

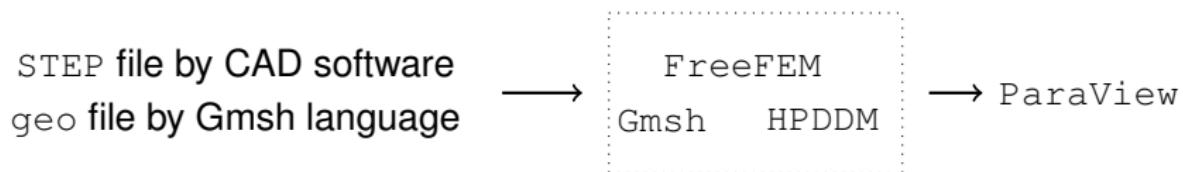
An industrial application of a free boundary problem with contact angle and volume constraint

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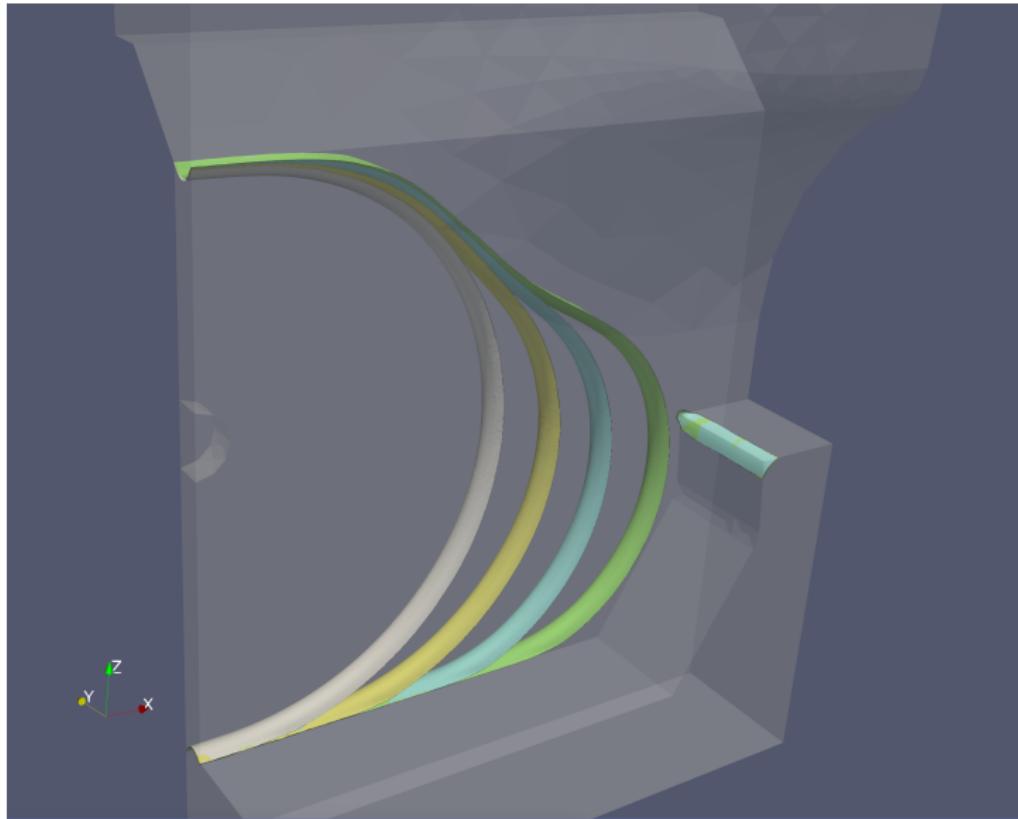
Joint work with DENSO to simulate a free boundary porblem

- ▶ aiming to replace COMSOL FEM analysis by FreeFEM
- ▶ more sophisticated numerical scheme than COMSOL
- ▶ pseudo time marching for gradient flow + stationary Newton iteration with 1.0~ 2.0 million unknowns on distributed parallel architecture
- ▶ volume conservation is treated within linear solver
- ▶ realistic computational geometry given by CAD software



