# PRISMS-Plasticity: An Open Source Crystal plasticity FE Code (Session2)

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#### Uniaxial Compression in Cu with random Orientation

#### Playing with the input files:

- 1) Change the loading to uniaxial tension.
- 2) Use a more refined mesh:

```
set Refine factor = 2
set Skip Output Steps = 1
```

3) Output QuadratureOutput and investigate the output file with just grainID and position:

```
set Refine factor = 0
set Skip Output Steps = 25
set Write Quadrature Output = true
set Skip Quadrature Output Steps = 25
```

If you are in the FCC\_RandomOrientationBlock folder as your current directory:

vim ../../../src/materialModels/crystalPlasticity/updateAfterIncrement.cc

Commenting all lines in the QuadratureOutput region except those you want:

Recompile the code using "make release" in the plasticity/applications/crystalPlasticity/fcc folder.

cd fcc/FCC\_RandomOrientationBlock mpirun -n 6 ../../main prm.prm







#### Uniaxial Compression in Cu with random Orientation

#### Playing with the input files:

4) Applying a cyclic loading using the Tabular BCs.

```
set Use Simple BCs = false
set Use Tabular BCs = true
set Tabular Boundary condition filename = boundaryconditions.txt
set Number of time data for Tabular BCs = 7
set Number of tabular boundary conditions = 4
set Tabular Time Table = 0,0.3,0.9,1.5,2.1,2.7,3
1 1 0 0 0 0 0 0 0
boundaryconditions.txt
3 2 0 0 0 0 0 0 0
5 3 0 0 0 0 0 0 0
6 3 0 -0.003 0.003 -0.003 0.003 -0.003 0.003 -0.003 0
```

```
set Total time = 3
set Skip Output Steps = 20
```

I made the simulation shorter in each cycle (strain amplitude of 0.3%) to make the simulation faster. Let's do the simulation.







#### Uniaxial Compression in Cu with random Orientation

#### Adding another variable to the visualization:

Adding Tzz as an ouput variable.

set Output Variable 1= true

Edit the updateAfterIncrement.cc line 125 to:

this->postprocessValues(cellID, q, 3, 0) = T[2][2];

Recompile the code.

Open the projectedFields-0024.pvtu using Paraview and check the variables. You should have the **outputVar1** which is Tzz.







- We start with the Dream3D to generate a microstructure from EBSD and study its response using PRISMS-Plasticity
- We have a pipeline prepared for Dream3D to generate the input file required for PRISMS-Plasticity in:

/Training\_Materials/Pre-Processing/fcc

- Go to file->Open.
- Looking into the prisms-plasticity folder: Training\_Materials/Pre-Processing/fcc.
- Select the PRISMS\_pipeline\_fcc.json file.

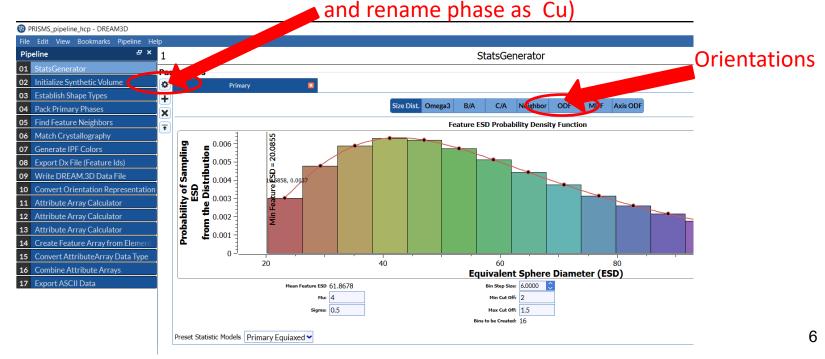






- This will open a prepared pipeline which can generate the PRISMS-Plasticity input files.
- In the pipeline, there are different parts numbered from 01 to 17.

