

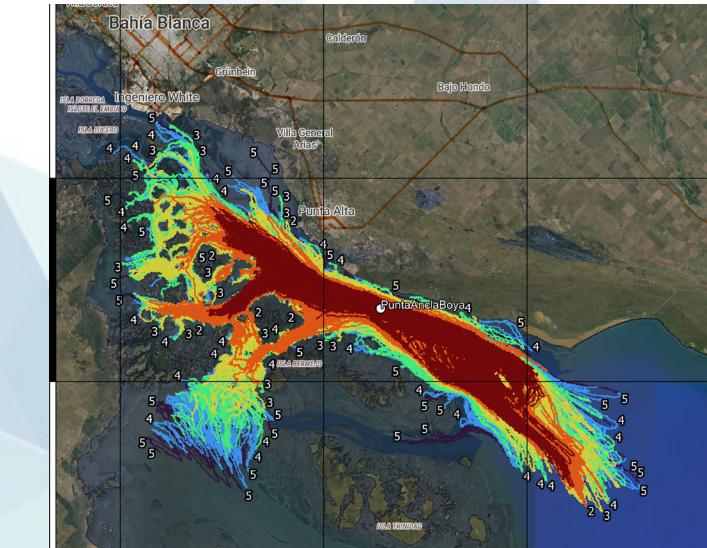
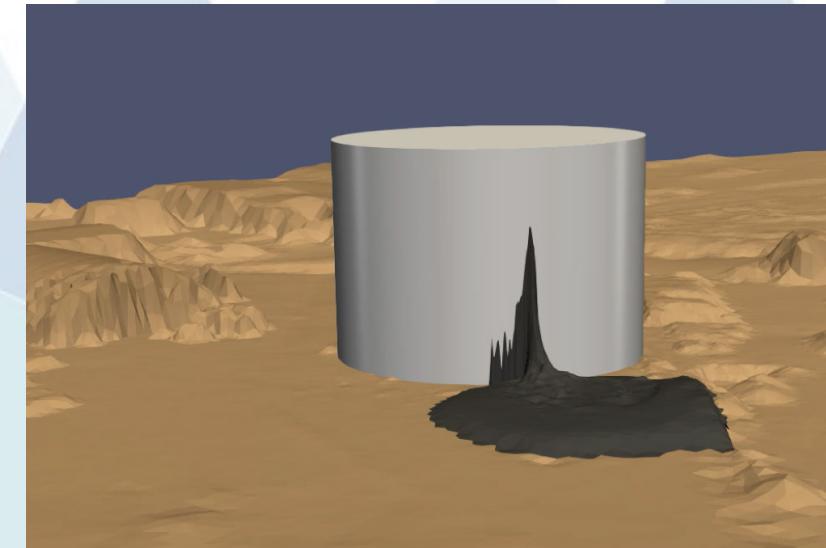
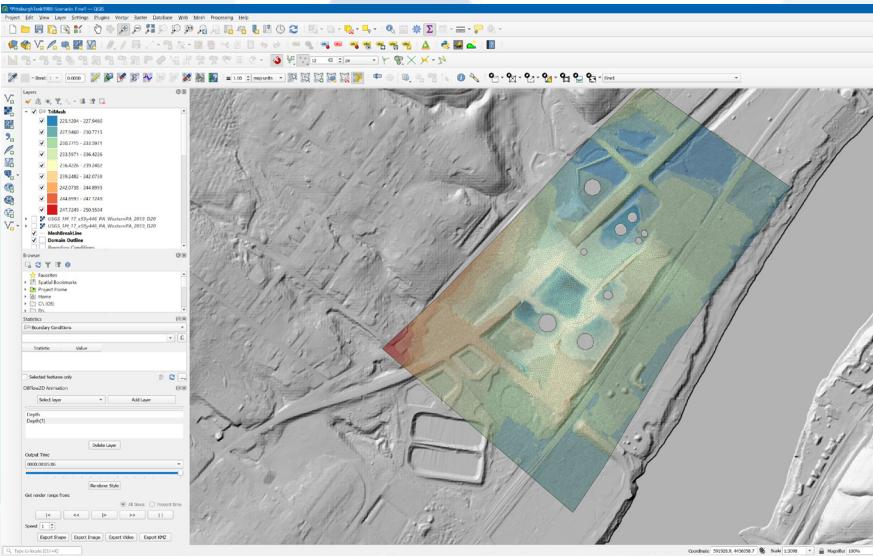
RESCUER W2 TRAINING PROGRAMME

WORKSHOP 2 UNIZAR ORGANIZATION



Universidad
Zaragoza

CHG



Industrial application of GPU codes

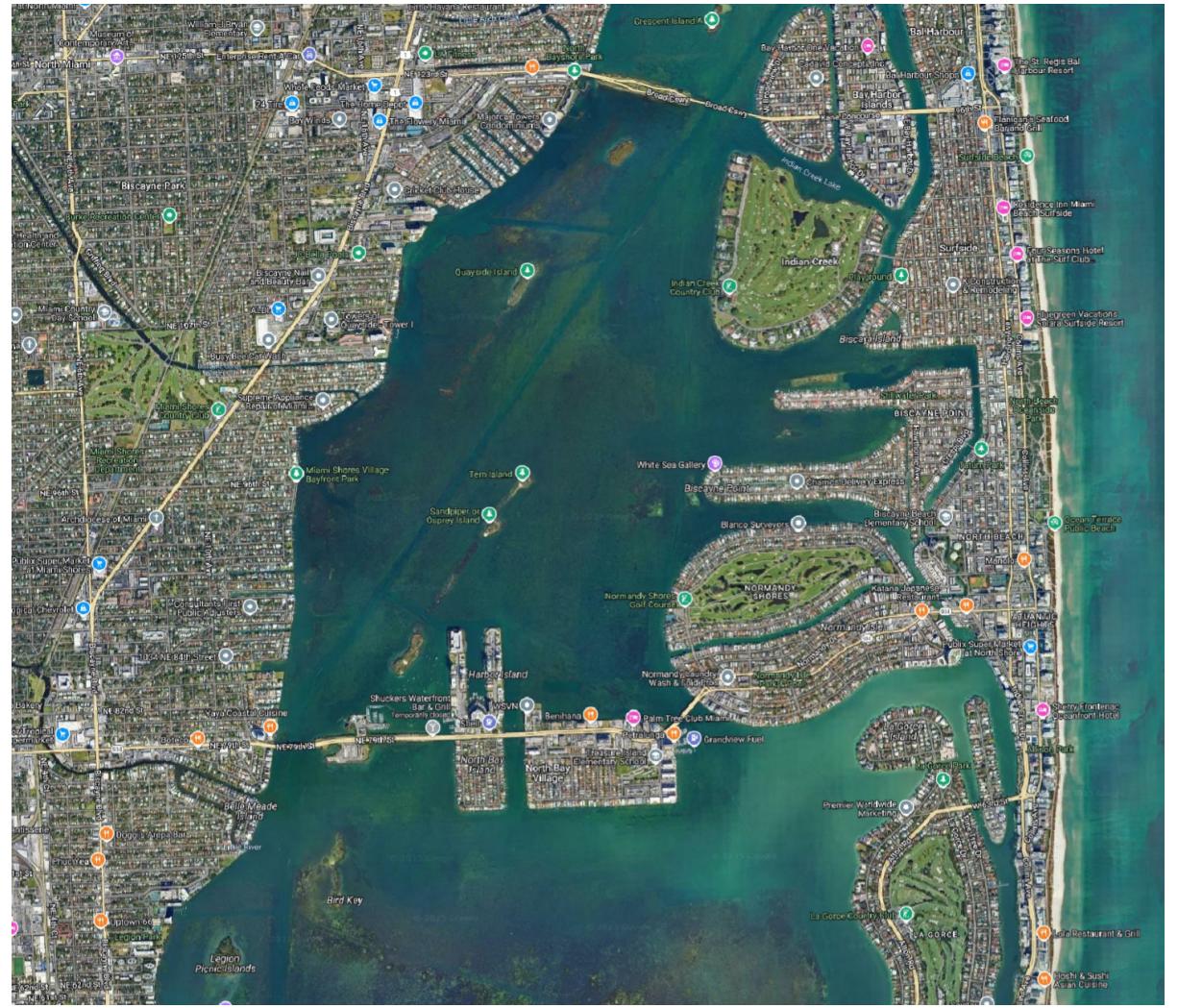
Reinaldo GARCIA, PhD

Director of Development and Applications
Hydronia, FL, USA. Hydronia Europe, Spain.

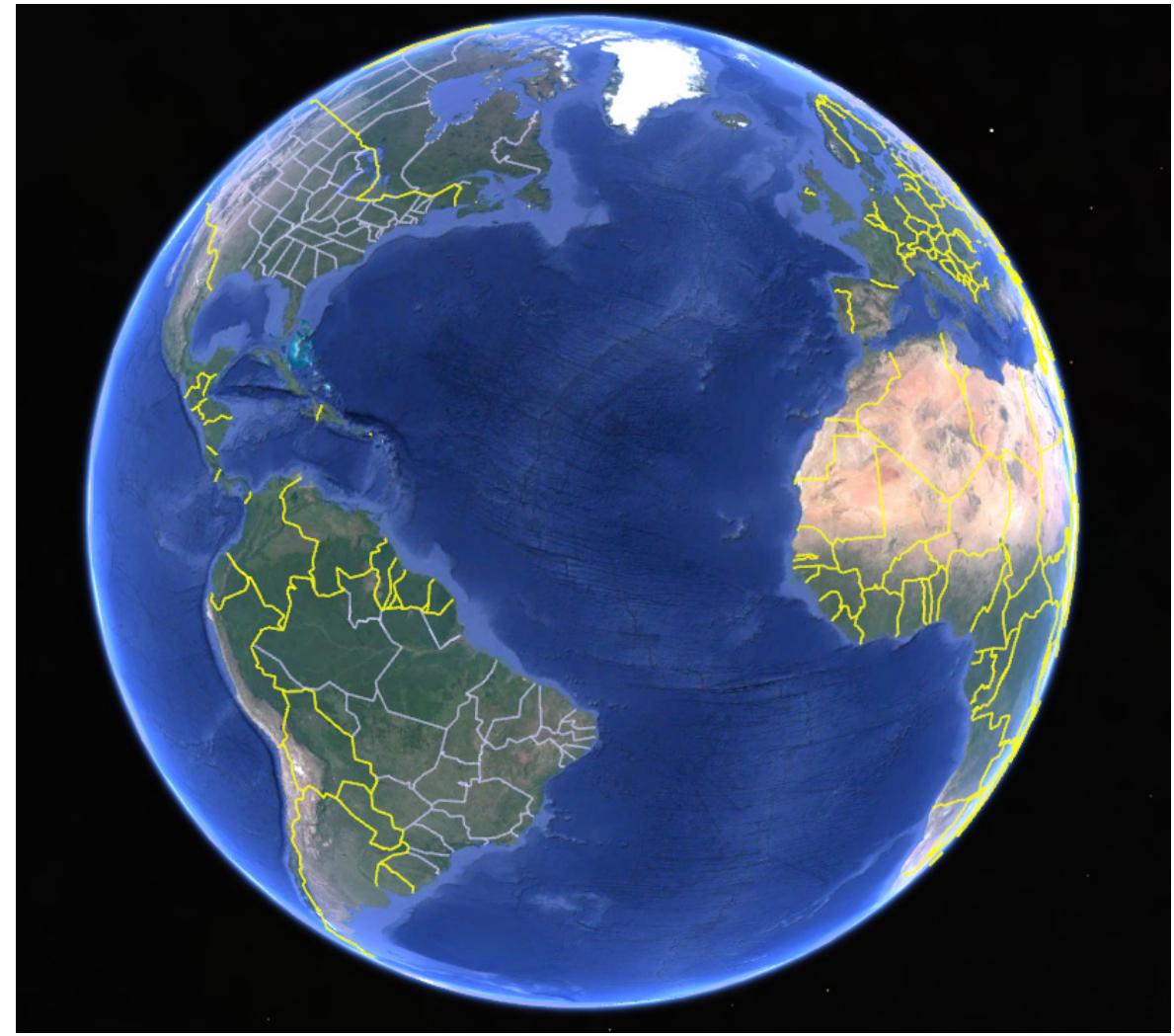
rey@hydronia.com

www.hydronia.com

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VS



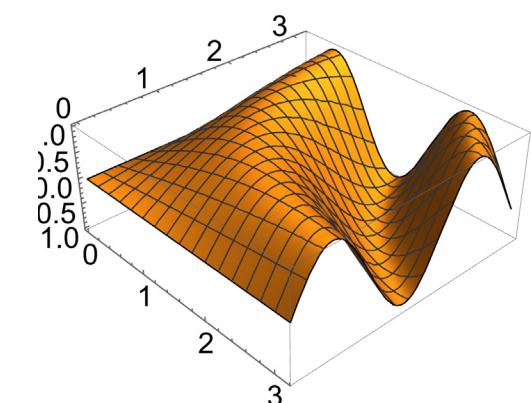
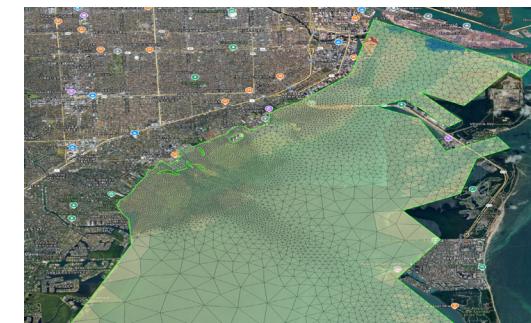
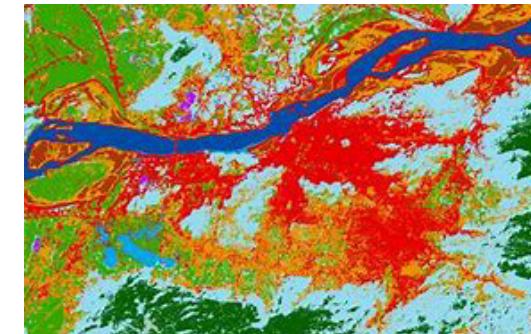
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Agenda

- Factors Impacting the Modeling Process
- RiverFlow2D/OilFlow2D Modeling Systems
- Three Case Studies [*“Real World” Applications*]
 - The sudden break of a large tailings dam
 - The dynamics of a large sub-tropical bay
 - Oil Pipelines and the break of an oil storage tank
- Discussion, questions, and attempt to provide answers.

Factors Affecting Cost/Effort of Industrial Modeling Applications

- Software cost
- Computer Hardware and Additional Software
- GIS Pre-processing (data processing)
- Model Conceptualization
- Model Setup
- Numerical Stability and Consistency
- ***Model Performance (Runtime)***
- Analysis of Results
- GIS post-processing



Total Cost of a Modeling Project



Factor affecting modeling cost	Cost	~ % of Total Effort
Software		??
Computer and Additional Software		??
GIS Pre-processing		??
Model Conceptualization		??
Model Setup		??
Numerical Stability and Consistency		??
Model Performance		??
Analysis of Results		??
GIS Post-processing		??
Total		100

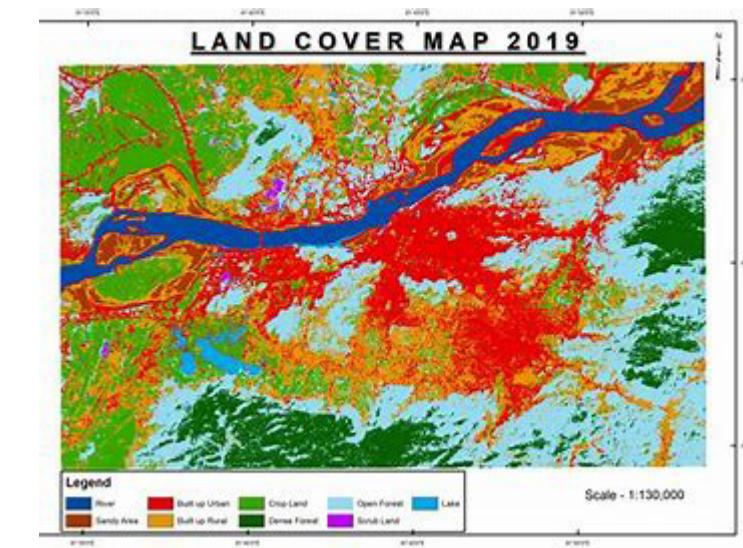
Computer/Software Cost

- Typically, *one-time* payment
- Yearly maintenance to ensure technical support and upgrades
- Can be distributed throughout many projects
- Same for Computer and Additional Software



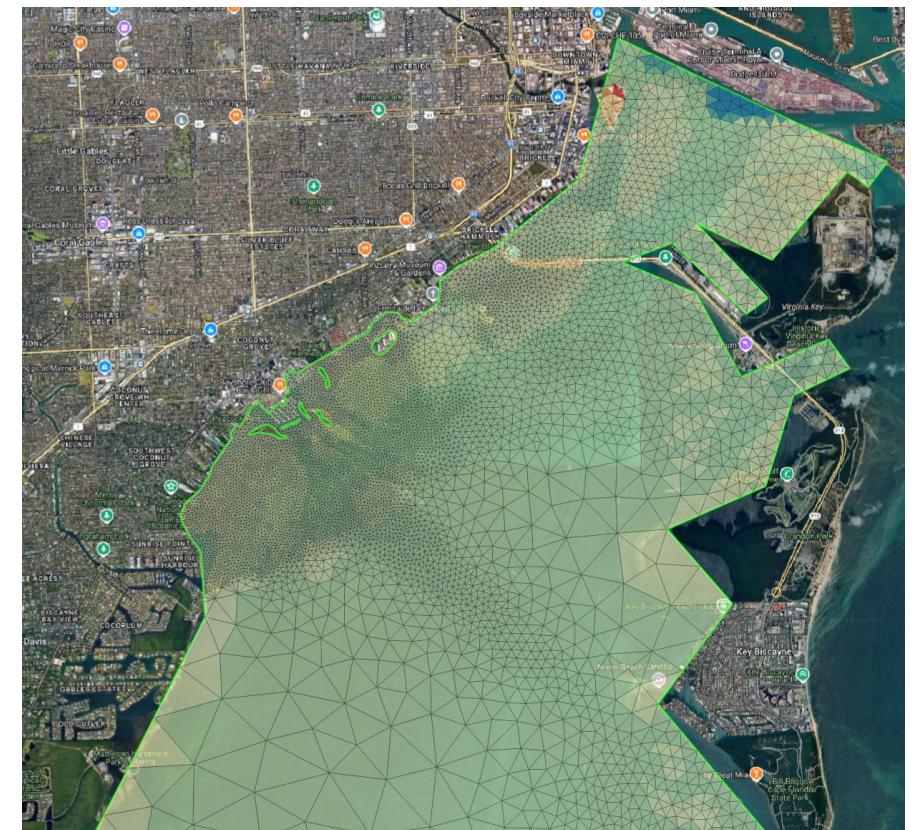
GIS Pre-processing and Model Conceptualization

- Common effort regardless the model performance
- Does not depend *[much]* on the selected model
- Required for all Modeling Applications



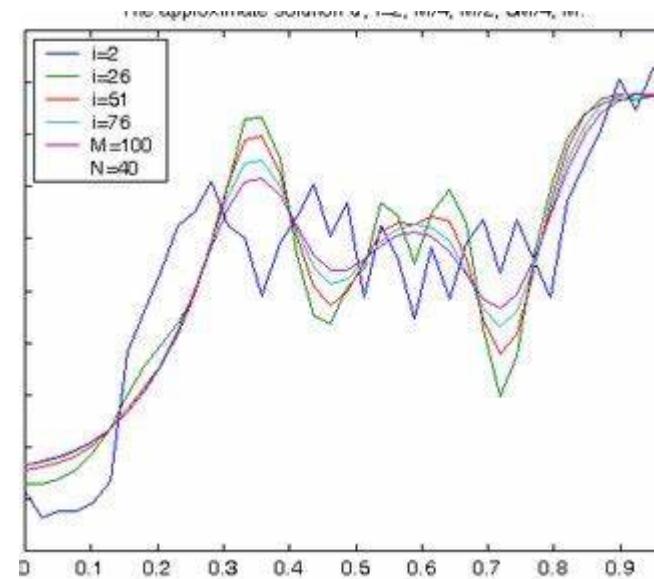
Model Setup

- Depends on Model Graphical User Interface
- Required in all Projects
- “Use the one you know best”
- SMS, QGIS, etc.



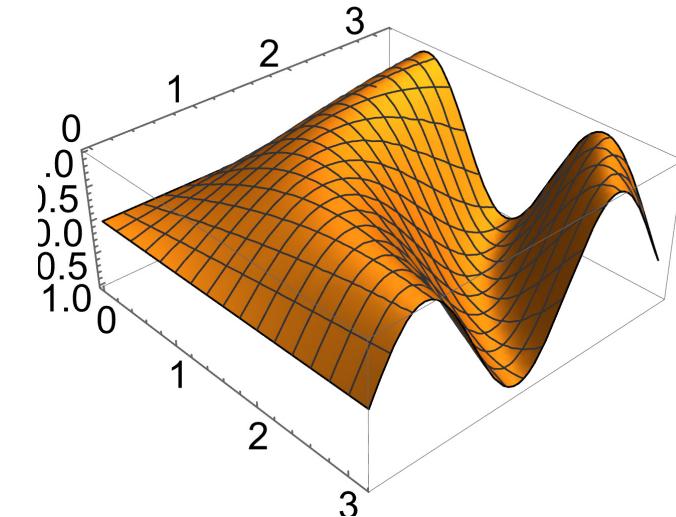
Numerical Stability and Consistency

- Highly Variable among Models
- In some models, Numerical Instabilities may require many trial-and-error runs, and tweaking the model to make it work
- Required task in all projects
- Often very time-consuming.



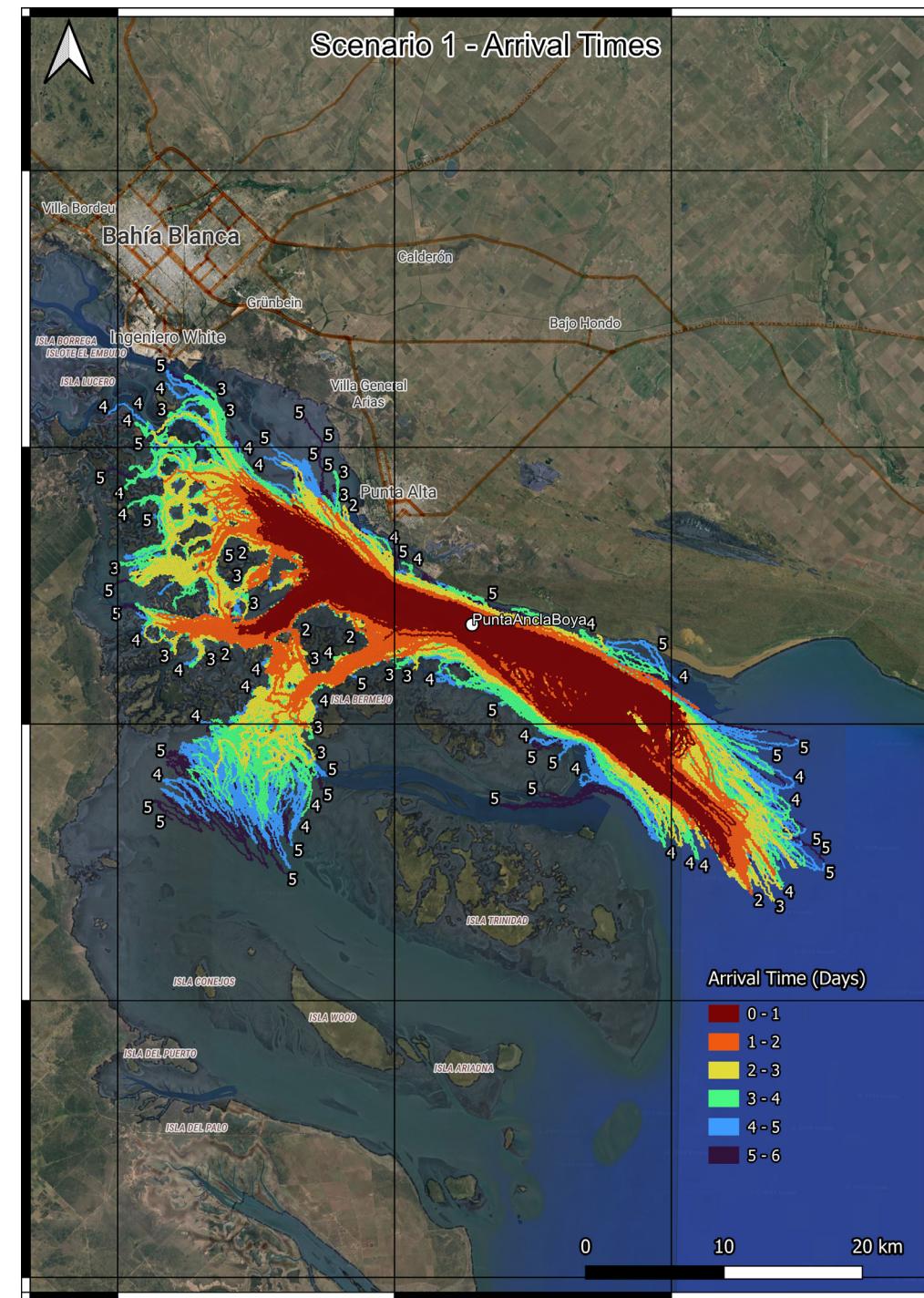
Model Performance

- Highly Variable among Models
- Depends on project size (number of cells) and simulation time
- Involves monitoring and waiting for runs
- Impacts most applications
- Very time-consuming task

