

材料力学

第八章 组合变形

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§ 8-1 概述

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§ 8-1 概 述

一、基本变形：

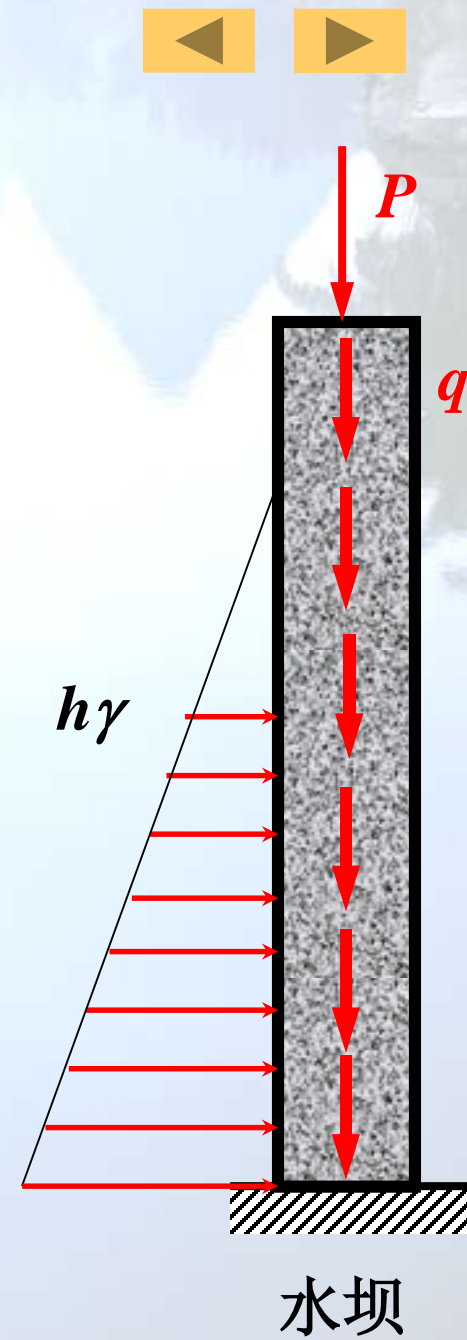
拉伸（压缩）、扭转、弯曲

二、组合变形：

两种或两种以上基本变形的组合。

- (1) 拉伸（压缩）和弯曲的组合；
- (2) 拉伸（压缩）和扭转的组合；
- (3) 弯曲和扭转的组合；
- (4) 弯曲和弯曲的组合；
- (5) 拉、弯、扭组合。







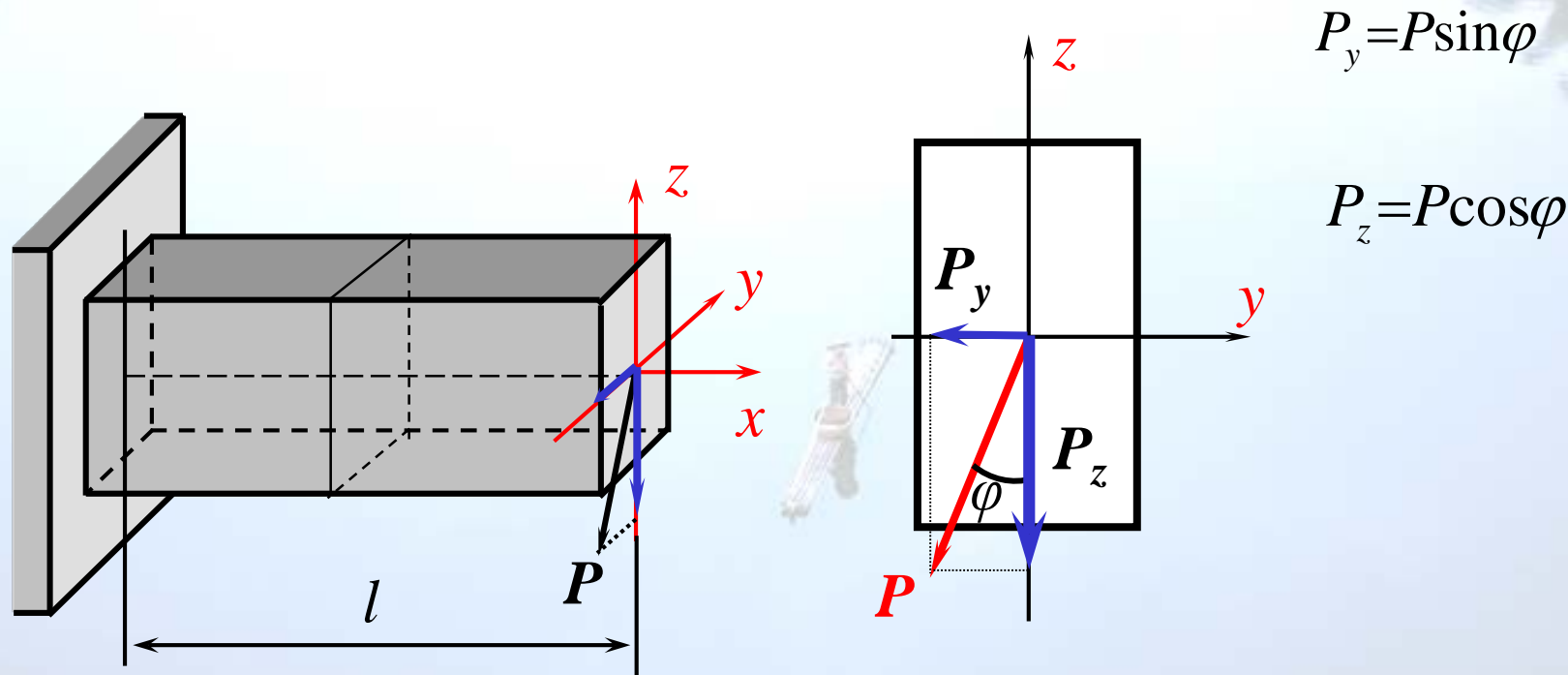
三、组合变形的研究方法 —— 叠加原理

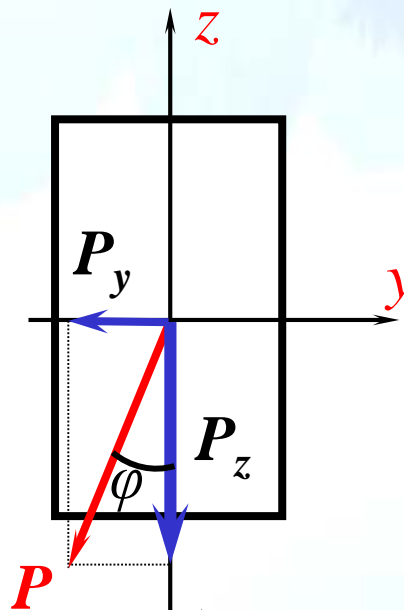
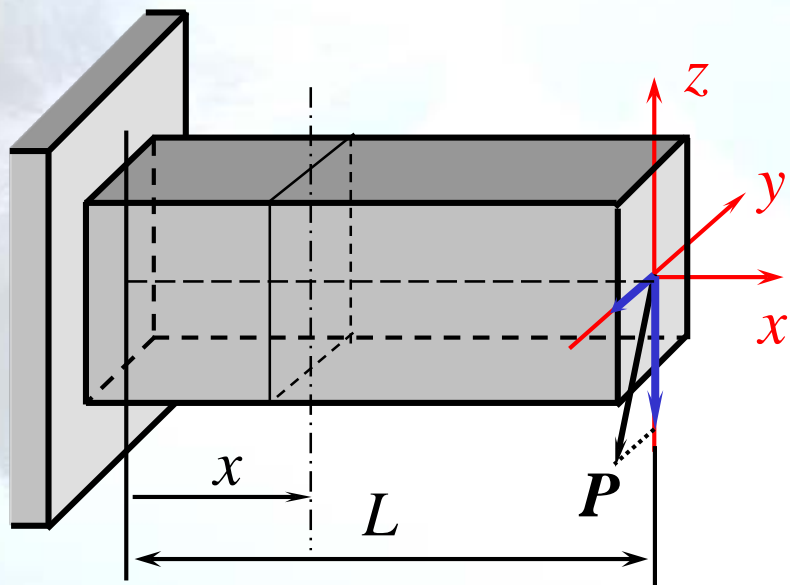
- ①外力分析：外力向形心简化并沿主惯性轴分解
- ②内力分析：求每个外力分量对应的内力方程和内力图，确定危险面。
- ③应力分析：画危险面应力分布图，叠加，建立危险点的强度条件。



§ 8-2 双对称轴梁非对称弯曲

1. 分解：将外载沿横截面的两个形心主轴分解，于是得到两个正交的平面弯曲。



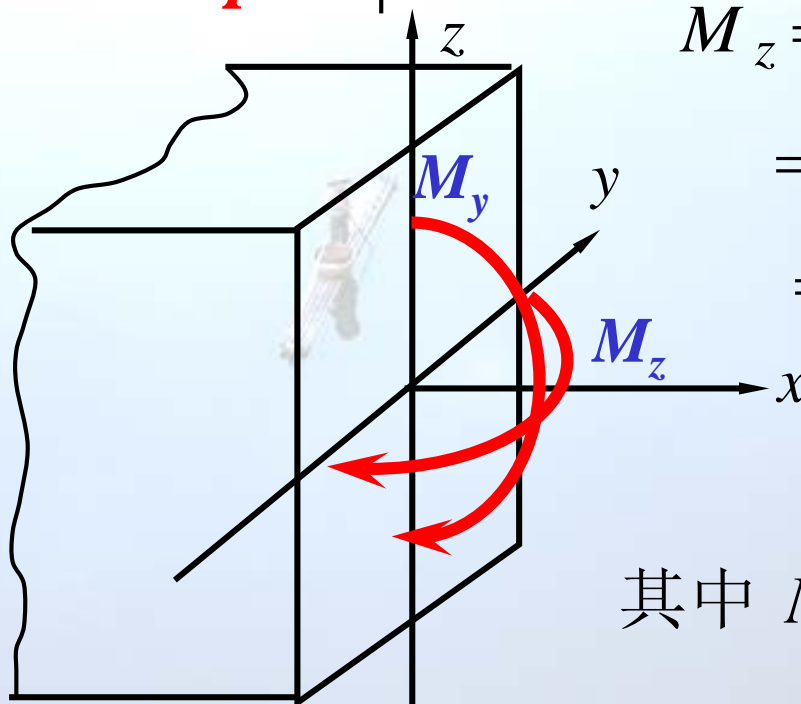
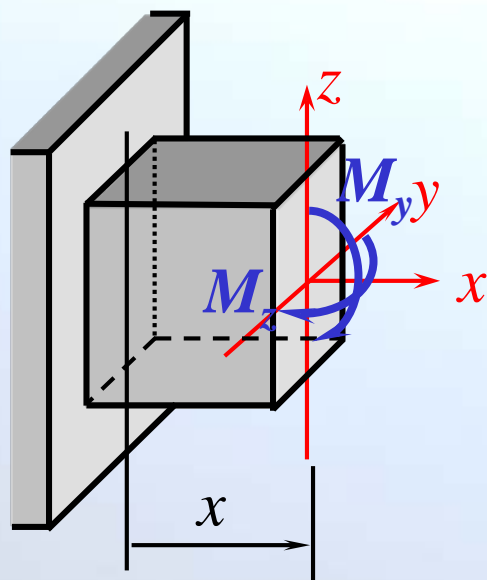


铅垂面内:

$$\begin{aligned} M_y &= P_z (l-x) \\ &= P \cos \varphi \cdot (l-x) \\ &= M \cos \varphi \end{aligned}$$

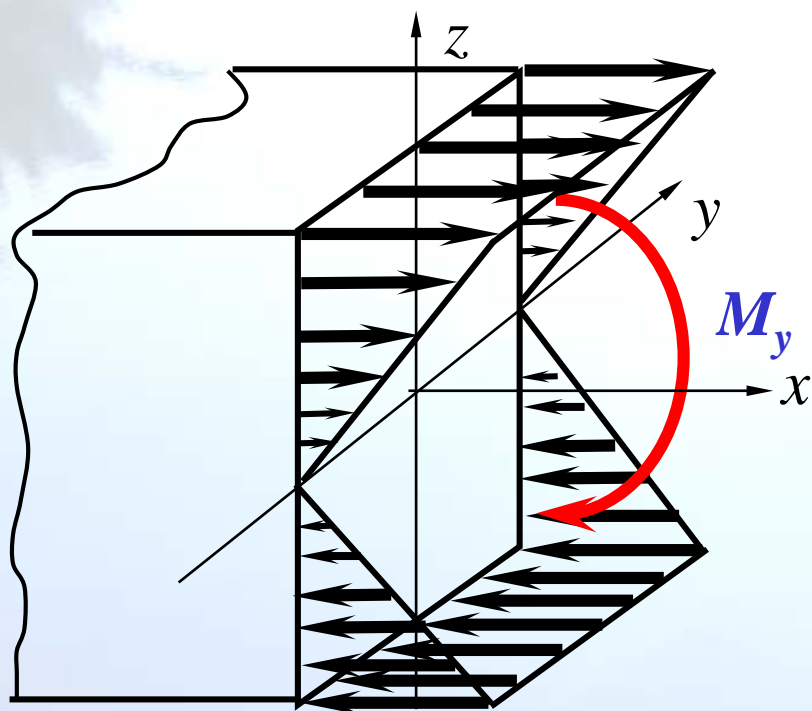
水平面内:

$$\begin{aligned} M_z &= P_y (l-x) \\ &= P \sin \varphi \cdot (l-x) \\ &= M \sin \varphi \end{aligned}$$

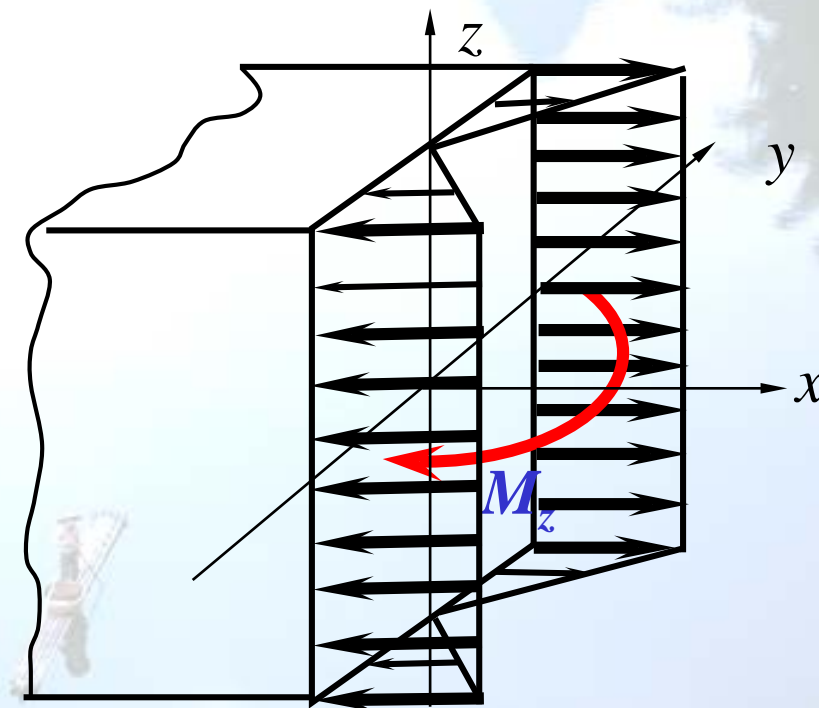


其中 $M = P(l-x)$

2. 叠加：对两个平面弯曲分别进行研究；然后将计算结果叠加起来。

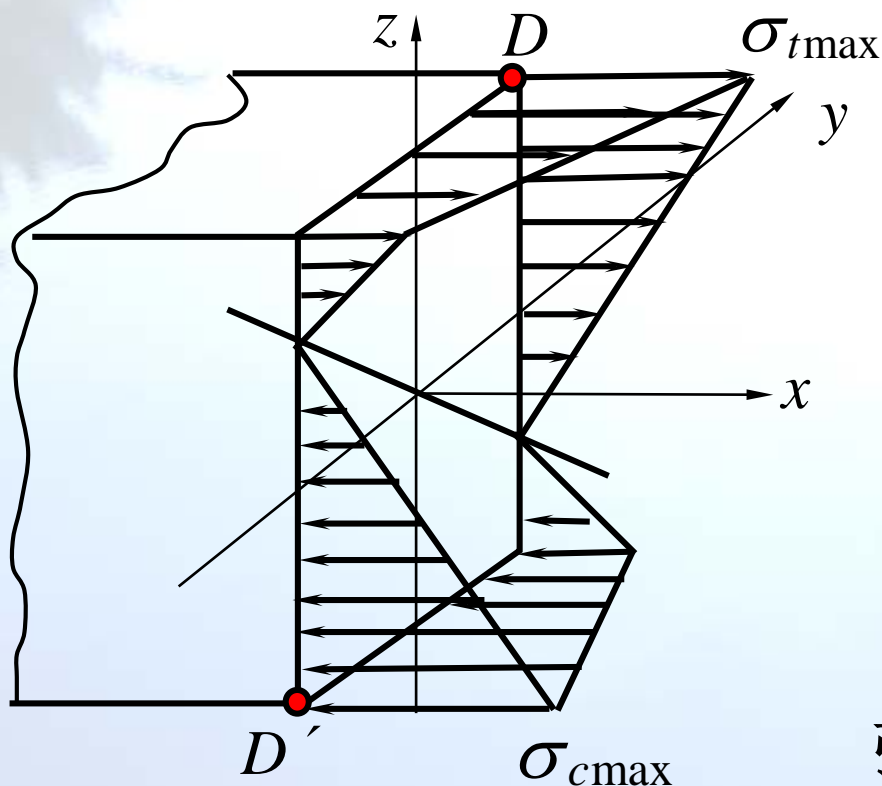


M_y 引起的应力: $\sigma' = \frac{M_y z}{I_y}$



M_z 引起的应力: $\sigma'' = \frac{M_z y}{I_z}$

$$\text{合应力: } \sigma = \sigma' + \sigma'' = \frac{M_y z}{I_y} + \frac{M_z y}{I_z}$$



$$\sigma_{\max} = \sigma'_{\max} + \sigma''_{\max}$$

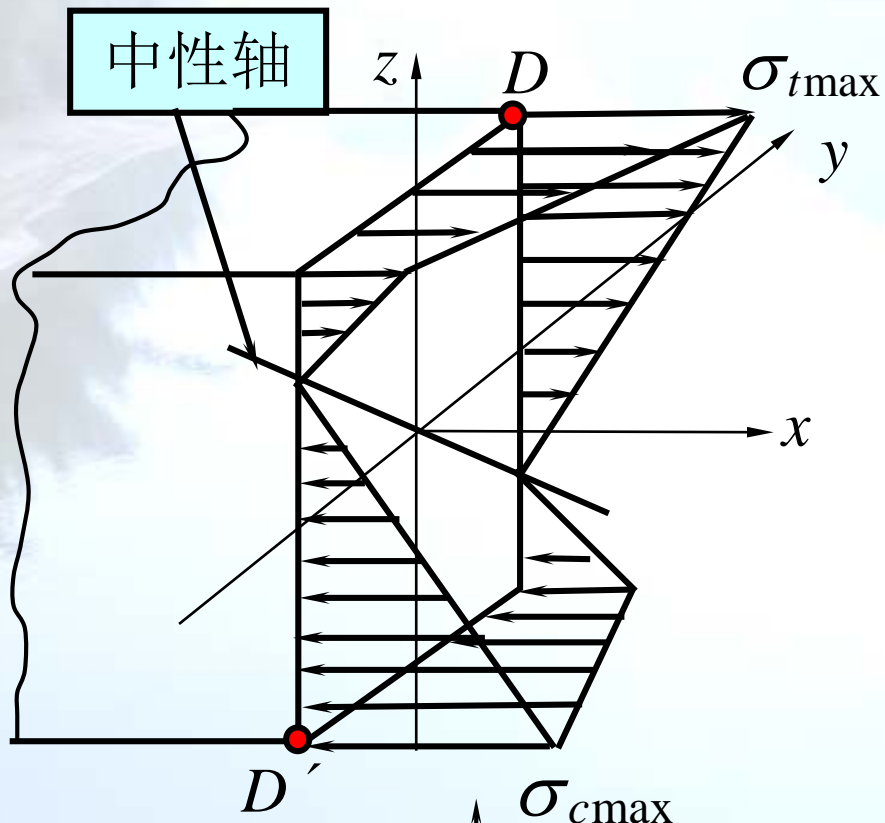
$$\therefore \sigma_{\max} = \frac{M_y}{W_y} + \frac{M_z}{W_z}$$

