

# Developer's Notes

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# Chapter 1

## OneStepNSProblem formalisation for several interactions

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version	?

### 1.1 LinearDS - Linear Time Invariant Relations

#### 1.1.1 General notations

We consider  $n$  dynamical systems of the form:

$$\dot{x}_i = A_i x_i + R_i \quad (1.1)$$

Each system is of dimension  $n_i$ , and we denote  $N = \sum_{i=1}^n n_i$ .

An interaction,  $I_\alpha$  is composed with a non smooth law,  $nsLaw_\alpha$  and a relation:

$$y_\alpha = C_\alpha X_\alpha + D_\alpha \lambda_\alpha \quad (1.2)$$

The “dimension” of the interaction, ie the size of vector  $y_\alpha$ , is denoted  $m_\alpha$  and we set:

$$M = \sum_{\alpha=1}^m m_\alpha$$

$m$  being the number of interactions in the Non Smooth Dynamical System.

$X_\alpha$  is a vector that represents the DS concerned by the interaction. Its dimension is noted  $N_\alpha$ , this for  $n_\alpha$  systems in the interaction.

$C_\alpha$  is a  $m_\alpha \times N_\alpha$  row-blocks matrix and  $D_\alpha$  a  $m_\alpha \times m_\alpha$  square matrix.

$$C_\alpha = \begin{bmatrix} C_\alpha^i & C_\alpha^j & \dots \end{bmatrix} \quad (1.3)$$

with  $i, j, \dots \in \mathcal{DS}_\alpha$  which is the set of DS belonging to interaction  $\alpha$ .

We also have the following relation:

$$\begin{bmatrix} R_\alpha^i \\ R_\alpha^j \\ \dots \end{bmatrix} = B_\alpha \lambda_\alpha = \begin{bmatrix} B_\alpha^i \\ B_\alpha^j \\ \dots \end{bmatrix} \lambda_\alpha \quad (1.4)$$

$R_\alpha^i$  represents the contribution of interaction  $\alpha$  on the reaction of the dynamical system  $i$ , and  $B_\alpha^i$  is a  $n_i \times m_\alpha$  block matrix.

And so:

$$R_i = \sum_{\beta \in \mathcal{I}_i} R_\beta^i = \sum_{\beta \in \mathcal{I}_i} B_\beta^i \lambda_\beta \quad (1.5)$$

with  $\mathcal{I}_i$  the set of interactions in which dynamical system number  $i$  is involved.

Introducing the time discretization, we get:

$$x_i^{k+1} - x_i^k = hA_i x_i^{k+1} + hR_i^{k+1} \quad (1.6)$$

$$y_\alpha^{k+1} = C_\alpha X_\alpha^{k+1} + D_\alpha \lambda_\alpha^{k+1} \quad (1.7)$$

$$R_i^{k+1} = \sum_{\beta \in \mathcal{I}_i} B_\beta^i \lambda_\beta^{k+1} \quad (1.8)$$

ie, with  $W_i = (I - hA_i)^{-1}$ :

$$x_i^{k+1} = W_i x_i^k + hW_i R_i^{k+1} \quad (1.9)$$

$$y_\alpha^{k+1} = C_\alpha W_\alpha X_\alpha^k + C_\alpha hW_\alpha \sum_{\beta \in \mathcal{I}_i} B_\beta^i \lambda_\beta^{k+1} + D_\alpha \lambda_\alpha^{k+1} \quad (1.10)$$

$$= C_\alpha W_\alpha X_\alpha^k + (C_\alpha hW_\alpha B_\alpha + D_\alpha) \lambda_\alpha^{k+1} + \sum_{\beta \neq \alpha} \left( \sum_{i \in \mathcal{DS}_\alpha \cap \mathcal{DS}_\beta} hC_\alpha^i W_i B_\beta^i \lambda_\beta^{k+1} \right) \quad (1.11)$$

with

$$W_\alpha = \begin{bmatrix} W_i & 0 & \dots \\ 0 & W_j & \dots \\ 0 & \dots & \dots \end{bmatrix} \quad (1.12) \quad \{\text{Walpha}\}$$

the block-diagonal matrix of all the  $W$  for the dynamical systems involved in interaction  $\alpha$ .

The global-assembled  $Y$  vector, of dimension  $M$ , composed by  $m$   $y_\alpha$  subvectors, is given by:

$$Y_{k+1} = q_{OSNSP} + M_{OSNSP} \Lambda_{k+1} \quad (1.13)$$

or,

$$Y_{k+1} = \begin{bmatrix} y_1 \\ \dots \\ y_m \end{bmatrix}_{k+1} = \begin{bmatrix} C_1^1 & \dots & C_1^n \\ \vdots & \dots & \vdots \\ C_m^1 & \dots & C_m^n \end{bmatrix} \begin{bmatrix} W_1 & 0 & \dots & 0 \\ 0 & W_2 & \ddots & \vdots \\ \vdots & \ddots & \ddots & \vdots \\ 0 & \dots & 0 & W_n \end{bmatrix} \begin{bmatrix} x_1 \\ \vdots \\ \vdots \\ x_n \end{bmatrix}_k \quad (1.14)$$

$$+ \begin{bmatrix} D_1 + h \sum_{j \in \mathcal{DS}_1} C_1^j W_j B_1^j & h \sum_{j \in \mathcal{DS}_1 \cap \mathcal{DS}_2} C_1^j W_j B_2^j & \dots \\ \vdots & \ddots & \\ h \sum_{j \in \mathcal{DS}_m} C_m^j W_j B_{m-1}^j & D_m + h \sum_{j \in \mathcal{DS}_m \cap \mathcal{DS}_{m-1}} C_m^j W_j B_m^j & \end{bmatrix} \begin{bmatrix} \lambda_1 \\ \vdots \\ \lambda_m \end{bmatrix}_{k+1}$$

To sum it up, the block-diagonal term of matrix  $M_{OSNSP}$ , for block-row  $\alpha$  is:

$$D_\alpha + h \sum_{j \in \mathcal{DS}_\alpha} C_\alpha^j W_j B_\alpha^j \quad (1.15)$$

This is an  $m_\alpha \times m_\alpha$  square matrix. The extra-diagonal block term, in position  $(\alpha, \beta)$  is:

$$h \sum_{j \in \mathcal{DS}_\alpha \cap \mathcal{DS}_\beta} C_\alpha^j W_j B_\beta^j \quad (1.16)$$

and is a  $m_\alpha \times m_\beta$  matrix. This matrix differs from 0 when interactions  $\alpha$  and  $\beta$  are coupled, ie have common DS.

Or, for the relation  $l$  of interaction  $\alpha$ , we get:

$$D_{\alpha,l} + h \sum_{j \in \mathcal{DS}_\alpha} C_{\alpha,l}^j W_j B_\alpha^j \quad (1.17)$$

for the diagonal, and

$$h \sum_{j \in \mathcal{DS}_\alpha \cap \mathcal{DS}_\beta} C_{\alpha,l}^j W_j B_\beta^j \quad (1.18)$$

for extra-diagonal terms.

$D_{\alpha,l}$ , row number  $l$  of  $D_\alpha$ , the same for  $C_{\alpha,l}$

Finally, the linked-Interaction map provides, for each interaction (named “current interaction”), the list of all the interactions (named “linked interaction”) that have common dynamical system with the “current interaction”.

### 1.1.2 A simple example

We consider  $n = 3$  dynamical systems and  $m = 2$  interactions:

$$\begin{aligned} I_\mu &\rightarrow \mathcal{DS}_\mu = \{DS_1, DS_3\}, m_\mu = 3 \\ I_\theta &\rightarrow \mathcal{DS}_\theta = \{DS_2, DS_3\}, m_\theta = 1 \end{aligned}$$

The linked-interaction map is :

$$\begin{aligned} I_\mu &\rightarrow I_{\theta, commonDS} = DS_3 \\ I_\theta &\rightarrow I_{\mu, commonDS} = DS_3 \end{aligned}$$

And:

$$M = 4, N = \sum_{i=1}^3 n_i$$

$$\mathcal{I}_1 = \{I_\mu\}$$

$$\mathcal{I}_2 = \{I_\theta\}$$

$$\mathcal{I}_3 = \{I_\mu, I_\theta\}$$

$$y_1 = \begin{bmatrix} C_1^1 & C_1^3 \end{bmatrix} \begin{bmatrix} x_1 \\ x_3 \end{bmatrix} + D_1 \lambda_1 \quad (1.19)$$

$$y_2 = \begin{bmatrix} C_2^2 & C_2^3 \end{bmatrix} \begin{bmatrix} x_2 \\ x_3 \end{bmatrix} + D_2 \lambda_2 \quad (1.20)$$

$$\begin{bmatrix} R_1 \\ R_2 \\ R_3 \end{bmatrix} = \begin{bmatrix} B_1^1 \lambda_1 \\ B_2^2 \lambda_2 \\ B_1^3 \lambda_1 + B_2^3 \lambda_2 \end{bmatrix} \quad (1.21)$$

$$M_{OSNSP} = \begin{bmatrix} D_1 + hC_1^1 W_1 B_1^1 + hC_1^3 W_3 B_1^3 & hC_1^3 W_3 B_2^3 \\ hC_2^3 W_3 B_1^3 & D_2 + hC_2^2 W_2 B_2^2 + hC_2^3 W_3 B_2^3 \end{bmatrix} \begin{bmatrix} \lambda_1 \\ \lambda_2 \end{bmatrix}_{k+1} \quad (1.22)$$

### 1.1.3 relative degree

Let us consider the global vector

$$Y = \begin{bmatrix} y_1 \\ \dots \\ y_M \end{bmatrix} = CX + D\Lambda \quad (1.23)$$

We denote by  $r_j$  the relative degree of equation  $j$ ,  $j \in [1..M]$ . We have:

$$y_j = \sum_{i=1}^n C_j^i x_i + D_{j,j} \lambda_j + \sum_{i \neq j, i=1}^m D_{j,i} \lambda_i \quad (1.24)$$

$D_{j,i}$  a scalar and  $C_j^i$  a  $1 \times n_i$  line-vector.

If  $D_{jj} \neq 0$ , then  $r_j = 0$ . Else, we should consider the first derivative of  $y_j$ .

Before that, recall that:

$$R_i = \sum_{k=1}^M B_k^i \lambda_j \quad (1.25)$$

Through many of the  $B_j^i$  are equal to zero, we keep them all in the following lines.

Then:

$$\dot{y}_j = \sum_{i=1}^n C_j^i (A_i x_i + \sum_{k=1}^M B_k^i \lambda_k) + f(\lambda_k)_{k \neq j} \quad (1.26)$$

$$= \sum_{i=1}^n C_j^i (A_i x_i + B_j^i \lambda_j + \sum_{k=1, k \neq j}^M B_k^i \lambda_k) + \dots \quad (1.27)$$

So, if  $\sum_{i=1}^n C_j^i B_j^i \neq 0$  (note that this corresponds to the product between line  $j$  of  $C$  and column  $j$  of  $B$ )

then  $r_j = 1$  else we consider the next derivative, and so on.

In derivative  $r$ , the coefficient of  $\lambda_j$  will be:

$$coeff_j = \sum_{i=1}^n C_j^i (A_i)^{r-1} B_j^i \quad (1.28)$$

if  $coeff_j \neq 0$  then  $r_j = r$ .

## 1.2 LagrangianDS - Lagrangian Linear Relations

### 1.2.1 General notations

We consider  $n$  dynamical systems, lagrangian and non linear, of the form:

$$M_i(q_i) \ddot{q}_i + N_i(\dot{q}_i, q_i) = F_{Int,i}(\dot{q}_i, q_i, t) + F_{Ext,i}(t) + p_i \quad (1.29)$$

Each system if of dimension  $n_i$ , and we denote  $N = \sum_{i=1}^n n_i$ .

An interaction,  $I_\alpha$  is composed with a non smooth law,  $nslaw_\alpha$  and a relation:

$$y_\alpha = H_\alpha Q_\alpha + b_\alpha \quad (1.30)$$



The “dimension” of the interaction, ie the size of vector  $y_\alpha$ , is denoted  $m_\alpha$  and we set:

$$M_y = \sum_{\alpha=1}^m m_\alpha$$

$m$  being the number of interactions in the Non Smooth Dynamical System.

$Q_\alpha$  is a vector that represents the DS concerned by the interaction. Its dimension is noted  $N_\alpha$ , this for  $n_\alpha$  systems in the interaction.

$H_\alpha$  is a  $m_\alpha \times N_\alpha$  row-blocks matrix and  $b_\alpha$  a  $m_\alpha$  vector.

$$H_\alpha = \begin{bmatrix} H_\alpha^i & H_\alpha^j & \dots \end{bmatrix} \quad (1.31)$$

with  $i, j, \dots \in \mathcal{DS}_\alpha$  which is the set of DS belonging to interaction  $\alpha$ .

We also have the following relation:

$$\begin{bmatrix} R_\alpha^i \\ R_\alpha^j \\ \dots \end{bmatrix} = {}^t H_\alpha \lambda_\alpha = \begin{bmatrix} {}^t H_\alpha^i \\ {}^t H_\alpha^j \\ \dots \end{bmatrix} \lambda_\alpha \quad (1.32)$$

$R_\alpha^i$  represents the contribution of interaction  $\alpha$  on the reaction of the dynamical system  $i$ , and  ${}^t H_\alpha^i$  is a  $n_i \times m_\alpha$  block matrix.

And so:

$$R_i = \sum_{\beta \in \mathcal{I}_i} R_\beta^i = \sum_{\beta \in \mathcal{I}_i} H_\beta^i \lambda_\beta \quad (1.33)$$

with  $\mathcal{I}_i$  the set of interactions in which dynamical system number  $i$  is involved.

Introducing the time discretisation, we get:

$$\begin{aligned} \dot{q}_i^{k+1} &= \dot{q}_{free,i} + W_i R_i^{k+1} \\ \dot{y}_\alpha^{k+1} &= H_\alpha \dot{Q}_\alpha^{k+1} \end{aligned} \quad (1.34)$$

$$R_i^{k+1} = \sum_{\beta \in \mathcal{I}_i} H_\beta^i \lambda_\beta^{k+1} \quad (1.35)$$

ie,

$$y_\alpha^{k+1} = H_\alpha Q_\alpha^{free} + H_\alpha W_\alpha {}^t H_\alpha \lambda_\alpha + \sum_{i \in \mathcal{DS}_\alpha} \sum_{\beta \in \mathcal{I}_i, \alpha \neq \beta} H_\alpha^i W_i H_\beta^j \lambda_\beta \quad (1.36)$$

with  $W_\alpha$  given by (1.12).

The global-assembled  $Y$  vector, of dimension  $M$ , composed by  $m$   $y_\alpha$  subvectors, is given by:

$$Y_{k+1} = q_{OSNSP} + M_{OSNSP} \Lambda_{k+1} \quad (1.37)$$

with:

$$q_{OSNSP}^\alpha = H_\alpha Q_\alpha^{free} \quad (1.38)$$

and for  $M_{OSNSP}$ , the block-diagonal term for block-row  $\alpha$  is

$$\sum_{j \in \mathcal{DS}_\alpha} H_\alpha^j W_j {}^t H_\alpha^j \quad (1.39)$$

an  $m_\alpha \times m_\alpha$  square matrix. The extra-diagonal block term, in position  $(\alpha, \beta)$  is:

$$\sum_{j \in \mathcal{DS}_\alpha \cap \mathcal{DS}_\beta} H_\alpha^j W_j {}^t H_\beta^j \quad (1.40)$$

and is a  $m_\alpha \times m_\beta$  matrix. This matrix differs from 0 when interactions  $\alpha$  and  $\beta$  are coupled, ie have common DS.

Or, for the relation  $l$  of interaction  $\alpha$ , we get:

$$\sum_{j \in \mathcal{DS}_\alpha} H_{\alpha,l}^j W_j^t H_\alpha^j \quad (1.41)$$

for the diagonal, and

$$\sum_{j \in \mathcal{DS}_\alpha \cap \mathcal{DS}_\beta} H_{\alpha,l}^j W_j^t H_\beta^j \quad (1.42)$$

for extra-diagonal terms.

$H_{\alpha,l}$ , row number  $l$  of  $H_\alpha$ .

WARNING: depending on linear and non linear case for the DS, there should be a factor  $h$  ahead  $W$ . See Bouncing Ball template.

## 1.3 Block matrix approach

The built of the OSNSProblem matrix could be computed using block matrix structure. This section describe these matrices. It is not implemented in Siconos. Using previous notations,  $n$  is the number of DS.  $m$  the number of iterations.

### 1.3.1 Block matrix of DS

$$M\dot{X} = AX + R$$

where  $M = \text{diag}(M_1, \dots, M_n)$  and  $A = \text{diag}(A_1, \dots, A_n)$ .

$$R = B\lambda$$

$$B = \begin{pmatrix} B_1^1 \dots B_m^1 \\ \vdots \\ B_1^n \dots B_m^n \end{pmatrix}$$

Some of  $B_j^i$  doesn't exist.

### 1.3.2 Block matrix of interaction

$$Y = CX + D\lambda$$

with  $D = \text{diag}(D_1 \dots D_m)$  and

$$C = \begin{pmatrix} C_1^1 \dots C_m^1 \\ \vdots \\ C_1^n \dots C_m^n \end{pmatrix}$$

Some of  $C_j^i$  doesn't exist.

### 1.3.3 OSNSProblem using block matrices

The Matrix of the OSNS Problem could be assembled using the following block-product-matrices  $CWB$ .

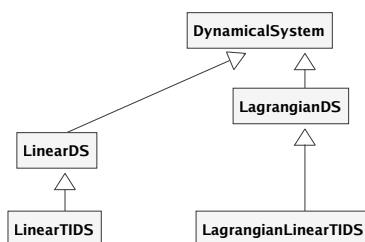
## Chapter 2

# Dynamical Systems formulations in Siconos.

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date	March 22, 2006
version	Kernel 1.1.4

### 2.1 Class Diagram

There are four possible formulation for dynamical systems in Siconos, two for first order systems and two for second order Lagrangian systems. The main class is `DynamicalSystem`, all other derived from this one, as shown in the following diagram:



{DSDiagram}

### 2.2 General non linear first order dynamical systems

→ **class** *DynamicalSystem*

This is the top class for dynamical systems. All other systems classes derived from this one.

A general dynamical systems is described by the following set of  $n$  equations, completed with initial conditions:

$$\dot{x} = f(x, t) + T(x)u(x, \dot{x}, t) + r \quad (2.1)$$

$$x(t_0) = x_0 \quad (2.2)$$

- $x$ : state of the system - Vector of size  $n$ .
- $f(x, t)$ : vector field - Vector of size  $n$ .

- $u(x, \dot{x}, t)$ : control term - Vector of size  $uSize$ .
- $T(x)$ :  $n \times uSize$  matrix, related to control term.
- $r$ : input due to non-smooth behavior - Vector of size  $n$ .

The Jacobian matrix,  $\nabla_x f(x, t)$ , of  $f$  according to  $x$ ,  $n \times n$  square matrix, is also a member of the class.

Initial conditions are given by the member  $x_0$ , vector of size  $n$ . This corresponds to  $x$  value when simulation is starting, ie after a call to `strategy->initialize()`.

There are plug-in functions in this class for  $f$  (vectorField),  $jacobianX$ ,  $u$  and  $T$ . All of them can handle a vector of user-defined parameters.

## 2.3 First order linear dynamical systems $\rightarrow$ class *LinearDS*

Derived from *DynamicalSystem*, described by the set of  $n$  equations and initial conditions:

$$\dot{x} = A(t)x(t) + Tu(t) + b(t) + r \quad (2.3)$$

$$x(t_0) = x_0 \quad (2.4)$$

With:

- $A(t)$ :  $n \times n$  matrix, state independent but possibly time-dependent.
- $b(t)$ : Vector of size  $n$ , possibly time-dependent.

Other variables are those of *DynamicalSystem* class.

$A$  and  $B$  have corresponding plug-in functions.

Warning: time dependence for  $A$  and  $b$  is not available at the time in the simulation part for this kind of dynamical systems.

Links with *vectorField* and its Jacobian are:

$$f(x, t) = A(t)x(t) + b(t) \quad (2.5)$$

$$jacobianX = \nabla_x f(x, t) = A(t) \quad (2.6)$$

## 2.4 Second order non linear Lagrangian dynamical systems $\rightarrow$ class *LagrangianDS*

Lagrangian second order non linear systems are described by the following set of  $nDof$  equations + initial conditions:

$$M(q)\ddot{q} + NNL(\dot{q}, q) + F_{Int}(\dot{q}, q, t) = F_{Ext}(t) + p \quad (2.7)$$

$$q(t_0) = q_0 \quad (2.8)$$

$$\dot{q}(t_0) = velocity_0 \quad (2.9)$$

With:

- $M(q)$ :  $nDof \times nDof$  matrix of inertia.
- $q$ : state of the system - Vector of size  $nDof$ .
- $\dot{q}$  or *velocity*: derivative of the state according to time - Vector of size  $nDof$ .

- $NNL(\dot{q}, q)$ : non linear terms, time-independent - Vector of size  $nDof$ .
- $F_{Int}(\dot{q}, q, t)$ : time-dependent linear terms - Vector of size  $nDof$ .
- $F_{Ext}(t)$ : external forces, time-dependent BUT do not depend on state - Vector of size  $nDof$ .
- $p$ : input due to non-smooth behavior - Vector of size  $nDof$ .

The following Jacobian are also member of this class:

- $\text{jacobianQFInt} = \nabla_q F_{Int}(t, q, \dot{q})$  -  $nDof \times nDof$  matrix.
- $\text{jacobianVelocityFInt} = \nabla_{\dot{q}} F_{Int}(t, q, \dot{q})$  -  $nDof \times nDof$  matrix.
- $\text{jacobianQNNL} = \nabla_q NNL(q, \dot{q})$  -  $nDof \times nDof$  matrix.
- $\text{jacobianVelocityNNL} = \nabla_{\dot{q}} NNL(q, \dot{q})$  -  $nDof \times nDof$  matrix.

There are plug-in functions in this class for  $F_{int}$ ,  $F_{Ext}$ ,  $M$ ,  $NNL$  and the four Jacobian matrices. All of them can handle a vector of user-defined parameters.

Links with first order dynamical system are:

$$n = 2nDof \quad (2.10)$$

$$x = \begin{bmatrix} q \\ \dot{q} \end{bmatrix} \quad (2.11)$$

$$f(x, t) = \begin{bmatrix} \dot{q} \\ M^{-1}(F_{Ext} - F_{Int} - NNL) \end{bmatrix} \quad (2.12)$$

$$\nabla_x f(x, t) = \begin{bmatrix} 0_{nDof \times nDof} & I_{nDof \times nDof} \\ \nabla_q(M^{-1})(F_{Ext} - F_{Int} - NNL) - M^{-1}\nabla_q(F_{Int} + NNL) & -M^{-1}\nabla_{\dot{q}}(F_{Int} + NNL) \end{bmatrix} \quad (2.13)$$

$$r = \begin{bmatrix} 0_{nDof} \\ p \end{bmatrix} \quad (2.14)$$

$$u(x, \dot{x}, t) = u_L(\dot{q}, q, t) \text{ (not yet implemented)} \quad (2.15)$$

$$T(x) = \begin{bmatrix} 0_{nDof} \\ T_L(q) \end{bmatrix} \text{ (not yet implemented)} \quad (2.16)$$

$$(2.17)$$

$$(2.18)$$

With  $0_n$  a vector of zero of size  $n$ ,  $0_{n \times m}$  a  $n \times m$  zero matrix and  $I_{n \times n}$ , identity  $n \times n$  matrix.

Warning: control terms ( $Tu$ ) are not fully implemented in Lagrangian systems. This will be part of future version.