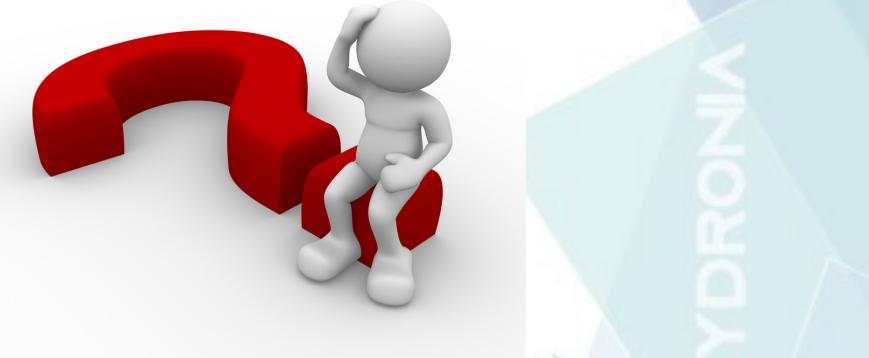


Analysis of Results and GIS post-processing

- Common to all Models
- Required in all Projects



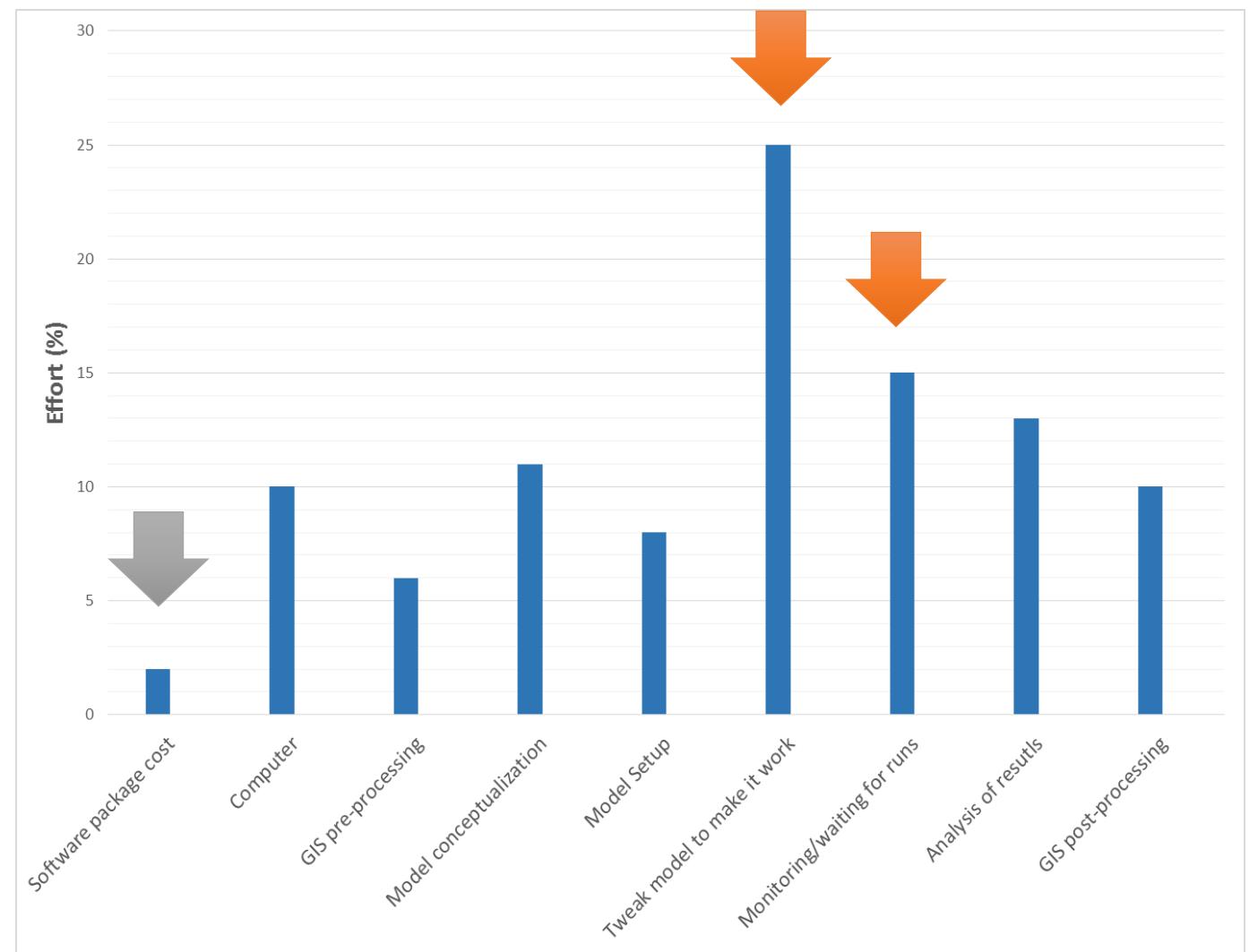
Total Cost of a Modeling Project



Factor affecting modeling cost	Cost	~ % of Total Effort
Software	One Time*	2
Computer and Additional Software	One Time*	10
GIS Pre-processing	All Projects	6
Model Conceptualization	All Projects	11
Model Setup	All Projects	8
Numerical Stability and Consistency	All Projects	25
Model Performance	All Projects	15
Analysis of Results	All Projects	13
GIS Post-processing	All Projects	10
Total		100

Factors Affecting Cost of Modeling Tasks

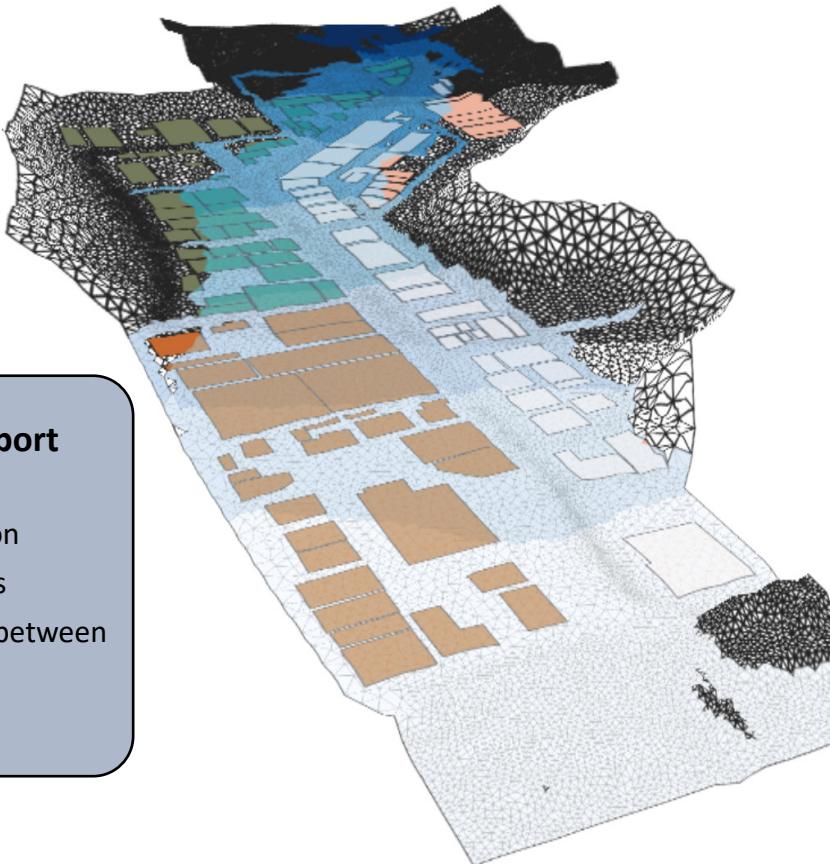
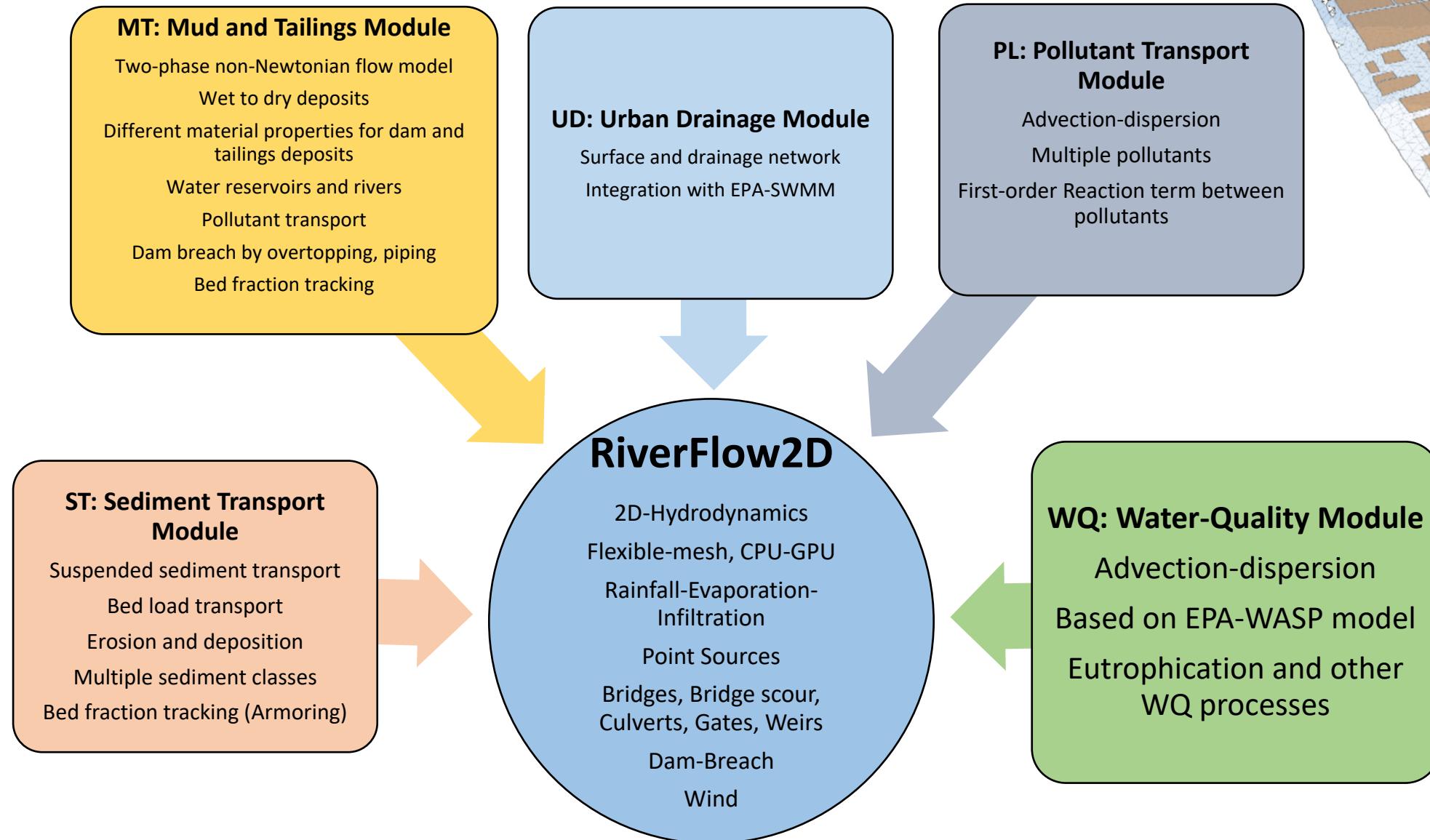
- Model package cost
- Computer and Software
- GIS pre-processing
- Model Conceptualization
- Model Setup
- **Tweak model to make it work**
- **Model Performance**
- Result analysis
- GIS post-processing



RiverFlow2D/OilFlow2D Modeling System

Developed since 2013 through an agreement between the
University of Zaragoza Computational Hydraulics Group and
Hydronia LLC USA.

RiverFlow2D Model



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OilFlow2D Model System

OL: Overland Flow Model

Evaporation

Infiltration

Hydraulic structures

Heat transfer with the environment

Fluid properties vary with temperature



OP: Oil Pipeline Module

Pipeline release volume calculator

Batch run of multiple spills

Integrated mapping for thousands of spills

OilFlow2D

2D-Oil and Viscous Fluids
Hydrodynamics

Flexible-mesh, CPU-GPU

Point sources

Rainfall-Evaporation-Infiltration

Hydraulic structures

Wind

Technical support in English, Spanish,
French and Portuguese

OW: Oil-on water spill Model

Oil trajectory by particle-tracking

Evaporation

Emulsification

Dissolution

Shore interaction

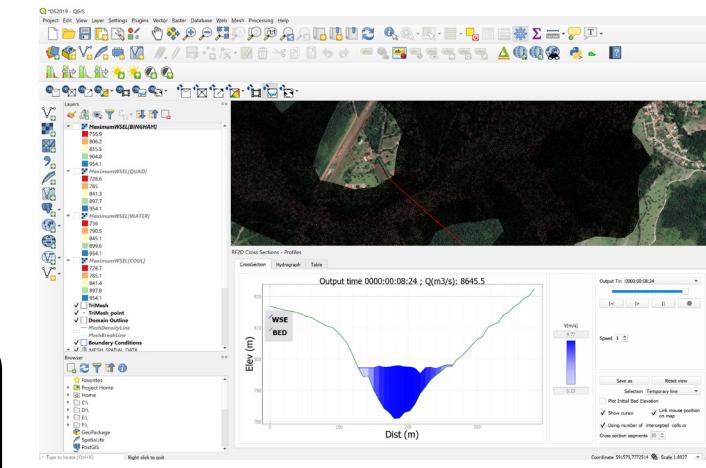
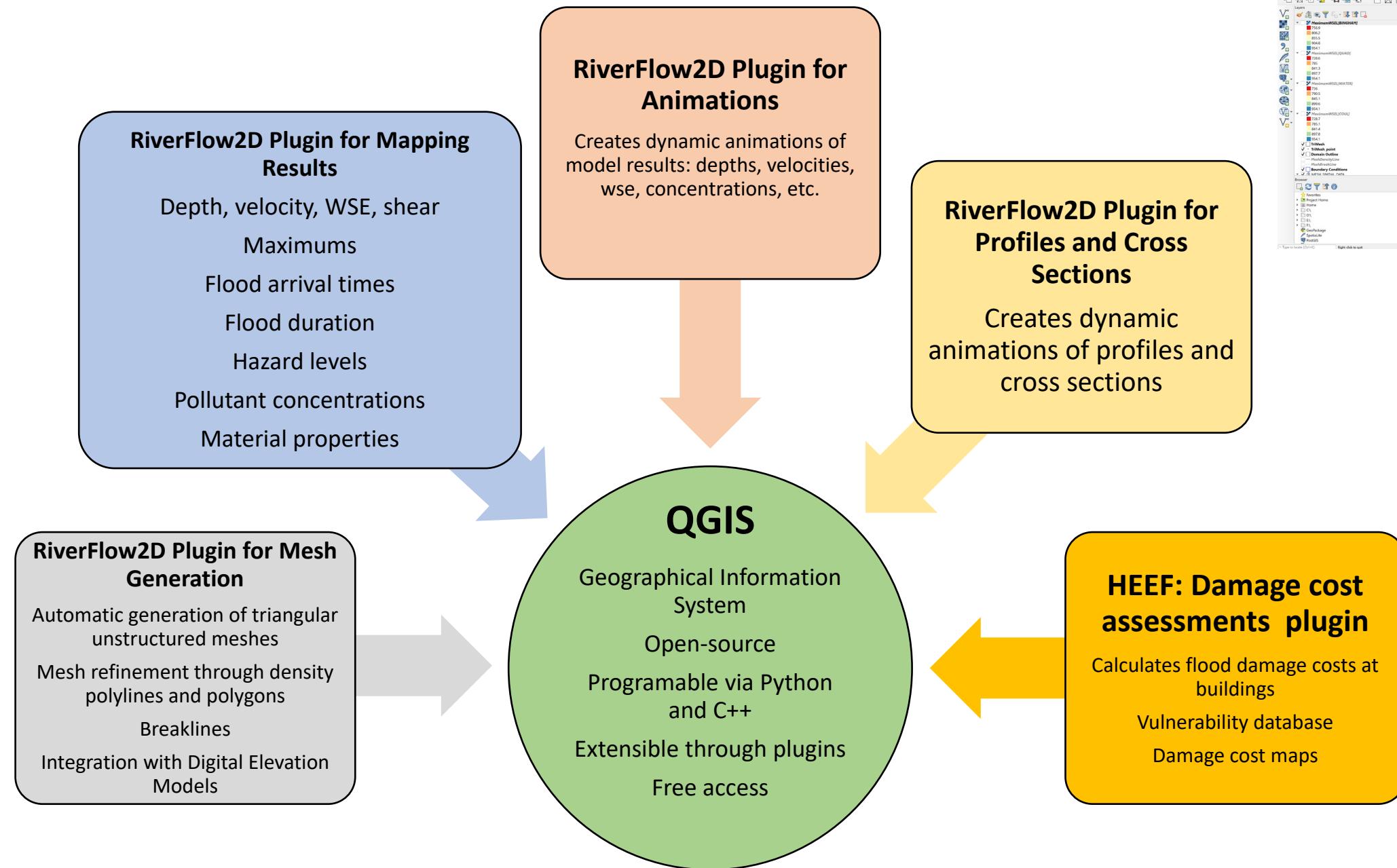
Containment Booms

Spills from moving ships

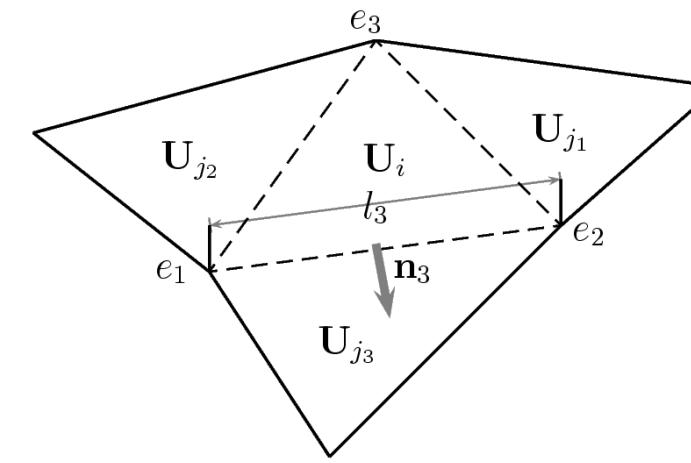
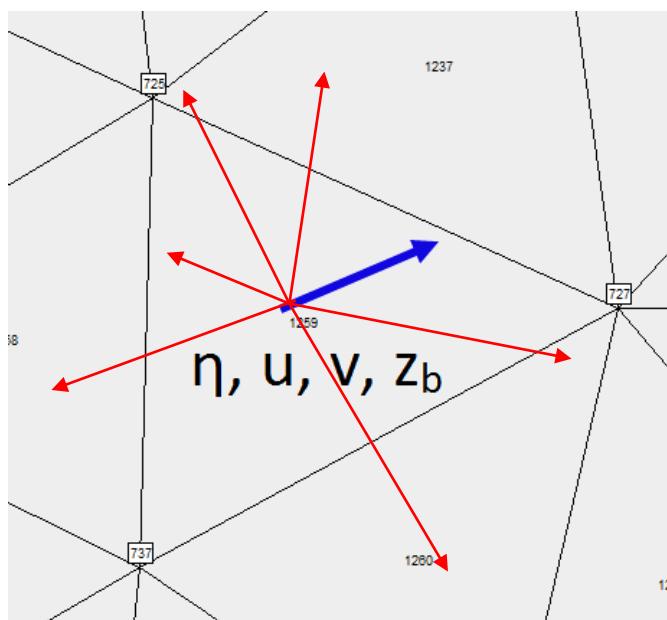
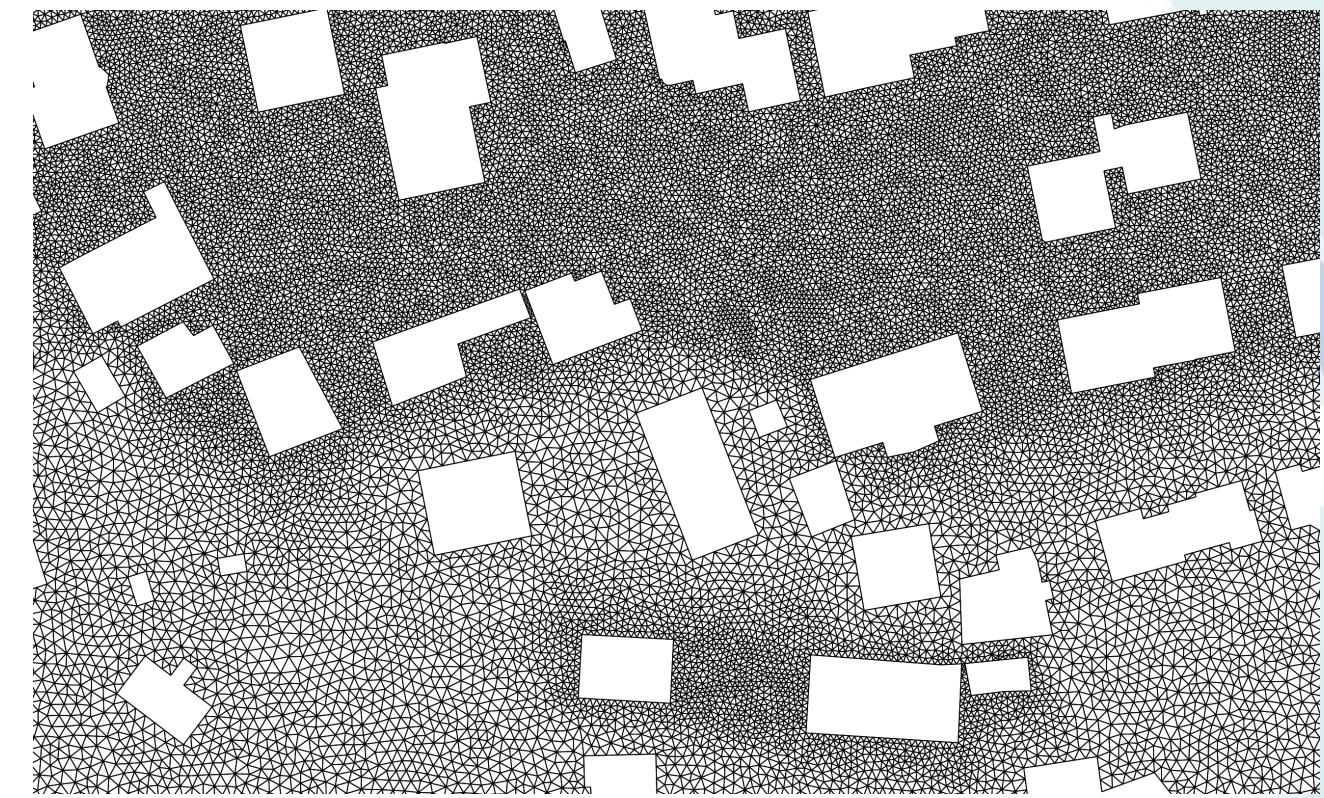


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QGIS-Based Graphical User Interface

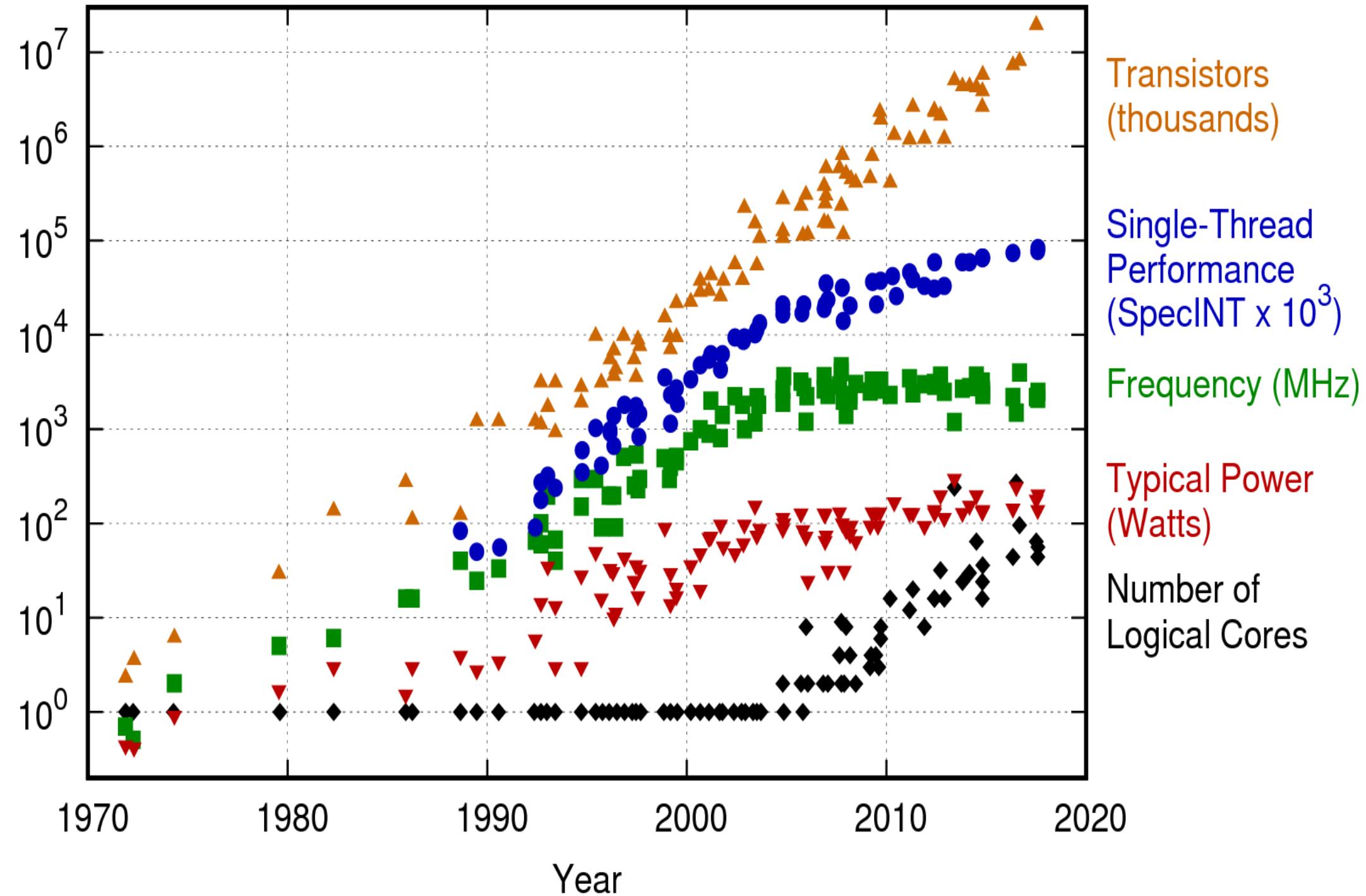


Flexible Mesh



Motivation for using GPUs

42 Years of Microprocessor Trend Data



Original data up to the year 2010 collected and plotted by M. Horowitz, F. Labonte, O. Shacham, K. Olukotun, L. Hammond, and C. Batten
New plot and data collected for 2010-2017 by K. Rupp