最大正应力在D和D' 点

强度条件:

危险截面在固定端:

$$\sigma_{\max} = \frac{M_y}{W_y} + \frac{M_z}{W_z} \leq [\sigma]$$




中性轴上的正应力为零:

$$\sigma=0$$

令合应力等于零:

$$\begin{aligned}\sigma &= \sigma' + \sigma'' = \frac{M_y z}{I_y} + \frac{M_z y}{I_z} \\ &= M \left(\frac{z}{I_y} \cos \varphi + \frac{y}{I_z} \sin \varphi \right) = 0\end{aligned}$$

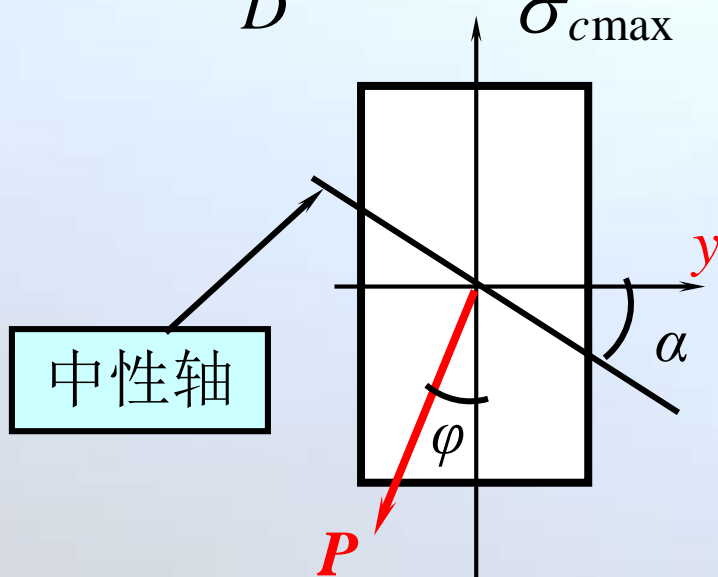
得中性轴方程:



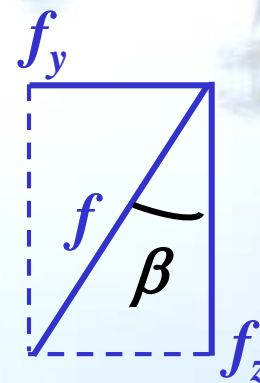
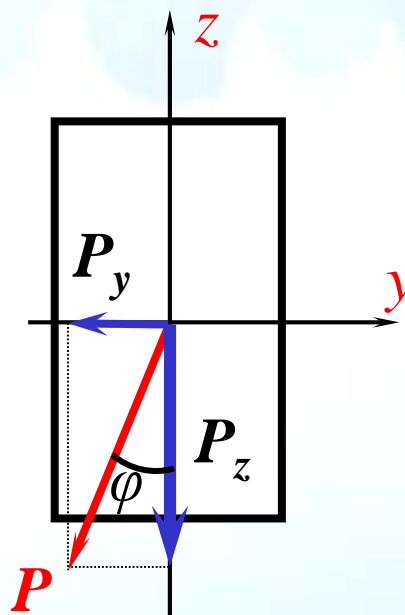
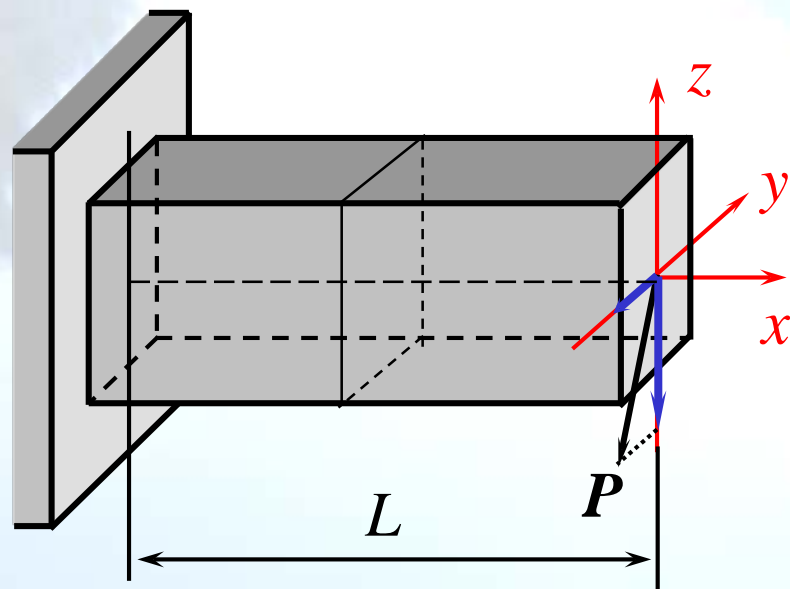
$$\frac{z}{I_y} \cos \varphi + \frac{y}{I_z} \sin \varphi = 0$$

$$\frac{z}{y} = -\frac{I_y}{I_z} \tan \varphi$$

$$\text{即: } \tan \alpha = -\frac{I_y}{I_z} \tan \varphi$$



变形计算



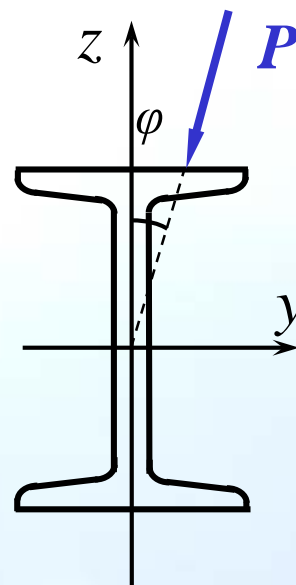
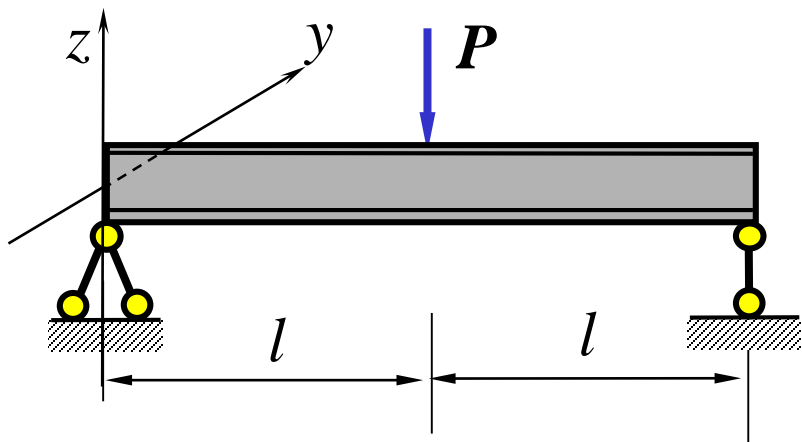
水平: $f_y = \frac{P_y L^3}{3EI_z}$

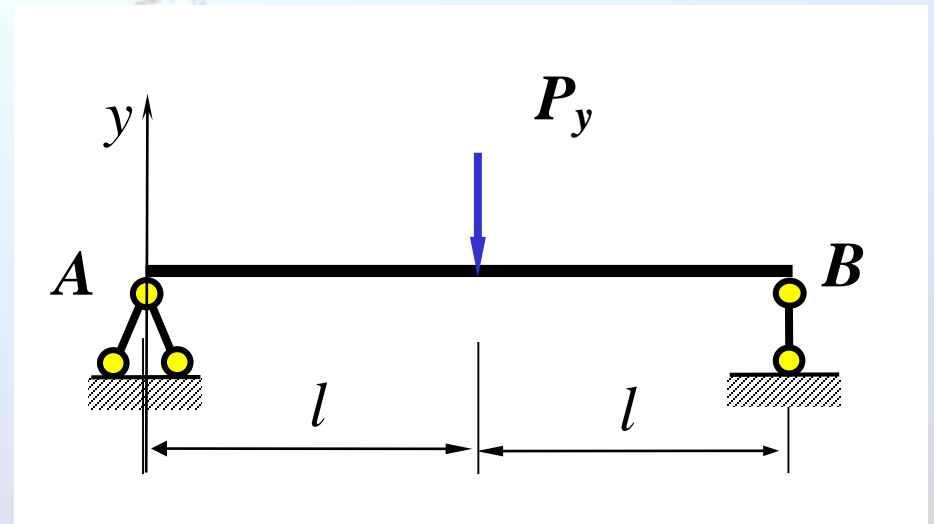
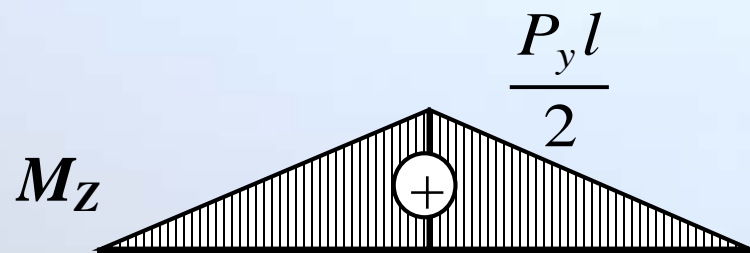
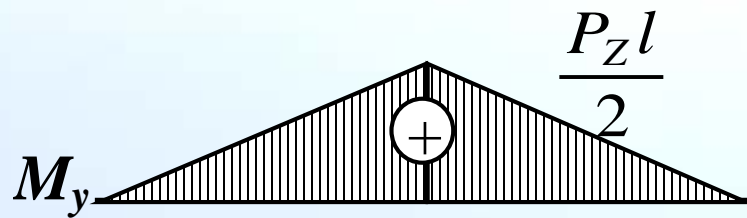
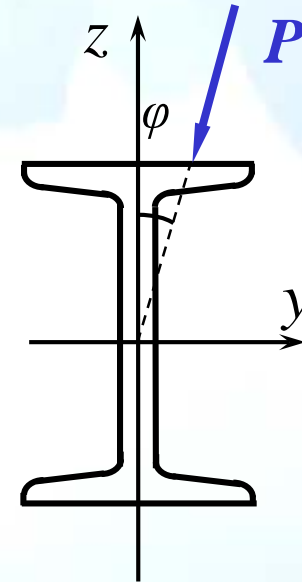
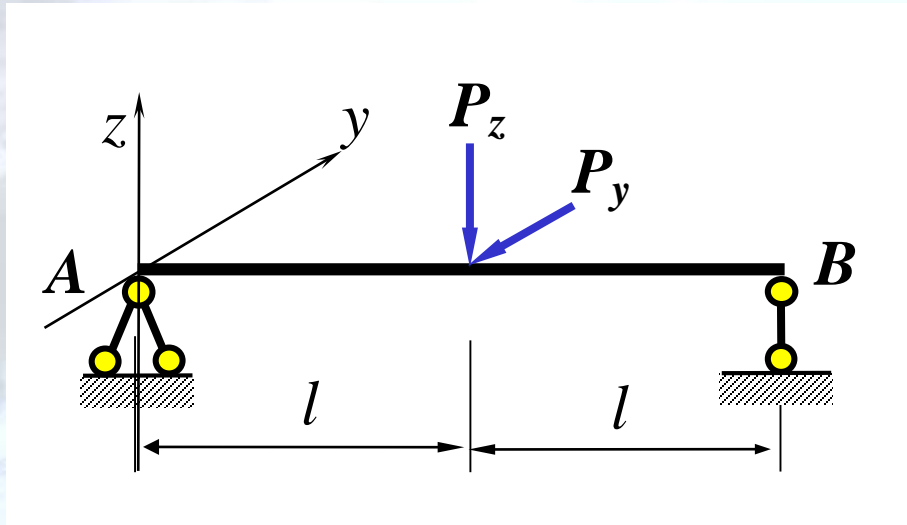
合位移: $f = \sqrt{f_y^2 + f_z^2} = \sqrt{\left(\frac{P_y L^3}{3EI_z}\right)^2 + \left(\frac{P_z L^3}{3EI_y}\right)^2}$

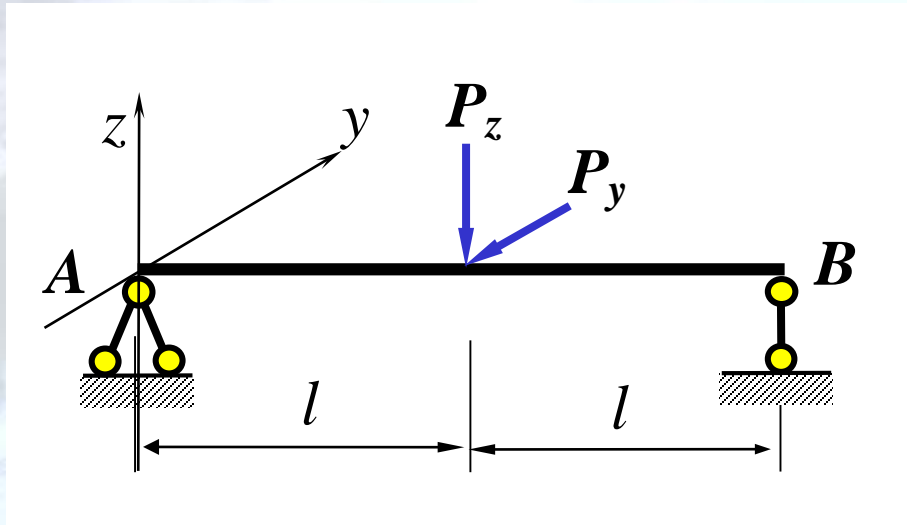
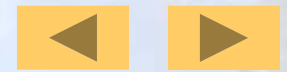
铅垂: $f_z = \frac{P_z L^3}{3EI_y}$

$\tan \beta = \frac{f_y}{f_z} = \frac{I_y}{I_z} \tan \varphi$, 当 $I_y = I_z$ 时, $\tan \beta = \tan \varphi$

[例1] 已知：32a工字钢， $l=2\text{m}$ ， $P=33\text{kN}$ ， $\varphi=15^\circ$ ， $[\sigma]=170\text{MPa}$ ，校核梁的强度。



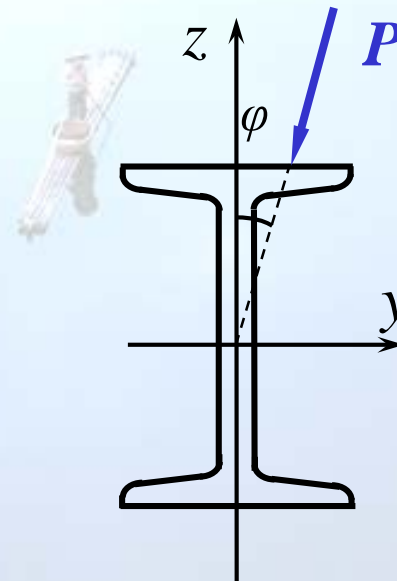
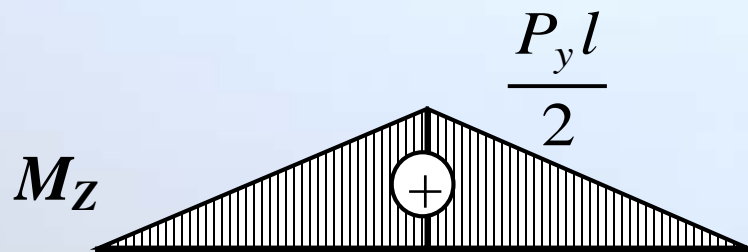
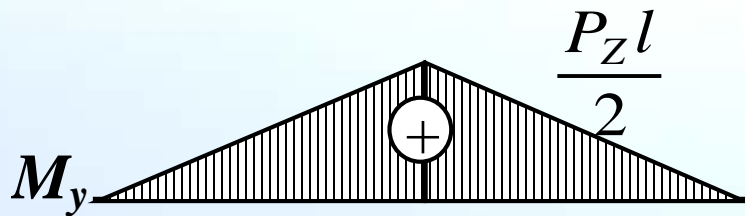