## 2.5 Second order linear and time-invariant Lagrangian dynamical systems $\rightarrow$ class *LagrangianLinearTIDS*

{Sec:LagrangianL.

$$M\ddot{q} + C\dot{q} + Kq = F_{Ext}(t) + p \quad (2.19)$$

With:

- $C$ : constant viscosity  $nDof \times nDof$  matrix
- $K$ : constant rigidity  $nDof \times nDof$  matrix

And:

$$F_{Int} = C\dot{q} + Kq \quad (2.20)$$

$$NNL = 0_{nDof} \quad (2.21)$$

## Chapter 3

# Dynamical Systems implementation in Siconos.

author	F. P�rignon
date	November 7, 2006
version	Kernel 1.3.0

### 3.1 Introduction

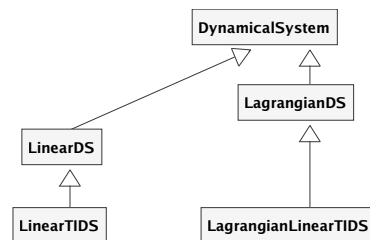
This document is only a sequel of notes and remarks on the way Dynamical Systems are implemented in Siconos.

It has to be completed, reviewed, reorganized etc etc for a future Developpers'Guide.

See also documentation in Doc/User/DynamicalSystemsInSiconos for a description of various dynamical systems types.

### 3.2 Class Diagram

There are four possible formulation for dynamical systems in Siconos, two for first order systems and two for second order Lagrangian systems. The main class is `DynamicalSystem`, all other derived from this one, as shown in the following diagram:



{DSDiagram}

### 3.3 Construction

Each constructor must:

- initialize all the members of the class and of the top-class if it exists

- allocate memory and set value for all required inputs
- allocate memory and set value for optional input if they are given as argument (in xml for example)
- check that given data are coherent and that the system is complete (for example, in the LagrangianDS if the internal forces are given as a plug-in, their Jacobian are also required. If they are not given, this leads to an exception).

No memory allocation is made for unused members  $\Rightarrow$  requires if statements in simulation. (if!=NULL ...).

### 3.3.1 DynamicalSystem

**Required data:**

n, x0, f, jacobianXF

**Optional:**

T,u

**Always allocated in constructor:**

x, x0, xFree, r, rhs, jacobianXF

Warning: default constructor is always private or protected and apart from the others and previous rules or remarks do not always apply to it. This for DS class and any of the derived ones.

### 3.3.2 LagrangianDS

**Required data:**

ndof, q0, velocity0, mass

**Optional:**

fInt and its Jacobian, fExt, NNL and its Jacobian.

**Always allocated in constructor:**

mass, q, q0, qFree, velocity, velocity0, velocityFree, p.

All other pointers to vectors/matrices are set to NULL by default.

Memory vectors are required but allocated during call to initMemory function.

Various rules:

- fInt (NNL) given as a plug-in  $\Rightarrow$  check that JacobianQ/Velocity are present (matrices or plug-in)
- any of the four Jacobian present  $\Rightarrow$  allocate memory for block-matrix jacobianX (connectToDS function)
- 

check: end of constructor or in initialize?

computeF and JacobianF + corresponding set functions: virtual or not?

## 3.4 Specific flags or members

- isAllocatedIn: to check inside-class memory allocation
- isPlugin: to check if operators are computed with plug-in or just directly set as a matrix or vector
- workMatrix: used to save some specific matrices in order to avoid recomputation if possible (inverse of mass ...)

### 3.5 plug-in management

DynamicalSystem class has a member named `parameterList` which is a *map*  $\langle \text{string}, \text{SimpleVector}^* \rangle$ , ie a list of pointers to `SimpleVector*`, with a string as a key to identified them. For example, `parametersList["mass"]` is a `SimpleVector*`, which corresponds to the last argument given in mass plug-in function.

By default, each parameters vectors must be initialized with a `SimpleVector` of size 1, as soon as the plug-in is declared. Moreover, to each vector corresponds a flag in `isAllocatedIn` map, to check if the corresponding vector has been allocated inside the class or not.

For example, in `DynamicalSystem`, if `isPlugin["vectorField"] == true`, then, during call to constructor or set function, it is necessary to defined the corresponding parameter:

```
parametersList["vectorField"] = newSimpleVector(1)
```

and to complete the `isAllocatedIn` flag:

```
isAllocatedIn["parameter_for_vectorField"] = true.
```



# Chapter 4

## Interactions

author	F. Pérignon
date	November 7, 2006
version	Kernel 1.3.0

### 4.1 Introduction

This document is only a sequel of notes and remarks on the way Interactions are implemented in Siconos.

It has to be completed, reviewed, reorganized etc etc for a future Developpers'Guide.  
See also documentation in Doc/User/Interaction.

### 4.2 Class Diagram

### 4.3 Description

#### 4.3.1 Redaction note F. PERIGNON

review of interactions (for EventDriven implementation) 17th May 2006.

- variable *nInter* renamed in *interactionSize*: represents the size of  $y$  and  $\lambda$ . NOT the number of relations !!
- add a variable *nsLawSize* that depends on the non-smooth law type.  
Examples:
  - NewtonImpact -> *nsLawSize* = 1
  - Friction 2D -> *nsLawSize* = 2
  - Friction 3D -> *nsLawSize* = 3
  - ...
  - *nsLawSize* = n with n dim of matrix D in :  $y = Cx + D\lambda$ , D supposed to be a full-ranked matrix.  
Warning: this case is represented by only one relation of size n.
- *numberOfRelations*: number of relations in the interaction,  $numberOfRelations = \frac{interactionSize}{nsLawSize}$ .

## Chapter 5

# Notes on the Non Smooth Dynamical System construction

author	F. Pérignon
date	November 7, 2006
version	Kernel 1.3.0

### 5.1 Introduction

### 5.2 Class Diagram

### 5.3 Description

Objects must be constructed in the following order:

- DynamicalSystems
- NonSmoothLaw: depends on nothing
- Relation: no link with an interaction during construction, this will be done during initialization.
- Interaction: default constructor is private and copy is forbidden. Two constructors: xml and from data. Required data are a DSSet, a NonSmoothLaw and a Relation (+ dim of the Interaction and a number).  
Interaction has an initialize function which allocates memory for y and lambda, links correctly the relation and initializes it .... This function is called at the end of the constructor. That may be better to call it in simulation->initialize? Pb: xml constructor needs memory allocation for y and lambda if they are provided in the input xml file.
- NonSmoothDynamicalSystem: default is private, copy forbidden. Two constructors: xml and from data. Required data are the DSSet and the InteractionsSet. The topology is declared and constructed (but empty) during constructor call of the nsds, but initialize in the Simulation, this because it can not be initialize until the nsds has been fully described (ie this to allow user to add DS, Inter ...) at any time in the model, but before simulation initialization).

### 5.4 misc

- no need to keep a number for Interactions? Only used in xml for OSI, to know which Interactions it holds.

- pb: the number of saved derivatives for  $y$  and  $\lambda$  in Interactions is set to 2. This must depends on the relative degree which is computes during Simulation initialize and thus too late. It is so not available when memory is allocated (Interaction construction). Problem-> to be reviewed.

## Chapter 6

# OneStepIntegrator and derived classes.

author	F. Pérignon
date	November 7, 2006
version	Kernel 1.3.0

### 6.1 Introduction

This document is only a sequel of notes and remarks on the way OneStepIntegrators are implemented in Siconos.

It has to be completed, reviewed, reorganized etc etc for a future Developers' Guide.

See also documentation in Doc/User/OneStepIntegrator for a description of various OSI.

### 6.2 Class Diagram

### 6.3 Misc

OSI review for consistency between Lsodar and Moreau:

- add set of DynamicalSystem\*
- add set of Interaction\*
- add link to strategy that owns the OSI
- remove td object in OSI -> future: replace it by a set of td (one per ds)
- add strat in constructors arg list

osi -> strat -> Model -> nsds -> topology

osi -> strat -> timeDiscretisation

let a timeDiscretisation object in the OSI? set of td (one per ds)?  
create a class of object that corresponds to DS on the simulation side ?  
will contain the DS, its discretization, theta for Moreau ... ?  
Allow setStrategyPtr operation? Warning: need reinitialisation.

Required input by user:

- list of DS or list of Interactions ?
- pointer to strategy
- ...

## 6.4 Construction

Each constructor must:

- 

### 6.4.1 Moreau

Two maps: one for  $W$ , and one for  $\theta$ . To each DS corresponds a  $\theta$  and a  $W$ .  
Strategy arg in each constructor.

**Required data:**

**Optional:**

**Always allocated in constructor:**

Warning: default constructor is always private or protected and apart from the others and previous rules or remarks do not always apply to it.

### 6.4.2 Lsodar

**Required data:**

**Optional:**

**Always allocated in constructor:**

## Chapter 7

# First Order Nonlinear Relation

author	O. Bonnefon
date	July, 1 2009
version	Kernel 3.0.0

## Chapter 8

# Computation of the number of Index Set and various levels

author	V. Acary
date	Septembre 16, 2011
version	Kernel 3.3.0

In this chapter, we give some hints on the automatic computation of the number of index sets, the number of derivatives in the `Interaction` and the `levelMin` and `LevelMax`.

### 8.1 Why is the relative degree not relevant ?

In this section, we give a very brief overview of the notion of relative degree.

#### 8.1.1 First order Linear complementary systems

A Linear Complementarity System (LCS) is defined by

$$\begin{cases} \dot{x} = Ax + B\lambda \\ y = Cx + D\lambda \\ 0 \leq y \perp \lambda \geq 0 \end{cases} \quad (8.1) \quad \{\text{eq:LCS-bis}\}$$

**Definition 1 (Relative degree in the SISO case)** *Let us consider a linear system in state representation given by the quadruplet  $(A, B, C, D) \in \mathbb{R}^{n \times n} \times \mathbb{R}^{n \times m} \times \mathbb{R}^{m \times n} \times \mathbb{R}^{m \times m}$ :*

$$\begin{cases} \dot{x} = Ax + B\lambda \\ y = Cx + D\lambda \end{cases} \quad (8.2) \quad \{\text{eq:LS}\}$$

- In the Single Input/ Single Output (SISO) case ( $m = 1$ ), the relative degree is defined by the first non zero Markov parameters :

$$D, CB, CAB, CA^2B, \dots, CA^{r-1}B, \dots \quad (8.3) \quad \{\text{eq:Markov-Param}\}$$

- In the multiple input/multiple output (MIMO) case ( $m > 1$ ), an uniform relative degree is defined as follows. If  $D$  is non singular, the relative degree is equal to 0. Otherwise, it is assumed to be the first positive integer  $r$  such that

$$CA^i B = 0, \quad i = 0 \dots r-2 \quad (8.4) \quad \{\text{eq:mimo-r}\}$$

while

$$CA^{r-1}B \text{ is non singular.} \quad (8.5) \quad \{\text{eq:mimo-r2}\}$$

The Markov parameters arise naturally when we derive with respect to time the output  $y$ ,

$$\begin{aligned} y &= Cx + D\lambda \\ \dot{y} &= CAx + CB\lambda, \text{ if } D = 0 \\ \ddot{y} &= CA^2x + CAB\lambda, \text{ if } D = 0, CB = 0 \\ &\dots \\ y^{(r)} &= CA^rx + CA^{r-1}B\lambda, \text{ if } D = 0, CB = 0, CA^{r-2}B = 0, r = 1 \dots r-2 \\ &\dots \end{aligned}$$

and the first non zero Markov parameter allows us to define the output  $y$  directly in terms of the input  $\lambda$ .

In continuous time, the nature of solutions depends strongly on the relative degree. When we want to perform the time-integration of such systems, we need also to reduce the relative degree or to know it to correctly operate.

We can observe that the relative degree 0 is well defined only by the relation ( $D$  nonsingular) and by the nonsmooth law. Indeed, let us imagine that the nonsmooth law is defined by  $0 \leq \dot{y} \perp \lambda \geq 0$ . We can easily see that the relative degree is reduced.

In the MIMO, the computation of non uniform relative degree is hard task. This is also the case for nonlinear systems.

### 8.1.2 Second order Lagrangian systems

Let us consider a second order linear and time-invariant Lagrangian dynamical system (see § 2.5)

$$\begin{cases} M\dot{v} + Cv + Kq = F_{Ext}(t) + p \\ \dot{q} = v \end{cases} \quad (8.6) \quad \{\text{eq:rd1}\}$$

together with a Lagrangian linear relation

$$y = Cq + e + D\lambda + Fz, \quad (8.7) \quad \{\text{eq:rd2}\}$$

$$p = C^t\lambda \quad (8.8) \quad \{\text{eq:rd3}\}$$

and a simple nonsmooth law,

$$0 \leq y \perp \lambda \geq 0 \quad (8.9) \quad \{\text{eq:rd4}\}$$

If  $D > 0$ , the relative degree is uniformly zero and the system can be solved without deriving the output (8.7). Indeed, we known that the solution of the LCP

$$0 \leq Cq + e + D\lambda + Fz, \perp \lambda \geq 0 \quad (8.10) \quad \{\text{eq:rd5}\}$$

is unique and Lipschitz with respect to  $q$ . It can be denoted as  $\lambda(q) = \text{SOL}(D, Cq + e + Fz)$ . Therefore, the differential equation (8.6) reduces to a standard ODE with a Lipschitz RHS

$$\begin{cases} M\dot{v} + Cv + Kq = F_{Ext}(t) + C^t\lambda(q) \\ \dot{q} = v \end{cases} \quad (8.11) \quad \{\text{eq:rd6}\}$$

In the case that we deal with unilateral contact, we usually have  $D = 0$  and the relative degree of the system is 2. In this case, the output has to be differentiated as

$$\dot{y} = C\dot{q}, \quad (8.12) \quad \{\text{eq:rd7}\}$$

and an impact law has to added, for instance the newton's impact law

$$\text{if } y = 0, \text{ when } \dot{y}^+ = -e\dot{y}^- \quad (8.13) \quad \{\text{eq:rd8}\}$$



In the same vein, the equations of motion (8.6) is not sufficient since the velocity may encounter jumps. The dynamics is usually replaced by a measure differential equation of the form

$$\begin{cases} Mdv + Cv^+(t)dt + Kq(t)dt = F_{Ext}(t)dt + di \\ \dot{q} = v \end{cases} \quad (8.14) \quad \{\text{eq:rd10}\}$$

where  $di$  is the measure that can be related to  $p$  thanks to

$$di = p dt + \sigma \delta_{t^*} \quad (8.15) \quad \{\text{eq:rd11}\}$$

is only one jump is expected at  $t^*$ .

### 8.1.3 Conclusion for the implementation

From the continuous time mathematical analysis, the relative degree is very important to know if we have to compute the derivatives of the output  $y^{(n)}$  and to consider various levels for the input  $p, \sigma, \dots$

However in the numerical practice, the time –discretization makes an assumption on the relative degree and treats the nonsmooth law at different levels. The resulting time discretized system possesses more or less variables.

Consider for instance (8.6) in the case of the Moreau scheme

$$\begin{cases} M(v_{k+1} - v_k) + h(Kq_{k+\theta} + Cv_{k+\theta}) = p_{k+1} = G(q_{k+1})\lambda_{k+1}, & (8.16a) \quad \{\text{eq:MoreauTS}\} \\ q_{k+1} = q_k + hv_{k+\theta}, & (8.16b) \\ \dot{y}_{k+1} = G^\top(q_{k+1})v_{k+1} & (8.16c) \\ \text{if } \bar{y}_{k+1}^\alpha \leq 0 \text{ then } 0 \leq \dot{y}_{k+1}^\alpha + e\dot{y}_k^\alpha \perp \lambda_{k+1}^\alpha \geq 0, & (8.16d) \quad \{\text{eq:MoreauTSd}\} \\ \text{otherwise } \lambda_{k+1}^\alpha = 0. & \end{cases}, \alpha \in \mathcal{I}$$

and the Schatzman–Paoli scheme

$$\begin{cases} M(q_{k+1} - 2q_k + q_{k-1}) + h^2(Kq_{k+\theta} + Cv_{k+\theta}) = p_{k+1}, & (8.17a) \\ v_{k+1} = \frac{q_{k+1} - q_{k-1}}{2h}, & (8.17b) \\ y_{k+1} = h \left( \frac{q_{k+1} + eq_{k-1}}{1+e} \right) & (8.17c) \\ p_{k+1} = G \left( \frac{q_{k+1} + eq_{k-1}}{1+e} \right) \lambda_{k+1} & (8.17d) \\ 0 \leq y_{k+1} \perp \lambda_{k+1} \geq 0. & (8.17e) \end{cases}$$

We can see easily that the number of derivatives (or levels) that we store for  $y$  and  $\lambda$  is independent on the relative degree but is chosen by the `OneStepIntegrator` with respect to the type of systems.

## 8.2 How to define and compute the various levels and the number of indexSets

### 8.2.1 $y$ related variables

The size of the vector  $y$  in the Interaction depends on

- the `OneStepIntegrator` type.
  - see the difference between the Moreau and Schatzman Paoli scheme,

- plan the time-discontinuous Galerkin scheme
- plan the Higher Order Moreau sweeping process (HOSP)
- the `Simulation` type.
  - In Timestepping or Event-driven we do not need the same number of stored  $y$
- the `NonSmoothLaw` type.
  - If we consider some cases with or without friction in Timestepping or Event-driven, we need to adapt the number of stored  $y$

Since the various levels of  $y$  are used to build the index sets we will need from 0 to a computed size that depends on the previous criteria. Only a part will be used in the `OneStepNSProblem`.

### 8.2.2 $\lambda$ related variables

The size of the vector `lambda` in the `Interaction` depends on the same criteria than in the previous section. Only, the number of `lambda` is not the same as  $y$  since a multiplier `lambda[i]` is not necessarily related to  $y[i]$

## 8.3 Rules for implementation

We can define new members in `Interaction`:

- `_lowerlevelForOutput`, this value is to 0 by default
- `_upperlevelForOutput`, this value must be computed at initialization with respect to the previous criteria
- `_lowerlevelForInput`, this value must be computed at initialization with respect to the previous criteria
- `_upperlevelForInput`, this value must be computed at initialization with respect to the previous criteria

This level are computed in `Simulation::ComputeLevelsForInputAndOutput`. A visitor is used for the `OneStepIntegrator`. Furthermore, four global levels are computed

- `_levelMinForOutput` this value is the minimum level for the output `Interaction::_lowerlevelForOutput` for all the interactions
- `_levelMaxForOutput` this value is the maximum level for the output `Interaction::_upperlevelForOutput` for all the interactions
- `_levelMinForInput` this value is the minimum level for the output `Interaction::_lowerlevelForInput` for all the interactions
- `_levelMaxForInput` this value is the maximum level for the output `Interaction::_upperlevelForInput` for all the interactions
- the values  $y[i]$  must be initialized from `_lowerlevelForOutput` to `_upperlevelForOutput`.
- the values `lambda[i]` must be initialized from `_lowerlevelForInput` to `_upperlevelForInput`.
- the values  $y[i]$  in `Interaction` must be used in priority to store the  $i$ -th derivative of  $y$ . When it is needed, higher index  $i$  can be used for other triggering variables. For instance, for an Event-Driven scheme with a Lagrangian systems with friction, sliding velocity must be stored.

- the values of `lambda[i]` must stored the various multiplier for the nonsmooth law. We affect the same index  $i$  as for the level of `y[i]` present in the corresponding nonsmooth law.
- The number of `IndexSets` should follows `_levelMaxForY`.

For the dynamical systems :

- The number of levels for `_r` and `_p` in the DS should follow `_lowerlevelForInput` and `_upperlevelForOutput` of the associated interactions. This is done in `Interaction::initialize`.
- A new variable should be added in the `LagrangianDS` to store the multiplier at the position level (`_tau` ?) to avoid the use of `_p[0]`. Indeed, we will continue to assume that `_p` is the input in the equation of motion. For `lambda` we can use `lambda[0]`

#### TODO LIST AND QUESTIONS

- What about the case of multiples interactions on a DS with various `_lowerlevelForInput` and `_upperlevelForOutput` ? Normally, all the levels should be correctly initialized thanks to the proposed implementation (r2821)
- `DynamicalSystem::_r` should be a `VectorOfVectors`
- `DynamicalSystem::_r` is split in `LagrangianDS`. a first part is `LagrangianDS::_p`. The other is not implemented !! `LagrangianDS::_tau` ?

## Chapter 9

# Newton's linearization for First Order Systems

author	O.Bonnefon, V. Acary
date	Sept, 07, 2007
last update	Feb, 2011 April, 2014
version	

This section is devoted to the implementation and the study of the algorithm. The interval of integration is  $[0, T]$ ,  $T > 0$ , and a grid  $t_0 = 0, t_{k+1} = t_k + h, k \geq 0, t_N = T$  is constructed. The approximation of a function  $f(\cdot)$  on  $[0, T]$  is denoted as  $f^N(\cdot)$ , and is a piecewise constant function, constant on the intervals  $[t_k, t_{k+1})$ . We denote  $f^N(t_k)$  as  $f_k$ . The time-step is  $h > 0$ .

### 9.1 Various first order dynamical systems with input/output relations

**FirstOrderR. Fully nonlinear case** Let us introduce the following system,

$$\begin{aligned} M\dot{x}(t) &= f(x(t), t) + r(t) \\ y(t) &= h(t, x(t), \lambda(t)) \\ r(t) &= g(t, x(t), \lambda(t)) \end{aligned} \tag{9.1} \quad \{\text{first-DS}\}$$

where  $\lambda(t) \in \mathbf{R}^m$  and  $y(t) \in \mathbf{R}^m$  are complementary variables related through a multi-valued mapping. According to the class of systems, we are studying, the function  $f$  and  $g$  are defined by a fully nonlinear framework or by affine functions. We have decided to present the time-discretization in its full generality and specialize the algorithms for each cases in Section ?? . This fully nonlinear case is not implemented in Siconos yet. This fully general case is not yet implemented in Siconos.

This case is implemented in Siconos with the relation `FirstOrderR` using the subtype `NonLinearR`

**FirstOrderType1R** Let us introduce a new notation,

$$\begin{aligned} M\dot{x}(t) &= f(x(t), t) + r(t) \\ y(t) &= h(t, x(t)) \\ r(t) &= g(t, \lambda(t)) \end{aligned} \tag{9.2} \quad \{\text{first-DS1}\}$$

This case is implemented in Siconos with the relation `FirstOrderType1R`.

**FirstOrderType2R** Let us introduce a new notation,

$$\begin{aligned} M\dot{x}(t) &= f(x(t), t) + r(t) \\ y(t) &= h(t, x(t), \lambda(t)) \\ r(t) &= g(t, \lambda(t)) \end{aligned} \tag{9.3} \quad \{\text{first-DS2}\}$$

This case is implemented in Siconos with the relation `FirstOrderType2R`.

**Linear case** Let us introduce a new notation,

$$\begin{aligned} M\dot{x}(t) &= Ax(t) + r(t) + b(t) \\ y(t) &= h(x(t), \lambda(t), z) = Cx + Fz + D\lambda \\ r(t) &= g(t, \lambda(t)) = B\lambda \end{aligned} \tag{9.4} \quad \{\text{first-DS3}\}$$

## 9.2 Time-discretizations

### 9.2.1 Standard $\theta - \gamma$ scheme.

Let us now proceed with the time discretization of (9.4) by a fully implicit scheme :

$$\begin{aligned} Mx_{k+1} &= Mx_k + h\theta f(x_{k+1}, t_{k+1}) + h(1 - \theta)f(x_k, t_k) + h\gamma r(t_{k+1}) + h(1 - \gamma)r(t_k) \\ y_{k+1} &= h(t_{k+1}, x_{k+1}, \lambda_{k+1}) \\ r_{k+1} &= g(t_{k+1}, x_{k+1}, \lambda_{k+1}) \\ \text{NsLaw}(y_{k+1}, \lambda_{k+1}) \end{aligned} \tag{9.5} \quad \{\text{eq:toto1}\}$$

where  $\theta = [0, 1]$  and  $\gamma \in [0, 1]$ . As in (?), we call the problem (9.5) the “one-step nonsmooth problem”.

