30 -015- 33900

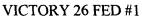
Submit in duplicate to appropriate district office. See Rule 401 & Rule 1122

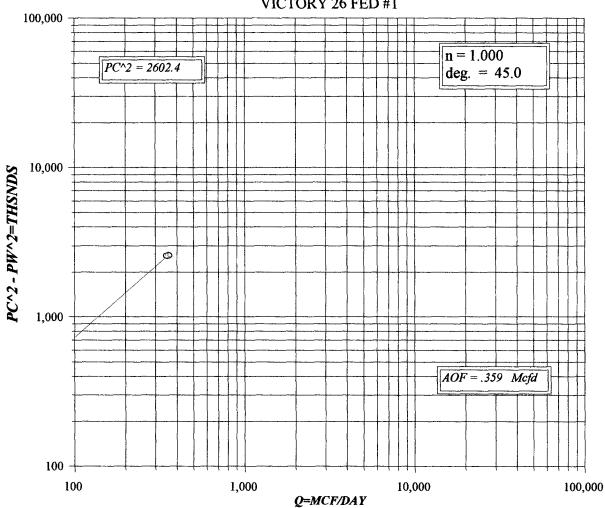
Form C-122

State of New Mexico
Energy Minerals and Natural Resources
Oil Conservation Division
2040 South Pacheco Revised October, 1999

							Santa F	e, NM			₹.	Co	i Im					
			MULT	IPOIN	TAN	D ONE PO	INT B	ACK	PRESSURE	TES	ST FOR G	AS V	VELL					
perat	or			MEWE	3OUR1	NE OIL			Lease or Unit Name				VICTORY 26 FED					
уре Т						· · · · · · · · · · · · · · · · · · ·	Test Date					Well No.						
omnl	✓ Initial		Annual Total Depti		Specia		Plug Back TD Ele				5/11/20 Elevation	05	- Rae					
5/7/2005 11670												Unit Ltr - Sec - TWP - Rge A 26-20S-28E						
Csg. S		Vt.		Set At			Perforations:							County				
	5 1/2 17 4.892				116	70	From: 11422 To:			11498			EDDY					
lbg. S	1	Vt.	\$ \$	Set At			Perforations:					Pool						
	7/8	6.5	2.44	60.14	110	01	From: To:					BURTON FLAT						
Type \	Well-Single	-Bradenh	ead-G.G. or SIN		ultiple			Packer Set At 10961					Formation MORROW					
	cing Thru	Res	ervoir Temp		an Ann	ual Temp.	Baro. PressPa					Connec			SALES			
<u> </u>	TUBING	1	181	Gg   %CO <sub>2</sub>			  %N <sub>2</sub>	$\frac{13.2}{\% N_2}$ $\frac{13.2}{\% H_2 S}$ Prov			r	Meter	Run	Taps				
H 11001 11001				0.606 0.909				0.248 0			N/A				FLG			
·····				OW DA Press						NG DATA			ASING	DATA	Duration			
	Size Size		1			Diff.	Temp.		Press p.s.i.g.	Temp	3	Press p.s.i.g.		Temp.	of			
			·		<b></b>			<u> </u>					Flow					
SI	20.37.1000			- 10			77		1600						OA IVD C			
1	3.0 X 1.000			13	8	15.4	<b></b>		134	<del> </del>		<del> </del>			24 HRS			
3							<del>                                     </del>		<del> </del>		<del></del>							
4							<del>                                     </del>		<del> </del>	<del> </del> -								
5							<del>                                     </del>			T								
						RATE	OF FLO	OW C	ALCULATIO	NS								
No.	COEFFICIENT				_	Pressure	Flow Temp.				Super Compress			Rate of Flow				
	(24 Hour) 7.77			$h_{\mathbf{w}}P_{\mathbf{m}}$ $P_{\mathbf{m}}$			Fact	Gravity Factor	or F <sub>g</sub> Factor l			r F pv Q. Mcfd 355						
2		1.11					├								333			
3	<u> </u>	····		TOT	AL	FLOW	ME	TER	<del> </del>			·····	<del></del> .					
4				<del></del>			<del>                                     </del>					···						
5																		
No.	$P_r$ Temp. R $T_r$ Z				Z	Gas Liquid Hydrocarbon Ratio					N/A Mcf bbl.							
1_	<b> </b>						-	Gravity of Liquid Hydrocarbons					N/A Deg.					
2	TOTAL PLOW						Specific Gravity Separator Gas					0.606 XXXXXXX						
3	IOIA					<b>⊣</b> "	Specific Gravity Flowing Fluid N/A Critical Pressure 675					P.S.I.A. N/A P.S.I.A.						
5	<del> </del>			ļ			-1	l Tempe			354	_ F.S	R.	N/A	P.S.I.A. R			
Pc	161	3.2	P <sub>c</sub> 2	2602.	4	<del></del>	Citaca	richipe	Tatule				10,	14/11				
No.	$P_t^2$		$P_{\mathbf{w}}$	$P_{v}$		$P_c^2 - P_w^2$	(1)		$P_{a}^{2} =$		1.011	(2)	P	$n = \frac{1}{2}$	1.011			
1	1		165.3	27		2575.1	<b> </b> (		$P_c^2 =$		<del></del>	(2)		$\begin{bmatrix} 2 \\ c \end{bmatrix}^n =$				
2	<del>                                     </del>			<b></b>			4	]	$\overline{P_c^2 - P_w^2}$				$P_c^2$ -					
. 3	<del>                                     </del>						1	AOF	= 0		$P_0^2$ $\int_0^n =$		0.359					
	4						AOF = Q											
5		-					1				$P_c^2 - P_w^2$							
	lute Open F	low		0.359]		Mcfd	@ 15.02	5	Angle of Slope		υ - w _	45		Slope, n:	1			
Rema							~		BO 13 BW		······································			<u>• • • • • • • • • • • • • • • • • •</u>				
	oved By Di	vision:	<del>,</del>	Conduc									necked By:					
<u> </u>	·			<u> </u>	-	VBOURNE		MERV BUECKER					MB					