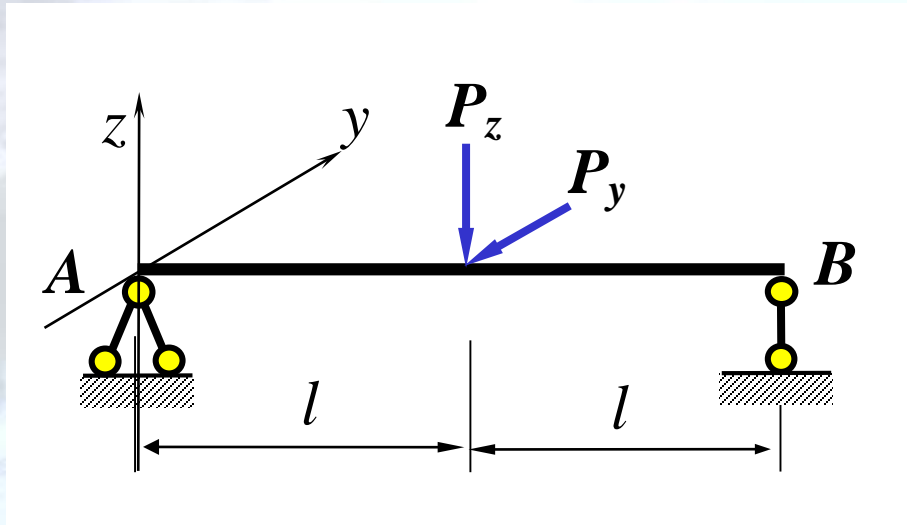


解： 危险截面在跨中

$$M_y = \frac{P_z}{2} \times l = 31.87 (\text{kN} \cdot \text{m})$$

$$M_z = \frac{P_y}{2} \times l = 8.54 (\text{kN} \cdot \text{m})$$





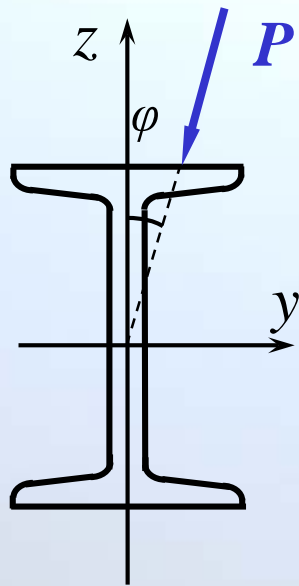
解:

$$M_y = \frac{P_z}{2} \times l = 31.87 (\text{kN} \cdot \text{m})$$

$$M_z = \frac{P_y}{2} \times l = 8.54 (\text{kN} \cdot \text{m})$$

查表得: $W_y = 692 (\text{cm}^3)$

$$W_z = 70.8 (\text{cm}^3)$$

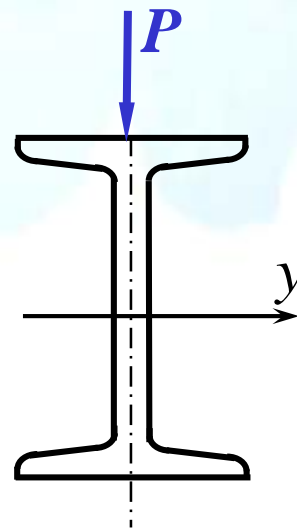
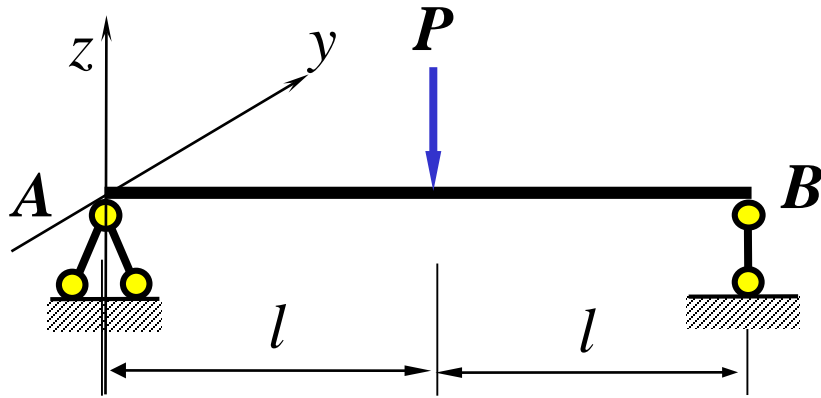


$$\therefore \sigma_{\max} = \frac{M_y}{W_y} + \frac{M_z}{W_z}$$

$$= \frac{31.87 \times 10^6}{692 \times 10^3} + \frac{8.54 \times 10^6}{70.8 \times 10^3}$$

$$= 46.1 + 120.6$$

$$= 166.7 (\text{MPa}) < [\sigma] \therefore \text{安全。}$$



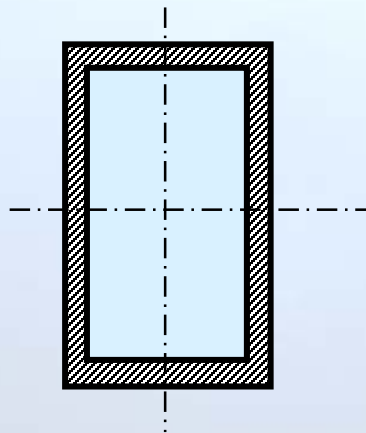
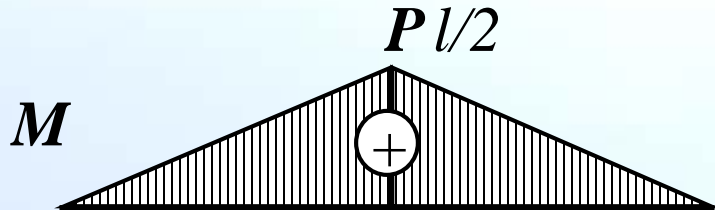
另：若 $\varphi=0^\circ$ ，求梁内最大正应力。

解： $M_{\max} = \frac{P}{2} \times l = 33(\text{kN}\cdot\text{m})$

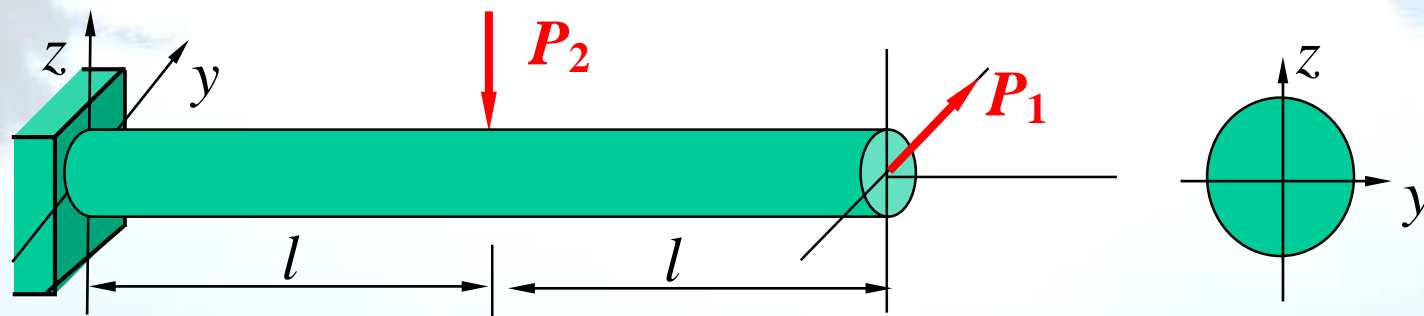
查表得： $W_y = 692(\text{cm}^3)$

$$\therefore \sigma_{\max} = \frac{M_{\max}}{W_y} = \frac{33 \times 10^6}{692 \times 10^3} = 47.7 \text{ (MPa)}$$

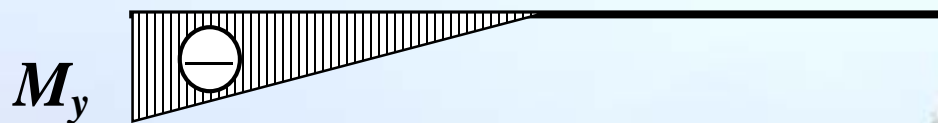
应力下降约3/4



[例2] 已知: $P_1=1.7\text{kN}$, $P_2=1.6\text{kN}$, $l=1\text{m}$, $[\sigma]=160\text{MPa}$,
试指出危险点的位置并设计圆截面杆的直径。



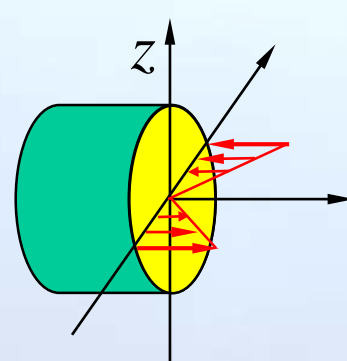
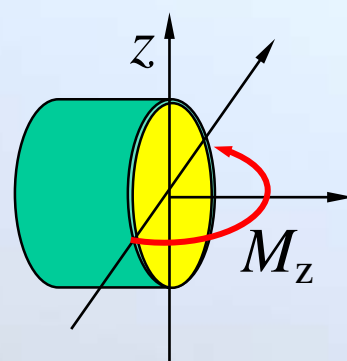
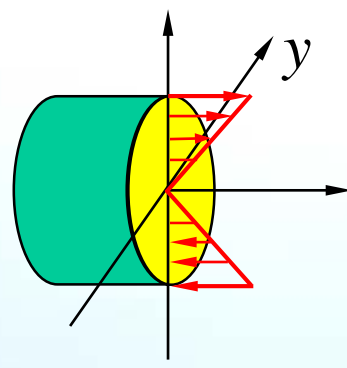
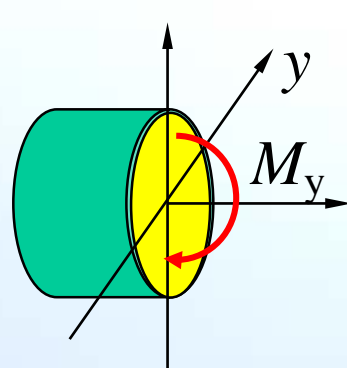
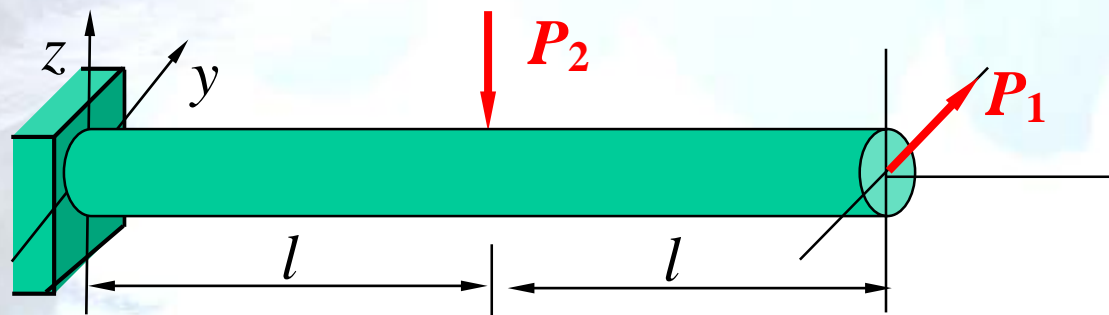
解: 危险截面在固定端



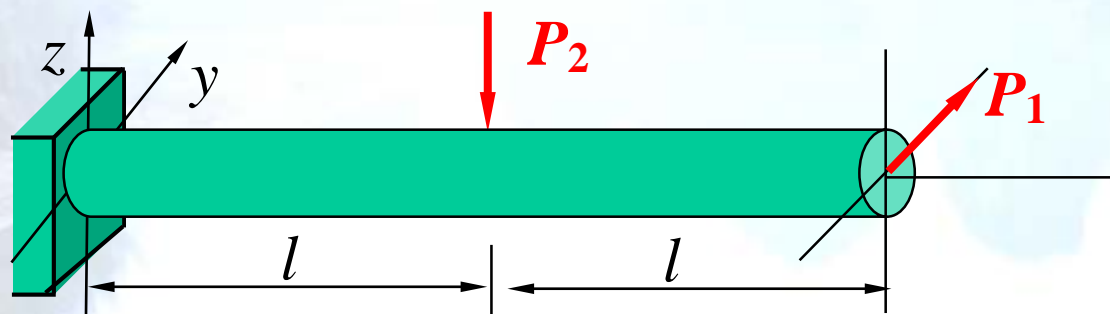
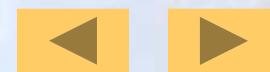
$$M_y = P_2 \times l = 1.6(\text{kN}\cdot\text{m})$$



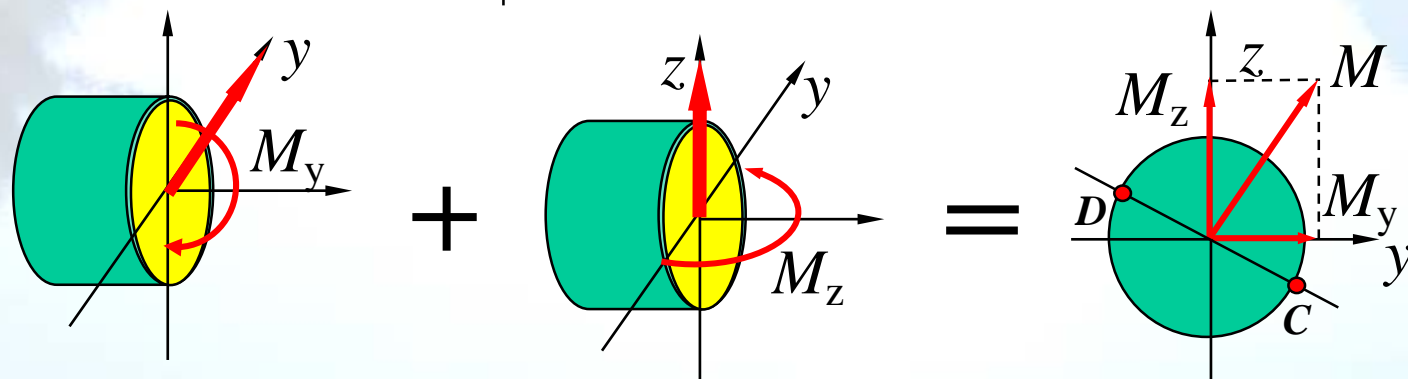
$$M_z = P_1 \times 2l = 3.4(\text{kN}\cdot\text{m})$$



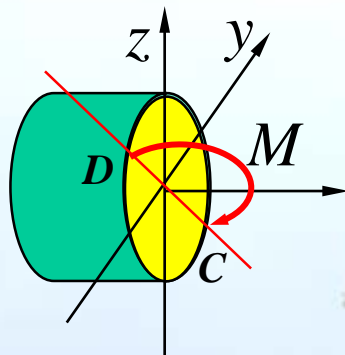
公式 $\sigma_{\max} = \frac{M_y}{W_y} + \frac{M_z}{W_z}$ 不能使用!



危险点在C、D两点



$$\begin{aligned} M &= \sqrt{M_y^2 + M_z^2} \\ &= \sqrt{1.6^2 + 3.4^2} \\ &= 3.76(\text{kN}\cdot\text{m}) \end{aligned}$$

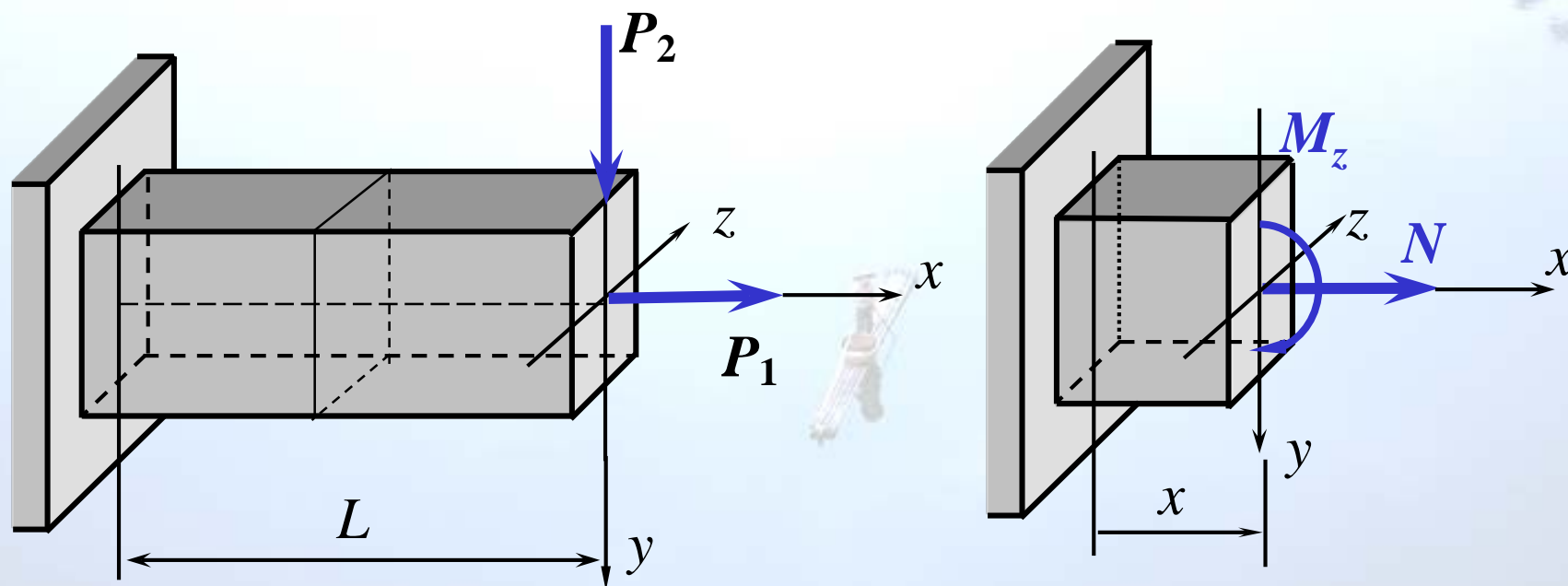


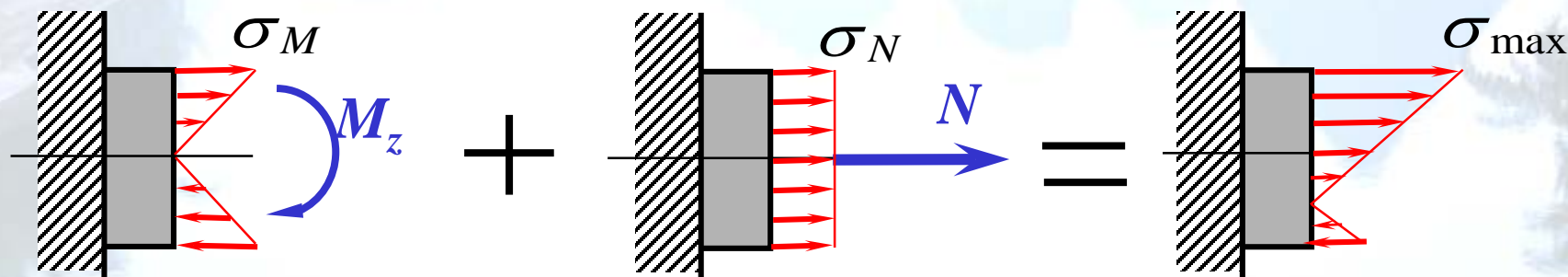
$$\sigma_{\max} = \frac{M}{W} = \frac{M}{\frac{\pi d^3}{32}} \leq [\sigma]$$

$$\begin{aligned} \therefore d &\geq \sqrt[3]{\frac{32M}{\pi[\sigma]}} \\ &= \sqrt[3]{\frac{32 \times 3.76 \times 10^6}{\pi \times 160}} \\ &= 62(\text{mm}) \end{aligned}$$