In the Siconos/Kernel module, the use of  $\gamma$  is activated in the class `EulerMoreauOSI` by the boolean `_useGamma`.

This time-discretization is slightly more general than a standard implicit Euler scheme. The main discrepancy lies in the choice of a  $\theta$ -method to integrate the nonlinear term. For  $\theta = 0$ , we retrieve the explicit integration of the smooth and single valued term  $f$ . Moreover for  $\gamma = 0$ , the term  $g$  is explicitly evaluated. The flexibility in the choice of  $\theta$  and  $\gamma$  allows the user to improve and control the accuracy, the stability and the numerical damping of the proposed method. For instance, if the smooth dynamics given by  $f$  is stiff, or if we have to use big step sizes for practical reasons, the choice of  $\theta > 1/2$  offers better stability with the respect to  $h$ .

### 9.2.2 Full $\theta - \gamma$ scheme

Another possible time-discretization is as follows.

$$\begin{aligned} Mx_{k+1} &= Mx_k + h\theta f(x_{k+1}, t_{k+1}) + h(1 - \theta)f(x_k, t_k) + hr(t_{k+\gamma}) \\ y_{k+\gamma} &= h(t_{k+\gamma}, x_{k+\gamma}, \lambda_{k+\gamma}) \\ r_{k+\gamma} &= g(t_{k+\gamma}, x_{k+\gamma}, \lambda_{k+\gamma}) \\ \text{NsLaw}(y_{k+\gamma}, \lambda_{k+\gamma}) \end{aligned} \tag{9.6} \quad \{\text{eq:toto1-ter}\}$$

We call the scheme (9.6) the full  $\theta - \gamma$  scheme since it uses also the evaluation at  $t_{k+\gamma}$  for the relation.

In the Siconos/Kernel module, the time-stepping scheme is activated in the class `EulerMoreauOSI` by the boolean `_useGammaForRelation`.

Another possibility for the time discretization in the nonlinear case would be

$$\begin{aligned}
 Mx_{k+1} &= Mx_k + hf(x_{k+\theta}, t_{k+\theta}) + hr(t_{k+\gamma}) \\
 y_{k+\gamma} &= h(t_{k+\gamma}, x_{k+\gamma}, \lambda_{k+\gamma}) \\
 r_{k+\gamma} &= g(t_{k+\gamma}, x_{k+\gamma}, \lambda_{k+\gamma}) \\
 \text{NsLaw}(y_{k+\gamma}, \lambda_{k+\gamma})
 \end{aligned}
 \tag{9.7} \quad \text{\texttt{\{eq:toto1-quat\}}}$$

This scheme has not been yet implemented in Siconos/Kernel.

### 9.3 Newton's linearization of (9.5)

Due to the fact that two of the studied classes of systems that are studied in this paper are affine functions in terms of  $f$  and  $g$ , we propose to solve the "one-step nonsmooth problem" (9.5) by performing an external Newton linearization.

**Newton's linearization of the first line of (9.5)** The first line of the problem (9.5) can be written under the form of a residue  $\mathcal{R}$  depending only on  $x_{k+1}$  and  $r_{k+1}$  such that

$$\mathcal{R}(x_{k+1}, r_{k+1}) = 0 \quad (9.8) \quad \{\text{eq:NL3}\}$$

with

$$\mathcal{R}(x, r) = M(x - x_k) - h\theta f(x, t_{k+1}) - h(1 - \theta)f(x_k, t_k) - h\gamma r - h(1 - \gamma)r_k. \quad (9.9)$$

The solution of this system of nonlinear equations is sought as a limit of the sequence  $\{x_{k+1}^\alpha, r_{k+1}^\alpha\}_{\alpha \in \mathbf{N}}$  such that

$$\begin{cases} x_{k+1}^0 = x_k \\ r_{k+1}^0 = r_k \\ \mathcal{R}_L(x_{k+1}^{\alpha+1}, r_{k+1}^{\alpha+1}) = \mathcal{R}(x_{k+1}^\alpha, r_{k+1}^\alpha) + [\nabla_x \mathcal{R}(x_{k+1}^\alpha, r_{k+1}^\alpha)] (x_{k+1}^{\alpha+1} - x_{k+1}^\alpha) + [\nabla_r \mathcal{R}(x_{k+1}^\alpha, r_{k+1}^\alpha)] (r_{k+1}^{\alpha+1} - r_{k+1}^\alpha) = 0 \end{cases} \quad (9.10) \quad \{\text{eq:NL7}\}$$

#### 9.3.1 Redaction note V. ACARY

What about  $r_{k+1}^0$  ?

The residu free  $\mathcal{R}_{\text{free}}$  is also defined (useful for implementation only):

$$\mathcal{R}_{\text{free}}(x) \triangleq M(x - x_k) - h\theta f(x, t_{k+1}) - h(1 - \theta)f(x_k, t_k),$$

which yields

$$\mathcal{R}(x, r) = \mathcal{R}_{\text{free}}(x) - h\gamma r - h(1 - \gamma)r_k.$$

$$\mathcal{R}(x_{k+1}^\alpha, r_{k+1}^\alpha) = \boxed{\mathcal{R}_{k+1}^\alpha \triangleq \mathcal{R}_{\text{free}}(x_{k+1}^\alpha) - h\gamma r_{k+1}^\alpha - h(1 - \gamma)r_k} \quad (9.11) \quad \{\text{eq:rfree-1}\}$$

$$\mathcal{R}_{\text{free}}(x_{k+1}^\alpha, r_{k+1}^\alpha) = \boxed{\mathcal{R}_{\text{free}, k+1}^\alpha \triangleq M(x_{k+1}^\alpha - x_k) - h\theta f(x_{k+1}^\alpha, t_{k+1}) - h(1 - \theta)f(x_k, t_k)}$$

At each time-step, we have to solve the following linearized problem,

$$\mathcal{R}_{k+1}^\alpha + (M - h\theta A_{k+1}^\alpha)(x_{k+1}^{\alpha+1} - x_{k+1}^\alpha) - h\gamma(r_{k+1}^{\alpha+1} - r_{k+1}^\alpha) = 0, \quad (9.12) \quad \{\text{eq:NL10}\}$$

with

$$A_{k+1}^\alpha = \nabla_x f(t_{k+1}, x_{k+1}^\alpha) \quad (9.13)$$

By using (9.11), we get

$$\mathcal{R}_{\text{free}}(x_{k+1}^\alpha, r_{k+1}^\alpha) - h\gamma r_{k+1}^{\alpha+1} - h(1 - \gamma)r_k + (M - h\theta A_{k+1}^\alpha)(x_{k+1}^{\alpha+1} - x_{k+1}^\alpha) = 0 \quad (9.14) \quad \{\text{eq:rfree-2}\}$$

The matrix  $W$  is clearly non singular for small  $h$ .

**Newton's linearization of the second line of (9.5)** The same operation is performed with the second equation of (9.5)

$$\mathcal{R}_y(x, y, \lambda) = y - h(t_{k+1}, x, \lambda) = 0 \quad (9.15)$$

which is linearized as

$$\begin{aligned} \mathcal{R}_{Ly}(x_{k+1}^{\alpha+1}, y_{k+1}^{\alpha+1}, \lambda_{k+1}^{\alpha+1}) &= \mathcal{R}_y(x_{k+1}^{\alpha}, y_{k+1}^{\alpha}, \lambda_{k+1}^{\alpha}) + (y_{k+1}^{\alpha+1} - y_{k+1}^{\alpha}) - \\ &C_{k+1}^{\alpha}(x_{k+1}^{\alpha+1} - x_{k+1}^{\alpha}) - D_{k+1}^{\alpha}(\lambda_{k+1}^{\alpha+1} - \lambda_{k+1}^{\alpha}) = 0 \end{aligned} \quad (9.16) \quad \{\text{eq:NL9}\}$$

This leads to the following linear equation

$$y_{k+1}^{\alpha+1} = y_{k+1}^{\alpha} - \mathcal{R}_{y_{k+1}}^{\alpha} + C_{k+1}^{\alpha}(x_{k+1}^{\alpha+1} - x_{k+1}^{\alpha}) + D_{k+1}^{\alpha}(\lambda_{k+1}^{\alpha+1} - \lambda_{k+1}^{\alpha}) \quad (9.17) \quad \{\text{eq:NL11y}\}$$

with,

$$C_{k+1}^{\alpha} = \nabla_x h(t_{k+1}, x_{k+1}^{\alpha}, \lambda_{k+1}^{\alpha}) \quad (9.18)$$

$$D_{k+1}^{\alpha} = \nabla_{\lambda} h(t_{k+1}, x_{k+1}^{\alpha}, \lambda_{k+1}^{\alpha})$$

and

$$\mathcal{R}_{y_{k+1}}^{\alpha} \triangleq y_{k+1}^{\alpha} - h(t_{k+1}, x_{k+1}^{\alpha}, \lambda_{k+1}^{\alpha}) \quad (9.19)$$

**Newton's linearization of the third line of (9.5)** The same operation is performed with the third equation of (9.5)

$$\mathcal{R}_r(r, x, \lambda) = r - g(t_{k+1}, x, \lambda) = 0 \quad (9.20)$$

which is linearized as

$$\mathcal{R}_{Lr}(r_{k+1}^{\alpha+1}, x_{k+1}^{\alpha+1}, \lambda_{k+1}^{\alpha+1}) = \mathcal{R}_{rk+1}^{\alpha} + (r_{k+1}^{\alpha+1} - r_{k+1}^{\alpha}) - K_{k+1}^{\alpha}(x_{k+1}^{\alpha+1} - x_{k+1}^{\alpha}) - B_{k+1}^{\alpha}(\lambda_{k+1}^{\alpha+1} - \lambda_{k+1}^{\alpha}) = 0 \quad (9.21) \quad \{\text{eq:NL9}\}$$

$$r_{k+1}^{\alpha+1} = g(t_{k+1}, x_{k+1}^{\alpha}, \lambda_{k+1}^{\alpha}) + K_{k+1}^{\alpha}(x_{k+1}^{\alpha+1} - x_{k+1}^{\alpha}) + B_{k+1}^{\alpha}(\lambda_{k+1}^{\alpha+1} - \lambda_{k+1}^{\alpha}) \quad (9.22) \quad \{\text{eq:rrL}\}$$

with,

$$K_{k+1}^{\alpha} = \nabla_x g(t_{k+1}, x_{k+1}^{\alpha}, \lambda_{k+1}^{\alpha}) \quad (9.23)$$

$$B_{k+1}^{\alpha} = \nabla_{\lambda} g(t_{k+1}, x_{k+1}^{\alpha}, \lambda_{k+1}^{\alpha})$$

and the residue for  $r$ :

$$\mathcal{R}_{rk+1}^{\alpha} = r_{k+1}^{\alpha} - g(t_{k+1}, x_{k+1}^{\alpha}, \lambda_{k+1}^{\alpha}) \quad (9.24)$$

**Reduction to a linear relation between  $x_{k+1}^{\alpha+1}$  and  $\lambda_{k+1}^{\alpha+1}$**  Inserting (9.22) into (9.14), we get the following linear relation between  $x_{k+1}^{\alpha+1}$  and  $\lambda_{k+1}^{\alpha+1}$ ,

$$\begin{aligned} \mathcal{R}_{\text{free},k+1}^{\alpha} - h\gamma \left[ g(t_{k+1}, x_{k+1}^{\alpha}, \lambda_{k+1}^{\alpha}) + B_{k+1}^{\alpha}(\lambda_{k+1}^{\alpha+1} - \lambda_{k+1}^{\alpha}) + K_{k+1}^{\alpha}(x_{k+1}^{\alpha+1} - x_{k+1}^{\alpha}) \right] \\ - h(1 - \gamma)r_k + (M - h\theta A_{k+1}^{\alpha})(x_{k+1}^{\alpha+1} - x_{k+1}^{\alpha}) = 0 \end{aligned} \quad (9.25) \quad \{\text{eq:rfree-3}\}$$



that is

$$(M - h\theta A_{k+1}^\alpha - h\gamma K_{k+1}^\alpha)(x_{k+1}^{\alpha+1} - x_{k+1}^\alpha) = -\mathcal{R}_{\text{free},k+1}^\alpha - h(1-\gamma)r_k + h\gamma \left[ g(t_{k+1}, x_{k+1}^\alpha, \lambda_{k+1}^\alpha) + B_{k+1}^\alpha(\lambda_{k+1}^{\alpha+1} - \lambda_{k+1}^\alpha) \right] \quad (9.26) \quad \{\text{eq:rfree-4}\}$$

Let us introduce some intermediate notation:

$$W_{k+1}^\alpha \triangleq M - h\theta A_{k+1}^\alpha - h\gamma K_{k+1}^\alpha \quad (9.27) \quad \{\text{eq:NL9}\}$$

$$x_{\text{free}}^\alpha \triangleq x_{k+1}^\alpha - (W_{k+1}^\alpha)^{-1}(\mathcal{R}_{\text{free},k+1}^\alpha - h(1-\gamma)r_k) \quad (9.28) \quad \{\text{eq:rfree-12}\}$$

and

$$x_p^\alpha \triangleq h\gamma(W_{k+1}^\alpha)^{-1} [g(t_{k+1}, x_{k+1}^\alpha, \lambda_{k+1}^\alpha) - B_{k+1}^\alpha(\lambda_{k+1}^\alpha)] + x_{\text{free}}^\alpha. \quad (9.29)$$

The relation (9.26) can be written as

$$x_{k+1}^{\alpha+1} \triangleq x_p^\alpha + [h\gamma(W_{k+1}^\alpha)^{-1}B_{k+1}^\alpha\lambda_{k+1}^{\alpha+1}] \quad (9.30) \quad \{\text{eq:rfree-13}\}$$

**Reduction to a linear relation between  $y_{k+1}^{\alpha+1}$  and  $\lambda_{k+1}^{\alpha+1}$ .** Inserting (9.30) into (9.17), we get the following linear relation between  $y_{k+1}^{\alpha+1}$  and  $\lambda_{k+1}^{\alpha+1}$ ,

$$y_{k+1}^{\alpha+1} = y_p + [h\gamma C_{k+1}^\alpha (W_{k+1}^\alpha)^{-1} B_{k+1}^\alpha + D_{k+1}^\alpha] \lambda_{k+1}^{\alpha+1} \quad (9.31)$$

with

$$y_p = y_{k+1}^\alpha - \mathcal{R}_{y,k+1}^\alpha + C_{k+1}^\alpha(x_q) - D_{k+1}^\alpha\lambda_{k+1}^\alpha \quad (9.32)$$

$$x_q = x_p^\alpha - x_{k+1}^\alpha \quad (9.33) \quad \{\text{eq:xqq}\}$$

**Mixed linear complementarity problem (MLCP)** To summarize, the problem to be solved in each Newton iteration is:

$$\begin{cases} y_{k+1}^{\alpha+1} = W_{\text{mlcp},k+1}^\alpha \lambda_{k+1}^{\alpha+1} + b_{k+1}^\alpha \\ -y_{k+1}^{\alpha+1} \in N_{[l,u]}(\lambda_{k+1}^{\alpha+1}). \end{cases} \quad (9.34) \quad \{\text{eq:NL14}\}$$

with  $W_{\text{mlcp},k+1} \in \mathbb{R}^{m \times m}$  and  $b \in \mathbb{R}^m$  defined by

$$\begin{aligned} W_{\text{mlcp},k+1}^\alpha &= h\gamma C_{k+1}^\alpha (W_{k+1}^\alpha)^{-1} B_{k+1}^\alpha + D_{k+1}^\alpha \\ b_{k+1}^\alpha &= y_p \end{aligned} \quad (9.35) \quad \{\text{eq:NL15}\}$$

The problem (9.34) is equivalent to a Mixed Linear Complementarity Problem (MLCP) which can be solved under suitable assumptions by many linear complementarity solvers such as pivoting techniques, interior point techniques and splitting/projection strategies. The reformulation into a standard

MLCP follows the same line as for the MCP in the previous section. One obtains,

$$\begin{aligned} y_{k+1}^{\alpha+1} &= -W_{k+1}^{\alpha} \lambda_{k+1}^{\alpha+1} + b_{k+1}^{\alpha} \\ (y_{k+1}^{\alpha+1})_i &= 0 \quad \text{for } i \in \{1..n\} \\ 0 &\leq (\lambda_{k+1}^{\alpha+1})_i \perp (y_{k+1}^{\alpha+1})_i \geq 0 \quad \text{for } i \in \{n..n+m\} \end{aligned} \tag{9.36} \quad \{\text{eq:MLCP1}\}$$

### 9.3.1 The special case of Newton's linearization of (9.5) with FirstOrderType2R (9.3)

Let us now proceed with the time discretization of (9.5) with FirstOrderType2R (9.3) by a fully implicit scheme :

$$\begin{aligned} Mx_{k+1} &= Mx_k + h\theta f(x_{k+1}, t_{k+1}) + h(1-\theta)f(x_k, t_k) + h\gamma r(t_{k+1}) + h(1-\gamma)r(t_k) \\ y_{k+1} &= h(t_{k+1}, x_{k+1}, \lambda_{k+1}) \\ r_{k+1} &= g(t_{k+1}, \lambda_{k+1}) \end{aligned} \tag{9.37} \quad \{\text{eq:mlcp2-toto1-}\}$$

**Newton's linearization of the first line of (9.37)** The linearization of the first line of the problem (9.37) is similar to the previous case so that (9.14) is still valid.

**Newton's linearization of the second line of (9.37)** The linearization of the second line of the problem (9.37) is similar to the previous case so that (9.17) is still valid.

**Newton's linearization of the third line of (9.37)** Since  $K_{k+1}^{\alpha} = \nabla_x g(t_{k+1}, \lambda_{k+1}^{\alpha}) = 0$ , the linearization of the third line of (9.37) reads as

$$r_{k+1}^{\alpha+1} = g(t_{k+1}, \lambda_{k+1}^{\alpha}) + B_{k+1}^{\alpha} (\lambda_{k+1}^{\alpha+1} - \lambda_{k+1}^{\alpha}) \tag{9.38} \quad \{\text{eq:mlcp2-rrL}\}$$

**Reduction to a linear relation between  $x_{k+1}^{\alpha+1}$  and  $\lambda_{k+1}^{\alpha+1}$**  Inserting (9.38) into (??), we get the following linear relation between  $x_{k+1}^{\alpha+1}$  and  $\lambda_{k+1}^{\alpha+1}$ , we get the linear relation

$$x_{k+1}^{\alpha+1} \triangleq x_p^{\alpha} + [h\gamma(W_{k+1}^{\alpha})^{-1} B_{k+1}^{\alpha} \lambda_{k+1}^{\alpha+1}] \tag{9.39} \quad \{\text{eq:mlcp2-rfree-}\}$$

with

$$x_p^{\alpha} \triangleq h\gamma(W_{k+1}^{\alpha})^{-1} [g(t_{k+1}, \lambda_{k+1}^{\alpha}) - B_{k+1}^{\alpha} (\lambda_{k+1}^{\alpha})] + x_{\text{free}}^{\alpha} \tag{9.40}$$

and

$$W_{k+1}^{\alpha} \triangleq M - h\theta A_{k+1}^{\alpha} \tag{9.41} \quad \{\text{eq:mlcp2-NL9}\}$$

**Reduction to a linear relation between  $y_{k+1}^{\alpha+1}$  and  $\lambda_{k+1}^{\alpha+1}$**  Inserting (9.39) into (9.17), we get the following linear relation between  $y_{k+1}^{\alpha+1}$  and  $\lambda_{k+1}^{\alpha+1}$ ,

$$y_{k+1}^{\alpha+1} = y_p + [h\gamma C_{k+1}^{\alpha} (W_{k+1}^{\alpha})^{-1} B_{k+1}^{\alpha} + D_{k+1}^{\alpha}] \lambda_{k+1}^{\alpha+1} \tag{9.42}$$

with

$$y_p = y_{k+1}^\alpha - \mathcal{R}_{y_{k+1}}^\alpha + C_{k+1}^\alpha(x_q) - D_{k+1}^\alpha \lambda_{k+1}^\alpha \quad (9.43)$$

$$x_q^\alpha = x_p^\alpha - x_{k+1}^\alpha \quad (9.44) \quad \{\text{eq:mlcp2-xqq}\}$$

### 9.3.2 The special case of Newton's linearization of (9.5) with FirstOrderType1R (9.2)

Let us now proceed with the time discretization of (9.5) with FirstOrderType1R (9.2) by a fully implicit scheme :

$$\begin{aligned} Mx_{k+1} &= Mx_k + h\theta f(x_{k+1}, t_{k+1}) + h(1 - \theta)f(x_k, t_k) + h\gamma r(t_{k+1}) + h(1 - \gamma)r(t_k) \\ y_{k+1} &= h(t_{k+1}, x_{k+1}) \\ r_{k+1} &= g(t_{k+1}, \lambda_{k+1}) \end{aligned} \quad (9.45) \quad \{\text{eq:mlcp3-toto1-1}\}$$

The previous derivation is valid with  $D_{k+1}^\alpha = 0$ .