## **MEWBOURNE OIL**





	UNIT :			SECTION :			TOWNSHII	205	   1		1613.2	Pc2 =	2602.4	1
	L:		H :		L/H		G/GMIX :	0.606	16	Pt2 =	21.7	Pw =	165.3	-ii
	%CO2 :		%N2 :	0.248	H2\$ :				: 5/11/05	l	0.0		#DIV/0!	*11
	d :			0.018183	GH .			RANGE :	: 28E #	l	0.0		#DIV/0!	•11
				*********			=======================================	*********	=======================================	II	0.0		#DIV/0!	*11
	VOL 1:	355	PSIA 1 :	147.2			RESV.TEMP	4000	ij	!				*H
	VOL 2		PSIA 2	147.2			KESV.IEMP	196.0	ii.	Pc2-Pw2≃	2575.1	Pw2 =	27.3	*((
	VOL 3:		PSIA 3				SHUT-IN PRI =	1613.2	H	!	#DIV/0!		#DIV/0!	*
	VOL 4		PSIA 4				Shorat PRI	1013.2	į.		#DIV/0!		#DIV/0!	•#
									ll 0	l :	#DIV/0!		#DIV/0!	*!!
				PCR :	675				11 11	, ,	n =	1.000		*
				TCR :					11			1.000		*
									** !!	Pc2/(Pc2-P	w2) =	1.011		*11
	LINE	RATE 1	l E	RATE 2		RATE 3	1 :	RATE 4	1 11		, -	#DIV/0!		*
	1	l į	l t			ŧ	1		i ü	i		#DIV/OI		*
	i	1ST	`2ND	'1ST	"2ND	1ST	'2ND	`1ST	'2ND			#DIV/0!		'n
				1		!	1		i ii					÷ii
1	QM (I	0.355	0.355 (	0.000 (	0.000	0.000	0.000	0.000	0.000	İ				-ii
2	TW I	534	534	534	534	534	534	534	534		w2]n =	1.011		٠ii
3	Ts [	656.0	656.0	656.0	656.0	656.0	656.0	656.0	[ 656.0 ]			#DIV/0!		÷Ϊ
٩,	T II	595.0	595.0	595.0	595.0	595.0	595.0	595.0	[ 595.0 j	1		#D!V/01		•11
PR (est)   5 Z(est)		0.22	2050	0.00		0.00	!	0.00	J II			#DIV/0!		-11
6	L(est)    TZ	0.961	0.958	#DIV/0!	#DIV/0!	#DIV/0I	#DIV/01	#DIV/0!	#DIV/0!					-11
7	GH/TZ	571.8 1 14.336	569.8	#DIV/0!	#DIV/01	#DIV/0!	#DIV/01	#DIV/01	] #DIV/0! [[		AOF≈ Q	0.359		1
8	eS II	1.712	14.386   1.715	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/01	#DIV/0!	l		#DIV/0!		*11
9	i-e-S	0.418	0.417	#DIV/0!	#DIV/0!   #DIV/0!		#DIV/01		,			#DIV/0!		*(1
10	Pt II	147.2	147.2	0.0	0.0	) #DIV/0! I 0.0	] #DIV/0!   1 0.0	#DIV/0I	#DIV/0!			#DIV/0!		*
	Pt2/1000 II		21.7	0.0	0.0	1 0.0	1 0.0	0.0 0.0	i 0.0 li					*11
12	Fr ii	0.018183	0.018183	0.018183	0.018183	0.018183	0.018183		0.0					*11
13	Fc=FrTZ	10.397	10.361	#DIV/0!	#DIV/0!	#DIV/01	#DIV/01	#DIV/0!	0.018183      #DIV/0!					*11
14	FcQm		3,68	#DIV/0!	#DIV/OI	#DIV/0!	#DIV/0!	#DIV/0!						-11
15 L	/H(FcQm);	13.6	13.5	#DIV/0!	#DIV/OI	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!      #DIV/0!					*((
16	Fw	5.664882	5.640272	#DIV/01	#DIV/OI	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!					-11
17	Pw2	27.3	27.3	#DIV/0!	#DIV/OI	#DIV/01	#DIV/0!	#DIV/0!	#DIV/01	i I				*1
18	Ps2	46.8	46.8	#DIV/0!	#DIV/0!	#DIV/01	#DIV/0!	#DIV/0!	#DIV/0!	ì				*11
19	Ps	216.3	216.4	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/01	#DIV/0!					-11
20	P	181.8	181.8	#DIV/0!	#DIV/0!	#DIV/OI	#DIV/01	#DIV/Q!	#DIV/Q!					-11
21	Pr	0.27	0.27	#DIV/0!	#DIV/0!	#DIV/01	#DIV/01	#DIV/0!	#DIV/0!					-11
22	Tr	1.68	1. <del>6</del> 8	1.68	1.68	1.68	1.68	1.68	1.68	İ				-11
23	Z	0.958	0.958 Į	#DIV/0! {	#D(V/Q)	#DIV/0!	[ #DIV/0!	#DIV/OI	#DIV/OI II	i		FORM C122-I	0	*55