

# Developer's Notes

Siconos Development Team

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# Contents

<b>1</b>	<b>OneStepNSProblem formalisation for several interactions</b>	<b>4</b>
1.1	LinearDS - Linear Time Invariant Relations . . . . .	4
1.1.1	General notations . . . . .	4
1.1.2	A simple example . . . . .	6
1.1.3	relative degree . . . . .	7
1.2	LagrangianDS - Lagrangian Linear Relations . . . . .	7
1.2.1	General notations . . . . .	7
1.3	Block matrix approach . . . . .	9
1.3.1	Block matrix of DS . . . . .	9
1.3.2	Block matrix of interaction . . . . .	9
1.3.3	OSNSProblem using block matrices . . . . .	9
<b>2</b>	<b>Dynamical Systems formulations in Siconos.</b>	<b>10</b>
2.1	Class Diagram . . . . .	10
2.2	General non linear first order dynamical systems → class <i>DynamicalSystem</i> . . . . .	10
2.3	First order linear dynamical systems → class <i>LinearDS</i> . . . . .	11
2.4	Second order non linear Lagrangian dynamical systems → class <i>LagrangianDS</i> . . . . .	11
2.5	Second order linear and time-invariant Lagrangian dynamical systems → class <i>Lagrangian-LinearTIDS</i> . . . . .	12
<b>3</b>	<b>Dynamical Systems implementation in Siconos.</b>	<b>13</b>
3.1	Introduction . . . . .	13
3.2	Class Diagram . . . . .	13
3.3	Construction . . . . .	13
3.3.1	DynamicalSystem . . . . .	14
3.3.2	LagrangianDS . . . . .	14
3.4	Specific flags or members . . . . .	14
3.5	plug-in management . . . . .	15
<b>4</b>	<b>Interactions</b>	<b>16</b>
4.1	Introduction . . . . .	16
4.2	Class Diagram . . . . .	16
4.3	Description . . . . .	16
<b>5</b>	<b>Notes on the Non Smooth Dynamical System construction</b>	<b>17</b>
5.1	Introduction . . . . .	17
5.2	Class Diagram . . . . .	17
5.3	Description . . . . .	17
5.4	misc . . . . .	17

<b>6</b>	<b>OneStepIntegrator and derived classes.</b>	<b>19</b>
6.1	Introduction . . . . .	19
6.2	Class Diagram . . . . .	19
6.3	Misc . . . . .	19
6.4	Construction . . . . .	20
6.4.1	Moreau . . . . .	20
6.4.2	Lsodar . . . . .	20
<b>7</b>	<b>First Order Nonlinear Relation</b>	<b>21</b>
<b>8</b>	<b>Computation of the number of Index Set and various levels</b>	<b>22</b>
8.1	Why is the relative degree not relevant ? . . . . .	22
8.1.1	First order Linear complementary systems . . . . .	22
8.1.2	Second order Lagrangian systems . . . . .	23
8.1.3	Conclusion for the implementation . . . . .	24
8.2	How to define and compute the various levels and the number of indexSets . . . . .	24
8.2.1	$y$ related variables . . . . .	24
8.2.2	$\lambda$ related variables . . . . .	25
8.3	Rules for implementation . . . . .	25
<b>9</b>	<b>Newton's linearization for First Order Systems</b>	<b>27</b>
9.1	Various first order dynamical systems with input/output relations . . . . .	27
9.2	Time-discretizations . . . . .	28
9.2.1	Standard $\theta - \gamma$ scheme. . . . .	28
9.2.2	Full $\theta - \gamma$ scheme . . . . .	28
9.3	Newton's linearization of (9.5) . . . . .	30
9.3.1	The special case of Newton's linearization of (9.5) with FirstOrderType2R (9.3) . . . . .	33
9.3.2	The special case of Newton's linearization of (9.5) with FirstOrderType1R (9.2) . . . . .	34
9.3.3	Time-discretization of the linear case (9.4) . . . . .	34
9.4	Newton's linearization of (9.6) . . . . .	36
<b>10</b>	<b>Newton's linearization for Lagrangian systems</b>	<b>40</b>
10.1	Various second order dynamical systems with input/output relations . . . . .	40
10.1.1	Lagrangian dynamical systems . . . . .	40
10.1.2	Fully nonlinear case . . . . .	41
10.1.3	Lagrangian Rheonomous relations . . . . .	41
10.1.4	Lagrangian Scleronomous relations . . . . .	41
10.2	Moreau's Time-discretizations . . . . .	42
10.3	Schatzman-Paoli 'scheme and its linearizations . . . . .	42
10.3.1	The scheme . . . . .	42
10.3.2	The Newton linearization . . . . .	42
10.3.3	Linear version of the scheme . . . . .	43
10.4	What about mixing OnestepIntegrator in Simulation? . . . . .	43
<b>11</b>	<b>NewtonEuler Dynamical Systems</b>	<b>45</b>
11.1	The equations of motion . . . . .	45
11.2	Basic elements of Lie groups and Lie algebras theory. . . . .	47
11.2.1	Differential equation (evolving) on a manifold $\mathcal{M}$ . . . . .	48
11.2.2	Lie algebra and Lie group . . . . .	48
11.2.3	Actions of a group $\mathcal{G}$ on manifold $\mathcal{M}$ . . . . .	49
11.2.4	Exponential map . . . . .	50
11.2.5	Translation (Trivialization) maps . . . . .	50
11.2.6	Adjoint representation . . . . .	51
11.2.7	Differential of the exponential map . . . . .	52
11.2.8	Differential of a map $f : \mathcal{G} \rightarrow \mathfrak{g}$ . . . . .	53

11.3	Lie group $SO(3)$ of finite rotations and Lie algebra $\mathfrak{so}(3)$ of infinitesimal rotations . . . .	54
11.3.1	Newton method and differential of a map $f : \mathcal{G} \rightarrow \mathfrak{g}$ . . . . .	57
11.4	Lie group of unit quaternions $H_1$ and pure imaginary quaternions $H_p$ . . . . .	58
11.5	Newton-Euler equation in quaternion form . . . . .	65
11.5.1	Mechanical systems with bilateral and unilateral constraints . . . . .	65
11.6	Time integration scheme in scheme . . . . .	66
11.6.1	Moreau–Jean scheme based on a $\theta$ -method . . . . .	66
11.6.2	Semi-explicit version Moreau–Jean scheme based on a $\theta$ -method . . . . .	67
11.6.3	Nearly implicit version Moreau–Jean scheme based on a $\theta$ -method implemented in siconos . . . . .	67
11.6.4	Computation of the Jacobian in special case . . . . .	68
11.6.5	Siconos implementation . . . . .	69
<b>12</b>	<b>NewtonEulerR: computation of <math>\nabla_q H</math></b>	<b>70</b>
12.0.1	Gradient computation, case of NewtonEuler with quaternion . . . . .	70
12.0.2	Ball case . . . . .	71
12.0.3	Case FC3D: using the local frame and momentum . . . . .	72
12.0.4	Case FC3D: using the local frame local velocities . . . . .	73
<b>13</b>	<b>Projection On constraints</b>	<b>74</b>
13.0.1	Velocity formulation . . . . .	74
13.0.2	Posion formulation . . . . .	74
<b>14</b>	<b>Simulation of a Cam Follower System</b>	<b>76</b>
14.0.1	The cam-follower as a Lagrangian NSDS. . . . .	76
14.0.2	Implementation in the platform . . . . .	78
14.0.3	Simulation . . . . .	83
<b>15</b>	<b>Quartic Formulation</b>	<b>86</b>
15.0.1	Slidding ? . . . . .	86
<b>16</b>	<b>Alart–Curnier Formulation</b>	<b>89</b>
16.1	Reduced formulation to local variables. . . . .	89
16.1.1	Formulation . . . . .	89
16.1.2	Structure of the Jacobians . . . . .	89
16.1.3	Computation of the gradients . . . . .	89
16.1.4	Rearranging the cases . . . . .	91
16.2	Formulation with global variables. . . . .	91
16.2.1	Formulation . . . . .	91
16.2.2	Structure of the Jacobians . . . . .	91
16.2.3	Simplification ? . . . . .	92

# Chapter 1

## OneStepNSProblem formalisation for several interactions

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date	May 16, 2006
version	?

### 1.1 LinearDS - Linear Time Invariant Relations

#### 1.1.1 General notations

We consider  $n$  dynamical systems of the form:

$$\dot{x}_i = A_i x_i + R_i \quad (1.1)$$

Each system is of dimension  $n_i$ , and we denote  $N = \sum_{i=1}^n n_i$ .

An interaction,  $I_\alpha$  is composed with a non smooth law,  $nsLaw_\alpha$  and a relation:

$$y_\alpha = C_\alpha X_\alpha + D_\alpha \lambda_\alpha \quad (1.2)$$

The “dimension” of the interaction, ie the size of vector  $y_\alpha$ , is denoted  $m_\alpha$  and we set:

$$M = \sum_{\alpha=1}^m m_\alpha$$

$m$  being the number of interactions in the Non Smooth Dynamical System.

$X_\alpha$  is a vector that represents the DS concerned by the interaction. Its dimension is noted  $N_\alpha$ , this for  $n_\alpha$  systems in the interaction.

$C_\alpha$  is a  $m_\alpha \times N_\alpha$  row-blocks matrix and  $D_\alpha$  a  $m_\alpha \times m_\alpha$  square matrix.

$$C_\alpha = \begin{bmatrix} C_\alpha^i & C_\alpha^j & \dots \end{bmatrix} \quad (1.3)$$

with  $i, j, \dots \in \mathcal{DS}_\alpha$  which is the set of DS belonging to interaction  $\alpha$ .

We also have the following relation:

$$\begin{bmatrix} R_\alpha^i \\ R_\alpha^j \\ \dots \end{bmatrix} = B_\alpha \lambda_\alpha = \begin{bmatrix} B_\alpha^i \\ B_\alpha^j \\ \dots \end{bmatrix} \lambda_\alpha \quad (1.4)$$

$R_\alpha^i$  represents the contribution of interaction  $\alpha$  on the reaction of the dynamical system  $i$ , and  $B_\alpha^i$  is a  $n_i \times m_\alpha$  block matrix.

And so:

$$R_i = \sum_{\beta \in \mathcal{I}_i} R_\beta^i = \sum_{\beta \in \mathcal{I}_i} B_\beta^i \lambda_\beta \quad (1.5)$$

with  $\mathcal{I}_i$  the set of interactions in which dynamical system number  $i$  is involved.

Introducing the time discretization, we get:

$$x_i^{k+1} - x_i^k = hA_i x_i^{k+1} + hR_i^{k+1} \quad (1.6)$$

$$y_\alpha^{k+1} = C_\alpha X_\alpha^{k+1} + D_\alpha \lambda_\alpha^{k+1} \quad (1.7)$$

$$R_i^{k+1} = \sum_{\beta \in \mathcal{I}_i} B_\beta^i \lambda_\beta^{k+1} \quad (1.8)$$

ie, with  $W_i = (I - hA_i)^{-1}$ :

$$x_i^{k+1} = W_i x_i^k + hW_i R_i^{k+1} \quad (1.9)$$

$$y_\alpha^{k+1} = C_\alpha W_\alpha X_\alpha^k + C_\alpha hW_\alpha \sum_{\beta \in \mathcal{I}_i} B_\beta^i \lambda_\beta^{k+1} + D_\alpha \lambda_\alpha^{k+1} \quad (1.10)$$

$$= C_\alpha W_\alpha X_\alpha^k + (C_\alpha hW_\alpha B_\alpha + D_\alpha) \lambda_\alpha^{k+1} + \sum_{\beta \neq \alpha} \left( \sum_{i \in \mathcal{DS}_\alpha \cap \mathcal{DS}_\beta} hC_\alpha^i W_i B_\beta^i \lambda_\beta^{k+1} \right) \quad (1.11)$$

with

$$W_\alpha = \begin{bmatrix} W_i & 0 & \dots \\ 0 & W_j & \dots \\ 0 & \dots & \dots \end{bmatrix} \quad (1.12) \quad \{\text{Walpha}\}$$

the block-diagonal matrix of all the  $W$  for the dynamical systems involved in interaction  $\alpha$ .

The global-assembled  $Y$  vector, of dimension  $M$ , composed by  $m$   $y_\alpha$  subvectors, is given by:

$$Y_{k+1} = q_{OSNSP} + M_{OSNSP} \Lambda_{k+1} \quad (1.13)$$

or,

$$Y_{k+1} = \begin{bmatrix} y_1 \\ \dots \\ y_m \end{bmatrix}_{k+1} = \begin{bmatrix} C_1^1 & \dots & C_1^n \\ \vdots & \dots & \vdots \\ C_m^1 & \dots & C_m^n \end{bmatrix} \begin{bmatrix} W_1 & 0 & \dots & 0 \\ 0 & W_2 & \ddots & \vdots \\ \vdots & \ddots & \ddots & \vdots \\ 0 & \dots & 0 & W_n \end{bmatrix} \begin{bmatrix} x_1 \\ \vdots \\ \vdots \\ x_n \end{bmatrix}_k \quad (1.14)$$

$$+ \begin{bmatrix} D_1 + h \sum_{j \in \mathcal{DS}_1} C_1^j W_j B_1^j & h \sum_{j \in \mathcal{DS}_1 \cap \mathcal{DS}_2} C_1^j W_j B_2^j & \dots \\ \vdots & \ddots & \vdots \\ h \sum_{j \in \mathcal{DS}_m} C_m^j W_j B_{m-1}^j & D_m + h \sum_{j \in \mathcal{DS}_m \cap \mathcal{DS}_{m-1}} C_m^j W_j B_m^j \end{bmatrix} \begin{bmatrix} \lambda_1 \\ \vdots \\ \lambda_m \end{bmatrix}_{k+1}$$

To sum it up, the block-diagonal term of matrix  $M_{OSNSP}$ , for block-row  $\alpha$  is:

$$D_\alpha + h \sum_{j \in \mathcal{DS}_\alpha} C_\alpha^j W_j B_\alpha^j \quad (1.15)$$

This is an  $m_\alpha \times m_\alpha$  square matrix. The extra-diagonal block term, in position  $(\alpha, \beta)$  is:

$$h \sum_{j \in \mathcal{DS}_\alpha \cap \mathcal{DS}_\beta} C_\alpha^j W_j B_\beta^j \quad (1.16)$$

and is a  $m_\alpha \times m_\beta$  matrix. This matrix differs from 0 when interactions  $\alpha$  and  $\beta$  are coupled, ie have common DS.

Or, for the relation  $l$  of interaction  $\alpha$ , we get:

$$D_{\alpha,l} + h \sum_{j \in \mathcal{DS}_\alpha} C_{\alpha,l}^j W_j B_\alpha^j \quad (1.17)$$

for the diagonal, and

$$h \sum_{j \in \mathcal{DS}_\alpha \cap \mathcal{DS}_\beta} C_{\alpha,l}^j W_j B_\beta^j \quad (1.18)$$

for extra-diagonal terms.

$D_{\alpha,l}$ , row number  $l$  of  $D_\alpha$ , the same for  $C_{\alpha,l}$

Finally, the linked-Interaction map provides, for each interaction (named “current interaction”), the list of all the interactions (named “linked interaction”) that have common dynamical system with the “current interaction”.

### 1.1.2 A simple example

We consider  $n = 3$  dynamical systems and  $m = 2$  interactions:

$$\begin{aligned} I_\mu &\rightarrow \mathcal{DS}_\mu = \{DS_1, DS_3\}, m_\mu = 3 \\ I_\theta &\rightarrow \mathcal{DS}_\theta = \{DS_2, DS_3\}, m_\theta = 1 \end{aligned}$$

The linked-interaction map is :

$$\begin{aligned} I_\mu &\rightarrow I_{\theta, \text{commonDS}} = DS_3 \\ I_\theta &\rightarrow I_{\mu, \text{commonDS}} = DS_3 \end{aligned}$$

And:

$$M = 4, N = \sum_{i=1}^3 n_i$$

$$\mathcal{I}_1 = \{I_\mu\}$$

$$\mathcal{I}_2 = \{I_\theta\}$$

$$\mathcal{I}_3 = \{I_\mu, I_\theta\}$$

$$y_1 = \begin{bmatrix} C_1^1 & C_1^3 \end{bmatrix} \begin{bmatrix} x_1 \\ x_3 \end{bmatrix} + D_1 \lambda_1 \quad (1.19)$$

$$y_2 = \begin{bmatrix} C_2^2 & C_2^3 \end{bmatrix} \begin{bmatrix} x_2 \\ x_3 \end{bmatrix} + D_2 \lambda_2 \quad (1.20)$$

$$\begin{bmatrix} R_1 \\ R_2 \\ R_3 \end{bmatrix} = \begin{bmatrix} B_1^1 \lambda_1 \\ B_2^2 \lambda_2 \\ B_1^3 \lambda_1 + B_2^3 \lambda_2 \end{bmatrix} \quad (1.21)$$

$$M_{OSNSP} = \begin{bmatrix} D_1 + hC_1^1 W_1 B_1^1 + hC_1^3 W_3 B_1^3 & hC_1^3 W_3 B_2^3 \\ hC_2^3 W_3 B_1^3 & D_2 + hC_2^2 W_2 B_2^2 + hC_2^3 W_3 B_2^3 \end{bmatrix} \begin{bmatrix} \lambda_1 \\ \lambda_2 \end{bmatrix}_{k+1} \quad (1.22)$$

### 1.1.3 relative degree

Let us consider the global vector

$$Y = \begin{bmatrix} y_1 \\ \dots \\ y_M \end{bmatrix} = CX + D\Lambda \quad (1.23)$$

We denote by  $r_j$  the relative degree of equation  $j$ ,  $j \in [1..M]$ . We have:

$$y_j = \sum_{i=1}^n C_j^i x_i + D_{j,j} \lambda_j + \sum_{i \neq j, i=1}^m D_{j,i} \lambda_i \quad (1.24)$$

$D_{j,i}$  a scalar and  $C_j^i$  a  $1 \times n_i$  line-vector.

If  $D_{jj} \neq 0$ , then  $r_j = 0$ . Else, we should consider the first derivative of  $y_j$ .

Before that, recall that:

$$R_i = \sum_{k=1}^M B_k^i \lambda_j \quad (1.25)$$

Through many of the  $B_j^i$  are equal to zero, we keep them all in the following lines.

Then:

$$\dot{y}_j = \sum_{i=1}^n C_j^i (A_i x_i + \sum_{k=1}^M B_k^i \lambda_k) + f(\lambda_k)_{k \neq j} \quad (1.26)$$

$$= \sum_{i=1}^n C_j^i (A_i x_i + B_j^i \lambda_j + \sum_{k=1, k \neq j}^M B_k^i \lambda_k) + \dots \quad (1.27)$$

So, if  $\sum_{i=1}^n C_j^i B_j^i \neq 0$  (note that this corresponds to the product between line  $j$  of  $C$  and column  $j$  of  $B$ )

then  $r_j = 1$  else we consider the next derivative, and so on.

In derivative  $r$ , the coefficient of  $\lambda_j$  will be:

$$coeff_j = \sum_{i=1}^n C_j^i (A_i)^{r-1} B_j^i \quad (1.28)$$

if  $coeff_j \neq 0$  then  $r_j = r$ .

## 1.2 LagrangianDS - Lagrangian Linear Relations

### 1.2.1 General notations

We consider  $n$  dynamical systems, lagrangian and non linear, of the form:

$$M_i(q_i) \ddot{q}_i + N_i(\dot{q}_i, q_i) = F_{Int,i}(\dot{q}_i, q_i, t) + F_{Ext,i}(t) + p_i \quad (1.29)$$

Each system if of dimension  $n_i$ , and we denote  $N = \sum_{i=1}^n n_i$ .

An interaction,  $I_\alpha$  is composed with a non smooth law,  $nslaw_\alpha$  and a relation:

$$y_\alpha = H_\alpha Q_\alpha + b_\alpha \quad (1.30)$$



The “dimension” of the interaction, ie the size of vector  $y_\alpha$ , is denoted  $m_\alpha$  and we set:

$$M_y = \sum_{\alpha=1}^m m_\alpha$$

$m$  being the number of interactions in the Non Smooth Dynamical System.

$Q_\alpha$  is a vector that represents the DS concerned by the interaction. Its dimension is noted  $N_\alpha$ , this for  $n_\alpha$  systems in the interaction.

$H_\alpha$  is a  $m_\alpha \times N_\alpha$  row-blocks matrix and  $b_\alpha$  a  $m_\alpha$  vector.

$$H_\alpha = \begin{bmatrix} H_\alpha^i & H_\alpha^j & \dots \end{bmatrix} \quad (1.31)$$

with  $i, j, \dots \in \mathcal{DS}_\alpha$  which is the set of DS belonging to interaction  $\alpha$ .

We also have the following relation:

$$\begin{bmatrix} R_\alpha^i \\ R_\alpha^j \\ \dots \end{bmatrix} = {}^t H_\alpha \lambda_\alpha = \begin{bmatrix} {}^t H_\alpha^i \\ {}^t H_\alpha^j \\ \dots \end{bmatrix} \lambda_\alpha \quad (1.32)$$

$R_\alpha^i$  represents the contribution of interaction  $\alpha$  on the reaction of the dynamical system  $i$ , and  ${}^t H_\alpha^i$  is a  $n_i \times m_\alpha$  block matrix.

And so:

$$R_i = \sum_{\beta \in \mathcal{I}_i} R_\beta^i = \sum_{\beta \in \mathcal{I}_i} H_\beta^i \lambda_\beta \quad (1.33)$$

with  $\mathcal{I}_i$  the set of interactions in which dynamical system number  $i$  is involved.

Introducing the time discretisation, we get:

$$\begin{aligned} \dot{q}_i^{k+1} &= \dot{q}_{free,i}^{k+1} + W_i R_i^{k+1} \\ \dot{y}_\alpha^{k+1} &= H_\alpha \dot{Q}_\alpha^{k+1} \end{aligned} \quad (1.34)$$

$$R_i^{k+1} = \sum_{\beta \in \mathcal{I}_i} H_\beta^i \lambda_\beta^{k+1} \quad (1.35)$$

ie,

$$y_\alpha^{k+1} = H_\alpha Q_\alpha^{free} + H_\alpha W_\alpha {}^t H_\alpha \lambda_\alpha + \sum_{i \in \mathcal{DS}_\alpha} \sum_{\beta \in \mathcal{I}_i, \alpha \neq \beta} H_\alpha^i W_i H_\beta^j \lambda_\beta \quad (1.36)$$

with  $W_\alpha$  given by (1.12).

The global-assembled  $Y$  vector, of dimension  $M$ , composed by  $m$   $y_\alpha$  subvectors, is given by:

$$Y_{k+1} = q_{OSNSP} + M_{OSNSP} \Lambda_{k+1} \quad (1.37)$$

with:

$$q_{OSNSP}^\alpha = H_\alpha Q_\alpha^{free} \quad (1.38)$$

and for  $M_{OSNSP}$ , the block-diagonal term for block-row  $\alpha$  is

$$\sum_{j \in \mathcal{DS}_\alpha} H_\alpha^j W_j {}^t H_\alpha^j \quad (1.39)$$

an  $m_\alpha \times m_\alpha$  square matrix. The extra-diagonal block term, in position  $(\alpha, \beta)$  is:

$$\sum_{j \in \mathcal{DS}_\alpha \cap \mathcal{DS}_\beta} H_\alpha^j W_j {}^t H_\beta^j \quad (1.40)$$

and is a  $m_\alpha \times m_\beta$  matrix. This matrix differs from 0 when interactions  $\alpha$  and  $\beta$  are coupled, ie have common DS.

Or, for the relation  $l$  of interaction  $\alpha$ , we get:

$$\sum_{j \in \mathcal{DS}_\alpha} H_{\alpha,l}^j W_j^t H_\alpha^j \quad (1.41)$$

for the diagonal, and

$$\sum_{j \in \mathcal{DS}_\alpha \cap \mathcal{DS}_\beta} H_{\alpha,l}^j W_j^t H_\beta^j \quad (1.42)$$

for extra-diagonal terms.

$H_{\alpha,l}$ , row number  $l$  of  $H_\alpha$ .

WARNING: depending on linear and non linear case for the DS, there should be a factor  $h$  ahead  $W$ . See Bouncing Ball template.

## 1.3 Block matrix approach

The built of the OSNSProblem matrix could be computed using block matrix structure. This section describe these matrices. It is not implemented in Siconos. Using previous notations,  $n$  is the number of DS.  $m$  the number of interactions.

### 1.3.1 Block matrix of DS

$$M\dot{X} = AX + R$$

where  $M = \text{diag}(M_1, \dots, M_n)$  and  $A = \text{diag}(A_1, \dots, A_n)$ .

$$R = B\lambda$$

$$B = \begin{pmatrix} B_1^1 \dots B_m^1 \\ \vdots \\ B_1^n \dots B_m^n \end{pmatrix}$$

Some of  $B_j^i$  doesn't exist.

### 1.3.2 Block matrix of interaction

$$Y = CX + D\lambda$$

with  $D = \text{diag}(D_1 \dots D_m)$  and

$$C = \begin{pmatrix} C_1^1 \dots C_m^1 \\ \vdots \\ C_1^n \dots C_m^n \end{pmatrix}$$

Some of  $C_j^i$  doesn't exist.

### 1.3.3 OSNSProblem using block matrices

The Matrix of the OSNS Problem could be assembled using the following block-product-matrices  $CWB$ .

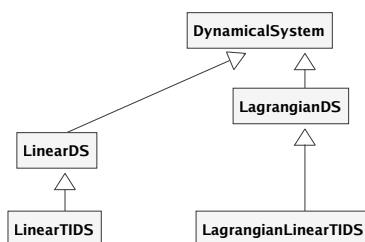
## Chapter 2

# Dynamical Systems formulations in Siconos.

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date	March 22, 2006
version	Kernel 1.1.4

### 2.1 Class Diagram

There are four possible formulation for dynamical systems in Siconos, two for first order systems and two for second order Lagrangian systems. The main class is `DynamicalSystem`, all other derived from this one, as shown in the following diagram:



{DSDiagram}

### 2.2 General non linear first order dynamical systems

→ **class** *DynamicalSystem*

This is the top class for dynamical systems. All other systems classes derived from this one.

A general dynamical systems is described by the following set of  $n$  equations, completed with initial conditions:

$$\begin{aligned} \dot{x} &= f(x, t) + T(x)u(x, \dot{x}, t) + r \\ x(t_0) &= x_0 \end{aligned} \tag{2.1}$$

(2.2)

- $x$ : state of the system - Vector of size  $n$ .
- $f(x, t)$ : vector field - Vector of size  $n$ .

- $u(x, \dot{x}, t)$ : control term - Vector of size  $uSize$ .
- $T(x)$ :  $n \times uSize$  matrix, related to control term.
- $r$ : input due to non-smooth behavior - Vector of size  $n$ .

The Jacobian matrix,  $\nabla_x f(x, t)$ , of  $f$  according to  $x$ ,  $n \times n$  square matrix, is also a member of the class.

Initial conditions are given by the member  $x_0$ , vector of size  $n$ . This corresponds to  $x$  value when simulation is starting, ie after a call to `strategy->initialize()`.

There are plug-in functions in this class for  $f$  (`vectorField`),  $jacobianX$ ,  $u$  and  $T$ . All of them can handle a vector of user-defined parameters.

## 2.3 First order linear dynamical systems $\rightarrow$ class *LinearDS*

Derived from `DynamicalSystem`, described by the set of  $n$  equations and initial conditions:

$$\dot{x} = A(t)x(t) + Tu(t) + b(t) + r \quad (2.3)$$

$$x(t_0) = x_0 \quad (2.4)$$

With:

- $A(t)$ :  $n \times n$  matrix, state independent but possibly time-dependent.
- $b(t)$ : Vector of size  $n$ , possibly time-dependent.

Other variables are those of `DynamicalSystem` class.

$A$  and  $B$  have corresponding plug-in functions.

Warning: time dependence for  $A$  and  $b$  is not available at the time in the simulation part for this kind of dynamical systems.

Links with `vectorField` and its Jacobian are:

$$f(x, t) = A(t)x(t) + b(t) \quad (2.5)$$

$$jacobianX = \nabla_x f(x, t) = A(t) \quad (2.6)$$

## 2.4 Second order non linear Lagrangian dynamical systems $\rightarrow$ class *LagrangianDS*

Lagrangian second order non linear systems are described by the following set of  $nDof$  equations + initial conditions:

$$M(q)\ddot{q} + NNL(\dot{q}, q) + F_{Int}(\dot{q}, q, t) = F_{Ext}(t) + p \quad (2.7)$$

$$q(t_0) = q_0 \quad (2.8)$$

$$\dot{q}(t_0) = velocity_0 \quad (2.9)$$

With:

- $M(q)$ :  $nDof \times nDof$  matrix of inertia.
- $q$ : state of the system - Vector of size  $nDof$ .
- $\dot{q}$  or *velocity*: derivative of the state according to time - Vector of size  $nDof$ .

- $NNL(\dot{q}, q)$ : non linear terms, time-independent - Vector of size  $nDof$ .
- $F_{Int}(\dot{q}, q, t)$ : time-dependent linear terms - Vector of size  $nDof$ .
- $F_{Ext}(t)$ : external forces, time-dependent BUT do not depend on state - Vector of size  $nDof$ .
- $p$ : input due to non-smooth behavior - Vector of size  $nDof$ .

The following Jacobian are also member of this class:

- $\text{jacobianQFInt} = \nabla_q F_{Int}(t, q, \dot{q})$  -  $nDof \times nDof$  matrix.
- $\text{jacobianVelocityFInt} = \nabla_{\dot{q}} F_{Int}(t, q, \dot{q})$  -  $nDof \times nDof$  matrix.
- $\text{jacobianQNNL} = \nabla_q NNL(q, \dot{q})$  -  $nDof \times nDof$  matrix.
- $\text{jacobianVelocityNNL} = \nabla_{\dot{q}} NNL(q, \dot{q})$  -  $nDof \times nDof$  matrix.

There are plug-in functions in this class for  $F_{int}$ ,  $F_{Ext}$ ,  $M$ ,  $NNL$  and the four Jacobian matrices. All of them can handle a vector of user-defined parameters.

Links with first order dynamical system are:

$$n = 2nDof \quad (2.10)$$

$$x = \begin{bmatrix} q \\ \dot{q} \end{bmatrix} \quad (2.11)$$

$$f(x, t) = \begin{bmatrix} \dot{q} \\ M^{-1}(F_{Ext} - F_{Int} - NNL) \end{bmatrix} \quad (2.12)$$

$$\nabla_x f(x, t) = \begin{bmatrix} 0_{nDof \times nDof} & I_{nDof \times nDof} \\ \nabla_q(M^{-1})(F_{Ext} - F_{Int} - NNL) - M^{-1}\nabla_q(F_{Int} + NNL) & -M^{-1}\nabla_{\dot{q}}(F_{Int} + NNL) \end{bmatrix} \quad (2.13)$$

$$r = \begin{bmatrix} 0_{nDof} \\ p \end{bmatrix} \quad (2.14)$$

$$u(x, \dot{x}, t) = u_L(\dot{q}, q, t) \text{ (not yet implemented)} \quad (2.15)$$

$$T(x) = \begin{bmatrix} 0_{nDof} \\ T_L(q) \end{bmatrix} \text{ (not yet implemented)} \quad (2.16)$$

$$(2.17)$$

With  $0_n$  a vector of zero of size  $n$ ,  $0_{n \times m}$  a  $n \times m$  zero matrix and  $I_{n \times n}$ , identity  $n \times n$  matrix.

Warning: control terms ( $Tu$ ) are not fully implemented in Lagrangian systems. This will be part of future version.

## 2.5 Second order linear and time-invariant Lagrangian dynamical systems $\rightarrow$ class *LagrangianLinearTIDS*

{Sec:LagrangianL

$$M\ddot{q} + C\dot{q} + Kq = F_{Ext}(t) + p \quad (2.18)$$

With:

- $C$ : constant viscosity  $nDof \times nDof$  matrix
- $K$ : constant rigidity  $nDof \times nDof$  matrix

And:

$$F_{Int} = C\dot{q} + Kq \quad (2.19)$$

$$NNL = 0_{nDof} \quad (2.20)$$

## Chapter 3

# Dynamical Systems implementation in Siconos.

author	F. P�rignon
date	November 7, 2006
version	Kernel 1.3.0

### 3.1 Introduction

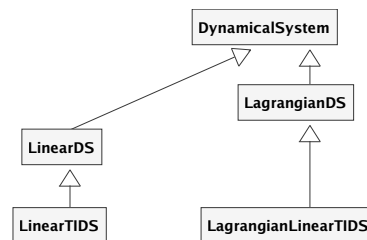
This document is only a sequel of notes and remarks on the way Dynamical Systems are implemented in Siconos.

It has to be completed, reviewed, reorganized etc etc for a future Developpers'Guide.

See also documentation in Doc/User/DynamicalSystemsInSiconos for a description of various dynamical systems types.

### 3.2 Class Diagram

There are four possible formulation for dynamical systems in Siconos, two for first order systems and two for second order Lagrangian systems. The main class is `DynamicalSystem`, all other derived from this one, as shown in the following diagram:



{DSDiagram}

### 3.3 Construction

Each constructor must:

- initialize all the members of the class and of the top-class if it exists

- allocate memory and set value for all required inputs
- allocate memory and set value for optional input if they are given as argument (in xml for example)
- check that given data are coherent and that the system is complete (for example, in the LagrangianDS if the internal forces are given as a plug-in, their Jacobian are also required. If they are not given, this leads to an exception).

No memory allocation is made for unused members  $\Rightarrow$  requires if statements in simulation. (if!=NULL ...).

### 3.3.1 DynamicalSystem

**Required data:**

n, x0, f, jacobianXF

**Optional:**

T,u

**Always allocated in constructor:**

x, x0, xFree, r, rhs, jacobianXF

Warning: default constructor is always private or protected and apart from the others and previous rules or remarks do not always apply to it. This for DS class and any of the derived ones.

### 3.3.2 LagrangianDS

**Required data:**

ndof, q0, velocity0, mass

**Optional:**

fInt and its Jacobian, fExt, NNL and its Jacobian.

**Always allocated in constructor:**

mass, q, q0, qFree, velocity, velocity0, velocityFree, p.

All other pointers to vectors/matrices are set to NULL by default.

Memory vectors are required but allocated during call to initMemory function.

Various rules:

- fInt (NNL) given as a plug-in  $\Rightarrow$  check that JacobianQ/Velocity are present (matrices or plug-in)
- any of the four Jacobian present  $\Rightarrow$  allocate memory for block-matrix jacobianX (connectToDS function)
- 

check: end of constructor or in initialize?

computeF and JacobianF + corresponding set functions: virtual or not?

## 3.4 Specific flags or members

- isAllocatedIn: to check inside-class memory allocation
- isPlugin: to check if operators are computed with plug-in or just directly set as a matrix or vector
- workMatrix: used to save some specific matrices in order to avoid recomputation if possible (inverse of mass ...)

### 3.5 plug-in management

DynamicalSystem class has a member named `parameterList` which is a *map*  $\langle \text{string}, \text{SimpleVector}^* \rangle$ , ie a list of pointers to `SimpleVector*`, with a string as a key to identified them. For example, `parametersList["mass"]` is a `SimpleVector*`, which corresponds to the last argument given in mass plug-in function.

