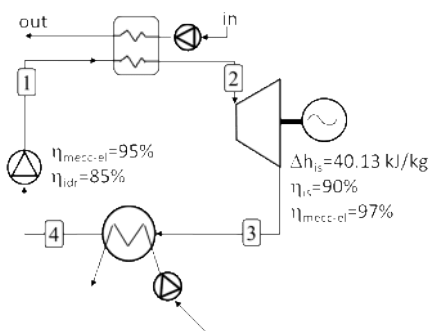
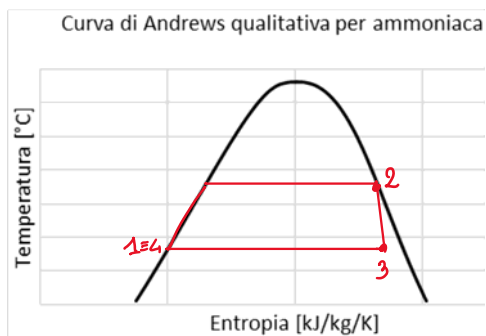


ESE 1

* CICLO RANKINE SOTTO (Liq. incoerente)

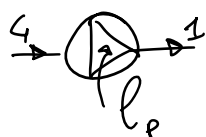
* DIFFERENZA PRESSIONE A CARICO DELLA POMPA NH₃

$$P_4 = P_{sat}(T_4 = 10^\circ\text{C}) = 6,15 \text{ bar}$$

$$P_2 = P_1 = P_{sat}(T_2 = 22^\circ\text{C}) = 9,13 \text{ bar}$$

$$\Delta P_{POMPA NH_3} = P_1 - P_4 = 2,97 \text{ bar}$$

} da tabelle NH₃

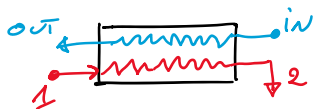
* h_1 ; m_{NH_3} ?

$$h_4 = h_{LS}(T_4 = 10^\circ\text{C}) = 389,7 \text{ kJ/kg}$$

$$\Delta h_{10} = \frac{\Delta P_{41}}{\rho} = 0,468 \text{ kJ/kg Liq. incoerente}$$

$$\Delta h_R = \frac{\Delta h_{10}}{\eta_{IDR}} = 0,551 \text{ kJ/kg}$$

$$h_1 = h_4 + \Delta h_R = 390,27 \text{ kJ/kg (usando Pura)}$$

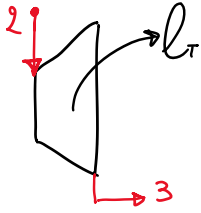


$$m_3(h_2 - h_1) = m_{in} c_{p,H_2O} \left(T_{in} - T_{out} \right) \quad \text{dato}$$

$$h_2 = h_{vs}(T = 22^\circ\text{C}) = 1624,68 \frac{\text{kJ}}{\text{kg}} \quad (\text{ciclo Rankine SOTTO})$$



$$\dot{m}_3 = \frac{\dot{m}_{in} C_{p,H_2O} (T_{in} - T_{out})}{(h_2 - h_1)} = 122,08 \text{ Kg/s}$$



$$h_{3,15} = h_2 - \Delta h_{is} = 1584,55 \text{ KJ/kg}$$

$$\eta_{15} = \frac{\Delta h_{15}}{\Delta h_{is}} = \frac{h_2 - h_{3,15}}{h_2 - h_{3,15}} = 0,9$$

↓

$$h_3 = 1588,57 \text{ KJ/kg}$$

$$h_3 = h_{L5}(T=10^\circ\text{C}) + (h_{vs} - h_{L5}) \bigg|_{T=10^\circ\text{C}} X_3$$

↓

$$X_3 = 0,9782 \quad \left(\text{TITOLO SCARICO TURBINA} \right)$$

* POTENZA POURE PRELIEVO H₂O MARE *

$$P_{POURE H_2O} = \left(\frac{\Delta P_{CACCIA}}{\sum \eta_{10R}} \cdot \dot{m}_{CACCIA} + \frac{\Delta P_{FREDDA}}{\sum \eta_{10R}} \cdot \dot{m}_{FREDDA} \right) / \eta_{MECC-EL} = 1555,8 \text{ KW}$$

* POTENZA NETTA *

$$P_{NETTA} = \dot{m}_{NH_3} (h_2 - h_3) \eta_{MECC-EL TURB} - \dot{m}_{NH_3} (h_1 - h_4) \eta_{MECC-EL POMP} - P_{POURE H_2O} = 2650,3 \text{ KW}$$