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Addressing Computational Challenge with RiverFlow2D/OilFlow2D GPU

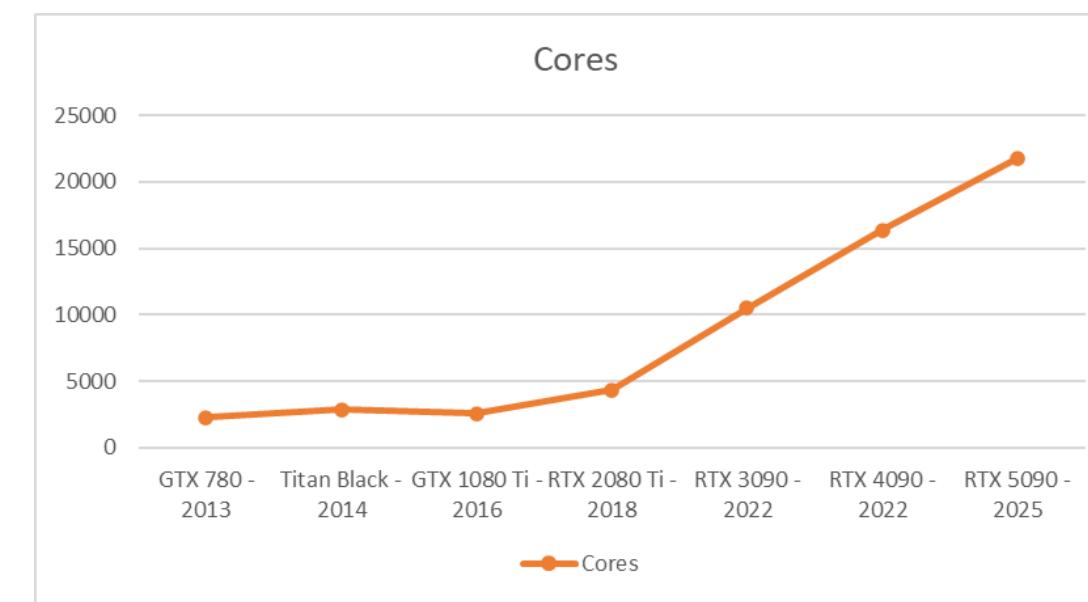
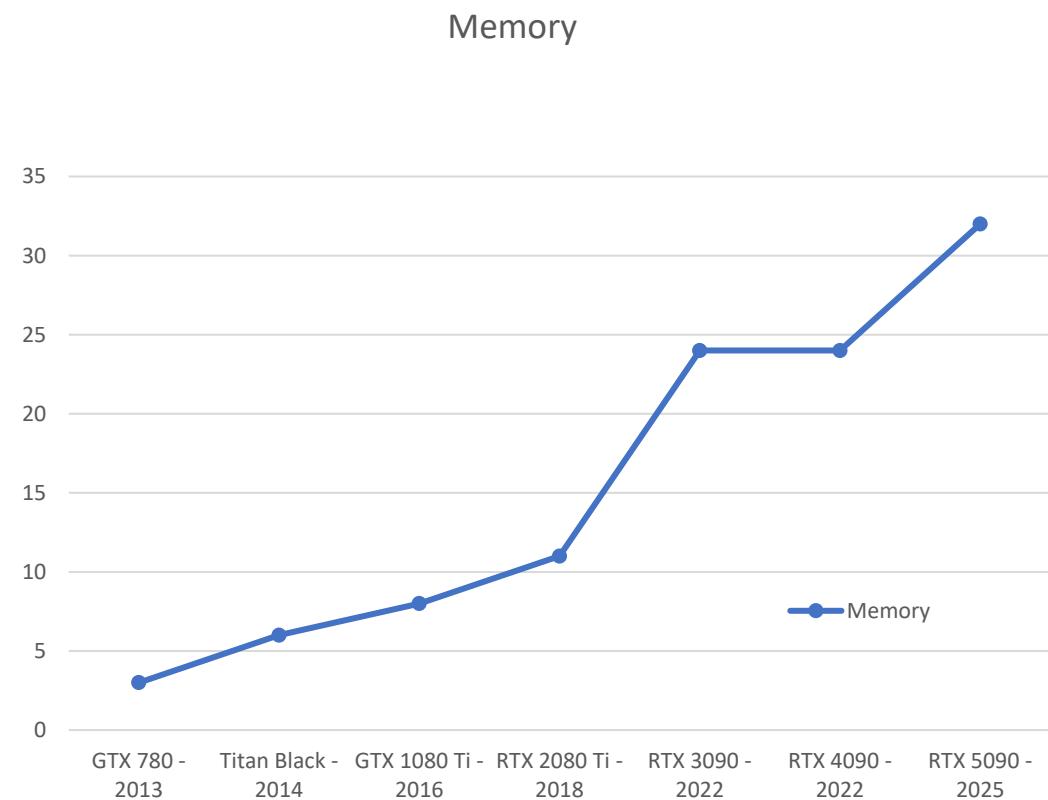
- CPU → Central Processing Unit (OpenMP)
- GPU → Video Cards
- GPUs → 15000+ processors (cores)
- Requires specialized programming (NVIDIA CUDA)



GPU CARD	Number of Cores	Memory GB	Cost US\$
GTX 1080 Ti	3,584	11	700
Tesla K80	2,496	12	3,000
Tesla P100	3,584	16	6,000
Tesla V100	5,120	16	19,500

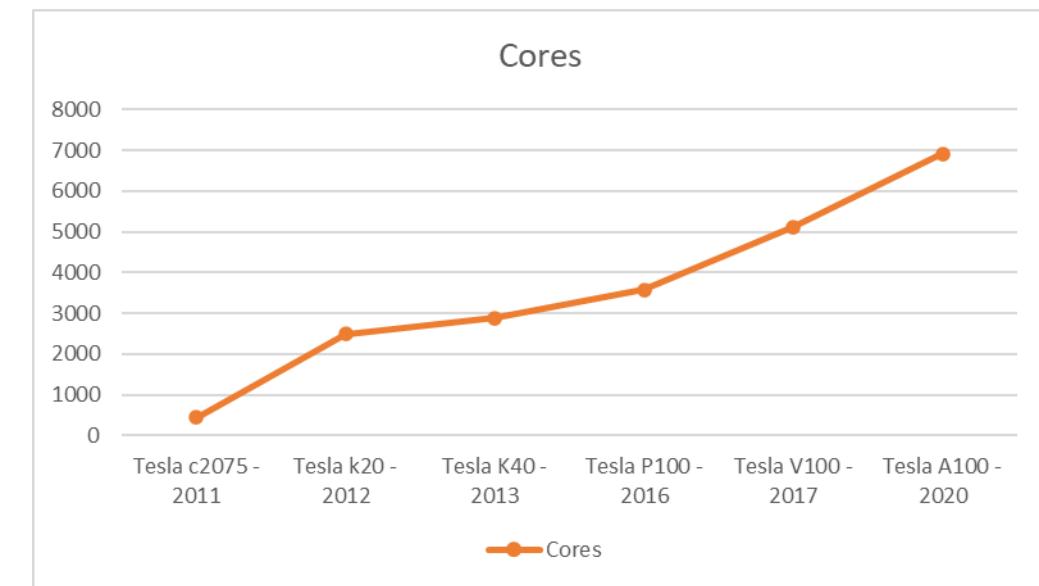
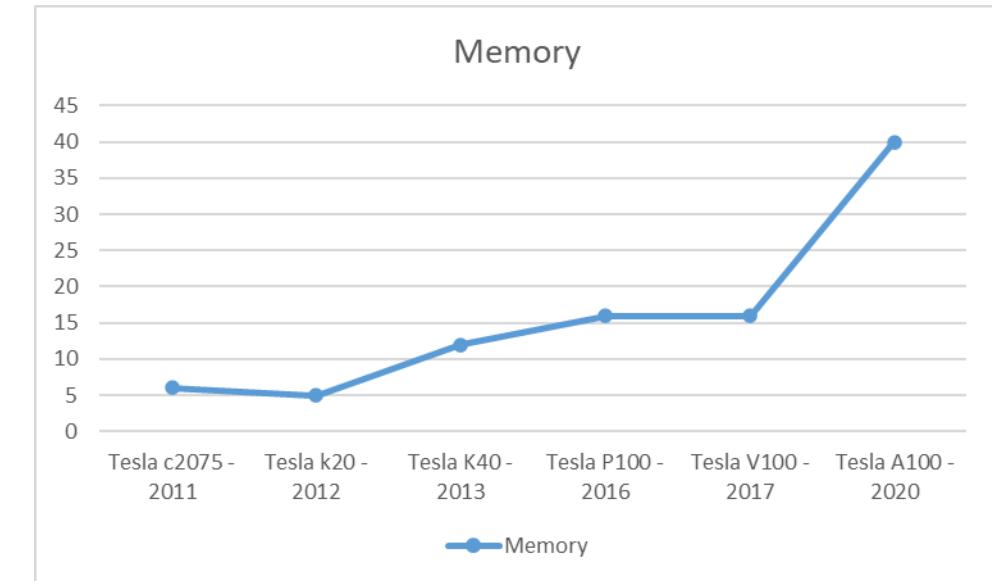
Evolution of NVIDIA Consumer GPUs

Card - Year	Memory (GB)	Cores
GTX 780 -2013	3	2304
Titan Black -2014	6	2880
GTX 1080 Ti -2016	8	2560
RTX 2080 Ti -2018	11	4352
RTX 3090 -2022	24	10496
RTX 4090 -2022	24	16384
RTX 5090 -2025	32	21760



Evolution of NVIDIA High-End GPUs

GPU Card - Year	Memory (GB)	Cores	Year Intro
Tesla c2075 - 2011	6	448	2011
Tesla k20 - 2012	5	2496	2012
Tesla K40 - 2013	12	2880	2013
Tesla P100 - 2016	16	3584	2016
Tesla V100 - 2017	16	5120	2017
Tesla A100 - 2020	40	6912	2020



Case Studies

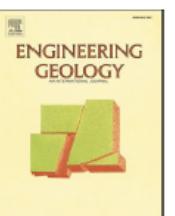
“Real-World” Modeling Applications

- Brumadinho Dam Break
- Biscayne Bay Salinity Model
- Ashland Tank-break

Brumadinho Dam Break

A decorative graphic in the top right corner consisting of overlapping triangles in shades of blue, teal, and white. The word "HYDRONIA" is written vertically in a light blue font along the top edge of this graphic.

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A GPU-accelerated Efficient Simulation Tool (EST) for 2D variable-density mud/debris flows over non-uniform erodible beds



S. Martínez-Aranda ^{*}, J. Murillo, P. García-Navarro

Fluid Dynamic Technologies-I3A, University of Zaragoza, Spain

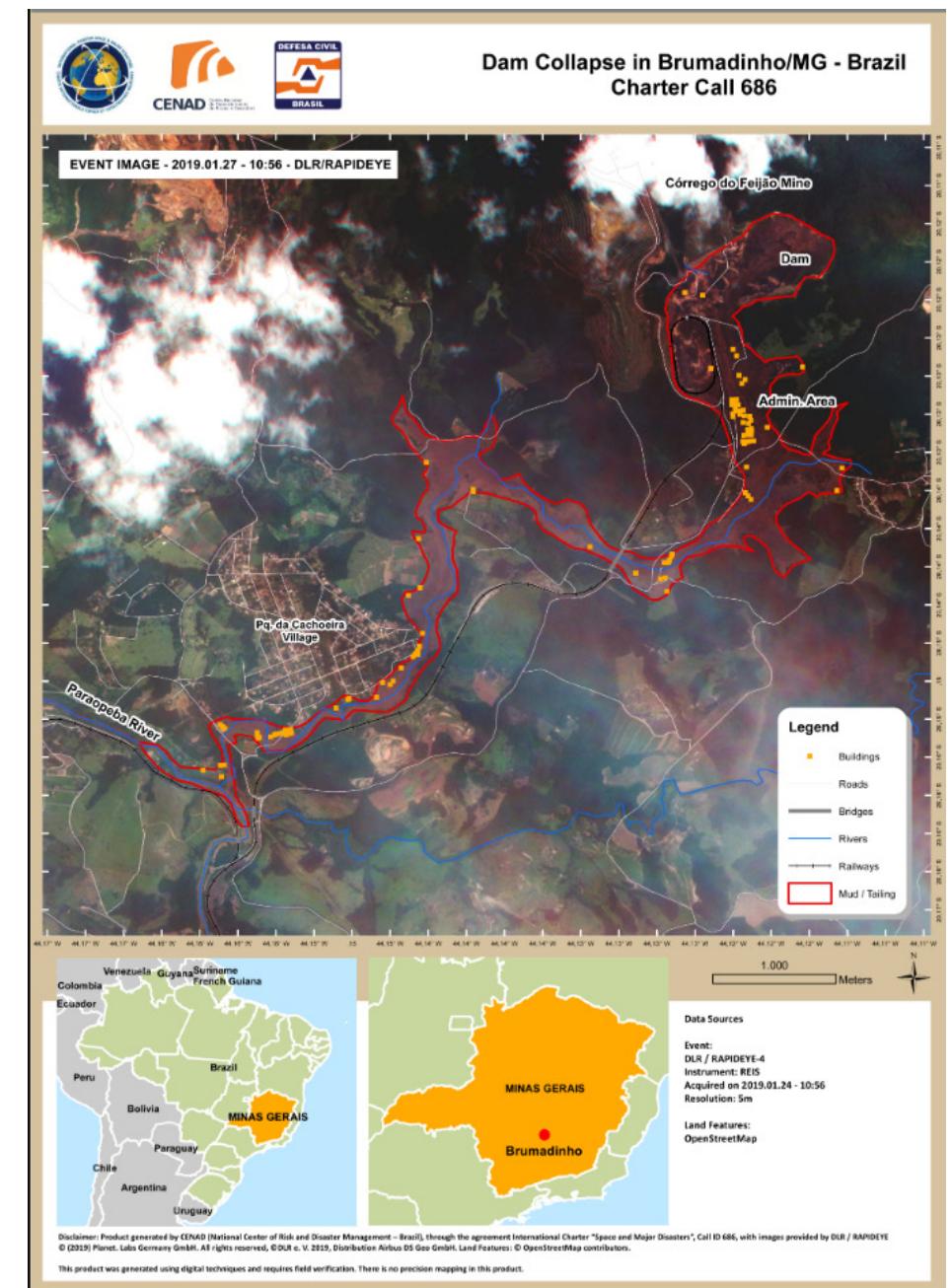
ARTICLE INFO

Keywords:
Mud/debris flow
Non-uniform erodible bed
Variable-density mixture
Augmented riemann solvers
Well-balanced schemes
Source terms integration
GPU-accelerated codes

ABSTRACT

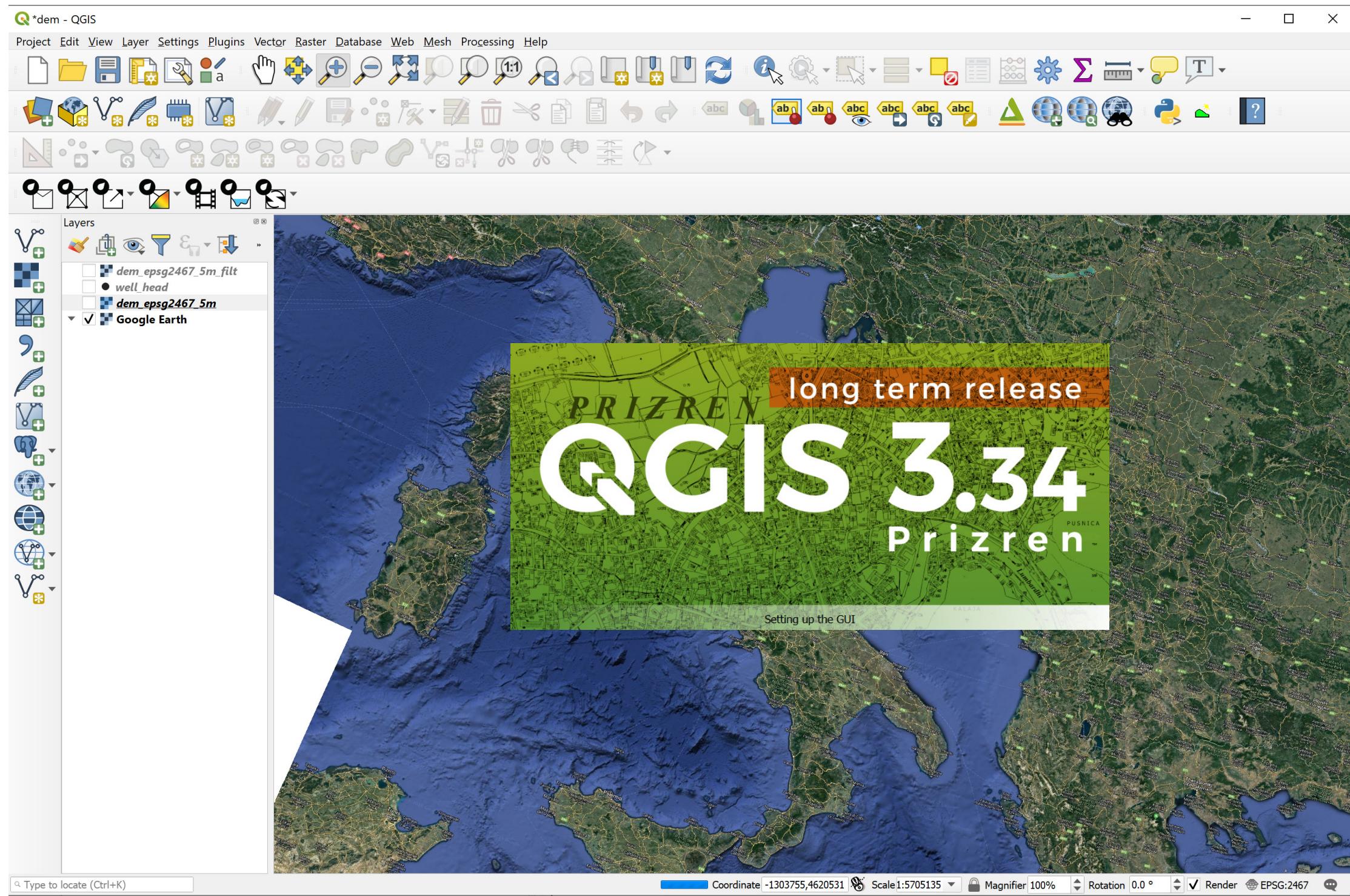
Mud/debris flows are among the most challenging gravity-driven flows in environmental and geophysical processes. Natural muddy slurries and debris are solid-laden fluids where the density of the mixture can be more than twice or three times the water density and, hence, the bulk solid phase can represent 40–80% of the flow column volume. Furthermore, these unsteady flows usually occur along steep and irregular terrain which requires a refined non-structured spatial discretization, increasing the computational times of the models. In this work a new upwind Roe-type solver for two-dimensional multi-grain mixture shallow-flow over non-uniform erodible bed is presented. The coupled system of depth-averaged equations is formed by the conservation equations for the mass and momentum of the variable-density mixture, the mass conservation equations for the N different solid phases transported in the flow and the continuity equation for the erodible bed layer, where the different solid phases can be exchanged independently modifying the bed level. The non-Newtonian rheological behavior of the multi-grain mixture is included into the momentum equations using six different basal resistance formulations. An accurate, robust and efficient x-split Augmented Roe (xA-Roe) solver for variable-density flow is derived, which requires a complete reformulation of the averaged-Roe values at the intercell edges and allows the mixture density to participate in the definition of the characteristic wave celerities of the local Riemann problem. The global time step is dynamically controlled by the wave celerities of the coupled system of equations, preserving the scheme stability even for high density gradients. The bed slope and basal resistance source terms are also upwind discretized and included into the intercell numerical fluxes, ensuring a well-balanced flux formulation in steady states and the correct treatment of wet-dry fronts. The proposed model is GPU-accelerated using a CUDA/C++ algorithm and applied to synthetic tests and the USGS debris dambreak experiments over erodible bed, demonstrating its robustness, accuracy and efficiency. Finally, the model is tested against a real-scale and long-term case, the mining-tailing dam failure occurred in Brumadinho (Brazil) in 2019. The numerical results show good agreement with the observed field data and the computational cost reduction obtained with the GPU-accelerated algorithm is up to 60 times compared to a CPU-based code.

- Córrego do Feijão 80 m high iron tailings mine
- At 12:28 PM on Friday, January 25, 2019, the dam failed, impacting areas more than 8km downstream from the dam site
- Estimated death toll > 300 persons