§ 8-3 拉伸(压缩)与弯曲的组合

一、拉(压)弯组合变形：杆件同时受横向力和轴向力的作用而产生的变形。





$$\sigma_{\max} = \sigma_M + \sigma_N$$

$$= \frac{M_z}{W_z} + \frac{P}{A}$$

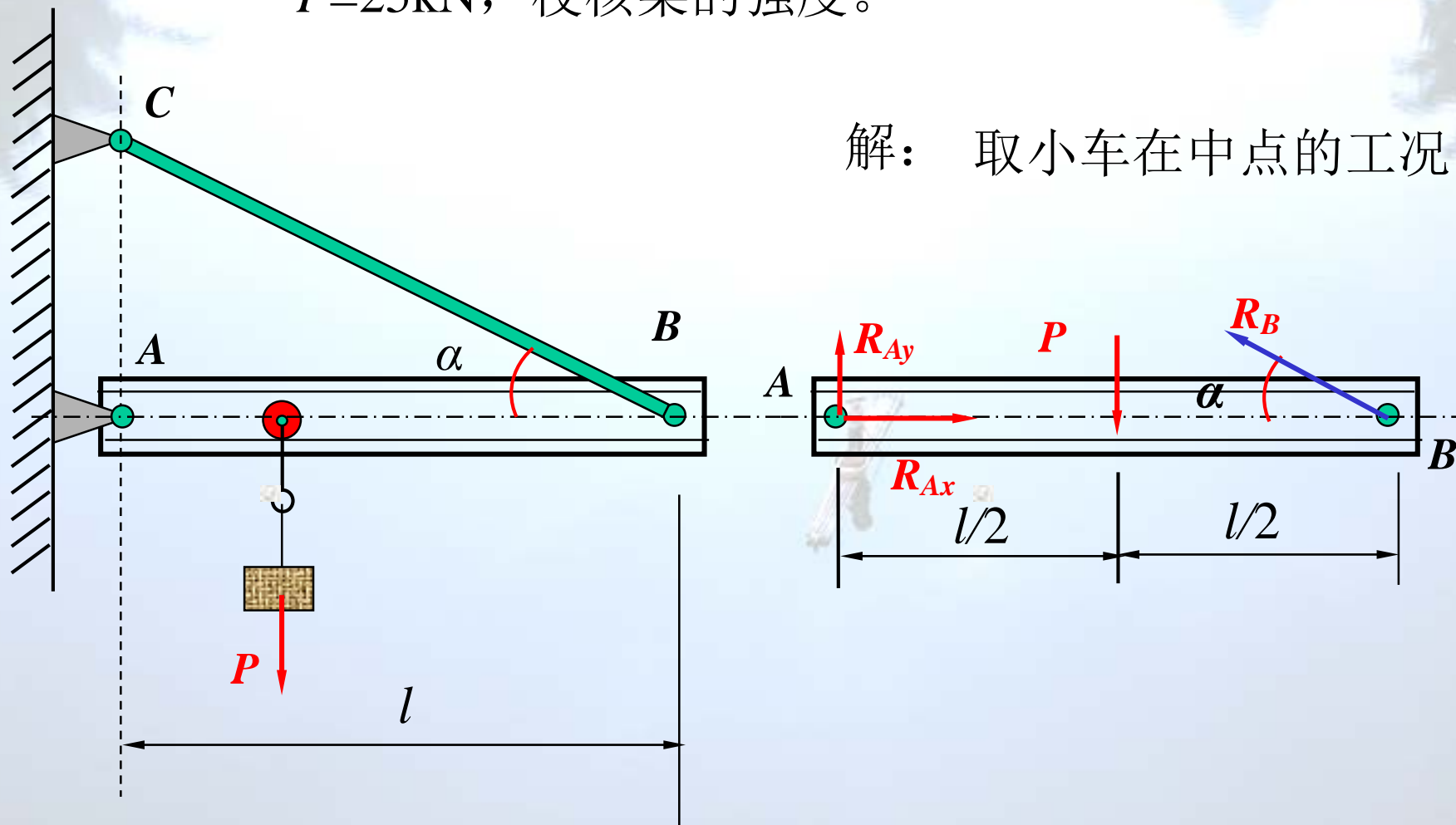
强度条件:

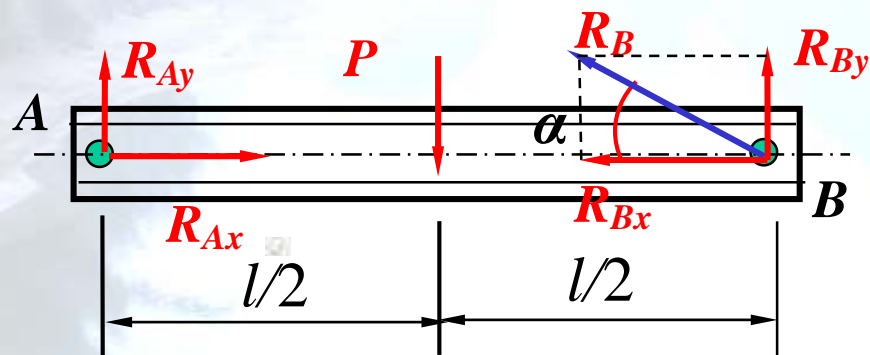
$$\sigma_{\max} = \frac{M_z}{W_z} + \frac{P}{A} \leq [\sigma]$$

[例3]

简易吊车， AB 梁为18号工字钢， $W=185\text{cm}^3$ ， $A=30.6\text{cm}^2$ ，梁长 $l=2.6\text{m}$ ， $\alpha=30^\circ$ ， $[\sigma]=120\text{MPa}$ ， $P=25\text{kN}$ ，校核梁的强度。

解： 取小车在中点的工况





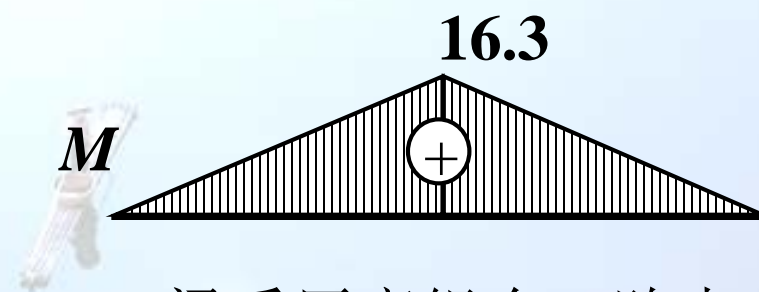
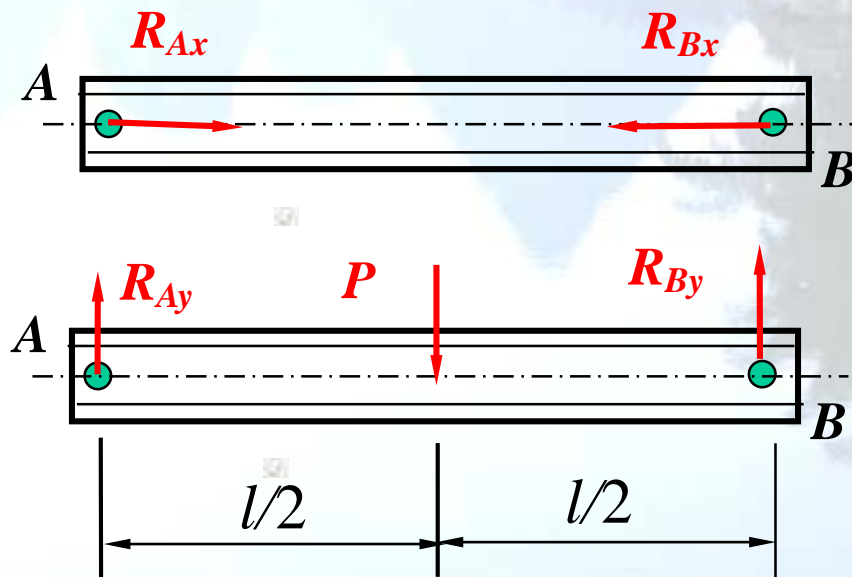
由理论力学得: $R_B = 25(\text{kN})$

$$R_{Ax} = 21.65(\text{kN})$$

$$R_{Ay} = \frac{P}{2} = 12.5(\text{kN})$$

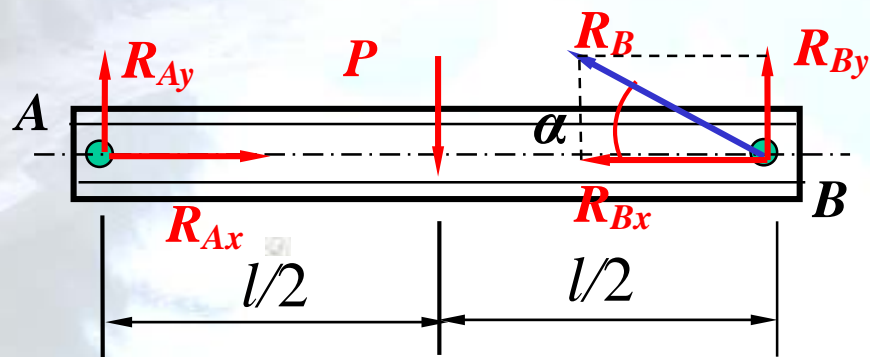
$$N = -R_{Ax} = -21.65(\text{kN})$$

$$M = R_{Ay} \cdot \frac{l}{2} = 16.3(\text{kN} \cdot \text{m})$$



AB梁受压弯组合，跨中为危险截面：

危险点在跨中上边缘，是压应力：

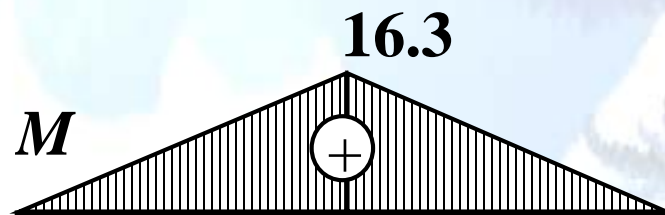


AB 梁受压弯组合，跨中为危险截面：

$$N = -R_{Ax} = -21.65(\text{kN})$$

$$M = R_{Ay} \cdot \frac{l}{2} = 16.3(\text{kN} \cdot \text{m})$$

危险点在跨中上边缘，是压应力：



$$\begin{aligned} \therefore \sigma_{\max}^c &= \frac{|N|}{A} + \frac{M}{W} \\ &= \frac{21.65 \times 10^3}{30.6 \times 10^2} + \frac{16.3 \times 10^6}{185 \times 10^3} \\ &= 7.09 + 88.1 \\ &= 95.2(\text{MPa}) < [\sigma] \\ &\therefore \text{安全!} \end{aligned}$$

当小车在B点时:

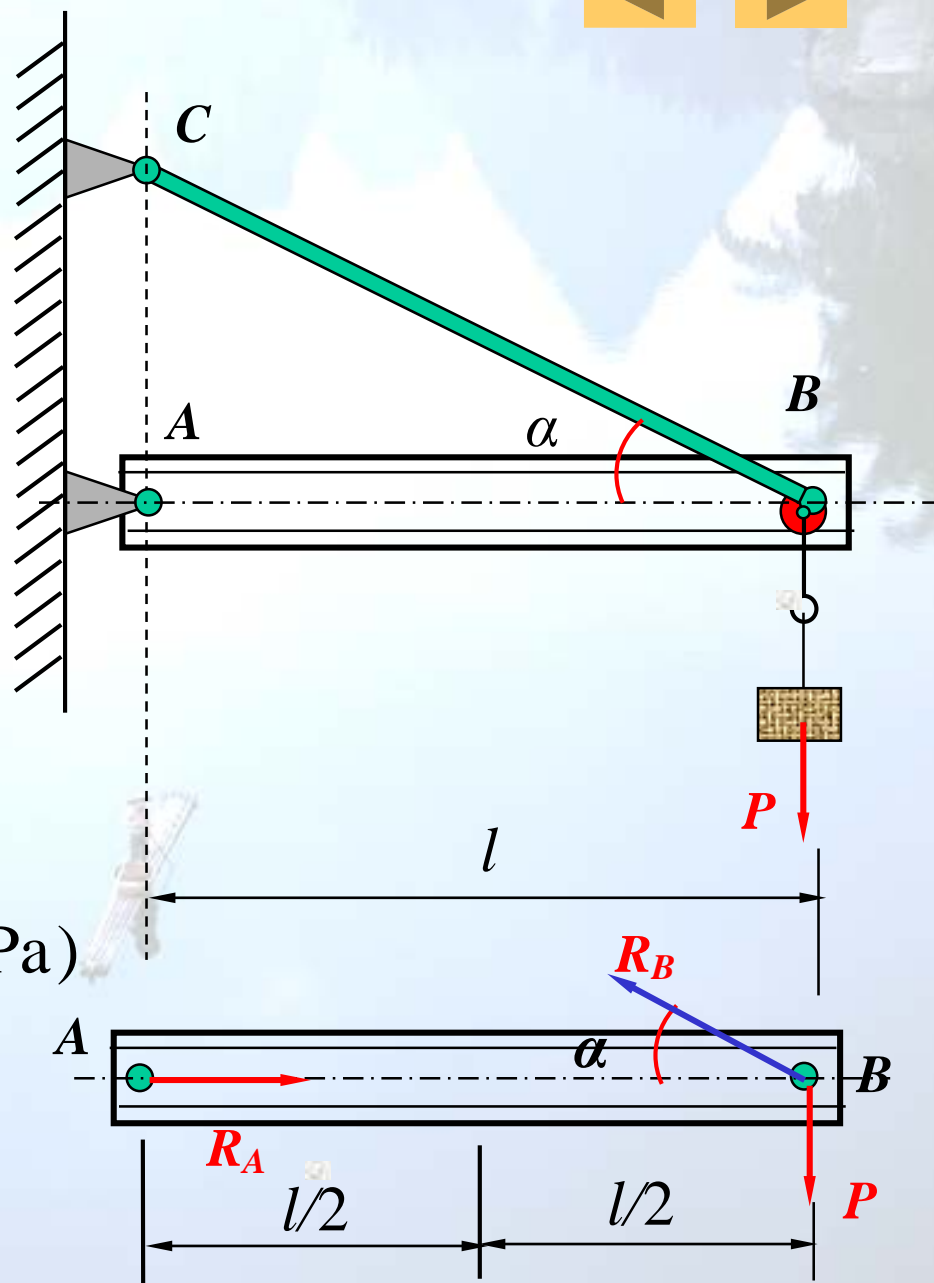
$$R_B = 50(\text{kN})$$

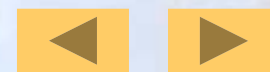
$$R_A = 43.3(\text{kN})$$

AB梁受轴向压缩:

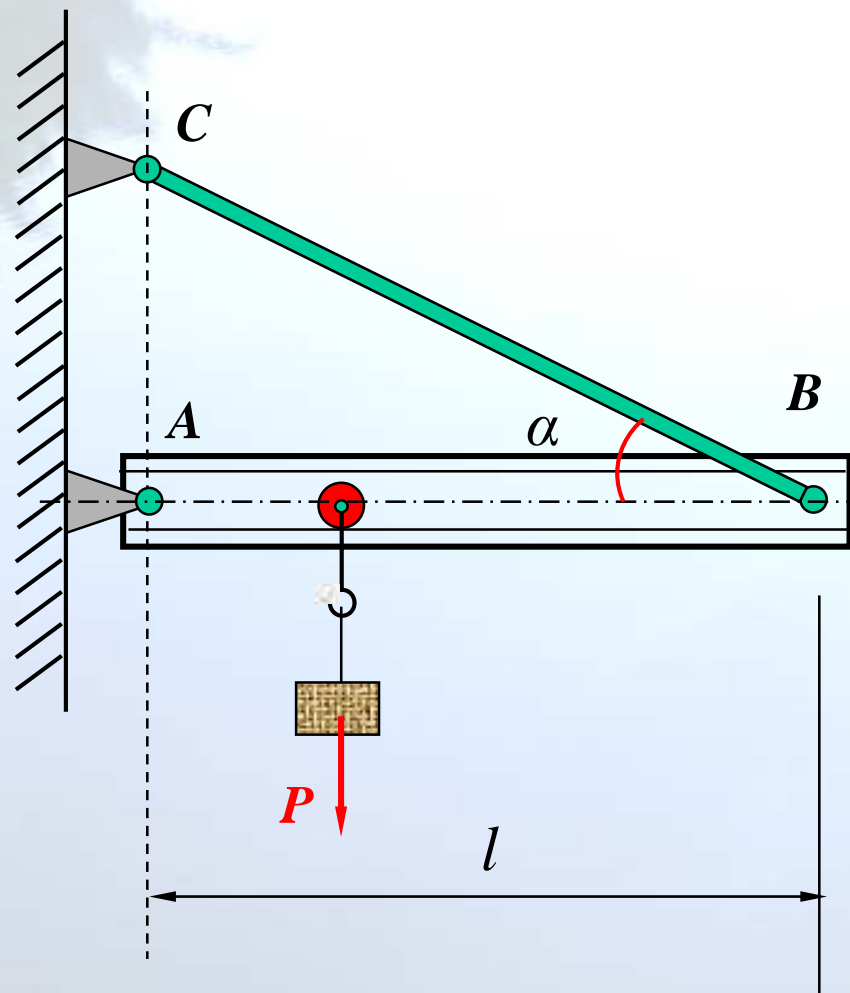
$$N = -R_A = -43.3(\text{kN})$$

$$\therefore \sigma = \frac{N}{A} = \frac{43.3 \times 10^3}{30.6 \times 10^2} = 14.1(\text{MPa})$$

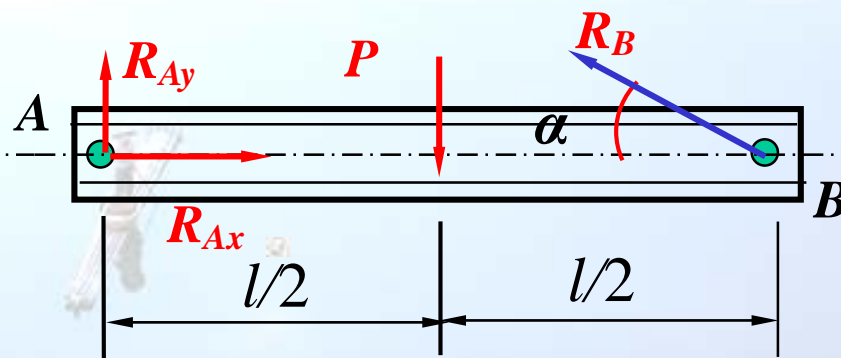


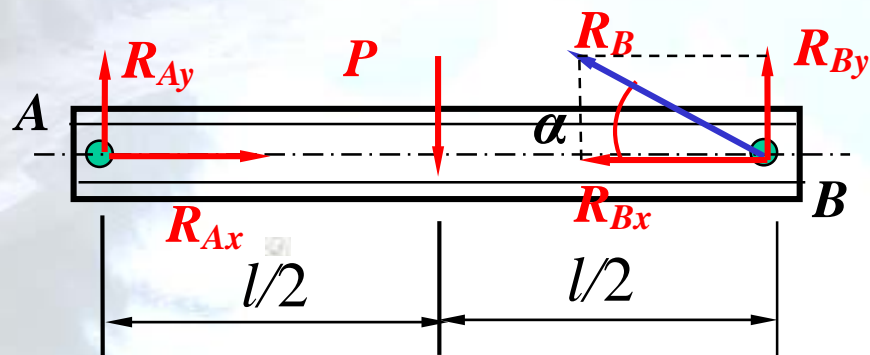


[例4] 简易吊车，梁长 $l=2.6\text{m}$ ， $\alpha=30^\circ$ ， $[\sigma]=120\text{MPa}$ ， $P=50\text{kN}$ ，试选择工字钢型号。