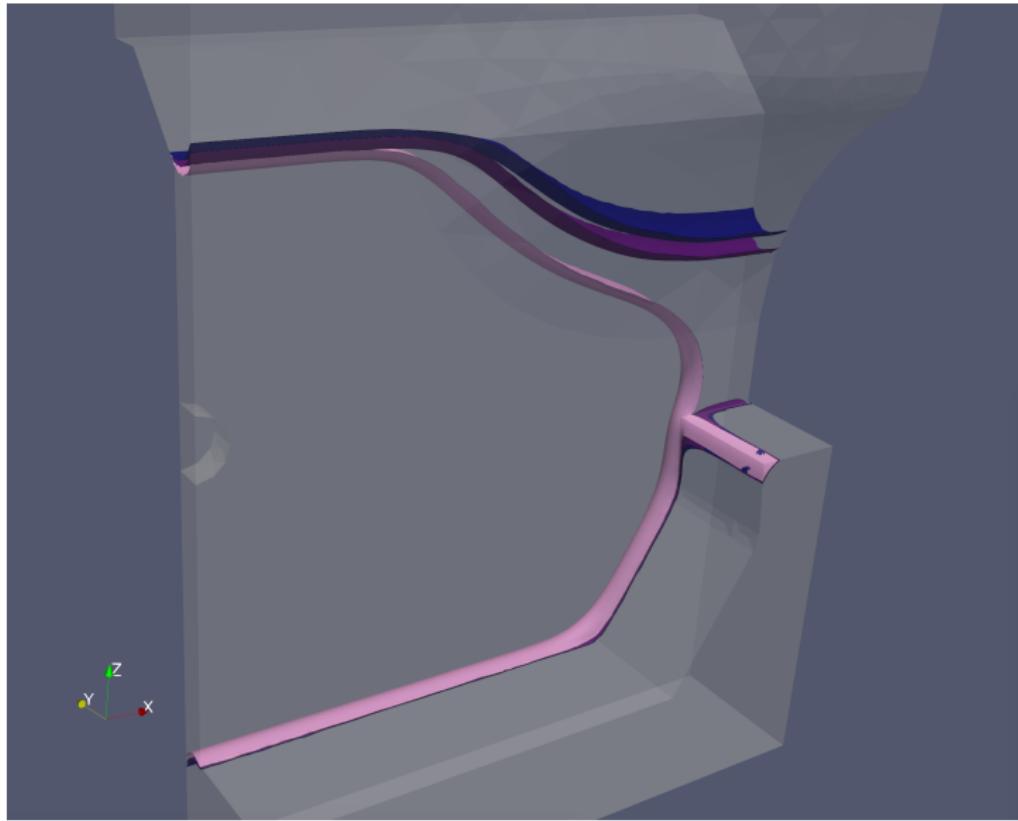
FreeFEM + Gmsh + HPPDM + $\alpha \gg$ COMSOL

computation of a model with $\theta = 30$



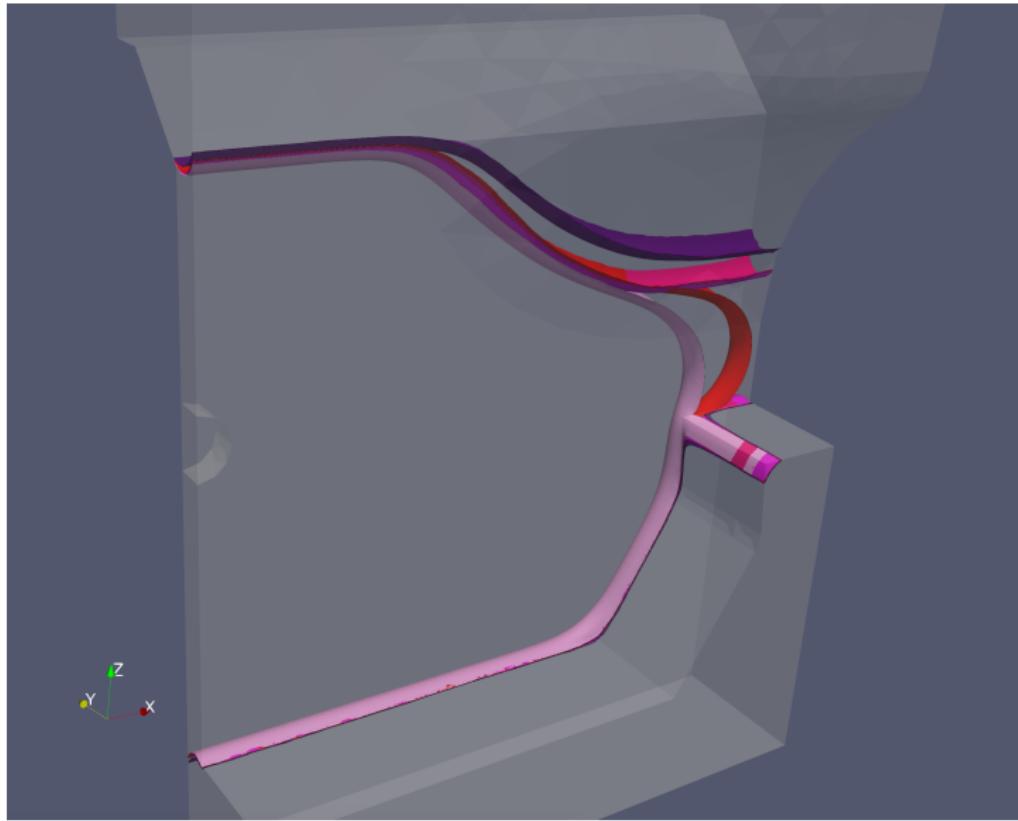
- ▶ liquid part is not yet reached to the other side but with leaking

computation of a model with $\theta = 30$



- ▶ liquid part has been reached to the other side with leaking

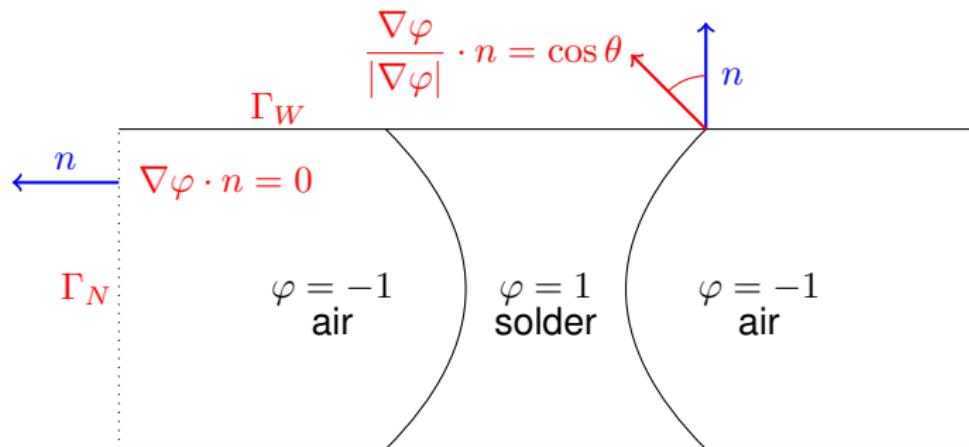
computation of a model with $\theta = 30$