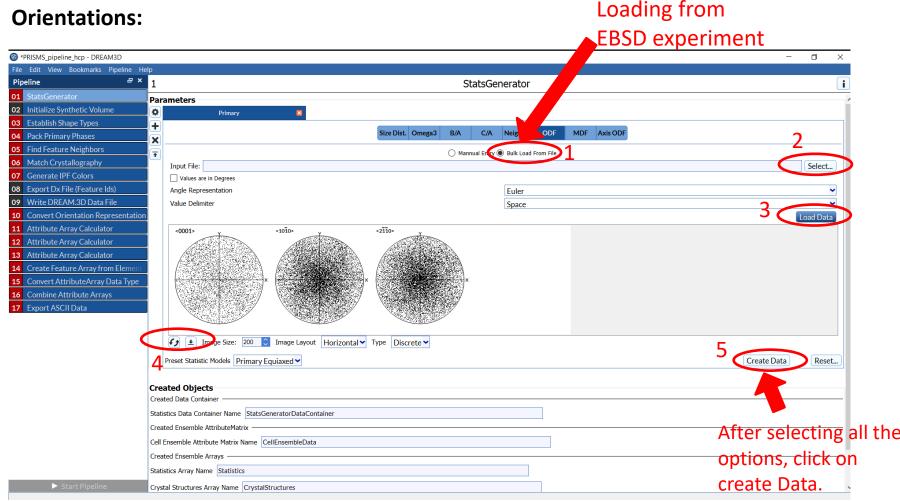
**O1 StatsGenerator**: Here, you can define the statistical information regarding the crystal structure, grain size, shape, orientation. Crystal structure (We'll choose Cubic











• From select, open the file Training\_Materials\Pre-Processing\fcc\copperdata1. Click on Load Data, then click on refresh, and finally click on Create Data.







#### Reading the texture from the EBSD experiment:

EBSD input file format for bulk load from file

```
File Edit Search View Encoding Language Settings Tools Macro Run
  1 Angle Count:588638
   1.05842 1.73449 0.49267 1
    1.04793 1.73497 0.4861
   0.70312 1.797
                     2.07639 1
    0.94064 2.49537 5.27844 1
    0.83093 1.1384
    0.69873 1.80268 2.07742 1
    1.60536 2.10196 5.05798 1
    3.85197 1.34008 4.20304 1
 10 3.97084 2.00518 0.65303 1
    0.68157 1.8056
             2.03406 3.28571 1
    3.75425 1.31183 0.01477 1
    4.03747 1.55849 0.74614 1
    3.06563 0.93898 5.6267
 16 1.73482 1.30826 3.16308 1
    1.74051 1.31024 3.15811 1
    1.74679 1.31532 0.0167
    1.74381 1.30945 0.01544 1
    1.74193 1.31495 0.01806 1
 21 1.7428
             1.30853 0.02107 1
    1.74027 1.30931 3.15521 1
             1.31609 3.15246 1
   2.29945 1.73205 3.2328
 25 3.04848 0.29176 1.61409 1
                                  1
 26 4.80671 1.82614 0.33644 1
```

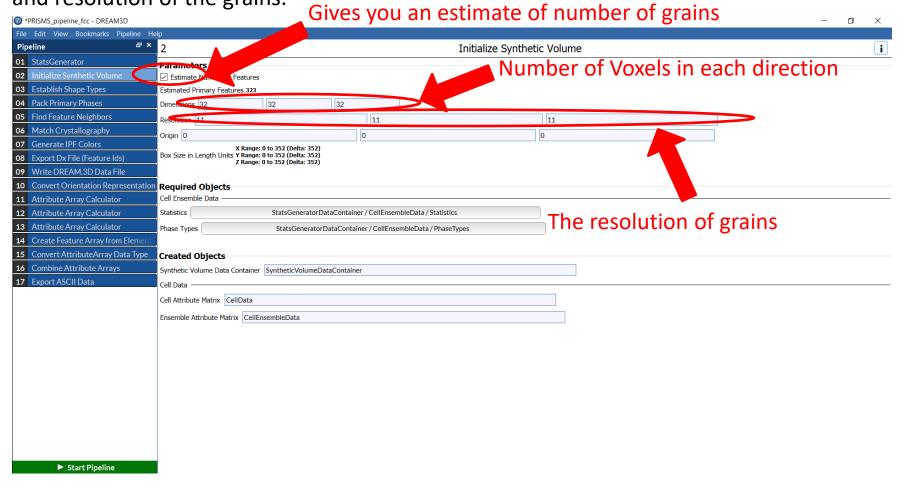








**O2 Initialize Synthetic volume**: Here, you define the number of voxels in each direction and resolution of the grains.