### 9.3.3 Time-discretization of the linear case (9.4)

Let us now proceed with the time discretization of (9.5) with FirstOrderLinearR (9.4) by a fully implicit scheme :

$$\begin{aligned} Mx_{k+1}^{\alpha+1} &= Mx_k + h\theta Ax_{k+1}^{\alpha+1} + h(1 - \theta)Ax_k + h\gamma r_{k+1}^{\alpha+1} + h(1 - \gamma)r(t_k) + hb \\ y_{k+1}^{\alpha+1} &= Cx_{k+1}^{\alpha+1} + D\lambda_{k+1}^{\alpha+1} + Fz + e \\ r_{k+1}^{\alpha+1} &= B\lambda_{k+1}^{\alpha+1} \end{aligned} \quad (9.46) \quad \{\text{eq:toto1-DS3}\}$$

$$\begin{aligned} R_{\text{free}} &= M(x_{k+1}^\alpha - x_k) - h\theta Ax_{k+1}^\alpha - h(1 - \theta)Ax_k - hb_{k+1} \\ R_{\text{free}} &= W(x_{k+1}^\alpha - x_k) - hAx_k - hb_{k+1} \end{aligned}$$

**Resulting Newton step (only one step)** For the sake of simplicity, let us assume that  $\gamma = 1$

$$\begin{aligned} (M - h\theta A)x_{k+1}^{\alpha+1} &= Mx_k + h(1 - \theta)Ax_k + hr_{k+1}^{\alpha+1} + hb \\ y_{k+1}^{\alpha+1} &= Cx_{k+1}^{\alpha+1} + D\lambda_{k+1}^{\alpha+1} + Fz + e \\ r_{k+1}^{\alpha+1} &= B\lambda_{k+1}^{\alpha+1} \end{aligned} \quad (9.47)$$

that lead to with:  $(M - h\theta A) = W$

$$\begin{aligned} x_{k+1}^{\alpha+1} &= W^{-1}(Mx_k + h(1 - \theta)Ax_k + r_{k+1}^{\alpha+1} + hb) = x_{\text{free}} + W^{-1}(r_{k+1}^{\alpha+1}) \\ y_{k+1}^{\alpha+1} &= (D + hCW^{-1}B)\lambda_{k+1}^{\alpha+1} + Fz + CW^{-1}(Mx_k + h(1 - \theta)Ax_k + hb) + e \end{aligned} \quad (9.48)$$

with  $x_{\text{free}} = x_{k+1}^\alpha + W^{-1}(-R_{\text{free}}) = x_{k+1}^\alpha - W^{-1}(W(x_{k+1}^\alpha - x_k) - hAx_k - hb_{k+1}) = W^{-1}(Mx_k + h(1 - \theta)Ax_k + hb_{k+1})$

$$\begin{aligned} y_{k+1}^{\alpha+1} &= (D + hCW^{-1}B)\lambda_{k+1}^{\alpha+1} + Fz + Cx_{\text{free}} + e \\ r_{k+1}^{\alpha+1} &= B\lambda_{k+1}^{\alpha+1} \end{aligned} \quad (9.49)$$

**Coherence with previous formulation**

$$y_p = y_{k+1}^\alpha - \mathcal{R}_{y_{k+1}}^\alpha + C_{k+1}^\alpha (x_p - x_{k+1}^\alpha) - D_{k+1}^\alpha \lambda_{k+1}^\alpha$$

$$y_p = Cx_k + D\lambda_k + C(\tilde{x}_{\text{free}}) - D\lambda_k + Fz + e$$

$$y_p = Cx_k + C(\tilde{x}_{\text{free}}) + Fz + e$$

$$y_p = Cx_k + C(\tilde{x}_{\text{free}}) + Fz + e$$

$$y_p = C(x_{\text{free}}) + Fz + e$$

## 9.4 Newton's linearization of (9.6)

In this section, we deal with only with the FirstOrderType2R case.

$$\begin{aligned} Mx_{k+1} &= Mx_k + h\theta f(x_{k+1}, t_{k+1}) + h(1 - \theta)f(x_k, t_k) + hr_{k+\gamma} \\ y_{k+\gamma} &= h(t_{k+\gamma}, x_{k+\gamma}, \lambda_{k+\gamma}) \\ r_{k+\gamma} &= g(t_{k+\gamma}, \lambda_{k+\gamma}) \end{aligned} \quad (9.50) \quad \{\text{eq:full-toto1-t}\}$$

**Newton's linearization of the first line of (9.50)** The first line of the problem (9.50) can be written under the form of a residue  $\mathcal{R}$  depending only on  $x_{k+1}$  and  $r_{k+\gamma}$  such that

$$\mathcal{R}(x_{k+1}, r_{k+\gamma}) = 0 \quad (9.51) \quad \{\text{eq:full-NL3}\}$$

with

$$\mathcal{R}(x, r) = M(x - x_k) - h\theta f(x, t_{k+1}) - h(1 - \theta)f(x_k, t_k) - hr.$$

The solution of this system of nonlinear equations is sought as a limit of the sequence  $\{x_{k+1}^\alpha, r_{k+\gamma}^\alpha\}_{\alpha \in \mathbb{N}}$  such that

$$\begin{cases} x_{k+1}^0 = x_k \\ r_{k+\gamma}^0 = (1 - \gamma)r_k + \gamma r_{k+1}^0 = r_k \\ \mathcal{R}_L(x_{k+1}^{\alpha+1}, r_{k+\gamma}^{\alpha+1}) = \mathcal{R}(x_{k+1}^\alpha, r_{k+\gamma}^\alpha) + \left[ \nabla_x \mathcal{R}(x_{k+1}^\alpha, r_{k+\gamma}^\alpha) \right] (x_{k+1}^{\alpha+1} - x_{k+1}^\alpha) + \\ \quad \left[ \nabla_r \mathcal{R}(x_{k+1}^\alpha, r_{k+\gamma}^\alpha) \right] (r_{k+\gamma}^{\alpha+1} - r_{k+\gamma}^\alpha) = 0 \end{cases} \quad (9.52) \quad \{\text{eq:full-NL7}\}$$

### 9.4.1 Redaction note V. ACARY

What about  $r_{k+\gamma}^0$  ?

The residu free is also defined (useful for implementation only):

$$\mathcal{R}_{\text{free}}(x) \triangleq M(x - x_k) - h\theta f(x, t_{k+1}) - h(1 - \theta)f(x_k, t_k).$$

We get

$$\mathcal{R}(x_{k+1}^\alpha, r_{k+\gamma}^\alpha) = \boxed{\mathcal{R}_{k+1}^\alpha \triangleq \mathcal{R}_{\text{free}}(x_{k+1}^\alpha) - hr_{k+\gamma}^\alpha} \quad (9.53) \quad \{\text{eq:full-rfree-1}\}$$

$$\mathcal{R}_{\text{free}}(x_{k+1}^\alpha) = \boxed{\mathcal{R}_{\text{free},k+1}^\alpha \triangleq M(x_{k+1}^\alpha - x_k) - h\theta f(x_{k+1}^\alpha, t_{k+1}) - h(1 - \theta)f(x_k, t_k)}$$

The computation of the Jacobian of  $\mathcal{R}$  with respect to  $x$ , denoted by  $W_{k+1}^\alpha$  leads to

$$W_{k+1}^\alpha \triangleq \nabla_x \mathcal{R}(x_{k+1}^\alpha) = M - h\theta \nabla_x f(x_{k+1}^\alpha, t_{k+1}). \quad (9.54) \quad \{\text{eq:full-NL9}\}$$

At each time-step, we have to solve the following linearized problem,

$$\mathcal{R}_{k+1}^\alpha + W_{k+1}^\alpha (x_{k+1}^{\alpha+1} - x_{k+1}^\alpha) - h(r_{k+\gamma}^{\alpha+1} - r_{k+\gamma}^\alpha) = 0, \quad (9.55) \quad \{\text{eq:full-NL10}\}$$

By using (9.53), we get

$$\mathcal{R}_{\text{free}}(x_{k+1}^\alpha) - hr_{k+\gamma}^{\alpha+1} + W_{k+1}^\alpha (x_{k+1}^{\alpha+1} - x_{k+1}^\alpha) = 0 \quad (9.56) \quad \{\text{eq:full-rfree-2}\}$$

$$x_{k+1}^{\alpha+1} = h(W_{k+1}^{\alpha})^{-1} r_{\gamma+1}^{\alpha+1} + x_{\text{free}}^{\alpha} \quad (9.57)$$

with :

$$x_{\text{free}}^{\alpha} \triangleq x_{k+1}^{\alpha} - (W_{k+1}^{\alpha})^{-1} \mathcal{R}_{\text{free},k+1}^{\alpha} \quad (9.58) \quad \{\text{eq:full-rfree-1}\}$$

The matrix  $W$  is clearly non singular for small  $h$ .

Note that the linearization is equivalent to the case (9.14) and (9.28) with  $\gamma = 1$  and replacing  $r_{k+1}$  by  $r_{k+\gamma}$ .

**Newton's linearization of the second line of (9.50)** The same operation is performed with the second equation of (9.50)

$$\mathcal{R}_y(x, y, \lambda) = y - h(t_{k+\gamma}, \gamma x + (1 - \gamma)x_k, \lambda) = 0 \quad (9.59)$$

which is linearized as

$$\begin{aligned} \mathcal{R}_{Ly}(x_{k+1}^{\alpha+1}, y_{k+\gamma}^{\alpha+1}, \lambda_{k+\gamma}^{\alpha+1}) &= \mathcal{R}_y(x_{k+1}^{\alpha}, y_{k+\gamma}^{\alpha}, \lambda_{k+\gamma}^{\alpha}) + (y_{k+\gamma}^{\alpha+1} - y_{k+\gamma}^{\alpha}) - \\ &\quad \gamma C_{k+1}^{\alpha} (x_{k+1}^{\alpha+1} - x_{k+1}^{\alpha}) - D_{k+\gamma}^{\alpha} (\lambda_{k+\gamma}^{\alpha+1} - \lambda_{k+\gamma}^{\alpha}) = 0 \end{aligned} \quad (9.60) \quad \{\text{eq:full-NL9}\}$$

This leads to the following linear equation

$$y_{k+\gamma}^{\alpha+1} = y_{k+\gamma}^{\alpha} - \mathcal{R}_{y,k+1}^{\alpha} + \gamma C_{k+1}^{\alpha} (x_{k+1}^{\alpha+1} - x_{k+1}^{\alpha}) + D_{k+\gamma}^{\alpha} (\lambda_{k+\gamma}^{\alpha+1} - \lambda_{k+\gamma}^{\alpha}) \quad (9.61) \quad \{\text{eq:full-NL11y}\}$$

with,

$$C_{k+\gamma}^{\alpha} = \nabla_x h(t_{k+1}, x_{k+\gamma}^{\alpha}, \lambda_{k+\gamma}^{\alpha}) \quad (9.62)$$

$$D_{k+\gamma}^{\alpha} = \nabla_{\lambda} h(t_{k+1}, x_{k+\gamma}^{\alpha}, \lambda_{k+\gamma}^{\alpha})$$

and

$$\mathcal{R}_{y,k+1}^{\alpha} \triangleq y_{k+\gamma}^{\alpha} - h(x_{k+\gamma}^{\alpha}, \lambda_{k+\gamma}^{\alpha}) \quad (9.63)$$

Note that the linearization is equivalent to the case (9.17) by replacing  $\lambda_{k+1}$  by  $\lambda_{k+\gamma}$  and  $x_{k+1}$  by  $x_{k+\gamma}$ .

**Newton's linearization of the third line of (9.50)** The same operation is performed with the third equation of (9.50)

$$\mathcal{R}_r(r, \lambda) = r - g(\lambda, t_{k+1}) = 0 \quad (9.64)$$

which is linearized as

$$\mathcal{R}_{L\lambda}(r_{k+\gamma}^{\alpha+1}, \lambda_{k+\gamma}^{\alpha+1}) = \mathcal{R}_{r,k+\gamma}^{\alpha} + (r_{k+\gamma}^{\alpha+1} - r_{k+\gamma}^{\alpha}) - B_{k+\gamma}^{\alpha} (\lambda_{k+\gamma}^{\alpha+1} - \lambda_{k+\gamma}^{\alpha}) = 0 \quad (9.65) \quad \{\text{eq:full-NL9}\}$$

$$r_{k+\gamma}^{\alpha+1} = g(\lambda_{k+\gamma}^{\alpha}, t_{k+\gamma}) - B_{k+\gamma}^{\alpha} \lambda_{k+\gamma}^{\alpha} + B_{k+\gamma}^{\alpha} \lambda_{k+\gamma}^{\alpha+1} \quad (9.66) \quad \{\text{eq:full-rrL}\}$$

with,

$$B_{k+\gamma}^\alpha = \nabla_\lambda g(\lambda_{k+\gamma}^\alpha, t_{k+\gamma}) \quad (9.67)$$

and the residue for  $r$ :

$$\mathcal{R}_{rk+\gamma}^\alpha = r_{k+\gamma}^\alpha - g(\lambda_{k+\gamma}^\alpha, t_{k+\gamma}) \quad (9.68)$$

Note that the linearization is equivalent to the case (9.22) by replacing  $\lambda_{k+1}$  by  $\lambda_{k+\gamma}$  and  $x_{k+1}$  by  $x_{k+\gamma}$ .

**Reduction to a linear relation between  $x_{k+1}^{\alpha+1}$  and  $\lambda_{k+\gamma}^{\alpha+1}$**  Inserting (9.66) into (9.58), we get the following linear relation between  $x_{k+1}^{\alpha+1}$  and  $\lambda_{k+1}^{\alpha+1}$ ,

$$x_{k+1}^{\alpha+1} = h(W_{k+1}^\alpha)^{-1} \left[ g(\lambda_{k+\gamma}^\alpha, t_{k+\gamma}) + B_{k+\gamma}^\alpha (\lambda_{k+\gamma}^{\alpha+1} - \lambda_{k+\gamma}^\alpha) \right] + x_{free}^\alpha \quad (9.69)$$

that is

$$x_{k+1}^{\alpha+1} = x_p + h(W_{k+1}^\alpha)^{-1} B_{k+\gamma}^\alpha \lambda_{k+\gamma}^{\alpha+1} \quad (9.70) \quad \{\text{eq:full-rfree-1}\}$$

with

$$x_p \triangleq h(W_{k+1}^\alpha)^{-1} \left[ g(\lambda_{k+\gamma}^\alpha, t_{k+\gamma}) - B_{k+\gamma}^\alpha (\lambda_{k+\gamma}^\alpha) \right] + x_{free}^\alpha \quad (9.71)$$

**Reduction to a linear relation between  $y_{k+1}^{\alpha+1}$  and  $\lambda_{k+\gamma}^{\alpha+1}$**  Inserting (9.70) into (9.61), we get the following linear relation between  $y_{k+1}^{\alpha+1}$  and  $\lambda_{k+1}^{\alpha+1}$ ,

$$y_{k+1}^{\alpha+1} = y_p + \left[ h\gamma C_{k+\gamma}^\alpha (W_{k+1}^\alpha)^{-1} B_{k+1}^\alpha + D_{k+1}^\alpha \right] \lambda_{k+1}^{\alpha+1} \quad (9.72)$$

with

$$y_p = y_{k+1}^\alpha - \mathcal{R}_{yk+1}^\alpha + \gamma C_{k+1}^\alpha (x_q) - D_{k+1}^\alpha \lambda_{k+1}^\alpha \quad (9.73)$$

that is

$$y_p = h(x_{k+\gamma}^\alpha, \lambda_{k+\gamma}^\alpha) + \gamma C_{k+1}^\alpha (x_q) - D_{k+1}^\alpha \lambda_{k+1}^\alpha \quad (9.74)$$

$$x_q = (x_p - x_{k+1}^\alpha) \quad (9.75) \quad \{\text{eq:full-xqq}\}$$

**The linear case**

$$\begin{aligned} y_p &= h(x_{k+\gamma}^\alpha, \lambda_{k+\gamma}^\alpha) + \gamma C_{k+1}^\alpha (x_q) - D_{k+1}^\alpha \lambda_{k+1}^\alpha \\ &= C_{k+1}^\alpha x_{k+\gamma}^\alpha + D_{k+1}^\alpha \lambda_{k+\gamma}^\alpha + \gamma C_{k+1}^\alpha (x_q) - D_{k+1}^\alpha \lambda_{k+1}^\alpha \\ &= C_{k+1}^\alpha (x_{k+\gamma}^\alpha + \gamma x_p - \gamma x_{k+1}^\alpha) \\ &= C_{k+1}^\alpha ((1-\gamma)x_k + \gamma x_{free}) \text{ since } x_p = x_{free} \end{aligned} \quad (9.76)$$

**Implementation details** For the moment (Feb. 2011), we set  $x_q = (1 - \gamma)x_k + \gamma x_{free}$  in the linear case. The nonlinear case is not yet implemented since we need to change the management of `H_alpha` in `Relation` to be able to compute the mid-point values. things that remain to do

- implement the function `BlockVector compute_g(t,lambda)` and `SimpleVector compute_h(t,x,lambda)` which takes into account the values of the argument and return a vector
- remove temporary computation in `Relation` of `Xq`, `g_alpha` and `H_alpha`. This should be stored somewhere else. (in the node of the graph)



## Chapter 10

# Newton's linearization for Lagrangian systems

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date	Sept, 20, 2011
version	

This section is devoted to the implementation and the study of the algorithm. The interval of integration is  $[0, T]$ ,  $T > 0$ , and a grid  $t_0 = 0, t_{k+1} = t_k + h, k \geq 0, t_N = T$  is constructed. The approximation of a function  $f(\cdot)$  on  $[0, T]$  is denoted as  $f^N(\cdot)$ , and is a piecewise constant function, constant on the intervals  $[t_k, t_{k+1})$ . We denote  $f^N(t_k)$  as  $f_k$ . The time-step is  $h > 0$ .

### 10.1 Various second order dynamical systems with input/output relations

#### 10.1.1 Lagrangian dynamical systems

The class `LagrangianDS` defines and computes a generic  $ndof$ -dimensional Lagrangian Non Linear Dynamical System of the form :

$$\begin{cases} M(q, z)\dot{v} + N(v, q, z) + F_{Int}(v, q, t, z) = F_{Ext}(t, z) + p \\ \dot{q} = v \end{cases} \quad (10.1)$$

where

- $q \in R^{ndof}$  is the set of the generalized coordinates,
- $\dot{q} = v \in R^{ndof}$  the velocity, i. e. the time derivative of the generalized coordinates (Lagrangian systems).
- $\ddot{q} = \dot{v} \in R^{ndof}$  the acceleration, i. e. the second time derivative of the generalized coordinates.
- $p \in R^{ndof}$  the reaction forces due to the Non Smooth Interaction.
- $M(q) \in R^{ndof \times ndof}$  is the inertia term saved in the `SiconosMatrix` mass.
- $N(\dot{q}, q) \in R^{ndof}$  is the non linear inertia term saved in the `SiconosVector` `_NNL`.
- $F_{Int}(\dot{q}, q, t) \in R^{ndof}$  are the internal forces saved in the `SiconosVector` `fInt`.
- $F_{Ext}(t) \in R^{ndof}$  are the external forces saved in the `SiconosVector` `fExt`.

- $z \in \mathbb{R}^{zSize}$  is a vector of arbitrary algebraic variables, some sort of discrete state.

The equation of motion is also shortly denoted as:

$$M(q, z)\dot{v} = F(v, q, t, z) + p \quad (10.2)$$

where  $F(v, q, t, z) \in \mathbb{R}^{ndof}$  collects the total forces acting on the system, that is

$$F(v, q, t, z) = F_{Ext}(t, z) - NNL(v, q, z) + F_{Int}(v, q, t, z) \quad (10.3)$$

This vector is stored in the SiconosVector `_Forces`

### 10.1.2 Fully nonlinear case

Let us introduce the following system,

$$\begin{cases} M(q, z)\dot{v} = F(v, q, t, z) + p \\ \dot{q} = v \\ y = h(t, q, \lambda) \\ p = g(t, q, \lambda) \end{cases} \quad (10.4) \quad \{\text{eq:FullyNonLinear}\}$$

where  $\lambda(t) \in \mathbb{R}^m$  and  $y(t) \in \mathbb{R}^m$  are complementary variables related through a multi-valued mapping. According to the class of systems, we are studying, the function  $F$ ,  $h$  and  $g$  are defined by a fully nonlinear framework or by affine functions. This fully nonlinear case is not implemented in Siconos yet. This fully general case is not yet implemented in Siconos.

### 10.1.3 Lagrangian Rheonomous relations

$$\begin{cases} M(q, z)\dot{v} = F(v, q, t, z) + p \\ \dot{q} = v \\ y = h(t, q) \\ p = G(t, q)\lambda \end{cases} \quad (10.5) \quad \{\text{eq:RheonomousNonLinear}\}$$

### 10.1.4 Lagrangian Scleronomous relations

$$\begin{cases} M(q, z)\dot{v} = F(v, q, t, z) + p \\ \dot{q} = v \\ y = h(q) \\ p = G(q)\lambda \end{cases} \quad (10.6) \quad \{\text{eq:ScleronomousNonLinear}\}$$

#### Fully Linear case

$$\begin{cases} M\dot{v} + Cv + Kq = F_{Ext}(t, z) + p \\ \dot{q} = v \\ y = Cq + e + D\lambda + Fz \\ p = C^T\lambda \end{cases} \quad (10.7) \quad \{\text{eq:FullyLinear}\}$$

## 10.2 Moreau's Time-discretizations

### 10.3 Schatzman-Paoli 'scheme and its linearizations

#### 10.3.1 The scheme

$$\left\{ \begin{array}{l} M(q_k)(q_{k+1} - 2q_k + q_{k-1}) - h^2 F(v_{k+\theta}, q_{k+\theta}, t_{k+\theta}) = p_{k+1}, \end{array} \right. \quad (10.8a)$$

$$v_{k+1} = \frac{q_{k+1} - q_{k-1}}{2h}, \quad (10.8b)$$

$$y_{k+1} = h \left( \frac{q_{k+1} + eq_{k-1}}{1+e} \right) \quad (10.8c)$$

$$p_{k+1} = G \left( \frac{q_{k+1} + eq_{k-1}}{1+e} \right) \lambda_{k+1} \quad (10.8d)$$

$$0 \leq y_{k+1} \perp \lambda_{k+1} \geq 0. \quad (10.8e)$$

10.3.1 Redaction note V. ACARY

Should we have

$$v_{k+1} = \frac{q_{k+1} - q_{k-1}}{2h}$$

or

$$v_{k+1} = \frac{q_{k+1} - q_k}{h}$$

? This question is particularly important for the initialization and the proposed  $\theta$ -scheme

#### 10.3.2 The Newton linearization

Let us define the residu on  $q$

$$\mathcal{R}(q) = M(q)(q - 2q_k + q_{k-1}) + h^2 F((\theta v(q) + (1 - \theta)v_k), \theta q + (1 - \theta)q_k, t_{k+\theta}) - p_{k+1} \quad (10.9) \quad \{\text{eq:residu}\}$$

with

$$v(q) = \frac{q - q_{k-1}}{2h} \quad (10.10) \quad \{\text{eq:residu-linq1}\}$$

that is

$$\mathcal{R}(q) = M(q)(q - 2q_k + q_{k-1}) + h^2 F((\theta \frac{q - q_{k-1}}{2h} + (1 - \theta)v_k), \theta q + (1 - \theta)q_k, t_{k+\theta}) - p_{k+1} \quad (10.11) \quad \{\text{eq:residu-linq2}\}$$

Neglecting  $\nabla_q M(q)$  we get

$$\nabla_q \mathcal{R}(q^\nu) = M(q^\nu) + h^2 \theta K(q^\nu, v^\nu) + \frac{1}{2} h \theta C(q^\nu, v^\nu) \quad (10.12) \quad \{\text{eq:iterationmat}\}$$

and we have to solve

$$\nabla_q \mathcal{R}(q^\nu)(q^{\nu+1} - q^\nu) = -\mathcal{R}(q^\nu). \quad (10.13) \quad \{\text{eq:iterationloop}\}$$

### 10.3.3 Linear version of the scheme

$$\begin{cases} M(q_{k+1} - 2q_k + q_{k-1}) + h^2(Kq_{k+\theta} + Cv_{k+\theta}) = p_{k+1}, \end{cases} \quad (10.14a)$$

$$\begin{cases} v_{k+1} = \frac{q_{k+1} - q_{k-1}}{2h}, \end{cases} \quad (10.14b)$$

$$\begin{cases} y_{k+1} = h \left( \frac{q_{k+1} + eq_{k-1}}{1+e} \right) \end{cases} \quad (10.14c)$$

$$\begin{cases} p_{k+1} = G \left( \frac{q_{k+1} + eq_{k-1}}{1+e} \right) \lambda_{k+1} \end{cases} \quad (10.14d)$$

$$\begin{cases} 0 \leq y_{k+1} \perp \lambda_{k+1} \geq 0. \end{cases} \quad (10.14e)$$

Let us define the residu on  $q$

$$\mathcal{R}(q) = M(q - 2q_k + q_{k-1}) + h^2(K(\theta q + (1 - \theta)q_k)) + C(\theta v(q) + (1 - \theta)v_k)) - p_{k+1} \quad (10.15) \quad \{\text{eq:residu-linq}\}$$

with

$$v(q) = \frac{q - q_{k-1}}{2h} \quad (10.16) \quad \{\text{eq:residu-linq1}\}$$

that is

$$\mathcal{R}(q) = M(q - 2q_k + q_{k-1}) + h^2(K(\theta q + (1 - \theta)q_k)) + h^2C(\theta \frac{q - q_{k-1}}{2h} + (1 - \theta)v_k)) - p_{k+1} \quad (10.17) \quad \{\text{eq:residu-linq2}\}$$

In this linear case, assuming that  $q^0 = q^\vee = q_k$ , we get

$$\mathcal{R}(q^\vee) = M(-q_k + q_{k-1}) + h^2(Kq_k) + h^2C(\theta \frac{q_k - q_{k-1}}{2h} + (1 - \theta)v_k)) - p_{k+1} \quad (10.18) \quad \{\text{eq:residu-linq2}\}$$

## 10.4 What about mixing OnestepIntegrator in Simulation?

Let us consider that we have two simple linear Lagrangian Dynamical systems

{Sec:MissingOSI}

$$\begin{cases} M_1 \dot{v}_1 = F_{1,Ext}(t) + p_1 \\ \dot{q}_1 = v_1 \end{cases} \quad (10.19) \quad \{\text{eq:FullyLinear1}\}$$

and

$$\begin{cases} M_2 \dot{v}_2 = F_{2,Ext}(t) + p_2 \\ \dot{q}_2 = v_2 \end{cases} \quad (10.20) \quad \{\text{eq:FullyLinear1}\}$$

These Dynamical systems (10.20) and (10.20) might numerically solved by choosing two different time-stepping schemes. Let us choose for instance Moreau's scheme for(10.20)

$$\begin{cases} M_1(v_{1,k+1} - v_{1,k}) = F_{1,Ext}(t_{k+1}) + p_{1,k+1} \\ q_{1,k+1} = q_k + hv_{1,k+\theta} \end{cases} \quad (10.21) \quad \{\text{eq:FullyLinear1}\}$$

and Schatzman–Paoli's sheme for (10.20)

$$\begin{cases} M_2(q_{2,k+1} - 2q_{2,k} + q_{2,k-1}) = F_{2,Ext}(t_{k+1}) + p_{2,k+1} \\ v_{2,k+1} = \frac{q_{2,k+1} - q_{2,k-1}}{2h} \end{cases} \quad (10.22) \quad \{\text{eq:FullyLinear1}\}$$

Let us consider known that we have a LagrangianLinearTIR between this two DSs such that

$$\begin{aligned} y &= q_1 - q_2 \geq 0 \\ p &= \begin{bmatrix} 1 \\ -1 \end{bmatrix} \lambda \end{aligned} \quad (10.23) \quad \{\text{eq:LTIR-2DS}\}$$

and a complementarity condition

$$0 \leq y \perp \lambda \geq 0 \quad (10.24) \quad \{\text{eq:CP}\}$$

Many questions are raised when we want to deal with the discrete systems:

- Which rules should we use for the discretization of (10.24) ?

$$\text{if } \bar{y}_{k+1} \leq 0, \text{ then } 0 \leq \dot{y}_{k+1} + e\dot{y}_k \perp \hat{\lambda}_{k+1} \geq 0 \quad (10.25) \quad \{\text{eq:CP-TS1}\}$$

or

$$0 \leq y_{k+1} + ey_{k-1} \perp \tilde{\lambda}_{k+1} \geq 0 \quad (10.26) \quad \{\text{eq:CP-TS2}\}$$

- Should we assume that  $y_{k+1} = q_{1,k+1} - q_{2,k+1}$  and  $\dot{y}_{k+1} = v_{1,k+1} - v_{2,k+1}$
- How can we link  $\hat{\lambda}_{k+1}$  and  $\tilde{\lambda}_{k+1}$  with  $p_{1,k+1}$  and  $p_{2,k+1}$  ?