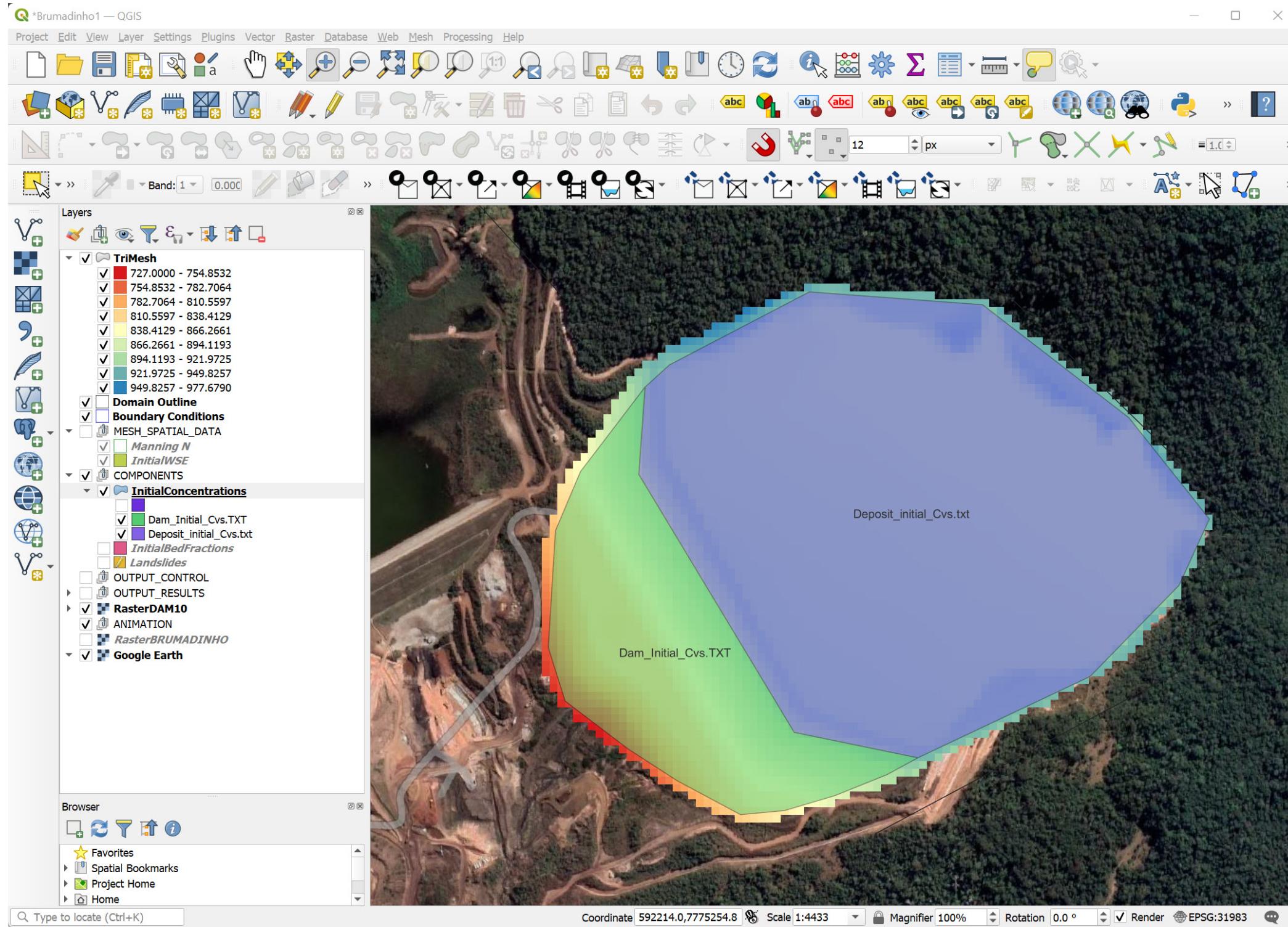




: OilFlow2D™ –QGIS Integration



Different material properties

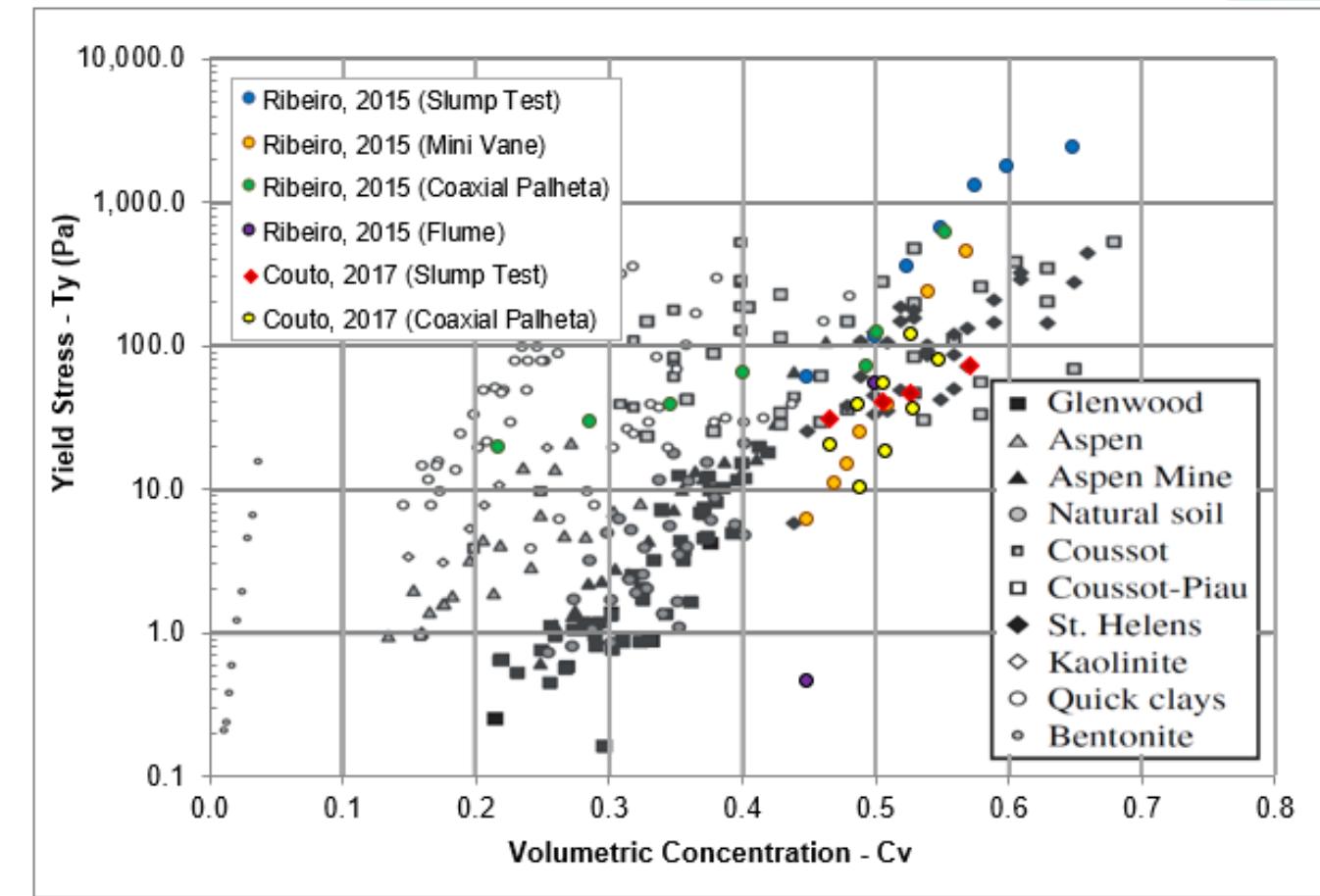
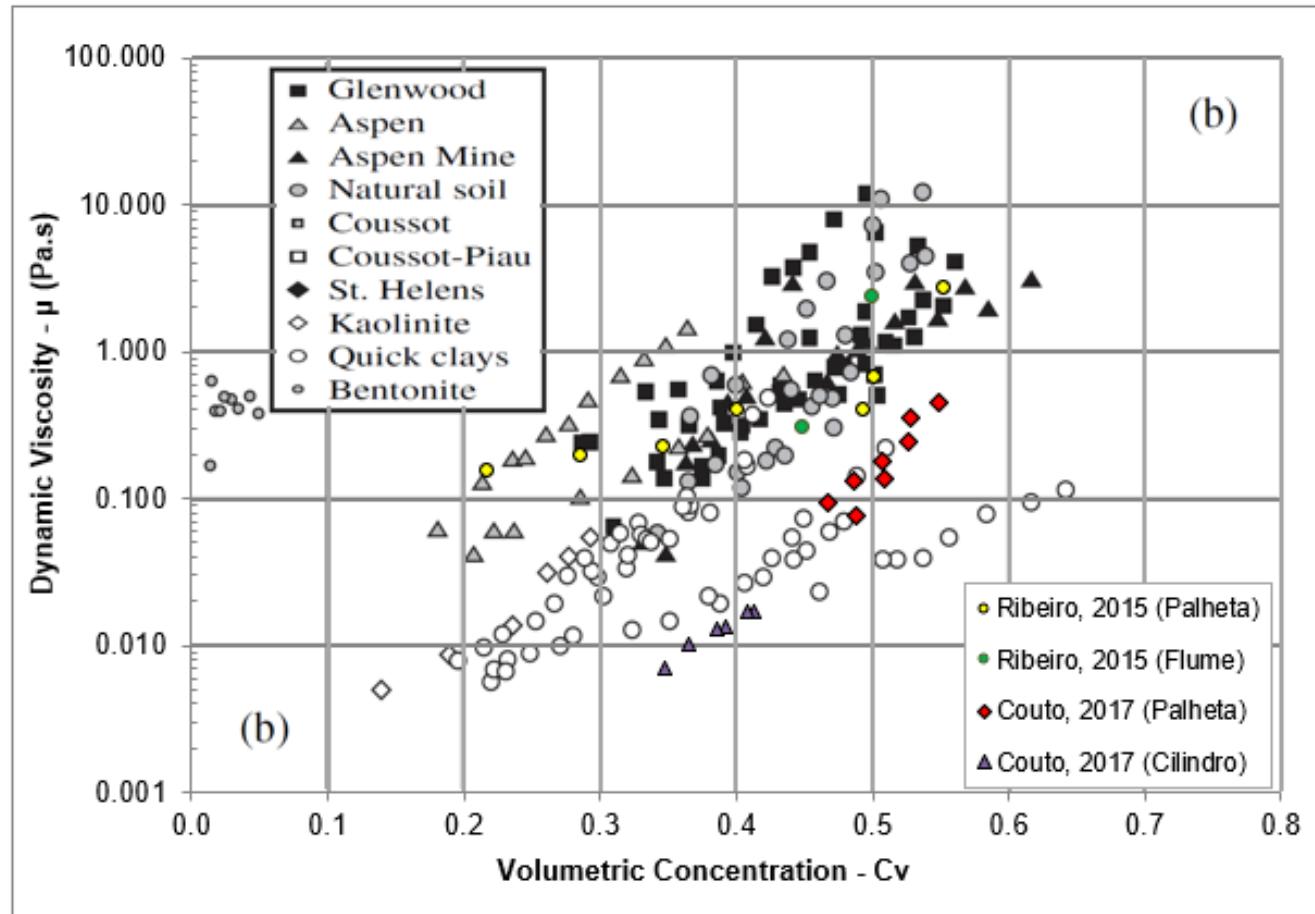


Flexible Mesh

- 382,966 Cells
- Mesh area: 10.5 km².
- Average cell size: 7.4 m.
- Minimum cell size: 3.6 m.
- Maximum cell size: 12.1 m.



Mudflow Parameters Estimation

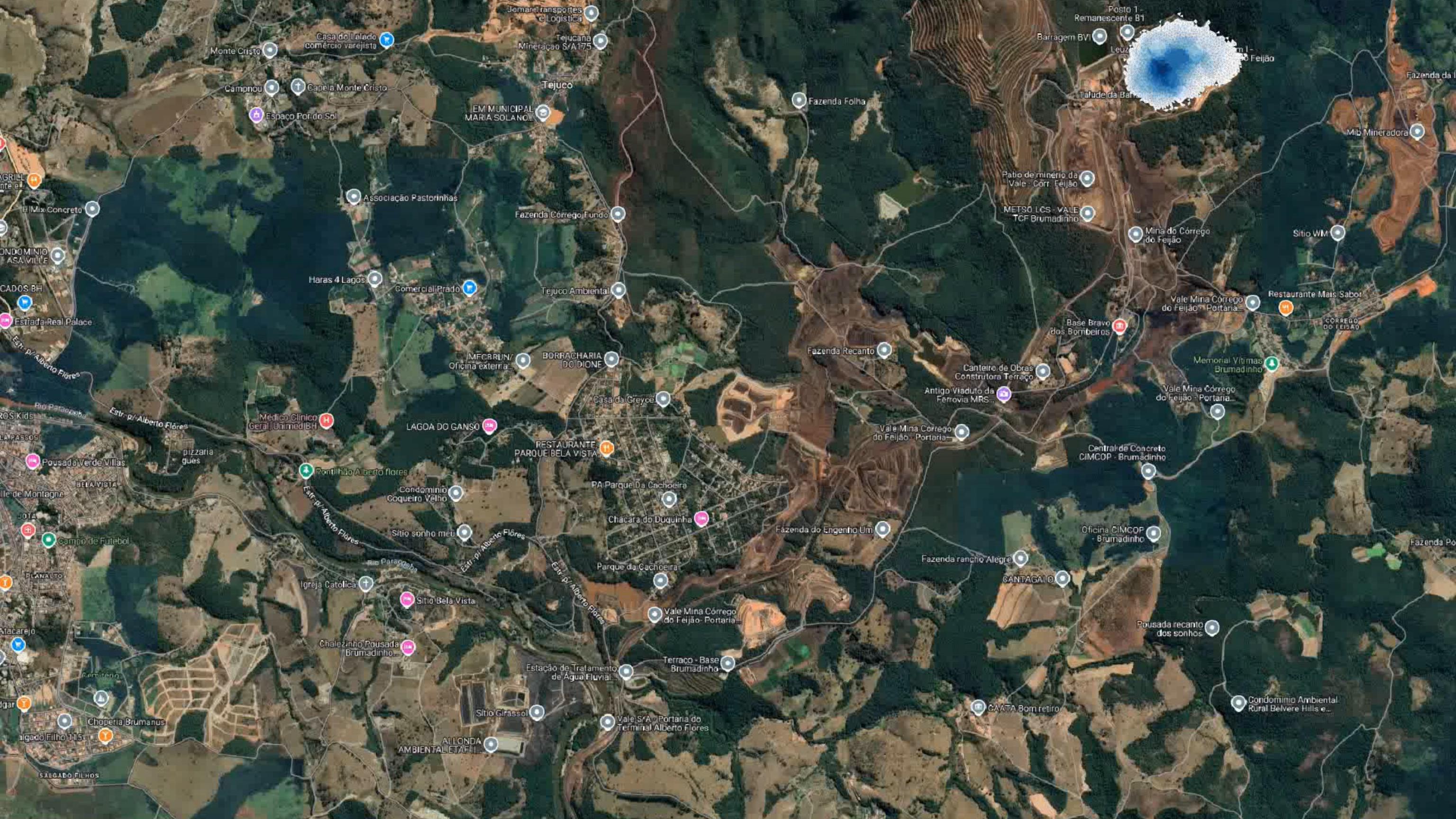


COUTO, N.M. 2015. *Retroanálise da propagação decorrente da ruptura da Barragem do fundão com diferentes modelos numéricos e hipóteses de simulação.*

Dissertação de Mestrado - Universidade Federal de Minas Gerais (UFMG). Belo Horizonte, 188 p.

JULIEN, P. Y. Erosion and Sedimentation. Second Edition, 2010.

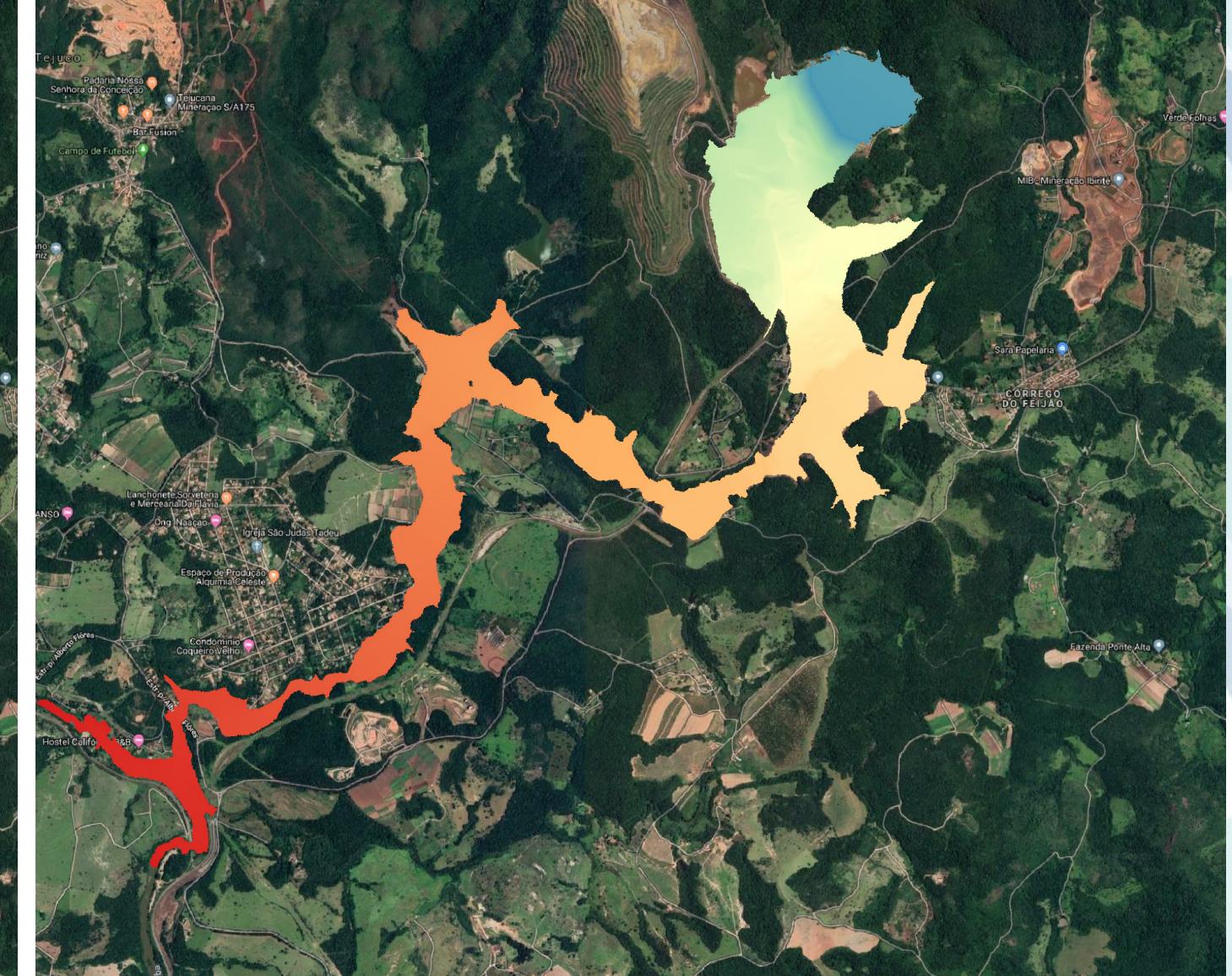
RIBEIRO, V. Q. F. Proposta de metodologia para avaliação dos efeitos de rupturas de estruturas de disposição de rejeitos. 2015. 267 f.. Dissertação (Mestrado) – Escola de Engenharia, Universidade Federal de Minas Gerais, Belo Horizonte, 2015



Observed



Simulated



Observed

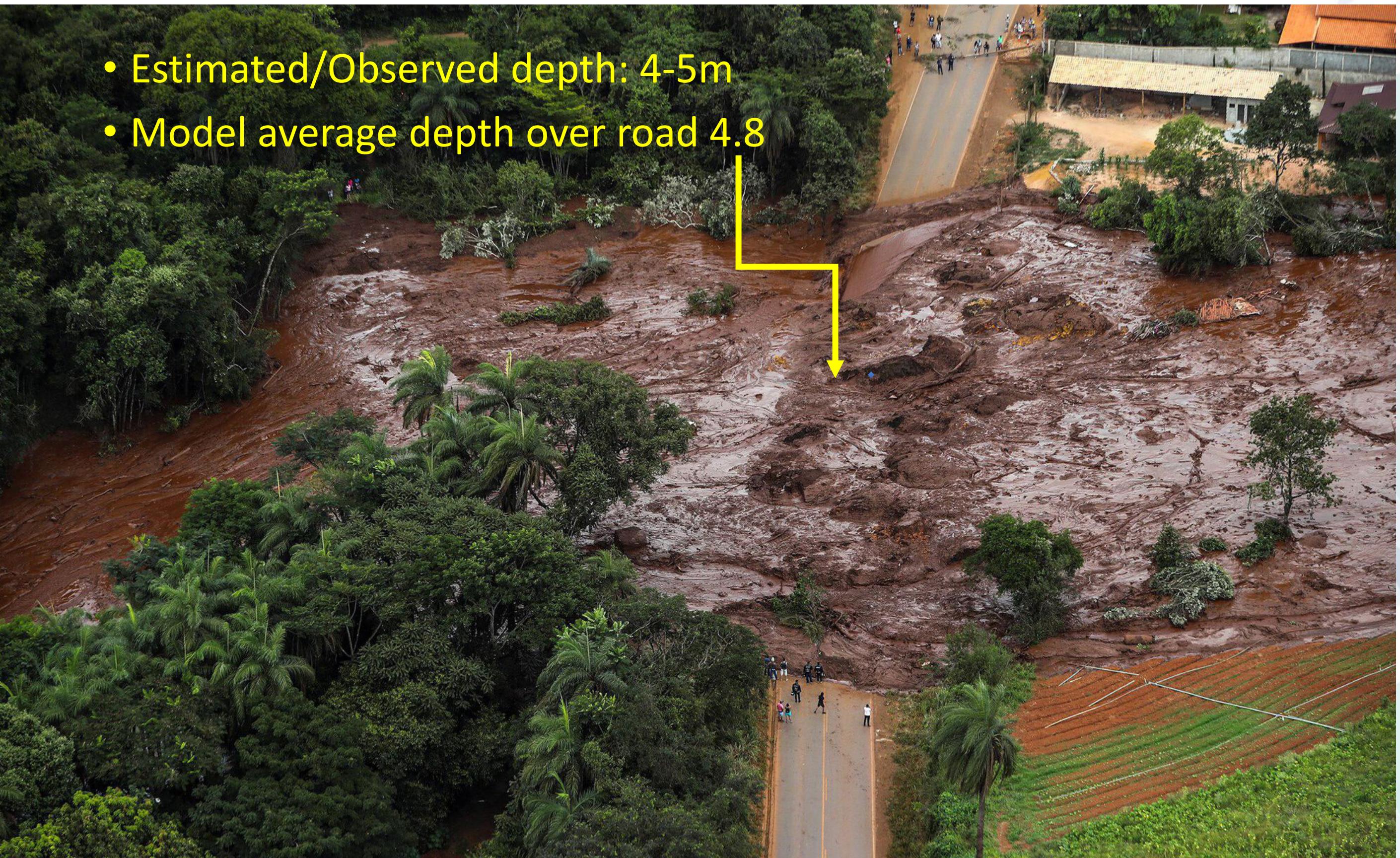


Simulated

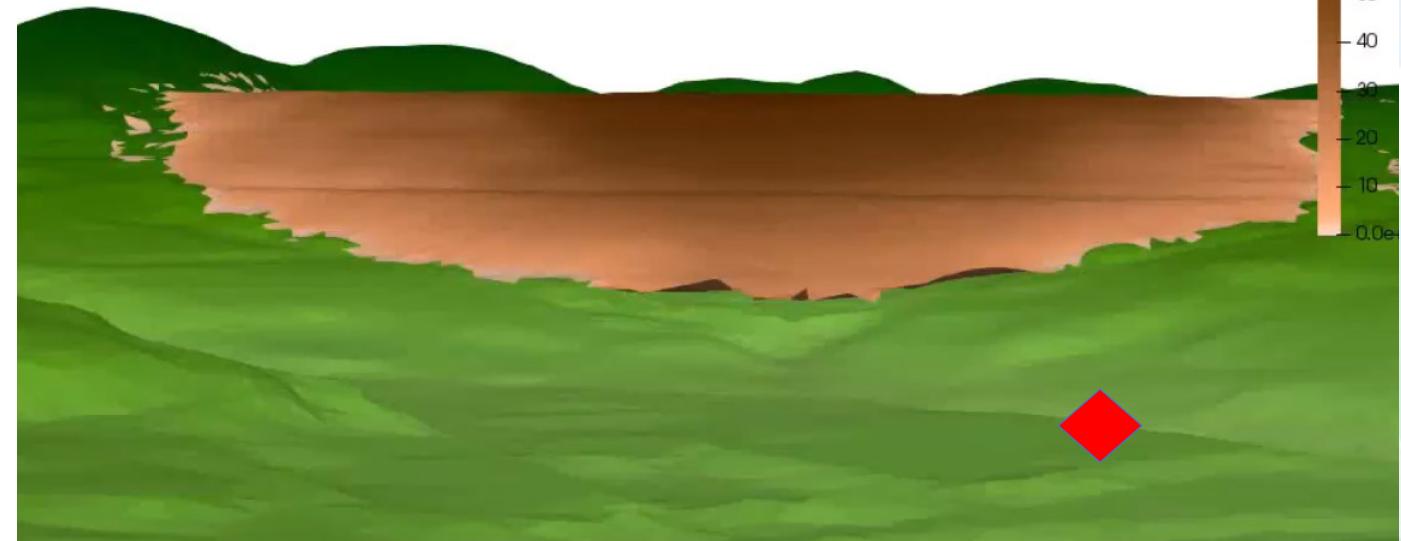


Alberto Flores Road Crossing

- Estimated/Observed depth: 4-5m
- Model average depth over road 4.8



No need to guess mobilized tailings volume

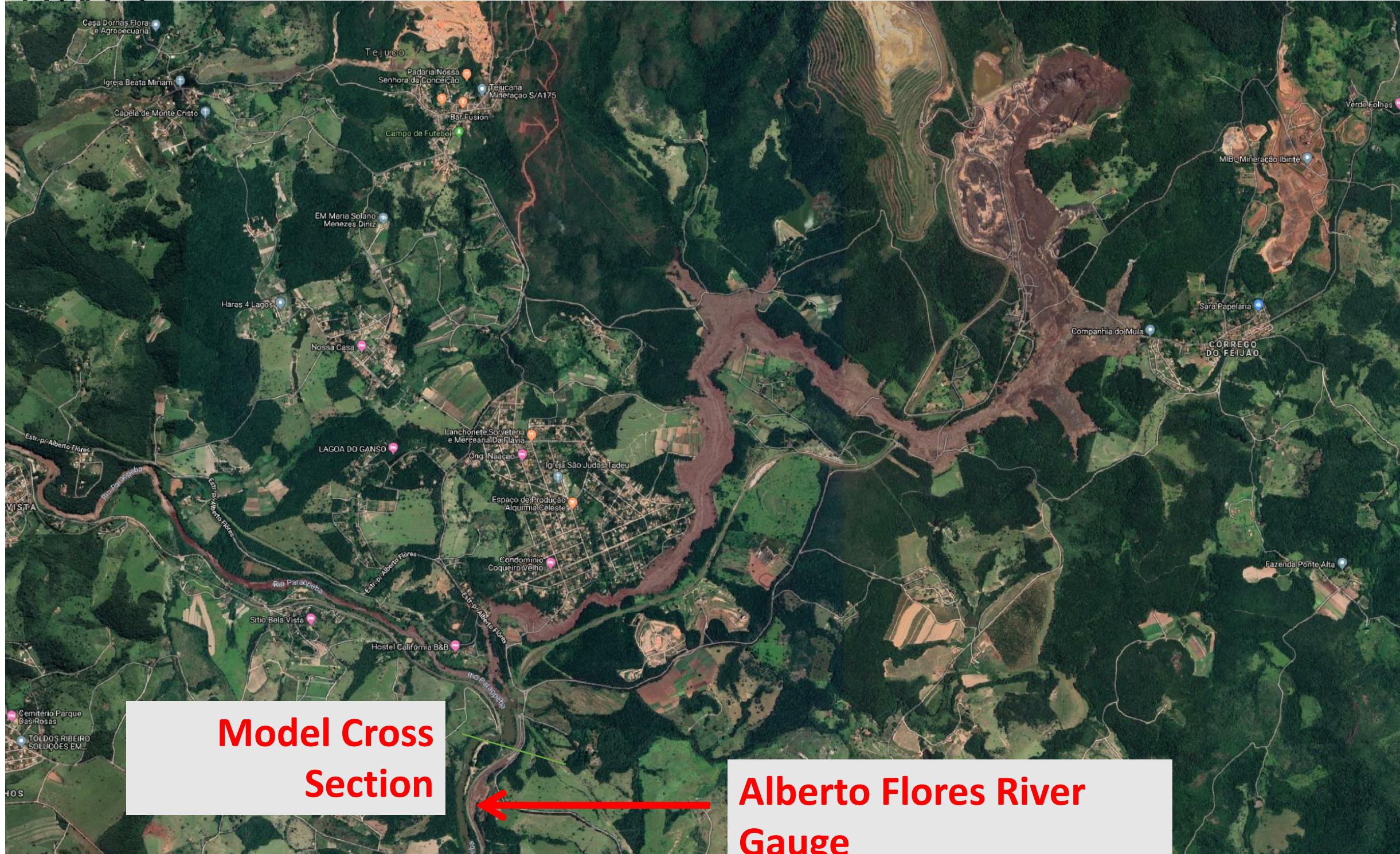


Parameter	Observed	RiverFlow2D Simulation
Mobilized volume ($m^3 \times 10^6$)	9.6	9.747
Time of arrival to reference point (seconds)	23	21