解： 取小车在中点的工况





$$R_B = 50(\text{kN})$$

$$R_{Ax} = 43.3(\text{kN})$$

$$R_{Ay} = \frac{P}{2} = 25(\text{kN})$$

AB梁受压弯组合，跨中为危险截面：

$$N = -R_{Ax} = -43.3(\text{kN})$$

$$M = R_{Ay} \cdot \frac{l}{2} = 32.5(\text{kN} \cdot \text{m})$$

由弯曲强度进行试算：

$$\sigma_{\max} = \frac{M}{W} \leq [\sigma]$$

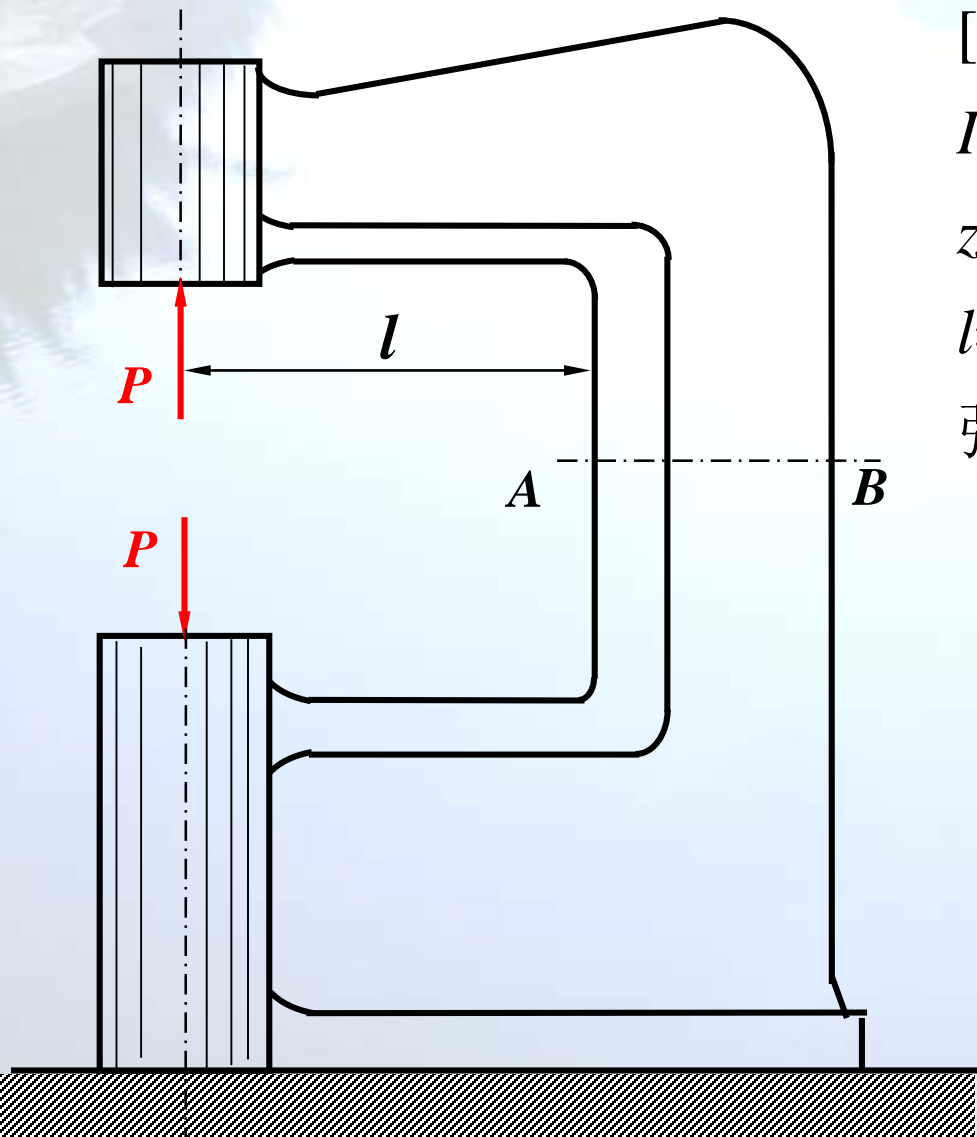
$$W \geq \frac{M}{[\sigma]} = \frac{32.5 \times 10^6}{120} \\ = 270 \times 10^3 (\text{mm}^3)$$

∴ 选22a工字钢， $W = 309 \text{cm}^3$

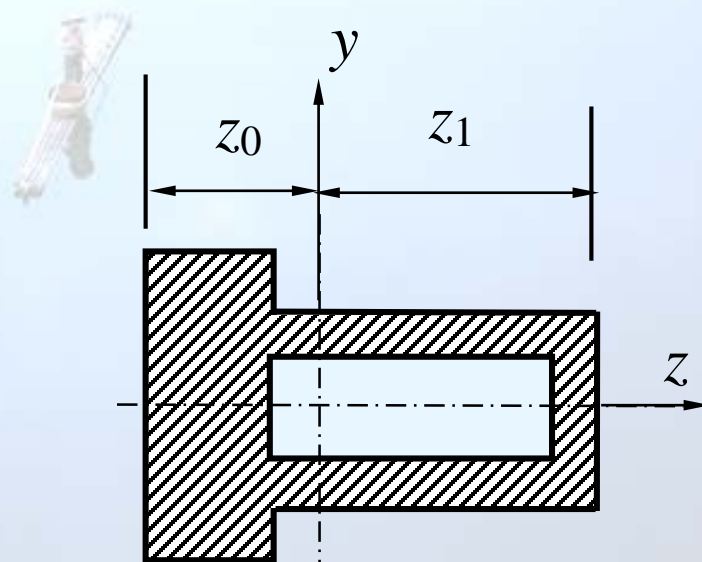
$$\therefore \sigma_{\max}^c = \frac{|N|}{A} + \frac{M}{W} \\ = \frac{43.3 \times 10^3}{42.128 \times 10^2} + \frac{32.5 \times 10^6}{309 \times 10^3} \\ = 115.5(\text{MPa}) < [\sigma]$$

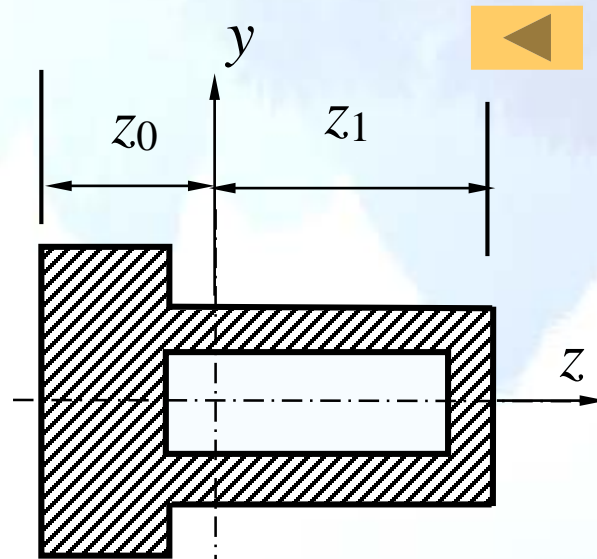
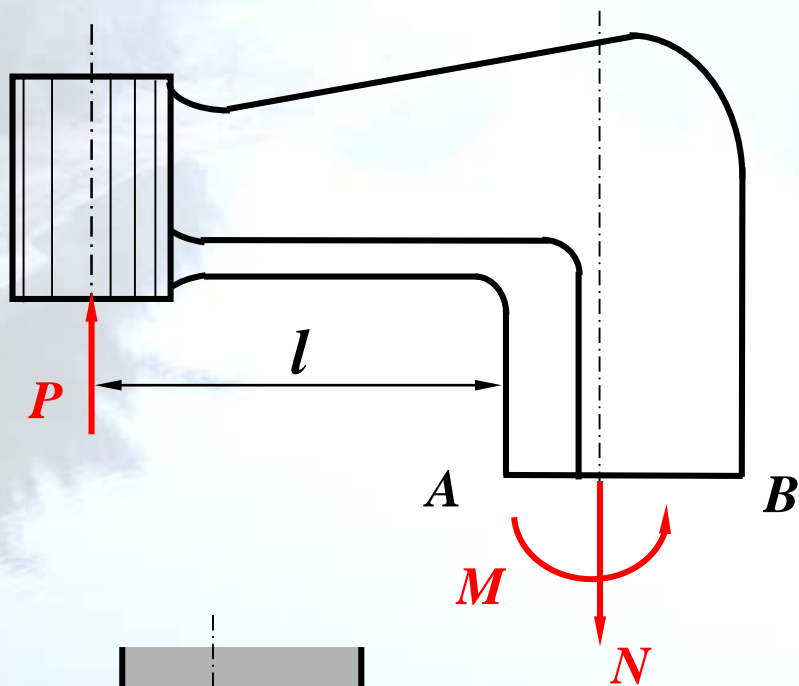
∴ 可以选22a工字钢！

[例4]



已知：冲压机，铸铁机身，
 $[\sigma_t]=30\text{MPa}$ ， $[\sigma_c]=160\text{MPa}$ ，
 $I_y=5310\text{cm}^4$ ， $A=150\text{cm}^2$ ，
 $z_0=7.5\text{cm}$ ， $z_1=12.5\text{cm}$ ，
 $l=35\text{cm}$ ， $P=40\text{kN}$ ，校核立柱
强度。





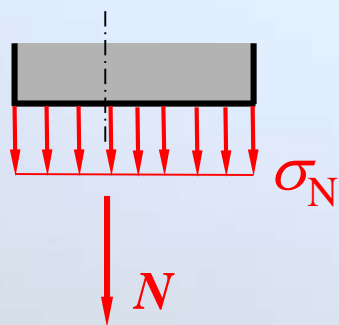
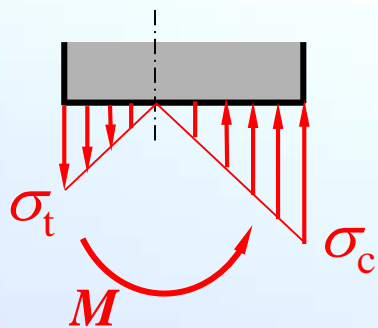
解: $N = P = 40(\text{kN})$

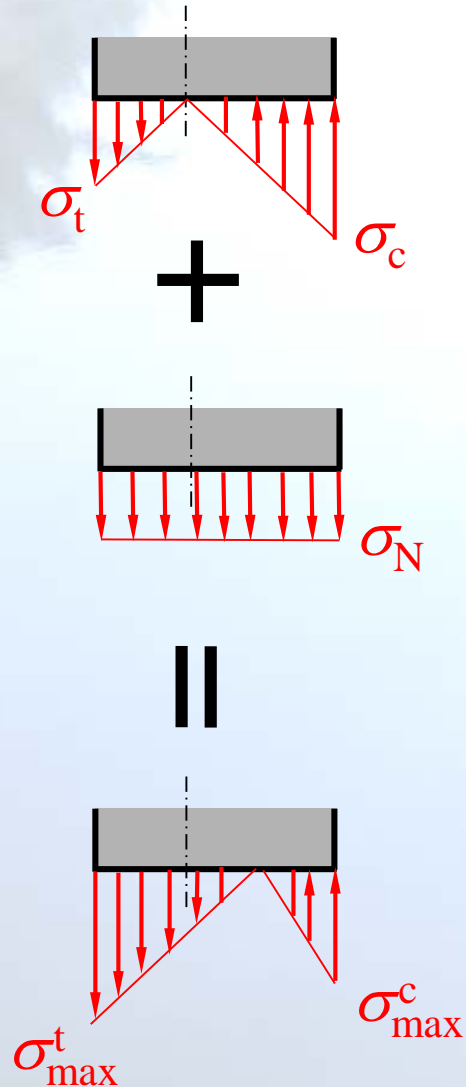
$$M = P \cdot (l + z_0) = 17(\text{kN} \cdot \text{m})$$

$$\sigma_N = \frac{N}{A} = \frac{40 \times 10^3}{150 \times 10^2} = 2.67(\text{MPa})$$

$$\sigma_t = \frac{M \cdot z_0}{I_y} = \frac{17 \times 10^6 \times 75}{5310 \times 10^4} = 24(\text{MPa})$$

$$\sigma_c = \frac{M \cdot z_1}{I_y} = \frac{17 \times 10^6 \times 125}{5310 \times 10^4} = 40(\text{MPa})$$



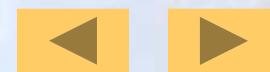


$$\begin{aligned}\sigma_{\max}^t &= \sigma_t + \sigma_N = 24 + 2.67 \\ &= 26.7(\text{MPa}) < [\sigma_t]\end{aligned}$$

$$\begin{aligned}\sigma_{\max}^c &= \sigma_c - \sigma_N = 40 - 2.67 \\ &= 37.3(\text{MPa}) < [\sigma_c]\end{aligned}$$

∴ 该立柱安全!

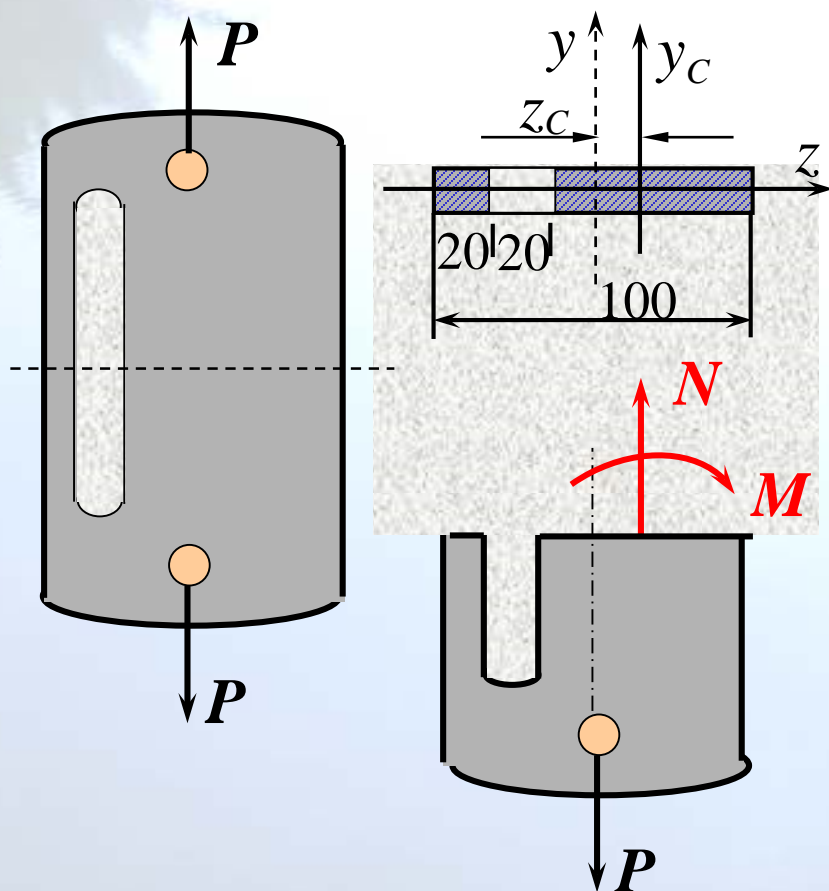




[例5] 图示钢板，厚度 $t=10\text{mm}$ ，受力 $P=100\text{kN}$ ，试求最大正应力；若将缺口移至板宽的中央，则最大正应力为多少？

解：内力分析如图

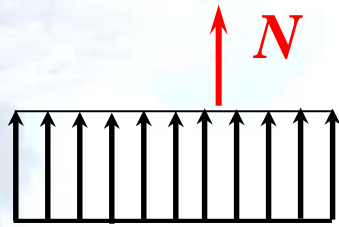
坐标如图，形心位置



$$z_c = \frac{20 \times 10 \times 20}{100 \times 10 - 20 \times 10} = 5\text{mm}$$

$$\begin{aligned} I_{y_c} &= \frac{10 \times 100^3}{12} + 10 \times 100 \times 5^2 \\ &\quad - \left[\frac{10 \times 20^3}{12} + 10 \times 20 \times 25^2 \right] \\ &= 7.27 \times 10^5 \text{ mm}^4 \end{aligned}$$

$$M = P \cdot z_c = 500\text{N} \cdot \text{m}$$



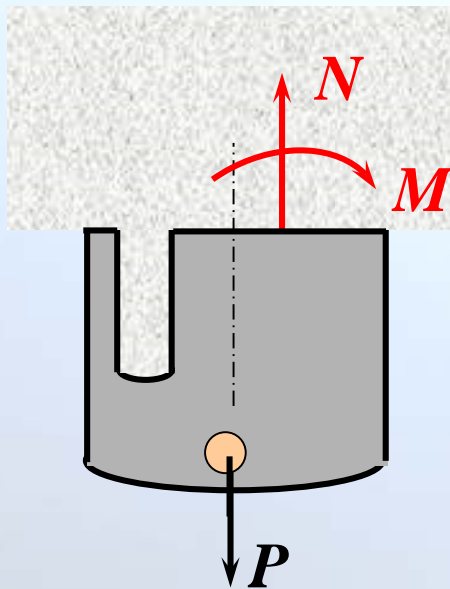
应力分析如图

$$\sigma_{\max}^t = \frac{N}{A} + \frac{M|z|_{\max}}{I_{yc}}$$



$$= \frac{100 \times 10^3}{800} + \frac{500 \times 10^3 \times 55}{7.27 \times 10^5}$$

$$= 125 + 37.8 = 162.8 \text{ MPa}$$

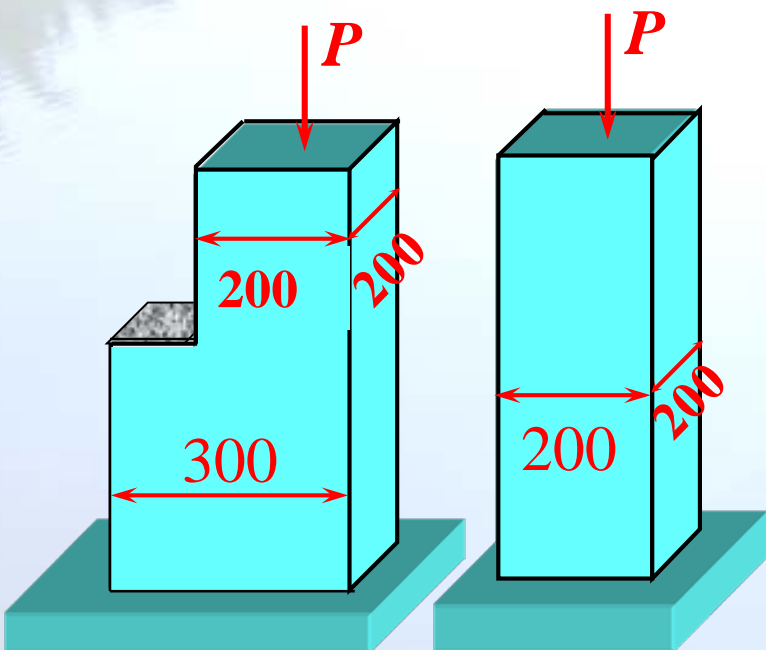


孔移至板中间时

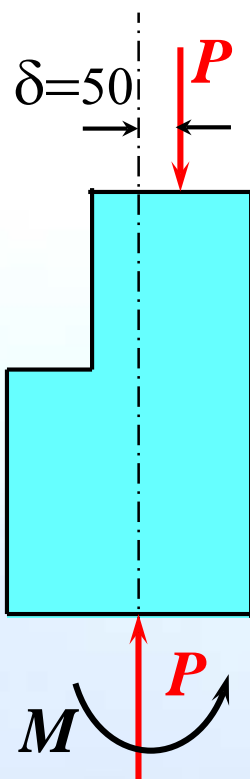
$$\sigma_{\max} = \frac{N}{A} = \frac{100 \times 10^3}{800} = 125 \text{ (MPa)}$$

[例6] 图示不等截面与等截面杆，受力 $P=350\text{kN}$ ，试分别求出两柱内的最大正应力(绝对值)。

解：图（1）



图（1）



图（2）

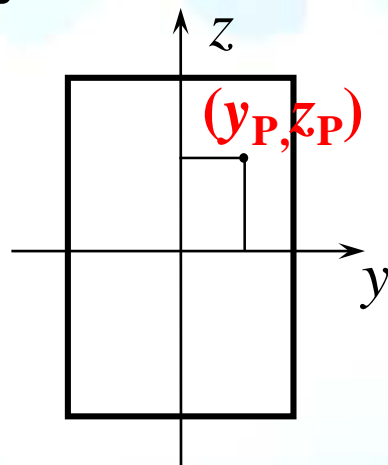
$$\begin{aligned}\sigma_{1\max} &= \frac{P}{A_1} + \frac{M}{W_{z1}} \\ &= \frac{350 \times 10^3}{0.2 \times 0.3} + \frac{350 \times 10^3 \times 0.05 \times 6}{0.2 \times 0.3^2} \\ &= 11.7 \text{ MPa}\end{aligned}$$