The third is the more difficult question and it seems that it is not reasonable to deal with two DS related by one interaction with different osi. In practice, this should be avoided in Siconos.

# Chapter 11

## NewtonEuler Dynamical Systems

Author	O. Bonnefon	2010
Revision	section ?? to ?? V. Acary	05/09/2011
Revision	section ?? V. Acary	01/06/2016
Revision	complete edition V. Acary	06/01/2017

### 11.1 The equations of motion

In the maximal coordinates framework, the most natural choice for the kinematic variables and for the formulation of the equations of motion is the Newton/Euler formalism, where the equation of motion describes the translational and rotational dynamics of each body using a specific choice of parameters. For the translational motion, the position of the center of mass  $x_g \in \mathbb{R}^3$  and its velocity  $v_g = \dot{x}_g \in \mathbb{R}^3$  is usually chosen. For the rotational motion, a common choice is to choose the angular velocity  $\Omega \in \mathbb{R}^3$  of the body expressed in the body-fixed frame. The orientation of the body is usually defined by the rotation matrix  $R$  of the body-fixed frame with respect to a given inertial frame. The angular velocity can be then expressed as :

$$\tilde{\Omega} = R^\top \dot{R}, \text{ or equivalently, } \dot{R} = R\tilde{\Omega} \quad (11.1) \quad \{\text{eq:angularveloc}\}$$

where the matrix  $\tilde{\Omega} \in \mathbb{R}^{3 \times 3}$  is given by  $\tilde{\Omega}x = \Omega \times x$  for all  $x \in \mathbb{R}^3$ . Using these coordinates, the equations of motion are given by

$$\begin{cases} m \dot{v}_g &= f(t, x_g, v_g, R, \Omega) \\ I\dot{\Omega} + \Omega \times I\Omega &= M(t, x_g, v_g, R, \Omega) \\ \dot{x}_g &= v_g \\ \dot{R} &= R\tilde{\Omega} \end{cases} \quad (11.2) \quad \{\text{eq:motion-Newton}\}$$

where  $m > 0$  is the mass,  $I \in \mathbb{R}^{3 \times 3}$  is the matrix of moments of inertia around the center of mass and the axis of the body-fixed frame.

The vectors  $f(\cdot) \in \mathbb{R}^3$  and  $M(\cdot) \in \mathbb{R}^3$  are the total forces and torques applied to the body. It is important to outline that the total applied forces  $f(\cdot)$  has to be expressed in a consistent frame w.r.t. to  $v_g$ . In our case, it has to be expressed in the inertial frame. The same applies for the moment  $M$  that has to be expressed in the body-fixed frame. If we consider a moment  $m(\cdot)$  expressed in the inertial frame, then it has to be convected to the body-fixed frame thanks to

$$M(\cdot) = R^\top m(\cdot) \quad (11.3) \quad \{\text{eq:convected_mom}\}$$

#### 11.1.1 Redaction note V. ACARY

todo : add the formulation in the inertial frame of the Euler equation with  $\omega = R\Omega$

In the numerical practice, the choice of the rotation matrix is not convenient since it introduces redundant parameters. Since  $R$  must belong to  $SO^+(3)$ , we have also to satisfy  $\det(R) = 1$  and  $R^{-1} = R^\top$ . In Siconos we choose to parametrize the rotation with a unit quaternion  $p \in \mathbb{R}^4$  such that  $R = \Phi(q)$  and  $\dot{p} = \Psi(p)\Omega$ . This parameterization has no singularity and has only one redundant variable that is determined by imposing  $\|p\| = 1$ . Formulae for  $\Phi$  and  $\Psi$  can be found in any textbooks.

11.1.1.2 Redaction note V. ACARY  
 todo : add the formulae

We denote by  $q$  the vector of coordinates of the position and the orientation of the body, and by  $v$  the body twist:

$$q := \begin{bmatrix} x_g \\ p \end{bmatrix}, \quad v := \begin{bmatrix} v_g \\ \Omega \end{bmatrix}. \quad (11.4)$$

The relation between  $v$  and the time derivative of  $q$  is

$$\dot{q} = \begin{bmatrix} \dot{x}_g \\ \Psi(p)\dot{p} \end{bmatrix} = \begin{bmatrix} I & 0 \\ 0 & \Psi(p) \end{bmatrix} v := T(q)v \quad (11.5) \quad \{\text{eq:TT}\}$$

with  $T(q) \in \mathbb{R}^{7 \times 6}$ . Note that the twist  $v$  is not directly the time derivative of the coordinate vector as a major difference with Lagrangian systems.

11.1.1.3 Redaction note V. ACARY  
 todo :Add an explicit formulae for the  $T(q)$

The Newton-Euler equation in compact form may be written as:

$$\begin{cases} \dot{q} = T(q)v, \\ M\dot{v} = F(t, q, v) \end{cases} \quad (11.6) \quad \{\text{eq:Newton-Euler}\}$$

where  $M \in \mathbb{R}^{6 \times 6}$  is the total inertia matrix

$$M := \begin{pmatrix} mI_{3 \times 3} & 0 \\ 0 & I \end{pmatrix}, \quad (11.7)$$

and  $F(t, q, v) \in \mathbb{R}^6$  collects all the forces and torques applied to the body

$$F(t, q, v) := \begin{pmatrix} f(t, x_g, v_g, R, \Omega) \\ I\Omega \times \Omega + M(t, x_g, v_g, R, \Omega) \end{pmatrix}. \quad (11.8)$$

When a collection of bodies is considered, we will use the same notation as in (11.6) extending the definition of the variables  $q, v$  and the operators  $M, F$  in a straightforward way.

### 11.1.1 Mechanical systems with bilateral and unilateral constraints

{section22}

Let us consider that the system (11.6) is subjected to  $m$  constraints, with  $m_e$  holonomic bilateral constraints

$$h^\alpha(q) = 0, \alpha \in \mathcal{E} \subset \mathbb{N}, |\mathcal{E}| = m_e, \quad (11.9) \quad \{\text{eq:bilateral-con}\}$$

and  $m_i$  unilateral constraints

$$g_N^\alpha(q) \geq 0, \alpha \in \mathcal{I} \subset \mathbb{N}, |\mathcal{I}| = m_i. \quad (11.10) \quad \{\text{eq:unilateral-con}\}$$

Let us denote as  $J_h^\alpha(q) = \nabla_q^\top h^\alpha(q)$  the Jacobian matrix of the bilateral constraint  $h^\alpha(q)$  with respect to  $q$  and as  $J_{g_N}^\alpha(q)$  respectively for  $g_N^\alpha(q)$ . The bilateral constraints at the velocity level can be obtained as:

$$0 = \dot{h}^\alpha(q) = J_h^\alpha(q)\dot{q} = J_h^\alpha(q)T(q)v := H^\alpha(q)v, \quad \alpha \in \mathcal{E}. \quad (11.11) \quad \{\text{eq:bilateral-con}\}$$

By duality and introducing a Lagrange multiplier  $\lambda^\alpha, \alpha \in \mathcal{E}$ , the constraint generates a force applied to the body equal to  $H^{\alpha,\top}(q)\lambda^\alpha$ . For the unilateral constraints, a Lagrange multiplier  $\lambda_N^\alpha, \alpha \in \mathcal{I}$  is also associated and the constraints at the velocity level can also be derived as

$$0 \leq \dot{g}_N^\alpha(q) = J_{g_N}^\alpha(q)\dot{q} = J_{g_N}^\alpha(q)T(q)v, \text{ if } g_N^\alpha(q) = 0, \quad \alpha \in \mathcal{I}. \quad (11.12) \quad \{\text{eq:unilateral-c}\}$$

Again, the force applied to the body is given by  $(J_{g_N}^\alpha(q)T(q))^\top \lambda_N^\alpha$ . Nevertheless, there is no reason that  $\lambda_N^\alpha = r_N^\alpha$  and  $u_N = J_{g_N}^\alpha(q)T(q)v$  if the  $g_n$  is not chosen as the signed distance (the gap function). This is the reason why we prefer directly define the normal and the tangential local relative velocity with respect to the twist vector as

$$u_N^\alpha := G_N^\alpha(q)v, \quad u_T^\alpha := G_T^\alpha(q)v, \quad \alpha \in \mathcal{I}, \quad (11.13) \quad \{\text{eq:unilateral-c}\}$$

and the associated force as  $G_N^{\alpha,\top}(q)r_N^\alpha$  and  $G_T^{\alpha,\top}(q)r_T^\alpha$ . For the sake of simplicity, we use the notation  $u^\alpha := G^\alpha(q)v$  and its associated total force generated by the contact  $\alpha$  as  $G^{\alpha,\top}(q)r^\alpha := G_N^{\alpha,\top}(q)r_N^\alpha + G_T^{\alpha,\top}(q)r_T^\alpha$ .

The complete system of equation of motion can finally be written as

$$\left\{ \begin{array}{l} \dot{q} = T(q)v, \\ M\dot{v} = F(t, q, v) + H^\top(q)\lambda + G^\top(q)r, \\ H^\alpha(q)v = 0, \\ r^\alpha = 0, \quad \text{if } g_N^\alpha(q) > 0, \\ K^{\alpha,*} \ni \hat{u}^\alpha \perp r^\alpha \in K^\alpha, \quad \text{if } g_N^\alpha(q) = 0, \\ u_N^{\alpha,+} = -e_r^\alpha u_N^{\alpha,-}, \quad \text{if } g_N^\alpha(q) = 0 \text{ and } u_N^{\alpha,-} \leq 0, \end{array} \right\} \quad \begin{array}{l} \alpha \in \mathcal{E} \\ \alpha \in \mathcal{I} \end{array} \quad (11.14) \quad \{\text{eq:NewtonEuler-t}\}$$

where the definition of the variables  $\lambda \in \mathbf{R}^{m_e}, r \in \mathbf{R}^{3m_i}$  and the operators  $H, G$  are extended to collect all the variables for each constraints.

Note that all the constraints are written at the velocity integrators. Another strong advantage is the straightforward introduction of the contact dissipation processes that are naturally written at the velocity level such as the Newton impact law and the Coulomb friction. Indeed, in Mechanics, dissipation processes are always given in terms of rates of changes, or if we prefer, in terms of velocities.

**Siconos Notation** In the siconos notation, we have for the applied torques on the system the following decomposition

$$F(t, q, v) := \left( I\Omega \times \Omega + M(t, x_g, v_g, R, \Omega) \right) := \left( -m_{gyr}(\Omega) + m_{ext}(t) - m_{int}(x_g, v_g, R, \Omega) \right). \quad (11.15)$$

with

$$m_{gyr} := (\Omega \times I\Omega) \quad (11.16)$$

In the siconos notation, we have for the relation

$$C = J^\alpha(q) \quad CT = J^\alpha(q)T(q) \quad (11.17) \quad \{\text{eq:2}\}$$

**Computation of  $T$  for unit quaternion**

$$\dot{p} = \frac{1}{2}p \begin{bmatrix} 0 \\ \Omega \end{bmatrix} \quad (11.18) \quad \{\text{eq:3}\}$$

Using the matrix representation of quaternion that encode the quaternion multiplication,

$$\hat{p} = \begin{bmatrix} p_0 & -p_1 & -p_2 & -p_3 \\ p_1 & p_0 & -p_3 & p_2 \\ p_2 & p_3 & -p_0 & -p_1 \\ p_3 & -p_2 & p_1 & p_0 \end{bmatrix}, \quad (11.19) \quad \{\text{eq:4}\}$$



we get

$$T(q) = \begin{bmatrix} I_{3 \times 3} & 0_{3 \times 4} \\ 0_{3 \times 3} & \begin{matrix} p_1 & p_0 & -p_3 & p_2 \\ p_2 & p_3 & -p_0 & -p_1 \\ p_3 & -p_2 & p_1 & p_0 \end{matrix} \end{bmatrix} \quad (11.20) \quad \{\text{eq:5}\}$$

## 11.2 Time integration scheme in scheme

### 11.2.1 Moreau–Jean scheme based on a $\theta$ -method

The complete Moreau–Jean scheme based on a  $\theta$ -method is written as follows

$$\left\{ \begin{array}{l} q_{k+1} = q_k + hT(q_{k+\theta})v_{k+\theta} \\ M(v_{k+1} - v_k) - hF(t_{k+\theta}, q_{k+\theta}, v_{k+\theta}) = H^\top(q_{k+1})Q_{k+1} + G^\top(q_{k+1})P_{k+1}, \\ H^\alpha(q_{k+1})v_{k+1} = 0 \\ P_{k+1}^\alpha = 0, \\ K^{\alpha,*} \ni \hat{u}_{k+1}^\alpha \perp P_{k+1}^\alpha \in K^\alpha \end{array} \right\} \quad \begin{array}{l} \alpha \in \mathcal{E} \\ \alpha \notin \mathcal{I}^\nu \\ \alpha \in \mathcal{I}^\nu \end{array} \quad (11.21) \quad \{\text{eq:Moreau-Jean-}\}$$

where  $\mathcal{I}^\nu$  is the set of forecast constraints, that may be evaluated as

$$\mathcal{I}^\nu = \{\alpha \mid \bar{g}_N^\alpha := g_N + \frac{h}{2}u_N^\alpha \leq 0\}. \quad (11.22) \quad \{\text{eq:10}\}$$

### 11.2.2 Semi-explicit version Moreau–Jean scheme based on a $\theta$ -method

$$\left\{ \begin{array}{l} q_{k+1} = q_k + hT(q_k)v_{k+\theta} \\ M(v_{k+1} - v_k) - hF(t_k, q_k, v_k) = H^\top(q_k)Q_{k+1} + G^\top(q_k)P_{k+1}, \\ H^\alpha(q_{k+1})v_{k+1} = 0 \\ P_{k+1}^\alpha = 0, \\ K^{\alpha,*} \ni \hat{u}_{k+1}^\alpha \perp P_{k+1}^\alpha \in K^\alpha \end{array} \right\} \quad \begin{array}{l} \alpha \in \mathcal{E} \\ \alpha \notin \mathcal{I}^\nu \\ \alpha \in \mathcal{I}^\nu \end{array} \quad (11.23) \quad \{\text{eq:Moreau-Jean-}\}$$

In this version, the new velocity  $v_{k+1}$  can be computed explicitly, assuming that the inverse of  $M$  is easily written, as

$$v_{k+1} = v_k + M^{-1}hF(t_k, q_k, v_k) + M^{-1}(H^\top(q_k)Q_{k+1} + G^\top(q_k)P_{k+1}) \quad (11.24) \quad \{\text{eq:Moreau-Jean-}\}$$

### 11.2.3 Nearly implicit version Moreau–Jean scheme based on a $\theta$ -method implemented in siconos

A first simplification is made considering a given value of  $q_{k+1}$  in  $T()$ ,  $H()$  and  $G()$  denoted by  $\bar{q}_k$ . This limits the computation of the Jacobians of this operators with respect to  $q$ .

$$\left\{ \begin{array}{l} q_{k+1} = q_k + hT(\bar{q}_k)v_{k+\theta} \\ M(v_{k+1} - v_k) - h\theta F(t_{k+1}, q_{k+1}, v_{k+1}) - h(1-\theta)F(t_k, q_k, v_k) = H^\top(\bar{q}_k)Q_{k+1} + G^\top(\bar{q}_k)P_{k+1}, \\ H^\alpha(\bar{q}_k)v_{k+1} = 0 \\ P_{k+1}^\alpha = 0, \\ K^{\alpha,*} \ni \hat{u}_{k+1}^\alpha \perp P_{k+1}^\alpha \in K^\alpha \end{array} \right\} \quad \begin{array}{l} \alpha \in \mathcal{E} \\ \alpha \notin \mathcal{I}^\nu \\ \alpha \in \mathcal{I}^\nu \end{array} \quad (11.25) \quad \{\text{eq:Moreau-Jean-}\}$$

The nonlinear residu is defined as

$$\mathcal{R}(v) = M(v - v_k) - h\theta F(t_{k+1}, q(v), v) - h(1 - \theta)F(t_k, q_k, v_k) - H^\top(\bar{q}_k)Q_{k+1} - G^\top(\bar{q}_k)P_{k+1} \quad (11.26) \quad \{\text{eq:Moreau-Jean-1}\}$$

with

$$q(v) = q_k + hT(\bar{q}_k)((1 - \theta)v_k + \theta v). \quad (11.27) \quad \{\text{eq:Moreau-Jean-1}\}$$

At each time step, we have to solve

$$\mathcal{R}(v_{k+1}) = 0 \quad (11.28) \quad \{\text{eq:Moreau-Jean-1}\}$$

together with the constraints.

Let us write a linearization of the problem to design a Newton procedure:

$$\nabla_v^\top \mathcal{R}(v_{k+1}^\tau)(v_{k+1}^{\tau+1} - v_{k+1}^\tau) = -\mathcal{R}(v_{k+1}^\tau). \quad (11.29) \quad \{\text{eq:Moreau-Jean-1}\}$$

The computation of  $\nabla_v^\top \mathcal{R}(v_{k+1}^\tau)$  is as follows

$$\nabla_v^\top \mathcal{R}(v) = M - h\theta \nabla_v F(t_{k+1}, q(v), v) \quad (11.30) \quad \{\text{eq:1}\}$$

with

$$\begin{aligned} \nabla_v F(t_{k+1}, q(v), v) &= D_2 F(t_{k+1}, q(v), v) \nabla_v q(v) + D_3 F(t_{k+1}, q(v), v) \\ &= h\theta D_2 F(t_{k+1}, q(v), v) T(\bar{q}_k) + D_3 F(t_{k+1}, q(v), v) \end{aligned} \quad (11.31) \quad \{\text{eq:6}\}$$

where  $D_i$  denotes the derivation with respect the  $i^{th}$  variable. The complete Jacobian is then given by

$$\nabla_v^\top \mathcal{R}(v) = M - h\theta D_3 F(t_{k+1}, q(v), v) - h^2 \theta^2 D_2 F(t_{k+1}, q(v), v) T(\bar{q}_k) \quad (11.32) \quad \{\text{eq:7}\}$$

In siconos, we ask the user to provide the functions  $D_3 F(t_{k+1}, q, v)$  and  $D_2 F(t_{k+1}, q, v)$ .

Let us denote by  $W^\tau$  the inverse of Jacobian of the residu,

$$W^\tau = (M - h\theta D_3 F(t_{k+1}, q(v), v) - h^2 \theta^2 D_2 F(t_{k+1}, q(v), v) T(\bar{q}_k))^{-1}. \quad (11.33) \quad \{\text{eq:11}\}$$

and by  $\mathcal{R}_{free}(v)$  the free residu,

$$\mathcal{R}_{free}(v) = M(v - v_k) - h\theta F(t_{k+1}, q(v), v) - h(1 - \theta)F(t_k, q_k, v_k). \quad (11.34) \quad \{\text{eq:12}\}$$

The linear equation 11.29 that we have to solve is equivalent to

$$v_{k+1}^{\tau+1} = v_{k+1}^\tau - W \mathcal{R}_{free}(v_{k+1}^\tau) + W H^\top(\bar{q}_k) Q_{k+1}^{\tau+1} + W G^\top(\bar{q}_k) P_{k+1}^{\tau+1} \quad (11.35) \quad \{\text{eq:13}\}$$

We define  $v_{free}$  as

$$v_{free} = v_{k+1}^\tau - W \mathcal{R}_{free}(v_{k+1}^\tau) \quad (11.36) \quad \{\text{eq:15}\}$$

The local velocity at contact can be written

$$u_{n,k+1}^{\tau+1} = G(\bar{q}_k)[v_{free}^\tau + W H^\top(\bar{q}_k) Q_{k+1}^{\tau+1} + W G^\top(\bar{q}_k) P_{k+1}^{\tau+1}] \quad (11.37) \quad \{\text{eq:14}\}$$

and for the equality constraints

$$u_{k+1}^{\tau+1} = H(\bar{q}_k)[v_{free}^\tau + W H^\top(\bar{q}_k) Q_{k+1}^{\tau+1} + W G^\top(\bar{q}_k) P_{k+1}^{\tau+1}] \quad (11.38) \quad \{\text{eq:14}\}$$

Finally, we get a linear relation between  $u_{n,k+1}^{\tau+1}$  and the multiplier

$$u_{k+1}^{\tau+1} = \begin{bmatrix} H(\bar{q}_k) \\ G(\bar{q}_k) \end{bmatrix} v_{free}^\tau + \begin{bmatrix} H(\bar{q}_k) W H^\top(\bar{q}_k) & H(\bar{q}_k) W G^\top(\bar{q}_k) \\ G(\bar{q}_k) W H^\top(\bar{q}_k) & G(\bar{q}_k) W G^\top(\bar{q}_k) \end{bmatrix} \begin{bmatrix} Q_{k+1}^{\tau+1} \\ P_{k+1}^{\tau+1} \end{bmatrix} \quad (11.39) \quad \{\text{eq:16}\}$$

**choices for  $\bar{q}_k$**  Two choices are possible for  $\bar{q}_k$

1.  $\bar{q}_k = q_k$
2.  $\bar{q}_k = q_{k+1}^\tau$

11.2.1 Redaction note V. ACARY  
todo list:

- add the projection step for the unit quaternion
- describe the computation of H and G that can be hybrid

## 11.2.4 Computation of the Jacobian in special case

**Moment of gyroscopic forces** Let us denote by the basis vector  $e_i$  given the  $i^{th}$  column of the identity matrix  $I_{3 \times 3}$ . The Jacobian of  $m_{gyr}$  is given by

$$\nabla_{\Omega}^\top m_{gyr}(\Omega) = \nabla_{\Omega}^\top (\Omega \times I \Omega) = [e_i \times I \Omega + \Omega \times I e_i, i = 1, 2, 3] \quad (11.40) \quad \{\text{eq:8}\}$$

**Linear internal wrench** If the internal wrench is given by

$$F_{int}(t, q, v) = \begin{bmatrix} f_{int}(t, q, v) \\ m_{int}(t, q, v) \end{bmatrix} = C v + K q, \quad C \in \mathbf{R}^{6 \times 6}, \quad K \in \mathbf{R}^{6 \times 7} \quad (11.41) \quad \{\text{eq:9}\}$$

we get

$$\begin{aligned} \nabla_v F(t_{k+1}, q(v), v) &= h \theta K T(\bar{q}_k) + C \\ \nabla_v^\top \mathcal{R}(v) &= M - h \theta C - h^2 \theta^2 K T(\bar{q}_k) \end{aligned} \quad (11.42) \quad \{\text{eq:6}\}$$

## 11.2.5 Siconos implementation

The expression:  $\mathcal{R}_{free}(v_{k+1}^\tau) = M(v - v_k) - h \theta F(t_{k+1}, q(v_{k+1}^\tau), v_{k+1}^\tau) - h(1 - \theta)F(t_k, q_k, v_k)$  is computed in `MoreauJeanOSI::computeResidu()` and saved in `ds->workspace(DynamicalSystem::freeresidu)`

The expression:  $\mathcal{R}(v_{k+1}^\tau) = \mathcal{R}_{free}(v_{k+1}^\tau) - h(1 - \theta)F(t_k, q_k, v_k) - H^\top(\bar{q}_k)Q_{k+1} - G^\top(\bar{q}_k)P_{k+1}$  is computed in `MoreauJeanOSI::computeResidu()` and saved in `ds->workspace(DynamicalSystem::free)`.