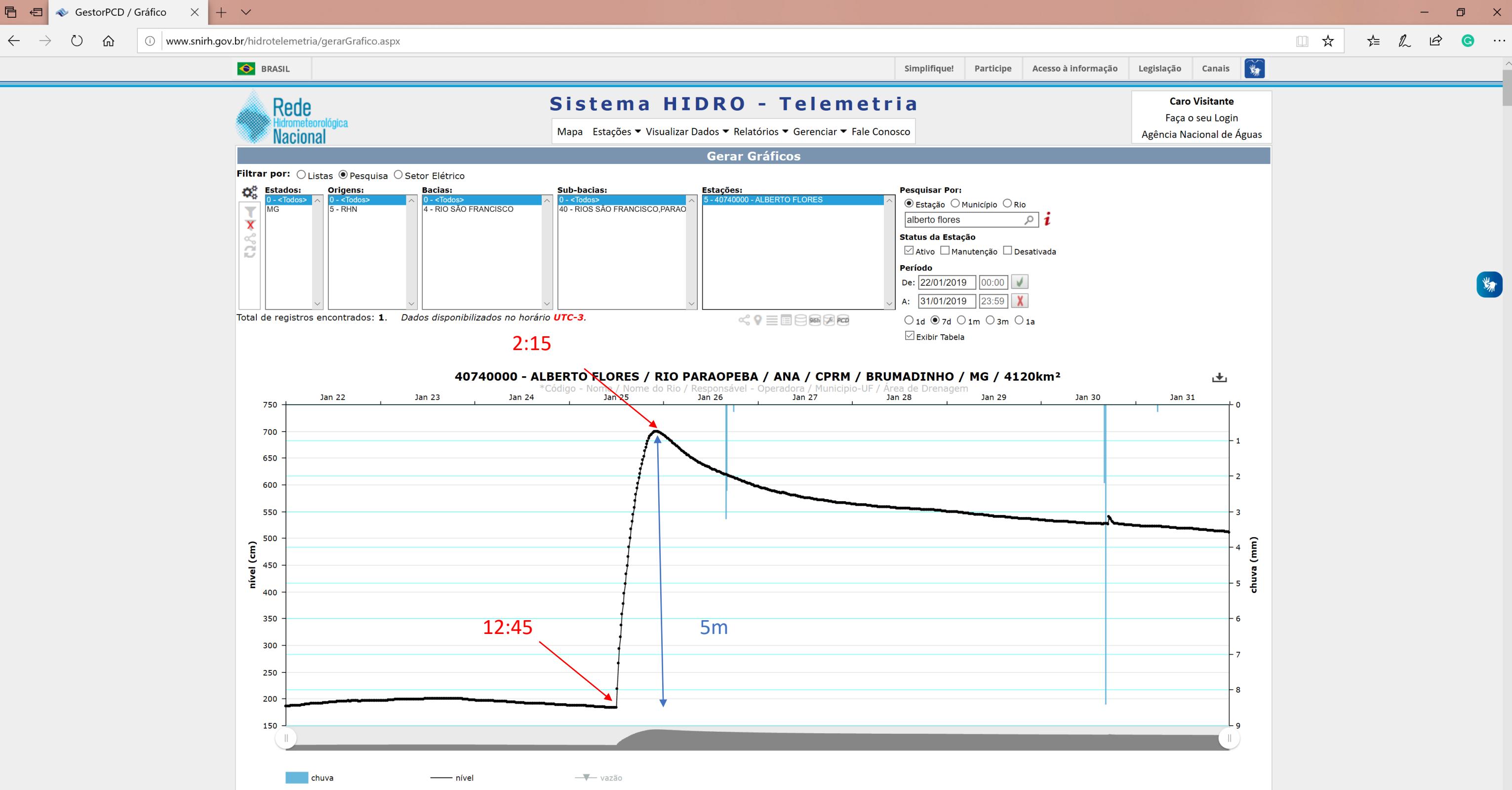
Inflow BC from Paraopeba River, Brazil



Comparison of Frontal Wave Arrival Time to Paraopeba River

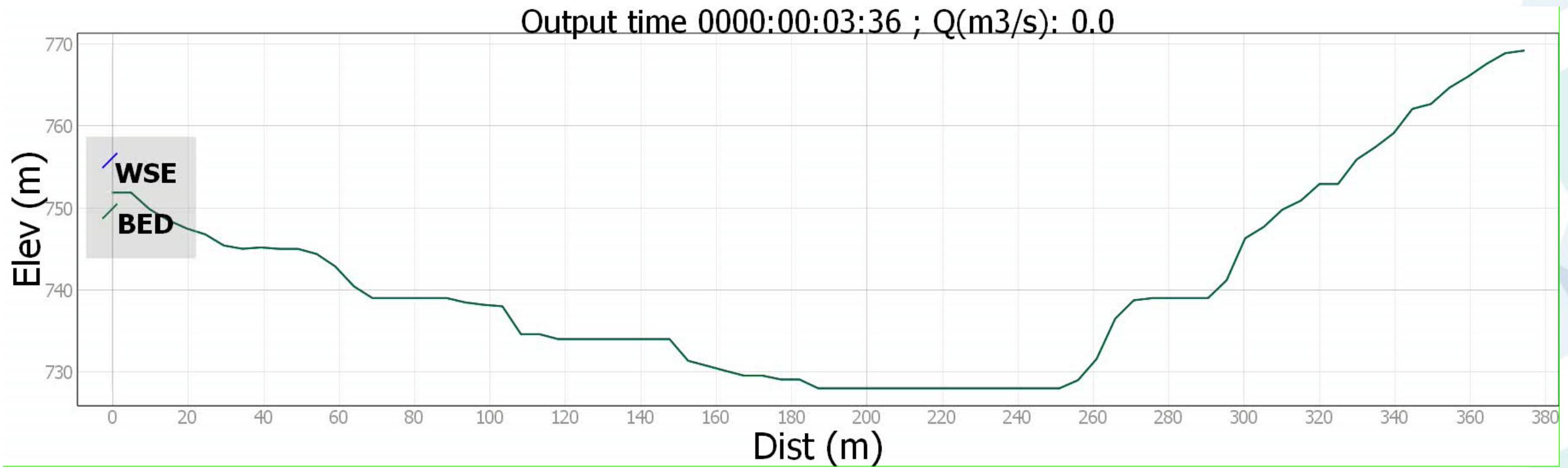


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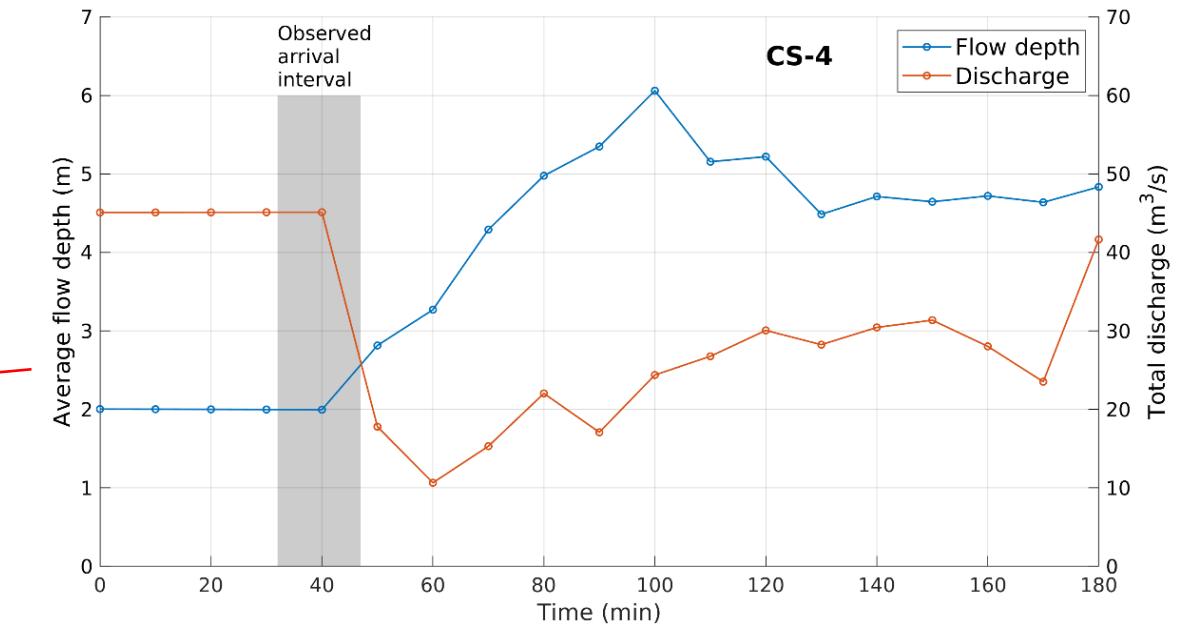
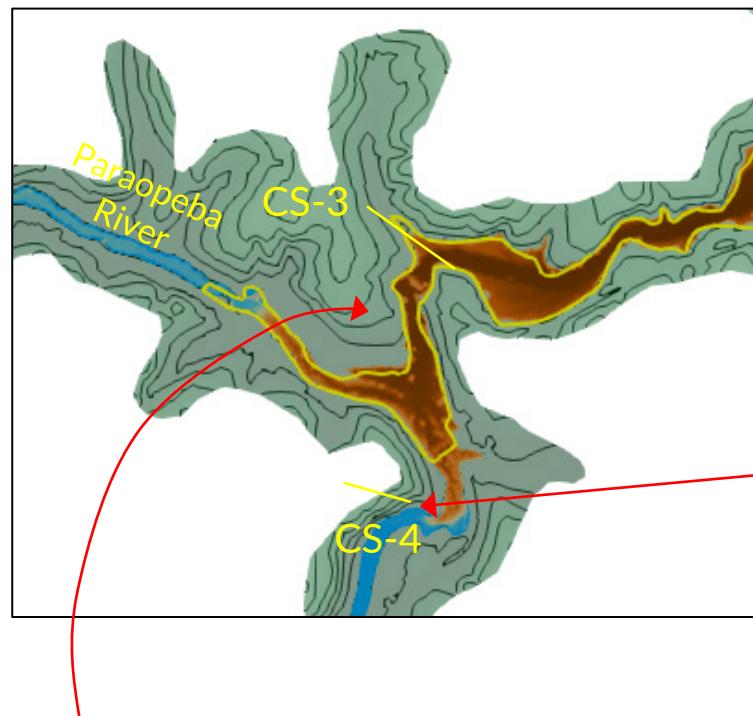


Output time 0000:00:03:36 ; Q(m³/s): 0.0



Model-Observations Comparison

Predicted temporal evolution at CS-4



	Observed	Computed
Released tailings volume (m^3)	$9.6 \cdot 10^6$	$9.747 \cdot 10^6$
Affected area (m^2)	$3.3 \cdot 10^6$	$3.604 \cdot 10^6$
Final mud elevation at CS-3 (m)	$\approx 4 - 5$	4.9
Arrival time to CS-4 (min)	32 – 47	43.5
Free surface increment at CS-4 (m)	5.11	4.06

Brumadinho Dam Break GPU Acceleration

NVIDIA RTX 4090 GPU	
Memory	24 GB
Cores	16,384



Mesh	No. Cells	Intel CPU	GTX 1080 Ti	RTX 3090	RTX 4090	Max Speedup
Mesh 1	19,792	00:00:12:08	00:00:00:43	00:00:00:27	00:00:00:19	16x
Mesh 2	150,055	00:04:16:31	00:00:08:45	00:00:04:03	00:00:02:05	125x
Mesh 3	1,096,772	04:04:03:32	00:02:38:27	00:01:03:15	00:00:33:12	181x

RiverFlow2D Evolution in Time

Biscayne Bay, FL, USA

Operational Model



Biscayne Bay Operational Model



Project Funded by the Environmental Protection Agency EPA USA (2019-2023)

A collaborative project between the University, the Government, and the Private Sector.

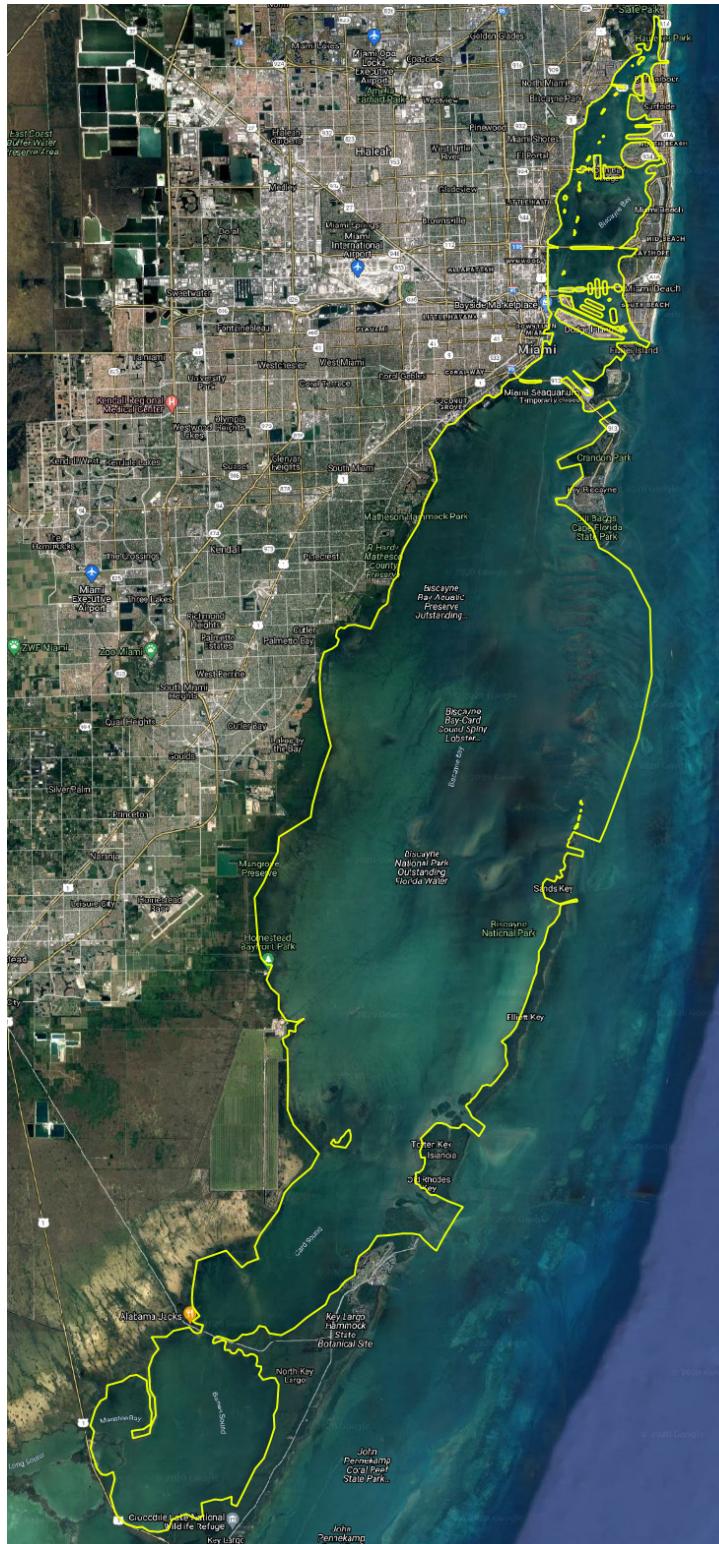
- Institute of Environment, Florida International University FIU
- DERM (Miami Dade County Division of Environmental Resources Management)
- Hydronia

BBOM Implementation

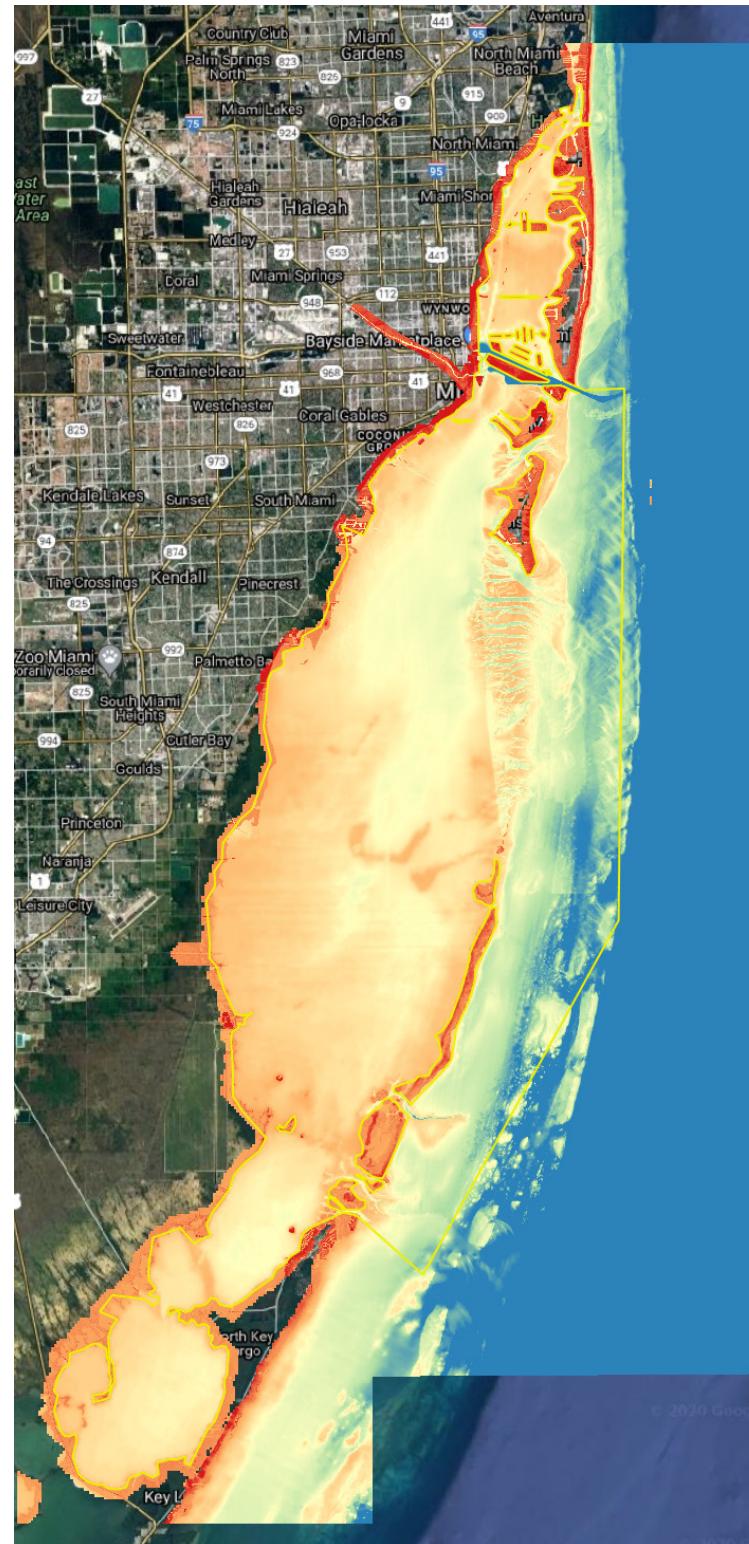
Bathymetric data

- NOAA Continuously Updated Digital Elevation Model (CUDEM) –
1/9 Arc-Second Resolution Bathymetric-Topographic Tiles.
- Updated on 2019-09-03.
- 0.5-3 m resolution.

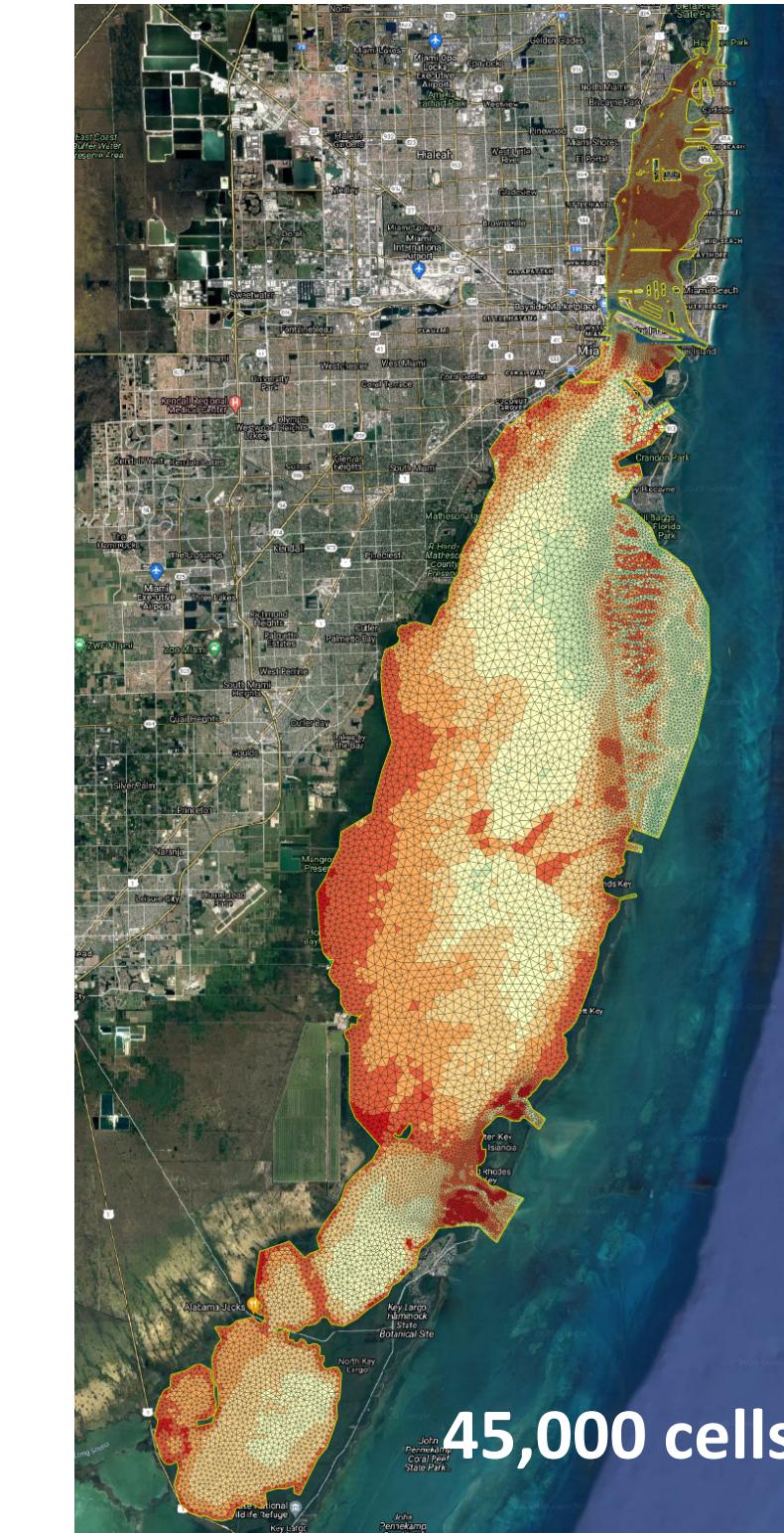
Model area (~17 x 82 km)



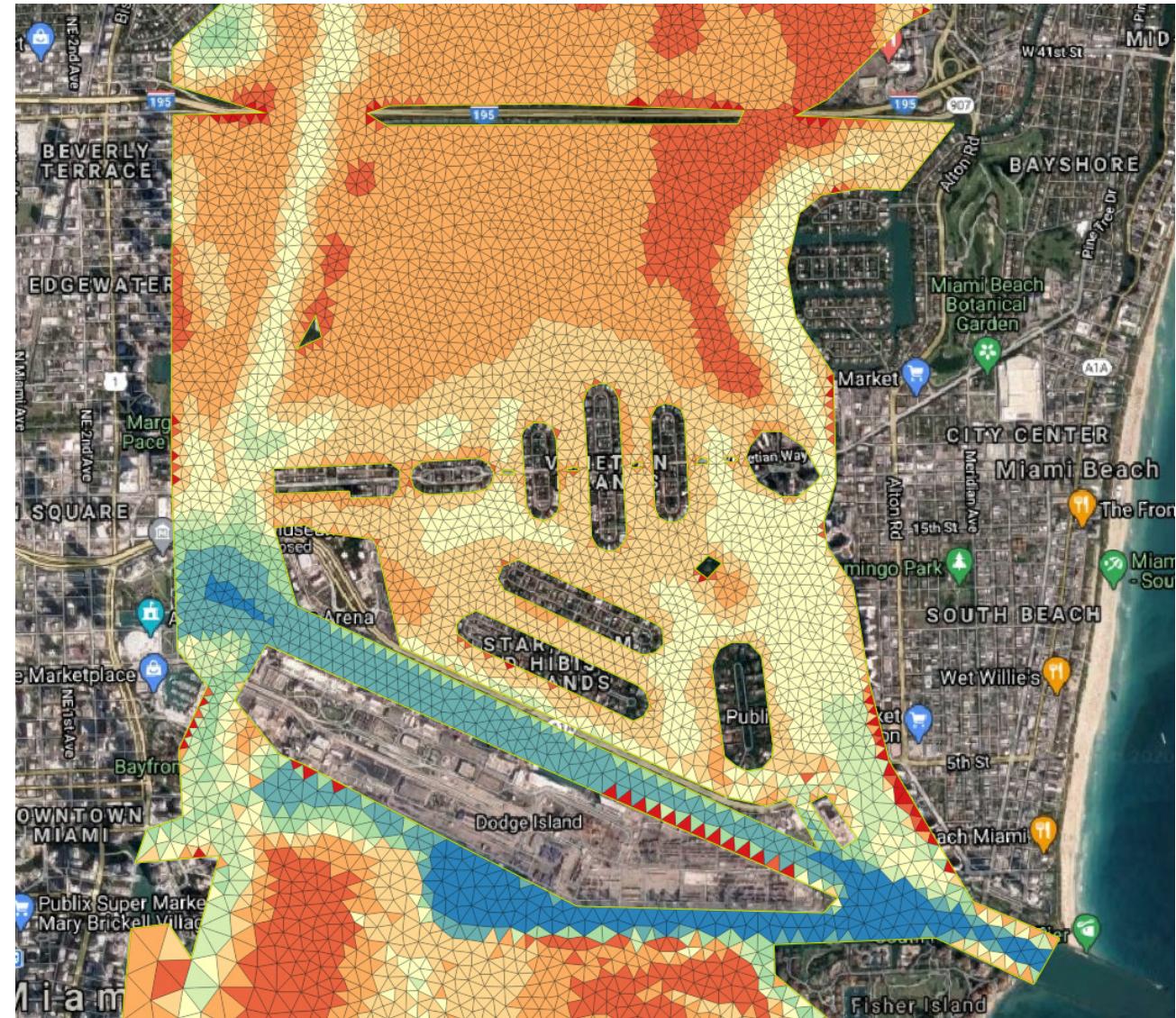
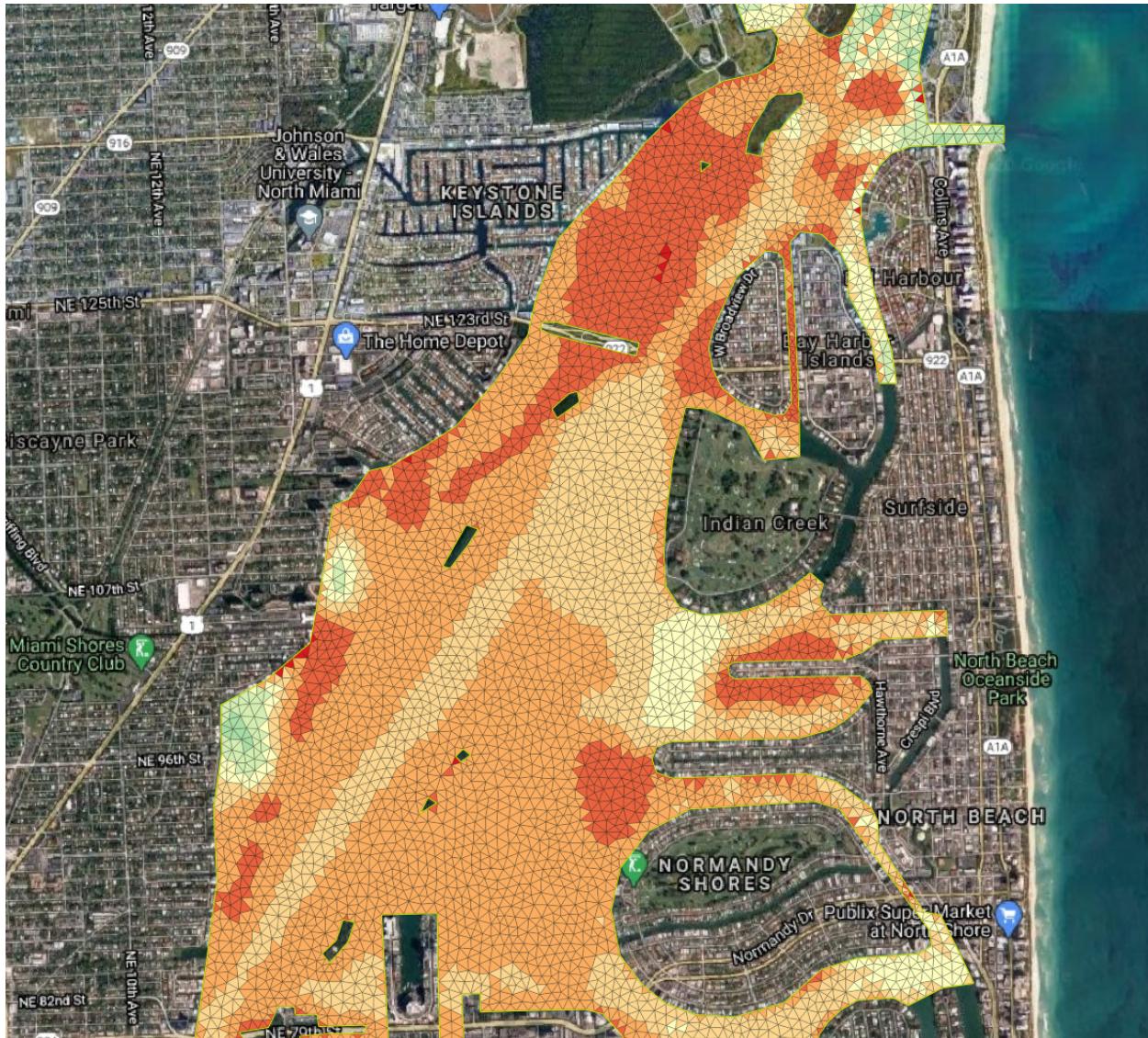
Topo-bathymetry