- ▶ volume of the liquid part with filling has calculated by bisection

solder filling problem with contact angle

- indicator function : φ , solder : $\varphi = 1$, air : $\varphi = -1$.
- contact angle : $\frac{\nabla \varphi}{|\nabla \varphi|} \cdot n = \cos \theta$ on Γ_W
- volume conservation : $\int_{\Omega} \frac{\varphi + 1}{2} = V_0$
- free energy : $J(\varphi) := \frac{1}{2} \int_{\Omega} \kappa |\nabla \varphi|^2 + (\varphi + 1)^2(\varphi - 1)^2$ with $\kappa > 0$



variational setting : 1/3

set for solution embed. with boundary condi. and volume constraint

$$W(c, \cos \theta) := \left\{ \varphi \in H^{3/2}(\Omega); \int_{\Omega} \varphi = c, \frac{\nabla \varphi}{|\nabla \varphi|} \cdot n = \cos \theta \text{ on } \Gamma_W, \right. \\ \left. \nabla \varphi \cdot n = 0 \text{ on } \Gamma_N \right\}.$$

$$\partial\Omega = \Gamma_W \cup \Gamma_N.$$

functional $J: \Omega \rightarrow \mathbb{R}$ with $\kappa > 0$,

$$J(\varphi) := \frac{1}{2} \int_{\Omega} \kappa |\nabla \varphi|^2 + (\varphi + 1)^2(\varphi - 1)^2.$$

minimization of the energy

$$\varphi \in W(c, \cos \theta) \quad J(\varphi) \leq J(\psi) \quad \forall \psi \in W(c, \cos \theta).$$

variation of the energy

$$\varphi \in W(c, \cos \theta), \delta \varphi \in W(0, 0) \Rightarrow \varphi + \delta \varphi \in W(c, \cos \theta)$$

$$J(\varphi + \delta \varphi) - J(\varphi) = \int_{\Omega} \kappa \nabla \varphi \cdot \nabla \delta \varphi + 2\varphi(\varphi^2 - 1)\delta \varphi + O(|\delta \varphi|^2).$$

suppose that an extremal attains the minimum of the energy

variational setting : 2/3

$$\forall \delta\varphi \in W(0,0)$$

$$\begin{aligned} 0 &= \int_{\Omega} \kappa \nabla \varphi \cdot \nabla \delta\varphi + 2\varphi(\varphi^2 - 1)\delta\varphi \\ &= \int_{\Omega} -\nabla \cdot \kappa \nabla \varphi \delta\varphi + \int_{\Gamma_W \cup \Gamma_N} \kappa \nabla \varphi \cdot n \delta\varphi + 2 \int_{\Omega} \varphi(\varphi^2 - 1)\delta\varphi, \end{aligned}$$

by taking $\delta\varphi \in W(0,0) \cap H_0^1(\Omega)$

$$-\nabla \cdot \kappa \nabla \varphi + 2\varphi(\varphi^2 - 1) = 0 \quad \text{in } \Omega$$

definition of $W(c, \cos \theta)$ implies boundary conditions and volume constraint

$$\nabla \varphi \cdot n = |\nabla \varphi| \cos \theta \qquad \qquad \text{on } \Gamma_W,$$

$$\nabla \varphi \cdot n = 0 \qquad \qquad \qquad \text{on } \Gamma_N,$$

$$\int_{\Omega} \varphi = c.$$

variational setting : 3/3

affine space with volume constraint

$$V(c) := \left\{ \varphi \in H^1(\Omega) ; \int_{\Omega} \varphi = c \right\}.$$

$$(F(\varphi), \psi) := \int_{\Omega} \kappa \nabla \varphi \cdot \nabla \psi + \int_{\Omega} 2\varphi(\varphi^2 - 1)\psi - \int_{\Gamma_W} \kappa |\nabla \varphi| \cos \theta \psi$$

$$\psi \in H_{00}^{1/2}(\Gamma_W), \nabla \varphi \in H^{-1/2}(\Gamma_W)^3$$

nonlinear stationary problem

$$\text{find } \varphi \in V(c) \quad (F(\varphi), \psi) = 0 \quad \forall \psi \in V(0).$$

solved by Newton iteration

differential calculus

$$\varphi \in V(c), \delta \varphi, \psi \in V(0)$$

$$(F'(\varphi) \delta \varphi, \psi) = \int_{\Omega} \kappa \nabla \delta \varphi \cdot \nabla \psi + \int_{\Omega} (6\varphi^2 - 2) \delta \varphi \psi - \int_{\Gamma_W} \kappa \frac{\nabla \varphi \cdot \nabla \delta \varphi}{|\nabla \varphi|} \cos \theta \psi.$$