11.2.2 Redaction note V. ACARY

really a bad name for the buffer `ds->workspace(DynamicalSystem::free)`. Why we are chosing this name ? to save some memory ?

The expression:  $v_{free} = v_{k+1}^\tau - W \mathcal{R}_{free}(v_{k+1}^\tau)$  is compute in `MoreauJeanOSI::computeFreeState()` and saved in `d->workspace(DynamicalSystem::free)`.

The computation:  $v_{k+1}^{\tau+1} = v_{free} + W H^\top(\bar{q}_k)Q_{k+1}^{\tau+1} + W G^\top(\bar{q}_k)P_{k+1}^{\tau+1}$  is done in `MoreauJeanOSI::updateState` and stored in `d->twist()`.

## Chapter 12

# NewtonEulerR: computation of $\nabla_q H$

### 12.0.1 Gradient computation, case of NewtonEuler with quaternion

In the section,  $q$  is the quaternion of the dynamical system.

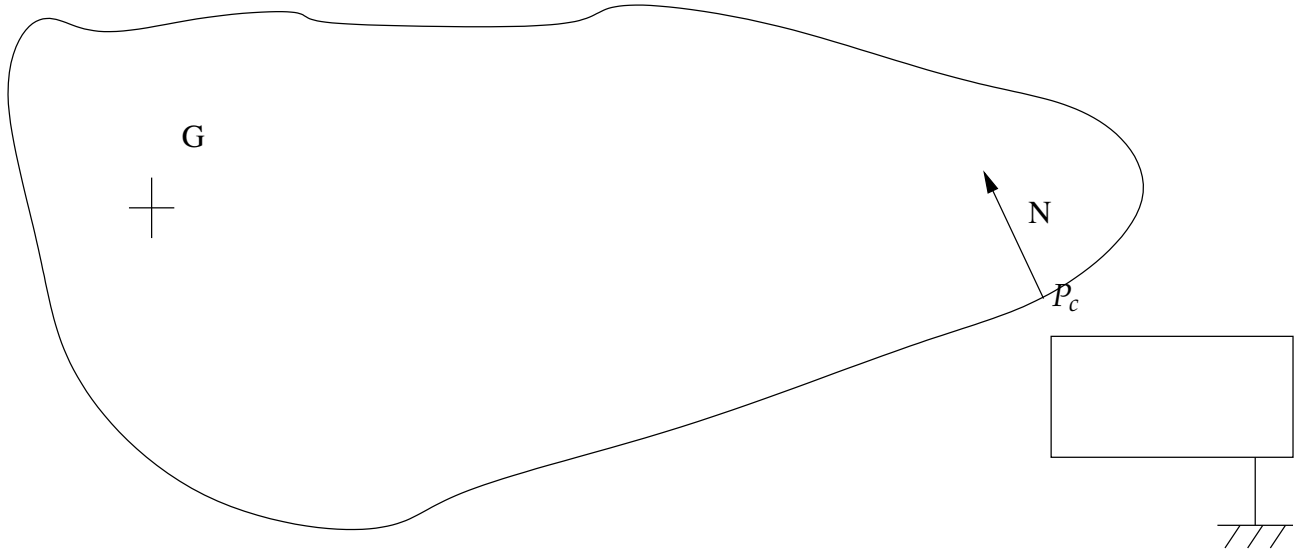


Figure 12.1: Impact of one DS.

{figCase}

The normal vector  $N$  is view as a constant.

$$\tilde{h}(q) = P_c\left(\frac{q}{\|q\|}\right)$$

$${}^t\nabla h(q)(\delta q) = \lim_{e \rightarrow 0} \frac{(\tilde{h}(q + e\delta q) - \tilde{h}(q)) \cdot N}{e}$$

$\nabla_q h$  consist in computing  $P_c\left(\frac{q+\delta q}{\|q+\delta q\|}\right) - P_c(q)$ .

$$GP(q) = qG_0P_0{}^c q$$

$$\begin{aligned} GP\left(\frac{q + \delta q}{\|q + \delta q\|}\right) &= (q + \delta q)G_0P_0{}^c(q + \delta q)\frac{1}{\|q + \delta q\|^2} \\ &= (q + \delta q){}^c q GP(q) q {}^c (q + \delta q)\frac{1}{\|q + \delta q\|^2} \end{aligned}$$

$$\begin{aligned}
&= ((1,0,0,0) + \delta q \text{ }^c q) GP(q) ((1,0,0,0) + q \text{ }^c \delta q) \frac{1}{\|q + \delta q\|^2} \\
&= GP(q) + \delta q \text{ }^c q GP(q) + GP(q) q \text{ }^c \delta q + 0(\delta q)^2 \frac{1}{\|q + \delta q\|^2}
\end{aligned}$$

So, because G is independant of  $q$ :

$$P\left(\frac{q + \delta q}{\|q + \delta q\|}\right) - P(q) = q GP\left(\frac{q + \delta q}{\|q + \delta q\|}\right) - GP(q) = \delta q \text{ }^c q GP(q) + GP(q) q \text{ }^c \delta q + 0(\delta q)^2 + GP(q) \frac{1}{\|q + \delta q\|^2}$$

For the directional derivation, we chose  $\delta q = \epsilon * (1, 0, 0, 0)$ . using a equivalent to  $\frac{1}{1+\epsilon}$

$$\lim_{\epsilon \rightarrow 0} \frac{P\left(\frac{q + \delta q}{\|q + \delta q\|}\right) - P(q)}{\epsilon} = \text{ }^c q GP(q) + GP(q) q - 2q_i GP(q)$$

For the directional derivation, we chose  $\delta q = \epsilon * (0, 1, 0, 0) = \epsilon * e_i$

$$\lim_{\epsilon \rightarrow 0} \frac{P\left(\frac{q + \delta q}{\|q + \delta q\|}\right) - P(q)}{\epsilon} = e_i \text{ }^c q GP(q) - GP(q) q e_i - 2q_i GP(q)$$

Application to the NewtonEulerRImpact:

$$\begin{aligned}
H : \mathbb{R}^7 &\rightarrow \mathbb{R} \\
\nabla_q H &\in \mathcal{M}^{1,7} \\
\nabla_q H &= \begin{pmatrix} N_x \\ N_y \\ N_z \\ (\text{ }^c q GP(q) + GP(q) q - 2q_0 GP(q)).N \\ (e_2 \text{ }^c q GP(q) - GP(q) q e_2 - 2q_1 GP(q)).N \\ (e_3 \text{ }^c q GP(q) - GP(q) q e_3 - 2q_2 GP(q)).N \\ (e_4 \text{ }^c q GP(q) - GP(q) q e_4 - 2q_3 GP(q)).N \end{pmatrix}
\end{aligned}$$

### 12.0.2 Ball case

It is the case where  $GP = -N$ : for  $e_2$ :

$$\begin{aligned}
&(0, 1, 0, 0).(\underline{q_0}, -\underline{p}).(0, -N) = \\
&\left( \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} \cdot \underline{p}, \begin{pmatrix} q_0 \\ 0 \\ 0 \end{pmatrix} - \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} * \underline{p} \right) \cdot (0, -N) = \\
&\left( ?, -\underline{p}_x N - \left( \begin{pmatrix} q_0 \\ 0 \\ 0 \end{pmatrix} - \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} * \underline{p} \right) * N \right) =
\end{aligned}$$

and:

$$\begin{aligned}
&(0, -N).(\underline{q_0}, \underline{p}).(0, 1, 0, 0) = \\
&(N.\underline{p}, -q_0 N - N * \underline{p}).(0, 1, 0, 0) = \\
&\left( ?, (N.\underline{p}) \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} + \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} * (q_0 N + N * \underline{p}) \right) =
\end{aligned}$$

$$\left( ?, (N.\underline{p}) \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} + q_0 \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} * N + \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} * (N * \underline{p}) \right)$$

sub then and get the resulting vector.N:

$$\left[ -\underline{p}_x N - N.\underline{p} \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} + () * N - \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} * (N * \underline{p}) \right].N =$$

$$-\underline{p}_x - N_x N.\underline{p} + 0 - \left( \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} * (N * \underline{p}) \right).N =$$

using  $a * (b * c) = b(a.c) - c(a.b)$  leads to

$$-q_1 - N_x N.\underline{p} - (q_1 N - N_x \underline{p}).N =$$

$$-q_1 - N_x N.\underline{p} - q_1 + N_x N.\underline{p} = -2q_1$$

for  $e1 = (1, 0, 0, 0)$ :

$$(q_0, -\underline{p}).(0, -N) = (?, -q_0 N + \underline{p} * N)$$

$$(0, -N).(q_0, \underline{p}) = (?, -q_0 N - \underline{p} * N)$$

So

$$\nabla_q H = \begin{pmatrix} N_x \\ N_y \\ N_z \\ 0 \\ 0 \\ 0 \\ 0 \end{pmatrix}$$

### 12.0.3 Case FC3D: using the local frame and momentum

$$\begin{pmatrix} m\dot{V} \\ I\dot{\Omega} + \Omega I \Omega \end{pmatrix} = \begin{pmatrix} F_{ext} + R \\ M_{ext R_{obj}} + (R * PG)_{R_{obj}} \end{pmatrix}$$

with  $*$  vectoriel product,  $R$  reaction in the globla frame.  $P$  the point of contact.  $r$  is the reaction in the local frame.  $M_{R_{obj}toR_{abs}} = M_{R_{abs}toR_{obj}}^t r = R$  with:

$$M_{R_C to R_{abs}} = \begin{pmatrix} nx & t_1x & t_2x \\ ny & t_1y & t_2y \\ nz & t_1z & t_2z \end{pmatrix}$$

we have :

$$\begin{pmatrix} R \\ (R * PG)_{R_{obj}} \end{pmatrix} = \begin{pmatrix} I_3 \\ M_{R_{abs}toR_{obj}} N_{PG} \end{pmatrix}.R$$

$$= \begin{pmatrix} I_3 \\ M_{R_{abs}toR_{obj}} N_{PG} \end{pmatrix}.M_{R_{obj}toR_{abs}} r$$

$$N_{PG} = \begin{pmatrix} 0 & PG_z & -PG_y \\ -PG_z & 0 & PG_x \\ PG_y & -PG_x & 0 \end{pmatrix}$$

that is:

$$\begin{pmatrix} m\dot{V} \\ I\dot{\Omega} + \Omega I \Omega \end{pmatrix} = \begin{pmatrix} M_{R_C to R_{abs}} \\ M_{R_{abs}toR_{obj}} N_{PG} M_{R_C to R_{abs}} \end{pmatrix} r$$

So  $jachqt = MN$

### 12.0.4 Case FC3D: using the local frame local velocities

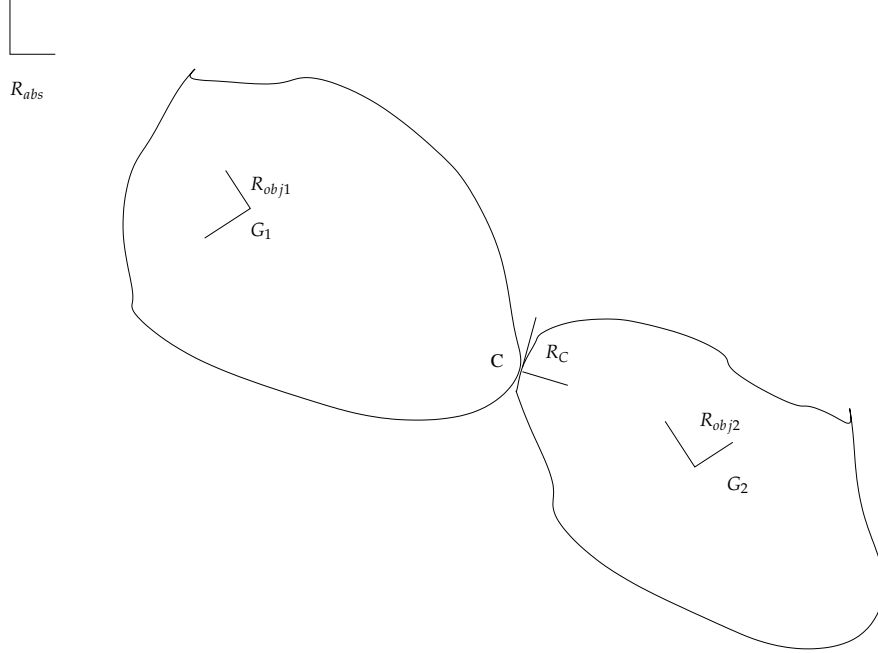


Figure 12.2: Two objects colliding.

{figCase}

We are looking for an operator named  $CT$  such that:

$$V_C = \begin{pmatrix} V_N \\ V_T \\ V_S \end{pmatrix}_{R_C} = CT \begin{pmatrix} V_{G1} R_{abs} \\ \Omega_1 R_{obj1} \\ V_{G2} R_{abs} \\ \Omega_2 R_{obj2} \end{pmatrix}$$

$$V_C = V_{G1} R_{abs} + w_1 * G_1 P_{R_{abs}} - (V_{G2} R_{abs} + w_2 * G_1 P_{R_{abs}})$$

where  $w_1$  and  $w_2$  are given in  $R_{abs}$ . We note  $M_{R_{obj1}toR_{abs}}$  the matrice converting the object 1 coordinate to the absolute coordinate. We note  $N_{GP}$  the matrice such that  $w_1 * G_1 P_{R_{abs}} = N_{GC} w_1$ . Endly, we note  $M_{R_{abs}toR_C}$  converting the absolute coordinate to the  $R_C$  frame. we get:

$$CT = M_{R_{abs}toR_C} \begin{pmatrix} I_3 & N_{G1C} M_{R_{obj1}toR_{abs}} & -I_3 & -N_{G2C} M_{R_{obj2}toR_{abs}} \end{pmatrix}$$

#### 12.0.4.a Expression of $M_{R_{obj1}toR_{abs}}$

Using quaternion, we get :

$$M_{R_{obj1}toR_{abs}} = \begin{pmatrix} q \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} {}^c q & q \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix} {}^c q & q \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix} {}^c q \end{pmatrix} \quad (12.1) \quad \{\text{eq:newton\_Mobjt}\}$$

#### 12.0.4.b Expression of $N_1$

$$N_{GC} = \begin{pmatrix} 0 & G_1 C_z & -G_1 C_y \\ -G_1 C_z & 0 & G_1 C_x \\ G_1 C_y & -G_1 C_x & 0 \end{pmatrix}$$

# Chapter 13

## Projection On constraints

### 13.0.1 Velocity formulation

The first step consists in doing a velocity formulation of the system:

$$\begin{aligned} M\dot{v} &= F_{ext} + B\lambda \\ \dot{q} &= Tv \\ y &= h(q) \\ NSLAW(y, \lambda, \dots) \end{aligned} \tag{13.1} \quad \{\text{NE\_Dyn1}\}$$

The constraint  $\dot{q} = Tv$  is sufficient to keep a normal quaternion. Because of the speed formulation,  $h(q)$  could violate the NSLAW. A solution could be to add a formulation in position. We must underline that the constraints  $|Q| = 1$  is implicit in this system. Indeed, the direction  $\dot{q} = Tv$  is tangential to the sphere.

### 13.0.2 Posion formulation

It consists in writting a position formulation on the system:

$$h(q) = \begin{pmatrix} HI(q) \\ HE(q) \end{pmatrix} \tag{13.2} \quad \{\text{NE\_Dyn1}\}$$

#### 13.0.2.a Approach using q

We are looking for  $q_1$  from  $q_0$ :

$$q_1 = q_0 + \nabla HI \wedge_I + \nabla HE \wedge_E \tag{13.3}$$

Assume that  $h(q_0)$  doesn't satisfy the constraints, ie  $HI(q_0) \not\perp 0$  or  $HE(q_0) \neq 0$ . Linearize  $h$  leads to:

$$0 \leq HI(q_0) + \nabla^t HI(\nabla HI \wedge_I + \nabla HE \wedge_E) \perp \wedge_I \geq 0 \tag{13.4}$$

$$0 = HE(q_0) + \nabla^t HE(\nabla HI \wedge_I + \nabla HE \wedge_E) \tag{13.5}$$

The getting system could be written has a MLCP:

$$C \ni h(q_0) + \nabla^t h(\nabla h \wedge), \wedge \in C^* \tag{13.6}$$

In the case of a quaternion  $Q$  for the rotation representation, it is noteworthy that this system doesn't deal with the constraints  $|Q| = 1$ . Thus, the direction  $(q_1, q_0)$  can be normal to this constraint, in that case this approach doesn't work. (It happens in practice) The solution that consists in normaliaed q after this formulation is not convenient because, it could be incompatible with  $|Q| = 1$ . A better approach is to add this constraint.



The constraint  $|Q| = 1$  in the system HE:

$$\tilde{H}E(q) = \begin{pmatrix} HE(q) \\ |Q| - 1 \end{pmatrix} \quad (13.7)$$

The formulation described above can be done.

### 13.0.2.b Approach using V

It consists in building the OSNSP using  $CT$  instead of  $C$ .

$$h(q_1) = h(q_0) + \nabla^t H \delta q \quad (13.8) \quad \{\text{NE\_projV}\}$$

ie:

$$h(q_1) = h(q_0) + \nabla^t H T V \quad (13.9) \quad \{\text{NE\_projV}\}$$

We are looking for  $q_1$  such that:

$$q_1 - q_0 = \nabla H \Lambda \quad (13.10)$$

We have

$$\delta q = TV, \quad {}^t T \delta q = {}^t T T V, \quad ({}^t T T)^{-1} {}^t T \delta q = V$$

ie

$$h(q_1) = h(q_0) + {}^t \nabla_q h T ({}^t T T)^{-1} {}^t T \nabla_q h \Lambda \quad (13.11)$$

With  $C = {}^t \nabla_q h$  leading to the problem:

$$K \ni h(q_0) + C T ({}^t T T)^{-1} {}^t (C T) \Lambda \in K^* \quad (13.12)$$

## Chapter 14

# Simulation of a Cam Follower System

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The free body dynamics can be described by a linear second order system. An external input is considered acting directly on the follower. This input is a non linear forcing component coming from the valve. The follower motion is constrained to a phase space region bounded by the cam position. The non conservative Newton restitution law is used for the computation of the post impact velocity. The cam is assumed to be massive therefore only rotational displacement is allowed. Under these assumptions, the free body dynamics of the follower can be described by

$$\mu \frac{d^2 u(t)}{dt^2} + \zeta \frac{du(t)}{dt} + \kappa u(t) = f_v(t), \quad \text{if } u(t) > c(t). \quad (14.1) \quad \{\text{eq:sols}\}$$

where  $\mu$ ,  $\zeta$  and  $\kappa$  are constant parameters for the follower mass, friction viscous damping and spring stiffness respectively. The state of the follower is given by the position  $u(t)$  and velocity  $v(t) = \frac{du}{dt}$ . The external forcing is given by  $f_v(t)$ . The cam angular position determines  $c(t)$  that defines the holonomic (i.e. constraint only on the position) rheonomic (i.e. time varying) constraint. The dynamic behavior when impacts occurs (i.e.  $u(t) = c(t)$ ) is modelled via Newton's impact law that in this case is given by

$$v(t^+) = \frac{dc}{dt} - r \left( v(t^-) - \frac{dc}{dt} \right) = (1+r) \frac{dc}{dt} - rv(t^-), \quad \text{if } u(t) = c(t). \quad (14.2) \quad \{\text{eq:il}\}$$

where  $v(t^+)$  and  $v(t^-)$  are the post and pre impact velocities respectively,  $\frac{dc}{dt}$  is the velocity vector of the cam at the contact point with the follower, and  $r \in [0, 1]$  is the restitution coefficient to model from plastic to elastic impacts. In Figure 14.1 is presented the schematic diagram of the physical cam-follower system. In Figure 14.1.a for  $t = 0$ , 14.1.b for  $t = \beta$ , and 14.1.c the profile of the constraint position  $\delta c(t)$ , velocity  $\frac{dc}{dt}(t)$  and acceleration  $\frac{d^2c}{dt^2}(t)$ . It is possible to visualize the follower displacement as a function of the cam position. It is also important to notice that different types of cams and followers profiles are used in practical applications.