By default, each parameters vectors must be initialized with a `SimpleVector` of size 1, as soon as the plug-in is declared. Moreover, to each vector corresponds a flag in `isAllocatedIn` map, to check if the corresponding vector has been allocated inside the class or not.

For example, in `DynamicalSystem`, if `isPlugin["vectorField"] == true`, then, during call to constructor or set function, it is necessary to defined the corresponding parameter:

```
parametersList["vectorField"] = newSimpleVector(1)
```

and to complete the `isAllocatedIn` flag:

```
isAllocatedIn["parameter_for_vectorField"] = true.
```



# Chapter 4

## Interactions

author	F. Pérignon
date	November 7, 2006
version	Kernel 1.3.0

### 4.1 Introduction

This document is only a sequel of notes and remarks on the way Interactions are implemented in Siconos.

It has to be completed, reviewed, reorganized etc etc for a future Developpers'Guide.

See also documentation in Doc/User/Interaction.

### 4.2 Class Diagram

### 4.3 Description

#### 4.3.1 Redaction note F. PERIGNON

review of interactions (for EventDriven implementation) 17th May 2006.

- variable *nInter* renamed in *interactionSize*: represents the size of  $y$  and  $\lambda$ . NOT the number of relations !!
- add a variable *nsLawSize* that depends on the non-smooth law type.  
Examples:
  - NewtonImpact -> *nsLawSize* = 1
  - Friction 2D -> *nsLawSize* = 2
  - Friction 3D -> *nsLawSize* = 3
  - ...
  - *nsLawSize* = n with n dim of matrix D in :  $y = Cx + D\lambda$ , D supposed to be a full-ranked matrix.  
Warning: this case is represented by only one relation of size n.
- *numberOfRelations*: number of relations in the interaction,  $numberOfRelations = \frac{interactionSize}{nsLawSize}$ .

## Chapter 5

# Notes on the Non Smooth Dynamical System construction

author	F. Pérignon
date	November 7, 2006
version	Kernel 1.3.0

### 5.1 Introduction

### 5.2 Class Diagram

### 5.3 Description

Objects must be constructed in the following order:

- DynamicalSystems
- NonSmoothLaw: depends on nothing
- Relation: no link with an interaction during construction, this will be done during initialization.
- Interaction: default constructor is private and copy is forbidden. Two constructors: xml and from data. Required data are a DSSet, a NonSmoothLaw and a Relation (+ dim of the Interaction and a number).  
Interaction has an initialize function which allocates memory for y and lambda, links correctly the relation and initializes it .... This function is called at the end of the constructor. That may be better to call it in simulation->initialize? Pb: xml constructor needs memory allocation for y and lambda if they are provided in the input xml file.
- NonSmoothDynamicalSystem: default is private, copy forbidden. Two constructors: xml and from data. Required data are the DSSet and the InteractionsSet. The topology is declared and constructed (but empty) during constructor call of the nsds, but initialize in the Simulation, this because it can not be initialize until the nsds has been fully described (ie this to allow user to add DS, Inter ...) at any time in the model, but before simulation initialization).

### 5.4 misc

- no need to keep a number for Interactions? Only used in xml for OSI, to know which Interactions it holds.

- pb: the number of saved derivatives for  $y$  and  $\lambda$  in Interactions is set to 2. This must depends on the relative degree which is computes during Simulation initialize and thus too late. It is so not available when memory is allocated (Interaction construction). Problem-> to be reviewed.

## Chapter 6

# OneStepIntegrator and derived classes.

author	F. Pérignon
date	November 7, 2006
version	Kernel 1.3.0

### 6.1 Introduction

This document is only a sequel of notes and remarks on the way OneStepIntegrators are implemented in Siconos.

It has to be completed, reviewed, reorganized etc etc for a future Developers' Guide.

See also documentation in Doc/User/OneStepIntegrator for a description of various OSI.

### 6.2 Class Diagram

### 6.3 Misc

OSI review for consistency between Lsodar and Moreau:

- add set of DynamicalSystem\*
- add set of Interaction\*
- add link to strategy that owns the OSI
- remove td object in OSI -> future: replace it by a set of td (one per ds)
- add strat in constructors arg list

osi -> strat -> Model -> nsds -> topology  
osi -> strat -> timeDiscretisation

let a timeDiscretisation object in the OSI? set of td (one per ds)?  
create a class of object that corresponds to DS on the simulation side ?  
will contain the DS, its discretization, theta for Moreau ... ?  
Allow setStrategyPtr operation? Warning: need reinitialisation.

Required input by user:

- list of DS or list of Interactions ?
- pointer to strategy
- ...

## 6.4 Construction

Each constructor must:

- 

### 6.4.1 Moreau

Two maps: one for  $W$ , and one for  $\theta$ . To each DS corresponds a  $\theta$  and a  $W$ .  
Strategy arg in each constructor.

**Required data:**

**Optional:**

**Always allocated in constructor:**

Warning: default constructor is always private or protected and apart from the others and previous rules or remarks do not always apply to it.

### 6.4.2 Lsodar

**Required data:**

**Optional:**

**Always allocated in constructor:**

## Chapter 7

# First Order Nonlinear Relation

author	O. Bonnefon
date	July, 1 2009
version	Kernel 3.0.0

## Chapter 8

# Computation of the number of Index Set and various levels

author	V. Acary
date	Septembre 16, 2011
version	Kernel 3.3.0

In this chapter, we give some hints on the automatic computation of the number of index sets, the number of derivatives in the `Interaction` and the `levelMin` and `LevelMax`.

### 8.1 Why is the relative degree not relevant ?

In this section, we give a very brief overview of the notion of relative degree.

#### 8.1.1 First order Linear complementary systems

A Linear Complementarity System (LCS) is defined by

$$\begin{cases} \dot{x} = Ax + B\lambda \\ y = Cx + D\lambda \\ 0 \leq y \perp \lambda \geq 0 \end{cases} \quad (8.1) \quad \{\text{eq:LCS-bis}\}$$

**Definition 1 (Relative degree in the SISO case)** *Let us consider a linear system in state representation given by the quadruplet  $(A, B, C, D) \in \mathbb{R}^{n \times n} \times \mathbb{R}^{n \times m} \times \mathbb{R}^{m \times n} \times \mathbb{R}^{m \times m}$ :*

$$\begin{cases} \dot{x} = Ax + B\lambda \\ y = Cx + D\lambda \end{cases} \quad (8.2) \quad \{\text{eq:LS}\}$$

- In the Single Input/ Single Output (SISO) case ( $m = 1$ ), the relative degree is defined by the first non zero Markov parameters :

$$D, CB, CAB, CA^2B, \dots, CA^{r-1}B, \dots \quad (8.3) \quad \{\text{eq:Markov-Param}\}$$

- In the multiple input/multiple output (MIMO) case ( $m > 1$ ), an uniform relative degree is defined as follows. If  $D$  is non singular, the relative degree is equal to 0. Otherwise, it is assumed to be the first positive integer  $r$  such that

$$CA^i B = 0, \quad i = 0 \dots r-2 \quad (8.4) \quad \{\text{eq:mimo-r}\}$$

while

$$CA^{r-1}B \text{ is non singular.} \quad (8.5) \quad \{\text{eq:mimo-r2}\}$$

The Markov parameters arise naturally when we derive with respect to time the output  $y$ ,

$$\begin{aligned} y &= Cx + D\lambda \\ \dot{y} &= CAx + CB\lambda, \text{ if } D = 0 \\ \ddot{y} &= CA^2x + CAB\lambda, \text{ if } D = 0, CB = 0 \\ &\dots \\ y^{(r)} &= CA^rx + CA^{r-1}B\lambda, \text{ if } D = 0, CB = 0, CA^{r-2}B = 0, r = 1 \dots r-2 \\ &\dots \end{aligned}$$

and the first non zero Markov parameter allows us to define the output  $y$  directly in terms of the input  $\lambda$ .

In continuous time, the nature of solutions depends strongly on the relative degree. When we want to perform the time-integration of such systems, we need also to reduce the relative degree or to know it to correctly operate.

We can observe that the relative degree 0 is well defined only by the relation ( $D$  nonsingular) and by the nonsmooth law. Indeed, let us imagine that the nonsmooth law is defined by  $0 \leq \dot{y} \perp \lambda \geq 0$ . We can easily see that the relative degree is reduced.

In the MIMO, the computation of non uniform relative degree is hard task. This is also the case for nonlinear systems.

### 8.1.2 Second order Lagrangian systems

Let us consider a second order linear and time-invariant Lagrangian dynamical system (see § 2.5)

$$\begin{cases} M\dot{v} + Cv + Kq = F_{Ext}(t) + p \\ \dot{q} = v \end{cases} \quad (8.6) \quad \{\text{eq:rd1}\}$$

together with a Lagrangian linear relation

$$y = Cq + e + D\lambda + Fz, \quad (8.7) \quad \{\text{eq:rd2}\}$$

$$p = C^t\lambda \quad (8.8) \quad \{\text{eq:rd3}\}$$

and a simple nonsmooth law,

$$0 \leq y \perp \lambda \geq 0 \quad (8.9) \quad \{\text{eq:rd4}\}$$

If  $D > 0$ , the relative degree is uniformly zero and the system can be solved without deriving the output (8.7). Indeed, we known that the solution of the LCP

$$0 \leq Cq + e + D\lambda + Fz, \perp \lambda \geq 0 \quad (8.10) \quad \{\text{eq:rd5}\}$$

is unique and Lipschitz with respect to  $q$ . It can be denoted as  $\lambda(q) = \text{SOL}(D, Cq + e + Fz)$ . Therefore, the differential equation (8.6) reduces to a standard ODE with a Lipschitz RHS

$$\begin{cases} M\dot{v} + Cv + Kq = F_{Ext}(t) + C^t\lambda(q) \\ \dot{q} = v \end{cases} \quad (8.11) \quad \{\text{eq:rd6}\}$$

In the case that we deal with unilateral contact, we usually have  $D = 0$  and the relative degree of the system is 2. In this case, the output has to be differentiated as

$$\dot{y} = C\dot{q}, \quad (8.12) \quad \{\text{eq:rd7}\}$$

and an impact law has to added, for instance the newton's impact law

$$\text{if } y = 0, \text{ when } \dot{y}^+ = -e\dot{y}^- \quad (8.13) \quad \{\text{eq:rd8}\}$$



In the same vein, the equations of motion (8.6) is not sufficient since the velocity may encounter jumps. The dynamics is usually replaced by a measure differential equation of the form

$$\begin{cases} Mdv + Cv^+(t)dt + Kq(t)dt = F_{Ext}(t)dt + di \\ \dot{q} = v \end{cases} \quad (8.14) \quad \{\text{eq:rd10}\}$$

where  $di$  is the measure that can be related to  $p$  thanks to

$$di = p dt + \sigma \delta_{t^*} \quad (8.15) \quad \{\text{eq:rd11}\}$$

is only one jump is expected at  $t^*$ .

### 8.1.3 Conclusion for the implementation

From the continuous time mathematical analysis, the relative degree is very important to know if we have to compute the derivatives of the output  $y^{(n)}$  and to consider various levels for the input  $p, \sigma, \dots$

However in the numerical practice, the time –discretization makes an assumption on the relative degree and treats the nonsmooth law at different levels. The resulting time discretized system possesses more or less variables.

Consider for instance (8.6) in the case of the Moreau scheme

$$\begin{cases} M(v_{k+1} - v_k) + h(Kq_{k+\theta} + Cv_{k+\theta}) = p_{k+1} = G(q_{k+1})\lambda_{k+1}, & (8.16a) \quad \{\text{eq:MoreauTS}\} \\ q_{k+1} = q_k + hv_{k+\theta}, & (8.16b) \\ \dot{y}_{k+1} = G^\top(q_{k+1})v_{k+1} & (8.16c) \\ \text{if } \bar{y}_{k+1}^\alpha \leq 0 \text{ then } 0 \leq \dot{y}_{k+1}^\alpha + e\dot{y}_k^\alpha \perp \lambda_{k+1}^\alpha \geq 0, \alpha \in \mathcal{I} & (8.16d) \quad \{\text{eq:MoreauTSd}\} \\ \text{otherwise } \lambda_{k+1}^\alpha = 0. \end{cases}$$

and the Schatzman–Paoli scheme

$$\begin{cases} M(q_{k+1} - 2q_k + q_{k-1}) + h^2(Kq_{k+\theta} + Cv_{k+\theta}) = p_{k+1}, & (8.17a) \\ v_{k+1} = \frac{q_{k+1} - q_{k-1}}{2h}, & (8.17b) \\ y_{k+1} = h \left( \frac{q_{k+1} + eq_{k-1}}{1+e} \right) & (8.17c) \\ p_{k+1} = G \left( \frac{q_{k+1} + eq_{k-1}}{1+e} \right) \lambda_{k+1} & (8.17d) \\ 0 \leq y_{k+1} \perp \lambda_{k+1} \geq 0. & (8.17e) \end{cases}$$

We can see easily that the number of derivatives (or levels) that we store for  $y$  and  $\lambda$  is independent on the relative degree but is chosen by the `OneStepIntegrator` with respect to the type of systems.

## 8.2 How to define and compute the various levels and the number of indexSets

### 8.2.1 $y$ related variables

The size of the vector  $y$  in the Interaction depends on

- the `OneStepIntegrator` type.
  - see the difference between the Moreau and Schatzman Paoli scheme,

- plan the time-discontinuous Galerkin scheme
- plan the Higher Order Moreau sweeping process (HOSP)
- the `Simulation` type.
  - In Timestepping or Event-driven we do not need the same number of stored  $y$
- the `NonSmoothLaw` type.
  - If we consider some cases with or without friction in Timestepping or Event-driven, we need to adapt the number of stored  $y$

Since the various levels of  $y$  are used to build the index sets we will need from 0 to a computed size that depends on the previous criteria. Only a part will be used in the `OneStepNSProblem`.

### 8.2.2 $\lambda$ related variables

The size of the vector `lambda` in the `Interaction` depends on the same criteria than in the previous section. Only, the number of `lambda` is not the same as  $y$  since a multiplier `lambda[i]` is not necessarily related to  $y[i]$

## 8.3 Rules for implementation

We can define new members in `Interaction`:

- `_lowerlevelForOutput`, this value is to 0 by default
- `_upperlevelForOutput`, this value must be computed at initialization with respect to the previous criteria
- `_lowerlevelForInput`, this value must be computed at initialization with respect to the previous criteria
- `_upperlevelForInput`, this value must be computed at initialization with respect to the previous criteria

This level are computed in `Simulation::ComputeLevelsForInputAndOutput`. A visitor is used for the `OneStepIntegrator`. Furthermore, four global levels are computed

- `_levelMinForOutput` this value is the minimum level for the output `Interaction::_lowerlevelForOutput` for all the interactions
- `_levelMaxForOutput` this value is the maximum level for the output `Interaction::_upperlevelForOutput` for all the interactions
- `_levelMinForInput` this value is the minimum level for the output `Interaction::_lowerlevelForInput` for all the interactions
- `_levelMaxForInput` this value is the maximum level for the output `Interaction::_upperlevelForInput` for all the interactions
- the values  $y[i]$  must be initialized from `_lowerlevelForOutput` to `_upperlevelForOutput`.
- the values `lambda[i]` must be initialized from `_lowerlevelForInput` to `_upperlevelForInput`.
- the values  $y[i]$  in `Interaction` must be used in priority to store the  $i$ -th derivative of  $y$ . When it is needed, higher index  $i$  can be used for other triggering variables. For instance, for an Event-Driven scheme with a Lagrangian systems with friction, sliding velocity must be stored.

- the values of `lambda[i]` must stored the various multiplier for the nonsmooth law. We affect the same index  $i$  as for the level of `y[i]` present in the corresponding nonsmooth law.
- The number of `IndexSets` should follows `_levelMaxForY`.

For the dynamical systems :

- The number of levels for `_r` and `_p` in the DS should follow `_lowerlevelForInput` and `_upperlevelForOutput` of the associated interactions. This is done in `Interaction::initialize`.
- A new variable should be added in the `LagrangianDS` to store the multiplier at the position level (`_tau` ?) to avoid the use of `_p[0]`. Indeed, we will continue to assume that `_p` is the input in the equation of motion. For `lambda` we can use `lambda[0]`

#### TODO LIST AND QUESTIONS

- What about the case of multiples interactions on a DS with various `_lowerlevelForInput` and `_upperlevelForOutput` ? Normally, all the levels should be correctly initialized thanks to the proposed implementation (r2821)
- `DynamicalSystem::_r` should be a `VectorOfVectors`
- `DynamicalSystem::_r` is split in `LagrangianDS`. a first part is `LagrangianDS::_p`. The other is not implemented !! `LagrangianDS::_tau` ?

## Chapter 9

# Newton's linearization for First Order Systems

author	O.Bonnefon, V. Acary
date	Sept, 07, 2007
last update	Feb, 2011 April, 2014
version	

This section is devoted to the implementation and the study of the algorithm. The interval of integration is  $[0, T]$ ,  $T > 0$ , and a grid  $t_0 = 0, t_{k+1} = t_k + h, k \geq 0, t_N = T$  is constructed. The approximation of a function  $f(\cdot)$  on  $[0, T]$  is denoted as  $f^N(\cdot)$ , and is a piecewise constant function, constant on the intervals  $[t_k, t_{k+1})$ . We denote  $f^N(t_k)$  as  $f_k$ . The time-step is  $h > 0$ .

### 9.1 Various first order dynamical systems with input/output relations

**FirstOrderR. Fully nonlinear case** Let us introduce the following system,

$$\begin{aligned} M\dot{x}(t) &= f(x(t), t) + r(t) \\ y(t) &= h(t, x(t), \lambda(t)) \\ r(t) &= g(t, x(t), \lambda(t)) \end{aligned} \tag{9.1} \quad \{\text{first-DS}\}$$

where  $\lambda(t) \in \mathbf{R}^m$  and  $y(t) \in \mathbf{R}^m$  are complementary variables related through a multi-valued mapping. According to the class of systems, we are studying, the function  $f$  and  $g$  are defined by a fully nonlinear framework or by affine functions. We have decided to present the time-discretization in its full generality and specialize the algorithms for each cases in Section ?? . This fully nonlinear case is not implemented in Siconos yet. This fully general case is not yet implemented in Siconos.

This case is implemented in Siconos with the relation `FirstOrderR` using the subtype `NonLinearR`

**FirstOrderType1R** Let us introduce a new notation,

$$\begin{aligned} M\dot{x}(t) &= f(x(t), t) + r(t) \\ y(t) &= h(t, x(t)) \\ r(t) &= g(t, \lambda(t)) \end{aligned} \tag{9.2} \quad \{\text{first-DS1}\}$$

This case is implemented in Siconos with the relation `FirstOrderType1R`.

**FirstOrderType2R** Let us introduce a new notation,

$$\begin{aligned} M\dot{x}(t) &= f(x(t), t) + r(t) \\ y(t) &= h(t, x(t), \lambda(t)) \\ r(t) &= g(t, \lambda(t)) \end{aligned} \tag{9.3} \quad \{\text{first-DS2}\}$$

This case is implemented in Siconos with the relation `FirstOrderType2R`.

**Linear case** Let us introduce a new notation,

$$\begin{aligned} M\dot{x}(t) &= Ax(t) + r(t) + b(t) \\ y(t) &= h(x(t), \lambda(t), z) = Cx + Fz + D\lambda \\ r(t) &= g(t, \lambda(t)) = B\lambda \end{aligned} \tag{9.4} \quad \{\text{first-DS3}\}$$

## 9.2 Time-discretizations

### 9.2.1 Standard $\theta - \gamma$ scheme.

Let us now proceed with the time discretization of (9.4) by a fully implicit scheme :

$$\begin{aligned} Mx_{k+1} &= Mx_k + h\theta f(x_{k+1}, t_{k+1}) + h(1 - \theta)f(x_k, t_k) + h\gamma r(t_{k+1}) + h(1 - \gamma)r(t_k) \\ y_{k+1} &= h(t_{k+1}, x_{k+1}, \lambda_{k+1}) \\ r_{k+1} &= g(t_{k+1}, x_{k+1}, \lambda_{k+1}) \\ \text{NsLaw}(y_{k+1}, \lambda_{k+1}) \end{aligned} \tag{9.5} \quad \{\text{eq:toto1}\}$$

where  $\theta = [0, 1]$  and  $\gamma \in [0, 1]$ . As in [? ], we call the problem (9.5) the “one-step nonsmooth problem”.

In the Siconos/Kernel module, the use of  $\gamma$  is activated in the class `EulerMoreauOSI` by the boolean `_useGamma`.

This time-discretization is slightly more general than a standard implicit Euler scheme. The main discrepancy lies in the choice of a  $\theta$ -method to integrate the nonlinear term. For  $\theta = 0$ , we retrieve the explicit integration of the smooth and single valued term  $f$ . Moreover for  $\gamma = 0$ , the term  $g$  is explicitly evaluated. The flexibility in the choice of  $\theta$  and  $\gamma$  allows the user to improve and control the accuracy, the stability and the numerical damping of the proposed method. For instance, if the smooth dynamics given by  $f$  is stiff, or if we have to use big step sizes for practical reasons, the choice of  $\theta > 1/2$  offers better stability with the respect to  $h$ .

### 9.2.2 Full $\theta - \gamma$ scheme

Another possible time-discretization is as follows.

$$\begin{aligned} Mx_{k+1} &= Mx_k + h\theta f(x_{k+1}, t_{k+1}) + h(1 - \theta)f(x_k, t_k) + hr(t_{k+\gamma}) \\ y_{k+\gamma} &= h(t_{k+\gamma}, x_{k+\gamma}, \lambda_{k+\gamma}) \\ r_{k+\gamma} &= g(t_{k+\gamma}, x_{k+\gamma}, \lambda_{k+\gamma}) \\ \text{NsLaw}(y_{k+\gamma}, \lambda_{k+\gamma}) \end{aligned} \tag{9.6} \quad \{\text{eq:toto1-ter}\}$$

We call the scheme (9.6) the full  $\theta - \gamma$  scheme since it uses also the evaluation at  $t_{k+\gamma}$  for the relation.

In the Siconos/Kernel module, the time-stepping scheme is activated in the class `EulerMoreauOSI` by the boolean `_useGammaForRelation`.

Another possibility for the time discretization in the nonlinear case would be

$$\begin{aligned}
 Mx_{k+1} &= Mx_k + hf(x_{k+\theta}, t_{k+\theta}) + hr(t_{k+\gamma}) \\
 y_{k+\gamma} &= h(t_{k+\gamma}, x_{k+\gamma}, \lambda_{k+\gamma}) \\
 r_{k+\gamma} &= g(t_{k+\gamma}, x_{k+\gamma}, \lambda_{k+\gamma}) \\
 \text{NsLaw}(y_{k+\gamma}, \lambda_{k+\gamma})
 \end{aligned}
 \tag{9.7} \quad \text{\texttt{\{eq:toto1-quat\}}}$$

This scheme has not been yet implemented in Siconos/Kernel.

### 9.3 Newton's linearization of (9.5)

Due to the fact that two of the studied classes of systems that are studied in this paper are affine functions in terms of  $f$  and  $g$ , we propose to solve the "one-step nonsmooth problem" (9.5) by performing an external Newton linearization.

**Newton's linearization of the first line of (9.5)** The first line of the problem (9.5) can be written under the form of a residue  $\mathcal{R}$  depending only on  $x_{k+1}$  and  $r_{k+1}$  such that

$$\mathcal{R}(x_{k+1}, r_{k+1}) = 0 \quad (9.8) \quad \{\text{eq:NL3}\}$$

with

$$\mathcal{R}(x, r) = M(x - x_k) - h\theta f(x, t_{k+1}) - h(1 - \theta)f(x_k, t_k) - h\gamma r - h(1 - \gamma)r_k. \quad (9.9)$$

The solution of this system of nonlinear equations is sought as a limit of the sequence  $\{x_{k+1}^\alpha, r_{k+1}^\alpha\}_{\alpha \in \mathbb{N}}$  such that

$$\begin{cases} x_{k+1}^0 = x_k \\ r_{k+1}^0 = r_k \\ \mathcal{R}_L(x_{k+1}^{\alpha+1}, r_{k+1}^{\alpha+1}) = \mathcal{R}(x_{k+1}^\alpha, r_{k+1}^\alpha) + [\nabla_x \mathcal{R}(x_{k+1}^\alpha, r_{k+1}^\alpha)] (x_{k+1}^{\alpha+1} - x_{k+1}^\alpha) + [\nabla_r \mathcal{R}(x_{k+1}^\alpha, r_{k+1}^\alpha)] (r_{k+1}^{\alpha+1} - r_{k+1}^\alpha) = 0 \end{cases} \quad (9.10) \quad \{\text{eq:NL7}\}$$

#### 9.3.1 Redaction note V. ACARY

What about  $r_{k+1}^0$  ?

The residu free  $\mathcal{R}_{\text{free}}$  is also defined (useful for implementation only):

$$\mathcal{R}_{\text{free}}(x) \triangleq M(x - x_k) - h\theta f(x, t_{k+1}) - h(1 - \theta)f(x_k, t_k),$$

which yields

$$\mathcal{R}(x, r) = \mathcal{R}_{\text{free}}(x) - h\gamma r - h(1 - \gamma)r_k.$$

$$\mathcal{R}(x_{k+1}^\alpha, r_{k+1}^\alpha) = \boxed{\mathcal{R}_{k+1}^\alpha \triangleq \mathcal{R}_{\text{free}}(x_{k+1}^\alpha) - h\gamma r_{k+1}^\alpha - h(1 - \gamma)r_k} \quad (9.11) \quad \{\text{eq:rfree-1}\}$$

$$\mathcal{R}_{\text{free}}(x_{k+1}^\alpha, r_{k+1}^\alpha) = \boxed{\mathcal{R}_{\text{free},k+1}^\alpha \triangleq M(x_{k+1}^\alpha - x_k) - h\theta f(x_{k+1}^\alpha, t_{k+1}) - h(1 - \theta)f(x_k, t_k)}$$

At each time-step, we have to solve the following linearized problem,

$$\mathcal{R}_{k+1}^\alpha + (M - h\theta A_{k+1}^\alpha)(x_{k+1}^{\alpha+1} - x_{k+1}^\alpha) - h\gamma(r_{k+1}^{\alpha+1} - r_{k+1}^\alpha) = 0, \quad (9.12) \quad \{\text{eq:NL10}\}$$

with

$$A_{k+1}^\alpha = \nabla_x f(t_{k+1}, x_{k+1}^\alpha) \quad (9.13)$$

By using (9.11), we get

$$\mathcal{R}_{\text{free}}(x_{k+1}^\alpha, r_{k+1}^\alpha) - h\gamma r_{k+1}^{\alpha+1} - h(1 - \gamma)r_k + (M - h\theta A_{k+1}^\alpha)(x_{k+1}^{\alpha+1} - x_{k+1}^\alpha) = 0 \quad (9.14) \quad \{\text{eq:rfree-2}\}$$

The matrix  $W$  is clearly non singular for small  $h$ .

**Newton's linearization of the second line of (9.5)** The same operation is performed with the second equation of (9.5)

$$\mathcal{R}_y(x, y, \lambda) = y - h(t_{k+1}, x, \lambda) = 0 \quad (9.15)$$

which is linearized as

$$\begin{aligned} \mathcal{R}_{Ly}(x_{k+1}^{\alpha+1}, y_{k+1}^{\alpha+1}, \lambda_{k+1}^{\alpha+1}) &= \mathcal{R}_y(x_{k+1}^{\alpha}, y_{k+1}^{\alpha}, \lambda_{k+1}^{\alpha}) + (y_{k+1}^{\alpha+1} - y_{k+1}^{\alpha}) - \\ &C_{k+1}^{\alpha}(x_{k+1}^{\alpha+1} - x_{k+1}^{\alpha}) - D_{k+1}^{\alpha}(\lambda_{k+1}^{\alpha+1} - \lambda_{k+1}^{\alpha}) = 0 \end{aligned} \quad (9.16) \quad \{\text{eq:NL9}\}$$

This leads to the following linear equation

$$y_{k+1}^{\alpha+1} = y_{k+1}^{\alpha} - \mathcal{R}_{y_{k+1}}^{\alpha} + C_{k+1}^{\alpha}(x_{k+1}^{\alpha+1} - x_{k+1}^{\alpha}) + D_{k+1}^{\alpha}(\lambda_{k+1}^{\alpha+1} - \lambda_{k+1}^{\alpha}) \quad (9.17) \quad \{\text{eq:NL11y}\}$$

with,

$$C_{k+1}^{\alpha} = \nabla_x h(t_{k+1}, x_{k+1}^{\alpha}, \lambda_{k+1}^{\alpha}) \quad (9.18)$$

$$D_{k+1}^{\alpha} = \nabla_{\lambda} h(t_{k+1}, x_{k+1}^{\alpha}, \lambda_{k+1}^{\alpha})$$

and

$$\mathcal{R}_{y_{k+1}}^{\alpha} \triangleq y_{k+1}^{\alpha} - h(x_{k+1}^{\alpha}, \lambda_{k+1}^{\alpha}) \quad (9.19)$$

**Newton's linearization of the third line of (9.5)** The same operation is performed with the third equation of (9.5)

$$\mathcal{R}_r(r, x, \lambda) = r - g(t_{k+1}, x, \lambda) = 0 \quad (9.20)$$

which is linearized as

$$\mathcal{R}_{Lr}(r_{k+1}^{\alpha+1}, x_{k+1}^{\alpha+1}, \lambda_{k+1}^{\alpha+1}) = \mathcal{R}_{rk+1}^{\alpha} + (r_{k+1}^{\alpha+1} - r_{k+1}^{\alpha}) - K_{k+1}^{\alpha}(x_{k+1}^{\alpha+1} - x_{k+1}^{\alpha}) - B_{k+1}^{\alpha}(\lambda_{k+1}^{\alpha+1} - \lambda_{k+1}^{\alpha}) = 0 \quad (9.21) \quad \{\text{eq:NL9}\}$$

$$r_{k+1}^{\alpha+1} = g(t_{k+1}, x_{k+1}^{\alpha}, \lambda_{k+1}^{\alpha}) + K_{k+1}^{\alpha}(x_{k+1}^{\alpha+1} - x_{k+1}^{\alpha}) + B_{k+1}^{\alpha}(\lambda_{k+1}^{\alpha+1} - \lambda_{k+1}^{\alpha}) \quad (9.22) \quad \{\text{eq:rrL}\}$$

with,

$$K_{k+1}^{\alpha} = \nabla_x g(t_{k+1}, x_{k+1}^{\alpha}, \lambda_{k+1}^{\alpha}) \quad (9.23)$$

$$B_{k+1}^{\alpha} = \nabla_{\lambda} g(t_{k+1}, x_{k+1}^{\alpha}, \lambda_{k+1}^{\alpha})$$

and the residue for  $r$ :

$$\mathcal{R}_{rk+1}^{\alpha} = r_{k+1}^{\alpha} - g(t_{k+1}, x_{k+1}^{\alpha}, \lambda_{k+1}^{\alpha}) \quad (9.24)$$

**Reduction to a linear relation between  $x_{k+1}^{\alpha+1}$  and  $\lambda_{k+1}^{\alpha+1}$**  Inserting (9.22) into (9.14), we get the following linear relation between  $x_{k+1}^{\alpha+1}$  and  $\lambda_{k+1}^{\alpha+1}$ ,

$$\begin{aligned} \mathcal{R}_{\text{free},k+1}^{\alpha} - h\gamma \left[ g(t_{k+1}, x_{k+1}^{\alpha}, \lambda_{k+1}^{\alpha}) + B_{k+1}^{\alpha}(\lambda_{k+1}^{\alpha+1} - \lambda_{k+1}^{\alpha}) + K_{k+1}^{\alpha}(x_{k+1}^{\alpha+1} - x_{k+1}^{\alpha}) \right] \\ - h(1 - \gamma)r_k + (M - h\theta A_{k+1}^{\alpha})(x_{k+1}^{\alpha+1} - x_{k+1}^{\alpha}) = 0 \end{aligned} \quad (9.25) \quad \{\text{eq:rffree-3}\}$$



that is

$$(M - h\theta A_{k+1}^\alpha - h\gamma K_{k+1}^\alpha)(x_{k+1}^{\alpha+1} - x_{k+1}^\alpha) = -\mathcal{R}_{\text{free},k+1}^\alpha - h(1-\gamma)r_k + h\gamma \left[ g(t_{k+1}, x_{k+1}^\alpha, \lambda_{k+1}^\alpha) + B_{k+1}^\alpha(\lambda_{k+1}^{\alpha+1} - \lambda_{k+1}^\alpha) \right] \quad (9.26) \quad \{\text{eq:rfree-4}\}$$

Let us introduce some intermediate notation:

$$W_{k+1}^\alpha \triangleq M - h\theta A_{k+1}^\alpha - h\gamma K_{k+1}^\alpha \quad (9.27) \quad \{\text{eq:NL9}\}$$

$$x_{\text{free}}^\alpha \triangleq x_{k+1}^\alpha - (W_{k+1}^\alpha)^{-1}(\mathcal{R}_{\text{free},k+1}^\alpha - h(1-\gamma)r_k) \quad (9.28) \quad \{\text{eq:rfree-12}\}$$

and

$$x_p^\alpha \triangleq h\gamma(W_{k+1}^\alpha)^{-1} [g(t_{k+1}, x_{k+1}^\alpha, \lambda_{k+1}^\alpha) - B_{k+1}^\alpha(\lambda_{k+1}^\alpha)] + x_{\text{free}}^\alpha. \quad (9.29)$$

The relation (9.26) can be written as

$$x_{k+1}^{\alpha+1} \triangleq x_p^\alpha + \left[ h\gamma(W_{k+1}^\alpha)^{-1} B_{k+1}^\alpha \lambda_{k+1}^{\alpha+1} \right] \quad (9.30) \quad \{\text{eq:rfree-13}\}$$

**Reduction to a linear relation between  $y_{k+1}^{\alpha+1}$  and  $\lambda_{k+1}^{\alpha+1}$ .** Inserting (9.30) into (9.17), we get the following linear relation between  $y_{k+1}^{\alpha+1}$  and  $\lambda_{k+1}^{\alpha+1}$ ,

$$y_{k+1}^{\alpha+1} = y_p + \left[ h\gamma C_{k+1}^\alpha (W_{k+1}^\alpha)^{-1} B_{k+1}^\alpha + D_{k+1}^\alpha \right] \lambda_{k+1}^{\alpha+1} \quad (9.31)$$

with

$$y_p = y_{k+1}^\alpha - \mathcal{R}_{y_{k+1}}^\alpha + C_{k+1}^\alpha(x_q) - D_{k+1}^\alpha \lambda_{k+1}^\alpha \quad (9.32)$$

$$x_q = x_p^\alpha - x_{k+1}^\alpha \quad (9.33) \quad \{\text{eq:xqq}\}$$

**Mixed linear complementarity problem (MLCP)** To summarize, the problem to be solved in each Newton iteration is:

$$\begin{cases} y_{k+1}^{\alpha+1} = W_{\text{mlcp},k+1}^\alpha \lambda_{k+1}^{\alpha+1} + b_{k+1}^\alpha \\ -y_{k+1}^{\alpha+1} \in N_{[l,u]}(\lambda_{k+1}^{\alpha+1}). \end{cases} \quad (9.34) \quad \{\text{eq:NL14}\}$$

with  $W_{\text{mlcp},k+1}^\alpha \in \mathbb{R}^{m \times m}$  and  $b \in \mathbb{R}^m$  defined by

$$\begin{aligned} W_{\text{mlcp},k+1}^\alpha &= h\gamma C_{k+1}^\alpha (W_{k+1}^\alpha)^{-1} B_{k+1}^\alpha + D_{k+1}^\alpha \\ b_{k+1}^\alpha &= y_p \end{aligned} \quad (9.35) \quad \{\text{eq:NL15}\}$$

The problem (9.34) is equivalent to a Mixed Linear Complementarity Problem (MLCP) which can be solved under suitable assumptions by many linear complementarity solvers such as pivoting techniques, interior point techniques and splitting/projection strategies. The reformulation into a standard

MLCP follows the same line as for the MCP in the previous section. One obtains,

$$\begin{aligned} y_{k+1}^{\alpha+1} &= -W_{k+1}^{\alpha} \lambda_{k+1}^{\alpha+1} + b_{k+1}^{\alpha} \\ (y_{k+1}^{\alpha+1})_i &= 0 \quad \text{for } i \in \{1..n\} \\ 0 \leq (\lambda_{k+1}^{\alpha+1})_i \perp (y_{k+1}^{\alpha+1})_i &\geq 0 \quad \text{for } i \in \{n..n+m\} \end{aligned} \tag{9.36} \quad \{\text{eq:MLCP1}\}$$

### 9.3.1 The special case of Newton's linearization of (9.5) with FirstOrderType2R (9.3)

Let us now proceed with the time discretization of (9.5) with FirstOrderType2R (9.3) by a fully implicit scheme :

$$\begin{aligned} Mx_{k+1} &= Mx_k + h\theta f(x_{k+1}, t_{k+1}) + h(1-\theta)f(x_k, t_k) + h\gamma r(t_{k+1}) + h(1-\gamma)r(t_k) \\ y_{k+1} &= h(t_{k+1}, x_{k+1}, \lambda_{k+1}) \\ r_{k+1} &= g(t_{k+1}, \lambda_{k+1}) \end{aligned} \tag{9.37} \quad \{\text{eq:mlcp2-toto1-}\}$$

**Newton's linearization of the first line of (9.37)** The linearization of the first line of the problem (9.37) is similar to the previous case so that (9.14) is still valid.

