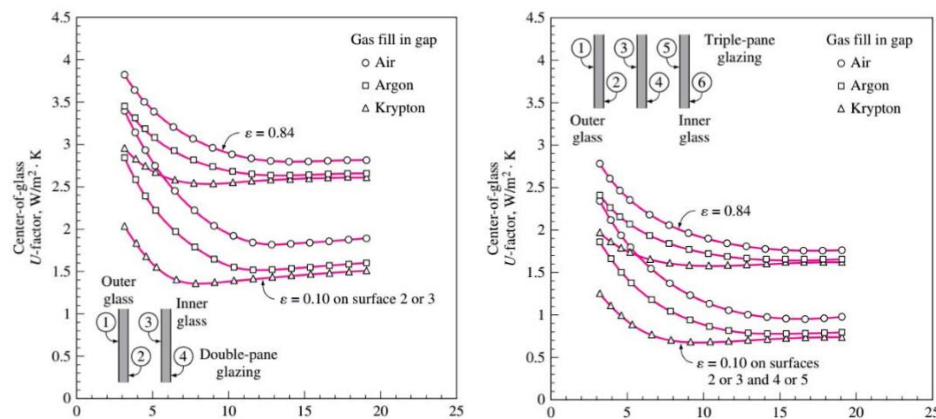


Week8 Assignment

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Task 1 Using the diagrams given in the presentation calculate how much (%) is the effect of applying different modifications (changing the gas, adding an extra pane, using a low emissivity coating) on the U value with respect to a benchmark case of double layer with air and no coating? (keep the gap thickness to be 13 mm)



(1) Changing the gas:

By changing the gas filled in the gap from air to argon, the U of the center of the glass decreases from $2.8 \frac{W}{m^2 K}$ to $2.7 \frac{W}{m^2 K}$, which means the U decreases 4.57%.

By changing the gas filled in the gap from air to krypton, the U of the center of the glass decreases from $2.8 \frac{W}{m^2 K}$ to $2.6 \frac{W}{m^2 K}$, which means the U decreases 7.14%.

(2) Adding an extra pane:

The U of the center of the glass decreases from $2.8 \frac{W}{m^2 K}$ to $1.8 \frac{W}{m^2 K}$, which means the U decreases 35.71%.

(3) Using a low emissivity coating:

When the glass surfaces are coated with a film that has an emissivity of 0.1,

The U of the center of the glass decreases from $1.8 \frac{W}{m^2 K}$ to $1 \frac{W}{m^2 K}$, which means the U decreases 35.71%.

Task 2 Consider the house that we analyzed in the last two examples, calculate the heating and cooling load of the other windows which are fixed 14.4 m² on the west, fixed 3.6 m² on the south and an operable 3.6 m² on the south (the same window and frame type). How much does the total value change if I change the frame of the window from wooden one to aluminium ?

PIACENZA, Italy

WMO#: 160840

Lat: 44.92N Long: 9.73E Elev: 138 StdP: 99.68 Time Zone: 1.00 (EUW) Period: 89-10 WBAN: 99999

Annual Heating and Humidification Design Conditions

Coldest Month	Heating DB		Humidification DP/MCDB and HR						Coldest month WS/MCDB				MCWS/PCWD to 99.6% DB	
			99.6%			99%			0.4%		1%			
	99.6%	99%	DP	HR	MCDB	DP	HR	MCDB	WS	MCDB	WS	MCDB	MCWS	PCWD
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)
1	-6.2	-4.8	-11.6	1.4	3.1	-8.8	1.8	1.8	8.8	5.6	7.7	6.2	2.1	250

(1)

Annual Cooling, Dehumidification, and Enthalpy Design Conditions

Hottest Month	Hottest Month DB Range	Cooling DB/MCWB						Evaporation WB/MCDB						MCWS/PCWD to 0.4% DB	
		0.4%		1%		2%		0.4%		1%		2%			
		DB	MCWB	DB	MCWB	DB	MCWB	WB	MCDB	WB	MCDB	WB	MCDB	MCWS	PCWD
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)
8	11.9	33.1	22.7	31.9	22.4	30.3	21.8	24.6	30.2	23.7	29.2	22.9	28.3	2.4	90

(2)

Table 13 Fenestration Solar Load Factors FF_s

Exposure	Single Family Detached	Multifamily
North	0.44	0.27
Northeast	0.21	0.43
East	0.31	0.56
Southeast	0.37	0.54
South	0.47	0.53
Southwest	0.58	0.61
West	0.56	0.65
Northwest	0.46	0.57
Horizontal	0.58	0.73

