Exercise 7 - Autumn 2013

TMT4185 Materialteknologi

All exercise numbers are from *Materials Science and Engineering*, 7th edition.

- 10.2 a) Rewrite the expression for the total free energy change for nucleation (Equation 10.1) for the case of a cubic nucleus of edge length a (instead of a sphere of radius r). Now differentiate this expression with respect to a (per Equation 10.2) and solve for both the critical cube edge length, a^* , and also ΔG^* .
 - b) Is ΔG^* greater for a cube or a sphere? Why?
- 10.20 Using the isothermal transformation diagram for a 1.13 wt% C steel alloy (Figure 10.39), determine the final microstructure (in terms of just the microconstituents present) of a small specimen that has been subjected to the following time–temperature treatments. In each case assume that the specimen begins at 920 °C and that it has been held at this temperature long enough to have achieved a complete and homogeneous austenitic structure.
 - a) Rapidly cool to 250 °C, hold for 10³ s, then quench to room temperature.
 - b) Rapidly cool to 775 °C, hold for 500 s, then quench to room temperature.
 - c) Rapidly cool to 400 °C, hold for 500 s, then quench to room temperature.
 - d) Rapidly cool to 700 °C, hold for 10⁵ s, then quench to room temperature.
 - e) Rapidly cool to 650 °C, hold at this temperature for 3 s, rapidly cool to 400 °C, hold for 25 s, then quench to room temperature.
 - f) Rapidly cool to 350 °C, hold for 300 s, then quench to room temperature.
 - g) Rapidly cool to 675 °C, hold for 7 s, then quench to room temperature.
 - h) Rapidly cool to $600\,^{\circ}$ C, hold at this temperature for 7 s, rapidly cool to $450\,^{\circ}$ C, hold for 4 s, then quench to room temperature.
- 10.27 Name the microstructural products of 4340 alloy steel specimens that are first completely transformed to austenite, then cooled to room temperature at the following rates:
 - a) $0.005 \, ^{\circ}\text{C/s}$
 - b) $0.05 \, ^{\circ}\text{C/s}$
 - c) $0.5 \, ^{\circ}\text{C/s}$
 - d) $5 \,^{\circ}\text{C/s}$

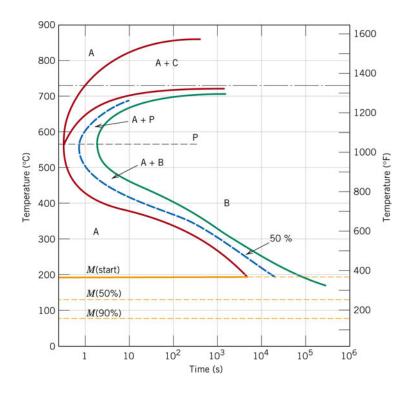


Figure 10.39: Isothermal transformation diagram for a 1.13 wt% C iron-carbon alloy: A, austenite; B, bainite; C, proeutectoid cementite; M, martensite; P, pearlite.

- 10.30 Briefly explain why fine pearlite is harder and stronger than coarse pearlite, which in turn is harder and stronger than spheroidite.
- 10D5 An alloy steel (4340) is to be used in an application requiring a minimum tensile strength of 1515 MPa (220,000 psi) and a minimum ductility of 40% RA. Oil quenching followed by tempering is to be used. Briefly describe the tempering heat treatment.
- 11.17 If it is assumed that, for steel alloys, the average cooling rate of the heat-affected zone in the vicinity of a weld is 10 °C/s, compare the microstructures and associated properties that will result for 1080 (eutectoid) and 4340 alloys in their HAZs.
- 11D15 A solution heat-treated 2014 aluminum alloy is to be precipitation hardened to have a minimum yield strength of 345 MPa (50,000 psi) and a ductility of at least 12%EL. Specify a practical precipitation heat treatment in terms of temperature and time that would give these mechanical characteristics. Justify your answer.

Hint: You need to use the graph from the 7th edition of the textbook for this problem (given on the next page).

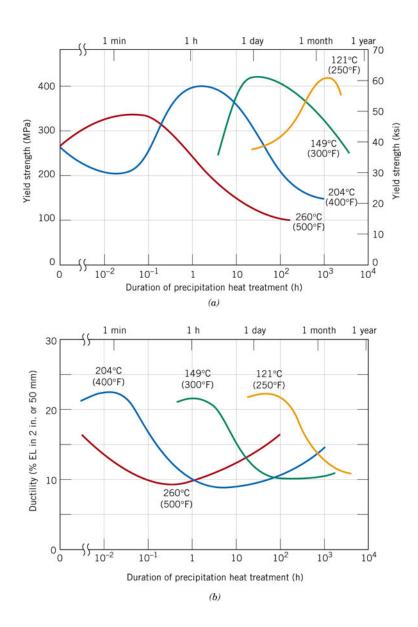


Figure 11.27: The precipitation hardening characteristics of a 2014 aluminum alloy (0.9 wt% Si, 4.4 wt% Cu, 0.8 wt% Mn, 0.5 wt% Mg) at four different aging temperatures: (a) yield strength, and (b) ductility (%EL).