non-linear solver

Newton iteration

$\varphi^0 \in V(0)$: initial guess

loop $k = 0, 1, 2, \dots$

find $\delta\varphi \in V(0)$

$$(F'(\varphi^k)\delta\varphi, \psi) = (F(\varphi^k), \psi) \quad \forall \psi \in V(0)$$

$$\varphi^{k+1} := \varphi^k - \delta\varphi$$

find $\delta\varphi \in V(0)$

$$\begin{aligned} & \int_{\Omega} \kappa \nabla \delta\varphi \cdot \nabla \psi - 2 \int_{\Omega} \delta\varphi \psi + 6 \int_{\Omega} (\varphi^k)^2 \delta\varphi \psi - \int_{\Gamma_W} \kappa \frac{\nabla \varphi^k \cdot \nabla \delta\varphi}{|\nabla \varphi^k|} \cos \theta \psi \\ &= \int_{\Omega} \kappa \nabla \varphi^k \cdot \nabla \psi + \int_{\Omega} 2\varphi^k ((\varphi^k)^2 - 1) \psi - \int_{\Gamma_W} \kappa |\nabla \varphi^k| \cos \theta \psi \end{aligned} \quad \forall \psi \in V(0)$$

- ▶ P2 finite element approximation to compute $\nabla \varphi^k$
- ▶ Newton iteration needs to start from an appropriate initial guess
gradient flow solution with pseudo time marching
- ▶ $V(0) := \{\varphi \in H^1(\Omega); \int_{\Omega} \varphi = 0\}$: how to implement?

a way to find good initial guess for Newton iteration

gradient flow solution

an initial condition $\varphi(\tau)|_{\tau=0} = \varphi_0 \in V(c)$. $\frac{\partial \varphi}{\partial \tau} \rightarrow 0$ as $\tau \rightarrow +\infty$

$$\int_{\Omega} \frac{\partial \varphi}{\partial \tau} \psi = -(F(\varphi), \psi)$$

Crank-Nicolson scheme with $n + \frac{1}{2}$ -time step, $\varphi^{n+\frac{1}{2}} = \frac{\varphi^{n+1} + \varphi^n}{2}$,

$$\int_{\Omega} \frac{\varphi^{n+1} - \varphi^n}{\Delta \tau} \psi = -(F(\varphi^{n+\frac{1}{2}}), \psi)$$

Newton iteration at k -step with $\varphi_k^{n+\frac{1}{2}} = \frac{\varphi_k^{n+1} + \varphi^n}{2}$.

$$(F_{\text{CN}}(\varphi_k^{n+1}, \varphi^n), \psi) = \int_{\Omega} \frac{\varphi_k^{n+1} - \varphi^n}{\Delta \tau} \psi + (F(\varphi_k^{n+\frac{1}{2}}), \psi)$$

$$\begin{aligned} (F'_{\text{CN}}(\varphi_k^{n+1}, \varphi^n) \delta \varphi, \psi) &= \int_{\Omega} \frac{\delta \varphi}{\Delta \tau} + \frac{1}{2} \int_{\Omega} \kappa \nabla \delta \varphi \cdot \nabla \psi - \int_{\Omega} \delta \varphi \psi \\ &\quad + 3 \int_{\Omega} (\varphi_k^{n+\frac{1}{2}})^2 \delta \varphi \psi - \frac{1}{2} \int_{\Gamma_W} \kappa \frac{\nabla \varphi_k^{n+\frac{1}{2}} \cdot \nabla \delta \varphi}{|\nabla \varphi_k^{n+\frac{1}{2}}|} \cos \theta \psi \end{aligned}$$

linear solver with constraint

Linear solver with Lagrange multiplier $\int_{\Omega} \varphi = c \Leftrightarrow \vec{m}^T \vec{\varphi} = c$
indefinite system (KKT type) : harder to solve even with coercive A

$$\begin{bmatrix} A & \vec{m} \\ \vec{m}^T & 0 \end{bmatrix} \begin{bmatrix} \vec{\varphi} \\ \lambda \end{bmatrix} = \begin{bmatrix} \vec{f} \\ c \end{bmatrix}.$$

block factorization with Schur complement $s = -\vec{m}^T A^{-1} \vec{m}$

$$\begin{bmatrix} A & 0 \\ \vec{m}^T & s \end{bmatrix} \begin{bmatrix} I & A^{-1} \vec{m} \\ 0 & 1 \end{bmatrix} \begin{bmatrix} \vec{\varphi} \\ \lambda \end{bmatrix} = \begin{bmatrix} \vec{f} \\ c \end{bmatrix}.$$