### 14.0.1 The cam-follower as a Lagrangian NSDS.

It is possible to completely describe the cam-follower system as a driven impact oscillator into the framework of *Lagrangian NSDS* using a translation in space. Setting  $\hat{u}(t) = u(t) - c(t)$  and  $\hat{v}(t) = v(t) - dc/dt$ , then equations (14.1) and (14.2) can be expressed as (the argument  $t$  will not be explicitly written)

$$\mu \frac{d^2 \hat{u}}{dt^2} + \zeta \frac{d\hat{u}}{dt} + \kappa \hat{u} = f_v - \left( \mu \frac{d^2 c}{dt^2} + \zeta \frac{dc}{dt} + \kappa c \right) \equiv \hat{f}, \quad \text{if } \hat{u} > 0. \quad (14.3) \quad \{\text{eq:trans}\}$$

$$\hat{v}^+ = -r\hat{v}^-, \quad \text{if } \hat{u} = 0. \quad (14.4)$$

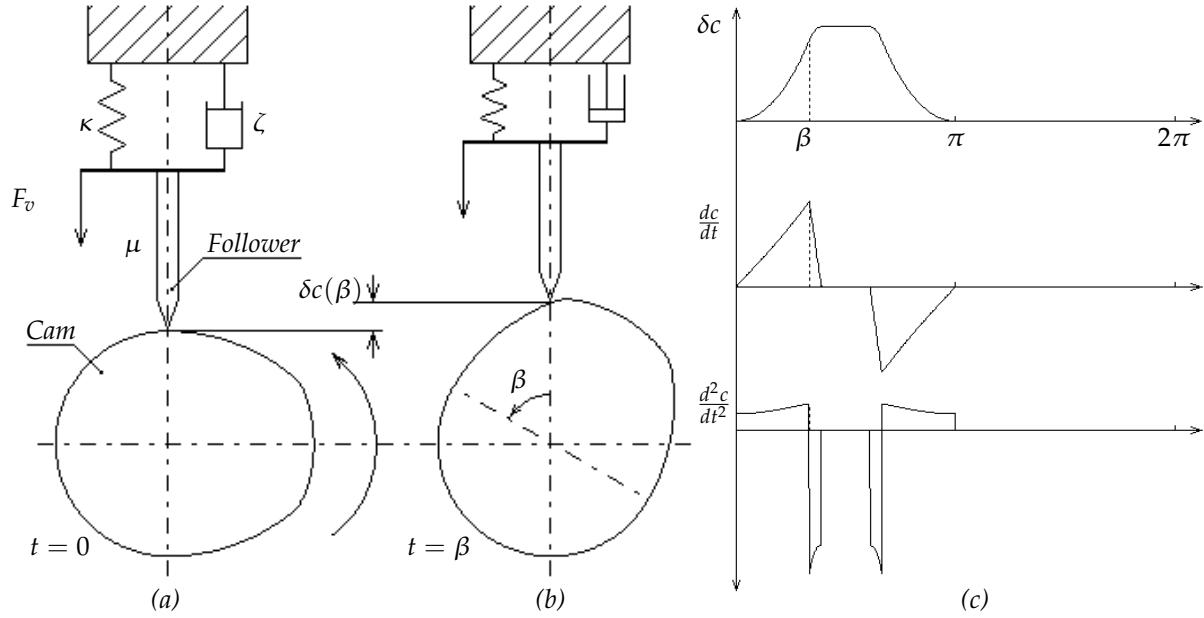


Figure 14.1: Cam-Shaft's schematics. (a)  $t=0$ . (b)  $t=\beta$ . (c) Constraint position  $\delta c(t)$ , velocity  $\frac{d\delta c}{dt}(t)$  and acceleration  $\frac{d^2\delta c}{dt^2}(t)$ .

{Fig:cam-shaft}

Using the framework presented in [2] we have that the equation of motion of a Lagrangian system may be stated as follows :

$$M(q)\ddot{q} + Q(q, \dot{q}) + F(q, \dot{q}, t) = F_{ext}(t) + R \quad (14.5) \quad \{\text{eq:lag1}\}$$

From the (14.3) we can derive all of the terms which define a Lagrangian NSDS. In our case the model is completely linear:

$$\begin{aligned} q &= [\hat{u}] \\ M(q) &= [\mu] \\ Q(q, \dot{q}) &= [0] \\ F(q, \dot{q}) &= [\zeta] \dot{q} + [\kappa] q \\ F_{ext} &= [\hat{f}] \end{aligned} \quad (14.6) \quad \{\text{eq:lag2}\}$$

The unilateral constraint requires that:

$$\hat{u} \geq 0$$

so we can obtain

$$\begin{aligned} y &= H^T q + b \\ H^T &= [1] \\ b &= 0 \end{aligned} \quad (14.7) \quad \{\text{eq:constr}\}$$

In the same way, the reaction force due to the constraint is written as follows:

$$R = H\lambda, \quad \text{with } H = [1]$$

The unilateral contact law may be formulated as follow:

$$0 \leq y \perp \lambda \geq 0 \quad (14.8) \quad \{\text{eq:17}\}$$

and the Newton's impact law:

$$\text{If } y = 0, \dot{y}^+ = -r\dot{y}^- \quad (14.9) \quad \{\text{eq:17}\}$$

## 14.0.2 Implementation in the platform

For the simulation of the cam follower system follow the steps

1. Move to the working directory `sample/CamFollower`  
`$cd sample/CamFollower`
2. Clean the directory from binary files using the `siconos` command  
`$siconos -c`
3. Compile the file `CamFollowerNoXml.cpp` in the sample folder (See the code at the end of the section)  
`$siconos CamFollowerNoXml.cpp`
4. Change the simulation parameters (*i.e.* Follower initial position and velocity, cam initial angle, simulations time, cam rotational speed in rpm, etc.) in the file `CamFollowerNoXml.cpp`.

Next we present the sample code for the `CamFollowerNoXml.cpp` file:

```
int main(int argc, char* argv[]) {
{
    // ===== Creation of the model =====
    // User-defined main parameters
    double rpm=358;
    double phi_0=0;
    unsigned int dsNumber = 1;    // the Follower and the ground
    unsigned int nDof = 1;        // degrees of freedom for the Follower
    double t0 = 0;                // initial computation time
    double T = 5;                // final computation time
    double h = 0.0001;           // time step
    int Kplot;
    Kplot=(int)(Tplot/h);
    double position_init = 0.4;   // initial position for lowest bead.
    double velocity_init = 0.4;   // initial velocity for lowest bead.

    // ===== Dynamical systems =====

    vector<DynamicalSystem*> vectorDS; // the list of DS
    vectorDS.resize(dsNumber,NULL);

    SiconosMatrix *Mass, *K, *C; // mass/rigidity/viscosity
    Mass = new SiconosMatrix(nDof,nDof);
    (*Mass)(0,0) = 1.221;
    K = new SiconosMatrix(nDof,nDof);
    (*K)(0,0) = 1430.8;
    C = new SiconosMatrix(nDof,nDof);
    (*C)(0,0) = 0;

    // Initial positions and velocities
    vector<SimpleVector*> position_0;
    vector<SimpleVector*> velocity_0;
    position_0.resize(dsNumber,NULL);
    velocity_0.resize(dsNumber,NULL);
    position_0[0] = new SimpleVector(nDof);
    velocity_0[0] = new SimpleVector(nDof);
    (*(position_0[0]))(0) = position_init;
```

```

(*(velocity_0[0]))(0) = velocity_init;

vectorDS[0] =
new LagrangianLinearTIDS(0,nDof,*(position_0[0]),*(velocity_0[0]),*Mass,*K,*C);

static_cast<LagrangianDS*>(vectorDS[0])
    ->setComputeFExtFunction("FollowerPlugin.so", "FollowerFExt");

// Example to set a list of parameters in FExt function.
// 1 - Create a simple vector that contains the required parameters.

// Here we set two parameters, the DS number.
SimpleVector * param = new SimpleVector(2);

(*param)(0)=rpm;
(*param)(1)=phi_0;
// 2 - Assign this param to the function FExt
static_cast<LagrangianDS*>(vectorDS[0])>setParametersListPtr(param,2);
// 2 corresponds to the position of FExt in the stl vector of possible parameters.
// 0 is mass, 1 Flnt.
// Now the cam rotational velocity in rpms will be available in FExt plugin.

// ===== Interactions =====

vector<Interaction*> interactionVector;
interactionVector.resize(1,NULL);
vector<DynamicalSystem*> *dsConcerned =
    new vector<DynamicalSystem*>(dsNumber);

// ===== Non Smooth Law =====
double e = 0.8;
// Interaction Follower-floor
SiconosMatrix *H = new SiconosMatrix(1,nDof);
(*H)(0,0) = 1.0;
NonSmoothLaw * nslaw = new NewtonImpactLawNSL(e);
Relation * relation = new LagrangianLinearR(*H);
(*dsConcerned)[0] = vectorDS[0];
interactionVector[0] = new Interaction("Follower-Ground",0,1, dsConcerned);
interactionVector[0]>setRelationPtr(relation);
interactionVector[0]>setNonSmoothLawPtr(nslaw);
// ===== Interactions =====

// ===== NonSmoothDynamicalSystem =====
bool isBVP =0;
NonSmoothDynamicalSystem * nsds =
    new NonSmoothDynamicalSystem(isBVP);

// Set DS of this NonSmoothDynamicalSystem
nsds->setDynamicalSystems(vectorDS);
// Set interactions of the NonSmoothDynamicalSystem
nsds->setInteractions(interactionVector);

// ===== Model =====

```

```

Model * Follower = new Model(t0,T);
// set NonSmoothDynamicalSystem of this model
Follower->setNonSmoothDynamicalSystemPtr(nsds);

// ===== Strategy =====

double theta = 0.5;          // theta for Moreau integrator
string solverName = "QP" ;

Strategy* S = new TimeStepping(Follower);

// - Time discretisation -
TimeDiscretisation * t = new TimeDiscretisation(h,S);

// - OneStepIntegrators -
vector<OneStepIntegrator*> vOSI;
vOSI.resize(dsNumber,NULL);
vOSI[0] = new Moreau(t,vectorDS[0],theta);
S->setOneStepIntegrators(vOSI);

// - OneStepNsProblem -
OneStepNSProblem * osnspb = new LCP(S,solverName,101, 0.0001,"max",0.6);
S->setOneStepNSProblemPtr(osnspb); // set OneStepNSProblem of the strategy
cout << "=== End of model loading === " << endl;
// ===== End of model definition=====

// ===== Computation=====

// — Strategy initialization —
S->initialize();
cout << "End of strategy initialisation" << endl;

int k = t->getK();           // Current step
int N = t->getNSteps();      // Number of time steps

// — Get the values to be plotted —
// -> saved in a matrix dataPlot
unsigned int outputSize = 8;

SiconosMatrix DataPlot(Kplot+1,outputSize );
// For the initial time step:

// time
DataPlot(k,0) = k*t->getH();

DataPlot(k,1) = static_cast<LagrangianDS*>(vectorDS[0])->getQ()(0);
DataPlot(k,2) = static_cast<LagrangianDS*>(vectorDS[0])->getVelocity()(0);
DataPlot(k,3) = (Follower->getNonSmoothDynamicalSystemPtr()->
    getInteractionPtr(0)->getLambda(1))(0);
DataPlot(k,4) = static_cast<LagrangianDS*>(vectorDS[0])->getFExt()(0);

// State of the Cam

```

```

double CamEqForce,CamPosition,CamVelocity,CamAcceleration;
CamEqForce=
    CamState(k*t->getH(),rpm,CamPosition,CamVelocity,CamAcceleration);
// Position of the Cam
DataPlot(k, 5) = CamPosition;
// Velocity of the Cam
DataPlot(k, 6) = CamVelocity;
// Acceleration of the Cam
DataPlot(k, 7) =
    CamPosition+static_cast<LagrangianDS*>(vectorDS[0])->getQ()(0);

// — Time loop —
cout << "Start computation ... " << endl;
while(k < N)
{
    // — Get values to be plotted —
    DataPlot(k,0) = k*t->getH();

    DataPlot(k,1) =
        static_cast<LagrangianDS*>(vectorDS[0])->getQ()(0);
    DataPlot(k,2) =
        static_cast<LagrangianDS*>(vectorDS[0])->getVelocity()(0);
    DataPlot(k,3) =
        (Follower->getNonSmoothDynamicalSystemPtr()->
        getInteractionPtr(0)->getLambda(1))(0);
    DataPlot(k,4) = static_cast<LagrangianDS*>(vectorDS[0])->getFExt()(0);

    CamEqForce=
    CamState(k*t->getH(),rpm,CamPosition,CamVelocity,CamAcceleration);

    DataPlot(k, 5) = CamPosition;
    DataPlot(k, 6) = CamVelocity;
    DataPlot(k, 7) = CamPosition+
        static_cast<LagrangianDS*>(vectorDS[0])->getQ()(0);
    // transfer of state i+1 into state i and time incrementation
    S->nextStep();
    // get current time step
    k = t->getK();
    // solve ...
    S->computeFreeState();
    S->computeOneStepNSProblem();
    // update
    S->update();
}
// — Output files —
DataPlot.rawWrite("result.dat", "ascii");
// — Free memory —
delete osnspb;
delete vOSI[0];
delete t;
delete S;
delete Follower;
delete nsds;

```

```
    delete interactionVector[0];
    delete relation;
    delete nslaw;
    delete H;
    delete dsConcerned;
    delete vectorDS[0];
    delete position_0[0];
    delete velocity_0[0];
    delete C;
    delete K;
    delete Mass;
}
```



### 14.0.3 Simulation

We have perform the simulation of the cam follower system for different values of the cam rotational speed with the SICONOS software package using a time-stepping numerical scheme with step size ( $h = 1e^{-4}$ ) and an event-driven scheme with minimum step size ( $h_{min} = 1e^{-12}$ ). Fig. 14.2 and 14.3 show the time simulations for different values of the cam rotational speed and Fig. 14.4 show the chaotic attractor at  $rpm = 660$  for impact and stroboscopic Poincaré sections.

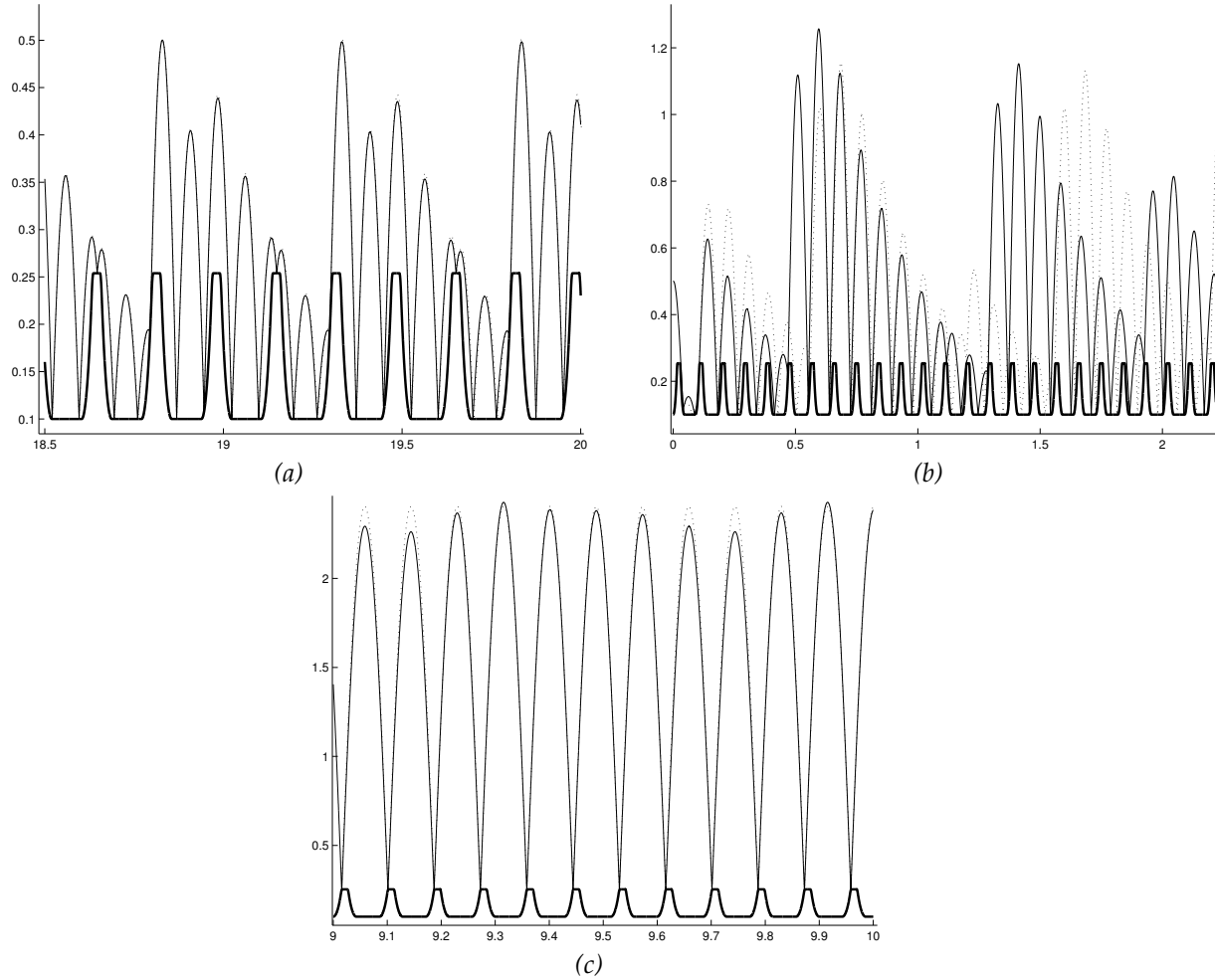


Figure 14.2: Time series using SICONOS platform. Time-stepping scheme (continuous line). Event-driven scheme (dashed line) (a)  $rpm=358$ . (b)  $rpm=660$ . (c)  $rpm=700$ .

{Fig:time\_compar:

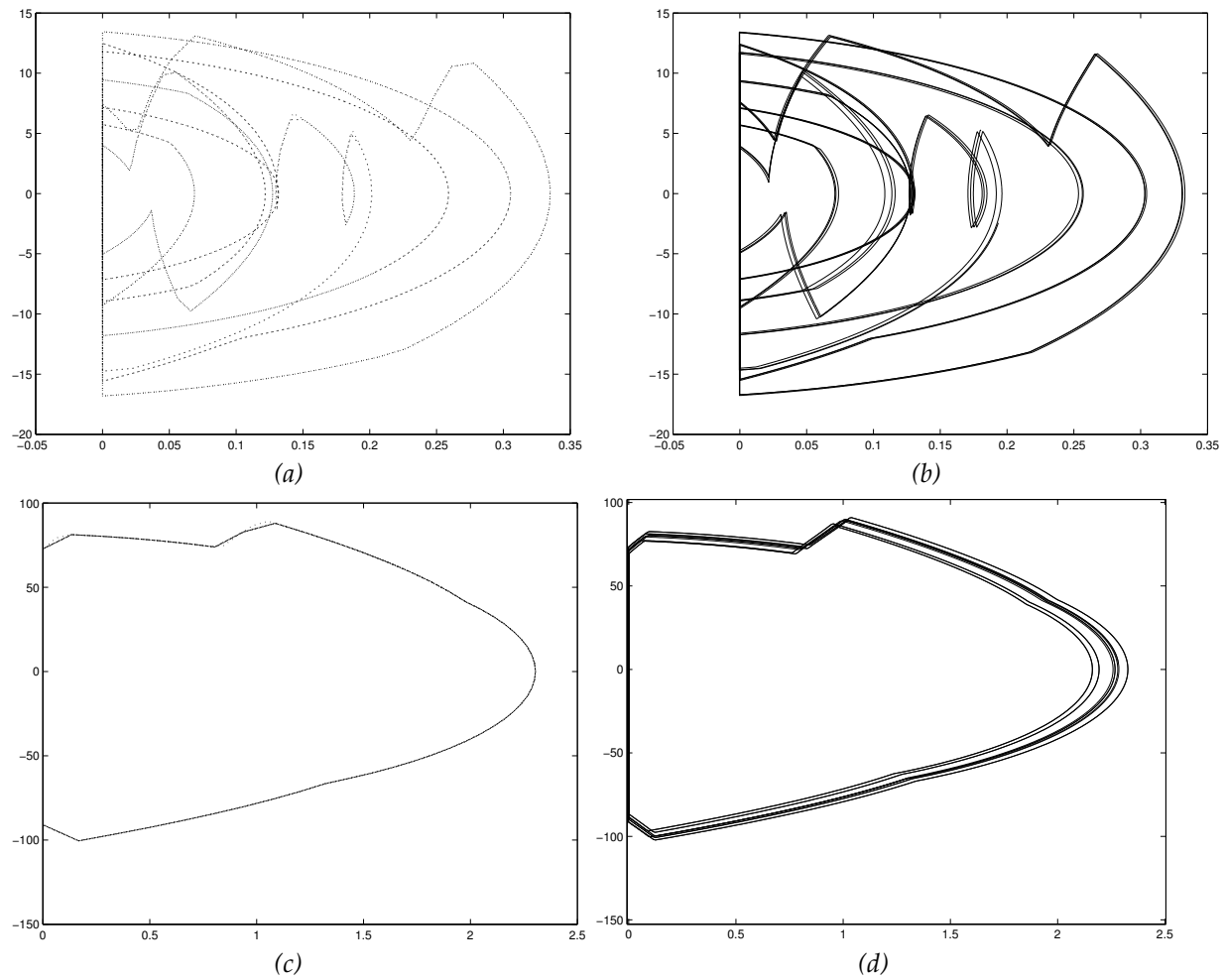


Figure 14.3: State space comparison using SICONOS platform. (a) rpm=358. Event Driven (b) rpm=358. Time Stepping ( $h = 1e^{-4}$ ) (c) rpm=700. Event Driven (d) rpm=700. Time Stepping ( $h = 1e^{-4}$ )

{Fig:state\_compar

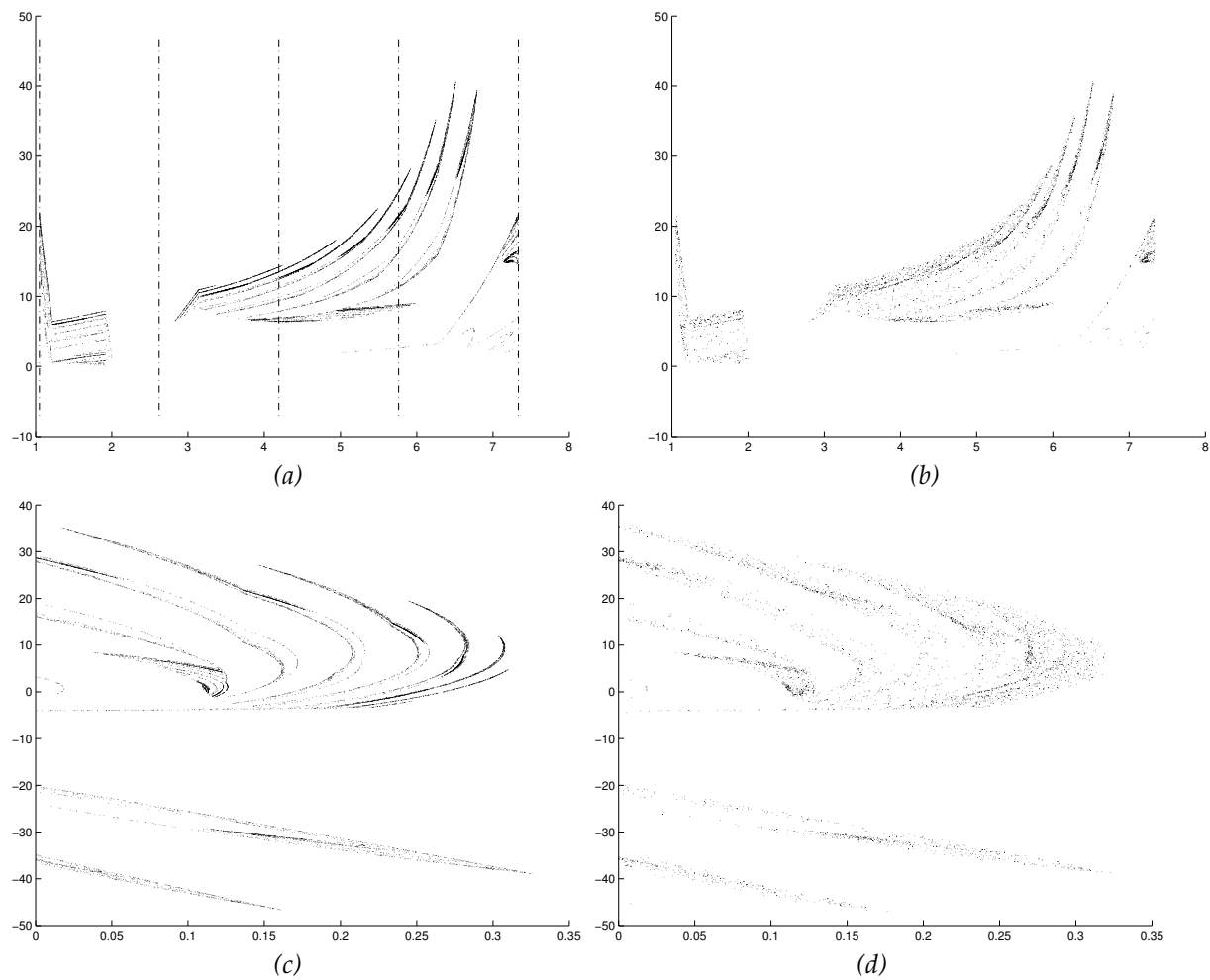


Figure 14.4: Attractors comparison using SICONOS platform at rpm=660. (a) Impact map. (Event Driven) (b) Impact Map. Time Stepping ( $h = 1e^{-4}$ ) (c) Stroboscopic map. (Event Driven) (d) Stroboscopic Map. Time Stepping ( $h = 1e^{-4}$ )