08 Export Dx File, 09: Write DREAM.3D Data File, 17: Export ASCII Data

Update the addresses here to a folder on your system.

After that, hit the Start Pipeline (Green button below pipelines)

You can check the generated files in the folder you selected.

Two outputs will be grainID.txt and orientations.txt.







#### grainID.txt:

This file assigns the grainID for each voxel. Important information from this file is:

- Number of header lines: 20
- Number of Voxel in each direction: 32\*32\*32

```
File Edit Search View Encoding Language Settings Tools Macro Run Plugins Window
    # object 1 are the regular positions. The grid is 50 50 50. The origin is
    # at [0 0 0], and the deltas are 1 in the first and third dimensions, and
    # 2 in the second dimension
  5 object 1 class gridpositions counts 50 50 50
  6 origin 0 0 0
 8 delta 0 1 0
      object 2 are the regular connections
 13 object 2 class gridconnections counts 50 50 50
 14
      object 3 are the data, which are in a one-to-one correspondence with
    # the positions ("dep" on positions). The positions increment in the order
    # "last index varies fastest", i.e. (x0, y0, z0), (x0, y0, z1), (x0, y0, z2)
      (x0, v1, z0), etc.
 19 #
 20 object 3 class array type int rank 0 items 125000 data follows
 21 1100 709 709 709 709 709 709 351 351 351 351 447 447 447 447 447 447 634 634
    1100 709 709 709 709 709 557 351 351 351 351 447
        1100 709 557 557 557 557 557 351 351 351 447 447 447 447
 24 1046 1046 1046 557 557 557 557 557 557 351 351 447 447 447 447 447 634
 26 1046 1046 1046 557 557 557 557 557 557 557 557 575 575 447 127 127
 27 1046 1046 557 557 557 557 557 557 557 557 575 575 575 575 127 127 127 842 84
                                                           length: 507,247 lines: 2,531
Normal text file
                                                                         In:1 Col:1 S
```







### Rate-independent formulation

We want to use the generated microstructures using the rate-dependent crystal plasticity model.

To do so, first we need to copy the following files: plasticity/src/materialModels/crystalPlasticity/MaterialModels/RateDependentModel/c alculatePlasticity.cc and userFunctions.cc and paste it in plasticity/src/materialModels/crystalPlasticity.

Then we need to recompile the code by going to the folder: plasticity/applications/crystalPlasticity and type:

Make release

Sometimes, by just doing make release, the updated file will not be compiled and the code still uses the previous version. To make sure that the code compiling with the recent version, you can temporarily move the updated files from the folder (calculatePlasticity.cc and userFunctions.cc) and type make release. It will give you errors. And then move those file back in the folder and recompile. This should work.







### Rate-independent formulation

Now, we'll copy the generated microstructure files of grainID.txt and orientations.txt to the folder plasticity/applications/crystalPlasticity/fcc/FCC\_Random\_RateDependent.

We need to update the prm.prm file in the following fields:

FE mesh: change to 32by32by32 (using set Subdivisions)

Set Output: True, and skip output steps of 5

Total time=5 DeltaT=0.005

Voxels in x,y,z=32; GrainID Filename=grainID.txt; Number Header lines=20







#### Rate-independent formulation

We're using some of the features useful for User Defined Crystal plasticity models:

**User Material Constants**: If you need to define new material constants in your model, you can use this field.

**User Material State Variables**: If you need to define new state variables in your model, you can use this field. You can also define the initial value for your sate variables.

$$\dot{\gamma}_0$$
  $m$   $cr1$   $cr2$   $Max1$   $Max2$  set User Material Constants 1 = 1.0e-3, 0.04, **1.0e-4, 1.0e-4**, 10000, 10000, 0, 0, 0, 0, 0

$$\dot{\gamma}^{\alpha} = \dot{\gamma}_0 \left| \frac{\tau^{\alpha} - \chi^{\alpha}}{s^{\alpha}} \right|^m \operatorname{sign}(\tau^{\alpha} - \chi^{\alpha})$$

 $\dot{\gamma}^{\alpha}$ : shearing rate  $\dot{\gamma}_0$  reference shearing rate  $s^{\alpha}$  slip resistance  $\chi^{\alpha}$  back stress

The rate-dependent model is numerically solved using two iterative schemes, one of them is located inside the other one. Each of these iterative schemes has its own threshold of error (cr1 and cr2) and maximum number of iterations (Max1 and Max2).