**Newton's linearization of the second line of (9.37)** The linearization of the second line of the problem (9.37) is similar to the previous case so that (9.17) is still valid.

**Newton's linearization of the third line of (9.37)** Since  $K_{k+1}^{\alpha} = \nabla_x g(t_{k+1}, \lambda_{k+1}^{\alpha}) = 0$ , the linearization of the third line of (9.37) reads as

$$r_{k+1}^{\alpha+1} = g(t_{k+1}, \lambda_{k+1}^{\alpha}) + B_{k+1}^{\alpha}(\lambda_{k+1}^{\alpha+1} - \lambda_{k+1}^{\alpha}) \tag{9.38} \quad \{\text{eq:mlcp2-rrL}\}$$

**Reduction to a linear relation between  $x_{k+1}^{\alpha+1}$  and  $\lambda_{k+1}^{\alpha+1}$**  Inserting (9.38) into (??), we get the following linear relation between  $x_{k+1}^{\alpha+1}$  and  $\lambda_{k+1}^{\alpha+1}$ , we get the linear relation

$$x_{k+1}^{\alpha+1} \triangleq x_p^{\alpha} + \left[ h\gamma(W_{k+1}^{\alpha})^{-1} B_{k+1}^{\alpha} \lambda_{k+1}^{\alpha+1} \right] \tag{9.39} \quad \{\text{eq:mlcp2-rfree-}\}$$

with

$$x_p^{\alpha} \triangleq h\gamma(W_{k+1}^{\alpha})^{-1} \left[ g(t_{k+1}, \lambda_{k+1}^{\alpha}) - B_{k+1}^{\alpha}(\lambda_{k+1}^{\alpha}) \right] + x_{\text{free}}^{\alpha} \tag{9.40}$$

and

$$W_{k+1}^{\alpha} \triangleq M - h\theta A_{k+1}^{\alpha} \tag{9.41} \quad \{\text{eq:mlcp2-NL9}\}$$

**Reduction to a linear relation between  $y_{k+1}^{\alpha+1}$  and  $\lambda_{k+1}^{\alpha+1}$**  Inserting (9.39) into (9.17), we get the following linear relation between  $y_{k+1}^{\alpha+1}$  and  $\lambda_{k+1}^{\alpha+1}$ ,

$$y_{k+1}^{\alpha+1} = y_p + \left[ h\gamma C_{k+1}^{\alpha} (W_{k+1}^{\alpha})^{-1} B_{k+1}^{\alpha} + D_{k+1}^{\alpha} \right] \lambda_{k+1}^{\alpha+1} \tag{9.42}$$

with

$$y_p = y_{k+1}^\alpha - \mathcal{R}_{y_{k+1}}^\alpha + C_{k+1}^\alpha(x_q) - D_{k+1}^\alpha \lambda_{k+1}^\alpha \quad (9.43)$$

$$x_q^\alpha = x_p^\alpha - x_{k+1}^\alpha \quad (9.44) \quad \{\text{eq:mlcp2-xqq}\}$$

### 9.3.2 The special case of Newton's linearization of (9.5) with FirstOrderType1R (9.2)

Let us now proceed with the time discretization of (9.5) with FirstOrderType1R (9.2) by a fully implicit scheme :

$$\begin{aligned} Mx_{k+1} &= Mx_k + h\theta f(x_{k+1}, t_{k+1}) + h(1-\theta)f(x_k, t_k) + h\gamma r(t_{k+1}) + h(1-\gamma)r(t_k) \\ y_{k+1} &= h(t_{k+1}, x_{k+1}) \\ r_{k+1} &= g(t_{k+1}, \lambda_{k+1}) \end{aligned} \quad (9.45) \quad \{\text{eq:mlcp3-toto1-l}\}$$

The previous derivation is valid with  $D_{k+1}^\alpha = 0$ .

### 9.3.3 Time-discretization of the linear case (9.4)

Let us now proceed with the time discretization of (9.5) with FirstOrderLinearR (9.4) by a fully implicit scheme :

$$\begin{aligned} Mx_{k+1}^{\alpha+1} &= Mx_k + h\theta Ax_{k+1}^{\alpha+1} + h(1-\theta)Ax_k + h\gamma r_{k+1}^{\alpha+1} + h(1-\gamma)r(t_k) + hb \\ y_{k+1}^{\alpha+1} &= Cx_{k+1}^{\alpha+1} + D\lambda_{k+1}^{\alpha+1} + Fz + e \\ r_{k+1}^{\alpha+1} &= B\lambda_{k+1}^{\alpha+1} \end{aligned} \quad (9.46) \quad \{\text{eq:toto1-DS3}\}$$

$$\begin{aligned} R_{\text{free}} &= M(x_{k+1}^\alpha - x_k) - h\theta Ax_{k+1}^\alpha - h(1-\theta)Ax_k - hb_{k+1} \\ R_{\text{free}} &= W(x_{k+1}^\alpha - x_k) - hAx_k - hb_{k+1} \end{aligned}$$

**Resulting Newton step (only one step)** For the sake of simplicity, let us assume that  $\gamma = 1$

$$\begin{aligned} (M - h\theta A)x_{k+1}^{\alpha+1} &= Mx_k + h(1-\theta)Ax_k + hr_{k+1}^{\alpha+1} + hb \\ y_{k+1}^{\alpha+1} &= Cx_{k+1}^{\alpha+1} + D\lambda_{k+1}^{\alpha+1} + Fz + e \\ r_{k+1}^{\alpha+1} &= B\lambda_{k+1}^{\alpha+1} \end{aligned} \quad (9.47)$$

that lead to with:  $(M - h\theta A) = W$

$$\begin{aligned} x_{k+1}^{\alpha+1} &= W^{-1}(Mx_k + h(1-\theta)Ax_k + r_{k+1}^{\alpha+1} + hb) = x_{\text{free}} + W^{-1}(r_{k+1}^{\alpha+1}) \\ y_{k+1}^{\alpha+1} &= (D + hCW^{-1}B)\lambda_{k+1}^{\alpha+1} + Fz + CW^{-1}(Mx_k + h(1-\theta)Ax_k + hb) + e \end{aligned} \quad (9.48)$$

with  $x_{\text{free}} = x_{k+1}^\alpha + W^{-1}(-R_{\text{free}}) = x_{k+1}^\alpha - W^{-1}(W(x_{k+1}^\alpha - x_k) - hAx_k - hb_{k+1}) = W^{-1}(Mx_k + h(1-\theta)Ax_k + hb_{k+1})$

$$\begin{aligned} y_{k+1}^{\alpha+1} &= (D + hCW^{-1}B)\lambda_{k+1}^{\alpha+1} + Fz + Cx_{\text{free}} + e \\ r_{k+1}^{\alpha+1} &= B\lambda_{k+1}^{\alpha+1} \end{aligned} \quad (9.49)$$

**Coherence with previous formulation**

$$y_p = y_{k+1}^\alpha - \mathcal{R}_{yk+1}^\alpha + C_{k+1}^\alpha (x_p - x_{k+1}^\alpha) - D_{k+1}^\alpha \lambda_{k+1}^\alpha$$

$$y_p = Cx_k + D\lambda_k + C(\tilde{x}_{\text{free}}) - D\lambda_k + Fz + e$$

$$y_p = Cx_k + C(\tilde{x}_{\text{free}}) + Fz + e$$

$$y_p = Cx_k + C(\tilde{x}_{\text{free}}) + Fz + e$$

$$y_p = C(x_{\text{free}}) + Fz + e$$

## 9.4 Newton's linearization of (9.6)

In this section, we deal with only with the FirstOrderType2R case.

$$\begin{aligned} Mx_{k+1} &= Mx_k + h\theta f(x_{k+1}, t_{k+1}) + h(1 - \theta)f(x_k, t_k) + hr_{k+\gamma} \\ y_{k+\gamma} &= h(t_{k+\gamma}, x_{k+\gamma}, \lambda_{k+\gamma}) \\ r_{k+\gamma} &= g(t_{k+\gamma}, \lambda_{k+\gamma}) \end{aligned} \quad (9.50) \quad \{\text{eq:full-toto1-t}\}$$

**Newton's linearization of the first line of (9.50)** The first line of the problem (9.50) can be written under the form of a residue  $\mathcal{R}$  depending only on  $x_{k+1}$  and  $r_{k+\gamma}$  such that

$$\mathcal{R}(x_{k+1}, r_{k+\gamma}) = 0 \quad (9.51) \quad \{\text{eq:full-NL3}\}$$

with

$$\mathcal{R}(x, r) = M(x - x_k) - h\theta f(x, t_{k+1}) - h(1 - \theta)f(x_k, t_k) - hr.$$

The solution of this system of nonlinear equations is sought as a limit of the sequence  $\{x_{k+1}^\alpha, r_{k+\gamma}^\alpha\}_{\alpha \in \mathbb{N}}$  such that

$$\begin{cases} x_{k+1}^0 = x_k \\ r_{k+\gamma}^0 = (1 - \gamma)r_k + \gamma r_{k+1}^0 = r_k \\ \mathcal{R}_L(x_{k+1}^{\alpha+1}, r_{k+\gamma}^{\alpha+1}) = \mathcal{R}(x_{k+1}^\alpha, r_{k+\gamma}^\alpha) + [\nabla_x \mathcal{R}(x_{k+1}^\alpha, r_{k+\gamma}^\alpha)](x_{k+1}^{\alpha+1} - x_{k+1}^\alpha) + \\ \quad [\nabla_r \mathcal{R}(x_{k+1}^\alpha, r_{k+\gamma}^\alpha)](r_{k+\gamma}^{\alpha+1} - r_{k+\gamma}^\alpha) = 0 \end{cases} \quad (9.52) \quad \{\text{eq:full-NL7}\}$$

### 9.4.1 Redaction note V. ACARY

What about  $r_{k+\gamma}^0$  ?

The residu free is also defined (useful for implementation only):

$$\mathcal{R}_{\text{free}}(x) \triangleq M(x - x_k) - h\theta f(x, t_{k+1}) - h(1 - \theta)f(x_k, t_k).$$

We get

$$\mathcal{R}(x_{k+1}^\alpha, r_{k+\gamma}^\alpha) = \boxed{\mathcal{R}_{k+1}^\alpha \triangleq \mathcal{R}_{\text{free}}(x_{k+1}^\alpha) - hr_{k+\gamma}^\alpha} \quad (9.53) \quad \{\text{eq:full-rfree-1}\}$$

$$\mathcal{R}_{\text{free}}(x_{k+1}^\alpha) = \boxed{\mathcal{R}_{\text{free},k+1}^\alpha \triangleq M(x_{k+1}^\alpha - x_k) - h\theta f(x_{k+1}^\alpha, t_{k+1}) - h(1 - \theta)f(x_k, t_k)}$$

The computation of the Jacobian of  $\mathcal{R}$  with respect to  $x$ , denoted by  $W_{k+1}^\alpha$  leads to

$$W_{k+1}^\alpha \triangleq \nabla_x \mathcal{R}(x_{k+1}^\alpha) = M - h\theta \nabla_x f(x_{k+1}^\alpha, t_{k+1}). \quad (9.54) \quad \{\text{eq:full-NL9}\}$$

At each time-step, we have to solve the following linearized problem,

$$\mathcal{R}_{k+1}^\alpha + W_{k+1}^\alpha(x_{k+1}^{\alpha+1} - x_{k+1}^\alpha) - h(r_{k+\gamma}^{\alpha+1} - r_{k+\gamma}^\alpha) = 0, \quad (9.55) \quad \{\text{eq:full-NL10}\}$$

By using (9.53), we get

$$\mathcal{R}_{\text{free}}(x_{k+1}^\alpha) - hr_{k+\gamma}^{\alpha+1} + W_{k+1}^\alpha(x_{k+1}^{\alpha+1} - x_{k+1}^\alpha) = 0 \quad (9.56) \quad \{\text{eq:full-rfree-2}\}$$

$$x_{k+1}^{\alpha+1} = h(W_{k+1}^{\alpha})^{-1} r_{\gamma+1}^{\alpha+1} + x_{\text{free}}^{\alpha} \quad (9.57)$$

with :

$$x_{\text{free}}^{\alpha} \triangleq x_{k+1}^{\alpha} - (W_{k+1}^{\alpha})^{-1} \mathcal{R}_{\text{free},k+1}^{\alpha} \quad (9.58) \quad \{\text{eq:full-rfree-1}\}$$

The matrix  $W$  is clearly non singular for small  $h$ .

Note that the linearization is equivalent to the case (9.14) and (9.28) with  $\gamma = 1$  and replacing  $r_{k+1}$  by  $r_{k+\gamma}$ .

**Newton's linearization of the second line of (9.50)** The same operation is performed with the second equation of (9.50)

$$\mathcal{R}_y(x, y, \lambda) = y - h(t_{k+\gamma}, \gamma x + (1 - \gamma)x_k, \lambda) = 0 \quad (9.59)$$

which is linearized as

$$\begin{aligned} \mathcal{R}_{Ly}(x_{k+1}^{\alpha+1}, y_{k+\gamma}^{\alpha+1}, \lambda_{k+\gamma}^{\alpha+1}) &= \mathcal{R}_y(x_{k+1}^{\alpha}, y_{k+\gamma}^{\alpha}, \lambda_{k+\gamma}^{\alpha}) + (y_{k+\gamma}^{\alpha+1} - y_{k+\gamma}^{\alpha}) - \\ &\quad \gamma C_{k+1}^{\alpha} (x_{k+1}^{\alpha+1} - x_{k+1}^{\alpha}) - D_{k+\gamma}^{\alpha} (\lambda_{k+\gamma}^{\alpha+1} - \lambda_{k+\gamma}^{\alpha}) = 0 \end{aligned} \quad (9.60) \quad \{\text{eq:full-NL9}\}$$

This leads to the following linear equation

$$y_{k+\gamma}^{\alpha+1} = y_{k+\gamma}^{\alpha} - \mathcal{R}_{y,k+1}^{\alpha} + \gamma C_{k+1}^{\alpha} (x_{k+1}^{\alpha+1} - x_{k+1}^{\alpha}) + D_{k+\gamma}^{\alpha} (\lambda_{k+\gamma}^{\alpha+1} - \lambda_{k+\gamma}^{\alpha}) \quad (9.61) \quad \{\text{eq:full-NL11y}\}$$

with,

$$C_{k+\gamma}^{\alpha} = \nabla_x h(t_{k+1}, x_{k+\gamma}^{\alpha}, \lambda_{k+\gamma}^{\alpha}) \quad (9.62)$$

$$D_{k+\gamma}^{\alpha} = \nabla_{\lambda} h(t_{k+1}, x_{k+\gamma}^{\alpha}, \lambda_{k+\gamma}^{\alpha})$$

and

$$\mathcal{R}_{y,k+1}^{\alpha} \triangleq y_{k+\gamma}^{\alpha} - h(x_{k+\gamma}^{\alpha}, \lambda_{k+\gamma}^{\alpha}) \quad (9.63)$$

Note that the linearization is equivalent to the case (9.17) by replacing  $\lambda_{k+1}$  by  $\lambda_{k+\gamma}$  and  $x_{k+1}$  by  $x_{k+\gamma}$ .

**Newton's linearization of the third line of (9.50)** The same operation is performed with the third equation of (9.50)

$$\mathcal{R}_r(r, \lambda) = r - g(\lambda, t_{k+1}) = 0 \quad (9.64)$$

which is linearized as

$$\mathcal{R}_{L\lambda}(r_{k+\gamma}^{\alpha+1}, \lambda_{k+\gamma}^{\alpha+1}) = \mathcal{R}_{r,k+\gamma}^{\alpha} + (r_{k+\gamma}^{\alpha+1} - r_{k+\gamma}^{\alpha}) - B_{k+\gamma}^{\alpha} (\lambda_{k+\gamma}^{\alpha+1} - \lambda_{k+\gamma}^{\alpha}) = 0 \quad (9.65) \quad \{\text{eq:full-NL9}\}$$

$$r_{k+\gamma}^{\alpha+1} = g(\lambda_{k+\gamma}^{\alpha}, t_{k+\gamma}) - B_{k+\gamma}^{\alpha} \lambda_{k+\gamma}^{\alpha} + B_{k+\gamma}^{\alpha} \lambda_{k+\gamma}^{\alpha+1} \quad (9.66) \quad \{\text{eq:full-rrL}\}$$

with,

$$B_{k+\gamma}^\alpha = \nabla_\lambda g(\lambda_{k+\gamma}^\alpha, t_{k+\gamma}) \quad (9.67)$$

and the residue for  $r$ :

$$\mathcal{R}_{rk+\gamma}^\alpha = r_{k+\gamma}^\alpha - g(\lambda_{k+\gamma}^\alpha, t_{k+\gamma}) \quad (9.68)$$

Note that the linearization is equivalent to the case (9.22) by replacing  $\lambda_{k+1}$  by  $\lambda_{k+\gamma}$  and  $x_{k+1}$  by  $x_{k+\gamma}$ .

**Reduction to a linear relation between  $x_{k+1}^{\alpha+1}$  and  $\lambda_{k+\gamma}^{\alpha+1}$**  Inserting (9.66) into (9.58), we get the following linear relation between  $x_{k+1}^{\alpha+1}$  and  $\lambda_{k+1}^\alpha$ ,

$$x_{k+1}^{\alpha+1} = h(W_{k+1}^\alpha)^{-1} \left[ g(\lambda_{k+\gamma}^\alpha, t_{k+\gamma}) + B_{k+\gamma}^\alpha (\lambda_{k+\gamma}^{\alpha+1} - \lambda_{k+\gamma}^\alpha) \right] + x_{free}^\alpha \quad (9.69)$$

that is

$$x_{k+1}^{\alpha+1} = x_p + h(W_{k+1}^\alpha)^{-1} B_{k+\gamma}^\alpha \lambda_{k+\gamma}^{\alpha+1} \quad (9.70) \quad \{\text{eq:full-rfree-1}\}$$

with

$$x_p \triangleq h(W_{k+1}^\alpha)^{-1} \left[ g(\lambda_{k+\gamma}^\alpha, t_{k+\gamma}) - B_{k+\gamma}^\alpha (\lambda_{k+\gamma}^\alpha) \right] + x_{free}^\alpha \quad (9.71)$$

**Reduction to a linear relation between  $y_{k+1}^{\alpha+1}$  and  $\lambda_{k+\gamma}^{\alpha+1}$**  Inserting (9.70) into (9.61), we get the following linear relation between  $y_{k+1}^{\alpha+1}$  and  $\lambda_{k+1}^\alpha$ ,

$$y_{k+1}^{\alpha+1} = y_p + \left[ h\gamma C_{k+\gamma}^\alpha (W_{k+1}^\alpha)^{-1} B_{k+1}^\alpha + D_{k+1}^\alpha \right] \lambda_{k+1}^{\alpha+1} \quad (9.72)$$

with

$$y_p = y_{k+1}^\alpha - \mathcal{R}_{yk+1}^\alpha + \gamma C_{k+1}^\alpha (x_q) - D_{k+1}^\alpha \lambda_{k+1}^\alpha \quad (9.73)$$

that is

$$y_p = h(x_{k+\gamma}^\alpha, \lambda_{k+\gamma}^\alpha) + \gamma C_{k+1}^\alpha (x_q) - D_{k+1}^\alpha \lambda_{k+1}^\alpha \quad (9.74)$$

$$x_q = (x_p - x_{k+1}^\alpha) \quad (9.75) \quad \{\text{eq:full-xqq}\}$$

**The linear case**

$$\begin{aligned} y_p &= h(x_{k+\gamma}^\alpha, \lambda_{k+\gamma}^\alpha) + \gamma C_{k+1}^\alpha (x_q) - D_{k+1}^\alpha \lambda_{k+1}^\alpha \\ &= C_{k+1}^\alpha x_{k+\gamma}^\alpha + D_{k+1}^\alpha \lambda_{k+\gamma}^\alpha + \gamma C_{k+1}^\alpha (x_q) - D_{k+1}^\alpha \lambda_{k+1}^\alpha \\ &= C_{k+1}^\alpha (x_{k+\gamma}^\alpha + \gamma x_p - \gamma x_{k+1}^\alpha) \\ &= C_{k+1}^\alpha ((1-\gamma)x_k + \gamma x_{free}) \text{ since } x_p = x_{free} \end{aligned} \quad (9.76)$$

**Implementation details** For the moment (Feb. 2011), we set  $x_q = (1 - \gamma)x_k + \gamma x_{free}$  in the linear case. The nonlinear case is not yet implemented since we need to change the management of `H_alpha` in `Relation` to be able to compute the mid-point values. things that remain to do

- implement the function `BlockVector compute_g(t,lambda)` and `SimpleVector compute_h(t,x,lambda)` which takes into account the values of the argument and return a vector
- remove temporary computation in `Relation` of `Xq`, `g_alpha` and `H_alpha`. This should be stored somewhere else. (in the node of the graph)



## Chapter 10

# Newton's linearization for Lagrangian systems

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date	Sept, 20, 2011
version	

This section is devoted to the implementation and the study of the algorithm. The interval of integration is  $[0, T]$ ,  $T > 0$ , and a grid  $t_0 = 0$ ,  $t_{k+1} = t_k + h$ ,  $k \geq 0$ ,  $t_N = T$  is constructed. The approximation of a function  $f(\cdot)$  on  $[0, T]$  is denoted as  $f^N(\cdot)$ , and is a piecewise constant function, constant on the intervals  $[t_k, t_{k+1})$ . We denote  $f^N(t_k)$  as  $f_k$ . The time-step is  $h > 0$ .

### 10.1 Various second order dynamical systems with input/output relations

#### 10.1.1 Lagrangian dynamical systems

The class `LagrangianDS` defines and computes a generic `ndof`-dimensional Lagrangian Non Linear Dynamical System of the form :

$$\begin{cases} M(q, z)\ddot{v} + N(v, q, z) + F_{Int}(v, q, t, z) = F_{Ext}(t, z) + p \\ \dot{q} = v \end{cases} \quad (10.1)$$

where

- $q \in R^{ndof}$  is the set of the generalized coordinates,
- $\dot{q} = v \in R^{ndof}$  the velocity, i. e. the time derivative of the generalized coordinates (Lagrangian systems).
- $\ddot{q} = \ddot{v} \in R^{ndof}$  the acceleration, i. e. the second time derivative of the generalized coordinates.
- $p \in R^{ndof}$  the reaction forces due to the Non Smooth Interaction.
- $M(q) \in R^{ndof \times ndof}$  is the inertia term saved in the `SiconosMatrix` mass.
- $N(\dot{q}, q) \in R^{ndof}$  is the non linear inertia term saved in the `SiconosVector` `_NNL`.
- $F_{Int}(\dot{q}, q, t) \in R^{ndof}$  are the internal forces saved in the `SiconosVector` `fInt`.

- $F_{Ext}(t) \in \mathbb{R}^{ndof}$  are the external forces saved in the SiconosVector fExt.
- $z \in \mathbb{R}^{zSize}$  is a vector of arbitrary algebraic variables, some sort of discrete state.

The equation of motion is also shortly denoted as:

$$M(q, z)\dot{v} = F(v, q, t, z) + p \quad (10.2)$$

where  $F(v, q, t, z) \in \mathbb{R}^{ndof}$  collects the total forces acting on the system, that is

$$F(v, q, t, z) = F_{Ext}(t, z) - NNL(v, q, z) + F_{Int}(v, q, t, z) \quad (10.3)$$

This vector is stored in the SiconosVector `_Forces`

### 10.1.2 Fully nonlinear case

Let us introduce the following system,

$$\begin{cases} M(q, z)\dot{v} = F(v, q, t, z) + p \\ \dot{q} = v \\ y = h(t, q, \lambda) \\ p = g(t, q, \lambda) \end{cases} \quad (10.4) \quad \{\text{eq:FullyNonLinear}\}$$

where  $\lambda(t) \in \mathbb{R}^m$  and  $y(t) \in \mathbb{R}^m$  are complementary variables related through a multi-valued mapping. According to the class of systems, we are studying, the function  $F$ ,  $h$  and  $g$  are defined by a fully nonlinear framework or by affine functions. This fully nonlinear case is not implemented in Siconos yet. This fully general case is not yet implemented in Siconos.

### 10.1.3 Lagrangian Rheonomous relations

$$\begin{cases} M(q, z)\dot{v} = F(v, q, t, z) + p \\ \dot{q} = v \\ y = h(t, q) \\ p = G(t, q)\lambda \end{cases} \quad (10.5) \quad \{\text{eq:RheonomousNonLinear}\}$$

### 10.1.4 Lagrangian Scleronomous relations

$$\begin{cases} M(q, z)\dot{v} = F(v, q, t, z) + p \\ \dot{q} = v \\ y = h(q) \\ p = G(q)\lambda \end{cases} \quad (10.6) \quad \{\text{eq:ScleronomousNonLinear}\}$$

#### Fully Linear case

$$\begin{cases} M\dot{v} + Cv + Kq = F_{Ext}(t, z) + p \\ \dot{q} = v \\ y = Cq + e + D\lambda + Fz \\ p = C^T\lambda \end{cases} \quad (10.7) \quad \{\text{eq:FullyLinear}\}$$

## 10.2 Moreau's Time-discretizations

### 10.3 Schatzman-Paoli 'scheme and its linearizations

#### 10.3.1 The scheme

$$\left\{ \begin{array}{l} M(q_k)(q_{k+1} - 2q_k + q_{k-1}) - h^2 F(v_{k+\theta}, q_{k+\theta}, t_{k+\theta}) = p_{k+1}, \end{array} \right. \quad (10.8a)$$

$$v_{k+1} = \frac{q_{k+1} - q_{k-1}}{2h}, \quad (10.8b)$$

$$y_{k+1} = h \left( \frac{q_{k+1} + eq_{k-1}}{1+e} \right) \quad (10.8c)$$

$$p_{k+1} = G \left( \frac{q_{k+1} + eq_{k-1}}{1+e} \right) \lambda_{k+1} \quad (10.8d)$$

$$0 \leq y_{k+1} \perp \lambda_{k+1} \geq 0. \quad (10.8e)$$

10.3.1 Redaction note V. ACARY

Should we have

$$v_{k+1} = \frac{q_{k+1} - q_{k-1}}{2h}$$

or

$$v_{k+1} = \frac{q_{k+1} - q_k}{h}$$

? This question is particularly important for the initialization and the proposed  $\theta$ -scheme

#### 10.3.2 The Newton linearization

Let us define the residu on  $q$

$$\mathcal{R}(q) = M(q)(q - 2q_k + q_{k-1}) + h^2 F((\theta v(q) + (1 - \theta)v_k), \theta q + (1 - \theta)q_k, t_{k+\theta}) - p_{k+1} \quad (10.9) \quad \{\text{eq:residu}\}$$

with

$$v(q) = \frac{q - q_{k-1}}{2h} \quad (10.10) \quad \{\text{eq:residu-linq1}\}$$

that is

$$\mathcal{R}(q) = M(q)(q - 2q_k + q_{k-1}) + h^2 F((\theta \frac{q - q_{k-1}}{2h} + (1 - \theta)v_k), \theta q + (1 - \theta)q_k, t_{k+\theta}) - p_{k+1} \quad (10.11) \quad \{\text{eq:residu-linq2}\}$$

Neglecting  $\nabla_q M(q)$  we get

$$\nabla_q \mathcal{R}(q^\nu) = M(q^\nu) + h^2 \theta K(q^\nu, v^\nu) + \frac{1}{2} h \theta C(q^\nu, v^\nu) \quad (10.12) \quad \{\text{eq:iterationmat}\}$$

and we have to solve

$$\nabla_q \mathcal{R}(q^\nu)(q^{\nu+1} - q^\nu) = -\mathcal{R}(q^\nu). \quad (10.13) \quad \{\text{eq:iterationloop}\}$$

### 10.3.3 Linear version of the scheme

$$\begin{cases} M(q_{k+1} - 2q_k + q_{k-1}) + h^2(Kq_{k+\theta} + Cv_{k+\theta}) = p_{k+1}, \end{cases} \quad (10.14a)$$

$$\begin{cases} v_{k+1} = \frac{q_{k+1} - q_{k-1}}{2h}, \end{cases} \quad (10.14b)$$

$$\begin{cases} y_{k+1} = h \left( \frac{q_{k+1} + eq_{k-1}}{1+e} \right) \end{cases} \quad (10.14c)$$

$$\begin{cases} p_{k+1} = G \left( \frac{q_{k+1} + eq_{k-1}}{1+e} \right) \lambda_{k+1} \end{cases} \quad (10.14d)$$

$$\begin{cases} 0 \leq y_{k+1} \perp \lambda_{k+1} \geq 0. \end{cases} \quad (10.14e)$$

Let us define the residu on  $q$

$$\mathcal{R}(q) = M(q - 2q_k + q_{k-1}) + h^2(K(\theta q + (1 - \theta)q_k)) + C(\theta v(q) + (1 - \theta)v_k)) - p_{k+1} \quad (10.15) \quad \{\text{eq:residu-linq}\}$$

with

$$v(q) = \frac{q - q_{k-1}}{2h} \quad (10.16) \quad \{\text{eq:residu-linq1}\}$$

that is

$$\mathcal{R}(q) = M(q - 2q_k + q_{k-1}) + h^2(K(\theta q + (1 - \theta)q_k)) + h^2C(\theta \frac{q - q_{k-1}}{2h} + (1 - \theta)v_k)) - p_{k+1} \quad (10.17) \quad \{\text{eq:residu-linq2}\}$$

In this linear case, assuming that  $q^0 = q^\vee = q_k$ , we get

$$\mathcal{R}(q^\vee) = M(-q_k + q_{k-1}) + h^2(Kq_k) + h^2C(\theta \frac{q_k - q_{k-1}}{2h} + (1 - \theta)v_k)) - p_{k+1} \quad (10.18) \quad \{\text{eq:residu-linq2}\}$$

## 10.4 What about mixing OnestepIntegrator in Simulation?

Let us consider that we have two simple linear Lagrangian Dynamical systems

{Sec:MissingOSI}

$$\begin{cases} M_1 \dot{v}_1 = F_{1,Ext}(t) + p_1 \\ \dot{q}_1 = v_1 \end{cases} \quad (10.19) \quad \{\text{eq:FullyLinear1}\}$$

and

$$\begin{cases} M_2 \dot{v}_2 = F_{2,Ext}(t) + p_2 \\ \dot{q}_2 = v_2 \end{cases} \quad (10.20) \quad \{\text{eq:FullyLinear1}\}$$

These Dynamical systems (10.20) and (10.20) might numerically solved by choosing two different time-stepping schemes. Let us choose for instance Moreau's scheme for(10.20)

$$\begin{cases} M_1(v_{1,k+1} - v_{1,k}) = F_{1,Ext}(t_{k+1}) + p_{1,k+1} \\ q_{1,k+1} = q_k + hv_{1,k+\theta} \end{cases} \quad (10.21) \quad \{\text{eq:FullyLinear1}\}$$

and Schatzman–Paoli's sheme for (10.20)

$$\begin{cases} M_2(q_{2,k+1} - 2q_{2,k} + q_{2,k-1}) = F_{2,Ext}(t_{k+1}) + p_{2,k+1} \\ v_{2,k+1} = \frac{q_{2,k+1} - q_{2,k-1}}{2h} \end{cases} \quad (10.22) \quad \{\text{eq:FullyLinear1}\}$$

Let us consider known that we have a LagrangianLinearTIR between this two DSs such that

$$y = q_1 - q_2 \geq 0$$

$$p = \begin{bmatrix} 1 \\ -1 \end{bmatrix} \lambda \quad (10.23) \quad \{\text{eq:LTIR-2DS}\}$$

and a complementarity condition

$$0 \leq y \perp \lambda \geq 0 \quad (10.24) \quad \{\text{eq:CP}\}$$

Many questions are raised when we want to deal with the discrete systems:

- Which rules should we use for the discretization of (10.24) ?

$$\text{if } \bar{y}_{k+1} \leq 0, \text{ then } 0 \leq \dot{y}_{k+1} + e\dot{y}_k \perp \hat{\lambda}_{k+1} \geq 0 \quad (10.25) \quad \{\text{eq:CP-TS1}\}$$

or

$$0 \leq y_{k+1} + ey_{k-1} \perp \tilde{\lambda}_{k+1} \geq 0 \quad (10.26) \quad \{\text{eq:CP-TS2}\}$$

- Should we assume that  $y_{k+1} = q_{1,k+1} - q_{2,k+1}$  and  $\dot{y}_{k+1} = v_{1,k+1} - v_{2,k+1}$
- How can we link  $\hat{\lambda}_{k+1}$  and  $\tilde{\lambda}_{k+1}$  with  $p_{1,k+1}$  and  $p_{2,k+1}$  ?

The third is the more difficult question and it seems that it is not reasonable to deal with two DS related by one interaction with different osi. In practice, this should be avoided in Siconos.