图（2）

$$\sigma_{2\max} = \frac{P}{A} = \frac{350000}{0.2 \times 0.2} = 8.75 \text{ MPa}$$

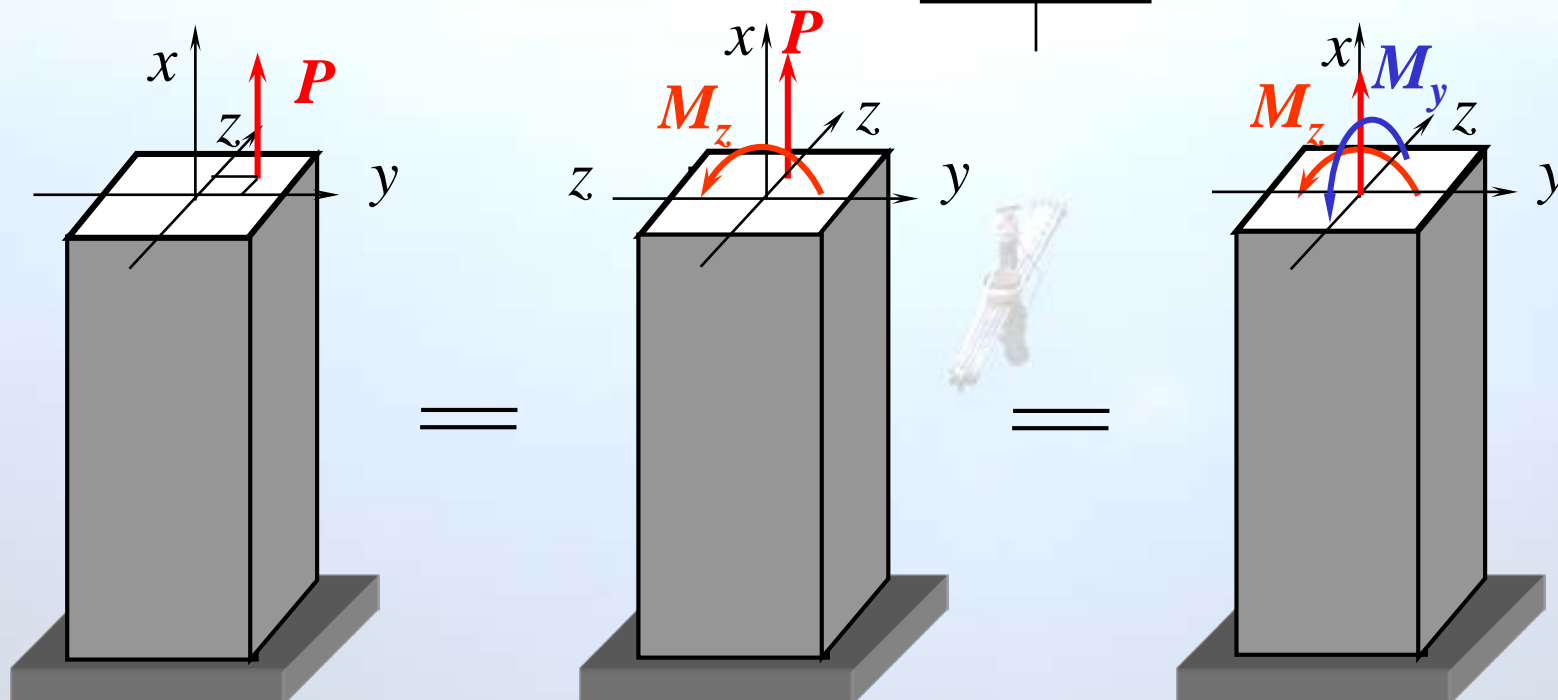
§ 8-4 偏心拉（压）· 截面核心

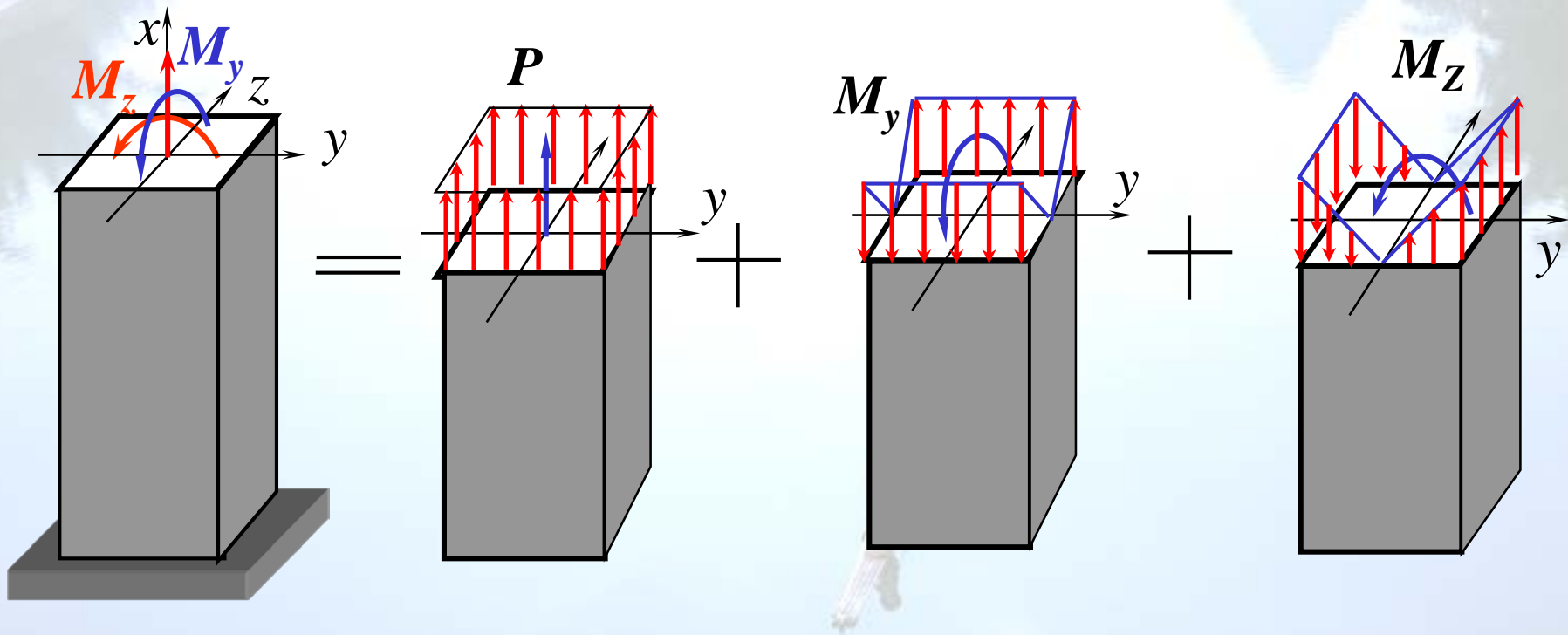
一、偏心拉（压）



$$M_z = P \cdot y_P$$

$$M_y = P \cdot z_P$$

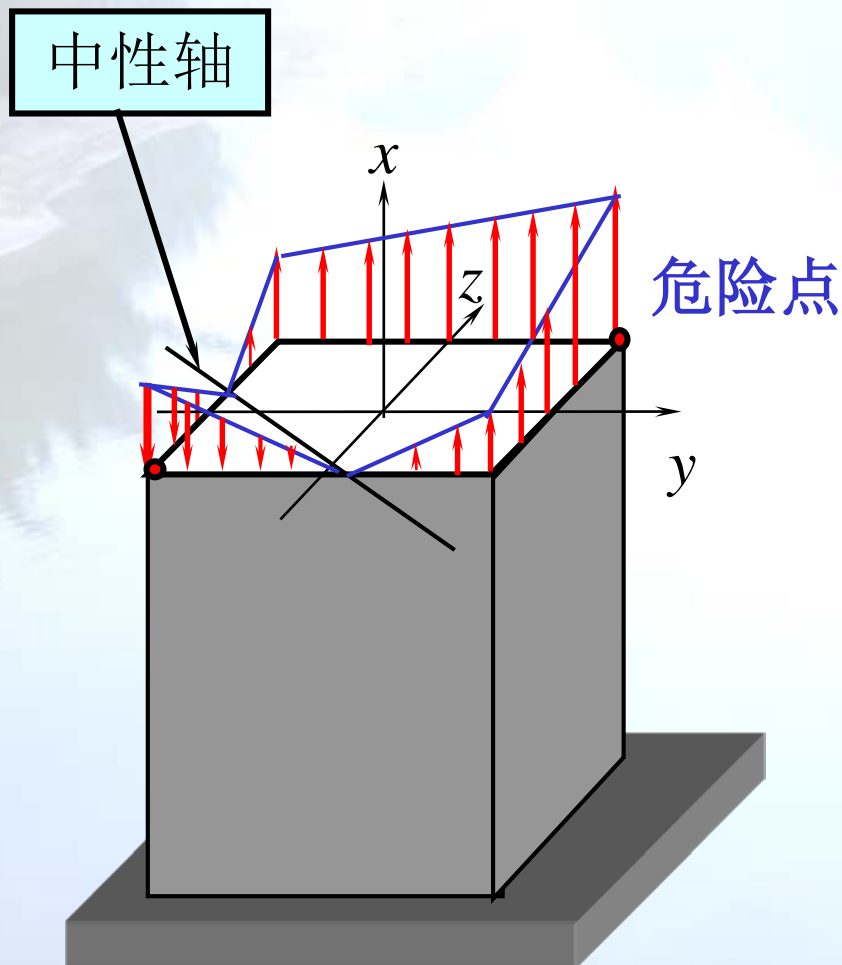




$$\sigma_N = \frac{P}{A}$$

$$\sigma_{M_y} = \frac{M_y z}{I_y}$$

$$\sigma_{M_z} = \frac{M_z y}{I_z}$$



$$\sigma = \frac{P}{A} + \frac{M_z y}{I_z} + \frac{M_y z}{I_y}$$

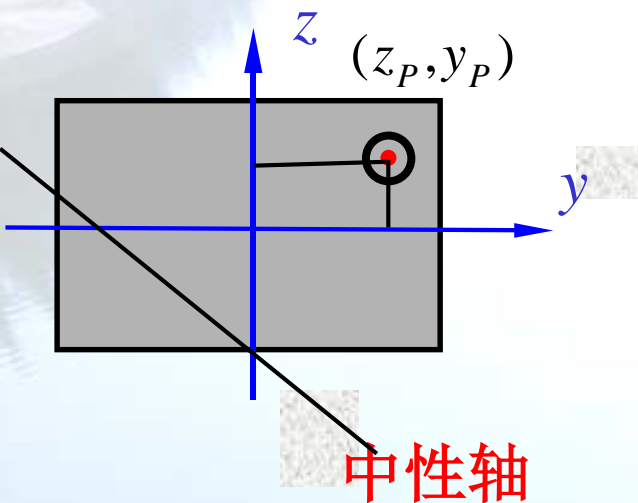
$$\sigma_{t\max} = \frac{P}{A} + \frac{M_z}{W_z} + \frac{M_y}{W_y}$$

$$\sigma_{c\max} = -\frac{P}{A} + \frac{M_z}{W_z} + \frac{M_y}{W_y}$$

强度条件:

$$\sigma_{\max} = \frac{P}{A} + \frac{M_z}{W_z} + \frac{M_y}{W_y} \leq [\sigma]$$

二、中性轴方程



$$\text{令: } \sigma_x = \frac{P}{A} + \frac{M_z y_0}{I_z} + \frac{M_y z_0}{I_y} = 0$$

$$\frac{P}{A} + \frac{P y_P y_0}{A i_z^2} + \frac{P z_P z_0}{A i_y^2} = \frac{P}{A} \left(1 + \frac{y_P y_0}{i_z^2} + \frac{z_P z_0}{i_y^2} \right) = 0$$

$$1 + \frac{y_P y_0}{i_z^2} + \frac{z_P z_0}{i_y^2} = 0$$

中性轴在y和z轴上的截距 a_y , a_z :

$$\text{令 } z_0 = 0, \quad 1 + \frac{y_P a_y}{i_z^2} = 0,$$

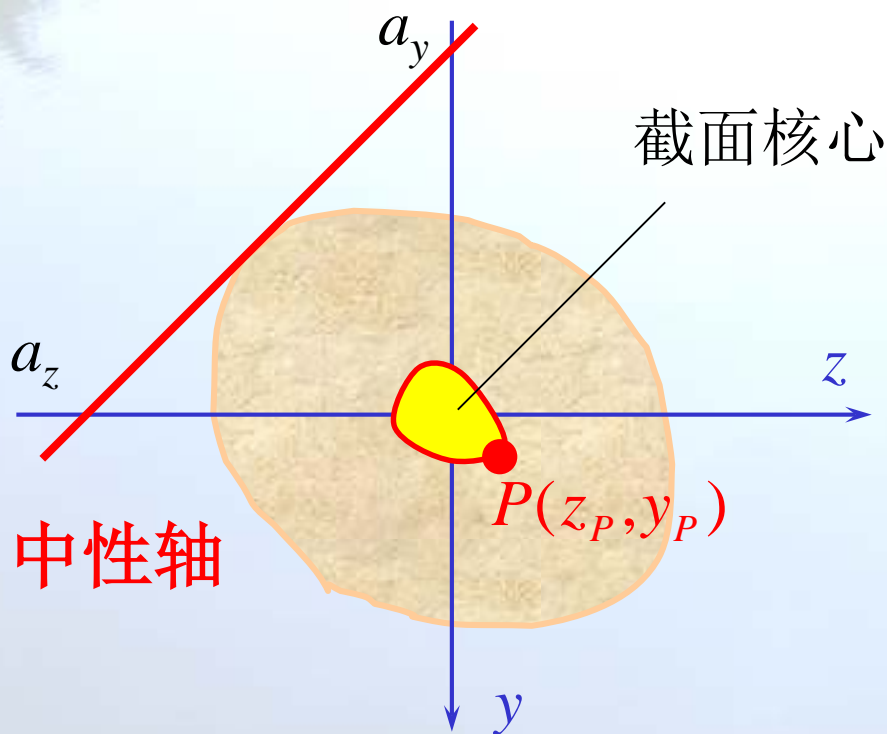
$$\text{令 } y_0 = 0, \quad 1 + \frac{z_P a_z}{i_y^2} = 0$$

$$\therefore \begin{cases} a_y = -\frac{i_z^2}{y_P}, \\ a_z = -\frac{i_y^2}{z_P}, \end{cases}$$