two linear solution with coercive (positive) matrix A

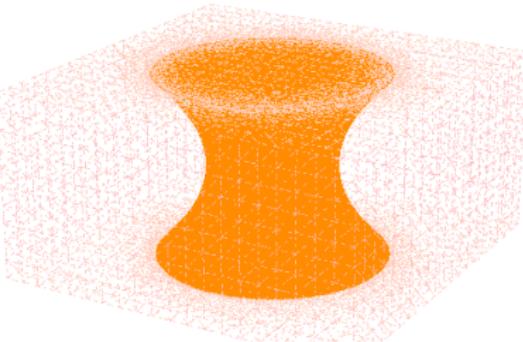
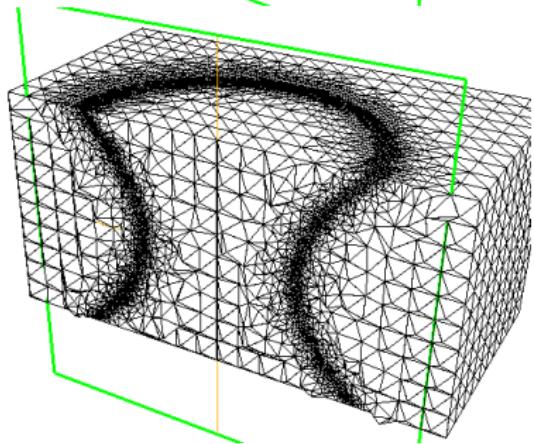
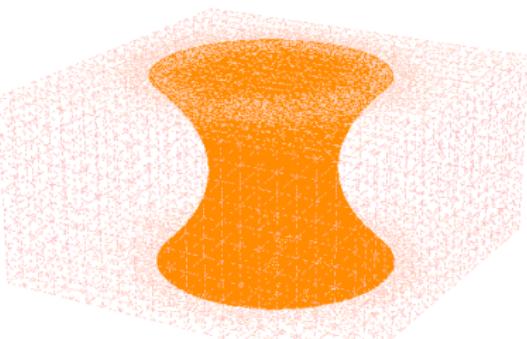
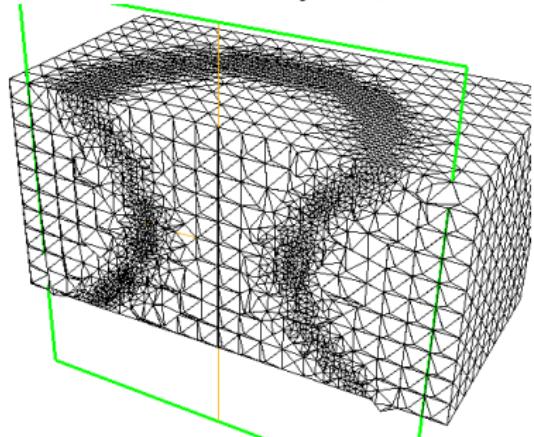
- ▶ solve \vec{w} : $A\vec{w} = \vec{m}$
- ▶ $s = -\vec{m}^T \vec{w}$
- ▶ solve $\vec{\varphi}$: $A\vec{\varphi} = \vec{f}$
- ▶ solve λ : $s\lambda = c - \vec{m}^T \vec{\varphi}$
- ▶ $\vec{\varphi} = \vec{\varphi} - \lambda \vec{w}$

question : A is coercive, $(A + A^T)/2 > 0$?

... seems to be ok with good initial guess of Newton iteration

An algorithm to find extremal with mesh refinement : 2/2

mesh refinement by mmg3d



computational efficiency with FreeFEM

performance of an academic problem

level	# unknowns	refinement parameter
0	35,301	uniform mesh $20 \times 20 \times 10$, $h = 0.1$
1	461,573	$ \varphi < 0.6 : h/4$, $ \varphi < 0.9 : h/2$
2	1,693,049	$ \varphi < 0.3 : h/8$, $ \varphi < 0.6 : h/4$, $ \varphi < 0.9 : h/2$
3	1,781,054	$ \varphi < 0.3 : h/8$, $ \varphi < 0.6 : h/4$, $ \varphi < 0.9 : h/2$
4	1,792,096	$ \varphi < 0.3 : h/8$, $ \varphi < 0.6 : h/4$, $ \varphi < 0.9 : h/2$

level	# unknowns	# Newton	PARDISO	additive Schwarz	AMG
0	35,301	7	12.048	10.937	8.198
1	461,573	8	320.845	271.790	347.003
2	1,693,049	5	1,107.044	919.195	703.402
3	1,781,054	4	996.045	802.735	602.678
4	1,792,096	4	1,024.829	807.679	615.471
total (sec.)			3,510.67	2,919.68	2,352.85

Intel Core i7-6770HQ CPU @ 2.60GHz 4 cores

performance of actual geometry

package	hpddm	hypre
preconditioner	additive Schwarz	AMG
# iteration	12	116
time (sec.)	4.848	17.199