# Chapter 11

## NewtonEuler Dynamical Systems

Author	O. Bonnefon	2010
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Revision	section ?? V. Acary	01/06/2016
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### 11.1 The equations of motion

In the maximal coordinates framework, the most natural choice for the kinematic variables and for the formulation of the equations of motion is the Newton/Euler formalism, where the equation of motion describes the translational and rotational dynamics of each body using a specific choice of parameters. For the translational motion, the position of the center of mass  $x_g \in \mathbb{R}^3$  and its velocity  $v_g = \dot{x}_g \in \mathbb{R}^3$  is usually chosen. For the orientation of the body is usually defined by the rotation matrix  $R$  of the body-fixed frame with respect to a given inertial frame.

For the rotational motion, a common choice is to choose the rotational velocity  $\Omega \in \mathbb{R}^3$  of the body expressed in the body-fixed frame. This choice comes from the formulation of a rigid body motion of a point  $X$  in the inertial frame as

$$x(t) = \Phi(t, X) = x_g(t) + R(t)X. \quad (11.1) \quad \{\text{eq:1}\}$$

The velocity of this point can be written as

$$\dot{x}(t) = v_g(t) + \dot{R}(t)X \quad (11.2) \quad \{\text{eq:2}\}$$

Since  $R^\top R = I$ , we get  $R^\top \dot{R} + \dot{R}^\top R = 0$ . We can conclude that it exists a matrix  $\tilde{\Omega} := R^\top \dot{R}$  such that  $\tilde{\Omega} + \tilde{\Omega}^\top = 0$ , i.e. a skew symmetric matrix. The notation  $\tilde{\Omega}$  comes from the fact that there is a bijection between the skew symmetric matrix in  $\mathbb{R}^{3 \times 3}$  and  $\mathbb{R}^3$  such that

$$\tilde{\Omega}x = \Omega \times x, \quad \forall x \in \mathbb{R}^3. \quad (11.3) \quad \{\text{eq:3}\}$$

The rotational velocity is then related to the  $R$  by :

$$\tilde{\Omega} = R^\top \dot{R}, \text{ or equivalently, } \dot{R} = R\tilde{\Omega} \quad (11.4) \quad \{\text{eq:angularveloc}\}$$

Using these coordinates, the equations of motion are given by

$$\begin{cases} m \dot{v}_g &= f(t, x_g, v_g, R, \Omega) \\ I \dot{\Omega} + \Omega \times I \Omega &= M(t, x_g, v_g, R, \Omega) \\ \dot{x}_g &= v_g \\ \dot{R} &= R\tilde{\Omega} \end{cases} \quad (11.5) \quad \{\text{eq:motion-Newton}\}$$

where  $m > 0$  is the mass,  $I \in \mathbb{R}^{3 \times 3}$  is the matrix of moments of inertia around the center of mass and the axis of the body-fixed frame.

The vectors  $f(\cdot) \in \mathbb{R}^3$  and  $M(\cdot) \in \mathbb{R}^3$  are the total forces and torques applied to the body. It is important to outline that the total applied forces  $f(\cdot)$  has to be expressed in a consistent frame w.r.t. to  $v_g$ . In our case, it has to be expressed in the inertial frame. The same applies for the moment  $M$  that has to be expressed in the body-fixed frame. If we consider a moment  $m(\cdot)$  expressed in the inertial frame, then it has to be convected to the body-fixed frame thanks to

$$M(\cdot) = R^\top m(\cdot) \quad (11.6) \quad \{\text{eq:convected\_mom}\}$$

**Remark 1** If we perform the time derivation of  $RR^\top = I$  rather than  $R^\top R = I$ , we get  $R\dot{R}^\top + \dot{R}R^\top = 0$ . We can conclude that it exists a matrix  $\tilde{\omega} := \dot{R}R^\top$  such that  $\tilde{\omega} + \tilde{\omega}^\top = 0$ , i.e. a skew symmetric matrix. Clearly, we have

$$\tilde{\omega} = R\tilde{\Omega}R^\top \quad (11.7) \quad \{\text{eq:4}\}$$

and it can be proved that is equivalent to  $\omega = R\Omega$ . The vector  $\omega$  is the rotational velocity expressed in the inertial frame. The equation of motion can also be expressed in the inertial frame as follows

$$\left\{ \begin{array}{lcl} m \dot{v}_g & = & f(t, x_g, v_g, R, R^\top \omega) \\ J(R)\dot{\omega} + \omega \times J(R)\omega & = & m(t, x_g, v_g, R, \omega) \\ \dot{x}_g & = & v_g \\ \dot{R} & = & \tilde{\omega}R \end{array} \right. \quad (11.8) \quad \{\text{eq:motion-Newton}\}$$

where the matrix  $J(R) = RIR^\top$  is the inertia matrix in the inertial frame. Defining the angular momentum with respect to the inertial frame as

$$\pi(t) = J(R(t))\omega(t) \quad (11.9) \quad \{\text{eq:1}\}$$

the equation of the angular motion is derived from the balance equation of the angular momentum

$$\dot{\pi}(t) = m(t, x_g, v_g, R, \omega). \quad (11.10) \quad \{\text{eq:5}\}$$

For a given constant (time invariant)  $\tilde{\Omega}$ , let us consider the differential equation

$$\left\{ \begin{array}{l} \dot{R}(t) = R\tilde{\Omega} \\ R(0) = I \end{array} \right. \quad (11.11) \quad \{\text{eq:5}\}$$

Let us recall the definition of the matrix exponential,

$$\exp(A) = \sum_{k=0}^{\infty} \frac{1}{k!} A^k \quad (11.12) \quad \{\text{eq:6}\}$$

A trivial solution of (11.11) is  $R(t) = \exp(t\tilde{\Omega})$  since

$$\frac{d}{dt}(\exp(At)) = \exp(At)A. \quad (11.13) \quad \{\text{eq:7}\}$$

More generally, with the initial condition  $R(t_0) = R_0$ , we get the solution

$$R(t) = R_0 \exp((t - t_0)\tilde{\Omega}) \quad (11.14) \quad \{\text{eq:8}\}$$

Another interpretation is as follows. From a (incremental) rotation vector,  $\Omega$  and its associated matrix  $\tilde{\Omega}$ , we obtain a rotation matrix by the exponentiation of  $\tilde{\Omega}$ :

$$R = \exp(\tilde{\Omega}). \quad (11.15) \quad \{\text{eq:9}\}$$

Since we note that  $\tilde{\Omega}^3 = -\theta^2 \tilde{\Omega}$  with  $\theta = \|\Omega\|$ , it is possible to get a closed form of the matrix exponential of  $\tilde{\Omega}$

$$\begin{aligned} \exp(\tilde{\Omega}) &= \sum_{k=0}^{\infty} \frac{1}{k!} (\tilde{\Omega})^k \\ &= I_{3 \times 3} + \sum_{k=1}^{\infty} \frac{(-1)^{k-1}}{(2k-1)!} \theta^{2k-1} \tilde{\Omega} + \left( \sum_{k=0}^{\infty} \frac{(-1)^{k-1}}{(2k)!} \theta^{2k-2} \tilde{\Omega}^2 \right) \\ &= I_{3 \times 3} + \frac{\sin \theta}{\theta} \tilde{\Omega} + \frac{(\cos \theta - 1)}{\theta^2} \tilde{\Omega}^2 \end{aligned} \quad (11.16) \quad \{\text{eq:10}\}$$

that is

$$R = I_{3 \times 3} + \frac{\sin \theta}{\theta} \tilde{\Omega} + \frac{(\cos \theta - 1)}{\theta^2} \tilde{\Omega}^2 \quad (11.17) \quad \{\text{eq:11}\}$$

The formula (11.17) is the Euler–Rodrigues formula that allows to compute the rotation matrix on closed form.

#### 11.1.1.1 Redaction note V. ACARY

todo :

- add the formulation in the inertial frame of the Euler equation with  $\omega = R\Omega$ .
- Check that (11.16) is the Euler-Rodrigues formula and not the Olinde Rodrigues formula. (division by  $\theta$ )

In the numerical practice, the choice of the rotation matrix is not convenient since it introduces redundant parameters. Since  $R$  must belong to  $SO^+(3)$ , we have also to satisfy  $\det(R) = 1$  and  $R^{-1} = R^\top$ . In general, we use a reduced vector of parameters  $p \in \mathbb{R}^{n_p}$  such  $R = \Phi(p)$  and  $\dot{p} = \psi(p)\Omega$ . We denote by  $q$  the vector of coordinates of the position and the orientation of the body, and by  $v$  the body twist:

$$q := \begin{bmatrix} x_g \\ p \end{bmatrix}, \quad v := \begin{bmatrix} v_g \\ \Omega \end{bmatrix}. \quad (11.18)$$

The relation between  $v$  and the time derivative of  $q$  is

$$\dot{q} = \begin{bmatrix} \dot{x}_g \\ \psi(p)\dot{p} \end{bmatrix} = \begin{bmatrix} I & 0 \\ 0 & \psi(p) \end{bmatrix} v := T(q)v \quad (11.19) \quad \{\text{eq:TT}\}$$

with  $T(q) \in \mathbb{R}^{3+n_p \times 6}$ . Note that the twist  $v$  is not directly the time derivative of the coordinate vector as a major difference with Lagrangian systems.

The Newton-Euler equation in compact form may be written as:

$$\boxed{\begin{cases} \dot{q} = T(q)v, \\ M\dot{v} = F(t, q, v) \end{cases}} \quad (11.20) \quad \{\text{eq:Newton-Euler}\}$$

where  $M \in \mathbb{R}^{6 \times 6}$  is the total inertia matrix

$$M := \begin{pmatrix} mI_{3 \times 3} & 0 \\ 0 & I \end{pmatrix}, \quad (11.21)$$

and  $F(t, q, v) \in \mathbb{R}^6$  collects all the forces and torques applied to the body

$$F(t, q, v) := \begin{pmatrix} f(t, x_g, v_g, R, \Omega) \\ I\Omega \times \Omega + M(t, x_g, v_g, R, \Omega) \end{pmatrix}. \quad (11.22)$$

When a collection of bodies is considered, we will use the same notation as in (11.20) extending the definition of the variables  $q, v$  and the operators  $M, F$  in a straightforward way.

## 11.2 Basic elements of Lie groups and Lie algebras theory.

Let us recall the definitions of the Lie group Theory taken from [2] and [4].



### 11.2.1 Differential equation (evolving) on a manifold $\mathcal{M}$

**Definition 2** A  $d$ -dimensional manifold  $\mathcal{M}$  is a  $d$ -dimensional smooth surface  $M \subset \mathbb{R}^n$  for some  $n \geq d$ .

**Definition 3** Let  $\mathcal{M}$  be a  $d$ -dimensional manifold and suppose that  $\rho(t) \in \mathcal{M}$  is a smooth curve such that  $\rho(0) = p$ . A tangent vector at  $p$  is defined as

$$a = \left. \frac{d}{dt}(\rho(t)) \right|_{t=0}. \quad (11.23) \quad \{\text{eq:12}\}$$

The set of all tangents at  $p$  is called the tangent space at  $p$  and denoted by  $T\mathcal{M}|_p$ . It has the structure of a linear space.

**Definition 4** A (tangent) vector field on  $\mathcal{M}$  is a smooth function  $F : \mathcal{M} \rightarrow T\mathcal{M}$  such that  $F(p) \in T\mathcal{M}|_p$  for all  $p \in \mathcal{M}$ . The collection of all vector fields on  $\mathcal{M}$  is denoted by  $\mathcal{X}(\mathcal{M})$ .

**Definition 5 (Differential equation (evolving) on  $\mathcal{M}$ )** Let  $F$  be a tangent vector field on  $\mathcal{M}$ . By a differential equation (evolving) on  $\mathcal{M}$  we mean a differential equation of the form

$$\dot{y} = F(y), t \geq 0, y(0) \in \mathcal{M} \quad (11.24) \quad \{\text{eq:13}\}$$

where  $F \in \mathcal{X}(\mathcal{M})$ . Whenever convenient, we allow  $F$  in (11.24) to be a function of time,  $F = F(t, y)$ . The flow of  $F$  is the solution operator  $\Psi_{t,F} : \mathcal{M} \rightarrow \mathcal{M}$  such that

$$y(t) = \Psi_{t,F}(y(0)). \quad (11.25) \quad \{\text{eq:14}\}$$

### 11.2.2 Lie algebra and Lie group

**Definition 6 (commutator)** Given two vector fields  $F, G$  on  $\mathbb{R}^n$ , the commutator  $H = [F, G]$  can be computed componentwise at a given point  $y \in \mathbb{R}^n$  as

$$H_i(y) = \sum_{j=1}^n G_j(y) \frac{\partial F_i(y)}{\partial y_j} F_j(y) \frac{\partial G_i(y)}{\partial y_j}. \quad (11.26) \quad \{\text{eq:15}\}$$

**Lemma 1** The commutator of vector fields satisfies the identities

$$\begin{aligned} [F, G] &= [G, F] && \text{(skewsymmetry),} \\ [\alpha F, G] &= \alpha [F, G], \alpha \in \mathbb{R} \\ [F + G, H] &= [F, H] + [G, H] && \text{(bilinearity),} \\ 0 &= [F, [G, H]] + [G, [H, F]] + [H, [F, G]] && \text{(Jacobi identity).} \end{aligned} \quad (11.27) \quad \{\text{eq:16}\}$$

**Definition 7** A Lie algebra of vector fields is a collection of vector fields which is closed under linear combination and commutation. In other words, letting  $\mathfrak{g}$  denote the Lie algebra,

$$\begin{aligned} B \in \mathfrak{g} &\implies \alpha B \in \mathfrak{g} \text{ for all } \alpha \in \mathbb{R}. \\ B_1, B_2 \in \mathfrak{g} &\implies B_1 + B_2, [B_1, B_2] \in \mathfrak{g} \end{aligned} \quad (11.28) \quad \{\text{eq:17}\}$$

Given a collection of vector fields  $B = B_1, B_2, \dots$ , the least Lie algebra of vector fields containing  $B$  is called the Lie algebra generated by  $B$

**Definition 8** A Lie algebra is a linear space  $V$  equipped with a Lie bracket, a bilinear, skew-symmetric mapping

$$[\cdot, \cdot] : V \times V \rightarrow V \quad (11.29) \quad \{\text{eq:18}\}$$

that obeys identities (11.27) from Lemma 1

**Definition 9 ((General) Lie algebra)** A Lie algebra homomorphism is a linear map between two Lie algebras,  $\varphi : \mathfrak{g} \rightarrow \mathfrak{h}$ , satisfying the identity

$$\varphi([v, w]_{\mathfrak{g}}) = [\varphi(v), \varphi(w)]_{\mathfrak{h}}, v, w \text{ in } \mathfrak{g}. \quad (11.30) \quad \{\text{eq:19}\}$$

An invertible homomorphism is called an isomorphism.

**Definition 10** A Lie group is a differential manifold  $\mathcal{G}$  equipped with a product  $\cdot : \mathcal{G} \times \mathcal{G} \rightarrow \mathcal{G}$  satisfying

$$\begin{aligned} p \cdot (q \cdot r) &= (p \cdot q) \cdot r, \forall p, q, r \in \mathcal{G} && \text{(associativity)} \\ \exists I \in \mathcal{G} \text{ such that } I \cdot p &= p \cdot I = p, \forall p \in \mathcal{G} && \text{(identity element)} \\ \forall p \in \mathcal{G}, \exists p^{-1} \in \mathcal{G} \text{ such that } p^{-1} \cdot p &= I && \text{(inverse)} \\ \text{The maps } (p, r) \rightarrow p \cdot r \text{ and } p \rightarrow p^{-1} &\text{ are smooth functions} && \text{(smoothness)} \end{aligned} \quad (11.31) \quad \{\text{eq:20}\}$$

**Definition 11 (Lie algebra  $\mathfrak{g}$  of a Lie group  $\mathcal{G}$ )** The Lie algebra  $\mathfrak{g}$  of a Lie group  $\mathcal{G}$  is defined as the linear space of all tangents to  $\mathcal{G}$  at the identity  $I$ . The Lie bracket in  $\mathfrak{g}$  is defined as

$$[a, b] = \left. \frac{\partial^2}{\partial s \partial t} \rho(s) \sigma(t) \rho(-s) \right|_{s=t=0} \quad (11.32) \quad \{\text{eq:21}\}$$

where  $\rho(s)$  and  $\sigma(t)$  are two smooth curves on  $\mathcal{G}$  such that  $\rho(0) = \sigma(0) = I$ , and  $\dot{\rho}(0) = a$  and  $\dot{\sigma}(0) = b$ .

### 11.2.3 Actions of a group $\mathcal{G}$ on manifold $\mathcal{M}$

**Definition 12** A left action of Lie Group  $\mathcal{G}$  on a manifold  $\mathcal{M}$  is a smooth map  $\Lambda^l : \mathcal{G} \times \mathcal{M} \rightarrow \mathcal{M}$  satisfying

$$\begin{aligned} \Lambda^l(I, y) &= y, \quad \forall y \in \mathcal{M} \\ \Lambda^l(p, \Lambda(r, y)) &= \Lambda^l(p \cdot r, y), \quad \forall p, r \in \mathcal{G}, \quad \forall y \in \mathcal{M}. \end{aligned} \quad (11.33) \quad \{\text{eq:22}\}$$

**Definition 13** A right action of Lie Group  $\mathcal{G}$  on a manifold  $\mathcal{M}$  is a smooth map  $\Lambda^r : \mathcal{M} \times \mathcal{G} \rightarrow \mathcal{M}$  satisfying

$$\begin{aligned} \Lambda^r(y, I) &= y, \quad \forall y \in \mathcal{M} \\ \Lambda^r(\Lambda(y, r), p) &= \Lambda^r(y, r \cdot p), \quad \forall p, r \in \mathcal{G}, \quad \forall y \in \mathcal{M}. \end{aligned} \quad (11.34) \quad \{\text{eq:23}\}$$

A given smooth curve  $S(\cdot) : t \in \mathbf{R} \mapsto S(t) \in \mathcal{G}$  in  $\mathcal{G}$  such that  $S(0) = I$  produces a flow  $\Lambda^l(S(t), \cdot)$  (resp.  $\Lambda^r(\cdot, S(t))$ ) on  $\mathcal{M}$  and by differentiation we find a tangent vector field

$$F(y) = \left. \frac{d}{dt} (\Lambda^l(S(t), y)) \right|_{t=0} \quad (\text{resp. } F(y) = \left. \frac{d}{dt} (\Lambda^r(y, S(t))) \right|_{t=0}) \quad (11.35) \quad \{\text{eq:24}\}$$

that defines a ordinary differential equation on a Lie Group

$$\dot{y}(t) = F(y(t)) = \left. \frac{d}{dt} (\Lambda^l(S(t), y)) \right|_{t=0} \quad (\text{resp. } \dot{y}(t) = F(y(t)) = \left. \frac{d}{dt} (\Lambda^r(y, S(t))) \right|_{t=0}) \quad (11.36) \quad \{\text{eq:25}\}$$

**Lemma 2** Let  $\lambda_*^l : \mathfrak{g} \rightarrow \mathcal{X}(\mathcal{M})$  (resp.  $\lambda_*^r : \mathfrak{g} \rightarrow \mathcal{X}(\mathcal{M})$ ) be defined as

$$\lambda_*^l(a)(y) = \left. \frac{d}{ds} \Lambda^l(\rho(s), y) \right|_{s=0} \quad (\text{resp. } \lambda_*^r(a)(y) = \left. \frac{d}{ds} \Lambda^r(y, \rho(s)) \right|_{s=0}) \quad (11.37) \quad \{\text{eq:26}\}$$

where  $\rho(s)$  is a curve in  $\mathcal{G}$  such that  $\rho(0) = I$  and  $\dot{\rho}(0) = a$ . Then  $\lambda_g^l$  is a linear map between Lie algebras such that

$$[a, b]_{\mathfrak{g}} = [\lambda_*^l(a), \lambda_*^l(b)]_{\mathcal{X}(\mathcal{M})}. \quad (11.38) \quad \{\text{eq:27}\}$$

The following product between an element of an algebra  $a \in \mathfrak{g}$  with an element of a group  $\sigma \in \mathcal{G}$  can be defined. This will served as a basis for defining the exponential map.

**Definition 14** We define the left product  $(\cdot, \cdot)^l : \mathfrak{g} \times \mathcal{G} \rightarrow \mathcal{G}$  of an element of an algebra  $a \in \mathfrak{g}$  with an element of a group  $\sigma \in \mathcal{G}$  as

$$(a, \sigma)^l = a \cdot \sigma = \left. \frac{d}{ds} \rho(s) \cdot \sigma \right|_{s=0} \quad (11.39) \quad \{\text{eq:28}\}$$

where  $\rho(s)$  is a smooth curve such that  $\dot{\rho}(0) = a$  and  $\rho(0) = I$ . In the same way, we can define the right product  $(\cdot, \cdot)^r : \mathcal{G} \times \mathfrak{g} \rightarrow \mathcal{G}$

$$(\sigma, a)^r = \sigma \cdot a = \left. \frac{d}{ds} \sigma \cdot \rho(s) \right|_{s=0} \quad (11.40) \quad \{\text{eq:29}\}$$

### 11.2.4 Exponential map

**Definition 15** Let  $\mathcal{G}$  be a Lie group and  $\mathfrak{g}$  its Lie algebra. The exponential mapping  $\exp : \mathfrak{g} \rightarrow \mathcal{G}$  is defined as  $\exp(a) = \sigma(1)$  where  $\sigma(t)$  satisfies the differential equation

$$\dot{\sigma}(t) = a \cdot \sigma(t), \quad \sigma(0) = I. \quad (11.41) \quad \{\text{eq:30}\}$$

Let us define  $a^k$  as

$$\begin{cases} a^k = \underbrace{a \cdot a \cdot \dots \cdot a}_{k \text{ times}} \cdot a & \text{for } k \geq 1 \\ a^0 = I \end{cases} \quad (11.42) \quad \{\text{eq:31}\}$$

The exponential map can be expressed as

$$\exp(at) = \sum_{k=0}^{\infty} \frac{(ta)^k}{k!} \quad (11.43) \quad \{\text{eq:32}\}$$

since it is a solution of (11.41). A simple computation allows to check this claim:

$$\frac{d}{dt} \exp(at) = \sum_{k=1}^{\infty} k t^{k-1} \frac{a^k}{k!} = a \cdot \sum_{k=0}^{\infty} t^k \frac{a^k}{k!} = a \cdot \exp(at). \quad (11.44) \quad \{\text{eq:33}\}$$

A similar computation gives

$$\frac{d}{dt} \exp(at) = \sum_{k=0}^{\infty} t^k \frac{a^k}{k!} \cdot a = \exp(at) \cdot a. \quad (11.45) \quad \{\text{eq:34}\}$$

The exponential mapping  $\exp : \mathfrak{g} \rightarrow \mathcal{G}$  can also be defined as  $\exp(a) = \sigma(1)$  where  $\sigma(t)$  satisfies the differential equation

$$\dot{\sigma}(t) = \sigma(t) \cdot a, \quad \sigma(0) = I. \quad (11.46) \quad \{\text{eq:35}\}$$

**Theorem 1** Let  $\Lambda^l : \mathcal{G} \times \mathcal{M} \rightarrow \mathcal{M}$  be a left group action and  $\lambda^l : \mathfrak{g} \rightarrow \mathcal{X}(\mathcal{M})$  the corresponding Lie algebra homomorphism. For any  $a \in \mathfrak{g}$  the flow of the vector field  $F = \lambda_a^l(a)$ , i.e. the solution of the equation

$$\dot{y}(t) = F(y(t)) = \lambda_*^l(a)(y(t)), \quad t \geq 0, y(0) = y_0 \in \mathcal{M}, \quad (11.47) \quad \{\text{eq:36}\}$$

is given as

$$y(t) = \Lambda^l(\exp(ta), y_0). \quad (11.48) \quad \{\text{eq:37}\}$$

Let  $\Lambda^r : \mathcal{M} \times \mathcal{G} \rightarrow \mathcal{M}$  be a right group action and  $\lambda^r : \mathfrak{g} \rightarrow \mathcal{X}(\mathcal{M})$  the corresponding Lie algebra homomorphism. For any  $a \in \mathfrak{g}$  the flow of the vector field  $F = \lambda_*^r(a)$ , i.e. the solution of the equation

$$\dot{y}(t) = F(y(t)) = \lambda_*^r(a)(y(t)), \quad t \geq 0, y(0) = y_0 \in \mathcal{M}, \quad (11.49) \quad \{\text{eq:38}\}$$

is given as

$$y(t) = \Lambda^r(y_0, \exp(ta)). \quad (11.50) \quad \{\text{eq:39}\}$$

### 11.2.5 Translation (Trivialization) maps

The left and right translation maps defined by

$$\begin{aligned} L_z : \mathcal{G} \times \mathcal{G} &\rightarrow \mathcal{G} & (\text{left translation map}) \\ y &\mapsto z \cdot y \end{aligned} \quad (11.51) \quad \{\text{eq:148}\}$$

and

$$\begin{aligned} R_z(y) : \mathcal{G} \times \mathcal{G} &\rightarrow \mathcal{G} & (\text{right translation map}) \\ y &\mapsto y \cdot z \end{aligned} \quad (11.52) \quad \{\text{eq:149}\}$$

If we identify the manifold  $\mathcal{M}$  with the group  $\mathcal{G}$ , The left and right translations can be interpreted as the simplest example of group action on the manifold. Note that the left translation map can be viewed as a left or right action on the group.

If we consider  $L_z(y)$  as a right group action  $L_z(y) = \Lambda^r(z, y) = z \cdot y$ , by differentiation we get a  $L'_z : T\mathfrak{g} \cong \mathfrak{g} \rightarrow T_z\mathcal{G}$  with  $\dot{\rho}(0) = a$  such that

$$\lambda'_*(a)(z) = L'_z(a) = \left. \frac{d}{ds} \Lambda^r(z, \rho(s)) \right|_{s=0} = z \cdot a \quad (11.53) \quad \{\text{eq:150}\}$$

The map

$$\begin{aligned} L'_z : \mathfrak{g} &\rightarrow T_z\mathcal{G} \\ a &\mapsto z \cdot a \end{aligned} \quad (11.54) \quad \{\text{eq:152}\}$$

determines an isomorphism of  $\mathfrak{g}$  with the tangent space  $T_z\mathcal{G}$ . In other words, the tangent space can be identified to  $\mathfrak{g}$  as

$$T_z\mathcal{G} = \{L'_z(a) = z \cdot a \mid a \in \mathfrak{g}\} \quad (11.55) \quad \{\text{eq:153}\}$$

Respectively, if we consider  $R_z(y)$  as a left group action  $R_z(y) = \Lambda^l(y, z) = y \cdot z$ , by differentiation we get a  $R'_z : T\mathfrak{g} \cong \mathfrak{g} \rightarrow T_z\mathcal{G}$  with  $\dot{\rho}(0) = a$  such that

$$\lambda'_*(a)(z) = R'_z(a) = \left. \frac{d}{ds} \Lambda^l(\rho(s), z) \right|_{s=0} = a \cdot z \quad (11.56) \quad \{\text{eq:150}\}$$

The map

$$\begin{aligned} R'_z : \mathfrak{g} &\rightarrow T_z\mathcal{G} \\ a &\mapsto a \cdot z \end{aligned} \quad (11.57) \quad \{\text{eq:152}\}$$

determines an isomorphism of  $\mathfrak{g}$  with the tangent space  $T_z\mathcal{G}$ . In other words, the tangent space can be identified to  $\mathfrak{g}$  as

$$T_z\mathcal{G} = \{R'_z(a) = a \cdot z \mid a \in \mathfrak{g}\} \quad (11.58) \quad \{\text{eq:153}\}$$

Any tangent vector  $F : \mathcal{G} \rightarrow T_z\mathcal{G}$  can be written in either of the forms

$$F(z) = L'_z(f(a)) = R'_z(g(z)) \quad (11.59) \quad \{\text{eq:155}\}$$

where  $f, g : \mathcal{G} \rightarrow \mathfrak{g}$ .

### 11.2.6 Adjoint representation

**Definition 16** Let  $p \in \mathcal{G}$  and let  $\sigma(t)$  be a smooth curve on  $\mathcal{G}$  such that  $\sigma(0) = I$  and  $\dot{\sigma}(0) = b \in \mathfrak{g}$ . The adjoint representation is defined as

$$\text{Ad}_p(b) = \left. \frac{d}{dt} p\sigma(t)p^{-1} \right|_{t=0} \quad (11.60) \quad \{\text{eq:40}\}$$

The derivative of  $\text{Ad}$  with respect to the first argument is denoted  $\text{ad}$ . Let  $\rho(s)$  be a smooth curve on  $\mathcal{G}$  such that  $\rho(0) = I$  and  $\dot{\rho}(0) = a$ , it yields:

$$\text{ad}_a(b) = \left. \frac{d}{ds} \text{Ad}_{\rho(s)}(b) \right|_{s=0} = [a, b] \quad (11.61) \quad \{\text{eq:41}\}$$

The adjoint representation can also be expressed with the map

$$\text{Ad}_p(b) = (L_p \cdot R_{p^{-1}})'(b) = (L'_p \cdot R'_{p^{-1}})(b) = p \cdot b \cdot p^{-1} \quad (11.62) \quad \{\text{eq:154}\}$$

For a tangent vector given in (11.59), we have

$$g(z) = \text{Ad}_z(f(z)) \quad (11.63) \quad \{\text{eq:151}\}$$

Another important relation relating  $\text{Ad}$ ,  $\text{ad}$  and  $\exp$  is

$$\text{Ad}_{\exp(a)} = \exp \text{ad}_a \quad (11.64) \quad \{\text{eq:164}\}$$

### 11.2.7 Differential of the exponential map

There are multiple ways to represent the differential of  $\exp(\cdot)$  at a point  $a \in \mathfrak{g}$ . Let us start by the following definition of the differential map at  $a \in \mathfrak{g}$

$$\begin{aligned} \exp'_a : \mathfrak{g} &\rightarrow T_{\exp(a)}\mathcal{G} \\ v &\mapsto \exp'_a(v) = \left. \frac{d}{dt} \exp(a + tv) \right|_{t=0} \end{aligned} \quad (11.65) \quad \{\text{eq:147}\}$$

The definition is very similar to the definition of the directional derivative of  $\exp$  in the direction  $v \in \mathfrak{g}$  at a point  $a \in \mathfrak{g}$ . Using the expression (11.58) of the tangent space at  $\exp(a)$ , we can defined another expression of the differential map denoted as  $d^l \exp_a : \mathfrak{g} \rightarrow \mathfrak{g}$  such that

$$d^l \exp_a = L'_{\exp^{-1}(a)} \cdot \exp'_a = L'_{\exp(-a)} \cdot \exp'_a \quad (11.66) \quad \{\text{eq:156}\}$$

This expression appears as a trivialization of the differential map  $\exp'_a$ . Using the expression of  $L'_z$  in (11.57). In [4, Theorem 2.14.13], an explicit formula relates  $d^l \exp_a$  to the iteration of the adjoint operator:

$$d^l \exp_a(b) = \sum_{k=0}^{\infty} \frac{(-1)^k}{(k+1)!} (\text{ad}_a(b))^k := \frac{e - \exp \cdot \text{ad}_a}{\text{ad}_a}(b) \quad (11.67) \quad \{\text{eq:43}\}$$

where  $(\text{ad}_a)^k$  is the  $k$ th iteration of the adjoint operator:

$$\begin{cases} (\text{ad}_a)^k(b) = \underbrace{[a, [a, [\dots, a, [a, b]]]}_{k \text{ times}} & \text{for } k \geq 1 \\ (\text{ad}_a)^0(b) = b \end{cases} \quad (11.68) \quad \{\text{eq:44}\}$$

It is also possible to define the right trivialized differential of the exponential map

$$d^r \exp_a = R'_{\exp^{-1}(a)} \cdot \exp'_a = R'_{\exp(-a)} \cdot \exp'_a \quad (11.69) \quad \{\text{eq:162}\}$$

that is

$$d^r \exp_a(b) = \exp'_a(b) \cdot \exp(-a) \quad (11.70) \quad \{\text{eq:163}\}$$

With these expression, we have equivalently for

$$\exp'_a(b) = \exp_a \cdot d^l \exp_a(b) \quad \text{and} \quad \exp'_a(b) = d^r \exp_a(b) \cdot \exp(a) \quad (11.71) \quad \{\text{eq:157}\}$$

To avoid to burden to much the notation, we introduced the unified definition of the differential map that corresponds to  $\text{dexp} = d^r \exp$

**Definition 17** *The differential of the exponential mapping, denoted by  $\text{dexp}_a : \mathfrak{g} \times \mathfrak{g} \rightarrow \mathfrak{g}$  is defined as the “right trivialized” tangent of the exponential map*

$$\frac{d}{dt}(\exp(a(t))) = \text{dexp}_{a(t)}(a'(t)) \exp(a(t)) \quad (11.72) \quad \{\text{eq:42}\}$$

An explicit formula relates  $\text{dexp}_a$  to the iteration of the adjoint operator:

$$\text{dexp}_a(b) = \sum_{k=0}^{\infty} \frac{1}{(k+1)!} (\text{ad}_a(b))^k := \frac{\exp \cdot \text{ad}_a - e}{\text{ad}_a}(b) \quad (11.73) \quad \{\text{eq:43}\}$$

As for  $\text{Ad}_a$  and  $\text{ad}_a$ , the mapping  $\text{dexp}_a(b)$  is a linear mapping in its second argument for a fixed  $a$ . Using the relation (11.64), we can also relate the right and the left trivialization tangent

$$\text{d}^l \text{exp}_a(b) = (\text{Ad}_{\text{exp}(a)} \cdot \text{dexp}(a))(b) = (\text{exp}(\text{ad}_{-a}) \cdot \frac{e - \text{exp} \cdot \text{ad}_a}{\text{ad}_a})(b) = \frac{e - \text{exp} \cdot \text{ad}_{-a}}{\text{ad}_a}(b) = \text{dexp}_{-a}(b) \quad (11.74) \quad \{\text{eq:165}\}$$

It is also possible to define the the “left trivialized” tangent of the exponential map

$$\frac{d}{dt}(\text{exp}(a(t))) = \text{exp}(a(t)) \text{d}^l \text{exp}_{a(t)}(a'(t)) = \text{exp}(a(t)) \text{dexp}_{-a(t)}(a'(t)) = \quad (11.75) \quad \{\text{eq:46}\}$$

### 11.2.2 Redaction note V. ACARY

other notation and Lie derivative

$$Df \cdot \hat{\Omega}(p) = (\hat{\Omega}^r f)(p) \quad (11.76) \quad \{\text{eq:178}\}$$

**Inverse of the exponential map** The function  $\text{dexp}_a$  is an analytical function so it possible to invert it to get

$$\text{dexp}_a^{-1} = \sum_{k=0}^{\infty} \frac{B_k}{(k)!} (\text{ad}_a)^k(b) \quad (11.77) \quad \{\text{eq:45}\}$$

where  $B_k$  are the Bernouilli number.