Table 10 Peak Irradiance, W/m²

Exposure		Latitude							
		20°	25°	30°	35°	40°	45°	50°	55° 60°
North	E _D	125	106	92	84	81	85	96	112 136
	E _d	128	115	103	93	84	76	69	62 55
	E _t	253	221	195	177	166	162	164	174 191
Northeast/Northwest	E _D	460	449	437	425	412	399	386	374 361
	E _d	177	169	162	156	151	147	143	140 137
	E _t	637	618	599	581	563	546	529	513 498
East/West	E _D	530	543	552	558	560	559	555	547 537
	E _d	200	196	193	190	189	188	187	187 187
	E _t	730	739	745	748	749	747	742	734 724
Southeast/Southwest	E _D	282	328	369	405	436	463	485	503 517
	E _d	204	203	203	204	205	207	210	212 215
	E _t	485	531	572	609	641	670	695	715 732
South	E _D	0	60	139	214	283	348	408	464 515
	E _d	166	193	196	200	204	209	214	219 225
	E _t	166	253	335	414	487	557	622	683 740
Horizontal	E _D	845	840	827	806	776	738	691	637 574
	E _d	170	170	170	170	170	170	170	170 170
	E _t	1015	1010	997	976	946	908	861	807 744

$$\Delta T_{\text{cooling}} = 31.9 - 24 = 7.9^{\circ}\text{C}$$

$$\Delta T_{\text{heating}} = 20 - (-4.8) = 24.8^{\circ}\text{C}$$

$$DR=11.9^{\circ}\text{C}$$

The cooling load of the fixed window on the west:

$$A=14.4 \text{ m}^2$$

$$CF_{\text{window}_{\text{west}}(\text{Heat Transfer})} = U_{\text{window}_{\text{west}}} (\Delta T_{\text{cooling}} - 0.46DR)$$

$$= 2.84 \times (7.9 - 0.46 \times 11.9) = 6.89 \frac{\text{W}}{\text{m}^2}$$

$$CF_{\text{window}_{\text{west}}(\text{Irradiation})} = \text{PXi} \times \text{SHGC} \times \text{IAC} \times \text{FF}_s$$

$$Q_{\text{window}_{\text{west}}} = CF_{\text{window}_{\text{west}}} \times A_{\text{window}_{\text{west}}}$$

$$= [CF_{window_{west}(Heat\ Transfer)} + CF_{window_{west}(Irradiation)}] \times A_{window_{west}}$$

$$= (6.89 + 747 \times 0.54 \times 1 \times 0.56) \times 14.4 = 3352.1\text{ W}$$

The heating load of the fixed window on the west:

$$Q_{window_{west}} = HF_{window_{west}} \times A_{window_{west}}$$

$$= U_{window_{west}} \times \Delta T_{cooling} \times A_{window_{west}}$$

$$= 2.84 \times 24.8 \times 14.4 = 1014.2\text{ W}$$

When the frame are to be aluminium,

$$U_{window_{west}} = 3.61 \frac{\text{W}}{\text{m}^2 \text{ K}}, HAGC = 0.56$$

$$CF'_{window_{west}(Heat\ Transfer)} = U'_{window_{west}} (\Delta T_{cooling} - 0.46DR)$$

$$= 3.61 \times (7.9 - 0.46 \times 11.9) = 8.76 \frac{\text{W}}{\text{m}^2}$$

$$\text{Cooling Load: } Q'_{window_{west}} = CF'_{window_{west}} \times A_{window_{west}}$$

$$= [CF'_{window_{west}(Heat\ Transfer)} + CF'_{window_{west}(Irradiation)}] \times A_{window_{west}}$$

$$= (8.76 + 747 \times 0.54 \times 1 \times 0.56) \times 14.4 = 3499.5\text{ W}$$

$$\text{Heating Load: } Q'_{window_{west}} = HF'_{window_{west}} \times A_{window_{west}}$$

$$= U'_{window_{west}} \times \Delta T_{heating} \times A_{window_{west}}$$

$$= 3.61 \times 24.8 \times 14.4 = 1289.2\text{ W}$$

The cooling load of the fixed window on the south:

$$A = 3.6\text{ m}^2$$

$$CF_{window_{south}(Heat\ Transfer)} = U_{window_{south}} (\Delta T_{cooling} - 0.46DR)$$

$$= 2.84 \times (7.9 - 0.46 \times 11.9) = 6.89 \frac{\text{W}}{\text{m}^2}$$

$$CF_{window_{south}(Irradiation)} = PXI \times SHGC \times IAC \times FF_s$$

$$Q_{window_{south}} = CF_{window_{south}} \times A_{window_{south}}$$

$$= [CF_{window_{south}(Heat Transfer)} + CF_{window_{south}(Irradiation)}] \times A_{window_{south}}$$