Computation of Euler characteristic : 1/2

stripe shape of the interface between solid and liquid part



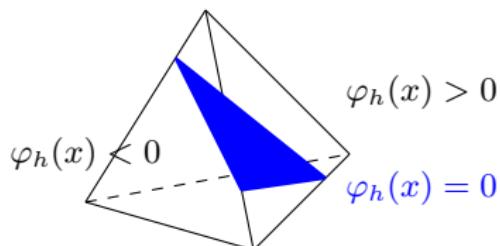
Vertex = 4

Edge = 4

Face = 1

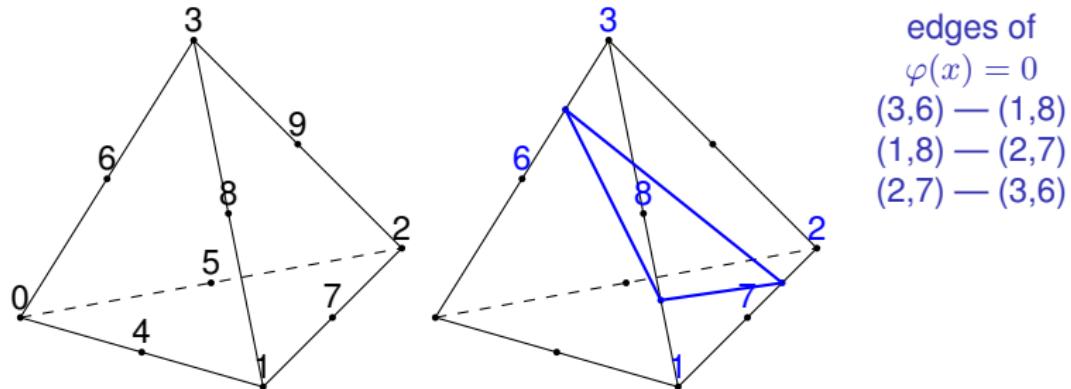
$$V - E + F = 4 - 4 + 1 = 1$$

indicator function $\varphi_h(x)$ by P2



element-wise detection of zero
iso-surface approximated by P1

Computation of Euler characteristic : 2/2



- ▶ perturbe $\varphi(P_k) = 0$ ($0 \leq k < 10$) with $\varepsilon > 0$ to avoid zero surface passing on P2 nodes
- ▶ edge of triangle of zero surface $\varphi = 0$ is shared with other elements
- ▶ presence of edge of the surface triangle is registered as an entry of CSR sparse matrix

implementation	time (sec.)	core
FreeFEM script	248.85	1
FreeFEM script	196.23	6 : parallel only over elements
C++ dynamic loading	2.15	1

in C++ implementation CSR matrix is managed by STL list

C++ coding to extend FreEFEM with dynamic loading : 1/2

function to compute Euler characteristic and number of liquid/sold domain

```
checkconnectivity(mesh3 Th3, real[int] &gg, int[int] &ivars)
```

FreeFEM script C++ function

input	mesh3 Th3	atype<Mesh3 *>
	real[int] &gg	atype<KN<double> *>
output	int[int] &ivars	atype<KN<long> *>

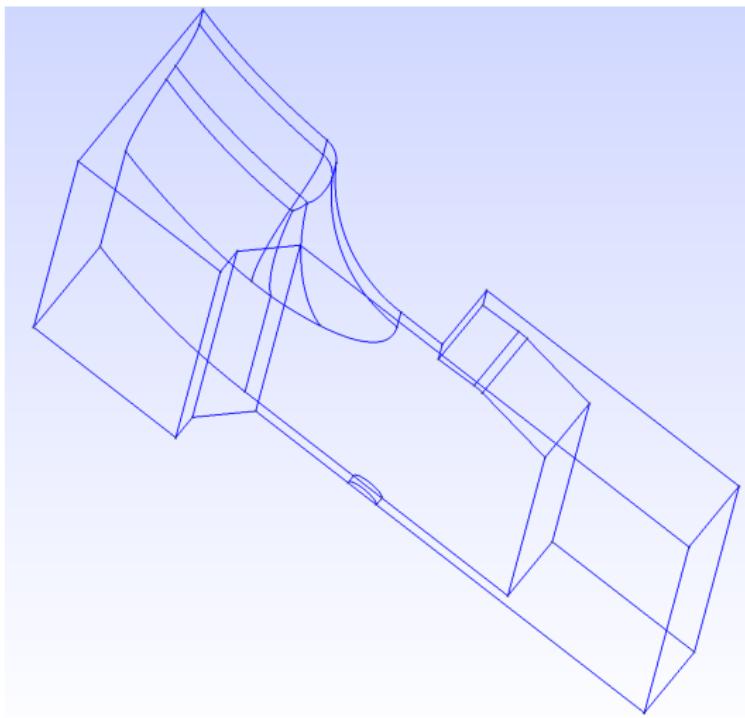
FreeFEM script : cf. 6.14 Finite elemens connectivity

```
mesh3 Th;
fespace Vh(Th, P2);
for (int k = 0; k < Vh.nt; k++) {
    for (int j = 4; j < 10; j++) { // running middle nodes of P2
        int ii = Vh(k, j);
```

C++ implementation : cf. femlib/FESpace.hpp

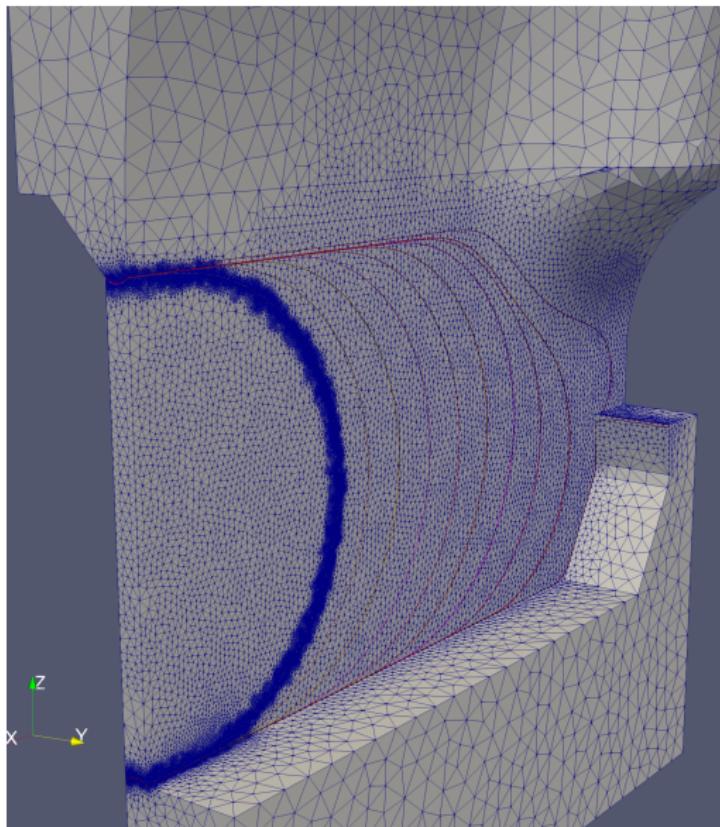
```
Mesh3 *pTh;
FESpace3 *pVh = new FESpace3(*pTh, DataFE<Mesh3>::P2);
FESpace3 &Vh = *pVh;
for (int k = 0; k < Vh.NbOfElements; k++) {
    for (int j = 4; j < 10; j++) { // running middle nodes of P2
        int ii = Vh(k, j);
```