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**Backstress parameters** 

### Implementing your own crystal plasticity model

The only files you need to update are: plasticity/src/materialModels/crystalPlasticity/MaterialModels/RateDependentModel/c alculatePlasticity.cc and userFunctions.cc

calculatePlasticity.cc: The main implementation.

userFunctions.cc: Auxiliary files you need to use in the calculatePlasticity.cc.

**Documentation for user defined crystal plasticity models:** https://github.com/prisms-center/plasticity/blob/master/docs/User%20defined%20material%20model%20manual.pdf

Let's briefly go over the calculatePlasticity.cc of the rate-dependent model as an example to see how it looks like.







#### Periodic BCs

To use the periodic BCs, it is better that the generated microstructure is periodic as well. To use the periodic BCs, one cannot use **set Refine factor** to refine the mesh.

C.P. Przybyla, "Microstructure-sensitive extreme value probabilities of fatigue in advanced engineering alloys." PhD Thesis, Georgia Institute of Technology (2010) section 5.5.

This is crucial in calculations of fatigue resistance when smaller microstructure instantiations are employed that represent bulk, i.e., subsurface, material response. Przybyla (2010) (See the references) presented the details of the periodic BCs (PBCs) required to mimic the subsurface microstructure during the fatigue simulation. In PRISMS-Fatigue framework, **PBCs are implemented using a set of linear constraints**.

These constraints are defined on three components of opposing Faces, parallel Edges, and Vertices. Rigid body motion is also excluded by assigning additional constraints. Three sets of constraints are applied on nodes on opposing Faces (in the direction perpendicular to those Faces), nodes on each set of four parallel Edges (in the two directions perpendicular to the direction in which the Edges are parallel), and Vertices (in all directions). The contraction or expansion of the dimensions of the actual microstructure volume are considered.







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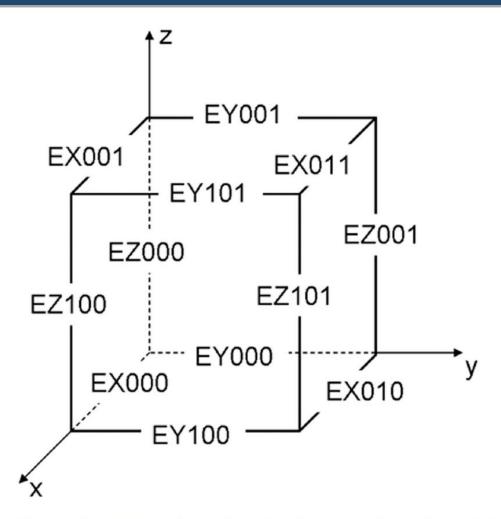
#### Periodic BCs

**Table 5.1:** Description of symbols used to describe nodes sets at vertices and faces.

	· · ·
Symbol	Description
REF	Reference node located at $x = 0$ , $y = 0 & z = 0$
V000	Node at vertex located at $x = 0$ , $y = 0 & z = 0$
V001	Node at vertex located at $x = 0$ , $y = 0 & z = h$
V010	Node at vertex located at $x = 0$ , $y = h \& z = 0$
V100	Node at vertex located at $x = h$ , $y = 0 & z = 0$
V011	Node at vertex located at $x = 0$ , $y = h \& z = h$
V101	Node at vertex located at $x = h$ , $y = 0 & z = h$
V110	Node at vertex located at $x = h$ , $y = h \& z = 0$
V111	Node at vertex located at $x = h$ , $y = h \& z = h$
FXP	Face nodes excluding edges and vertices for surface normal to $x$ axis at $x = h$
FXN	Face nodes excluding edges and vertices for surface normal to $x$ axis at $x = 0$
FYP	Face nodes excluding edges and vertices for surface normal to $y$ axis at $y = h$
FYN	Face nodes excluding edges and vertices for surface normal to y axis at $y = 0$
FZP	Face nodes excluding edges and vertices for surface normal to z axis at $x = h$
FZN	Face nodes excluding edges and vertices for surface normal to z axis at $x = 0$



