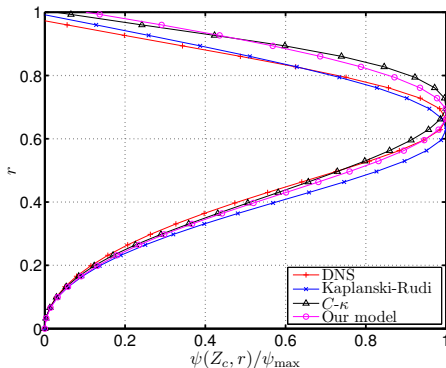


Figure: The profiles of ψ along the line $z = Z_c$ and $r \in (0, 1)$.

Conclusion

- FreeFem++ is a powerful tool to handle this problem.
- The missing information can be reconstructed easily in FreeFem++.
- The reconstruction can provide the necessary vortex ring information for practical/engineering studies of fuel injectors.

Future Work with FreeFem++

- Validate our novel numerical scheme of Navier-Stokes equations and theoretical analysis.
- Implement a time-dependent two-phase flow model .

Thanks for your attention.