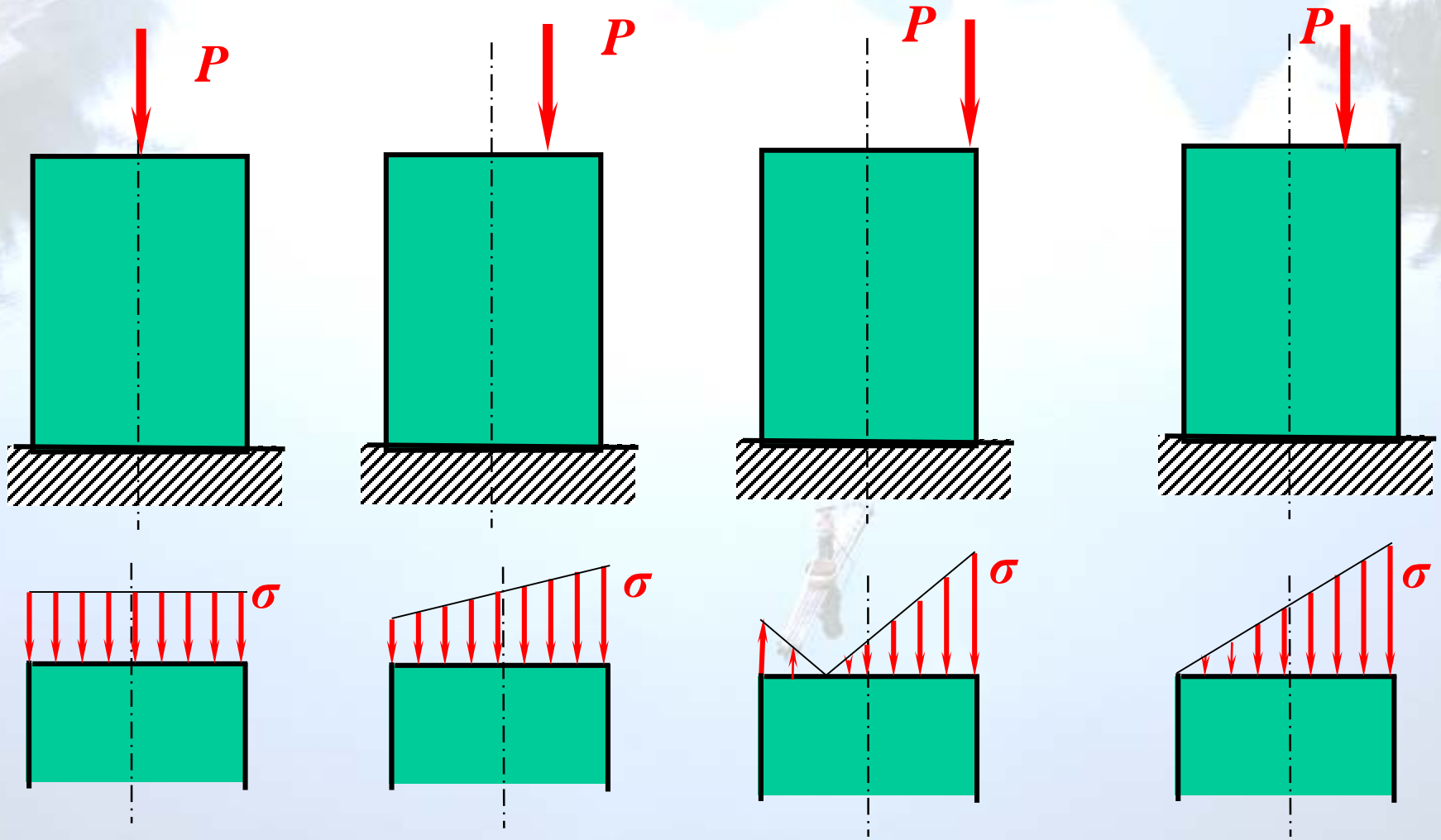
三、截面核心：

$$a_y = -\frac{i_z^2}{y_P}, \quad a_z = -\frac{i_y^2}{z_P},$$

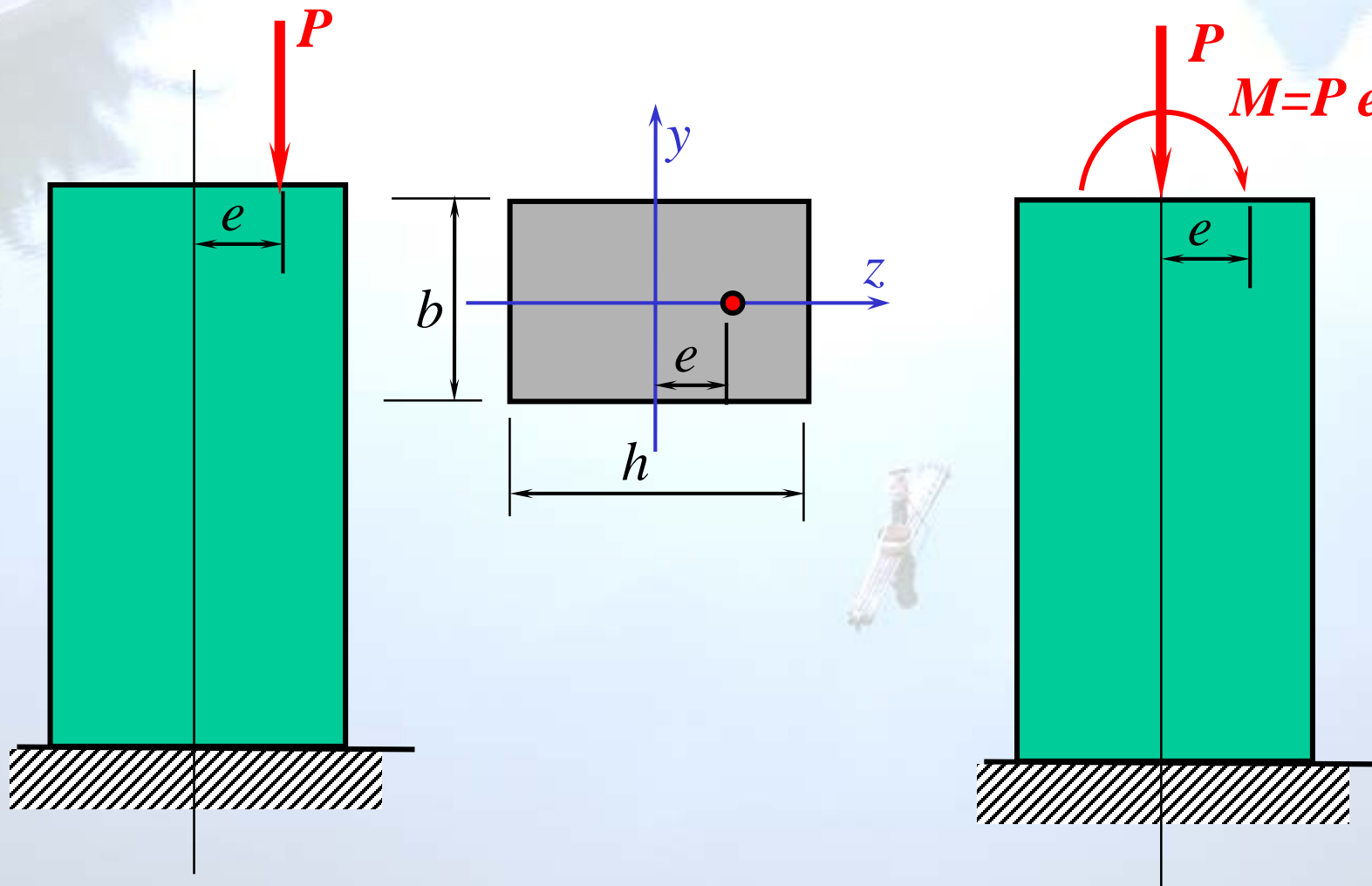
当 y_P 和 z_P 逐步减小时，中性轴将移出横截面，截面上只存在拉应力。

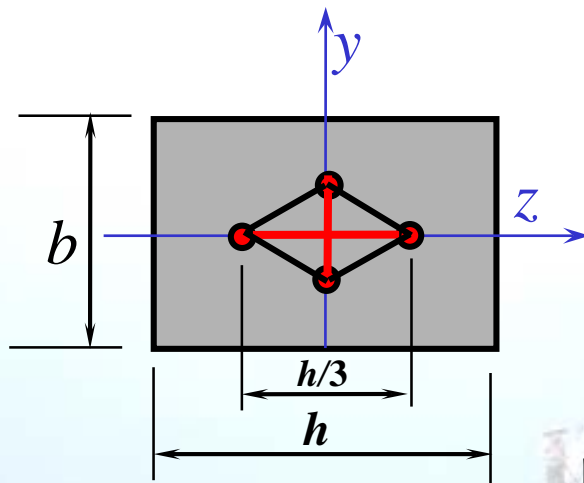
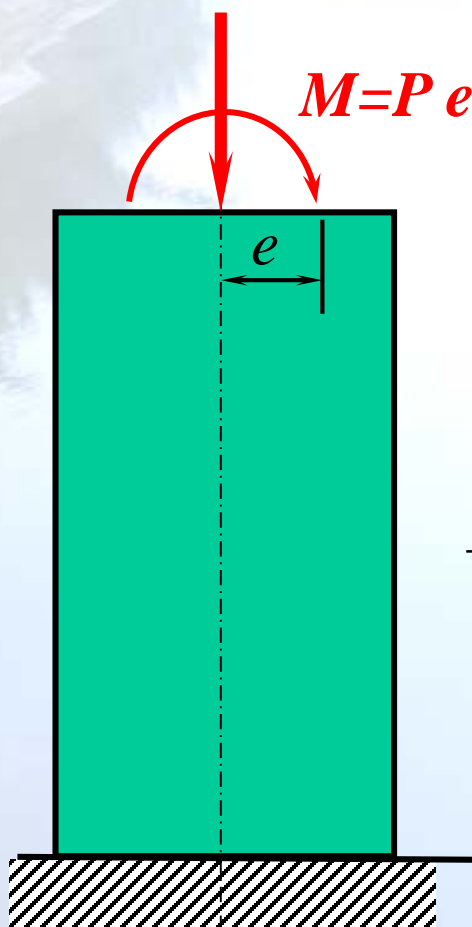


当外力作用点位于截面形心附近的一个区域内时，可以保证中性轴不穿过横截面，横截面上无压应力（或拉应力），此区域称为截面核心。



[例]: 矩形截面立柱, 欲使柱内不出现拉应力, 求 P 力的作用区域。





$$\sigma_{t \max} = \frac{M}{W_y} - \frac{P}{A} \leq 0$$

$$\frac{Pe}{bh^2/6} - \frac{P}{bh} \leq 0$$

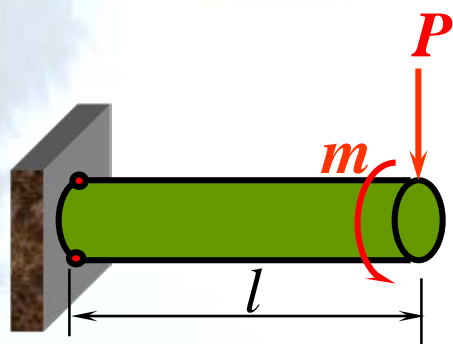
$$\therefore e \leq \frac{h}{6}$$

由对称性可知，在 z 轴上的作用区域为 $h/3$

同理可知，在 y 轴上的作用区域为 $b/3$

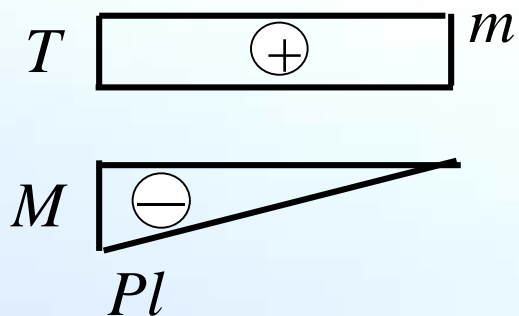
可以证明，当 P 力作用在由此四点围成的菱形内时，横截面上无拉应力。该菱形区域称为**截面核心**

§ 8-5 弯曲与扭转的组合

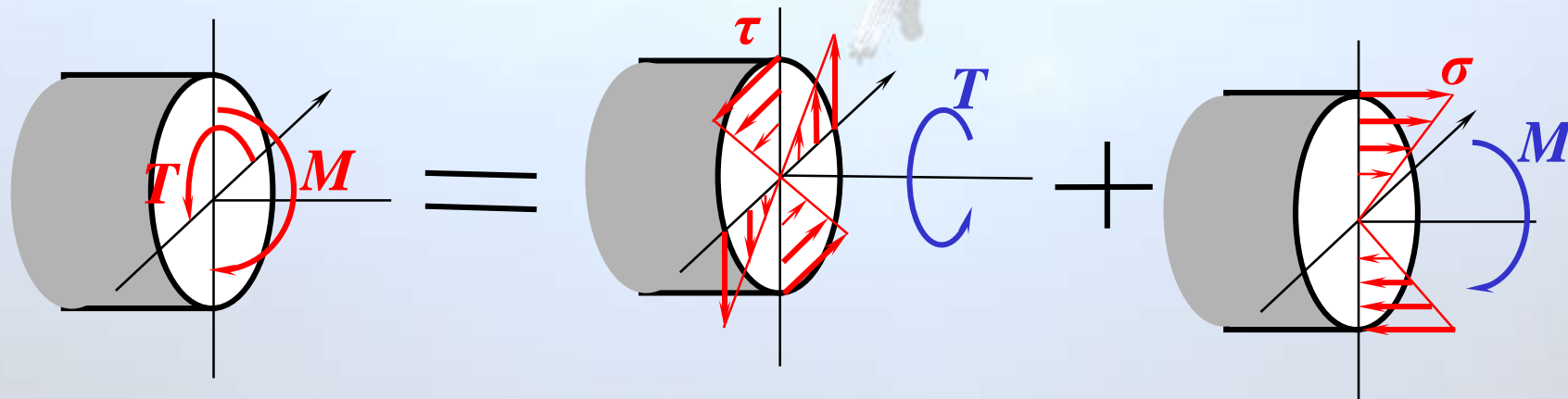


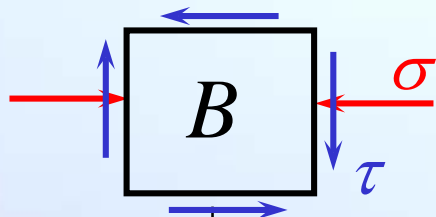
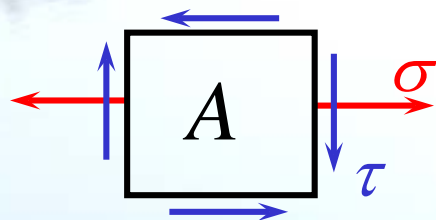
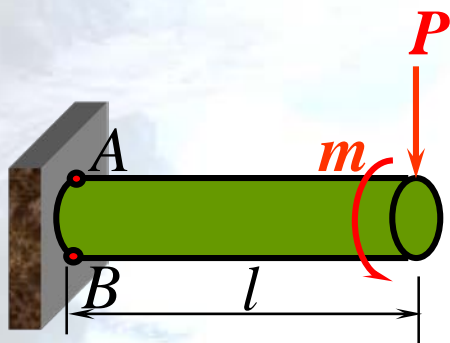
危险截面在固定端

危险点在固定端的上、下两点



$$\tau = \frac{T}{W_t}, \quad \sigma = \frac{M}{W}$$



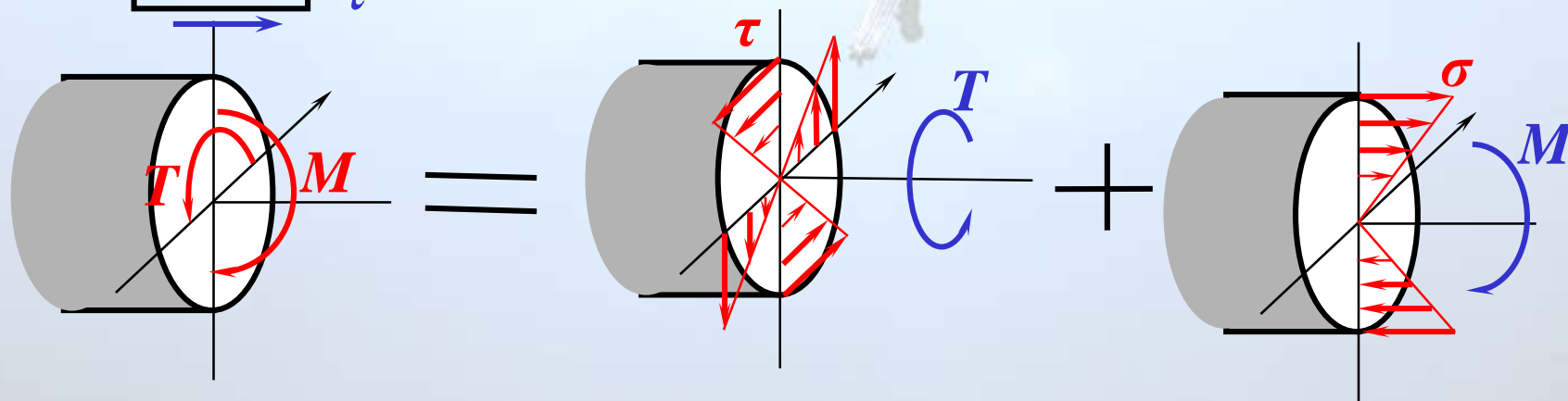


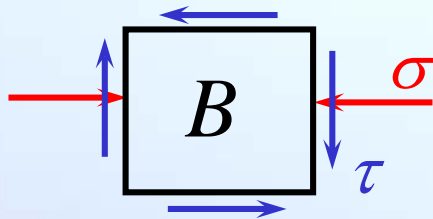
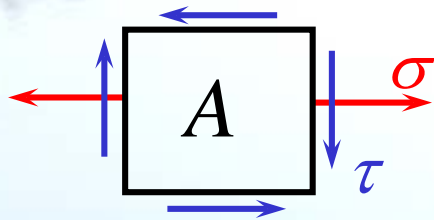
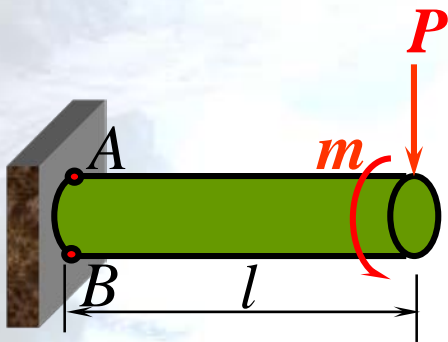
$$\sigma_{r3} = \sqrt{\sigma^2 + 4\tau^2}$$

$$\sigma_{r4} = \sqrt{\sigma^2 + 3\tau^2}$$

$$\sigma_{r3} = \sqrt{\left(\frac{M}{W}\right)^2 + 4\left(\frac{T}{W_t}\right)^2}$$

$$\sigma_{r4} = \sqrt{\left(\frac{M}{W}\right)^2 + 3\left(\frac{T}{W_t}\right)^2}$$





$$\therefore W_t = 2W$$

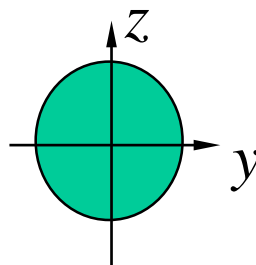
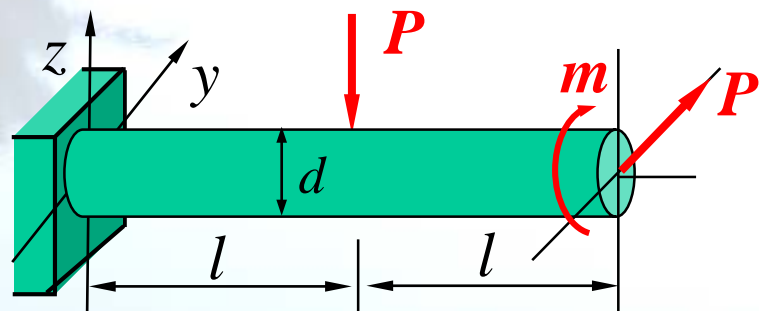
$$\therefore \sigma_{r3} = \sqrt{\left(\frac{M}{W}\right)^2 + 4\left(\frac{T}{2W}\right)^2}$$

即：

$$\sigma_{r3} = \frac{\sqrt{M^2 + T^2}}{W}$$

$$\sigma_{r4} = \frac{\sqrt{M^2 + 0.75T^2}}{W}$$

[例7] 已知： $P=4.2\text{kN}$ ， $m=1.5\text{kN}\cdot\text{m}$ ， $l=0.5\text{m}$ ， $d=100\text{mm}$ ，
 $[\sigma]=80\text{MPa}$ ，按第三强度理论校核杆的强度。

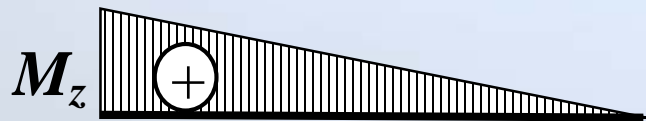
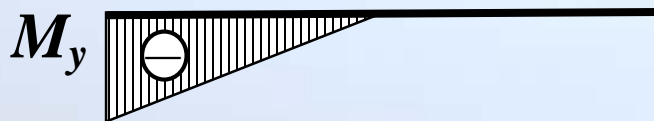
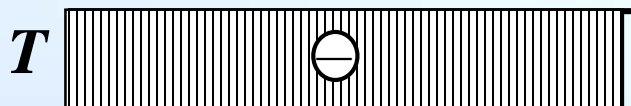


解： 危险截面在固定端

$$T = m = 1.5(\text{kN}\cdot\text{m})$$

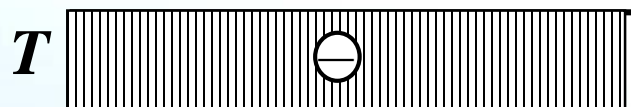
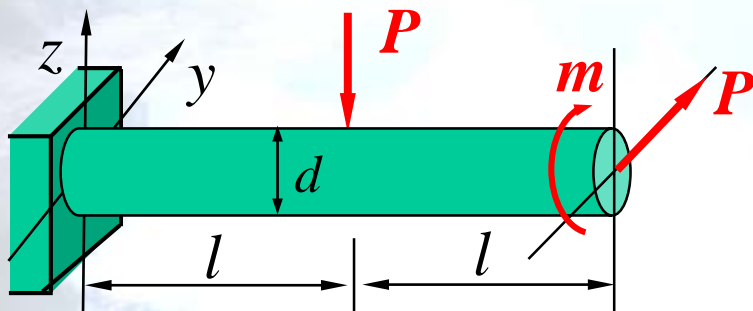
$$M_y = P \times l = 2.1(\text{kN}\cdot\text{m})$$

$$M_z = P \times 2l = 4.2(\text{kN}\cdot\text{m})$$



将弯矩合成：

$$M = \sqrt{M_y^2 + M_z^2} = \sqrt{2.1^2 + 4.2^2} = 4.7(\text{kN}\cdot\text{m})$$



$$\sigma_{r3} = \frac{\sqrt{M^2 + T^2}}{W}$$
$$= \frac{\sqrt{4.7^2 + 1.5^2} \times 10^6}{\frac{3.14 \times 100^3}{32}}$$

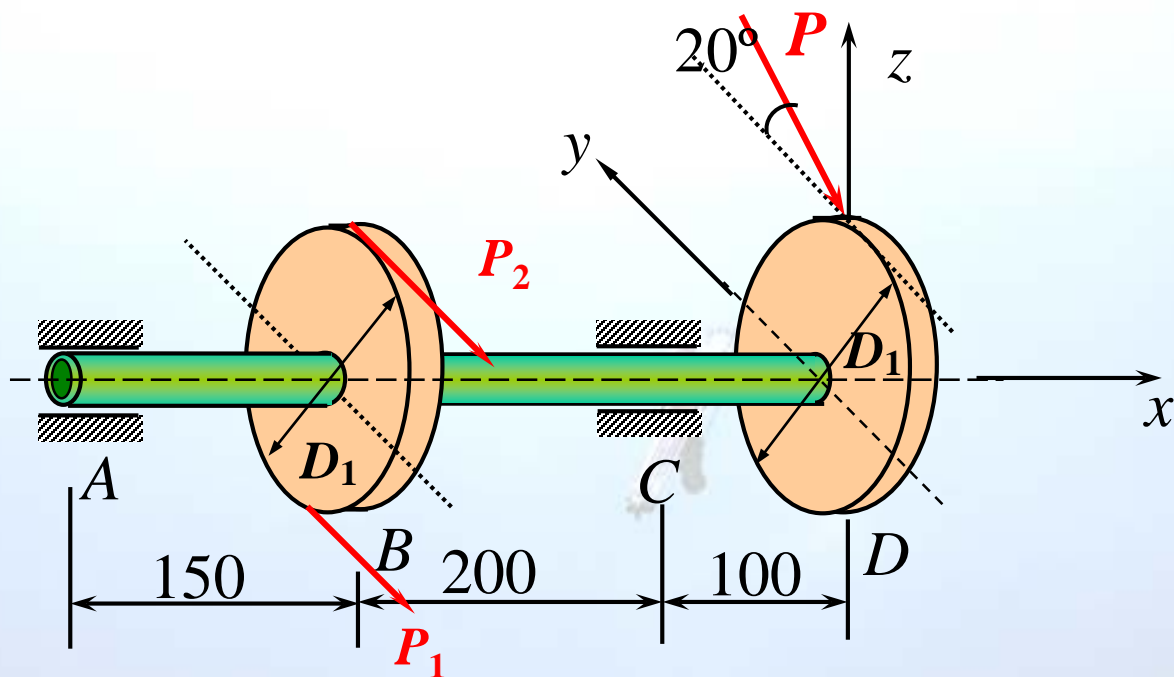
$$= 50.3 \text{ MPa} < [\sigma]$$

安全!