{Fig:attractor\_co

# Chapter 15

## Quartic Formulation

### 15.0.1 Slidding ?

It consists in finding  $\alpha > 0$  and  $R \in \partial K_\mu$  such that  $-\alpha \begin{pmatrix} 0 \\ R_T \end{pmatrix} = MR + q$ . That is :

$$\left[ M + \begin{pmatrix} 0 & 0 & 0 \\ 0 & \alpha & 0 \\ 0 & 0 & \alpha \end{pmatrix} \right] R + q = 0 \quad (15.1) \quad \{\text{eq\_quartic1}\}$$

#### 15.0.1.a $R_T$ is on a conic

The first line of the system 15.1 and the  $R \in \partial K_\mu$  is the intersection between a plan and a cone in  $\mathbb{R}^3$ , ended:

$$\begin{aligned} \mu R_N &= \| R_T \| \\ \frac{M_{11}}{\mu} \| R_T \| &= -q_1 - M_{12}R_{T1} - M_{13}R_{T2} \end{aligned} \quad (15.2) \quad \{\text{eq\_quartic2}\}$$

That is:

$$\begin{aligned} \mu^2 R_N^2 &= (R_{T1}^2 + R_{T2}^2) \\ \frac{M_{11}^2}{\mu^2} (R_{T1}^2 + R_{T2}^2) &= (-q_1 - M_{12}R_{T1} - M_{13}R_{T2})^2 \end{aligned} \quad (15.3) \quad \{\text{eq\_quartic2}\}$$

That means that  $R_T$  is contained in a conic, focus and directrice are:

$$\begin{aligned} \mathcal{D} : q_1 + M_{12}R_{T1} + M_{13}R_{T2} &= 0 \\ \text{focus} : \mathcal{O} \\ \frac{M_{11}^2}{\mu^2} \text{Dist}(\mathcal{O}, R_T)^2 &= \text{Dist}(\mathcal{D}, R_T)^2 (M_{12}^2 + M_{13}^2) \\ \frac{\text{Dist}(\mathcal{O}, R_T)}{\text{Dist}(\mathcal{D}, R_T)} &= \frac{\mu \sqrt{(M_{12}^2 + M_{13}^2)}}{M_{11}} = e \end{aligned} \quad (15.4) \quad \{\text{eq\_quartic3}\}$$

The parametric equation is:

$$\begin{aligned} R_{T1} &= r \cos(\theta) \\ R_{T2} &= r \sin(\theta) \\ r &= \frac{p}{1 + e \cos(\theta - \phi)} \end{aligned} \quad (15.5) \quad \{\text{eq\_quartic4}\}$$

With  $p$  an simple expression of  $M_{11}, M_{12}, M_{13}$ , and  $\phi$  a constant angle between  $\mathcal{D}$  and  $(O, R_{T1})$

#### 15.0.1.b The two last line of the system 15.1

$$\frac{\| R_T \|}{\mu} \tilde{M}_1 + \left( \tilde{M} + \begin{pmatrix} \alpha & 0 \\ 0 & \alpha \end{pmatrix} \right) R_T + \tilde{q} = 0 \quad (15.6) \quad \{\text{eq\_quartic5}\}$$

$\tilde{M}$  is symetric, so it exists a unitary matrix  $V$  such that  $V\tilde{M}V^T = \begin{pmatrix} d_1 & 0 \\ 0 & d_2 \end{pmatrix}$ . One can get:

$$\frac{\|R_T\|}{\mu} V\tilde{M}_1 + V \left( \tilde{M} + \begin{pmatrix} \alpha & 0 \\ 0 & \alpha \end{pmatrix} \right) V^T V R_T + V\tilde{q} = 0 \quad (15.7) \quad \{\text{eq\_quartic6}\}$$

Rename:

$$\frac{\|\bar{R}_T\|}{\mu} \tilde{M}_1 + \begin{pmatrix} d_1 + \alpha & 0 \\ 0 & d_2 + \alpha \end{pmatrix} \bar{R}_T + \bar{q} = 0 \quad (15.8) \quad \{\text{eq\_quartic7}\}$$

In the plan, either  $V$  is a rotation or a symetrie. So  $\bar{R}_T = V R_T$  is a conic with the same focus and a rotated directrice, it means that it exists  $\phi_1$  such that :

$$\begin{aligned} \bar{R}_{T1} &= r \cos(\theta) \\ \bar{R}_{T2} &= r \sin(\theta) \\ r &= \frac{p}{1 + \cos(\theta - \phi_1)} \end{aligned} \quad (15.9) \quad \{\text{eq\_quartic8}\}$$

The equation 15.8 is :

$$\begin{aligned} (d_1 + \alpha) \bar{R}_{T1} &= -\bar{q}_1 + a_1 \|R_T\| \\ (d_2 + \alpha) \bar{R}_{T2} &= -\bar{q}_2 + a_2 \|R_T\| \end{aligned} \quad (15.10) \quad \{\text{eq\_quartic9}\}$$

The case ( $\bar{R}_{T1} = 0$  or  $\bar{R}_{T2} = 0$ ) has to be examine. We try to eliminate *alpha*:

$$\begin{aligned} d_1 \bar{R}_{T1} \bar{R}_{T2} + \alpha \bar{R}_{T1} \bar{R}_{T2} &= -\bar{q}_1 \bar{R}_{T2} + a_1 \bar{R}_{T2} \|R_T\| \\ d_2 \bar{R}_{T1} \bar{R}_{T2} + \alpha \bar{R}_{T1} \bar{R}_{T2} &= -\bar{q}_2 \bar{R}_{T1} + a_2 \bar{R}_{T1} \|R_T\| \end{aligned} \quad (15.11) \quad \{\text{eq\_quartic10}\}$$

that leads to:

$$(d_1 - d_2) \bar{R}_{T1} \bar{R}_{T2} = -\bar{q}_1 \bar{R}_{T2} + \bar{q}_2 \bar{R}_{T1} + (a_1 \bar{R}_{T2} - a_2 \bar{R}_{T1}) \|R_T\| \quad (15.12) \quad \{\text{eq\_quartic10}\}$$

The parametric expression of  $\bar{R}_T$  leads to:

$$\begin{aligned} (d_1 - d_2) r^2 \cos(\theta) \sin(\theta) &= -\bar{q}_1 r \sin(\theta) + \bar{q}_2 r \cos(\theta) + r(a_1 r \sin(\theta) - a_2 r \cos(\theta)) \\ \text{ie: } (d_1 - d_2) r \cos(\theta) \sin(\theta) &= -\bar{q}_1 \sin(\theta) + \bar{q}_2 \cos(\theta) + r(a_1 \sin(\theta) - a_2 \cos(\theta)) \end{aligned} \quad (15.13) \quad \{\text{eq\_quartic11}\}$$

with the expression of r:

$$\begin{aligned} (d_1 - d_2) \frac{p}{1 + \cos(\theta - \phi_1)} \cos(\theta) \sin(\theta) &= \\ -\bar{q}_1 \sin(\theta) + \bar{q}_2 \cos(\theta) + \frac{p}{1 + \cos(\theta - \phi_1)} (a_1 \sin(\theta) - a_2 \cos(\theta)) & \\ \text{ie: } (d_1 - d_2) p \cos(\theta) \sin(\theta) &= \\ (1 + \cos(\theta - \phi_1)) (-\bar{q}_1 \sin(\theta) + \bar{q}_2 \cos(\theta)) + p(a_1 \sin(\theta) - a_2 \cos(\theta)) & \end{aligned} \quad (15.14) \quad \{\text{eq\_quartic12}\}$$

$$\begin{aligned} \text{ie: } (d_1 - d_2) p \cos(\theta) \sin(\theta) &= \\ (1 + e(\cos(\theta) \cos(\phi_1) + \sin(\theta) \sin(\phi_1))) (-\bar{q}_1 \sin(\theta) + \bar{q}_2 \cos(\theta)) + p(a_1 \sin(\theta) - a_2 \cos(\theta)) & \end{aligned}$$

$$\begin{aligned} \text{ie: } (d_1 - d_2) p \cos(\theta) \sin(\theta) + \\ (1 + \cos(\theta) \cos(\phi_1) + \sin(\theta) \sin(\phi_1)) (\bar{q}_1 \sin(\theta) - \bar{q}_2 \cos(\theta)) + p(-a_1 \sin(\theta) + a_2 \cos(\theta)) &= 0 \end{aligned}$$

rename :

$$A \cos(\theta)^2 + B \sin(\theta)^2 + C \sin(\theta) \cos(\theta) + D \sin(\theta) + E \cos(\theta) = 0 \quad (15.15) \quad \{\text{eq\_quartic13}\}$$

with

$$\begin{aligned} A &= -e \bar{q}_2 \cos(\phi_1) \\ B &= e \bar{q}_1 \sin(\phi_1) \\ C &= (d_1 - d_2) p + \cos(\phi_1) \bar{q}_1 - \sin(\phi_1) \bar{q}_2 \\ D &= \bar{q}_1 - p a_1 \\ E &= -\bar{q}_2 + p a_2 \end{aligned} \quad (15.16) \quad \{\text{eq\_quartic12}\}$$

rename : Using the following set of unknown :

$$\begin{aligned} t &= \tan(\theta/2) \\ \sin(\theta) &= \frac{2t}{1+t^2} \\ \cos(\theta) &= \frac{1-t^2}{1+t^2} \end{aligned} \quad (15.17) \quad \{\text{eq\_quartic14}\}$$

leads to:

$$\begin{aligned} &A \frac{(1-t^2)^2}{1+t^2} + B \frac{4t^2}{1+t^2} + C \frac{2t(1-t^2)}{1+t^2} + D2t + E(1-t^2) = 0 \\ \text{ie: } &A(1-t^2)^2 + 4Bt^2 + C2t(1-t^2) + 2Dt(1+t^2) + E(1-t^2)(1+t^2) = 0 \\ &\text{ie: } P_4 = A - E \quad P_3 = -2C + 2D \quad P_2 = 4B - 2A \quad P_1 = 2C + 2D \quad P_0 = A + E \end{aligned} \quad (15.18) \quad \{\text{eq\_quartic13}\}$$

Finally, we get 4 possible values for  $R_T$ , checking the sign of  $\alpha$  and  $R_N$  selects the solutions.

#### 15.0.1.c case $R_{T12} = 0$

From 15.10,  $R_{T1}$  leads to:

$$\begin{aligned} \| R_T \| &= |\bar{R}_{T2}| = \frac{\bar{q}_1}{a_1} \\ \bar{R}_T &= \begin{pmatrix} 0 \\ \pm \frac{\bar{q}_1}{a_1} \end{pmatrix} \end{aligned} \quad (15.19) \quad \{\text{eq\_quartic14}\}$$

From 15.10,  $R_{T2}$  leads to:

$$\begin{aligned} \| R_T \| &= |\bar{R}_{T1}| = \frac{\bar{q}_2}{a_2} \\ \bar{R}_T &= \begin{pmatrix} \pm \frac{\bar{q}_2}{a_2} \\ 0 \end{pmatrix} \end{aligned} \quad (15.20) \quad \{\text{eq\_quartic14}\}$$

From  $\bar{R}_T$ , we have to check the coherence with the equation 15.9. If it is on the conic, we compute  $R$ , and the sign condition of the equation 15.1 must be check.

# Chapter 16

## Alart–Curnier Formulation

### 16.1 Reduced formulation to local variables.

#### 16.1.1 Formulation

Let us start with

$$\begin{aligned}\Phi_1(U, P) &= -U_{k+1} + \widehat{W}P_{k+1} + U_{\text{free}} \\ \Phi_2(U, P) &= P_N - \text{proj}_{\mathbb{R}_+^a}(P_N - \rho_N \circ (U_N + e \circ U_{N,k})) \\ \Phi_3(U, P) &= P_T - \text{proj}_{\widehat{\mathbf{D}}(P_N, U_N)}(P_T - \rho_T \circ U_T)\end{aligned}\tag{16.1} \quad \{\text{eq:AC-L7}\}$$

where the modified friction disk for a contact  $\alpha$  is

$$\widehat{\mathbf{D}}^\alpha(P_{N,k+1}^\alpha, U_{N,k+1}^\alpha) = \mathbf{D}(\mu(\text{proj}_{\mathbb{R}_+}(P_{N,k+1}^\alpha - \rho_N^\alpha(U_{N,k+1}^\alpha + e^\alpha U_{N,k}^\alpha))).\tag{16.2} \quad \{\text{eq:AC-L3}\}$$

#### 16.1.2 Structure of the Jacobians

Let us denote the one element of the generalized Jacobian by  $H(U, P) \in \partial\Phi(U, P)$  which has the structure

$$H(U, P) = \begin{bmatrix} -I & 0 & \widehat{W}_{\text{NN}} & \widehat{W}_{\text{NT}} \\ 0 & -I & \widehat{W}_{\text{TN}} & \widehat{W}_{\text{TT}} \\ \partial_{U_N}\Phi_2(U, P) & 0 & \partial_{P_N}\Phi_2(U, P) & 0 \\ \partial_{U_N}\Phi_3(U, P) & \partial_{U_T}\Phi_3(U, P) & \partial_{P_N}\Phi_3(U, P) & \partial_{P_T}\Phi_3(U, P) \end{bmatrix}\tag{16.3} \quad \{\text{eq:AC-L6}\}$$

#### 16.1.3 Computation of the gradients

Let us consider the single contact case.

**Computation of the gradients of  $\Phi_2$**

$$\Phi_2(U, P) = P_N - \text{proj}_{\mathbb{R}_+^a}(P_N - \rho_N(U_N + eU_{N,k}))\tag{16.4} \quad \{\text{eq:AC-T1}\}$$

- If  $P_N - \rho_N(U_N + eU_{N,k}) \geq 0$ , we get

$$\Phi_2(U, P) = +\rho_N(U_N + eU_{N,k})\tag{16.5} \quad \{\text{eq:AC-T2}\}$$

and

$$\begin{aligned}\partial_{U_N} \Phi_2(U, P) &= +\rho_N \\ \partial_{P_N} \Phi_2(U, P) &= 0\end{aligned}\tag{16.6} \quad \{\text{eq:AC-T3}\}$$

- If  $P_N - \rho_N(U_N + eU_{N,k}) < 0$ , we get

$$\Phi_2(U, P) = P_N \tag{16.7} \quad \{\text{eq:AC-T4}\}$$

and

$$\begin{aligned}\partial_{U_N} \Phi_2(U, P) &= 0 \\ \partial_{P_N} \Phi_2(U, P) &= 1\end{aligned}\tag{16.8} \quad \{\text{eq:AC-T5}\}$$

### Computation of the gradients of $\Phi_3$

$$\Phi_3(U, P) = P_T - \text{proj}_{\hat{D}(P_N, U_N)}(P_T - \rho_T U_T) \tag{16.9} \quad \{\text{eq:AC-TT1}\}$$

- If  $\|P_T - \rho_T U_T\| \leq \mu \max(0, P_N - \rho_N(U_N + eU_{N,k}))$ , we get

$$\Phi_3(U, P) = +\rho_T U_T \tag{16.10} \quad \{\text{eq:AC-TT2}\}$$

and

$$\begin{aligned}\partial_{U_N} \Phi_3(U, P) &= 0 \\ \partial_{P_N} \Phi_3(U, P) &= 0 \\ \partial_{U_T} \Phi_3(U, P) &= +\rho_T \\ \partial_{P_T} \Phi_3(U, P) &= 0\end{aligned}\tag{16.11} \quad \{\text{eq:AC-TT3}\}$$

- If  $\|P_T - \rho_T U_T\| > \mu \max(0, P_N - \rho_N(U_N + eU_{N,k}))$ , we get

$$\Phi_3(U, P) = P_T - \mu \max(0, P_N - \rho_N(U_N + eU_{N,k})) \frac{P_T - \rho_T U_T}{\|P_T - \rho_T U_T\|} \tag{16.12} \quad \{\text{eq:AC-TT4}\}$$

- If  $P_N - \rho_N(U_N + eU_{N,k}) \leq 0$ , we get

$$\Phi_3(U, P) = P_T \tag{16.13} \quad \{\text{eq:AC-TT5}\}$$

and

$$\begin{aligned}\partial_{U_N} \Phi_3(U, P) &= 0 \\ \partial_{P_N} \Phi_3(U, P) &= 0 \\ \partial_{U_T} \Phi_3(U, P) &= 0 \\ \partial_{P_T} \Phi_3(U, P) &= I_2\end{aligned}\tag{16.14} \quad \{\text{eq:AC-TT6}\}$$

- If  $P_N - \rho_N(U_N + eU_{N,k}) > 0$ , we get

$$\Phi_3(U, P) = P_T - \mu(P_N - \rho_N(U_N + eU_{N,k})) \frac{P_T - \rho_T U_T}{\|P_T - \rho_T U_T\|} \tag{16.15} \quad \{\text{eq:AC-TT7}\}$$



and

$$\begin{aligned}
\partial_{U_N} \Phi_3(U, P) &= \mu \rho_N \frac{P_T - \rho_T U_T}{\|P_T - \rho_T U_T\|} \text{WARNING case was not taken into account} \\
\partial_{P_N} \Phi_3(U, P) &= -\mu \frac{P_T - \rho_T U_T}{\|P_T - \rho_T U_T\|} \\
\partial_{U_T} \Phi_3(U, P) &= \mu \rho_T (P_N - \rho_N (U_N + e U_{N,k})) \Gamma(P_T - \rho_T U_T) \\
\partial_{P_T} \Phi_3(U, P) &= I_2 - \mu (P_N - \rho_N (U_N + e U_{N,k})) \Gamma(P_T - \rho_T U_T)
\end{aligned} \tag{16.16} \quad \{\text{eq:AC-TT8}\}$$

### 16.1.4 Rearranging the cases

TO BE COMPLETED

## 16.2 Formulation with global variables.

### 16.2.1 Formulation

Let us start with

$$\begin{aligned}
\Psi_1^a(v, U, P) &= -\hat{M} v_{k+1} + H P_{k+1} + q \\
\Psi_1^b(v, U, P) &= -U_{k+1} + H^\top v_{k+1} + b \\
\Psi_2(v, U, P) &= P_N - \text{proj}_{\mathbb{R}_+^a} (P_N - \rho_N \circ (U_N + e \circ U_{N,k})) \\
\Psi_3(v, U, P) &= P_T - \text{proj}_{\hat{D}(P_N, U_N)} (P_T - \rho_T \circ U_T)
\end{aligned} \tag{16.17} \quad \{\text{eq:GAC-L1}\}$$

where the modified friction disk for a contact  $\alpha$  is

$$\hat{D}^\alpha(P_{N,k+1}^\alpha, U_{N,k+1}^\alpha) = D(\mu(\text{proj}_{\mathbb{R}_+^a} (P_{N,k+1}^\alpha - \rho_N^\alpha (U_{N,k+1}^\alpha + e^\alpha U_{N,k}^\alpha))). \tag{16.18} \quad \{\text{eq:GAC-L2}\}$$

### 16.2.2 Structure of the Jacobians

Let us denote the one element of the generalized Jacobian by  $H(v, U, P) \in \partial \Psi(s, U, P)$  which has the structure

$$H(v, U, P) = \begin{bmatrix} -\hat{M} & 0 & 0 & H_N & H_T \\ H_N^\top & -I & 0 & 0 & 0 \\ H_T^\top & 0 & -I & 0 & 0 \\ 0 & \partial_{U_N} \Psi_2(v, U, P) & 0 & \partial_{P_N} \Psi_2(v, U, P) & 0 \\ 0 & \partial_{U_N} \Psi_3(v, U, P) & \partial_{U_T} \Psi_3(v, U, P) & \partial_{P_N} \Psi_3(v, U, P) & \partial_{P_T} \Psi_3(v, U, P) \end{bmatrix} \tag{16.19} \quad \{\text{eq:GAC-L3}\}$$

We clearly have

$$\begin{aligned}
\partial_U \Psi_2(v, U, P) &= \partial_U \Phi_2(U, P) \\
\partial_P \Psi_2(v, U, P) &= \partial_P \Phi_2(U, P) \\
\partial_U \Psi_3(v, U, P) &= \partial_U \Phi_3(U, P) \\
\partial_P \Psi_3(v, U, P) &= \partial_P \Phi_3(U, P)
\end{aligned} \tag{16.20} \quad \{\text{eq:equivalentJa}\}$$

and we get

$$H(v, U, P) = \begin{bmatrix} -\widehat{M} & 0 & 0 & H_N & H_T \\ H_N^\top & -I & 0 & 0 & 0 \\ H_T^\top & 0 & -I & 0 & 0 \\ 0 & \partial_{U_N} \Phi_2(U, P) & 0 & \partial_{P_N} \Phi_2(U, P) & 0 \\ 0 & \partial_{U_N} \Phi_3(U, P) & \partial_{U_T} \Phi_3(U, P) & \partial_{P_N} \Phi_3(U, P) & \partial_{P_T} \Phi_3(U, P) \end{bmatrix} \quad (16.21) \quad \{\text{eq:GAC-L4}\}$$

### 16.2.3 Simplification ?

Since the second line  $\Psi_1^b$  is linear, we should be able to derive a reduced Jacobian using the chain rule.

Let us define  $\tilde{\Psi}$

$$\tilde{\Psi}(v, P) = \Psi(v, H^\top v + b, P) \quad (16.22) \quad \{\text{eq:chainrule}\}$$

$$\tilde{\Psi}_1(v, P) = -\widehat{M}v_{k+1} + HP_{k+1} + q$$

$$\tilde{\Psi}_2(v, P) = P_N - \text{proj}_{\mathbb{R}_+^a}(P_N - \rho_N \circ (H_N^\top v + b_N + e \circ U_{N,k})) \quad (16.23) \quad \{\text{eq:GAC-L5}\}$$

$$\tilde{\Psi}_3(v, P) = P_T - \text{proj}_{\widehat{\mathbf{D}}(P_N, U_N)}(P_T - \rho_T \circ (H_T^\top v + b_T))$$

**Chain rule**

$$\begin{aligned} \partial_v \tilde{\Psi}_{2,3}(v, P) &= \partial_v \Psi_{2,3}(v, H^\top v + b, P) \\ &= H_N^\top \partial_{U_N} \Phi_{2,3}(H^\top v + b, P) + H_T^\top \partial_{U_T} \Phi_{2,3}(H^\top v + b, P) \end{aligned} \quad (16.24) \quad \{\text{eq:chainrule1}\}$$

$$H(v, P) = \begin{bmatrix} -\widehat{M} & H_N & H_T \\ H_N^\top \partial_{U_N} \Phi_2(H^\top v + b, P) & \partial_{P_N} \Phi_2(H^\top v + b, P) & 0 \\ H_N^\top \partial_{U_N} \Phi_3(H^\top v + b, P) + H_T^\top \partial_{U_T} \Phi_3(H^\top v + b, P) & \partial_{P_N} \Phi_3(H^\top v + b, P) & \partial_{P_T} \Phi_3(H^\top v + b, P) \end{bmatrix} \quad (16.25) \quad \{\text{eq:GAC-L6}\}$$

**discussion**

- Formulae has to be checked carefully
- I do not known if there an interest in the simplification. With sparse matrices, it is perhaps easier to deal with (16.21)