### 11.2.8 Differential of a map $f : \mathcal{G} \rightarrow \mathfrak{g}$

We follow the notation developed in [3]. Let us first define the differential of the map  $f : \mathcal{G} \rightarrow \mathfrak{g}$  as

$$\begin{aligned} f'_z : T_z \mathcal{G} &\rightarrow T_{f(z)} \mathfrak{g} \cong \mathfrak{g} \\ b &\mapsto \left. \frac{d}{dt} f(z \cdot \exp(tL'_{z^{-1}}(b))) \right|_{t=0} \end{aligned} \quad (11.78) \quad \{\text{eq:166}\}$$

The image of  $b$  by  $f'_z$  is obtained by first identifying  $b$  with an element of  $v \in \mathfrak{g}$  thanks to the left representation of  $T_{f(z)} \mathfrak{g}$  view the left translation map  $v = tL'_z(b)$ . The exponential mapping transforms  $v$  an element  $y$  of the Lie Group  $\mathcal{G}$ . Then  $f'_z$  is obtained by

$$f'_z(b) = \lim_{t \rightarrow 0} \frac{f(z \cdot y) - f(z)}{t} \quad (11.79) \quad \{\text{eq:167}\}$$

As we have done for the exponential mapping, it is possible to get a left trivialization of

$$\text{d} f_z = (f \cdot L_z)' = f'_z \cdot L'_z \quad (11.80) \quad \{\text{eq:169}\}$$

thus

$$\text{d} f_z(a) = f'_z \cdot L'_z(a) = f'_z(L'_z(a)) = \left. \frac{d}{dt} f(z \cdot \exp(ta)) \right|_{t=0} \quad (11.81) \quad \{\text{eq:170}\}$$

**Newton Method** Let us imagine that we want to solve  $f(y) = 0$  for  $y \in \mathcal{G}$ . A newton method can be written as

### 11.3 Lie group $SO(3)$ of finite rotations and Lie algebra $\mathfrak{so}(3)$ of infinitesimal rotations

The presentation in this section follows the notation and the developments taken from [2? ]. For more details on Lie groups and Lie algebra, we refer to [4] and [? ].

The Lie group  $SO(3)$  is the group of linear proper orthogonal transformations in  $\mathbf{R}^3$  that may be represented by a set of matrices in  $\mathbf{R}^{3 \times 3}$  as

$$SO(3) = \{R \in \mathbf{R}^{3 \times 3} \mid R^T R = I, \det(R) = +1\} \quad (11.82) \quad \{\text{eq:47}\}$$

with the group law given by  $R_1 \cdot R_2 = R_1 R_2$  for  $R_1, R_2 \in SO(3)$ . The identity element is  $e = I_{3 \times 3}$ . At any point of  $R \in SO(3)$ , the tangent space  $T_R SO(3)$  is the set of tangent vectors at a point  $R$ .

**Left representation of the tangent space at  $R$ ,  $T_R SO(3)$**  Let  $S(t)$  be a smooth curve  $S(\cdot) : \mathbf{R} \rightarrow SO(3)$  in  $SO(3)$ . An element  $a$  of the tangent space at  $R$  is given by

$$a = \left. \frac{d}{dt} S(t) \right|_{t=0} \quad (11.83) \quad \{\text{eq:174}\}$$

such that  $S(0) = R$ . Since  $S(t) \in SO(3)$ , we have  $\frac{d}{dt}(S(t)) = \dot{S}(t)S^T(t) + S(t)\dot{S}^T(t) = 0$ . At  $t = 0$ , we get  $aR^T + Ra^T = 0$ . We conclude that it exists a skew-symmetric matrix  $\tilde{\Omega} = R^T a$  such that  $\tilde{\Omega}^T + \tilde{\Omega} = 0$ . Hence, a possible representation of  $T_R SO(3)$  is

$$T_R SO(3) = \{a = R\tilde{\Omega} \in \mathbf{R}^{3 \times 3} \mid \tilde{\Omega}^T + \tilde{\Omega} = 0\}. \quad (11.84) \quad \{\text{eq:49}\}$$

For  $R = I$ , the tangent space is directly given by the set of skew-symmetric matrices:

$$T_I SO(3) = \{\tilde{\Omega} \in \mathbf{R}^{3 \times 3} \mid \tilde{\Omega}^T + \tilde{\Omega} = 0\}. \quad (11.85) \quad \{\text{eq:50}\}$$

The tangent space  $T_I SO(3)$  with the Lie Bracket  $[\cdot, \cdot]$  defined by the matrix commutator

$$[A, B] = AB - BA \quad (11.86) \quad \{\text{eq:51}\}$$

is a Lie algebra that is denoted by

$$\mathfrak{so}(3) = \{\Omega \in \mathbf{R}^{3 \times 3} \mid \Omega + \tilde{\Omega}^T = 0\}. \quad (11.87) \quad \{\text{eq:53}\}$$

For skew symmetric matrices, the commutator can be expressed with the cross product in  $\mathbf{R}^3$

$$[\tilde{\Omega}, \tilde{\Gamma}] = \tilde{\Omega}\tilde{\Gamma} - \tilde{\Gamma}\tilde{\Omega} = \widetilde{\Omega \times \Gamma} \quad (11.88) \quad \{\text{eq:52}\}$$

We use  $T_I SO(3) \cong \mathfrak{so}(3)$  whenever there is no ambiguity.

The notation  $\tilde{\Omega}$  is implied by the fact that the Lie algebra is isomorphic to  $\mathbf{R}^3$  thanks to the operator  $\widetilde{(\cdot)} : \mathbf{R}^3 \rightarrow \mathfrak{so}(3)$  and defined by

$$\widetilde{(\cdot)} : \Omega \mapsto \tilde{\Omega} = \begin{bmatrix} 0 & -\Omega_3 & \Omega_2 \\ \Omega_3 & 0 & -\Omega_1 \\ -\Omega_2 & \Omega_1 & 0 \end{bmatrix} \quad (11.89) \quad \{\text{eq:54}\}$$

Note that  $\tilde{\Omega}x = \Omega \times x$ .

**A special (right) action of Lie Group  $\mathcal{G}$  on a manifold  $\mathcal{M}$ .** Let us come back to the representation of  $T_R SO(3)$  given in (11.84). It is clear it can be expressed with a representation that relies on  $\mathfrak{so}(3)$

$$T_R SO(3) = \{a = R\tilde{\Omega} \in \mathbb{R}^{3 \times 3} \mid \tilde{\Omega} \in \mathfrak{so}(3)\}. \quad (11.90) \quad \{\text{eq:58}\}$$

With (11.90), we see that there is a linear map that relates  $T_R SO(3)$  to  $\mathfrak{so}(3)$ . This can be formalized by noting that the left translation map for a point  $R \in SO(3)$

$$\begin{aligned} L_R &: SO(3) \rightarrow SO(3) \\ S &\mapsto L_R(S) = R \cdot S = RS \end{aligned} \quad (11.91) \quad \{\text{eq:59}\}$$

which is a diffeomorphism on  $SO(3)$  is a group action. In our case, we identify the manifold and the group. Hence, the mapping  $L_R$  can be viewed as a left or a right group action. We choose a right action such that  $\Lambda^r(R, S) = L_R(S) = R \cdot S$ . By differentiation, we get a mapping  $L'_R : T_S \mathfrak{so}(3) \cong \mathfrak{so}(3) \rightarrow T_R SO(3)$ . For a given  $\tilde{\Omega} \in \mathfrak{so}(3)$  and a point  $R$ , the differential  $L'_R$  is computed by computing the tangent vector field  $\lambda_*^r(a)(R)$  of the group action  $\Lambda^r(R, S)$  for a smooth curve  $S(t) : \mathbb{R} \rightarrow SO(3)$  such that  $\dot{S}(0) = \tilde{\Omega}$ :

$$\lambda_*^r(a)(R) := \left. \frac{d}{dt} \Lambda^r(R, S(t)) \right|_{t=0} = \left. \frac{d}{dt} L_R(S(t)) \right|_{t=0} = \left. \frac{d}{dt} R \cdot S(t) \right|_{t=0} = R \cdot \dot{S}(0) = R\tilde{\Omega} \in X(\mathcal{M}) \quad (11.92) \quad \{\text{eq:60}\}$$

Therefore, the vector field in (11.92) is a tangent vector field that defines a Lie-Type ordinary differential equation

$$\dot{R}(t) = \lambda_*^r(a)(R(t)) = R(t)\tilde{\Omega} \quad (11.93) \quad \{\text{eq:61}\}$$

In [1], the linear operator  $\lambda_*^r(a)$  is defined as the directional derivative with respect to  $S$  and denoted  $DL_R(S)$ . It defines a diffeomorphism between  $T_S SO(3)$  and  $T_R SO(3)$ . In particular, for  $S = I_{3 \times 3}$ , we get

$$\begin{aligned} DL_R(I_{3 \times 3}) : \mathfrak{so}(3) &\rightarrow T_R SO(3) \\ \tilde{\Omega} &\mapsto DL_R(I_{3 \times 3}) \cdot \tilde{\Omega} = R\tilde{\Omega} \end{aligned} \quad (11.94) \quad \{\text{eq:62}\}$$

We end up with a possible representation of  $T_R SO(3)$  as

$$T_R SO(3) = \{\tilde{\Omega}_R \mid \tilde{\Omega}_R = DL_R(I_{3 \times 3}) \cdot \tilde{\Omega} = R\tilde{\Omega}, \tilde{\Omega} \in \mathfrak{so}(3)\}. \quad (11.95) \quad \{\text{eq:63}\}$$

In other words, a tangent vector  $\tilde{\Omega} \in \mathfrak{so}(3)$  defines a left invariant vector field on  $SO(3)$  at the point  $R$  given by  $R\tilde{\Omega}$ .

#### 11.3.1 Redaction note V. ACARY

what happens at  $S(0) = R$ , with  $a = R\tilde{\Omega} = \dot{S}(0)$  and then  $\dot{y}(t) = F(y(t)) = R\tilde{\Omega}y(t) = R\Omega \times y(t) = \dot{S}(0)y(t)$ . What else ?

**Exponential map**  $\exp_{\mathfrak{m}} \mathfrak{so}(3) \rightarrow SO(3)$  The relations (11.35) and (11.36) show that it is possible to define a tangent vector field from a group action. We can directly apply Theorem 1 and we get that the solution of

$$\begin{cases} \dot{R}(t) = \lambda_*^r(a)(R(t)) = R(t)\tilde{\Omega} \\ R(0) = R_0 \end{cases} \quad (11.96) \quad \{\text{eq:130}\}$$

is

$$R(t) = R_0 \exp_{\mathfrak{m}}(t\tilde{\Omega}) \quad (11.97) \quad \{\text{eq:138}\}$$

Let us do the computation in this case. Let us assume that the solution can be sought as  $R(t) = \Lambda^r(y_0, S(t))$ . The initial condition imposes that  $R(0) = R_0 = \Lambda(R_0, I) = \Lambda(R_0, S(0))$  that implies



$S(0) = I$ . Since  $\Lambda(R_0, S(t))$  is the flow that is produced by  $S(t)$  and let us try to find the relation satisfied by  $S(\cdot)$ . For a smooth curve  $T(s) \in SO(3)$  such that  $\dot{T}(0) = \tilde{\Omega}$ , we have

$$\begin{aligned} \dot{R}(t) = \lambda_*^r(\tilde{\Omega})(R(t)) &= \left. \frac{d}{ds} \Lambda^r(R(t), T(s)) \right|_{s=0} \\ &= \left. \frac{d}{ds} \Lambda^r(\Lambda(R_0, S(t)), T(s)) \right|_{s=0} \\ &= \left. \frac{d}{ds} (\Lambda^r(R_0, S(t)) \cdot T(s)) \right|_{s=0} \\ &= D_2 \Lambda^r(R_0, S(t)) \cdot \dot{T}(0) \\ &= D_2 \Lambda^r(R_0, S(t)) \cdot \tilde{\Omega} \end{aligned} \quad (11.98) \quad \{\text{eq:64}\}$$

On the other side, the relation  $y(t) = \Lambda^r(y_0, S(t))$  gives  $\dot{y}(t) = D_2 \Lambda^r(y_0, S'(t))$  and we conclude that

$$\begin{cases} \dot{S}(t) = S(t) \cdot \tilde{\Omega} = S(t) \tilde{\Omega} \\ S(0) = I. \end{cases} \quad (11.99) \quad \{\text{eq:65}\}$$

The ordinary differential equation (11.99) is a matrix ODE that admits the following solution

$$S(t) = \expm(t\tilde{\Omega}) \quad (11.100) \quad \{\text{eq:66}\}$$

where  $\exp : \mathbf{R}^{3 \times 3} \rightarrow \mathbf{R}^{3 \times 3}$  is the matrix exponential defined by

$$\expm(A) = \sum_{k=0}^{\infty} \frac{1}{k!} (A)^k. \quad (11.101) \quad \{\text{eq:67}\}$$

We conclude that  $R(t) = \Lambda(R_0, S(t)) = R_0 \expm(t\tilde{\Omega})$  is the solution of (11.46).

We can use the closed form solution for the matrix exponential of  $t\tilde{\Omega} \in \mathfrak{so}(3)$  as

$$\expm(t\tilde{\Omega}) = I_{3 \times 3} + \frac{\sin t\theta}{\theta} \tilde{\Omega} + \frac{(\cos t\theta - 1)}{\theta^2} \tilde{\Omega}^2 \quad (11.102) \quad \{\text{eq:68}\}$$

with  $\theta = \|\Omega\|$ . For given  $\tilde{\Omega} \in \mathfrak{so}(3)$ , we have

$$\det(\tilde{\Omega}) = \det(\tilde{\Omega}^T) = \det(-\tilde{\Omega}^T) = (-1)^3 \det(\tilde{\Omega}) = -\det(\tilde{\Omega}) \quad (11.103) \quad \{\text{eq:69}\}$$

that implies that  $\det(\tilde{\Omega}) = 0$ . From (11.102), we conclude that

$$\det(\expm(t\tilde{\Omega})) = 1. \quad (11.104) \quad \{\text{eq:70}\}$$

Furthermore, we have  $\expm(t\tilde{\Omega}) \expm(-t\tilde{\Omega}) = \expm(t(\tilde{\Omega} - \tilde{\Omega})) = I$ . We can verify that  $\expm(t\tilde{\Omega}) \in SO(3)$ .

**Adjoint representation** In the case of  $SO(3)$ , the definition of the operator  $\text{Ad}$  gives

$$\text{Ad}_R(\tilde{\Omega}) = R\tilde{\Omega}R^T \quad (11.105) \quad \{\text{eq:121}\}$$

and then mapping  $\text{ad}_{\tilde{\Omega}}(\tilde{\Gamma})$  is defined by

$$\text{ad}_{\tilde{\Omega}}(\tilde{\Gamma}) = \tilde{\Omega}\tilde{\Gamma} - \tilde{\Gamma}\tilde{\Omega} = [\tilde{\Omega}, \tilde{\Gamma}] = \widetilde{\Omega \times \Gamma}. \quad (11.106) \quad \{\text{eq:56}\}$$

Using the isomorphism between  $\mathfrak{so}(3)$  and  $\mathbf{R}^3$ , it is possible to define the mapping  $\text{ad}_{\Omega}(\Gamma) : \mathbf{R}^3 \times \mathbf{R}^3 \rightarrow \mathbf{R}^3$  with the realization of the Lie algebra in  $\mathbf{R}^3$  as

$$\text{ad}_{\Omega}(\Gamma) = \tilde{\Omega}\Gamma = \Omega \times \Gamma \quad (11.107) \quad \{\text{eq:55}\}$$

**Differential of the exponential map**  $\text{dexpm}$  The differential of the exponential mapping, denoted by  $\text{dexpm}$  is defined as the 'right trivialized' tangent of the exponential map

$$\frac{d}{dt}(\exp(\tilde{\Omega}(t))) = \text{dexp}_{\tilde{\Omega}(t)}\left(\frac{d\tilde{\Omega}(t)}{dt}\right) \exp(\tilde{\Omega}(t)) \quad (11.108) \quad \{\text{eq:71}\}$$

The differential of the exponential mapping, denoted by  $\text{dexpm}$  is defined as the 'left trivialized' tangent of the exponential map

$$\frac{d}{dt}(\exp(\tilde{\Omega}(t))) = \text{dexp}_{\tilde{\Omega}(t)}\left(\frac{d\tilde{\Omega}(t)}{dt}\right) \exp(\tilde{\Omega}(t)) \quad (11.109) \quad \{\text{eq:72}\}$$

Using the formula (11.73) and the fact that  $\text{ad}_{\tilde{\Omega}}(\tilde{\Gamma}) = \tilde{\Omega}\tilde{\Gamma}$ , we can write the differential as

$$\begin{aligned} \text{dexp}_{\tilde{\Omega}}(\tilde{\Gamma}) &= \sum_{k=0}^{\infty} \frac{1}{(k+1)!} \text{ad}_{\tilde{\Omega}}^k(\tilde{\Gamma}) \\ &= \sum_{k=0}^{\infty} \frac{1}{(k+1)!} \tilde{\Omega}^k \tilde{\Gamma} \end{aligned} \quad (11.110) \quad \{\text{eq:122}\}$$

Using again the fact that  $\tilde{\Omega}^3 = -\theta^2 \tilde{\Omega}$ , we get

$$\begin{aligned} \text{dexp}_{\tilde{\Omega}} &= \sum_{k=0}^{\infty} \frac{1}{(k+1)!} \tilde{\Omega}^k \\ &= I + \sum_{k=0}^{\infty} \frac{(-1)^k}{((2(k+1)))!} \theta^{2k} \tilde{\Omega} + \sum_{k=0}^{\infty} \frac{(-1)^k}{((2(k+1)+1))!} \theta^{2k} \tilde{\Omega}^2 \end{aligned} \quad (11.111) \quad \{\text{eq:123}\}$$

Hence, we get

$$\text{dexp}_{\tilde{\Omega}} = I + \frac{(1 - \cos(\theta))}{\theta^2} \tilde{\Omega} + \frac{(\theta - \sin(\theta))}{\theta^3} \tilde{\Omega}^2 \quad (11.112) \quad \{\text{eq:124}\}$$

Since  $\text{dexp}_{\tilde{\Omega}}$  is a linear mapping from  $\mathfrak{so}(3)$  to  $\mathfrak{so}(3)$ , we will use the following notation

$$\text{dexp}_{\tilde{\Omega}} \tilde{\Gamma} := T(\Omega) \tilde{\Gamma} \quad (11.113) \quad \{\text{eq:172}\}$$

with

$$T(\Omega) := I + \frac{(1 - \cos(\theta))}{\theta^2} \tilde{\Omega} + \frac{(\theta - \sin(\theta))}{\theta^3} \tilde{\Omega}^2 \in \mathbb{R}^{3 \times 3} \quad (11.114) \quad \{\text{eq:173}\}$$

### 11.3.1 Newton method and differential of a map $f : \mathcal{G} \rightarrow \mathfrak{g}$

Finally, let us define the differential of the map  $f : SO(3) \rightarrow \mathfrak{so}(3)$  as

$$\begin{aligned} f'_R : T_R SO(3) &\rightarrow T_{f(R)} \mathfrak{so}(3) \cong \mathfrak{so}(3) \\ a &\mapsto \left. \frac{d}{dt} f(R \cdot \expm(t L'_{R^{-1}}(a))) \right|_{t=0} \end{aligned} \quad (11.115) \quad \{\text{eq:183}\}$$

The image of  $b$  by  $f'_z$  is obtained by first identifying  $a$  with an element of  $\tilde{\Omega} \in \mathfrak{so}(3)$  thanks to the left representation of  $T_{f(R)} \mathfrak{so}(3)$  view the left translation map  $\tilde{\Omega} = t L'_R(b)$ . The exponential mapping transforms  $\tilde{\Omega}$  an element  $S$  of the Lie Group  $SO(3)$ . Then  $f'_z$  is obtained by

$$f'_R(b) = \lim_{t \rightarrow 0} \frac{f(R \cdot S) - f(R)}{t} \quad (11.116) \quad \{\text{eq:184}\}$$

As we have done for the exponential mapping, it is possible to get a left trivialization of

$$d f_R = (f \circ L_R)' = f'_R \circ L'_R \quad (11.117) \quad \{\text{eq:185}\}$$

thus

$$d f_R(\tilde{\Omega}) = f'_R \circ L'_R(\tilde{\Omega}) = f'_R(L'_R(\tilde{\Omega})) = \left. \frac{d}{dt} f(R \cdot \expm(t \tilde{\Omega})) \right|_{t=0} \quad (11.118) \quad \{\text{eq:186}\}$$

### 11.3.2 Redaction note V. ACARY

The computation of this differential is non linear with respect to  $\tilde{\Omega}$ .

not clear if we write  $df_R(\tilde{\Omega})$ . Better understand the link with  $d\exp_{\tilde{\Omega}} \tilde{\Gamma}$

Sometimes, it can be formally written as

$$df_R(\tilde{\Omega}) = C(\tilde{\Omega})\tilde{\Omega} \quad (11.119) \quad \{\text{eq:180}\}$$

Nevertheless, an explicit expression of  $C(\cdot)$  is not necessarily trivial.

Let us consider a first simple example of a mapping  $f(R) = \tilde{R}x$  for a given  $x \in \mathbb{R}^3$ . The computation yields

$$\begin{aligned} df_R(\tilde{\Omega}) &= \left. \frac{d}{dt} R \exp(t\tilde{\Omega})x \right|_{t=0} \\ &= R \left. \frac{d}{dt} \exp(t\tilde{\Omega}) \right|_{t=0} x \\ &= R \underbrace{d\exp_{\tilde{\Omega}}(\tilde{\Omega})}_{\tilde{\Gamma}} \exp(t\tilde{\Omega}) \Big|_{t=0} x \\ &= R \underbrace{d\exp_{\tilde{\Omega}}(\tilde{\Omega})}_{\tilde{\Gamma}} x \\ &= RT(\tilde{\Omega})\tilde{\Omega}x \\ &= -RT(\tilde{\Omega})\tilde{x}\Omega \end{aligned} \quad (11.120) \quad \{\text{eq:181}\}$$

In that case, it is difficult to find an expression as in (11.119), but considering the function  $g(R)$  such that  $f(R) = \tilde{g}(x)$  we get

$$dg_R(\tilde{\Omega}) = -RT(\tilde{\Omega})\tilde{x}\Omega = C(\tilde{\Omega})\Omega \quad (11.121) \quad \{\text{eq:181}\}$$

with

$$C(\Omega) = -RT(\Omega)\tilde{x} \quad (11.122) \quad \{\text{eq:182}\}$$

## 11.4 Lie group of unit quaternions $H_1$ and pure imaginary quaternions $H_p$ .

In Siconos we choose to parametrize the rotation with a unit quaternion  $p \in H$  such that  $R = \Phi(p)$ . This parameterization has no singularity and has only one redundant variable that is determined by imposing  $\|p\| = 1$ .

**Quaternion definition.** There are many ways to define quaternions. The most convenient one is to define a quaternion as a  $2 \times 2$  complex matrix, that is an element of  $\mathbb{C}^{2 \times 2}$ . For this end, we write for  $z \in \mathbb{C}$ ,  $z = a + ib$  with  $a, b \in \mathbb{R}$  and  $i^2 = -1$  and its conjugate  $\bar{z} = a - ib$ . Let  $e, i, j, k$  the following matrices in  $\mathbb{C}^{2 \times 2}$

$$e = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}, \quad i = \begin{bmatrix} i & 0 \\ 0 & -i \end{bmatrix}, \quad j = \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix}, \quad k = \begin{bmatrix} 0 & i \\ i & 0 \end{bmatrix} \quad (11.123) \quad \{\text{eq:127}\}$$

**Definition 18** Let  $H$  be the set of all matrices of the form

$$p_0 e + p_1 i + p_2 j + p_3 k \quad (11.124) \quad \{\text{eq:128}\}$$

where  $(p_0, p_1, p_2, p_3) \in \mathbb{R}^4$ . Every Matrix in  $H$  is of the form

$$\begin{bmatrix} x & y \\ -\bar{y} & \bar{x} \end{bmatrix} \quad (11.125) \quad \{\text{eq:129}\}$$

where  $x = p_0 + ip_1$  and  $y = p_2 + ip_3$ . The matrices in  $H$  are called quaternions.

**Definition 19** The null quaternion generated by  $[0, 0, 0, 0] \in \mathbb{R}^4$  is denoted by  $0$ . Quaternions of the form  $p_1\mathbf{i} + p_2\mathbf{j} + p_3\mathbf{k}$  are called pure quaternions. The set of pure quaternions is denoted by  $H_p$ .

With the definition of  $H$  as a set of complex matrices, It can be show that  $H$  is a real vector space of dimension 4 with basis  $e, \mathbf{i}, \mathbf{j}, \mathbf{k}$ . Furthermore, with the matrix product,  $H$  is a real algebra.

**Representation of quaternions** Thanks to the equations (11.124), (11.124) and (11.125), we see that there are several manner to represent a quaternion  $p \in H$ . It can be represented as a complex matrix as in (11.125). It can also be represented as a vector in  $\mathbb{R}^4$ ,  $p = [p_0, p_1, p_2, p_3]$  with the isomorphism (11.124). In other words,  $H$  is isomorphic to  $\mathbb{R}^4$ . The first element  $p_0$  can also be viewed as a scalar and three last ones as a vector in  $\mathbb{R}^3$  denoted by  $\vec{p} = [p_1, p_2, p_3]$ , and in that case,  $H$  is viewed as  $\mathbb{R} \times \mathbb{R}^3$ . The quaternion can be written as  $p = (p_0, \vec{p})$ .

**Quaternion product** The quaternion product denoted by  $p \cdot q$  for  $p, q \in H_1$  is naturally defined as the product of complex matrices. With its representation in  $\mathbb{R} \times \mathbb{R}^3$ , the quaternion product is defined by

$$p \cdot q = \begin{bmatrix} p_0 q_0 - \vec{p} \cdot \vec{q} \\ p_0 \vec{q} + q_0 \vec{p} + \vec{p} \times \vec{q} \end{bmatrix}. \quad (11.126) \quad \{\text{eq:73}\}$$

Since the product is a matrix product, it is not communicative, but it is associative. The identity element for the quaternion product is

$$e = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} = (1, \vec{0}). \quad (11.127) \quad \{\text{eq:57}\}$$

Let us note that

$$(0, \vec{p}) \cdot (0, \vec{q}) = -(0, \vec{q}) \cdot (0, \vec{p}). \quad (11.128) \quad \{\text{eq:74}\}$$

The quaternion multiplication can also be represented as a matrix operation in  $\mathbb{R}^{4 \times 4}$ . Indeed, we have

$$p \cdot q = \begin{bmatrix} q_0 p_0 - q_1 p_1 - q_2 p_2 - q_3 p_3 \\ q_0 p_1 + q_1 p_0 - q_2 p_3 + q_3 p_2 \\ q_0 p_2 + q_1 p_3 + q_2 p_0 - q_3 p_1 \\ q_0 p_3 - q_1 p_2 + q_2 p_1 + q_3 p_0 \end{bmatrix} \quad (11.129) \quad \{\text{eq:75}\}$$

that can be represented as

$$p \cdot q = \begin{bmatrix} p_0 & -p_1 & -p_2 & -p_3 \\ p_1 & p_0 & -p_3 & p_2 \\ p_2 & p_3 & p_0 & -p_1 \\ p_3 & -p_2 & p_1 & p_0 \end{bmatrix} \begin{bmatrix} q_0 \\ q_1 \\ q_2 \\ q_3 \end{bmatrix} := [p.]q \quad (11.130) \quad \{\text{eq:76}\}$$

or

$$p \cdot q = \begin{bmatrix} q_0 & -q_1 & -q_2 & -q_3 \\ q_1 & q_0 & q_3 & -q_2 \\ q_2 & -q_3 & q_0 & q_1 \\ q_3 & q_2 & -q_1 & q_0 \end{bmatrix} \begin{bmatrix} p_0 \\ p_1 \\ p_2 \\ p_3 \end{bmatrix} := [q]p \quad (11.131) \quad \{\text{eq:77}\}$$

**Adjoint quaternion, inverse and norm** The adjoint quaternion of  $p$  is denoted by

$$p^* = \overline{\begin{bmatrix} x & y \\ -\bar{y} & \bar{x} \end{bmatrix}}^T = \begin{bmatrix} \bar{x} & -y \\ \bar{y} & x \end{bmatrix} = [p_0, -p_1, -p_2, -p_3] = (p_0, -\vec{p}) \quad (11.132)$$

We note that

$$p \cdot p^* = \begin{bmatrix} x & y \\ -\bar{y} & \bar{x} \end{bmatrix} \begin{bmatrix} \bar{x} & -y \\ \bar{y} & x \end{bmatrix} = \det \left( \begin{bmatrix} x & y \\ -\bar{y} & \bar{x} \end{bmatrix} \right) e = (x\bar{x} + y\bar{y})e = (p_0^2 + p_1^2 + p_2^2 + p_3^2)e \quad (11.133) \quad \{\text{eq:131}\}$$

The norm of a quaternion is given by  $|p|^2 = p^\top p = p_0^2 + p_1^2 + p_2^2 + p_3^2$ . In particular, we have  $p \cdot p^\star = p^\star \cdot p = |p|^2 e$ . This allows to define the reciprocal of a non zero quaternion by

$$p^{-1} = \frac{1}{|p|^2} p^\star \quad (11.134) \quad \{\text{eq:78}\}$$

A quaternion  $p$  is said to be unit if  $|p| = 1$ .

**Unit quaternion and rotation** For two vectors  $x \in \mathbb{R}^3$  and  $x' \in \mathbb{R}^3$ , we define the quaternion  $p_x = (0, x) \in \mathbf{H}_p$  and  $p_{x'} = (0, x') \in \mathbf{H}_p$ . For a given unit quaternion  $p$ , the transformation

$$p_{x'} = p \cdot p_x \cdot p^\star \quad (11.135) \quad \{\text{eq:79}\}$$

defines a rotation  $R$  such that  $x' = Rx$  given by

$$x' = (p_0^2 - p^\top \vec{p})x + 2p_0(\vec{p} \times x) + 2(\vec{p}^\top x)p = Rx \quad (11.136) \quad \{\text{eq:80}\}$$

The rotation matrix may be computed as

$$R = \Phi(p) = \begin{bmatrix} 1 - 2p_2^2 - 2p_3^2 & 2(p_1p_2 - p_3p_0) & 2(p_1p_3 + p_2p_0) \\ 2(p_1p_2 + p_3p_0) & 1 - 2p_1^2 - 2p_3^2 & 2(p_2p_3 - p_1p_0) \\ 2(p_1p_3 - p_2p_0) & 2(p_2p_3 + p_1p_0) & 1 - 2p_1^2 - 2p_2^2 \end{bmatrix} \quad (11.137) \quad \{\text{eq:81}\}$$

**Computation of the time derivative of a unit quaternion associated with a rotation.** The derivation with respect to time can be obtained as follows. The rotation transformation for a unit quaternion is given by

$$p_{x'}(t) = p(t) \cdot p_x \cdot p^\star(t) = p(t) \cdot p_x \cdot p^{-1}(t) \quad (11.138) \quad \{\text{eq:82}\}$$

and can be derived as

$$\begin{aligned} \dot{p}_{x'}(t) &= \dot{p}(t) \cdot p_x \cdot p^{-1}(t) + p(t) \cdot p_x \cdot \dot{p}^{-1}(t) \\ &= \dot{p}(t) \cdot p^{-1}(t) \cdot p_{x'}(t) + p_{x'}(t) \cdot p(t) \cdot \dot{p}^{-1}(t) \end{aligned} \quad (11.139) \quad \{\text{eq:83}\}$$

From  $p(t) \cdot p^{-1}(t) = e$ , we get

$$\dot{p}(t) \cdot p^{-1}(t) + p \cdot \dot{p}^{-1}(t) = 0 \quad (11.140) \quad \{\text{eq:84}\}$$

so (11.138) can be rewritten

$$\dot{p}_{x'}(t) = \dot{p}(t) \cdot p^{-1}(t) \cdot p_{x'}(t) - p_{x'}(t) \cdot \dot{p}(t) \cdot p^{-1}(t) \quad (11.141) \quad \{\text{eq:85}\}$$

The scalar part of  $\dot{p}(t) \cdot p^{-1}(t)$  is  $(\dot{p}(t) \cdot p^{-1}(t))_0 = p_0\dot{p}_0 + \vec{p}^\top \dot{\vec{p}}$ . Since  $p$  is a unit quaternion, we have

$$|p| = 1 \implies \frac{d}{dt}(p^\top p) = 0 = \dot{p}^\top p + p^\top \dot{p} = 2(p_0\dot{p}_0 + \vec{p}^\top \dot{\vec{p}}). \quad (11.142) \quad \{\text{eq:86}\}$$

Therefore, the scalar part  $(\dot{p}(t) \cdot p^{-1}(t))_0 = 0$ . The quaternion product  $\dot{p}(t) \cdot p^{-1}(t)$  and  $p_{x'}(t)$  is a product of quaternions with zero scalar part (see (11.128)), so we have

$$\dot{p}_{x'}(t) = 2\dot{p}(t) \cdot p^{-1}(t) \cdot p_{x'}(t). \quad (11.143) \quad \{\text{eq:87}\}$$

In terms of vector of  $\mathbb{R}^3$ , this corresponds to

$$\dot{x}'(t) = 2\overrightarrow{\dot{p}(t) \cdot p^{-1}(t)} \times x'(t). \quad (11.144) \quad \{\text{eq:88}\}$$

Since  $x'(t) = R(t)x$ , we have  $\dot{x}' = \dot{R}(t)x = \tilde{\omega}(t)R(t)x = \tilde{\omega}(t)x'(t)$ . Comparing (11.143) and (11.144), we get

$$\tilde{\omega}(t) = 2\overrightarrow{\dot{p}(t) \cdot p^{-1}(t)} \quad (11.145) \quad \{\text{eq:89}\}$$

or equivalently

$$\dot{p}(t) \cdot p^{-1}(t) = (0, \frac{\omega(t)}{2}) \quad (11.146) \quad \{\text{eq:90}\}$$

Finally, we can conclude that

$$\dot{p}(t) = (0, \frac{\omega(t)}{2}) \cdot p(t). \quad (11.147) \quad \{\text{eq:91}\}$$

Since  $\omega(t) = R(t)\Omega(t)$ , we have

$$(0, \omega(t)) = (0, R(t)\Omega(t)) = p(t) \cdot (0, \Omega(t)) \cdot \bar{p}(t) = p(t) \cdot (0, \Omega(t)) \cdot p^{-1}(t) \quad (11.148) \quad \{\text{eq:92}\}$$

and then

$$\dot{p}(t) = \frac{1}{2} p(t) \cdot (0, \Omega(t)). \quad (11.149) \quad \{\text{eq:93}\}$$

The time derivation is compactly written

$$\dot{p} = \frac{1}{2} p \cdot (0, \frac{\Omega}{2}) = [p.] p_{\frac{\Omega}{2}} = \Psi(p) \frac{\Omega}{2}, \quad (11.150) \quad \{\text{eq:94}\}$$

and using the matrix representation of product of quaternion we get

$$\Psi(p) = \begin{bmatrix} -p_1 & -p_2 & -p_3 \\ p_0 & -p_3 & p_2 \\ p_3 & p_0 & -p_1 \\ -p_2 & p_1 & p_0 \end{bmatrix} \quad (11.151) \quad \{\text{eq:95}\}$$

The relation (11.149) can be also inverted by writing

$$(0, \Omega(t)) = 2p^{-1}(t) \cdot \dot{p}(t) \quad (11.152) \quad \{\text{eq:96}\}$$

Using again matrix representation of product of quaternion, we get

$$\Omega(t) = \overrightarrow{2p^{-1}(t) \cdot \dot{p}(t)} = 2 \begin{bmatrix} -p_1 & p_0 & p_3 & -p_2 \\ -p_2 & -p_3 & p_0 & p_1 \\ -p_3 & p_2 & -p_1 & p_0 \end{bmatrix} \dot{p}(t) = 2\Psi(p)^\top \dot{p}(t) \quad (11.153) \quad \{\text{eq:97}\}$$

Note that we have  $\Psi^\top(p)\Psi(p) = I_{4 \times 4}$  and  $\Psi(p)\Psi^\top(p) = I_{3 \times 3}$

**Lie group structure of unit quaternions.** In terms of complex matrices, an unit quaternion  $p$  satisfies

$$\det \left( \begin{bmatrix} x & y \\ -\bar{y} & \bar{x} \end{bmatrix} \right) = 1 \quad (11.154) \quad \{\text{eq:125}\}$$

The set of all unit quaternions that we denote  $H_1$  is the set of unitary matrices of determinant equal to 1. From (11.133), we get that

$$p \cdot p^* = e \quad (11.155) \quad \{\text{eq:126}\}$$

It implies that the set  $H_1$  is the set of special unitary complex matrices. The set is a Lie group usually denoted as  $SU(2)$ . Since we used multiple representation of a quaternion, we continue to use  $H_1 \cong SU(2)$  as a notation but with the Lie group structure implied by  $SU(2)$ .