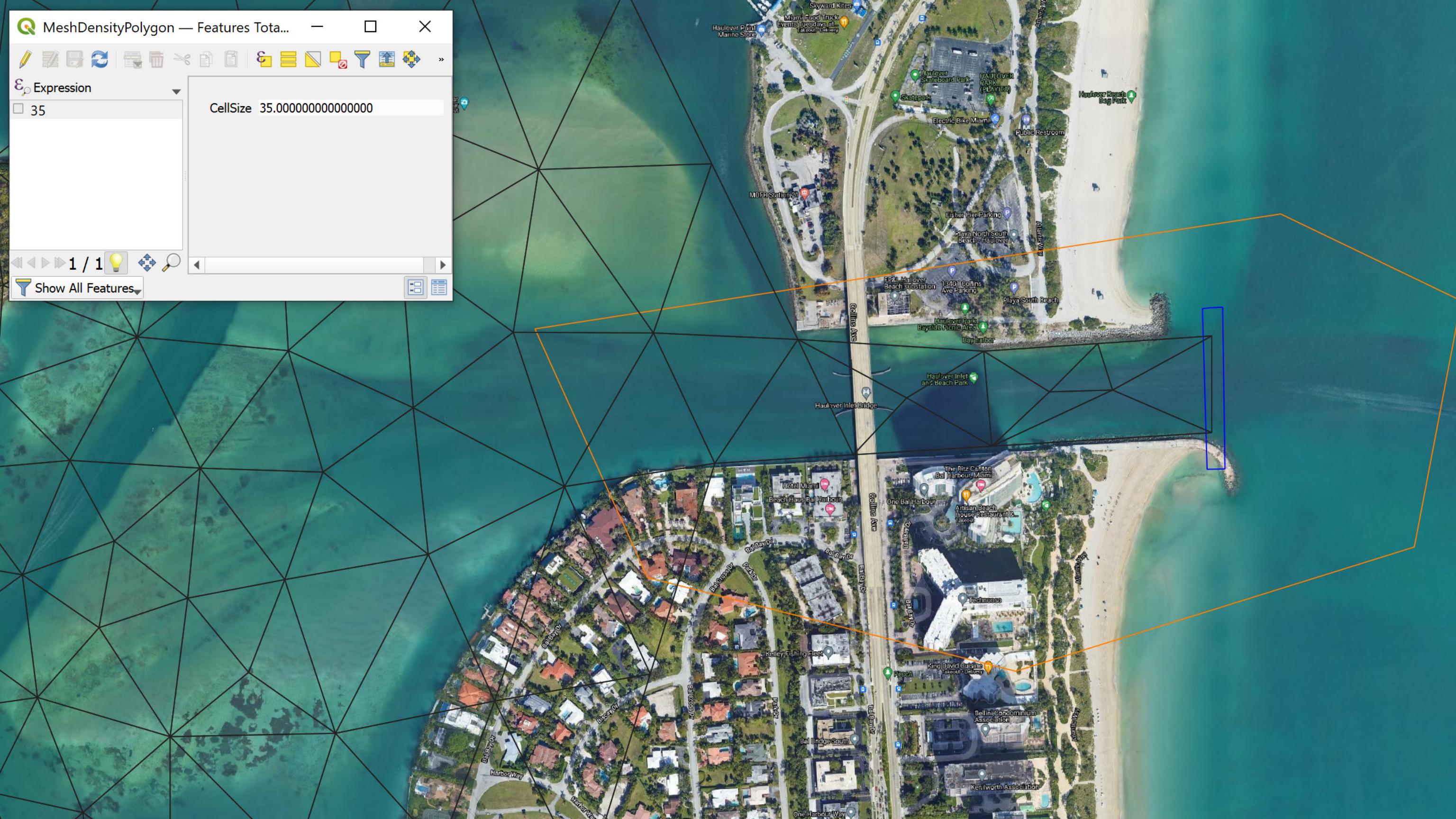
Model mesh



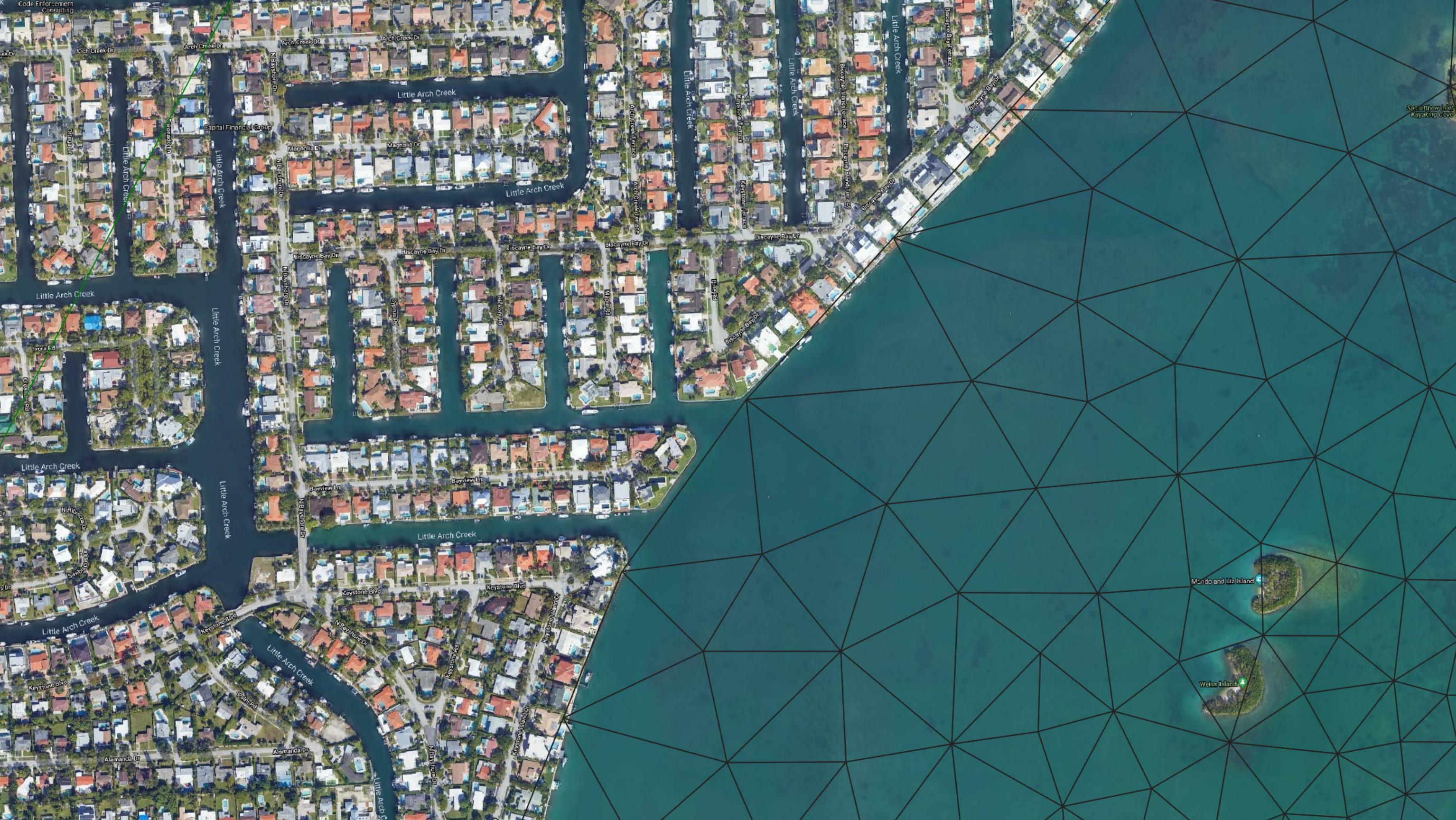
Mesh details









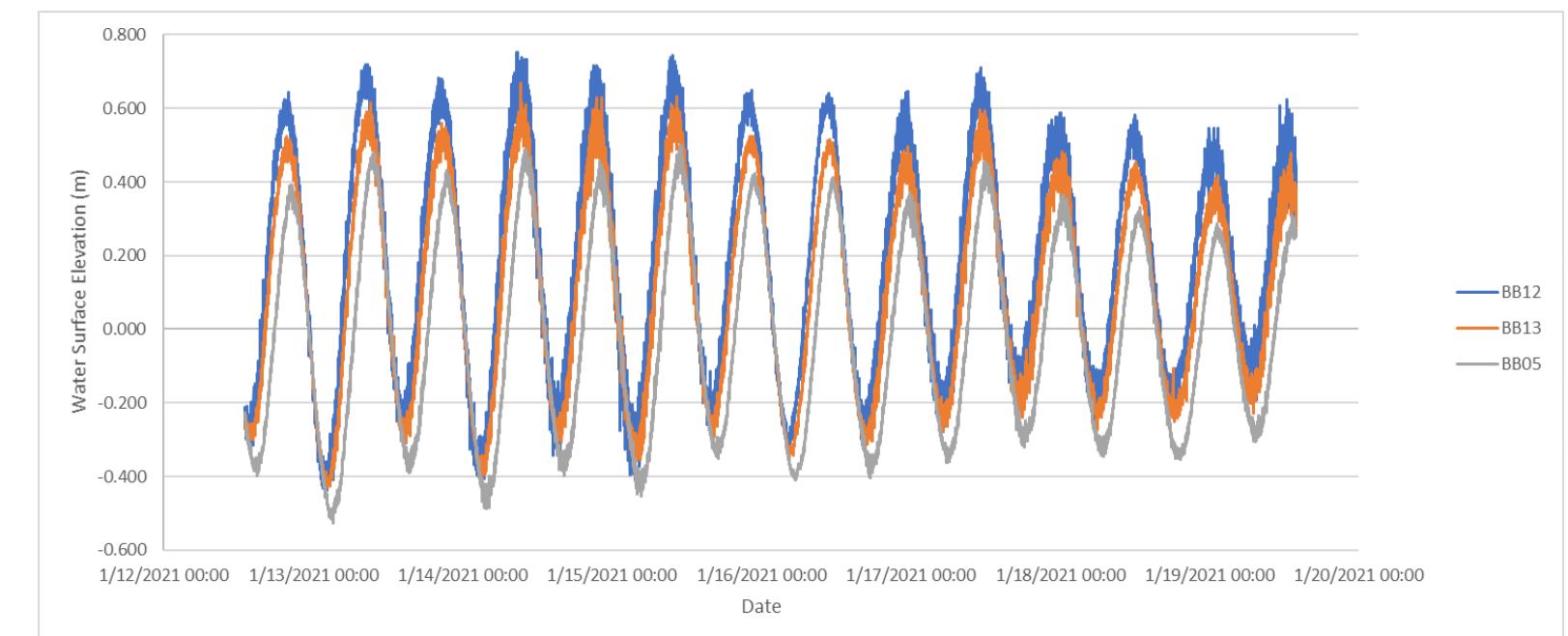
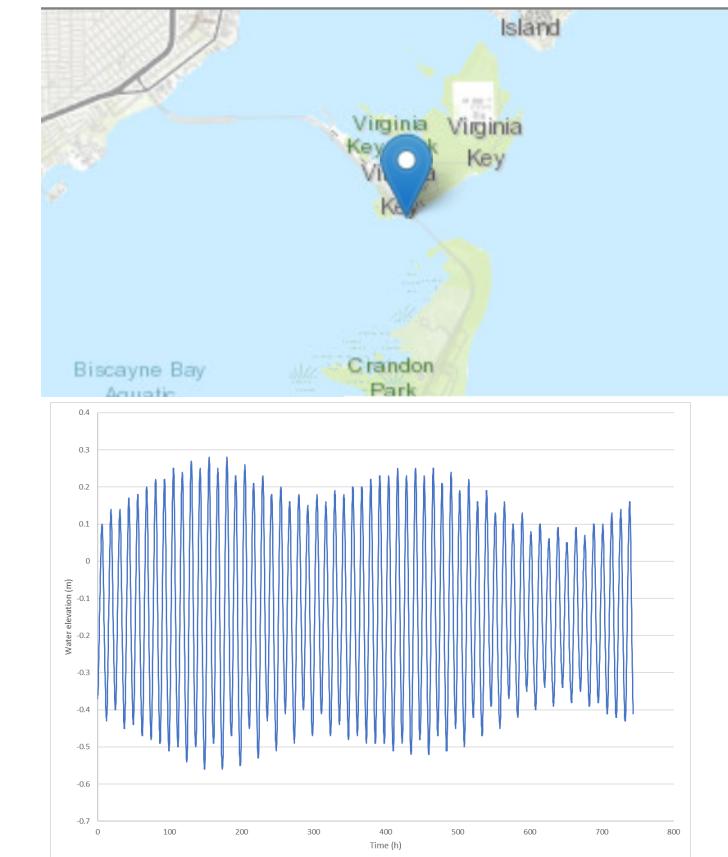




BBOM Implementation

Tides

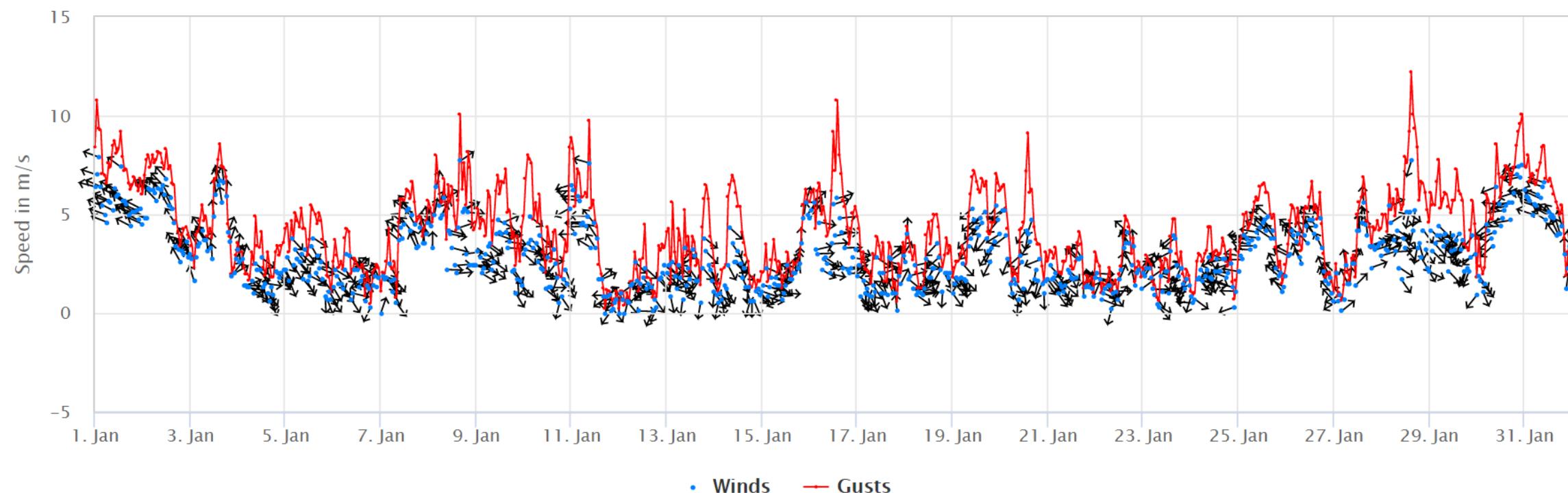
- NOAA Virginia Key station (Station id: 8723214).
- Established on 01/26/1995
- $25^{\circ} 43.9' N, 80^{\circ} 9.7' W$
- <https://tidesandcurrents.noaa.gov/stationhome.html?id=8723214>
- Measured water elevations at BB05, BB12, and BB13 stations from 1/12/2021 and 1/19/2021.



BBOM Implementation

Wind velocity

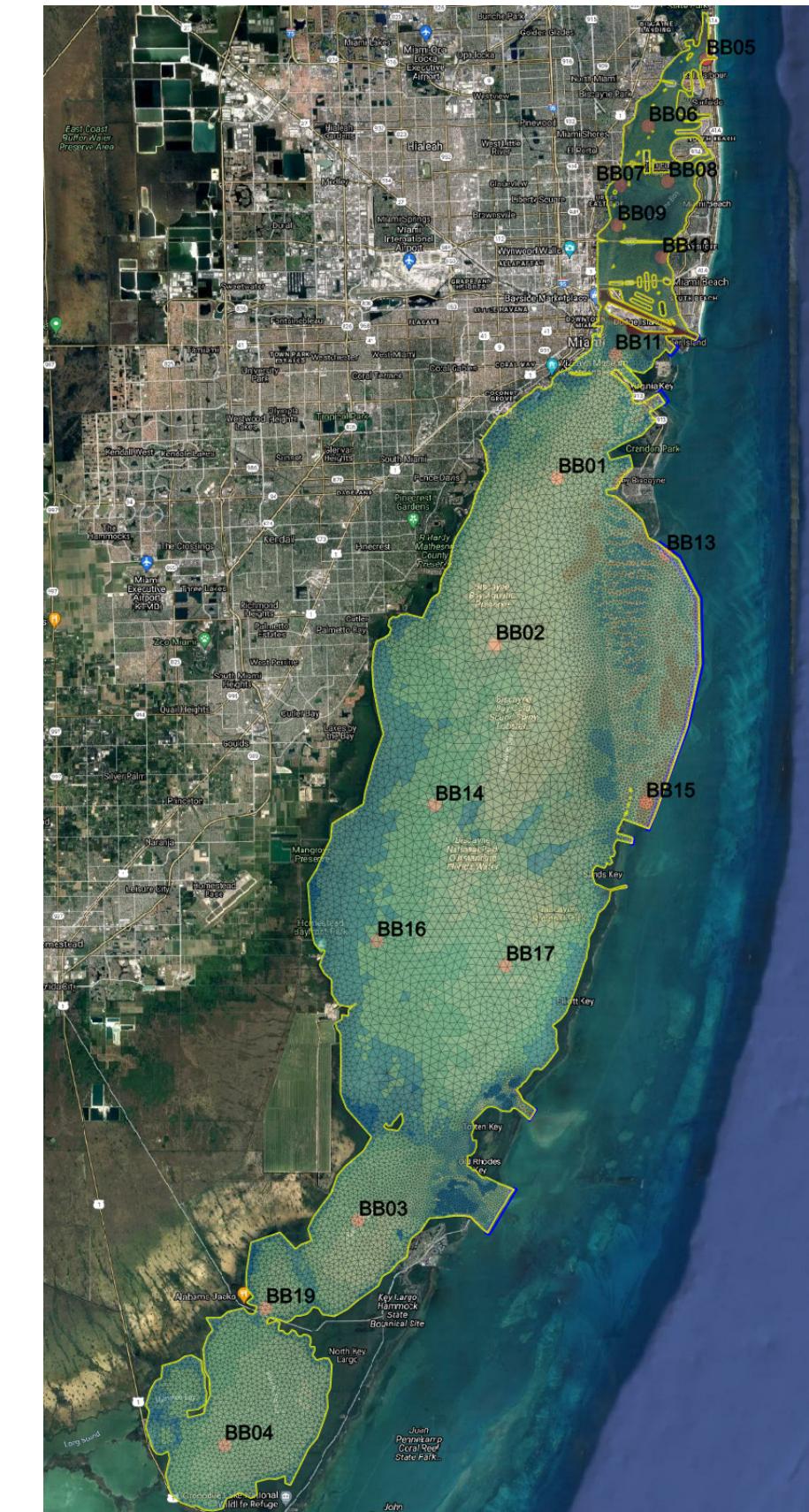
Figure 6 Wind speed at NOAA Virginia Key station 8723214 from 1/01/2021 to 1/31/2021. Source: NOAA/NOS/Center for Operational Oceanographic Products and Services.



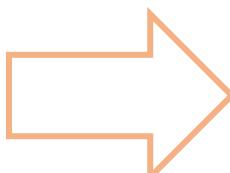
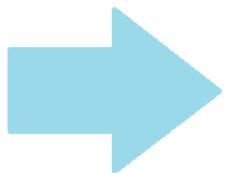
BBOM Implementation

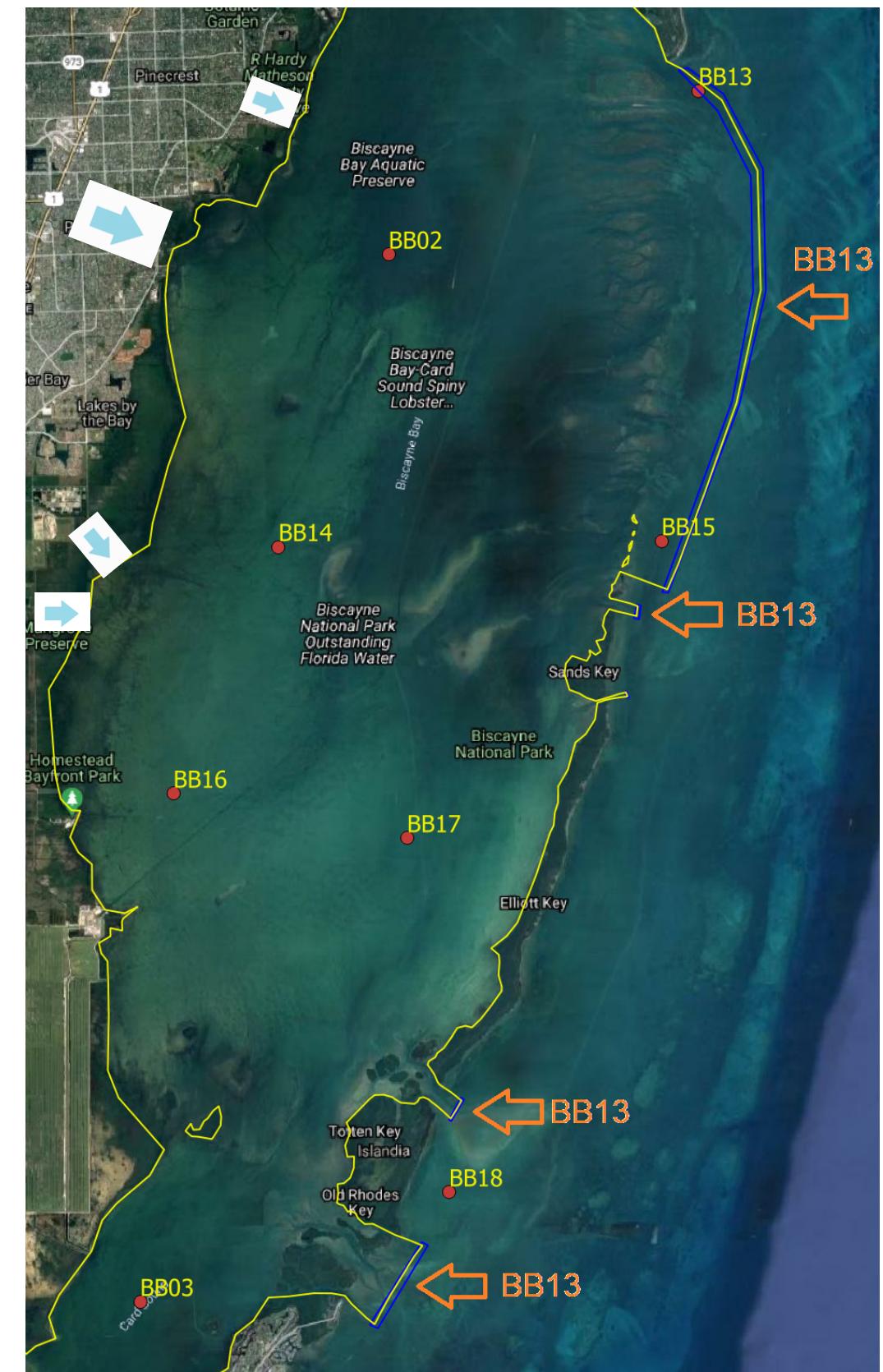
FIU Monitoring Campaigns to collect data for BOM calibration and validation

No.	Measurement campaign time period	
	Start	End
1	2017-10-10	2017-10-17
2	2018-06-20	2018-06-28
3	2019-04-01	2019-04-16
4	2019-10-29	2019-11-13
5	2020-08-19	2020-10-14
6	2021-01-07	2021-01-19