STEP file that is directly read by Gmsh



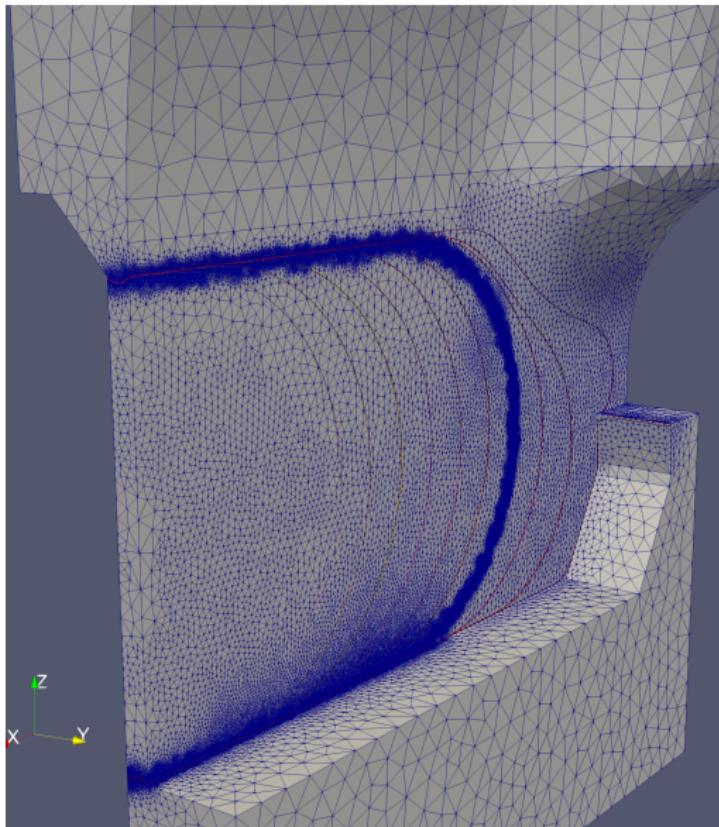
- ▶ using OpenCASCADE geometry engine
- ▶ setting of boundary conditions with geo file which includes STEP file