$$= (6.89 + 557 \times 0.54 \times 1 \times 0.47) \times 3.6 = 553.7 \text{ W}$$

The heating load of the fixed window on the south:

$$Q_{window_{south}} = HF_{window_{south}} \times A_{window_{south}}$$

$$= U_{window_{south}} \times \Delta T_{heating} \times A_{window_{south}}$$

$$= 2.84 \times 24.8 \times 3.6 = 253.6 \text{ W}$$

When the frame are to be aluminium,

$$U_{window_{south}} = 3.61 \frac{\text{W}}{\text{m}^2 \text{ K}}, HAGC = 0.56$$

$$CF'_{window_{south}(Heat Transfer)} = U'_{window_{south}} (\Delta T_{cooling} - 0.46DR)$$

$$= 3.61 \times (7.9 - 0.46 \times 11.9) = 8.76 \frac{\text{W}}{\text{m}^2}$$

$$\text{Cooling Load: } Q'_{window_{south}} = CF'_{window_{south}} \times A_{window_{south}}$$

$$= [CF'_{window_{south}(Heat Transfer)} + CF'_{window_{south}(Irradiation)}] \times A_{window_{south}}$$

$$= (8.76 + 557 \times 0.54 \times 1 \times 0.47) \times 3.6 = 559.3 \text{ W}$$

$$\text{Heating Load: } Q'_{window_{south}} = HF'_{window_{south}} \times A_{window_{south}}$$

$$= U'_{window_{west}} \times \Delta T_{heating} \times A_{window_{west}}$$

$$= 3.61 \times 24.8 \times 3.6 = 322.3 \text{ W}$$

The cooling load of the operable window on the south:

$$A = 3.6 \text{ m}^2$$

$$CF_{window_{south}(Heat Transfer)} = U_{window_{south}} (\Delta T_{cooling} - 0.46DR)$$

$$= 2.87 \times (7.9 - 0.46 \times 11.9) = 6.96 \frac{\text{W}}{\text{m}^2}$$

$$CF_{\text{window}_{\text{south}}(\text{Irradiation})} = \text{PXi} \times \text{SHGC} \times \text{IAC} \times \text{FF}_s$$

$$Q_{\text{window}_{\text{south}}} = CF_{\text{window}_{\text{south}}} \times A_{\text{window}_{\text{south}}}$$

$$= [CF_{\text{window}_{\text{south}}(\text{Heat Transfer})} + CF_{\text{window}_{\text{south}}(\text{Irradiation})}] \times A_{\text{window}_{\text{south}}}$$

$$= (6.96 + 557 \times 0.46 \times 1 \times 0.47) \times 3.6 = 458.6 \text{ W}$$

The heating load of the operable window on the south:

$$Q_{\text{window}_{\text{south}}} = HF_{\text{window}_{\text{south}}} \times A_{\text{window}_{\text{south}}}$$

$$= U_{\text{window}_{\text{south}}} \times \Delta T_{\text{heating}} \times A_{\text{window}_{\text{south}}}$$

$$= 2.87 \times 24.8 \times 3.6 = 256.2 \text{ W}$$

When the frame are to be aluminium,

$$U_{\text{window}_{\text{south}}} = 4.62 \frac{\text{W}}{\text{m}^2 \text{ K}}, \text{HAGC} = 0.55$$

$$CF'_{\text{window}_{\text{south}}(\text{Heat Transfer})} = U'_{\text{window}_{\text{south}}} (\Delta T_{\text{cooling}} - 0.46DR)$$

$$= 4.62 \times (7.9 - 0.46 \times 11.9) = 11.21 \frac{\text{W}}{\text{m}^2}$$

$$\text{Cooling Load: } Q'_{\text{window}_{\text{south}}} = CF'_{\text{window}_{\text{south}}} \times A_{\text{window}_{\text{south}}}$$

$$= [CF'_{\text{window}_{\text{south}}(\text{Heat Transfer})} + CF'_{\text{window}_{\text{south}}(\text{Irradiation})}] \times A_{\text{window}_{\text{south}}}$$

$$= (11.21 + 557 \times 0.55 \times 1 \times 0.47) \times 3.6 = 558.7 \text{ W}$$

$$\text{Heating Load: } Q'_{\text{window}_{\text{south}}} = HF'_{\text{window}_{\text{south}}} \times A_{\text{window}_{\text{south}}}$$

$$= U'_{\text{window}_{\text{west}}} \times \Delta T_{\text{heating}} \times A_{\text{window}_{\text{west}}}$$

$$= 4.62 \times 24.8 \times 3.6 = 412.5 \text{ W}$$