Boundary Conditions

- Tide: WSEL vs time 
- Flowrate Q vs time 
- Flow can enter or leave the mesh through the tide boundaries



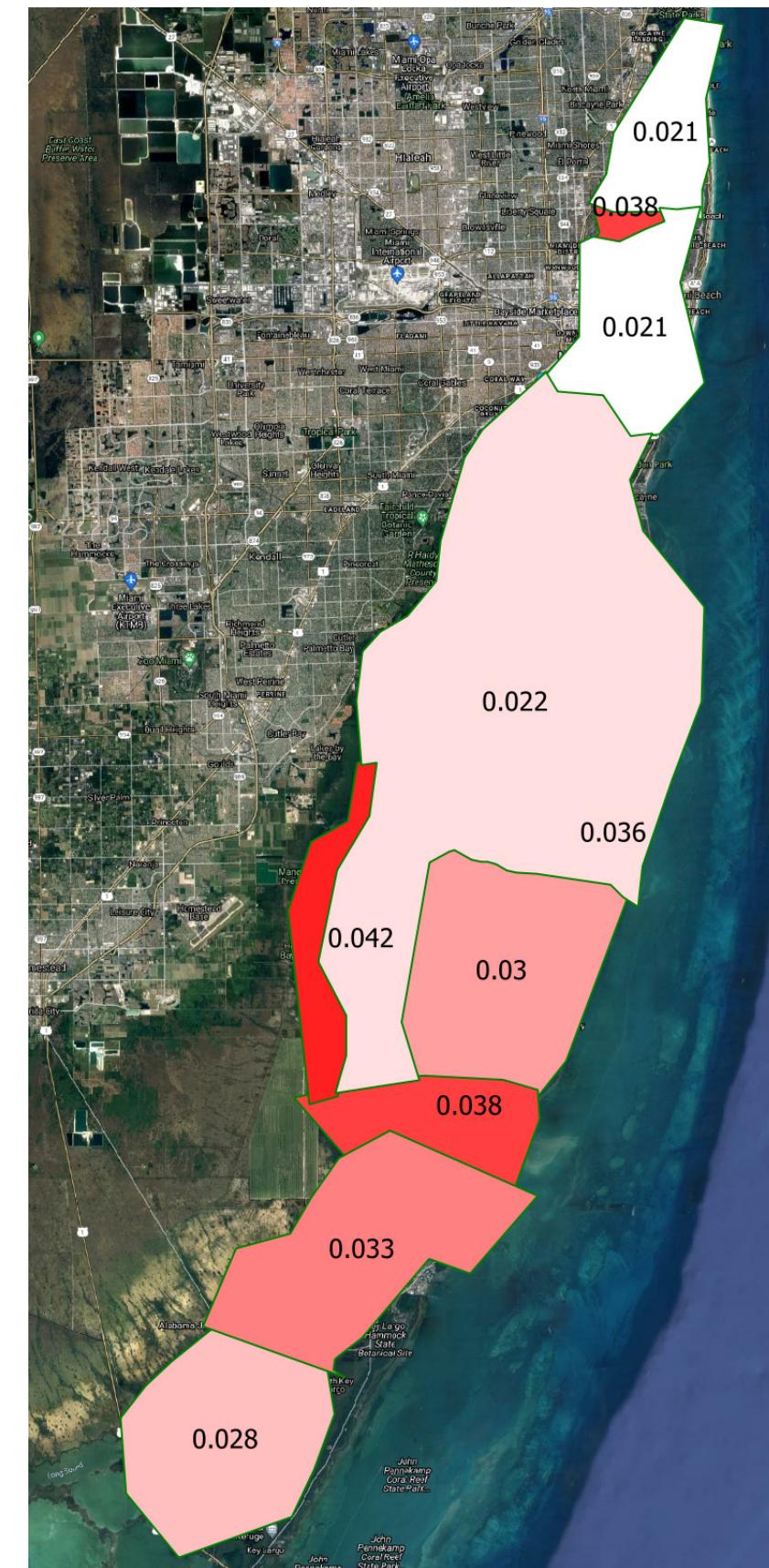
Bottom roughness

- Manning's n coefficient as calibration parameter
- Starting values derived from

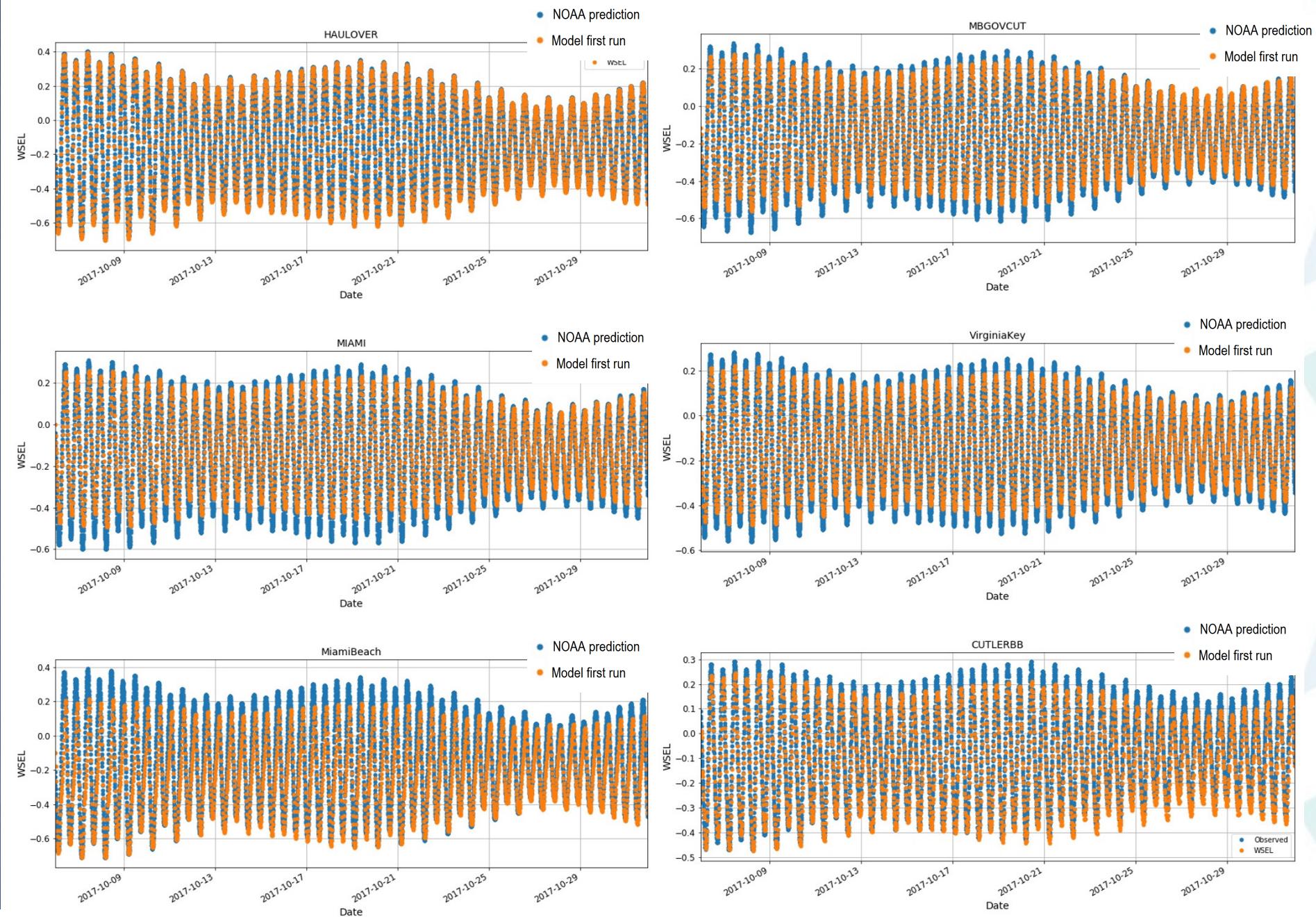
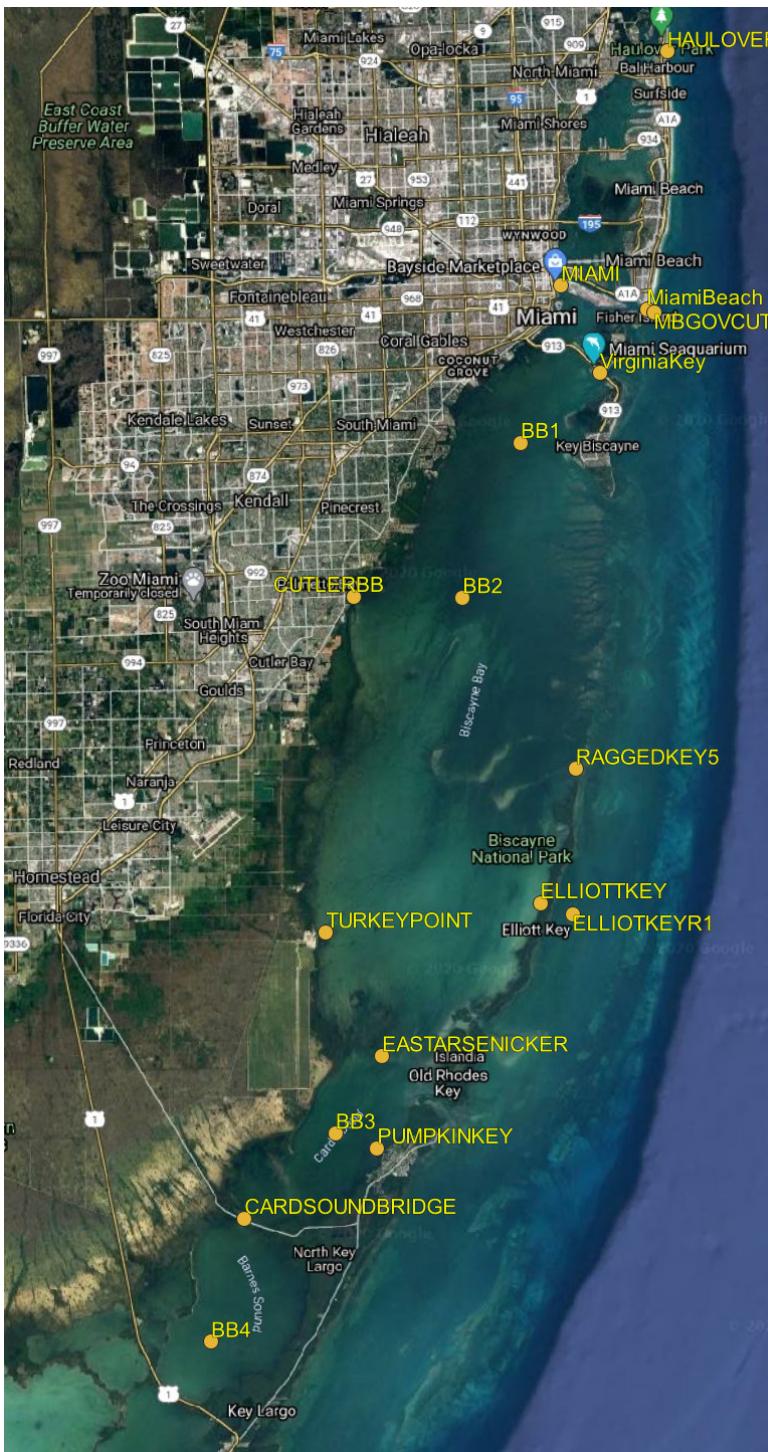
Development of Two-Dimensional Numerical Model of Hydrodynamics and Salinity for Biscayne Bay, Florida

Gary L. Brown, Robert McAdory, Gregory H. Nail,
Maria Soraya Sarruff, R. C. Berger, and Mitch A. Granat

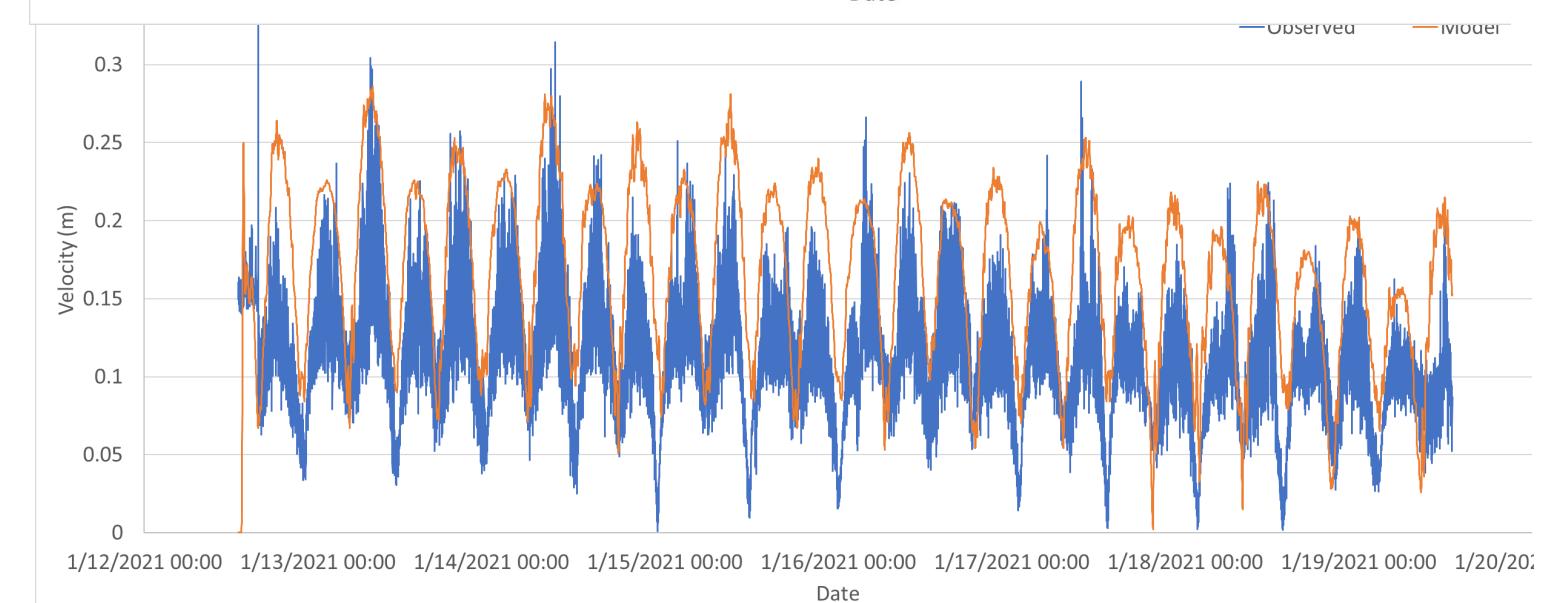
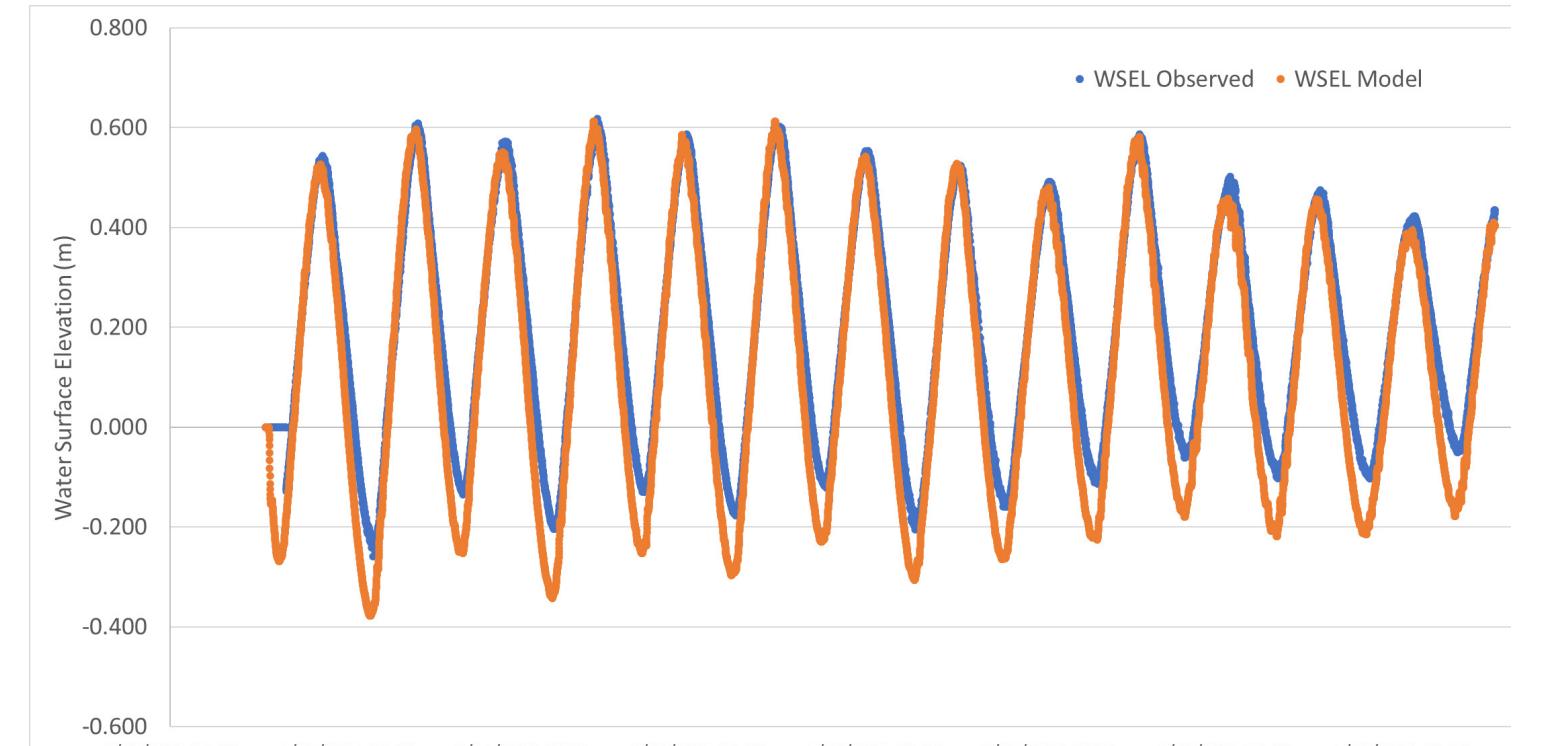
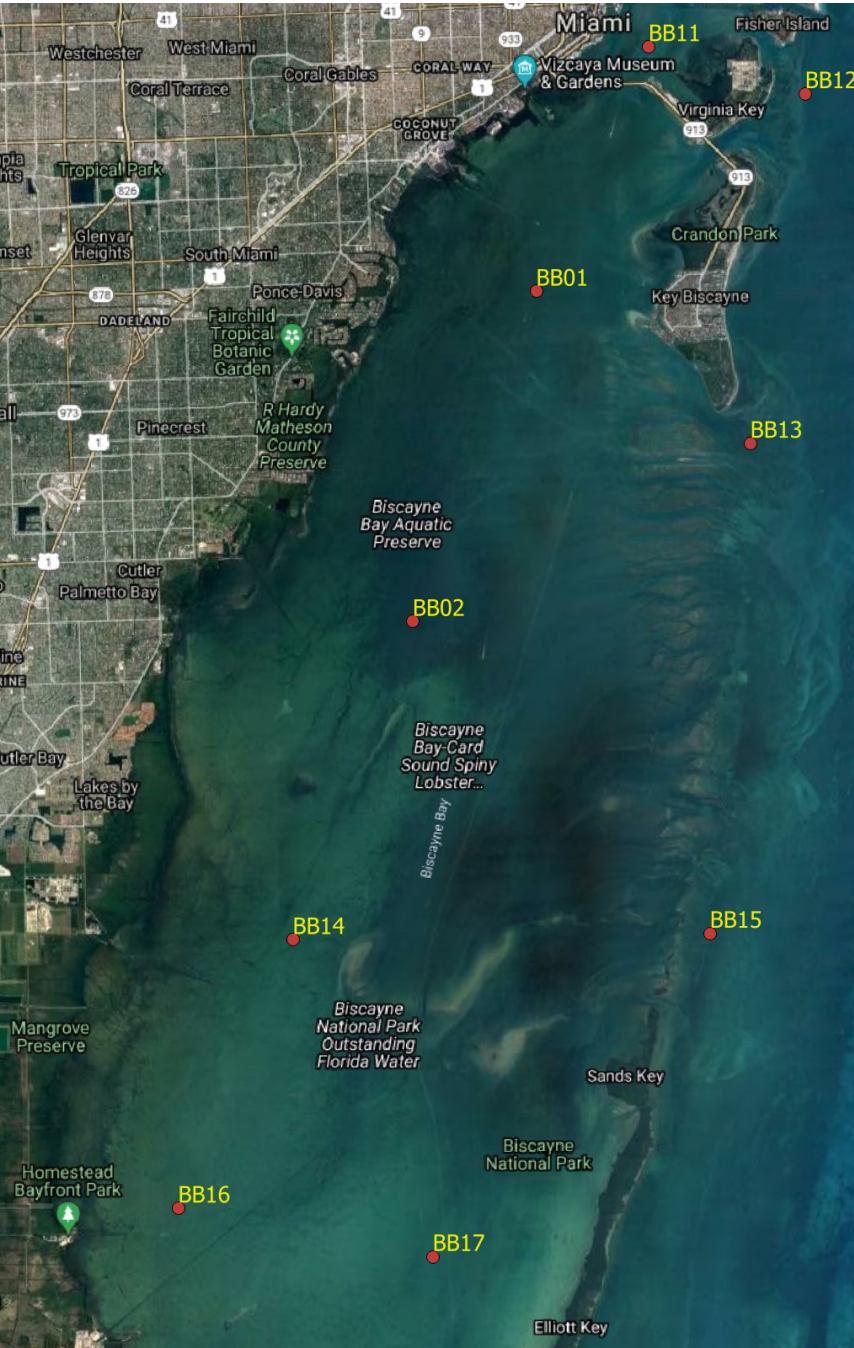
September 2003



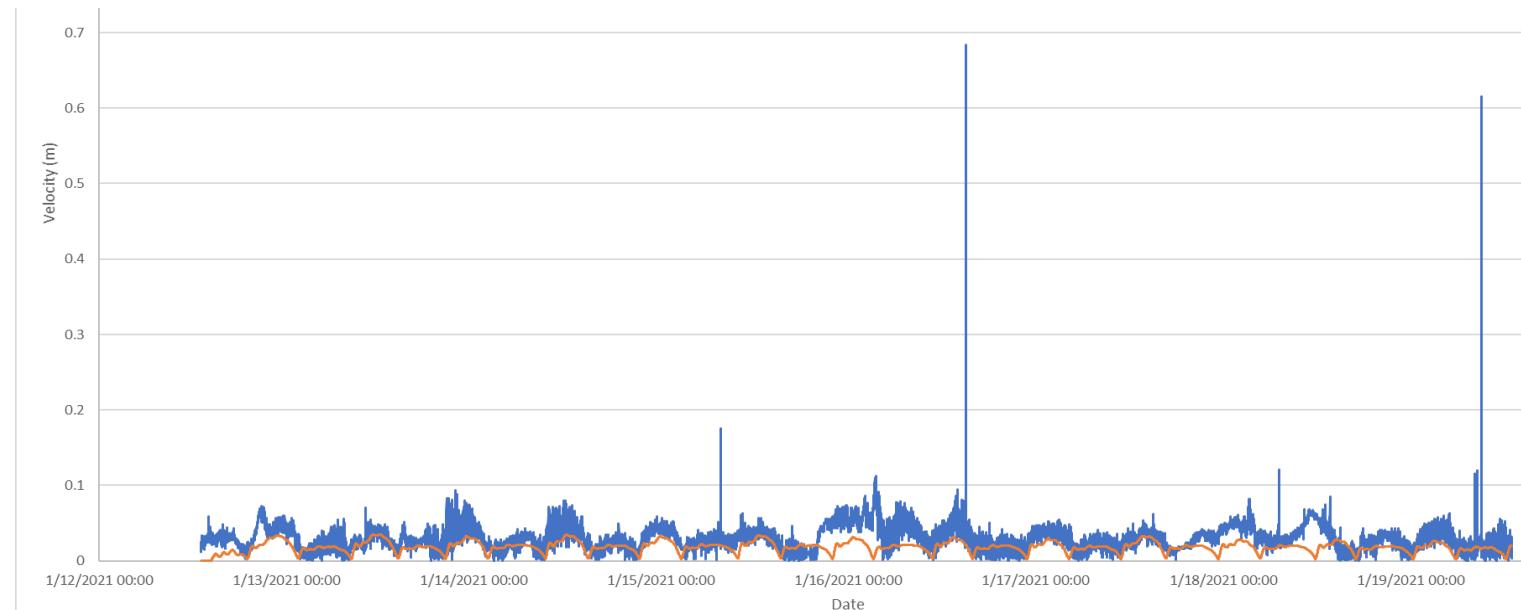
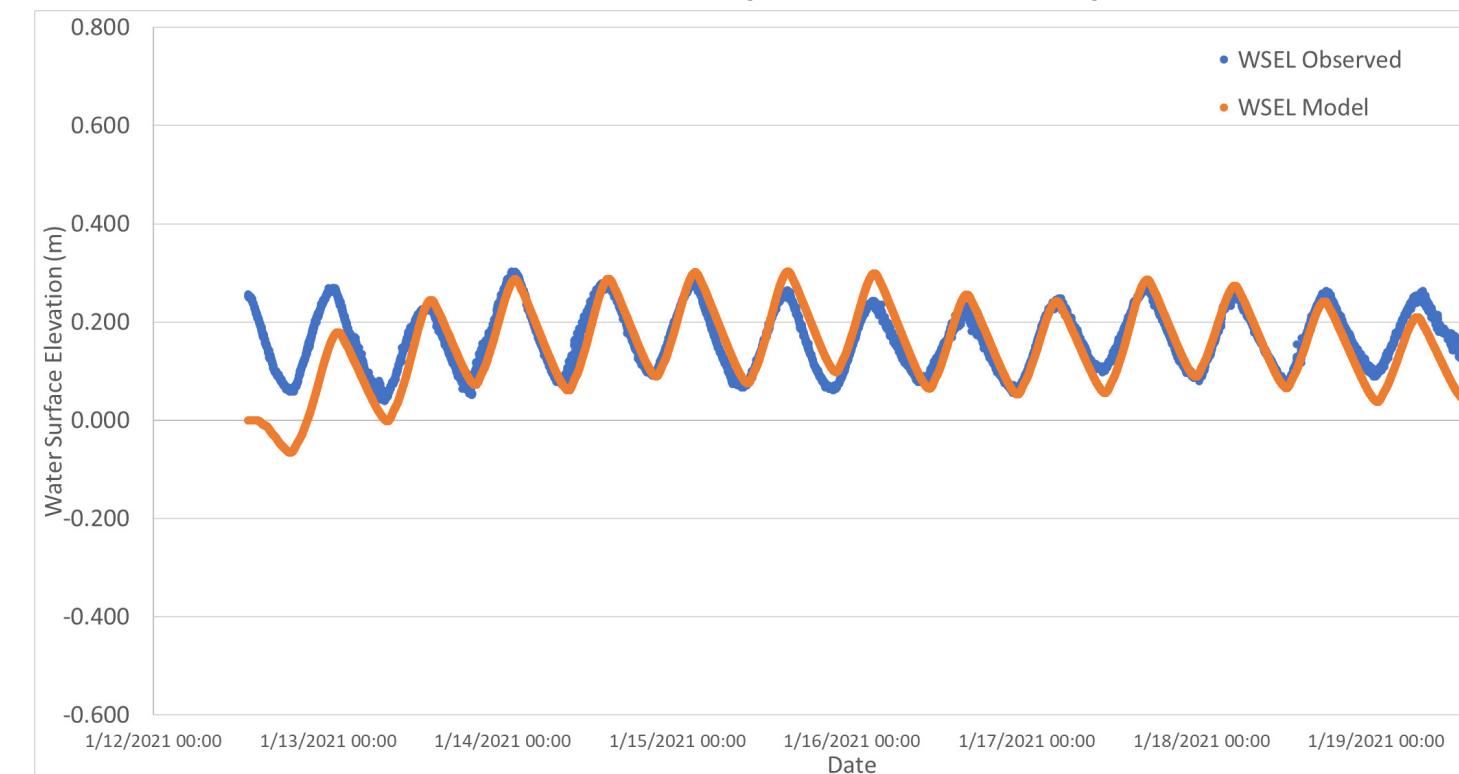
Water elevations (WSEL) from the first calibration run