#### Periodic BCs



**Figure 5.9:** Location of edge node sets. Note that these edge node sets do not include the nodes at the vertices of the model.







set Use Simple BCs = false
This flag defines if one use Simple BCs. In this case, it should be defined as false.

set Use Periodic BCs = true Flag to indicate whether to use Periodic BCs.

set Periodic Boundary condition Constraint filename = PeriodicBCsConstraints.txt

The name of the file which include the constraints between the Vertices, Edges, and Faces. For a specific type of BCs, this should not be changed. For example, if one models the fully periodic BCs with different loading conditions, this file should not be changed.

This file includes the linear constraints for Vertices, Edges, and Faces. For each constraint, the file has two lines, first one for DOFs and second one for their corresponding coefficients. The convention for the DOFs are defined in section 5.5 of Przybyla PhD Thesis (2010).







For the Vertices constraints, each row has 5 columns. The first column defines the number of DOFs involves in this constraint. All remaining 4 columns correspond to the DOFs of Vertices. In the case of Edges and Faces, we only have the latter 4 columns. In the cases of constraints for Edges, the first two columns correspond to the DOFs of the Edges, while the third and fourth columns correspond to the Vertices. In the case of Faces, the first two columns correspond to the DOFs of the Faces, while the third and fourth columns correspond to the Vertices. DOFs convention for Vertices, Edges, and Faces used here are described in the file as headers.

```
#set Vertices Periodic BCs row order:
 #0=V000 11=V000 22=V000 33=V100 14=V100 25=V100 36=V010 17=V010 28=V010 39=V001 110=V001 211=V001
 # 12=V110 1 13=V110 2 14=V110 3 15=V101 1 16=V101 2 17=V101 3 18=V011 1 19=V011 2 20=V011 3 21=V111 1 22=V111
 23=V111 3
 4 12 6 3 0
 41-1-11
# Edges Constraints: Each line has two rows, one for DOFs and one for their corresponding coefficient.
#set Edges Periodic BCs row order:
#0=EX000 11=EX000 22=EX000 33=EX001 14=EX001 25=EX001 36=EX010 17=EX010 28=EX010 39=EX011 1
10=EX011 2 11=EX011 3
# 12=EY000 1 13=EY000 2 14=EY000 3 15=EY001 1 16=EY001 2 17=EY001 3 18=EY100 1 19=EY100 2 20=EY100 3
21=EY101 1 22=EY101 2 23=EY101 3
#24=EZ000 125=EZ000 226=EZ000 327=EZ010 128=EZ010 229=EZ010 330=EZ100 131=EZ100 232=EZ100 3
33=EZ110 1 34=EZ110 2 35=EZ110 3
39189
-1 1 -1 1
```





# Vertices Constraints: Each line has two rows, one for DOFs and one for their corresponding coefficient.



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For the Vertices constraints, each row has 5 columns. The first column defines the number of DOFs involves in this constraint. All remaining 4 columns correspond to the DOFs of Vertices. In the case of Edges and Faces, we only have the latter 4 columns. In the cases of constraints for Edges, the first two columns correspond to the DOFs of the Edges, while the third and fourth columns correspond to the Vertices. In the case of Faces, the first two columns correspond to the DOFs of the Faces, while the third and fourth columns correspond to the Vertices.

```
# Faces Constraints: Each line has two rows, one for DOFs and one for their corresponding coefficient.

#set Faces Periodic BCs row order:

# 0=FXN_1 1=FXN_2 2=FXN_3 3=FXP_1 4=FXP_2 5=FXP_3 6=FYN_1 7=FYN_2 8=FYN_3 9=FYP_1 10=FYP_2 11=FYP_3 # 12=FZN_1 13=FZN_2 14=FZN_3 15=FZP_1 16=FZP_2 17=FZP_3 # Important note: The first column of all face constraint lines must always start with the positive faces, i.e., FXP,FYP, and FZP. 3 0 3 0 1 -1 -1 1
```

**Important note**: The first column of all **Faces** constraint lines must always start with the positive Faces, i.e., FXP,FYP, and FZP.