numerical result by dynamic refinement strategy : 1/5



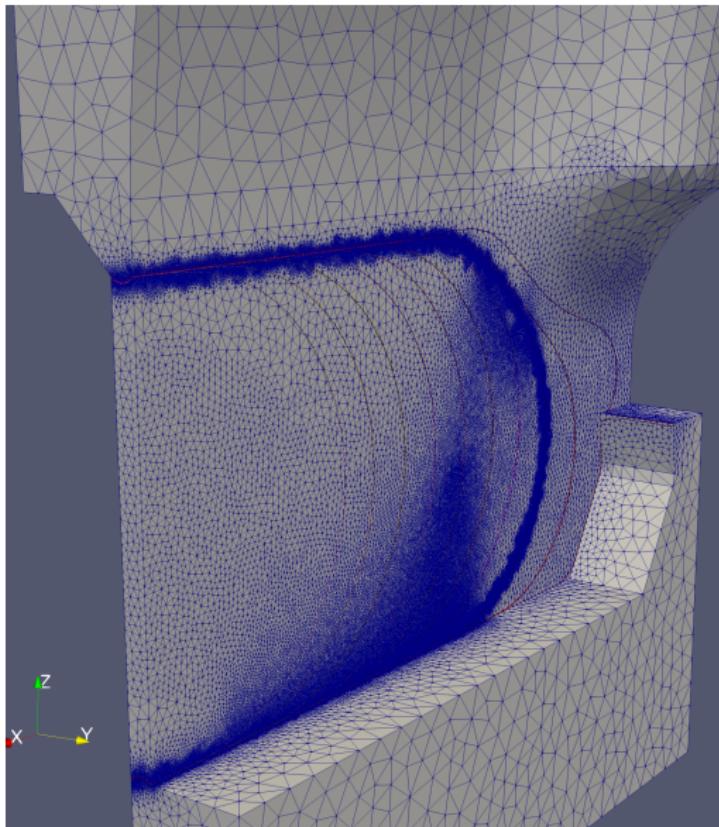
$\theta = 45$ degree, volume = 0.955323

numerical result by dynamic mesh refinement strategy : 2/5



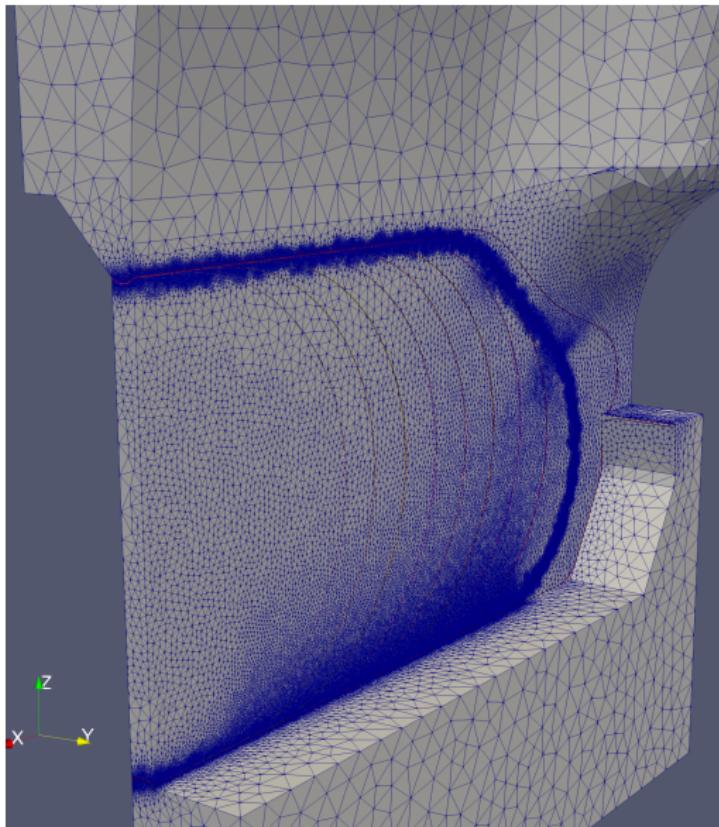
$\theta = 45$ degree, volume = 2.66561

numerical result by dynamic mesh refinement strategy : 3/5



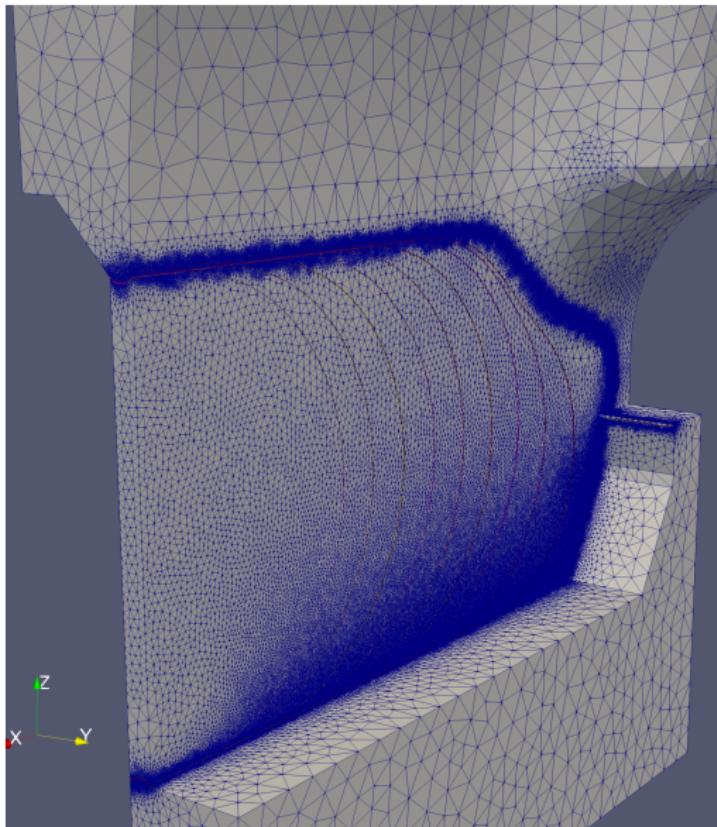
$\theta = 45$ degree, volume = 2.96374

numerical result by dynamic mesh refinement strategy : 4/5



$\theta = 45$ degree, volume = 3.26019

numerical result by dynamicmesh refinement strategy : 5/5



$\theta = 45$ degree, volume = 3.79139

conclusion

- ▶ Contact angle condition and volume constraint are imposed on the set to find a solution.
- ▶ Nonlinear boundary value problem is solved by Newton iteration with an initial guess that is obtained by pseudo time marching of gradient flow problem.
- ▶ Newton iteration combined with mesh refinement can find nonlinear solution efficiently.
- ▶ Volume constraint is treated as linear constraint for the linear system. Resulting system is a KKT type consisting of indefinite matrix and it is solved by two stages using Schur complement matrix.
- ▶ C++ implementation to compute Euler characteristics drastically shortens the computational time by FreeFEM script

FreeFEM on cloud

- ▶ <http://www.rescale.com> in conjunction with DENSO

FreeFEM + Gmsh + HPPDM + $\alpha \gg$ COMSOL

$\alpha \in \{ \text{nonlinear solver, time integration, optimization algorithm} \}$

Thanks to F. Hecht, P. Jolivet, S. Garnotel, F. Lahaye, and H. Ogawa