\downarrow
 $P_{EL,TUR} = 4276,3 \text{ KW}$

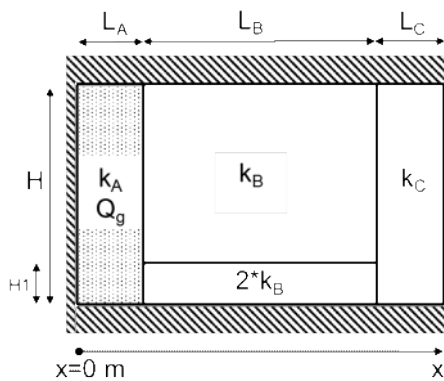
\downarrow
 $P_{POMPA, NH_3} = 70,8 \text{ KW}$

* IL RENDIMENTO IDEALE COINCIDE CON QUELLO DEL CICLO

DI CARNOT OPERANTE TRA T_{CACCIA} E T_{FREDDA}

$$\eta_{CARNOT} = 1 - \frac{T_{FREDDA} [K]}{T_{CACCIA} [K]} = 0,08$$

ESE 2*



$$T_{\infty} = 25^{\circ}\text{C}$$

Aria in quiete
(conv. NATURALE)

* $h_{\text{conv}}?$ CONV. NATURALE

$$Nu = 0,59 Ra^{0,25} = 0,59 (Gr \cdot Pr)^{0,25} \quad (\text{convezione})$$

$$Pr = \frac{c_p \mu}{K} \Big|_{\text{aria}} = 0,722$$

$$Gr = \frac{\rho \beta (T_{\text{parete}} - T_{\infty}) H^3}{\left(\frac{\mu}{\rho}\right)^2} = 3,02 \cdot 10^{10}$$

ASSUMENDO Aria come gas perfetto $\rightarrow \beta = \frac{1}{T_{\text{film}}} = \frac{1}{\frac{T_{\text{parete}} + T_{\infty}}{2}} = 0,00287 \frac{1}{K}$

$$\rho_{\text{aria}} = \frac{P}{R_{\text{aria}} \cdot T_{\text{film}}} = 1,0116 \text{ kg/m}^3$$

$$Nu = 0,59 (Gr \cdot Pr)^{0,25} = \frac{h_{\text{conv}} \cdot L_c}{K} \Rightarrow h_{\text{conv}} = 3,78 \text{ W/m}^2\text{K}$$

* $q_{\text{GEN}} \text{ [W/m}^3\text{]}?$ (generazione interna di potenza volumetrica)

$$\dot{Q}_{\text{conv}} = h_{\text{conv}} A_{\text{scambio}} (T_{\text{parete}} - T_{\infty}) = h_{\text{conv}} H \cdot \text{SPERS} (T_{\text{parete}} - T_{\infty}) = 566,82 \text{ W}$$

$$\dot{Q}_{\text{GEN}} = \dot{Q}_{\text{conv}} \quad (\text{STAZIONARIETÀ})$$

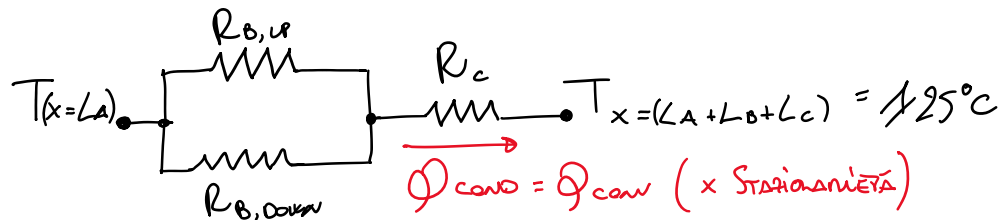
$$q_{GEN} = \frac{\dot{\Phi}_{GEN}}{V} = \frac{\dot{\Phi}_{GEN}}{L_A \cdot H \cdot S_{PRESS}} = 755,8 \text{ W/m}^3$$

* CALCOLO $T(x=L_A)$?

$$R_{B,UP} = \frac{L_B}{S_{PRESS} \cdot K_B (H - H_2)} = 0,3077 \frac{K}{W} \quad R_{B,DOWN} = \frac{L_B}{2 K_B H_2 \cdot S_{PRESS}} = 1 \frac{K}{W}$$

$$R_C = \frac{L_C}{K_C H \cdot S_{PRESS}} = 0,0067 \frac{K}{W}$$

* SCHEMA RESISTENZE *



$$T(x=L_A+L_B) = 125^\circ C + R_C \cdot \Phi_{COND} = 128,78^\circ C$$

— RESISTENZE PARALLELO $R_{B,UP}; R_{B,DOWN}$

$$R_B = \left(\frac{1}{R_{B,UP}} + \frac{1}{R_{B,DOWN}} \right)^{-1} = 0,2353 \frac{K}{W}$$

$$T(x=L_A) = T(x=L_A+L_B) + R_B \cdot \Phi_{COND} = 262,15^\circ C$$