#### Vertices:

V110 $_x$  –  $V010_x$  –  $V100_x$  +  $V000_x$  = 0 In the periodic BCs file, this becomes: 4 12 6 3 0 4 1 -1 -1 1

#### Edges:

-EX001 $_x$  +  $EX011_x$  -  $V011_x$  +  $V001_x$  = 0 In the periodic BCs file, this becomes: 3 9 18 9 -1 1 -1 1

One should note that we named this section Edges to show that it includes the DOFs of the Edges. However, the last two columns belong to the Vertices DOFs.

#### Faces:

$$-FXN_x + FXP_x - V100_x + V000_x = 0$$

As mentioned earlier, the first column of all face constraint lines must always start with the positive Faces, i.e., FXP,FYP, and FZP.

So we first rearrange the equation as follows:

$$FXP_x - FXN_x - V100_x + V000_x = 0$$

In the periodic BCs file, this becomes:

3030

1 -1 -1 1

One should note that we named this section Faces to show that it includes the DOFs of the Faces. However, the last two columns belong to the Vertices DOFs.







The number of linear constrains for Vertices, Edges, and Faces are defined next.

```
set Number of Vertices Constraints = 12
set Number of Edges Constraints = 14
set Number of Faces Constraints = 6
```

The above numbers describes the sample with periodic BCs in 2 directions and free surface in the third one. In the case of fully periodic BCs, the numbers become as follows:

```
set Number of Vertices Constraints = 12
set Number of Edges Constraints = 27
set Number of Faces Constraints = 9
```







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The next part defines the BCs which are applied to the Vertices. The notation used here is in line with the **section 5.5** of Przybyla PhD Thesis (2010). The first line control which Vertices DOF the BCs are applied to by assigning the value of 1. Otherwise, the value is 0 and that DOF has no predefined BCs. The second line define the values for BCs at the end of the total time.

```
# 0=V000_1;1=V000_2;2=V000_3; 3=V100_1;4=V100_2;5=V100_3; 6=
    V010_1;7=V010_2;8=V010_3; 9=V001_1;10=V001_2;11=V001_3;
# 12=V110_1;13=V110_2;14=V110_3; 15=V101_1;16=V101_2;17=V101_3
    ; 18=V011_1;19=V011_2;20=V011_3; 21=V111_1;22=V111_2;23=
    V111_3;
set Vertices Periodic BCs row 1 = 1,1,1, 1,1,1, 1,0,1, 1,1,0,
    1,0,0, 1,0,0, 0,0,0, 1,0,0
```







One can also define the periodic BCs along Tabular loading. First, this flag should be set to true:

```
set Use Tabular Periodic BCs = true
```

Next, the second line of the applying BCs in the input file lines, i.e., **set Vertices Periodic BCs row 2**, will be the applied BCs at the time of the periodic Tabular time, which is defined as follows:

```
set periodic Tabular time = 10
```

This is to define the **base rate** at which the BCs are applied. In other words, the **base rate** of BCs is equal to (Vertices Periodic BCs row 2)/(periodic Tabular time) for each DOF of Vertices.

For example, here, for the DOF of **3=V100**<sub>1</sub>, we defined the value of 0.05 in **set Vertices Periodic BCs row 2**. The **base rate** can then be calculated as:

base rate=0.05/(set periodic Tabular time)=0.05/10=0.005.







Finally, the Tabular BCs is applied using Tabular Periodic Time Table and their coefficients as follows:

```
set Tabular Periodic Time Table = 0,10,30,50,70,90,110
set Tabular Periodic Time Table Coefficient = 1,-1,1,-1,1,-1,1
```

The first line defines the time table, and second line defines the corresponding coefficients for each of these time spans. For each time span (i.e., between each two times inside the **Time Table**), the rate of deformation is applied as **(Corresponding Coefficient\*base rate)**.