◀ ▶

[例8] 图示空心圆轴，内径 $d=24\text{mm}$ ，外径 $D=30\text{mm}$ ，轮子直径 $D_1=400\text{mm}$ ， $P_1=1.2\text{kN}$ ， $P_1=2P_2$ ， $[\sigma]=120\text{MPa}$ ，试用第三强度理论校核此轴的强度。



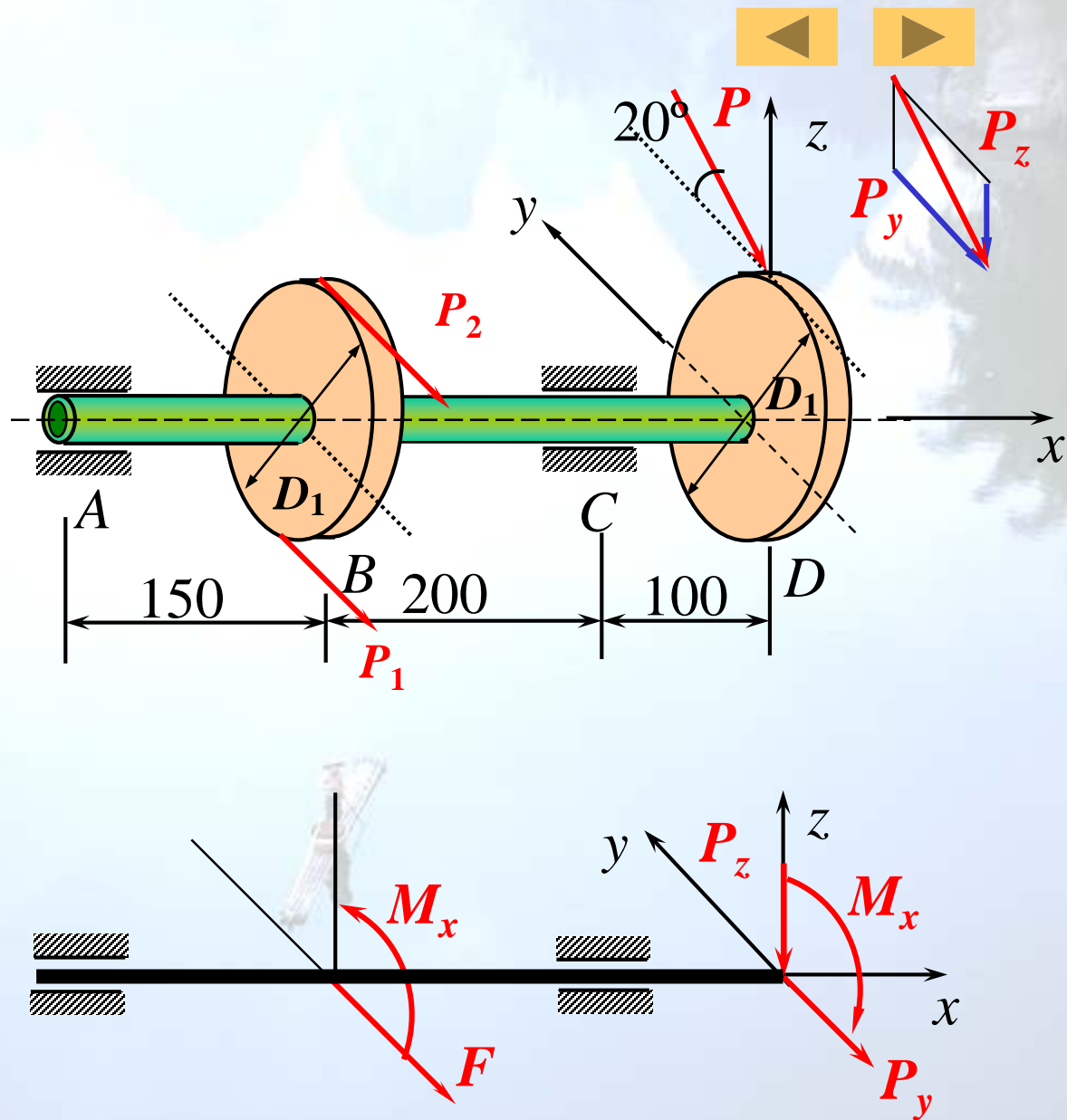
解：外力分析：

$$M_x = P_1 \cdot \frac{D_1}{2} - P_2 \cdot \frac{D_1}{2}$$

$$= 120(\text{N} \cdot \text{m})$$

$$F = P_1 + P_2$$

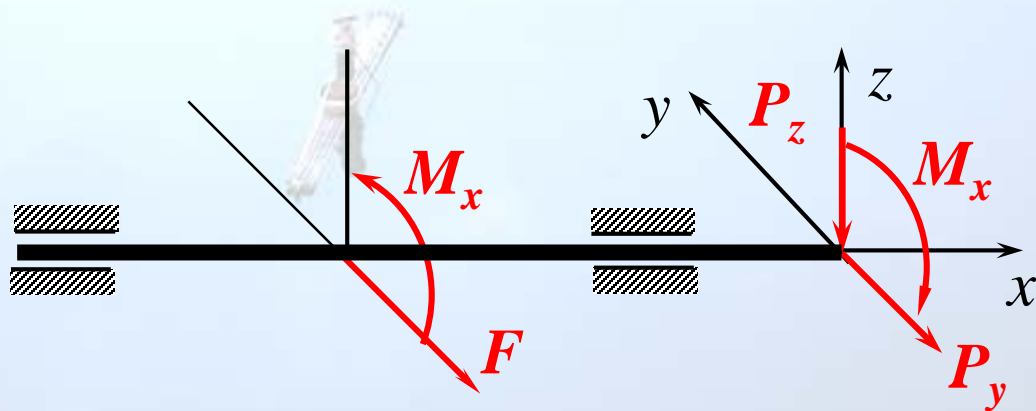
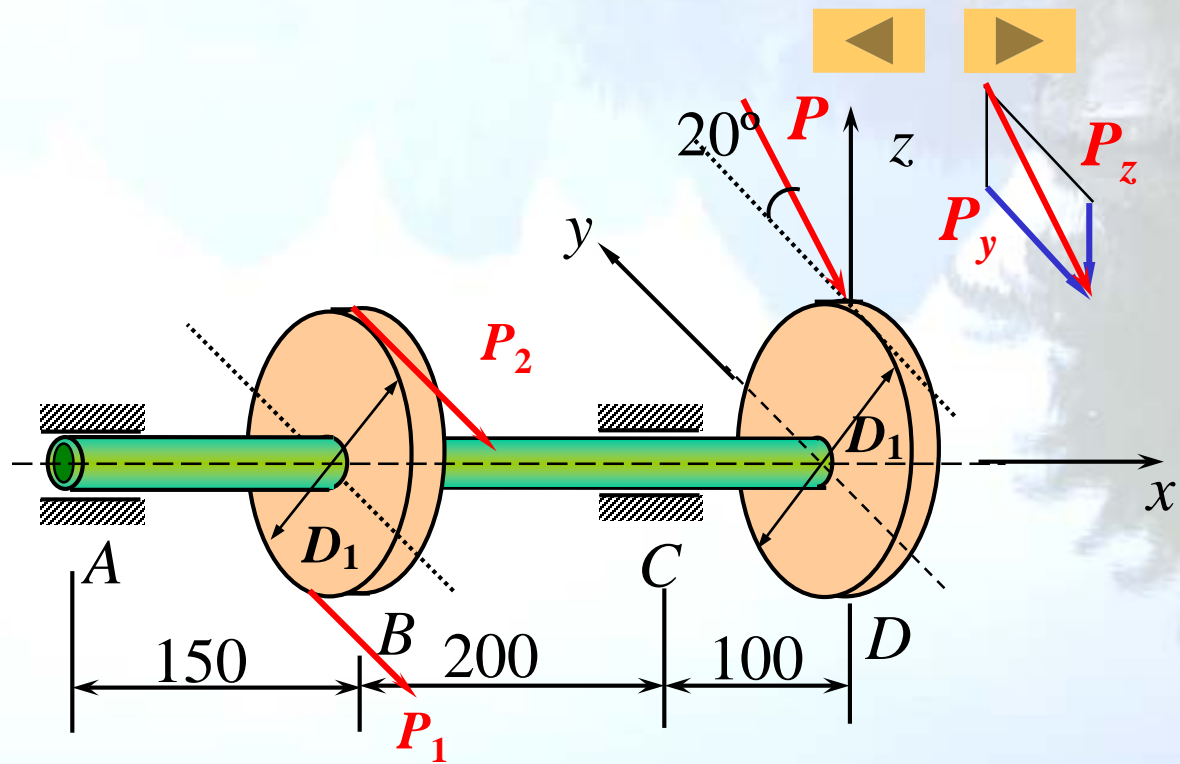
$$= 1.8(\text{kN})$$



$$\text{由 } M_x = P_y \cdot \frac{D_1}{2}$$

$$\text{得: } P_y = 0.6(\text{kN})$$

$$\begin{aligned} P_z &= P_y \cdot \tan 20^\circ \\ &= 0.218(\text{kN}) \end{aligned}$$



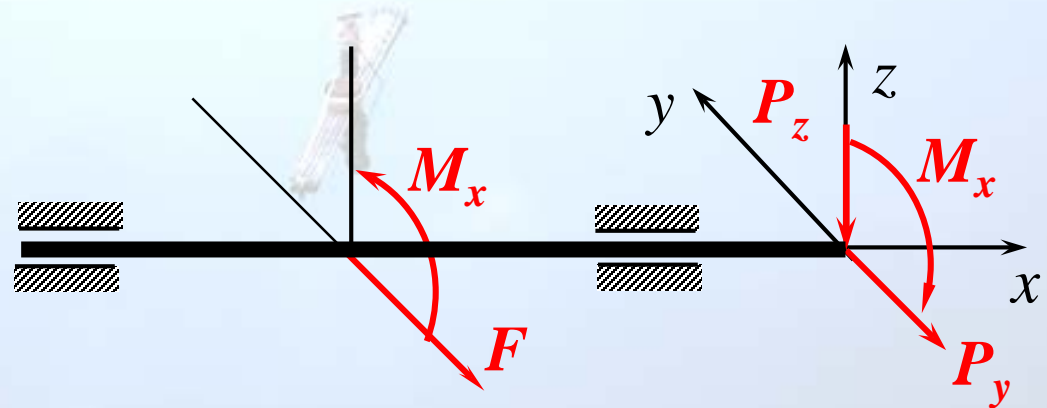
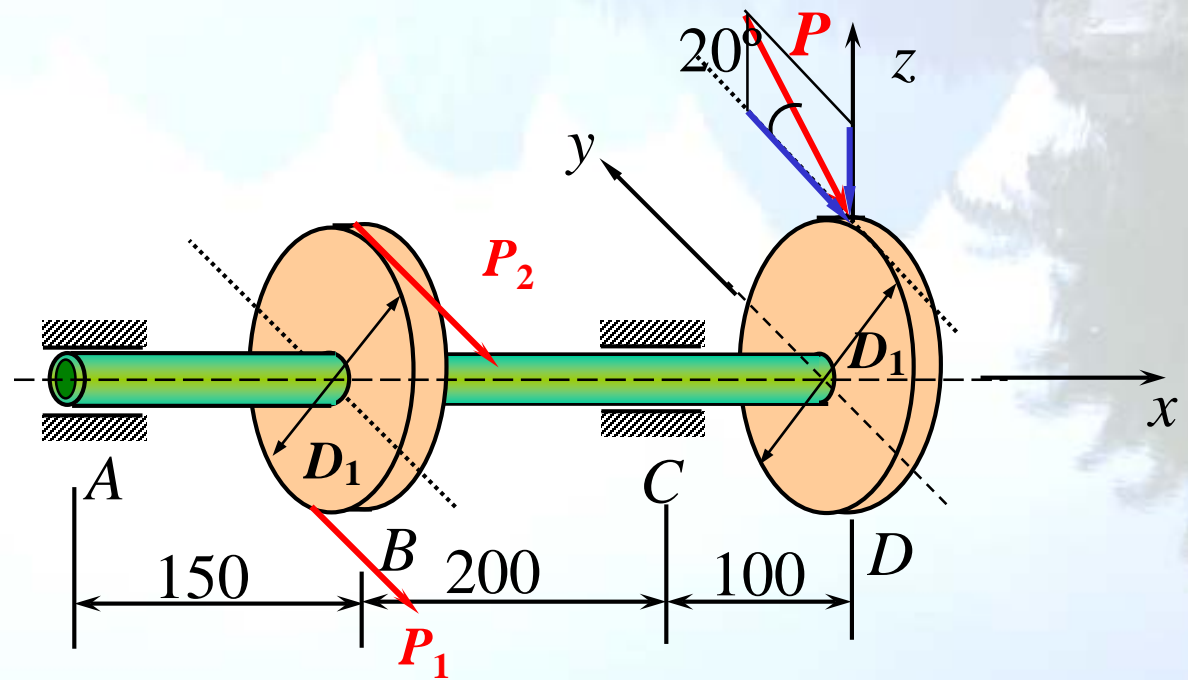
$$M_x = 120(\text{N} \cdot \text{m})$$

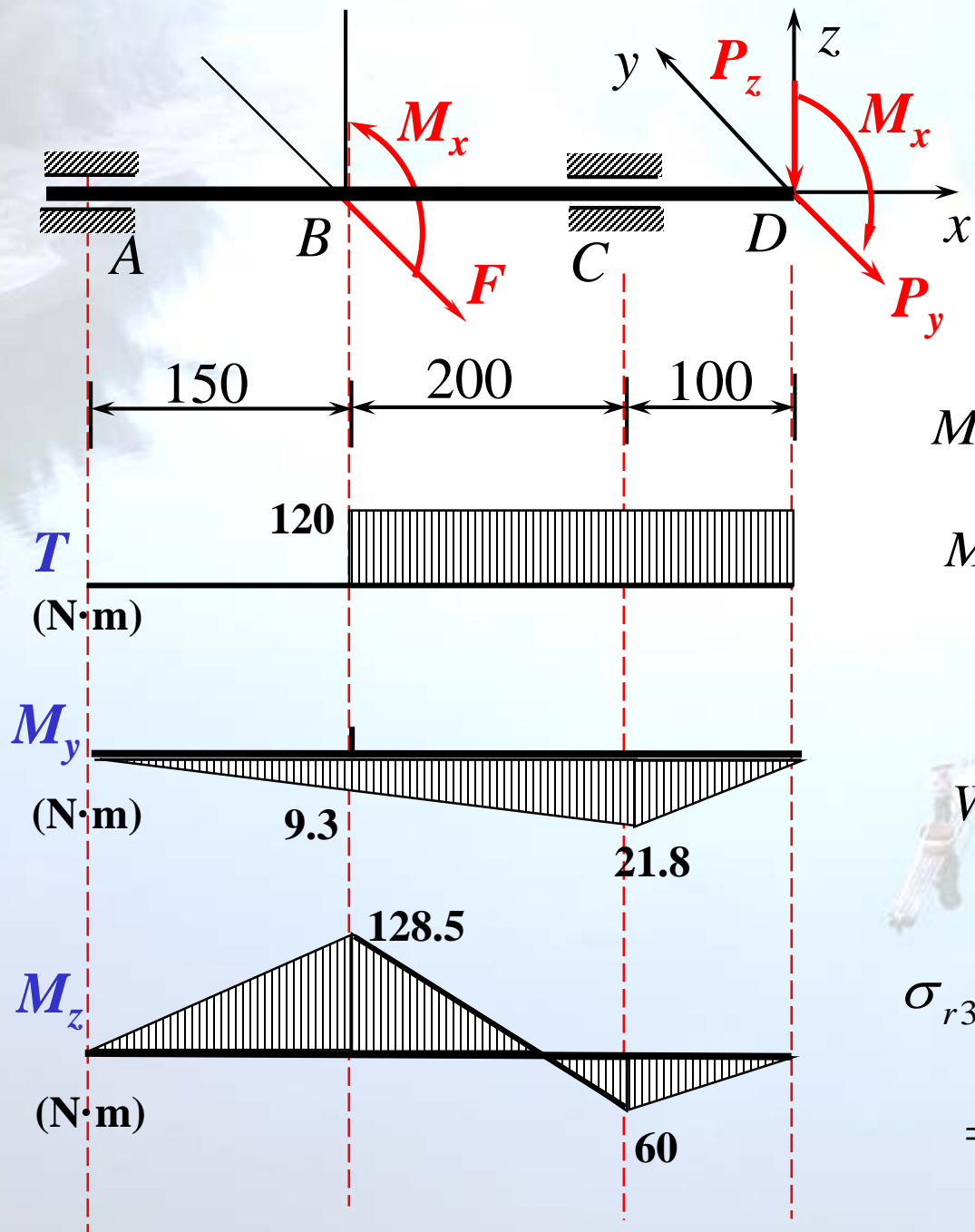
$$F = P_1 + P_2$$

$$= 1.8(\text{kN})$$

$$P_y = 0.6(\text{kN})$$

$$P_z = 0.218(\text{kN})$$





内力分析：弯扭组合变形

危险面内力为：

$$M_B = \sqrt{9.3^2 + 128.5^2} = 128.8(\text{N}\cdot\text{m})$$

$$M_C = \sqrt{21.8^2 + 60^2} = 63.8(\text{N}\cdot\text{m})$$

$\therefore B$ 截面是危险面。

$$W = \frac{\pi D^3}{32} [1 - (\frac{d}{D})^4] = 1564(\text{mm}^3)$$

$$\sigma_{r3} = \frac{\sqrt{M_B^2 + T^2}}{W} = \frac{\sqrt{128.8^2 + 120^2} \times 10^3}{1564}$$

$$= 112.5(\text{MPa}) < [\sigma]$$

\therefore 安全

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