Let us compute the tangent vector at a point  $p \in H_1$ . Let  $q(\cdot)$  be a smooth curve  $q(\cdot) : t \in \mathbf{R} \mapsto q(t) \in H_1$  in  $H_1$  such that  $q(0) = p$ . Since  $q(t) \in H_1$ , we have  $|q(t)| = 1$  and then  $\frac{d}{dt}|q(t)| = 2(q_0(0)\dot{q}_0(0) + \vec{q}^T(0)\vec{\dot{q}}(0)) = 0$ . At  $t = 0$ , we get

$$2(p_0 a_0 + \vec{p}^T \vec{a}) = 0. \quad (11.156) \quad \{\text{eq:48}\}$$

This relation imposes that the quaternions  $2p^* \cdot a \in H_1$  and  $2a \cdot p^* \in H_1$ , that is, have to be pure quaternions. Therefore, it exists  $\omega \in \mathbf{R}^3$  and  $\Omega \in \mathbf{R}^3$  such that

$$(0, \Omega) = 2p^* \cdot a \quad (11.157) \quad \{\text{eq:132}\}$$

and

$$(0, \omega) = 2a \cdot p^* \quad (11.158) \quad \{\text{eq:132}\}$$

In other terms, the tangent vector spaces at  $p \in H_1$  can be represented as a left representation

$$T_p H_1 = \{a \mid a = p \cdot (0, \frac{\Omega}{2}), \Omega \in \mathbb{R}^3\} \quad (11.159) \quad \{\text{eq:133}\}$$

or a right representation

$$T_p H_1 = \{a \mid a = (0, \frac{\omega}{2}) \cdot p, \omega \in \mathbb{R}^3\} \quad (11.160) \quad \{\text{eq:1330}\}$$

At  $p = e$ , we get the Lie algebra defined by

$$\mathfrak{h}_1 = T_e H_1 = \{a = (0, \frac{\Omega}{2}), \Omega \in \mathbb{R}^3\} \quad (11.161) \quad \{\text{eq:134}\}$$

equipped with the Lie bracket given by the commutator

$$[p, q] = p \cdot q - q \cdot p. \quad (11.162) \quad \{\text{eq:135}\}$$

We can easily verify that for  $a = (0, \frac{\Omega}{2})$ ,  $b = (0, \frac{\Gamma}{2}) \in \mathfrak{h}_1$ , we have

$$[a, b] = (0, \frac{\Omega}{2}) \cdot (0, \frac{\Gamma}{2}) - (0, \frac{\Gamma}{2}) \cdot (0, \frac{\Omega}{2}) = (0, \frac{\Omega \times \Gamma}{2}) \in \mathfrak{h}_1 \quad (11.163) \quad \{\text{eq:136}\}$$

As for  $\mathfrak{so}(3)$ , the Lie algebra  $\mathfrak{h}_1$  is isomorphic to  $\mathbb{R}^3$  thanks to the operator  $\widehat{(\cdot)} : \mathbb{R}^3 \rightarrow \mathfrak{h}_1$  and defined by

$$\widehat{(\cdot)} : \Omega \mapsto \widehat{\Omega} = (0, \frac{\Omega}{2}) \quad (11.164) \quad \{\text{eq:54}\}$$

With this operator, the Lie Bracket can be written

$$[\widehat{\Omega}, \widehat{\Gamma}] = \widehat{\Omega \times \Gamma} \quad (11.165) \quad \{\text{eq:137}\}$$

**A special (right) action of Lie Group  $\mathcal{G}$  on a manifold  $\mathcal{M}$ .** Let us come back to the representation of  $T_p H_1$  given in (11.159). It is clear it can be expressed with a representation that relies on  $\mathfrak{h}_1$

$$T_R SO(3) = \{a = p \cdot \widehat{\Omega} \mid \widehat{\Omega} \in \mathfrak{h}_1\}. \quad (11.166) \quad \{\text{eq:158}\}$$

With (11.90), we see that there is a linear map that relates  $T_p H_1$  to  $\mathfrak{h}_1$ . This linear map defines a vector field. A special group action is defined by the left translation map for a point  $p \in H_1$

$$\begin{aligned} L_p &: H_1 \rightarrow H_1 \\ q &\mapsto L_p(q) = p \cdot q \end{aligned} \quad (11.167) \quad \{\text{eq:159}\}$$

which is a diffeomorphism on  $H_1$ . In that case, we identify the manifold and the group. So,  $L_p$  can be viewed as a left or a right group action. We choose a right action. For our application where  $\mathcal{G} = \mathcal{M} = H_1$  and  $\Lambda^r(p, q) = L_p(q) = p \cdot q$ , we get

$$\lambda_*^r(a)(p) = \left. \frac{d}{dt} L_p(q(t)) \right|_{t=0} = \left. \frac{d}{dt} p \cdot q(t) \right|_{t=0} = p \cdot \dot{q}(0) = p \cdot \dot{q}(0) \in X(\mathcal{M}) \quad (11.168) \quad \{\text{eq:160}\}$$

for a smooth curve  $q(t)$  in  $H_1$ . Since  $q(\cdot)$  is a smooth curve in  $H_1$ ,  $\dot{q}(0)$  is a tangent vector at the point  $q(0) = I$ , that is an element  $a = \widehat{\Omega} \in \mathfrak{h}_1$  defined by the relation (11.44). Therefore, the vector field in (11.168) is a tangent vector field and we get

$$\dot{p}(t) = \lambda_*^r(a)(p(t)) = p(t) \cdot \widehat{\Omega} \quad (11.169) \quad \{\text{eq:161}\}$$

**Exponential map**  $\exp q : \mathfrak{h}_1 \rightarrow H_1$  We can directly apply Theorem 1 and we get that the solution of

$$\begin{cases} \dot{p}(t) = \lambda_*^r(a)(p(t)) = p(t) \cdot \hat{\Omega} \\ p(0) = R p_0 \end{cases} \quad (11.170) \quad \{\text{eq:130}\}$$

is

$$p(t) = p_0 \exp q(t \hat{\Omega}) \quad (11.171) \quad \{\text{eq:138}\}$$

The exponential mapping  $\exp q : \mathfrak{h}_1 \rightarrow H_1$  can also be defined as  $\exp q(\hat{\Omega}) = q(1)$  where  $q(t)$  satisfies the differential equation

$$\dot{q}(t) = q(t) \cdot \hat{\Omega}, \quad q(0) = e. \quad (11.172) \quad \{\text{eq:235}\}$$

Using the quaternion product, the exponential map can be expressed as

$$\exp q(t \hat{\Omega}) = \sum_{k=0}^{\infty} \frac{(t \hat{\Omega})^k}{k!} \quad (11.173) \quad \{\text{eq:232}\}$$

since it is a solution of (11.170). A simple computation allows to check this claim:

$$\frac{d}{dt} \exp q(t \hat{\Omega}) = \sum_{k=1}^{\infty} k t^{k-1} \frac{\hat{\Omega}^k}{k!} = \sum_{k=0}^{\infty} t^k \frac{t \hat{\Omega}^k}{k!} \cdot \hat{\Omega} = \exp q(t \hat{\Omega}) \cdot \hat{\Omega}. \quad (11.174) \quad \{\text{eq:233}\}$$

A closed form relation for the form the quaternion exponential can also be found by noting that

$$\hat{\Omega}^2 = -\left(\frac{\theta}{2}\right)^2 e, \text{ and } \hat{\Omega}^3 = -\left(\frac{\theta}{2}\right)^2 \hat{\Omega}. \quad (11.175) \quad \{\text{eq:140}\}$$

A simple expansion of (11.173) at  $t = 1$  equals

$$\begin{aligned} \exp q(\hat{\Omega}) &= \sum_{k=0}^{\infty} \frac{(\hat{\Omega})^k}{k!} \\ &= \sum_{k=0}^{\infty} \frac{(-1)^k}{(2k)!} \left(\frac{\theta}{2}\right)^{2k} e + \sum_{k=0}^{\infty} \frac{(-1)^k}{(2k+1)!} \left(\frac{\theta}{2}\right)^{2k+1} \hat{\Omega} \\ &= \cos\left(\frac{\theta}{2}\right) e + \frac{\sin\left(\frac{\theta}{2}\right)}{\frac{\theta}{2}} \hat{\Omega} \end{aligned} \quad (11.176) \quad \{\text{eq:141}\}$$

that is

$$\exp q(\hat{\Omega}) = \left(\cos\left(\frac{\theta}{2}\right), \sin\left(\frac{\theta}{2}\right) \frac{\Omega}{\theta}\right). \quad (11.177) \quad \{\text{eq:144}\}$$

**Adjoint representation** In the case of  $H_1$ , the definition of the operator  $\text{Ad}$  gives

$$\text{Ad}_p(\hat{\Omega}) = p \cdot \hat{\Omega} p^* \quad (11.178) \quad \{\text{eq:121}\}$$

and then mapping  $\text{ad}_{\hat{\Omega}}(\hat{\Gamma})$  is defined by

$$\text{ad}_{\hat{\Omega}}(\hat{\Gamma}) = \hat{\Omega} \hat{\Gamma} - \hat{\Gamma} \hat{\Omega} = [\hat{\Omega}, \hat{\Gamma}] = \widehat{\Omega \times \Gamma}. \quad (11.179) \quad \{\text{eq:56}\}$$

Using the isomorphism between  $\mathfrak{h}_1$  and  $\mathbf{R}^3$ , we can use the the mapping  $\text{ad}_{\Omega}(\Gamma) : \mathbf{R}^3 \times \mathbf{R}^3 \rightarrow \mathbf{R}^3$  given by (11.107) to get

$$\text{ad}_{\hat{\Omega}}(\hat{\Gamma}) = \widehat{\Omega \times \Gamma} = \widehat{\text{ad}_{\Omega}(\Gamma)} = \hat{\Omega} \Gamma \quad (11.180) \quad \{\text{eq:145}\}$$



**Differential of the exponential map**  $\text{dexpq}$  The differential of the exponential mapping, denoted by  $\text{dexpq}$  is defined as the 'right trivialized' tangent of the exponential map

$$\frac{d}{dt}(\text{expq}(\hat{\Omega}(t))) = \text{dexpq}_{\hat{\Omega}(t)}\left(\frac{d\hat{\Omega}(t)}{dt}\right) \text{expq}(\hat{\Omega}(t)) \quad (11.181) \quad \{\text{eq:71}\}$$

An explicit expression of  $\text{dexpq}_{\hat{\Omega}}(\hat{\Gamma})$  can also be developed either by developing the expansion and (11.165).

$$\text{dexpq}_{\hat{\Omega}}(\Gamma) = \sum_{k=0}^{\infty} \frac{1}{(k+1)!} \text{ad}_{\hat{\Omega}}^k(\hat{\Gamma}) = \widehat{T(\Omega)}\Gamma \quad (11.182) \quad \{\text{eq:168}\}$$

**Remark 2** Note that the time derivative in  $\mathbf{R}^4$  is not differential mapping. The standard time derivative of  $\text{expq}$  in the expression (11.177) gives

$$\frac{d}{dt} \text{expq}(\hat{\Gamma}(t)) = \left(-\frac{\sin(\theta)}{\theta} \Omega^T \Gamma, \frac{\sin(\theta)}{\theta} \Gamma + \frac{\theta \cos(\theta) - \sin(\theta)}{\theta^3} \Omega^T \Omega \Gamma\right) \quad (11.183) \quad \{\text{eq:171}\}$$

that can be expressed in  $\mathbf{R}^4$  by

$$\frac{d}{dt} \text{expq}(\hat{\Gamma}(t)) = \nabla \text{expq}(\hat{\Omega}) \hat{\Omega} \quad (11.184) \quad \{\text{eq:175}\}$$

with

$$\nabla \text{expq}(\hat{\Omega}) = \begin{bmatrix} -\frac{\sin(\theta)}{\theta} \Omega^T \\ \frac{\sin(\theta)}{\theta} I + \frac{\theta \cos(\theta) - \sin(\theta)}{\theta^3} \Omega^T \Omega \end{bmatrix} \quad (11.185) \quad \{\text{eq:176}\}$$

Clearly, we have

$$\nabla \text{expq}(\hat{\Omega}) \neq \text{dexpq}_{\hat{\Omega}} \quad (11.186) \quad \{\text{eq:177}\}$$

## Directional derivative and Jacobians of functions of a quaternion

### 11.4.1 Redaction note V. ACARY experimental

Let  $f : \mathbf{H}_1 \rightarrow \mathbf{R}$  be a mapping from the group to  $\mathbf{R}^3$ . The directional derivative of  $f$  in the direction  $\hat{\Omega} \in \mathfrak{h}_1$  at  $p \in \mathbf{H}_1$  is defined by

$$df_p(\hat{\Omega}) = \left. \frac{d}{dt} f(p \cdot \text{expq}(t\hat{\Omega})) \right|_{t=0} \quad (11.187) \quad \{\text{eq:139}\}$$

As a first simple example let us choose  $f(p) = \overrightarrow{p \cdot p_x \cdot p^*}$  for a given  $x \in \mathbf{R}^3$ , we get

$$\begin{aligned} DId \cdot \hat{\Omega}(p) &= (\hat{\Omega}^r f)(p) = \left. \frac{d}{dt} \overrightarrow{p \cdot \text{expq}(t\hat{\Omega}) \cdot p_x \cdot (p \cdot \text{expq}(t\hat{\Omega}))^*} \right|_{t=0} \\ &= p \cdot \left. \frac{d}{dt} \text{expq}(t\hat{\Omega}) \right|_{t=0} \cdot p_x \cdot p^* + p \cdot p_x \cdot \left. \left( p \cdot \frac{d}{dt} \text{expq}(t\hat{\Omega}) \right|_{t=0} \right)^* \end{aligned} \quad (11.188) \quad \{\text{eq:142}\}$$

We have from the definition of the time derivative of the exponential

$$\begin{aligned} \left. \frac{d}{dt} \text{expq}(t\hat{\Omega}) \right|_{t=0} &= \text{dexpq}_{\hat{\Omega}}(\hat{\Omega}) \text{expq}(t\hat{\Omega}) \Big|_{t=0} \\ &= \text{dexpq}_{\hat{\Omega}}(\hat{\Omega}) \end{aligned} \quad (11.189) \quad \{\text{eq:143}\}$$

Then, the directional derivative can be written

$$\begin{aligned} DId \cdot \hat{\Omega}(p) &= \overrightarrow{p \cdot \text{dexpq}_{\hat{\Omega}}(\hat{\Omega}) \cdot p_x \cdot p^* + p \cdot p_x \cdot (\text{dexpq}_{\hat{\Omega}}(\hat{\Omega}))^* \cdot p^*} \\ &= p \cdot (\text{dexpq}_{\hat{\Omega}}(\hat{\Omega}) \cdot p_x + p_x \cdot (\text{dexpq}_{\hat{\Omega}}(\hat{\Omega}))^*) \cdot p^* \end{aligned} \quad (11.190) \quad \{\text{eq:146}\}$$

## 11.5 Newton-Euler equation in quaternion form

**Computation of  $T$  for unit quaternion** The operator  $T(q)$  is directly obtained as

$$T(q) = \frac{1}{2} \begin{bmatrix} 2I_{3 \times 3} & 0_{3 \times 3} \\ 0_{4 \times 3} & \begin{matrix} -p_1 & -p_2 & -p_3 \\ p_0 & -p_3 & p_2 \\ p_3 & p_0 & -p_1 \\ -p_2 & p_1 & p_0 \end{matrix} \end{bmatrix} \quad (11.191) \quad \{\text{eq:98}\}$$

### 11.5.1 Redaction note V. ACARY

todo :

- computation of the directional derivative of  $R(\Omega) = \exp(\tilde{\Omega})$  in the direction  $\tilde{\Omega}$ , to get  $T(\Omega)$

**Quaternion representation** If the Lie group is described by unit quaternion, we get

$$SO(3) = \{p = (p_0, \vec{p}) \in \mathbb{R}^4 \mid |p| = 1\} \quad (11.192) \quad \{\text{eq:99}\}$$

with the composition law  $p_1 \cdot p_2$  given by the quaternion product.

Note that the concept of exponential map for Lie group that are not parameterized by matrices is also possible.

### 11.5.1 Mechanical systems with bilateral and unilateral constraints

{section22}

Let us consider that the system (11.20) is subjected to  $m$  constraints, with  $m_e$  holonomic bilateral constraints

$$h^\alpha(q) = 0, \alpha \in \mathcal{E} \subset N, |\mathcal{E}| = m_e, \quad (11.193) \quad \{\text{eq:bilateral-con}\}$$

and  $m_i$  unilateral constraints

$$g_N^\alpha(q) \geq 0, \alpha \in \mathcal{I} \subset N, |\mathcal{I}| = m_i. \quad (11.194) \quad \{\text{eq:unilateral-con}\}$$

Let us denote as  $J_h^\alpha(q) = \nabla_q^\top h^\alpha(q)$  the Jacobian matrix of the bilateral constraint  $h^\alpha(q)$  with respect to  $q$  and as  $J_{g_N}^\alpha(q)$  respectively for  $g_N^\alpha(q)$ . The bilateral constraints at the velocity level can be obtained as:

$$0 = \dot{h}^\alpha(q) = J_h^\alpha(q)\dot{q} = J_h^\alpha(q)T(q)v := H^\alpha(q)v, \quad \alpha \in \mathcal{E}. \quad (11.195) \quad \{\text{eq:bilateral-con}\}$$

By duality and introducing a Lagrange multiplier  $\lambda^\alpha, \alpha \in \mathcal{E}$ , the constraint generates a force applied to the body equal to  $H^{\alpha,\top}(q)\lambda^\alpha$ . For the unilateral constraints, a Lagrange multiplier  $\lambda_N^\alpha, \alpha \in \mathcal{I}$  is also associated and the constraints at the velocity level can also be derived as

$$0 \leq \dot{g}_N^\alpha(q) = J_{g_N}^\alpha(q)\dot{q} = J_{g_N}^\alpha(q)T(q)v, \text{ if } g_N^\alpha(q) = 0, \quad \alpha \in \mathcal{I}. \quad (11.196) \quad \{\text{eq:unilateral-con}\}$$

Again, the force applied to the body is given by  $(J_{g_N}^\alpha(q)T(q))^\top \lambda_N^\alpha$ . Nevertheless, there is no reason that  $\lambda_N^\alpha = r_N^\alpha$  and  $u_N = J_{g_N}^\alpha(q)T(q)v$  if the  $g_N$  is not chosen as the signed distance (the gap function). This is the reason why we prefer directly define the normal and the tangential local relative velocity with respect to the twist vector as

$$u_N^\alpha := G_N^\alpha(q)v, \quad u_T^\alpha := G_T^\alpha(q)v, \quad \alpha \in \mathcal{I}, \quad (11.197) \quad \{\text{eq:unilateral-con}\}$$

and the associated force as  $G_N^{\alpha,\top}(q)r_N^\alpha$  and  $G_T^{\alpha,\top}(q)r_T^\alpha$ . For the sake of simplicity, we use the notation  $u^\alpha := G^\alpha(q)v$  and its associated total force generated by the contact  $\alpha$  as  $G^{\alpha,\top}(q)r^\alpha := G_N^{\alpha,\top}(q)r_N^\alpha + G_T^{\alpha,\top}(q)r_T^\alpha$ .

The complete system of equation of motion can finally be written as

$$\left\{ \begin{array}{l} \dot{q} = T(q)v, \\ M\dot{v} = F(t, q, v) + H^\top(q)\lambda + G^\top(q)r, \\ H^\alpha(q)v = 0, \\ r^\alpha = 0, \quad \text{if } g_N^\alpha(q) > 0, \\ K^{\alpha,*} \ni \hat{u}^\alpha \perp r^\alpha \in K^\alpha, \quad \text{if } g_N^\alpha(q) = 0, \\ u_N^{\alpha,+} = -e_r^\alpha u_N^{\alpha,-}, \quad \text{if } g_N^\alpha(q) = 0 \text{ and } u_N^{\alpha,-} \leq 0, \end{array} \right\} \quad \begin{array}{l} \alpha \in \mathcal{E} \\ \alpha \in \mathcal{I} \end{array} \quad (11.198) \quad \{\text{eq:NewtonEuler-}\}$$

where the definition of the variables  $\lambda \in \mathbf{R}^{m_e}, r \in \mathbf{R}^{3m_i}$  and the operators  $H, G$  are extended to collect all the variables for each constraints.

Note that all the constraints are written at the velocity integrators. Another strong advantage is the straightforward introduction of the contact dissipation processes that are naturally written at the velocity level such as the Newton impact law and the Coulomb friction. Indeed, in Mechanics, dissipation processes are always given in terms of rates of changes, or if we prefer, in terms of velocities.

**Siconos Notation** In the siconos notation, we have for the applied torques on the system the following decomposition

$$F(t, q, v) := \left( \begin{array}{c} f(t, x_g, v_g, R, \Omega) \\ I\Omega \times \Omega + M(t, x_g, v_g, R, \Omega) \end{array} \right) := \left( \begin{array}{c} f_{ext}(t) - f_{int}(x_g, v_g, R, \Omega) \\ -M_{gyr}(\Omega) + M_{ext}(t) - M_{int}(x_g, v_g, R, \Omega) \end{array} \right). \quad (11.199)$$

with

$$M_{gyr} := (\Omega \times I\Omega) \quad (11.200)$$

In the siconos notation, we have for the relation

$$C = J^\alpha(q) \quad CT = J^\alpha(q)T(q) \quad (11.201) \quad \{\text{eq:100}\}$$

## 11.6 Time integration scheme in scheme

### 11.6.1 Moreau–Jean scheme based on a $\theta$ -method

The complete Moreau–Jean scheme based on a  $\theta$ -method is written as follows

$$\left\{ \begin{array}{l} q_{k+1} = q_k + hT(q_{k+\theta})v_{k+\theta} \\ M(v_{k+1} - v_k) - hF(t_{k+\theta}, q_{k+\theta}, v_{k+\theta}) = H^\top(q_{k+1})Q_{k+1} + G^\top(q_{k+1})P_{k+1}, \\ H^\alpha(q_{k+1})v_{k+1} = 0 \\ P_{k+1}^\alpha = 0, \\ K^{\alpha,*} \ni \hat{u}_{k+1}^\alpha \perp P_{k+1}^\alpha \in K^\alpha \end{array} \right\} \quad \begin{array}{l} \alpha \in \mathcal{E} \\ \alpha \notin \mathcal{I}^\nu \\ \alpha \in \mathcal{I}^\nu \end{array} \quad (11.202) \quad \{\text{eq:Moreau-Jean-}\}$$

where  $\mathcal{I}^\nu$  is the set of forecast constraints, that may be evaluated as

$$\mathcal{I}^\nu = \{\alpha \mid \bar{g}_N^\alpha := g_N + \frac{h}{2}u_N^\alpha \leq 0\}. \quad (11.203) \quad \{\text{eq:101}\}$$

### 11.6.2 Semi-explicit version Moreau–Jean scheme based on a $\theta$ -method

$$\left\{ \begin{array}{l} q_{k+1} = q_k + hT(q_k)v_{k+\theta} \\ M(v_{k+1} - v_k) - hF(t_k, q_k, v_k) = H^\top(q_k)Q_{k+1} + G^\top(q_k)P_{k+1}, \\ H^\alpha(q_{k+1})v_{k+1} = 0 \\ P_{k+1}^\alpha = 0, \\ K^{\alpha,*} \ni \hat{u}_{k+1}^\alpha \perp P_{k+1}^\alpha \in K^\alpha \end{array} \right\} \begin{array}{l} \alpha \in \mathcal{E} \\ \alpha \notin \mathcal{I}^\nu \\ \alpha \in \mathcal{I}^\nu \end{array} \quad (11.204) \quad \{\text{eq:Moreau-Jean-}\theta\}$$

In this version, the new velocity  $v_{k+1}$  can be computed explicitly, assuming that the inverse of  $M$  is easily written, as

$$v_{k+1} = v_k + M^{-1}hF(t_k, q_k, v_k) + M^{-1}(H^\top(q_k)Q_{k+1} + G^\top(q_k)P_{k+1}) \quad (11.205) \quad \{\text{eq:Moreau-Jean-}\theta\}$$

### 11.6.3 Nearly implicit version Moreau–Jean scheme based on a $\theta$ -method implemented in siconos

A first simplification is made considering a given value of  $q_{k+1}$  in  $T()$ ,  $H()$  and  $G()$  denoted by  $\bar{q}_k$ . This limits the computation of the Jacobians of this operators with respect to  $q$ .

$$\left\{ \begin{array}{l} q_{k+1} = q_k + hT(\bar{q}_k)v_{k+\theta} \\ M(v_{k+1} - v_k) - h\theta F(t_{k+1}, q_{k+1}, v_{k+1}) - h(1-\theta)F(t_k, q_k, v_k) = H^\top(\bar{q}_k)Q_{k+1} + G^\top(\bar{q}_k)P_{k+1}, \\ H^\alpha(\bar{q}_k)v_{k+1} = 0 \\ P_{k+1}^\alpha = 0, \\ K^{\alpha,*} \ni \hat{u}_{k+1}^\alpha \perp P_{k+1}^\alpha \in K^\alpha \end{array} \right\} \begin{array}{l} \alpha \in \mathcal{E} \\ \alpha \notin \mathcal{I}^\nu \\ \alpha \in \mathcal{I}^\nu \end{array} \quad (11.206) \quad \{\text{eq:Moreau-Jean-}\theta\}$$

The nonlinear residu is defined as

$$\mathcal{R}(v) = M(v - v_k) - h\theta F(t_{k+1}, q(v), v) - h(1-\theta)F(t_k, q_k, v_k) - H^\top(\bar{q}_k)Q_{k+1} - G^\top(\bar{q}_k)P_{k+1} \quad (11.207) \quad \{\text{eq:Moreau-Jean-}\theta\}$$

with

$$q(v) = q_k + hT(\bar{q}_k)((1-\theta)v_k + \theta v). \quad (11.208) \quad \{\text{eq:Moreau-Jean-}\theta\}$$

At each time step, we have to solve

$$\mathcal{R}(v_{k+1}) = 0 \quad (11.209) \quad \{\text{eq:Moreau-Jean-}\theta\}$$

together with the constraints.

Let us write a linearization of the problem to design a Newton procedure:

$$\nabla_v^\top \mathcal{R}(v_{k+1}^\tau)(v_{k+1}^{\tau+1} - v_{k+1}^\tau) = -\mathcal{R}(v_{k+1}^\tau). \quad (11.210) \quad \{\text{eq:Moreau-Jean-}\theta\}$$

The computation of  $\nabla_v^\top \mathcal{R}(v_{k+1}^\tau)$  is as follows

$$\nabla_v^\top \mathcal{R}(v) = M - h\theta \nabla_v F(t_{k+1}, q(v), v) \quad (11.211) \quad \{\text{eq:102}\}$$

with

$$\begin{aligned} \nabla_v F(t_{k+1}, q(v), v) &= D_2 F(t_{k+1}, q(v), v) \nabla_v q(v) + D_3 F(t_{k+1}, q(v), v) \\ &= h\theta D_2 F(t_{k+1}, q(v), v) T(\bar{q}_k) + D_3 F(t_{k+1}, q(v), v) \end{aligned} \quad (11.212) \quad \{\text{eq:103}\}$$

where  $D_i$  denotes the derivation with respect the  $i^{th}$  variable. The complete Jacobian is then given by

$$\nabla_v^\top \mathcal{R}(v) = M - h\theta D_3 F(t_{k+1}, q(v), v) - h^2 \theta^2 D_2 F(t_{k+1}, q(v), v) T(\bar{q}_k) \quad (11.213) \quad \{\text{eq:104}\}$$

In siconos, we ask the user to provide the functions  $D_3F(t_{k+1}, q, v)$  and  $D_2F(t_{k+1}, q, v)$ .

Let us denote by  $W^\tau$  the inverse of Jacobian of the residu,

$$W^\tau = (M - h\theta D_3F(t_{k+1}, q(v), v) - h^2\theta^2 D_2F(t_{k+1}, q(v), v)T(\bar{q}_k))^{-1}. \quad (11.214) \quad \{\text{eq:105}\}$$

and by  $\mathcal{R}_{free}(v)$  the free residu,

$$\mathcal{R}_{free}(v) = M(v - v_k) - h\theta F(t_{k+1}, q(v), v) - h(1 - \theta)F(t_k, q_k, v_k). \quad (11.215) \quad \{\text{eq:106}\}$$

The linear equation 11.210 that we have to solve is equivalent to

$$v_{k+1}^{\tau+1} = v_{k+1}^\tau - W\mathcal{R}_{free}(v_{k+1}^\tau) + WH^\top(\bar{q}_k)Q_{k+1}^{\tau+1} + WG^\top(\bar{q}_k)P_{k+1}^{\tau+1} \quad (11.216) \quad \{\text{eq:107}\}$$

We define  $v_{free}$  as

$$v_{free} = v_{k+1}^\tau - W\mathcal{R}_{free}(v_{k+1}^\tau) \quad (11.217) \quad \{\text{eq:108}\}$$

The local velocity at contact can be written

$$u_{n,k+1}^{\tau+1} = G(\bar{q}_k)[v_{free}^\tau + WH^\top(\bar{q}_k)Q_{k+1}^{\tau+1} + WG^\top(\bar{q}_k)P_{k+1}^{\tau+1}] \quad (11.218) \quad \{\text{eq:109}\}$$

and for the equality constraints

$$u_{k+1}^{\tau+1} = H(\bar{q}_k)[v_{free}^\tau + WH^\top(\bar{q}_k)Q_{k+1}^{\tau+1} + WG^\top(\bar{q}_k)P_{k+1}^{\tau+1}] \quad (11.219) \quad \{\text{eq:110}\}$$

Finally, we get a linear relation between  $u_{n,k+1}^{\tau+1}$  and the multiplier

$$u_{k+1}^{\tau+1} = \begin{bmatrix} H(\bar{q}_k) \\ G(\bar{q}_k) \end{bmatrix} v_{free}^\tau + \begin{bmatrix} H(\bar{q}_k)WH^\top(\bar{q}_k) & H(\bar{q}_k)WG^\top(\bar{q}_k) \\ G(\bar{q}_k)WH^\top(\bar{q}_k) & G(\bar{q}_k)WG^\top(\bar{q}_k) \end{bmatrix} \begin{bmatrix} Q_{k+1}^{\tau+1} \\ P_{k+1}^{\tau+1} \end{bmatrix} \quad (11.220) \quad \{\text{eq:111}\}$$

**choices for  $\bar{q}_k$**  Two choices are possible for  $\bar{q}_k$

1.  $\bar{q}_k = q_k$
2.  $\bar{q}_k = q_{k+1}^\tau$

#### 11.6.1 Redaction note V. ACARY

todo list:

- add the projection step for the unit quaternion
- describe the computation of H and G that can be hybrid

### 11.6.4 Computation of the Jacobian in special case

**Moment of gyroscopic forces** Let us denote by the basis vector  $e_i$  given the  $i^{th}$  column of the identity matrix  $I_{3 \times 3}$ . The Jacobian of  $M_{gyr}$  is given by

$$\nabla_\Omega^\top M_{gyr}(\Omega) = \nabla_\Omega^\top(\Omega \times I\Omega) = [e_i \times I\Omega + \Omega \times Ie_i, i = 1, 2, 3] \quad (11.221) \quad \{\text{eq:112}\}$$

**Linear internal wrench** If the internal wrench is given by

$$F_{int}(t, q, v) = \begin{bmatrix} f_{int}(t, q, v) \\ M_{int}(t, q, v) \end{bmatrix} = Cv + Kq, \quad C \in \mathbf{R}^{6 \times 6}, \quad K \in \mathbf{R}^{6 \times 7} \quad (11.222) \quad \{\text{eq:113}\}$$

we get

$$\begin{aligned} \nabla_v F(t_{k+1}, q(v), v) &= h\theta KT(\bar{q}_k) + C \\ \nabla_v^\top \mathcal{R}(v) &= M - h\theta C - h^2\theta^2 KT(\bar{q}_k) \end{aligned} \quad (11.223) \quad \{\text{eq:114}\}$$

**External moment given in the inertial frame** If the external moment denoted by  $m_{ext}(t)$  is expressed in inertial frame, we have

$$M_{ext}(q, t) = R^T m_{ext}(t) = \Phi(p) m_{ext}(t) \quad (11.224) \quad \{\text{eq:115}\}$$

In that case,  $M_{ext}(q, t)$  appears as a function  $q$  and we need to compute its Jacobian w.r.t  $q$ . This computation needs the computation of

$$\nabla_p M_{ext}(q, t) = \nabla_p \Phi(p) m_{ext}(t) \quad (11.225) \quad \{\text{eq:116}\}$$

Let us compute first

$$\Phi(p) m_{ext}(t) = \begin{bmatrix} (1 - 2p_2^2 - 2p_3^2)m_{ext,1} + 2(p_1p_2 - p_3p_0)m_{ext,2} + 2(p_1p_3 + p_2p_0)m_{ext,3} \\ 2(p_1p_2 + p_3p_0)m_{ext,1} + (1 - 2p_1^2 - 2p_3^2)m_{ext,2} + 2(p_2p_3 - p_1p_0)m_{ext,3} \\ 2(p_1p_3 - p_2p_0)m_{ext,1} + 2(p_2p_3 + p_1p_0)m_{ext,2} + (1 - 2p_1^2 - 2p_2^2)m_{ext,3} \end{bmatrix} \quad (11.226) \quad \{\text{eq:117}\}$$

Then we get

$$\nabla_p \Phi(p) m_{ext}(t) = \begin{bmatrix} -2p_3m_{ext,2} + 2p_2m_{ext,3} & 2p_2m_{ext,2} + 2p_3m_{ext,3} & -4p_2m_{ext,1} + 2p_1m_{ext,2} + 2p_0m_{ext,3} & -3p_3m_{ext,1} - 2p_0m_{ext,2} \\ 2p_3m_{ext,1} - 2p_1m_{ext,3} & 2p_2m_{ext,1} - 4p_1m_{ext,2} - 2p_1m_{ext,3} & & \end{bmatrix} \quad (11.227) \quad \{\text{eq:118}\}$$

### 11.6.5 Siconos implementation

The expression:  $\mathcal{R}_{free}(v_{k+1}^\tau) = M(v - v_k) - h\theta F(t_{k+1}, q(v_{k+1}^\tau), v_{k+1}^\tau) - h(1 - \theta)F(t_k, q_k, v_k)$  is computed in `MoreauJeanOSI::computeResidu()` and saved in `ds->workspace(DynamicalSystem::freeresidu)`

The expression:  $\mathcal{R}(v_{k+1}^\tau) = \mathcal{R}_{free}(v_{k+1}^\tau) - h(1 - \theta)F(t_k, q_k, v_k) - H^\top(\bar{q}_k)Q_{k+1} - G^\top(\bar{q}_k)P_{k+1}$  is computed in `MoreauJeanOSI::computeResidu()` and saved in `ds->workspace(DynamicalSystem::free)`.