For example, the above values for these two lines state that:

```
\mathsf{Time}_1 = 0; Time_2 = 10; Time_3 = 30; Time_4 = 50; Time_5 = 70; Time_6 = 90; Time_7 = 110;
```

The corresponding coefficients are:

```
Coefficient_1 = 1; Coefficient_2 = -1; Coefficient_3 = 1; Coefficient_4 = -1; Coefficient_5 = 1; Coefficient_6 = -1; Coefficient_7 = 1;
```

For the first time span, the applied BCs between  $(Time_1=0)$  to  $(Time_2=10)$  has the rate of:

```
(Coefficient<sub>1</sub>=1)*(base rate)
```

From  $(Time_2=10)$  and  $(Time_3=30)$ , the rate is the  $(Coefficient_2=-1)^*$  (base rate).

This tabular loading defines a cyclic loading with equal max compression and tension strains.







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### Periodic BCs (Simulation)

#### Let's try a simulation set (rate\_independent)!!!

Change the directory to the folder fcc/periodicBCs

#### Running prm\_UniaxialCyclicTabular.prm

The microstructure is 32\*32\*32-> Let's have the FE mesh 8\*8\*8 (for the sake of time) for 6 processors, if you have less processors, try 4\*4\*4!

set Skip Output Steps = 10

I made the simulation shorter in each cycle (strain amplitude of 0.3%) to make the simulation faster. Let's do the simulation.

set Vertices Periodic BCs row 2 = 0,0,0, 0.002,0,0, 0,0,0, 0,002,0,0, 0.002,0,0, 0.002,0,0, 0.002,0,0

= 0.2

set periodic Tabular time

set Tabular Periodic Time Table = 0,0.2,0.6,1,1.4,1.8,2.2

set Total time = 2.2

Finally, this prm file is for rate\_independent model. Let's modify it for rate\_dependent.







### Periodic BCs (Simulation)

Let's modify **prm\_UniaxialCyclicTabular.prm** file for rate\_dependent by adding these lines before elastic stiffness:

```
# Flag to indicate if User Material Model is enabled
set Enable User Material Model
                               = true
# Flag to indicate if User Material Model is enabled Phase 1
set Enable User Material Model 1
                                = true
# Number of User Material Constants in a Material model Phase 1
set Number of User Material Constants 1
                                    = 12
# Number of User Material State Variables in a Material model Phase 1
set Number of User Material State Variables 1
                                     = 62
# Material Constants in a Material model Phase 1
                           = 1.0e-3, 0.04, 1.0e-4, 1.0e-4, 10000, 10000, 0, 0, 0, 0, 0, 0.0, 0.0
set User Material Constants 1
# Material State Variables in a Material model Phase 1
```



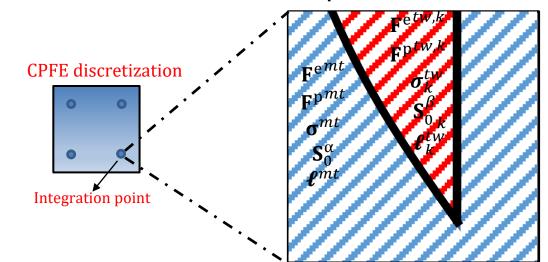
0.0, 0.0



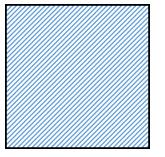


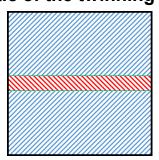
- The response of the material point is homogenized using Taylor model.
- Twinning and detwinning mechanisms can capture twin nucleation, twin growth, twin shrinkage, and detwinning.
- Multiple twin variants can be activated inside the material point.

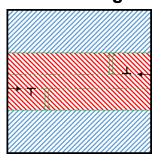
#### Schematic of a material point with twin