#### 11.6.2 Redaction note V. ACARY

really a bad name for the buffer `ds->workspace(DynamicalSystem::free)`. Why we are choosing this name ? to save some memory ?

The expression:  $v_{free} = v_{k+1}^\tau - W\mathcal{R}_{free}(v_{k+1}^\tau)$  is compute in `MoreauJeanOSI::computeFreeState()` and saved in `d->workspace(DynamicalSystem::free)`.

The computation:  $v_{k+1}^{\tau+1} = v_{free} + WH^\top(\bar{q}_k)Q_{k+1}^{\tau+1} + WG^\top(\bar{q}_k)P_{k+1}^{\tau+1}$  is done in `MoreauJeanOSI::updateState` and stored in `d->twist()`.

## Chapter 12

# NewtonEulerR: computation of $\nabla_q H$

### 12.0.1 Gradient computation, case of NewtonEuler with quaternion

In the section,  $q$  is the quaternion of the dynamical system.

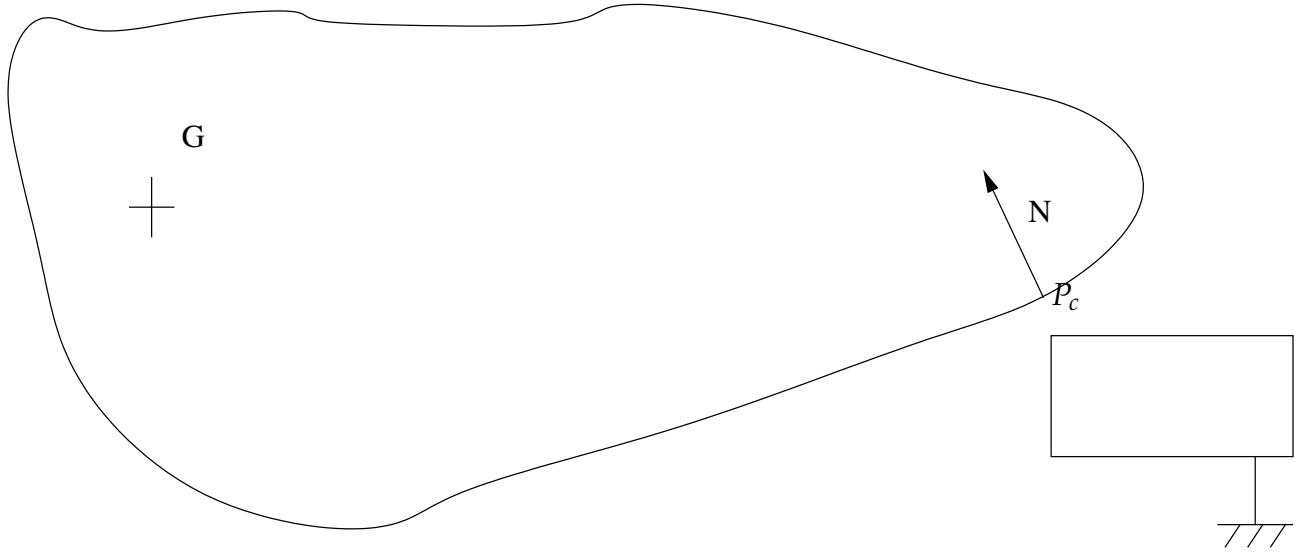


Figure 12.1: Impact of one DS.

{figCase}

The normal vector  $N$  is view as a constant.

$$\tilde{h}(q) = P_c\left(\frac{q}{\|q\|}\right)$$

$${}^t\nabla h(q)(\delta q) = \lim_{e \rightarrow 0} \frac{(\tilde{h}(q + e\delta q) - \tilde{h}(q)) \cdot N}{e}$$

$\nabla_q h$  consist in computing  $P_c\left(\frac{q + \delta q}{\|q + \delta q\|}\right) - P_c(q)$ .

$$GP(q) = qG_0P_0 {}^c q$$

$$\begin{aligned} GP\left(\frac{q + \delta q}{\|q + \delta q\|}\right) &= (q + \delta q)G_0P_0 {}^c (q + \delta q) \frac{1}{\|q + \delta q\|^2} \\ &= (q + \delta q) {}^c q GP(q) q {}^c (q + \delta q) \frac{1}{\|q + \delta q\|^2} \end{aligned}$$

$$\begin{aligned}
&= ((1,0,0,0) + \delta q \text{ }^c q) GP(q) ((1,0,0,0) + q \text{ }^c \delta q) \frac{1}{\|q + \delta q\|^2} \\
&= GP(q) + \delta q \text{ }^c q GP(q) + GP(q) q \text{ }^c \delta q + 0(\delta q)^2 \frac{1}{\|q + \delta q\|^2}
\end{aligned}$$

So, because G is independant of  $q$ :

$$P\left(\frac{q + \delta q}{\|q + \delta q\|}\right) - P(q) = q GP\left(\frac{q + \delta q}{\|q + \delta q\|}\right) - GP(q) = \delta q \text{ }^c q GP(q) + GP(q) q \text{ }^c \delta q + 0(\delta q)^2 + GP(q) \frac{1}{\|q + \delta q\|^2}$$

For the directional derivation, we chose  $\delta q = \epsilon * (1, 0, 0, 0)$ . using a equivalent to  $\frac{1}{1 + \epsilon}$

$$\lim_{\epsilon \rightarrow 0} \frac{P\left(\frac{q + \delta q}{\|q + \delta q\|}\right) - P(q)}{\epsilon} = \text{ }^c q GP(q) + GP(q) q - 2q_i GP(q)$$

For the directional derivation, we chose  $\delta q = \epsilon * (0, 1, 0, 0) = \epsilon * e_i$

$$\lim_{\epsilon \rightarrow 0} \frac{P\left(\frac{q + \delta q}{\|q + \delta q\|}\right) - P(q)}{\epsilon} = e_i \text{ }^c q GP(q) - GP(q) q e_i - 2q_i GP(q)$$

Application to the NewtonEulerRImpact:

$$\begin{aligned}
H &: \mathbb{R}^7 \rightarrow \mathbb{R} \\
\nabla_q H &\in \mathcal{M}^{1,7} \\
\nabla_q H &= \begin{pmatrix} N_x \\ N_y \\ N_z \\ ( \text{ }^c q GP(q) + GP(q) q - 2q_0 GP(q) ). N \\ (e_2 \text{ }^c q GP(q) - GP(q) q e_2 - 2q_1 GP(q) ). N \\ (e_3 \text{ }^c q GP(q) - GP(q) q e_3 - 2q_2 GP(q) ). N \\ (e_4 \text{ }^c q GP(q) - GP(q) q e_4 - 2q_3 GP(q) ). N \end{pmatrix}
\end{aligned}$$

### 12.0.2 Ball case

It is the case where  $GP = -N$ : for  $e_2$ :

$$\begin{aligned}
&(0, 1, 0, 0). (q_0, -\underline{p}). (0, -N) = \\
&\left( \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} . \underline{p}, \begin{pmatrix} q_0 \\ 0 \\ 0 \end{pmatrix} - \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} * \underline{p} \right). (0, -N) = \\
&\left( ?, -\underline{p}_x N - \left( \begin{pmatrix} q_0 \\ 0 \\ 0 \end{pmatrix} - \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} * \underline{p} \right) * N \right) =
\end{aligned}$$

and:

$$\begin{aligned}
&(0, -N). (q_0, \underline{p}). (0, 1, 0, 0) = \\
&(N. \underline{p}, -q_0 N - N * \underline{p}). (0, 1, 0, 0) = \\
&\left( ?, (N. \underline{p}) \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} + \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} * (q_0 N + N * \underline{p}) \right) =
\end{aligned}$$



$$\left( ?, (N.\underline{p}) \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} + q_0 \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} * N + \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} * (N * \underline{p}) \right)$$

sub then and get the resulting vector.N:

$$\left[ -\underline{p}_x N - N.\underline{p} \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} + () * N - \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} * (N * \underline{p}) \right].N =$$

$$-\underline{p}_x - N_x N.\underline{p} + 0 - \left( \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} * (N * \underline{p}) \right).N =$$

using  $a * (b * c) = b(a.c) - c(a.b)$  leads to

$$-q_1 - N_x N.\underline{p} - (q_1 N - N_x \underline{p}).N =$$

$$-q_1 - N_x N.\underline{p} - q_1 + N_x N.\underline{p} = -2q_1$$

for  $e1 = (1, 0, 0, 0)$ :

$$(q_0, -\underline{p}).(0, -N) = (?, -q_0 N + \underline{p} * N)$$

$$(0, -N).(q_0, \underline{p}) = (?, -q_0 N - \underline{p} * N)$$

So

$$\nabla_q H = \begin{pmatrix} N_x \\ N_y \\ N_z \\ 0 \\ 0 \\ 0 \\ 0 \end{pmatrix}$$

### 12.0.3 Case FC3D: using the local frame and momentum

$$\begin{pmatrix} m\dot{V} \\ I\dot{\Omega} + \Omega I \Omega \end{pmatrix} = \begin{pmatrix} Fect + R \\ Mext_{R_{obj}} + (R * PG)_{R_{obj}} \end{pmatrix}$$

with \* vectoriel product,  $R$  reaction in the globla frame.  $P$  the point of contact.  $r$  is the reaction in the local frame.  $M_{R_{obj}toR_{abs}} = M_{R_{abs}toR_{obj}}^t r = R$  with:

$$M_{R_C to R_{abs}} = \begin{pmatrix} nx & t_1x & t_2x \\ ny & t_1y & t_2y \\ nz & t_1z & t_2z \end{pmatrix}$$

we have :

$$\begin{pmatrix} R \\ (R * PG)_{R_{obj}} \end{pmatrix} = \begin{pmatrix} I_3 \\ M_{R_{abs}toR_{obj}} N_{PG} \end{pmatrix}.R$$

$$= \begin{pmatrix} I_3 \\ M_{R_{abs}toR_{obj}} N_{PG} \end{pmatrix}.M_{R_{obj}toR_{abs}} r$$

$$N_{PG} = \begin{pmatrix} 0 & PG_z & -PG_y \\ -PG_z & 0 & PG_x \\ PG_y & -PG_x & 0 \end{pmatrix}$$

that is:

$$\begin{pmatrix} m\dot{V} \\ I\dot{\Omega} + \Omega I \Omega \end{pmatrix} = \begin{pmatrix} M_{R_C to R_{abs}} \\ M_{R_{abs}toR_{obj}} N_{PG} M_{R_C to R_{abs}} \end{pmatrix} r$$

So  $jachqt = MN$

### 12.0.4 Case FC3D: using the local frame local velocities

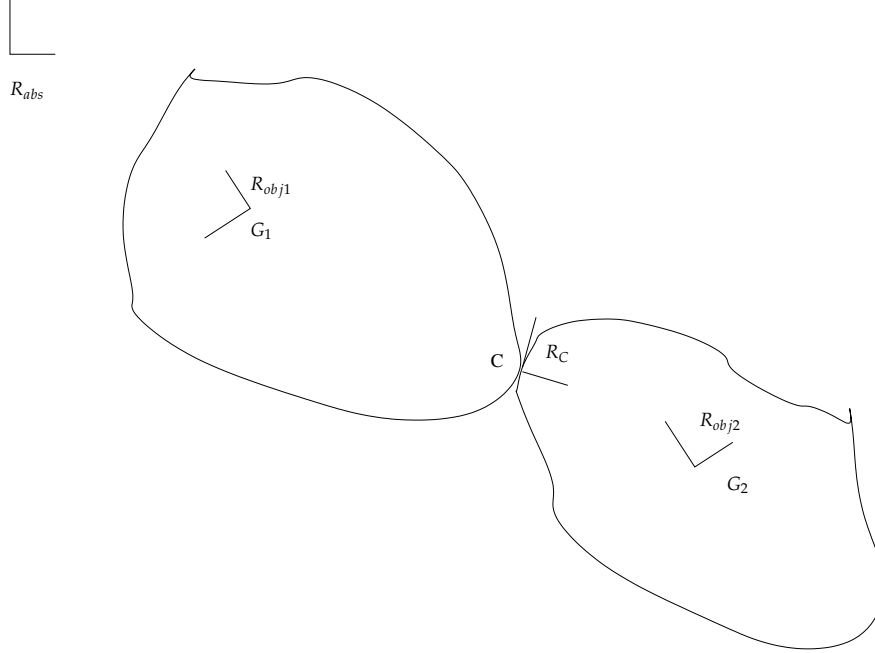


Figure 12.2: Two objects colliding.

{figCase}

We are looking for an operator named  $CT$  such that:

$$V_C = \begin{pmatrix} V_N \\ V_T \\ V_S \end{pmatrix}_{R_C} = CT \begin{pmatrix} V_{G1} R_{abs} \\ \Omega_1 R_{obj1} \\ V_{G2} R_{abs} \\ \Omega_2 R_{obj2} \end{pmatrix}$$

$$V_C = V_{G1} R_{abs} + w_1 * G_1 P_{R_{abs}} - (V_{G2} R_{abs} + w_2 * G_1 P_{R_{abs}})$$

where  $w_1$  and  $w_2$  are given in  $R_{abs}$ . We note  $M_{R_{obj1}toR_{abs}}$  the matrice converting the object 1 coordinate to the absolute coordinate. We note  $N_{GP}$  the matrice such that  $w_1 * G_1 P_{R_{abs}} = N_{GC} w_1$ . Endly, we note  $M_{R_{abs}toR_C}$  converting the absolute coordinate to the  $R_C$  frame. we get:

$$CT = M_{R_{abs}toR_C} \begin{pmatrix} I_3 & N_{G1C} M_{R_{obj1}toR_{abs}} & -I_3 & -N_{G2C} M_{R_{obj2}toR_{abs}} \end{pmatrix}$$

#### 12.0.4.a Expression of $M_{R_{obj1}toR_{abs}}$

Using quaternion, we get :

$$M_{R_{obj1}toR_{abs}} = \begin{pmatrix} q \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} {}^c q & q \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix} {}^c q & q \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix} {}^c q \end{pmatrix} \quad (12.1) \quad \{\text{eq:newton\_Mobjt}\}$$

#### 12.0.4.b Expression of $N_1$

$$N_{GC} = \begin{pmatrix} 0 & G_1 C_z & -G_1 C_y \\ -G_1 C_z & 0 & G_1 C_x \\ G_1 C_y & -G_1 C_x & 0 \end{pmatrix}$$

# Chapter 13

## Projection On constraints

### 13.0.1 Velocity formulation

The first step consists in doing a velocity formulation of the system:

$$\begin{aligned} M\dot{v} &= F_{ext} + B\lambda \\ \dot{q} &= Tv \\ y &= h(q) \\ NSLAW(y, \lambda, \dots) \end{aligned} \tag{13.1} \quad \{\text{NE\_Dyn1}\}$$

The constraint  $\dot{q} = Tv$  is sufficient to keep a normal quaternion. Because of the speed formulation,  $h(q)$  could violate the NSLAW. A solution could be to add a formulation in position. We must underline that the constraints  $|Q| = 1$  is implicit in this system. Indeed, the direction  $\dot{q} = Tv$  is tangential to the sphere.

### 13.0.2 Posion formulation

It consists in writting a position formulation on the system:

$$h(q) = \begin{pmatrix} HI(q) \\ HE(q) \end{pmatrix} \tag{13.2} \quad \{\text{NE\_Dyn1}\}$$

#### 13.0.2.a Approach using q

We are looking for  $q_1$  from  $q_0$ :

$$q_1 = q_0 + \nabla HI \wedge_I + \nabla HE \wedge_E \tag{13.3}$$

Assume that  $h(q_0)$  doesn't satisfy the constraints, ie  $HI(q_0) \not\perp 0$  or  $HE(q_0) \neq 0$ . Linearize  $h$  leads to:

$$0 \leq HI(q_0) + \nabla^t HI (\nabla HI \wedge_I + \nabla HE \wedge_E) \perp \wedge_I \geq 0 \tag{13.4}$$

$$0 = HE(q_0) + \nabla^t HE (\nabla HI \wedge_I + \nabla HE \wedge_E) \tag{13.5}$$

The getting system could be written has a MLCP:

$$C \ni h(q_0) + \nabla^t h(\nabla h \wedge), \wedge \in C^* \tag{13.6}$$

In the case of a quaternion  $Q$  for the rotation representation, it is noteworthy that this system doesn't deal with the constraints  $|Q| = 1$ . Thus, the direction  $(q_1, q_0)$  can be normal to this constraint, in that case this approach doesn't work. (It happens in practice) The solution that consists in normaliaed q after this formulation is not convenient because, it could be incompatible with  $|Q| = 1$ . A better approach is to add this constraint.

The constraint  $|Q| = 1$  in the system HE:

$$\tilde{H}E(q) = \begin{pmatrix} HE(q) \\ |Q| - 1 \end{pmatrix} \quad (13.7)$$

The formulation described above can be done.

### 13.0.2.b Approach using V

It consists in building the OSNSP using  $CT$  instead of  $C$ .

$$h(q_1) = h(q_0) + \nabla^t H \delta q \quad (13.8) \quad \{\text{NE\_projV}\}$$

ie:

$$h(q_1) = h(q_0) + \nabla^t H T V \quad (13.9) \quad \{\text{NE\_projV}\}$$

We are looking for  $q_1$  such that:

$$q_1 - q_0 = \nabla H \Lambda \quad (13.10)$$

We have

$$\delta q = TV, \quad {}^t T \delta q = {}^t T T V, \quad ({}^t T T)^{-1} {}^t T \delta q = V$$

ie

$$h(q_1) = h(q_0) + {}^t \nabla_q h T ({}^t T T)^{-1} {}^t T \nabla_q h \Lambda \quad (13.11)$$

With  $C = {}^t \nabla_q h$  leading to the problem:

$$K \ni h(q_0) + CT ({}^t T T)^{-1} {}^t (CT) \Lambda \in K^* \quad (13.12)$$

## Chapter 14

# Simulation of a Cam Follower System

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The free body dynamics can be described by a linear second order system. An external input is considered acting directly on the follower. This input is a non linear forcing component coming from the valve. The follower motion is constrained to a phase space region bounded by the cam position. The non conservative Newton restitution law is used for the computation of the post impact velocity. The cam is assumed to be massive therefore only rotational displacement is allowed. Under these assumptions, the free body dynamics of the follower can be described by

$$\mu \frac{d^2 u(t)}{dt^2} + \zeta \frac{du(t)}{dt} + \kappa u(t) = f_v(t), \quad \text{if } u(t) > c(t). \quad (14.1) \quad \{\text{eq:sols}\}$$

where  $\mu$ ,  $\zeta$  and  $\kappa$  are constant parameters for the follower mass, friction viscous damping and spring stiffness respectively. The state of the follower is given by the position  $u(t)$  and velocity  $v(t) = \frac{du}{dt}$ . The external forcing is given by  $f_v(t)$ . The cam angular position determines  $c(t)$  that defines the holonomic (i.e. constraint only on the position) rheonomic (i.e. time varying) constraint. The dynamic behavior when impacts occurs (i.e.  $u(t) = c(t)$ ) is modelled via Newton's impact law that in this case is given by

$$v(t^+) = \frac{dc}{dt} - r \left( v(t^-) - \frac{dc}{dt} \right) = (1+r) \frac{dc}{dt} - r v(t^-), \quad \text{if } u(t) = c(t). \quad (14.2) \quad \{\text{eq:il}\}$$

where  $v(t^+)$  and  $v(t^-)$  are the post and pre impact velocities respectively,  $\frac{dc}{dt}$  is the velocity vector of the cam at the contact point with the follower, and  $r \in [0, 1]$  is the restitution coefficient to model from plastic to elastic impacts. In Figure 14.1 is presented the schematic diagram of the physical cam-follower system. In Figure 14.1.a for  $t = 0$ , 14.1.b for  $t = \beta$ , and 14.1.c the profile of the constraint position  $\delta c(t)$ , velocity  $\frac{dc}{dt}(t)$  and acceleration  $\frac{d^2 c}{dt^2}(t)$ . It is possible to visualize the follower displacement as a function of the cam position. It is also important to notice that different types of cams and followers profiles are used in practical applications.

### 14.0.1 The cam-follower as a Lagrangian NSDS.

It is possible to completely describe the cam-follower system as a driven impact oscillator into the framework of *Lagrangian NSDS* using a translation in space. Setting  $\hat{u}(t) = u(t) - c(t)$  and  $\hat{v}(t) = v(t) - dc/dt$ , then equations (14.1) and (14.2) can be expressed as (the argument  $t$  will not be explicitly written)

$$\mu \frac{d^2 \hat{u}}{dt^2} + \zeta \frac{d\hat{u}}{dt} + \kappa \hat{u} = f_v - \left( \mu \frac{d^2 c}{dt^2} + \zeta \frac{dc}{dt} + \kappa c \right) \equiv \hat{f}, \quad \text{if } \hat{u} > 0. \quad (14.3) \quad \{\text{eq:trans}\}$$

$$\hat{v}^+ = -r \hat{v}^-, \quad \text{if } \hat{u} = 0. \quad (14.4)$$

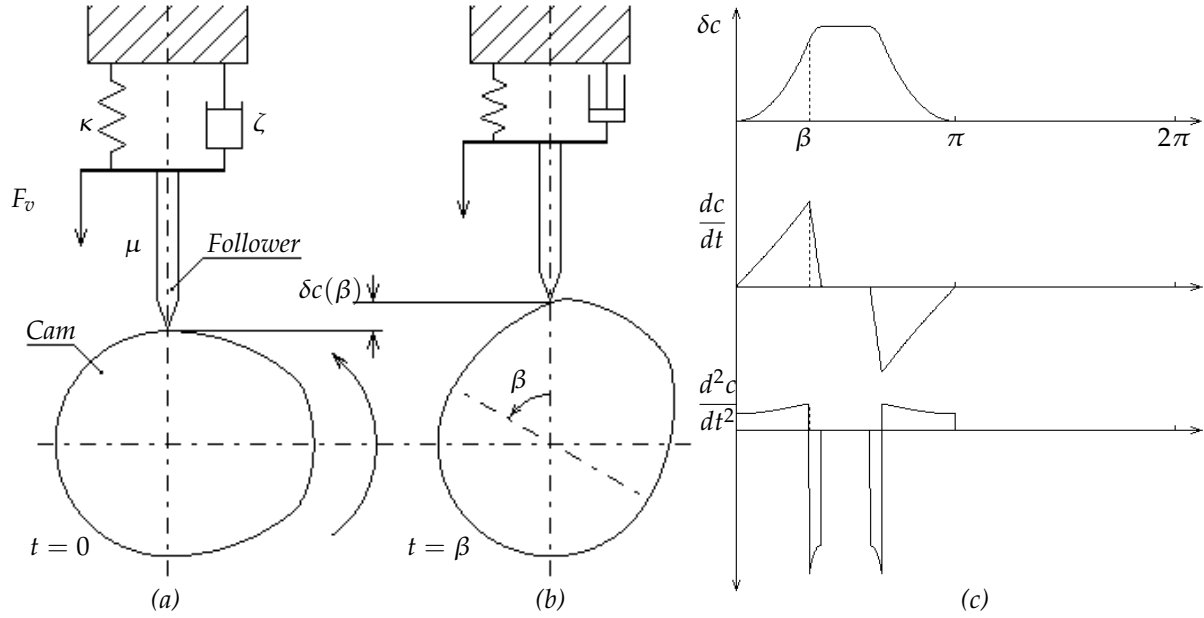


Figure 14.1: Cam-Shaft's schematics. (a)  $t=0$ . (b)  $t=\beta$ . (c) Constraint position  $\delta c(t)$ , velocity  $\frac{dc}{dt}(t)$  and acceleration  $\frac{d^2c}{dt^2}(t^2)$ .

{Fig:cam-shaft}

Using the framework presented in [2] we have that the equation of motion of a Lagrangian system may be stated as follows :

$$M(q)\ddot{q} + Q(q, \dot{q}) + F(\dot{q}, q, t) = F_{ext}(t) + R \quad (14.5) \quad \{\text{eq:lag1}\}$$

From the (14.3) we can derive all of the terms which define a Lagrangian NSDS. In our case the model is completely linear:

$$\begin{aligned} q &= [\hat{u}] \\ M(q) &= [\mu] \\ Q(q, \dot{q}) &= [0] \\ F(q, \dot{q}) &= [\zeta] \dot{q} + [\kappa] q \\ F_{ext} &= [\hat{f}] \end{aligned} \quad (14.6) \quad \{\text{eq:lag2}\}$$

The unilateral constraint requires that:

$$\hat{u} \geq 0$$

so we can obtain

$$\begin{aligned} y &= H^T q + b \\ H^T &= [1] \\ b &= 0 \end{aligned} \quad (14.7) \quad \{\text{eq:constr}\}$$

In the same way, the reaction force due to the constraint is written as follows:

$$R = H\lambda, \quad \text{with } H = [1]$$

The unilateral contact law may be formulated as follow:

$$0 \leq y \perp \lambda \geq 0 \quad (14.8) \quad \{\text{eq:119}\}$$

and the Newton's impact law:

$$\text{If } y = 0, \dot{y}^+ = -r\dot{y}^- \quad (14.9) \quad \{\text{eq:120}\}$$

### 14.0.2 Implementation in the platform

For the simulation of the cam follower system follow the steps

1. Move to the working directory `sample/CamFollower`  
`$cd sample/CamFollower`
2. Clean the directory from binary files using the `siconos` command  
`$siconos -c`
3. Compile the file `CamFollowerNoXml.cpp` in the sample folder (See the code at the end of the section)  
`$siconos CamFollowerNoXml.cpp`
4. Change the simulation parameters (*i.e.* Follower initial position and velocity, cam initial angle, simulations time, cam rotational speed in rpm, etc.) in the file `CamFollowerNoXml.cpp`.

Next we present the sample code for the `CamFollowerNoXml.cpp` file:

```
int main(int argc, char* argv[]) {
{
    // ===== Creation of the model =====
    // User-defined main parameters
    double rpm=358;
    double phi_0=0;
    unsigned int dsNumber = 1;    // the Follower and the ground
    unsigned int nDof = 1;        // degrees of freedom for the Follower
    double t0 = 0;                // initial computation time
    double T = 5;                // final computation time
    double h = 0.0001;           // time step
    int Kplot;
    Kplot=(int)(Tplot/h);
    double position_init = 0.4;    // initial position for lowest bead.
    double velocity_init = 0.4;    // initial velocity for lowest bead.

    // ===== Dynamical systems =====

    vector<DynamicalSystem*> vectorDS; // the list of DS
    vectorDS.resize(dsNumber,NULL);

    SiconosMatrix *Mass, *K, *C; // mass/rigidity/viscosity
    Mass = new SiconosMatrix(nDof,nDof);
    (*Mass)(0,0) = 1.221;
    K = new SiconosMatrix(nDof,nDof);
    (*K)(0,0) = 1430.8;
    C = new SiconosMatrix(nDof,nDof);
    (*C)(0,0) = 0;

    // Initial positions and velocities
    vector<SimpleVector*> position_0;
    vector<SimpleVector*> velocity_0;
    position_0.resize(dsNumber,NULL);
    velocity_0.resize(dsNumber,NULL);
    position_0[0] = new SimpleVector(nDof);
    velocity_0[0] = new SimpleVector(nDof);
    (*(position_0[0]))(0) = position_init;
```

```

(*(velocity_0[0]))(0) = velocity_init;

vectorDS[0] =
new LagrangianLinearTIDS(0,nDof,*(position_0[0]),*(velocity_0[0]),*Mass,*K,*C);

static_cast<LagrangianDS*>(vectorDS[0])
    ->setComputeFExtFunction("FollowerPlugin.so", "FollowerFExt");

// Example to set a list of parameters in FExt function.
// 1 - Create a simple vector that contains the required parameters.

// Here we set two parameters, the DS number.
SimpleVector * param = new SimpleVector(2);

(*param)(0)=rpm;
(*param)(1)=phi_0;
// 2 - Assign this param to the function FExt
static_cast<LagrangianDS*>(vectorDS[0])>setParametersListPtr(param,2);
// 2 corresponds to the position of FExt in the stl vector of possible parameters.
// 0 is mass, 1 Flnt.
// Now the cam rotational velocity in rpms will be available in FExt plugin.

// ===== Interactions =====

vector<Interaction*> interactionVector;
interactionVector.resize(1,NULL);
vector<DynamicalSystem*> *dsConcerned =
    new vector<DynamicalSystem*>(dsNumber);

// ===== Non Smooth Law =====
double e = 0.8;
// Interaction Follower-floor
SiconosMatrix *H = new SiconosMatrix(1,nDof);
(*H)(0,0) = 1.0;
NonSmoothLaw * nslaw = new NewtonImpactLawNSL(e);
Relation * relation = new LagrangianLinearR(*H);
(*dsConcerned)[0] = vectorDS[0];
interactionVector[0] = new Interaction("Follower-Ground",0,1, dsConcerned);
interactionVector[0]->setRelationPtr(relation);
interactionVector[0]->setNonSmoothLawPtr(nslaw);
// ===== Interactions =====

// ===== NonSmoothDynamicalSystem =====
bool isBVP =0;
NonSmoothDynamicalSystem * nsds =
    new NonSmoothDynamicalSystem(isBVP);

// Set DS of this NonSmoothDynamicalSystem
nsds->setDynamicalSystems(vectorDS);
// Set interactions of the NonSmoothDynamicalSystem
nsds->setInteractions(interactionVector);

// ===== Model =====

```



```

Model * Follower = new Model(t0,T);
// set NonSmoothDynamicalSystem of this model
Follower->setNonSmoothDynamicalSystemPtr(nsds);

// ===== Strategy =====

double theta = 0.5;          // theta for Moreau integrator
string solverName = "QP" ;

Strategy* S = new TimeStepping(Follower);

// - Time discretisation -
TimeDiscretisation * t = new TimeDiscretisation(h,S);

// - OneStepIntegrators -
vector<OneStepIntegrator*> vOSI;
vOSI.resize(dsNumber,NULL);
vOSI[0] = new Moreau(t,vectorDS[0],theta);
S->setOneStepIntegrators(vOSI);

// - OneStepNsProblem -
OneStepNSProblem * osnspb = new LCP(S,solverName,101, 0.0001,"max",0.6);
S->setOneStepNSProblemPtr(osnspb); // set OneStepNSProblem of the strategy
cout << "=== End of model loading === " << endl;
// ===== End of model definition=====

// ===== Computation=====

// — Strategy initialization —
S->initialize();
cout << "End of strategy initialisation" << endl;

int k = t->getK();           // Current step
int N = t->getNSteps();      // Number of time steps

// — Get the values to be plotted —
// -> saved in a matrix dataPlot
unsigned int outputSize = 8;

SiconosMatrix DataPlot(Kplot+1,outputSize );
// For the initial time step:

// time
DataPlot(k,0) = k*t->getH();

DataPlot(k,1) = static_cast<LagrangianDS*>(vectorDS[0])->getQ()(0);
DataPlot(k,2) = static_cast<LagrangianDS*>(vectorDS[0])->getVelocity()(0);
DataPlot(k,3) = (Follower->getNonSmoothDynamicalSystemPtr()->
    getInteractionPtr(0)->getLambda(1))(0);
DataPlot(k,4) = static_cast<LagrangianDS*>(vectorDS[0])->getFExt()(0);

// State of the Cam

```

```

double CamEqForce,CamPosition,CamVelocity,CamAcceleration;
CamEqForce=
    CamState(k*t->getH(),rpm,CamPosition,CamVelocity,CamAcceleration);
// Position of the Cam
DataPlot(k, 5) = CamPosition;
// Velocity of the Cam
DataPlot(k, 6) = CamVelocity;
// Acceleration of the Cam
DataPlot(k, 7) =
    CamPosition+static_cast<LagrangianDS*>(vectorDS[0])->getQ()(0);

// — Time loop —
cout << "Start computation ... " << endl;
while(k < N)
{
    // — Get values to be plotted —
    DataPlot(k,0) = k*t->getH();

    DataPlot(k,1) =
        static_cast<LagrangianDS*>(vectorDS[0])->getQ()(0);
    DataPlot(k,2) =
        static_cast<LagrangianDS*>(vectorDS[0])->getVelocity()(0);
    DataPlot(k,3) =
        (Follower->getNonSmoothDynamicalSystemPtr()->
        getInteractionPtr(0)->getLambda(1))(0);
    DataPlot(k,4) = static_cast<LagrangianDS*>(vectorDS[0])->getFExt()(0);

    CamEqForce=
    CamState(k*t->getH(),rpm,CamPosition,CamVelocity,CamAcceleration);

    DataPlot(k, 5) = CamPosition;
    DataPlot(k, 6) = CamVelocity;
    DataPlot(k, 7) = CamPosition+
        static_cast<LagrangianDS*>(vectorDS[0])->getQ()(0);
    // transfer of state i+1 into state i and time incrementation
    S->nextStep();
    // get current time step
    k = t->getK();
    // solve ...
    S->computeFreeState();
    S->computeOneStepNSProblem();
    // update
    S->update();
}
// — Output files —
DataPlot.rawWrite("result.dat", "ascii");
// — Free memory —
delete osnspb;
delete vOSI[0];
delete t;
delete S;
delete Follower;
delete nsds;

```

```
    delete interactionVector[0];
    delete relation;
    delete nslaw;
    delete H;
    delete dsConcerned;
    delete vectorDS[0];
    delete position_0[0];
    delete velocity_0[0];
    delete C;
    delete K;
    delete Mass;
}
```

### 14.0.3 Simulation

We have perform the simulation of the cam follower system for different values of the cam rotational speed with the SICONOS software package using a time-stepping numerical scheme with step size ( $h = 1e^{-4}$ ) and an event-driven scheme with minimum step size ( $h_{min} = 1e^{-12}$ ). Fig. 14.2 and 14.3 show the time simulations for different values of the cam rotational speed and Fig. 14.4 show the chaotic attractor at  $rpm = 660$  for impact and stroboscopic Poincaré sections.

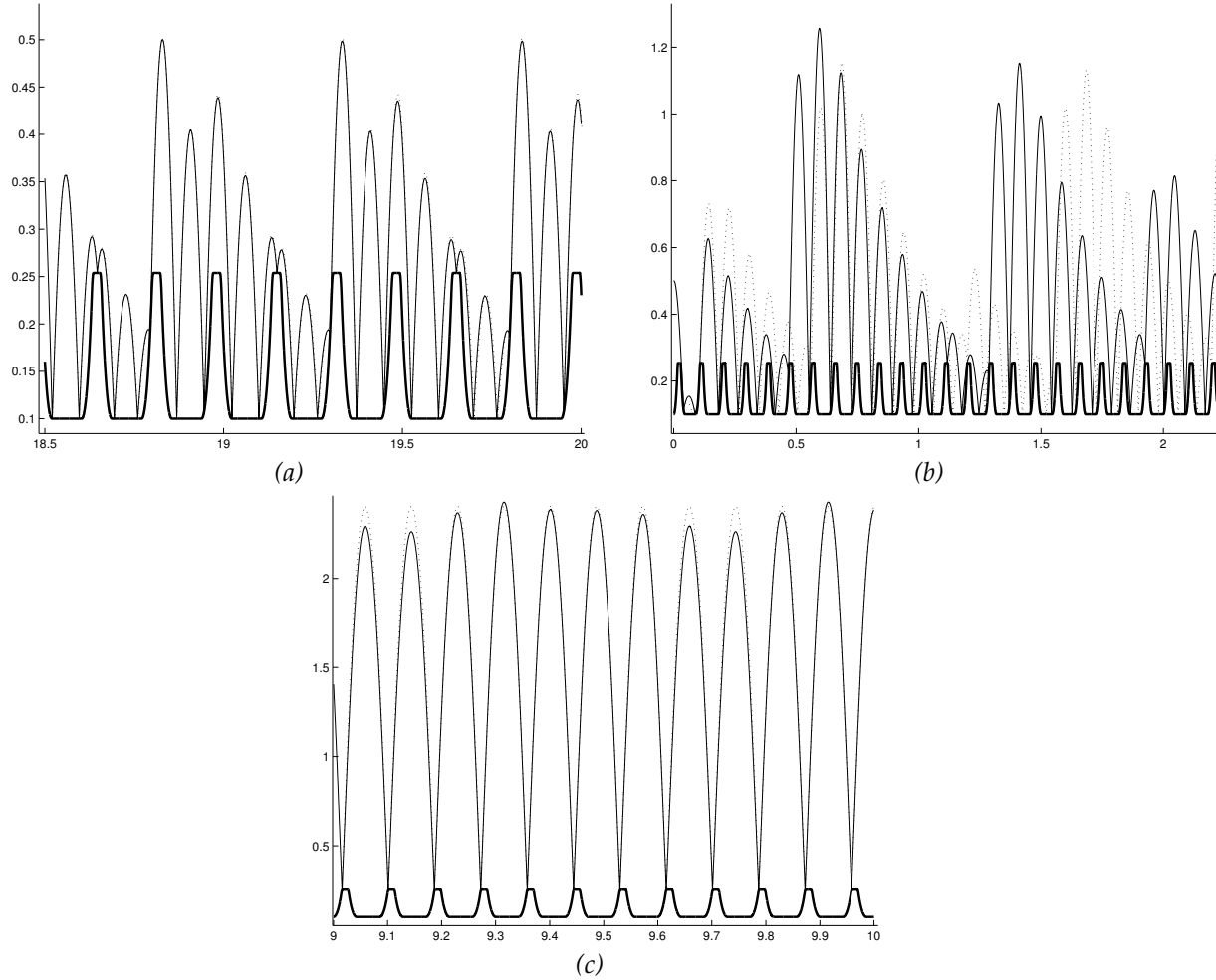


Figure 14.2: Time series using SICONOS platform. Time-stepping scheme (continuous line). Event-driven scheme (dashed line) (a)  $rpm=358$ . (b)  $rpm=660$ . (c)  $rpm=700$ .

{Fig:time\_compar

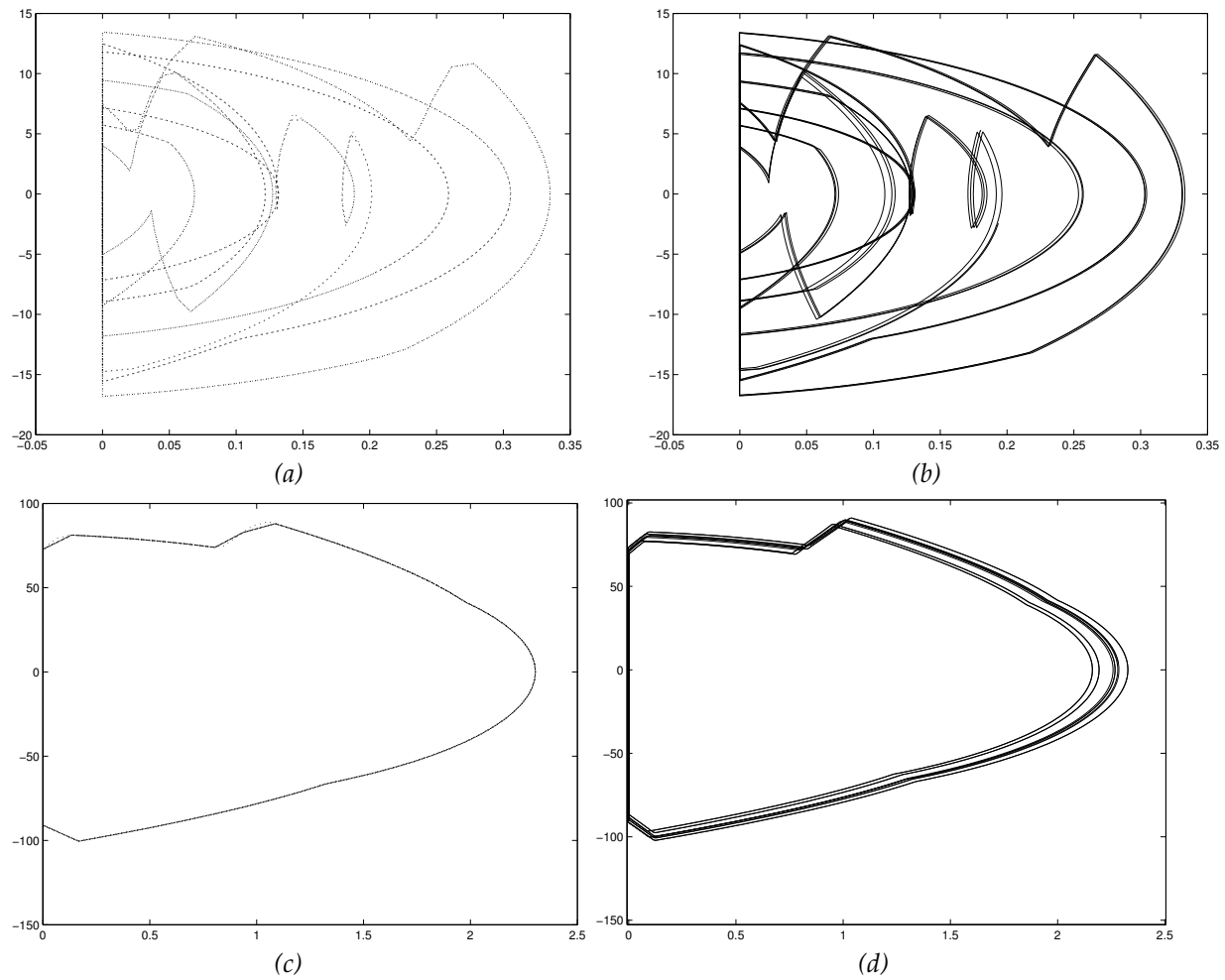


Figure 14.3: State space comparison using SICONOS platform. (a) rpm=358. Event Driven (b) rpm=358. Time Stepping ( $h = 1e^{-4}$ ) (c) rpm=700. Event Driven (d) rpm=700. Time Stepping ( $h = 1e^{-4}$ )

{Fig:state\_compa

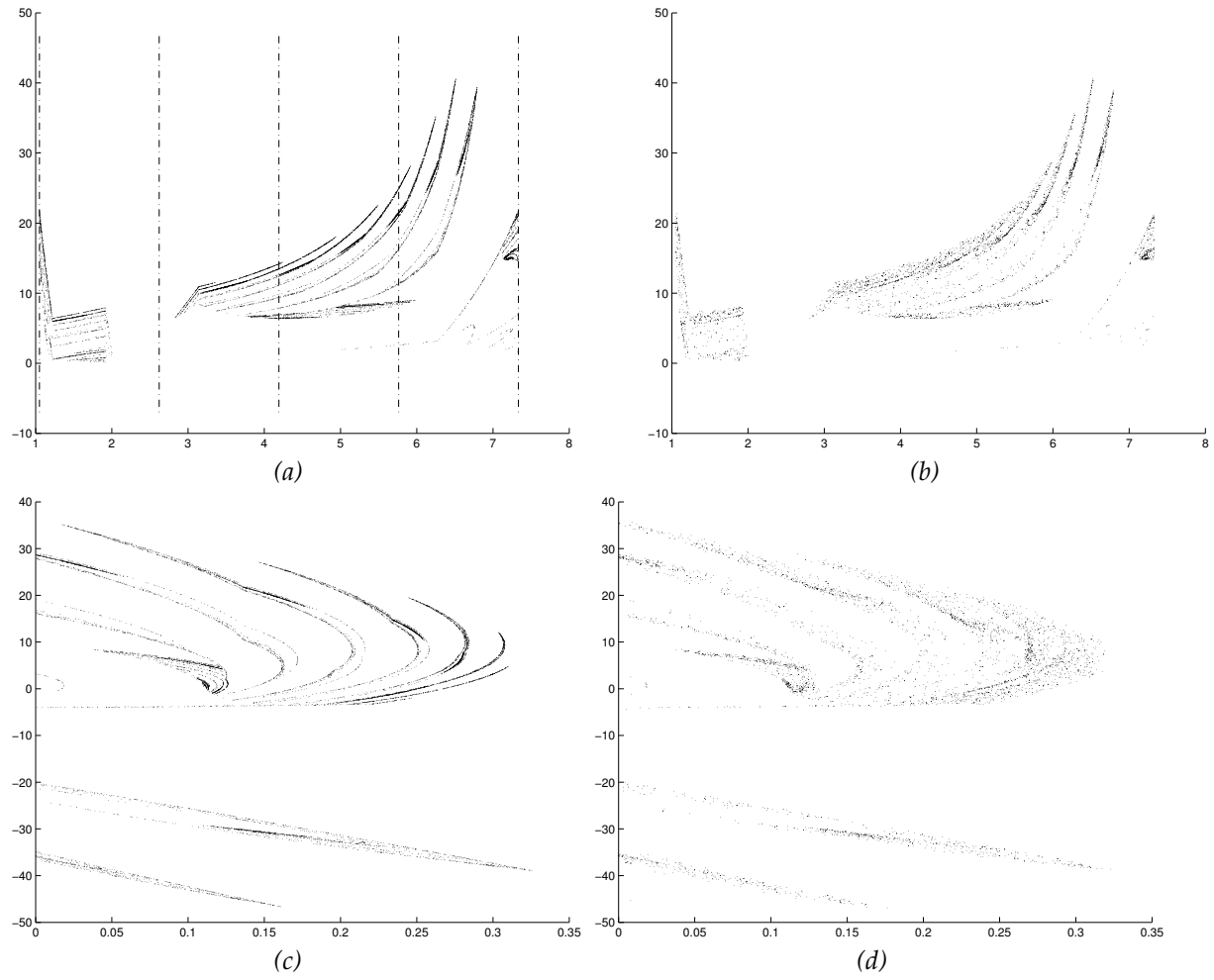


Figure 14.4: Attractors comparison using SICONOS platform at rpm=660. (a) Impact map. (Event Driven) (b) Impact Map. Time Stepping ( $h = 1e^{-4}$ ) (c) Stroboscopic map. (Event Driven) (d) Stroboscopic Map. Time Stepping ( $h = 1e^{-4}$ )

{Fig:attractor\_co

# Chapter 15

## Quartic Formulation

### 15.0.1 Slidding ?

It consists in finding  $\alpha > 0$  and  $R \in \partial K_\mu$  such that  $-\alpha \begin{pmatrix} 0 \\ R_T \end{pmatrix} = MR + q$ . That is :

$$\left[ M + \begin{pmatrix} 0 & 0 & 0 \\ 0 & \alpha & 0 \\ 0 & 0 & \alpha \end{pmatrix} \right] R + q = 0 \quad (15.1) \quad \{\text{eq\_quartic1}\}$$

#### 15.0.1.a $R_T$ is on a conic

The first line of the system 15.1 and the  $R \in \partial K_\mu$  is the intersection between a plan and a cone in  $\mathbb{R}^3$ , ended:

$$\begin{aligned} \mu R_N &= \| R_T \| \\ \frac{M_{11}}{\mu} \| R_T \| &= -q_1 - M_{12}R_{T1} - M_{13}R_{T2} \end{aligned} \quad (15.2) \quad \{\text{eq\_quartic2}\}$$

That is:

$$\begin{aligned} \mu^2 R_N^2 &= (R_{T1}^2 + R_{T2}^2) \\ \frac{M_{11}^2}{\mu^2} (R_{T1}^2 + R_{T2}^2) &= (-q_1 - M_{12}R_{T1} - M_{13}R_{T2})^2 \end{aligned} \quad (15.3) \quad \{\text{eq\_quartic2}\}$$

That means that  $R_T$  is contained in a conic, focus and directrice are:

$$\begin{aligned} \mathcal{D} : q_1 + M_{12}R_{T1} + M_{13}R_{T2} &= 0 \\ \text{focus} : \mathcal{O} \\ \frac{M_{11}^2}{\mu^2} \text{Dist}(\mathcal{O}, R_T)^2 &= \text{Dist}(\mathcal{D}, R_T)^2 (M_{12}^2 + M_{13}^2) \\ \frac{\text{Dist}(\mathcal{O}, R_T)}{\text{Dist}(\mathcal{D}, R_T)} &= \frac{\mu \sqrt{(M_{12}^2 + M_{13}^2)}}{M_{11}} = e \end{aligned} \quad (15.4) \quad \{\text{eq\_quartic3}\}$$

The parametric equation is:

$$\begin{aligned} R_{T1} &= r \cos(\theta) \\ R_{T2} &= r \sin(\theta) \\ r &= \frac{p}{1 + e \cos(\theta - \phi)} \end{aligned} \quad (15.5) \quad \{\text{eq\_quartic4}\}$$

With  $p$  an simple expression of  $M_{11}, M_{12}, M_{13}$ , and  $\phi$  a constant angle between  $\mathcal{D}$  and  $(O, R_{T1})$

**15.0.1.b The two last line of the system 15.1**

$$\frac{\|R_T\|}{\mu} \tilde{M}_1 + \left( \tilde{M} + \begin{pmatrix} \alpha & 0 \\ 0 & \alpha \end{pmatrix} \right) R_T + \tilde{q} = 0 \quad (15.6) \quad \{\text{eq\_quartic5}\}$$

$\tilde{M}$  is symetric, so it exists a unitary matrix  $V$  such that  $V\tilde{M}V^T = \begin{pmatrix} d_1 & 0 \\ 0 & d_2 \end{pmatrix}$ . One can get:

$$\frac{\|R_T\|}{\mu} V\tilde{M}_1 + V \left( \tilde{M} + \begin{pmatrix} \alpha & 0 \\ 0 & \alpha \end{pmatrix} \right) V^T V R_T + V\tilde{q} = 0 \quad (15.7) \quad \{\text{eq\_quartic6}\}$$

Rename:

$$\frac{\|\bar{R}_T\|}{\mu} \bar{M}_1 + \begin{pmatrix} d_1 + \alpha & 0 \\ 0 & d_2 + \alpha \end{pmatrix} \bar{R}_T + \bar{q} = 0 \quad (15.8) \quad \{\text{eq\_quartic7}\}$$

In the plan, either  $V$  is a rotation or a symetrie. So  $\bar{R}_T = V R_T$  is a conic with the same focus and a rotated directrice, it means that it exists  $\phi_1$  such that :

$$\begin{aligned} \bar{R}_{T1} &= r \cos(\theta) \\ \bar{R}_{T2} &= r \sin(\theta) \\ r &= \frac{p}{1 + e \cos(\theta - \phi_1)} \end{aligned} \quad (15.9) \quad \{\text{eq\_quartic8}\}$$

The equation 15.8 is :

$$\begin{aligned} (d_1 + \alpha) \bar{R}_{T1} &= -\bar{q}_1 + a_1 \|R_T\| \\ (d_2 + \alpha) \bar{R}_{T2} &= -\bar{q}_2 + a_2 \|R_T\| \end{aligned} \quad (15.10) \quad \{\text{eq\_quartic9}\}$$

The case ( $\bar{R}_{T1} = 0$  or  $\bar{R}_{T2} = 0$ ) has to be examine. We try to eliminate  $\alpha$ :

$$\begin{aligned} d_1 \bar{R}_{T1} \bar{R}_{T2} + \alpha \bar{R}_{T1} \bar{R}_{T2} &= -\bar{q}_1 \bar{R}_{T2} + a_1 \bar{R}_{T2} \|R_T\| \\ d_2 \bar{R}_{T1} \bar{R}_{T2} + \alpha \bar{R}_{T1} \bar{R}_{T2} &= -\bar{q}_2 \bar{R}_{T1} + a_2 \bar{R}_{T1} \|R_T\| \end{aligned} \quad (15.11) \quad \{\text{eq\_quartic10}\}$$

that leads to:

$$(d_1 - d_2) \bar{R}_{T1} \bar{R}_{T2} = -\bar{q}_1 \bar{R}_{T2} + \bar{q}_2 \bar{R}_{T1} + (a_1 \bar{R}_{T2} - a_2 \bar{R}_{T1}) \|R_T\| \quad (15.12) \quad \{\text{eq\_quartic10}\}$$

The parametric expression of  $\bar{R}_T$  leads to:

$$\begin{aligned} (d_1 - d_2) r^2 \cos(\theta) \sin(\theta) &= -\bar{q}_1 r \sin(\theta) + \bar{q}_2 r \cos(\theta) + r(a_1 r \sin(\theta) - a_2 r \cos(\theta)) \\ \text{ie: } (d_1 - d_2) r \cos(\theta) \sin(\theta) &= -\bar{q}_1 \sin(\theta) + \bar{q}_2 \cos(\theta) + r(a_1 \sin(\theta) - a_2 \cos(\theta)) \end{aligned} \quad (15.13) \quad \{\text{eq\_quartic11}\}$$

with the expression of  $r$ :

$$\begin{aligned} (d_1 - d_2) \frac{p}{1 + e \cos(\theta - \phi_1)} \cos(\theta) \sin(\theta) &= \\ -\bar{q}_1 \sin(\theta) + \bar{q}_2 \cos(\theta) + \frac{p}{1 + e \cos(\theta - \phi_1)} (a_1 \sin(\theta) - a_2 \cos(\theta)) & \\ \text{ie: } (d_1 - d_2) p \cos(\theta) \sin(\theta) &= \\ (1 + e \cos(\theta - \phi_1)) (-\bar{q}_1 \sin(\theta) + \bar{q}_2 \cos(\theta)) + p(a_1 \sin(\theta) - a_2 \cos(\theta)) & \end{aligned} \quad (15.14) \quad \{\text{eq\_quartic12}\}$$

$$\begin{aligned} \text{ie: } (d_1 - d_2) p \cos(\theta) \sin(\theta) &= \\ (1 + e(\cos(\theta) \cos(\phi_1) + \sin(\theta) \sin(\phi_1))) (-\bar{q}_1 \sin(\theta) + \bar{q}_2 \cos(\theta)) + p(a_1 \sin(\theta) - a_2 \cos(\theta)) & \end{aligned}$$

$$\begin{aligned} \text{ie: } (d_1 - d_2) p \cos(\theta) \sin(\theta) + \\ (1 + e \cos(\theta) \cos(\phi_1) + e \sin(\theta) \sin(\phi_1)) (\bar{q}_1 \sin(\theta) - \bar{q}_2 \cos(\theta)) + p(-a_1 \sin(\theta) + a_2 \cos(\theta)) &= 0 \end{aligned}$$

rename :

$$A \cos(\theta)^2 + B \sin(\theta)^2 + C \sin(\theta) \cos(\theta) + D \sin(\theta) + E \cos(\theta) = 0 \quad (15.15) \quad \{\text{eq\_quartic13}\}$$



with

$$\begin{aligned}
 A &= -e\bar{q}_2 \cos(\phi_1) \\
 B &= e\bar{q}_1 \sin(\phi_1) \\
 C &= (d_1 - d_2)p + e \cos(\phi_1)\bar{q}_1 - e \sin(\phi_1)\bar{q}_2 \\
 D &= \bar{q}_1 - pa_1 \\
 E &= -\bar{q}_2 + pa_2
 \end{aligned} \tag{15.16} \quad \{\text{eq\_quartic12}\}$$

rename : Using the following set of unknown :

$$\begin{aligned}
 t &= \tan(\theta/2) \\
 \sin(\theta) &= \frac{2t}{1+t^2} \\
 \cos(\theta) &= \frac{1-t^2}{1+t^2}
 \end{aligned} \tag{15.17} \quad \{\text{eq\_quartic14}\}$$

leads to:

$$\begin{aligned}
 &A \frac{(1-t^2)^2}{1+t^2} + B \frac{4t^2}{1+t^2} + C \frac{2t(1-t^2)}{1+t^2} + D2t + E(1-t^2) = 0 \\
 \text{ie: } &A(1-t^2)^2 + 4Bt^2 + C2t(1-t^2) + 2Dt(1+t^2) + E(1-t^2)(1+t^2) = 0 \\
 \text{ie: } &P_4 = A - E \quad P_3 = -2C + 2D \quad P_2 = 4B - 2A \quad P_1 = 2C + 2D \quad P_0 = A + E
 \end{aligned} \tag{15.18} \quad \{\text{eq\_quartic13}\}$$

Finally, we get 4 possible values for  $R_T$ , checking the sign of  $\alpha$  and  $R_N$  selects the solutions.

#### 15.0.1.c case $R_{T12} = 0$

From 15.10,  $R_{T1}$  leads to:

$$\begin{aligned}
 \| R_T \| &= |\bar{R}_{T2}| = \frac{\bar{q}_1}{a_1} \\
 \bar{R}_T &= \begin{pmatrix} 0 \\ \pm \frac{\bar{q}_1}{a_1} \end{pmatrix}
 \end{aligned} \tag{15.19} \quad \{\text{eq\_quartic14}\}$$

From 15.10,  $R_{T2}$  leads to:

$$\begin{aligned}
 \| R_T \| &= |\bar{R}_{T1}| = \frac{\bar{q}_2}{a_2} \\
 \bar{R}_T &= \begin{pmatrix} \pm \frac{\bar{q}_2}{a_2} \\ 0 \end{pmatrix}
 \end{aligned} \tag{15.20} \quad \{\text{eq\_quartic14}\}$$

From  $\bar{R}_T$ , we have to check the coherence with the equation 15.9. If it is on the conic, we compute  $R$ , and the sign condition of the equation 15.1 must be check.

## Chapter 16

# Alart–Curnier Formulation

### 16.1 Reduced formulation to local variables.

#### 16.1.1 Formulation

Let us start with

$$\begin{aligned}\Phi_1(U, P) &= -U_{k+1} + \widehat{W}P_{k+1} + U_{\text{free}} \\ \Phi_2(U, P) &= P_N - \text{proj}_{\mathbb{R}_+^a}(P_N - \rho_N \circ (U_N + e \circ U_{N,k})) \\ \Phi_3(U, P) &= P_T - \text{proj}_{\widehat{\mathbf{D}}(P_N, U_N)}(P_T - \rho_T \circ U_T)\end{aligned}\tag{16.1} \quad \{\text{eq:AC-L7}\}$$

where the modified friction disk for a contact  $\alpha$  is

$$\widehat{\mathbf{D}}^\alpha(P_{N,k+1}^\alpha, U_{N,k+1}^\alpha) = \mathbf{D}(\mu(\text{proj}_{\mathbb{R}_+}(P_{N,k+1}^\alpha - \rho_N^\alpha(U_{N,k+1}^\alpha + e^\alpha U_{N,k}^\alpha))).\tag{16.2} \quad \{\text{eq:AC-L3}\}$$

#### 16.1.2 Structure of the Jacobians

Let us denote the one element of the generalized Jacobian by  $H(U, P) \in \partial\Phi(U, P)$  which has the structure

$$H(U, P) = \begin{bmatrix} -I & 0 & \widehat{W}_{\text{NN}} & \widehat{W}_{\text{NT}} \\ 0 & -I & \widehat{W}_{\text{TN}} & \widehat{W}_{\text{TT}} \\ \partial_{U_N}\Phi_2(U, P) & 0 & \partial_{P_N}\Phi_2(U, P) & 0 \\ \partial_{U_N}\Phi_3(U, P) & \partial_{U_T}\Phi_3(U, P) & \partial_{P_N}\Phi_3(U, P) & \partial_{P_T}\Phi_3(U, P) \end{bmatrix}\tag{16.3} \quad \{\text{eq:AC-L6}\}$$

#### 16.1.3 Computation of the gradients

Let us consider the single contact case.

**Computation of the gradients of  $\Phi_2$**

$$\Phi_2(U, P) = P_N - \text{proj}_{\mathbb{R}_+^a}(P_N - \rho_N(U_N + eU_{N,k}))\tag{16.4} \quad \{\text{eq:AC-T1}\}$$

- If  $P_N - \rho_N(U_N + eU_{N,k}) \geq 0$ , we get

$$\Phi_2(U, P) = +\rho_N(U_N + eU_{N,k})\tag{16.5} \quad \{\text{eq:AC-T2}\}$$

and

$$\begin{aligned}\partial_{U_N} \Phi_2(U, P) &= +\rho_N \\ \partial_{P_N} \Phi_2(U, P) &= 0\end{aligned}\tag{16.6} \quad \{\text{eq:AC-T3}\}$$

- If  $P_N - \rho_N(U_N + eU_{N,k}) < 0$ , we get

$$\Phi_2(U, P) = P_N \tag{16.7} \quad \{\text{eq:AC-T4}\}$$

and

$$\begin{aligned}\partial_{U_N} \Phi_2(U, P) &= 0 \\ \partial_{P_N} \Phi_2(U, P) &= 1\end{aligned}\tag{16.8} \quad \{\text{eq:AC-T5}\}$$

### Computation of the gradients of $\Phi_3$

$$\Phi_3(U, P) = P_T - \text{proj}_{\hat{D}(P_N, U_N)}(P_T - \rho_T U_T) \tag{16.9} \quad \{\text{eq:AC-TT1}\}$$

- If  $\|P_T - \rho_T U_T\| \leq \mu \max(0, P_N - \rho_N(U_N + eU_{N,k}))$ , we get

$$\Phi_3(U, P) = +\rho_T U_T \tag{16.10} \quad \{\text{eq:AC-TT2}\}$$

and

$$\begin{aligned}\partial_{U_N} \Phi_3(U, P) &= 0 \\ \partial_{P_N} \Phi_3(U, P) &= 0 \\ \partial_{U_T} \Phi_3(U, P) &= +\rho_T \\ \partial_{P_T} \Phi_3(U, P) &= 0\end{aligned}\tag{16.11} \quad \{\text{eq:AC-TT3}\}$$

- If  $\|P_T - \rho_T U_T\| > \mu \max(0, P_N - \rho_N(U_N + eU_{N,k}))$ , we get

$$\Phi_3(U, P) = P_T - \mu \max(0, P_N - \rho_N(U_N + eU_{N,k})) \frac{P_T - \rho_T U_T}{\|P_T - \rho_T U_T\|} \tag{16.12} \quad \{\text{eq:AC-TT4}\}$$

- If  $P_N - \rho_N(U_N + eU_{N,k}) \leq 0$ , we get

$$\Phi_3(U, P) = P_T \tag{16.13} \quad \{\text{eq:AC-TT5}\}$$

and

$$\begin{aligned}\partial_{U_N} \Phi_3(U, P) &= 0 \\ \partial_{P_N} \Phi_3(U, P) &= 0 \\ \partial_{U_T} \Phi_3(U, P) &= 0 \\ \partial_{P_T} \Phi_3(U, P) &= I_2\end{aligned}\tag{16.14} \quad \{\text{eq:AC-TT6}\}$$

- If  $P_N - \rho_N(U_N + eU_{N,k}) > 0$ , we get

$$\Phi_3(U, P) = P_T - \mu(P_N - \rho_N(U_N + eU_{N,k})) \frac{P_T - \rho_T U_T}{\|P_T - \rho_T U_T\|} \tag{16.15} \quad \{\text{eq:AC-TT7}\}$$

and

$$\begin{aligned}
\partial_{U_N} \Phi_3(U, P) &= \mu \rho_N \frac{P_T - \rho_T U_T}{\|P_T - \rho_T U_T\|} \text{WARNING case was not taken into account} \\
\partial_{P_N} \Phi_3(U, P) &= -\mu \frac{P_T - \rho_T U_T}{\|P_T - \rho_T U_T\|} \\
\partial_{U_T} \Phi_3(U, P) &= \mu \rho_T (P_N - \rho_N (U_N + e U_{N,k})) \Gamma(P_T - \rho_T U_T) \\
\partial_{P_T} \Phi_3(U, P) &= I_2 - \mu (P_N - \rho_N (U_N + e U_{N,k})) \Gamma(P_T - \rho_T U_T)
\end{aligned} \tag{16.16} \quad \{\text{eq:AC-TT8}\}$$

### 16.1.4 Rearranging the cases

TO BE COMPLETED

## 16.2 Formulation with global variables.

### 16.2.1 Formulation

Let us start with

$$\begin{aligned}
\Psi_1^a(v, U, P) &= -\hat{M} v_{k+1} + H P_{k+1} + q \\
\Psi_1^b(v, U, P) &= -U_{k+1} + H^\top v_{k+1} + b \\
\Psi_2(v, U, P) &= P_N - \text{proj}_{\mathbb{R}_+^a} (P_N - \rho_N \circ (U_N + e \circ U_{N,k})) \\
\Psi_3(v, U, P) &= P_T - \text{proj}_{\hat{D}(P_N, U_N)} (P_T - \rho_T \circ U_T)
\end{aligned} \tag{16.17} \quad \{\text{eq:GAC-L1}\}$$

where the modified friction disk for a contact  $\alpha$  is

$$\hat{D}^\alpha(P_{N,k+1}^\alpha, U_{N,k+1}^\alpha) = D(\mu(\text{proj}_{\mathbb{R}_+^a} (P_{N,k+1}^\alpha - \rho_N^\alpha (U_{N,k+1}^\alpha + e^\alpha U_{N,k}^\alpha))). \tag{16.18} \quad \{\text{eq:GAC-L2}\}$$

### 16.2.2 Structure of the Jacobians

Let us denote the one element of the generalized Jacobian by  $H(v, U, P) \in \partial \Psi(s, U, P)$  which has the structure

$$H(v, U, P) = \begin{bmatrix} -\hat{M} & 0 & 0 & H_N & H_T \\ H_N^\top & -I & 0 & 0 & 0 \\ H_T^\top & 0 & -I & 0 & 0 \\ 0 & \partial_{U_N} \Psi_2(v, U, P) & 0 & \partial_{P_N} \Psi_2(v, U, P) & 0 \\ 0 & \partial_{U_N} \Psi_3(v, U, P) & \partial_{U_T} \Psi_3(v, U, P) & \partial_{P_N} \Psi_3(v, U, P) & \partial_{P_T} \Psi_3(v, U, P) \end{bmatrix} \tag{16.19} \quad \{\text{eq:GAC-L3}\}$$

We clearly have

$$\begin{aligned}
\partial_U \Psi_2(v, U, P) &= \partial_U \Phi_2(U, P) \\
\partial_P \Psi_2(v, U, P) &= \partial_P \Phi_2(U, P) \\
\partial_U \Psi_3(v, U, P) &= \partial_U \Phi_3(U, P) \\
\partial_P \Psi_3(v, U, P) &= \partial_P \Phi_3(U, P)
\end{aligned} \tag{16.20} \quad \{\text{eq:equivalentJaco}\}$$

and we get

$$H(v, U, P) = \begin{bmatrix} -\widehat{M} & 0 & 0 & H_N & H_T \\ H_N^\top & -I & 0 & 0 & 0 \\ H_T^\top & 0 & -I & 0 & 0 \\ 0 & \partial_{U_N} \Phi_2(U, P) & 0 & \partial_{P_N} \Phi_2(U, P) & 0 \\ 0 & \partial_{U_N} \Phi_3(U, P) & \partial_{U_T} \Phi_3(U, P) & \partial_{P_N} \Phi_3(U, P) & \partial_{P_T} \Phi_3(U, P) \end{bmatrix} \quad (16.21) \quad \{\text{eq:GAC-L4}\}$$

### 16.2.3 Simplification ?

Since the second line  $\Psi_1^b$  is linear, we should be able to derive a reduced Jacobian using the chain rule. Let us define  $\tilde{\Psi}$

$$\tilde{\Psi}(v, P) = \Psi(v, H^\top v + b, P) \quad (16.22) \quad \{\text{eq:chainrule}\}$$

$$\tilde{\Psi}_1(v, P) = -\widehat{M}v_{k+1} + HP_{k+1} + q$$

$$\tilde{\Psi}_2(v, P) = P_N - \text{proj}_{\mathbb{R}_+^a}(P_N - \rho_N \circ (H_N^\top v + b_N + e \circ U_{N,k})) \quad (16.23) \quad \{\text{eq:GAC-L5}\}$$

$$\tilde{\Psi}_3(v, P) = P_T - \text{proj}_{\widehat{\mathbf{D}}(P_N, U_N)}(P_T - \rho_T \circ (H_T^\top v + b_T))$$

#### Chain rule

$$\begin{aligned} \partial_v \tilde{\Psi}_{2,3}(v, P) &= \partial_v \Psi_{2,3}(v, H^\top v + b, P) \\ &= H_N^\top \partial_{U_N} \Phi_{2,3}(H^\top v + b, P) + H_T^\top \partial_{U_T} \Phi_{2,3}(H^\top v + b, P) \end{aligned} \quad (16.24) \quad \{\text{eq:chainrule1}\}$$

$$H(v, P) = \begin{bmatrix} -\widehat{M} & H_N & H_T \\ H_N^\top \partial_{U_N} \Phi_2(H^\top v + b, P) & \partial_{P_N} \Phi_2(H^\top v + b, P) & 0 \\ H_N^\top \partial_{U_N} \Phi_3(H^\top v + b, P) + H_T^\top \partial_{U_T} \Phi_3(H^\top v + b, P) & \partial_{P_N} \Phi_3(H^\top v + b, P) & \partial_{P_T} \Phi_3(H^\top v + b, P) \end{bmatrix} \quad (16.25) \quad \{\text{eq:GAC-L6}\}$$

#### discussion

- Formulae has to be checked carefully
- I do not know if there an interest in the simplification. With sparse matrices, it is perhaps easier to deal with (16.21)

#### References

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