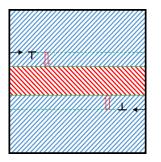


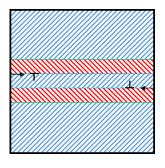
#### Schematic of the twinning and detwinning mechanisms in a material point











twin-free

Initial twin nucleation

the child propagation

twin growth due to twin shrinkage due to the parent propagation

detwinning











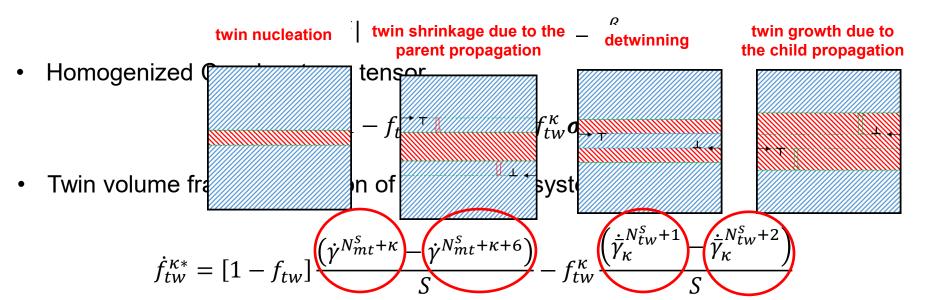
Multiplicative decomposition:

$$\mathbf{F} = \mathbf{F}^{\mathrm{e}mt} \mathbf{F}^{\mathrm{p}mt} = \mathbf{F}^{\mathrm{e}tw,k} \mathbf{F}^{\mathrm{p}tw,k}$$

Key idea of crystal plasticity

$$\mathbf{L}^{pmt} = \sum_{\alpha=1}^{N_s^{mt} + N_t^{mt}} \dot{\gamma}^{\alpha} \mathbf{S}^{\alpha} \operatorname{sign}(\tau^{\alpha}), \quad \mathbf{L}^{ptw,k} = \sum_{\beta=1}^{N_s^{tw} + N_t^{tw}} \dot{\bar{\gamma}}_{\kappa}^{\beta} \mathbf{S}_{k}^{\beta} \operatorname{sign}(\tau_{k}^{\beta})$$

Yield surface



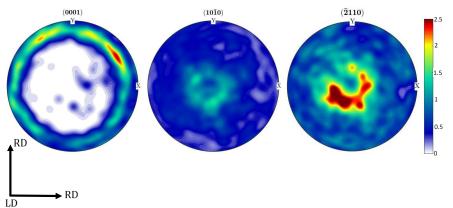


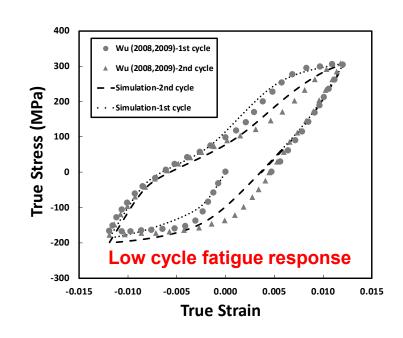




#### Mg alloy ZK60A sample (Wu et al., 2008,2009)

- Basal  $\langle a \rangle$  ( $\{0001\}\langle 11\bar{2}0 \rangle$ ), Prismatic  $\langle a \rangle$  ( $\{10\bar{1}0\}\langle 11\bar{2}0 \rangle$ ), and Pyramidal  $\langle c+a \rangle$  ( $\{\bar{1}\bar{1}22\}\langle \bar{1}\bar{1}23 \rangle$ ),
- Extension twin mode  $(\{10\overline{1}2\}\langle\overline{1}011\rangle)$





#### Calibrated values of crystal plasticity models

Mode	$s_0^{\alpha}$ (MPa)	$h_0^{\alpha}$ (MPa)	$s_s^{\alpha}$ (Mpa)	$\theta^{\alpha}$
Basal	20	10	21	2
Prismatic	140	20	155	2
Pyramidal <c+a></c+a>	240	1000	350	6
Twinning (operation A)	48	800	52	0
Twinning (operations B,C, D)	15	800	25	0

- $8 \times 9 \times 15$  FE cubic mesh
- Each element represents a single grain





PRISMS

#### Run the example of Cyclic deformation!!!

Copy the material model from plasticity/src/materialModels/crystalPlasticity/MaterialModels/RateIndependentAdvan cedTwinModel/calculatePlasticity.cc and paste it into the folder plasticity/src/materialModels/crystalPlasticity/.

Recompile the code!!! (it may not get recompiled appropriately just by make release!)

Go to folder plasticity/applications/crystalPlasticity/hcp/advancedTwinModel-Cyclic

Check the prm.prm file

Run the example