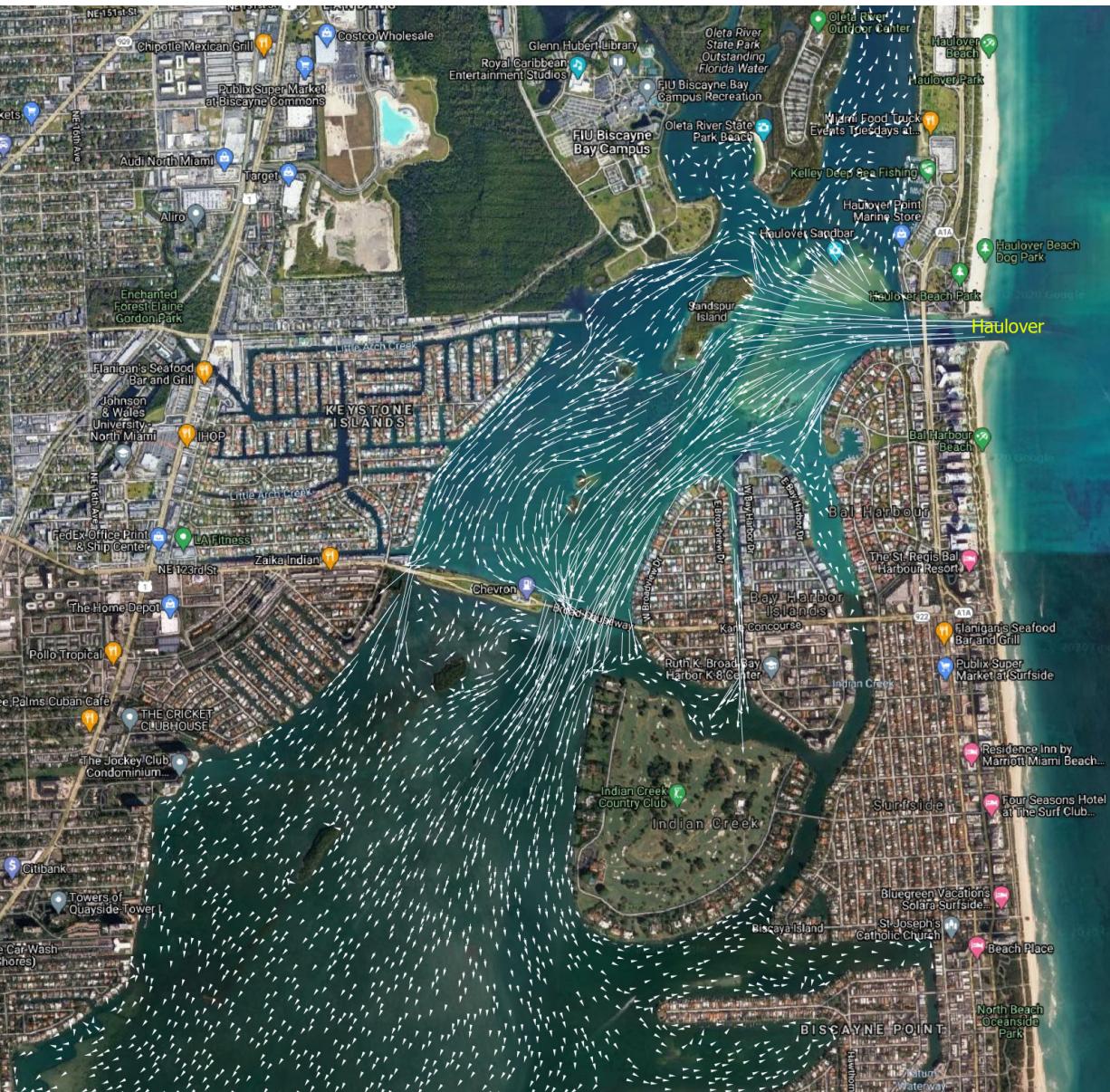
Water elevations (WSEL) and Velocities from the latest validation run (Jan-2021)



Water elevations (WSEL) and Velocities from the latest validation run (Jan-2021)



Some BBOM results



Velocity field near the northern end of Biscayne Bay. Haulover is the northern open boundary in the model.



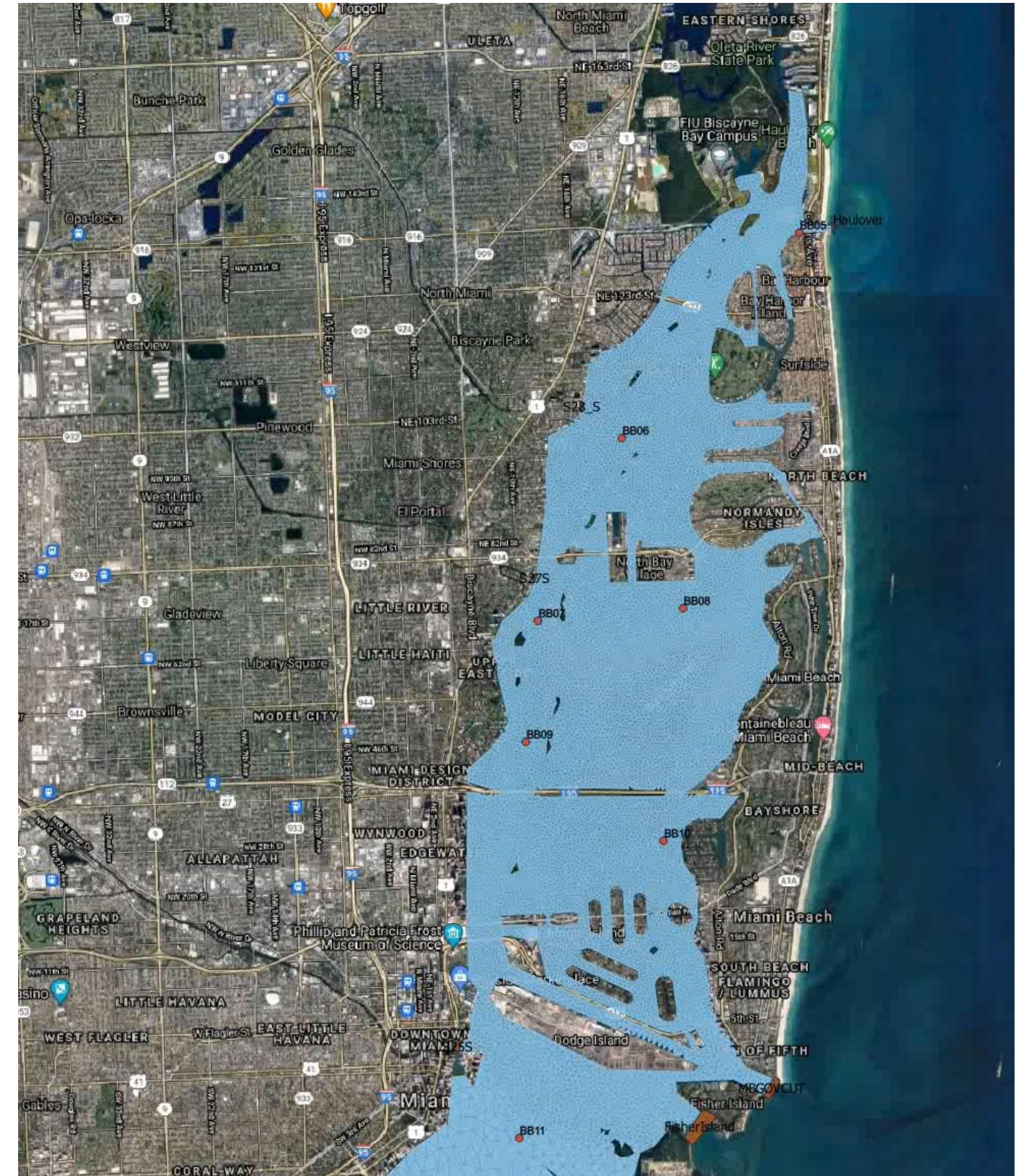
Velocity field between SR 934 and the 195. Note the higher velocities through the 195 bridges and the circulation patterns with large eddies.



Dynamics of Salinity distribution

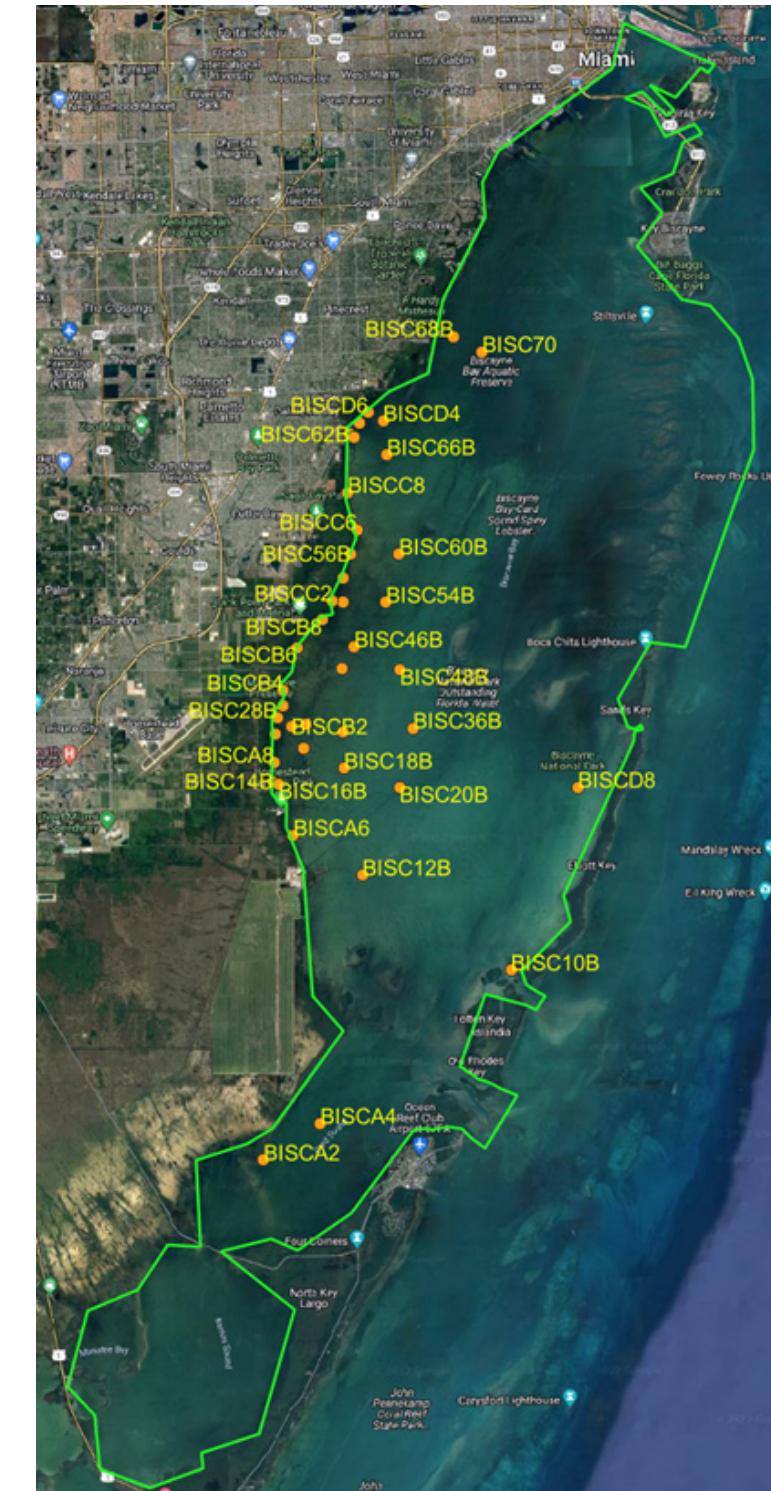


Pollutant dispersion from Miami and Little Rivers



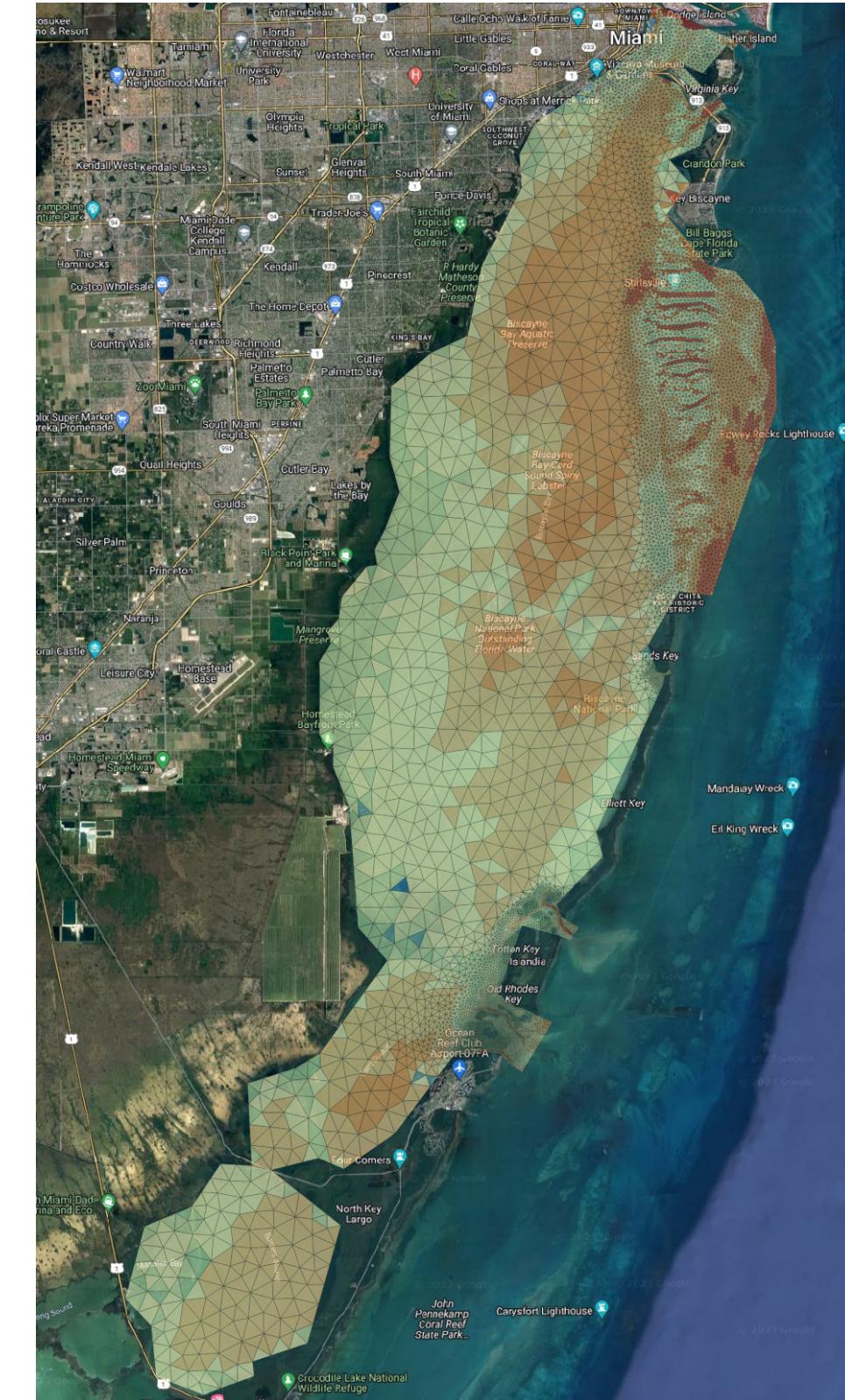
Validation Dataset

- Independent data set provided by the South Florida Water Management District (SFWMD).
- Validation period: One year
 - January 2019 and December 2019.
- Depths and salinities collected at 41 stations.



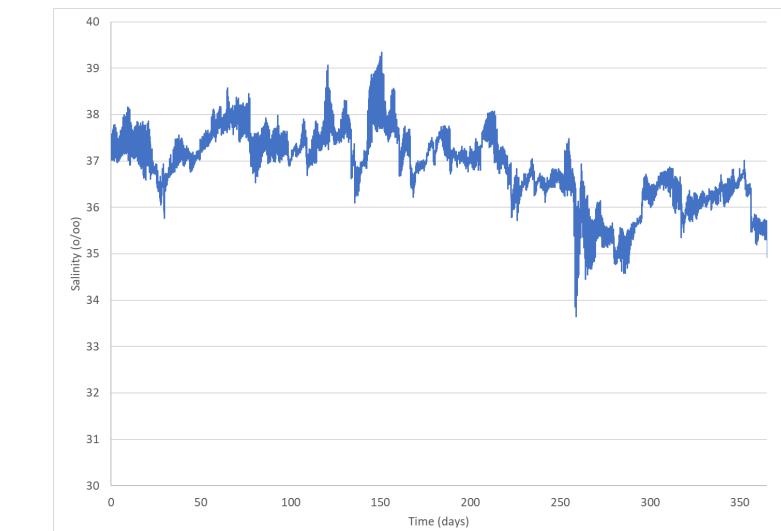
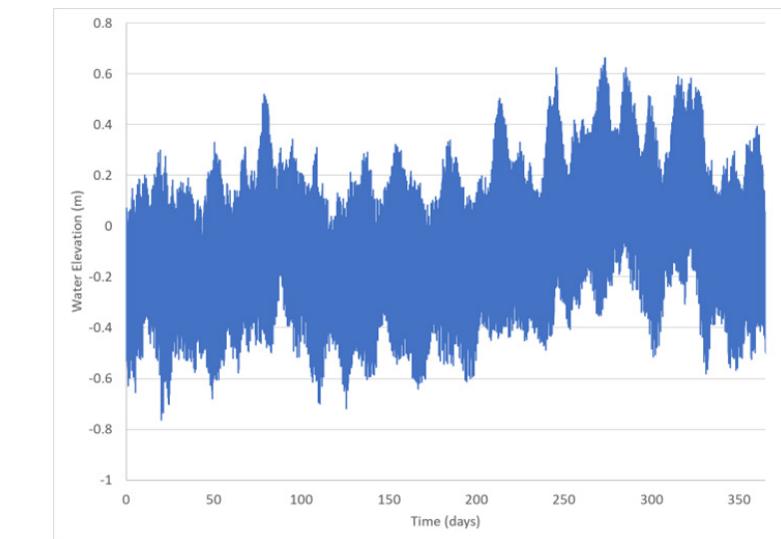
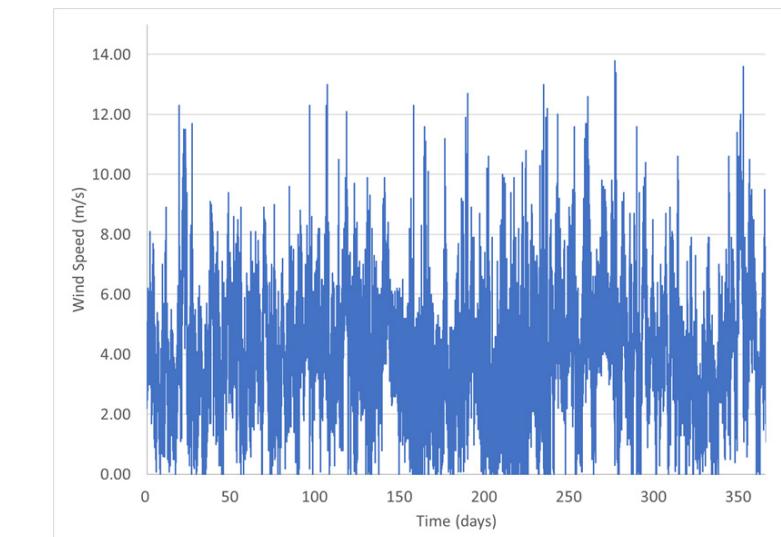
Model Implementation

- ~20,000 cell mesh
- Cell sizes: 26 m-1000 m
- Wind forces
- Tidal boundary conditions at ocean boundaries
- Inflow from canals
- Groundwater *inflow*



Data [January 2019 -December 2019]

Wind velocity NOAA Virginia Key station



Salinity from SFWMD station BISC10B

Some Results

- Comparison of observed vs model water elevations
- Comparison of observer vs model salinities
- Salinity maps and animations

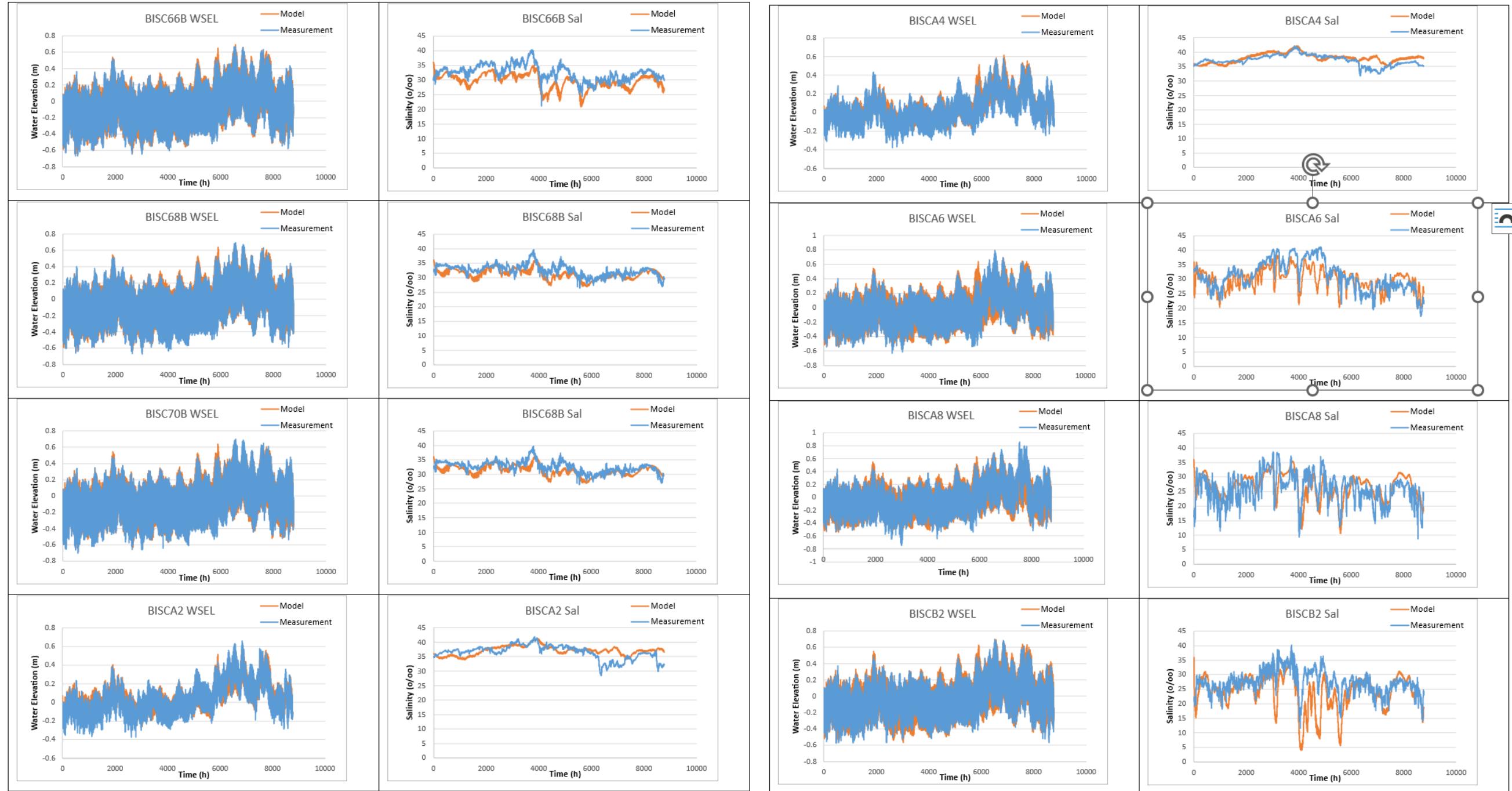


Figure 134 Water Surface elevations and salinities for stations BISC66B, BISC68B, BISC70B, and BISCA2. Comparison of model against measurements.

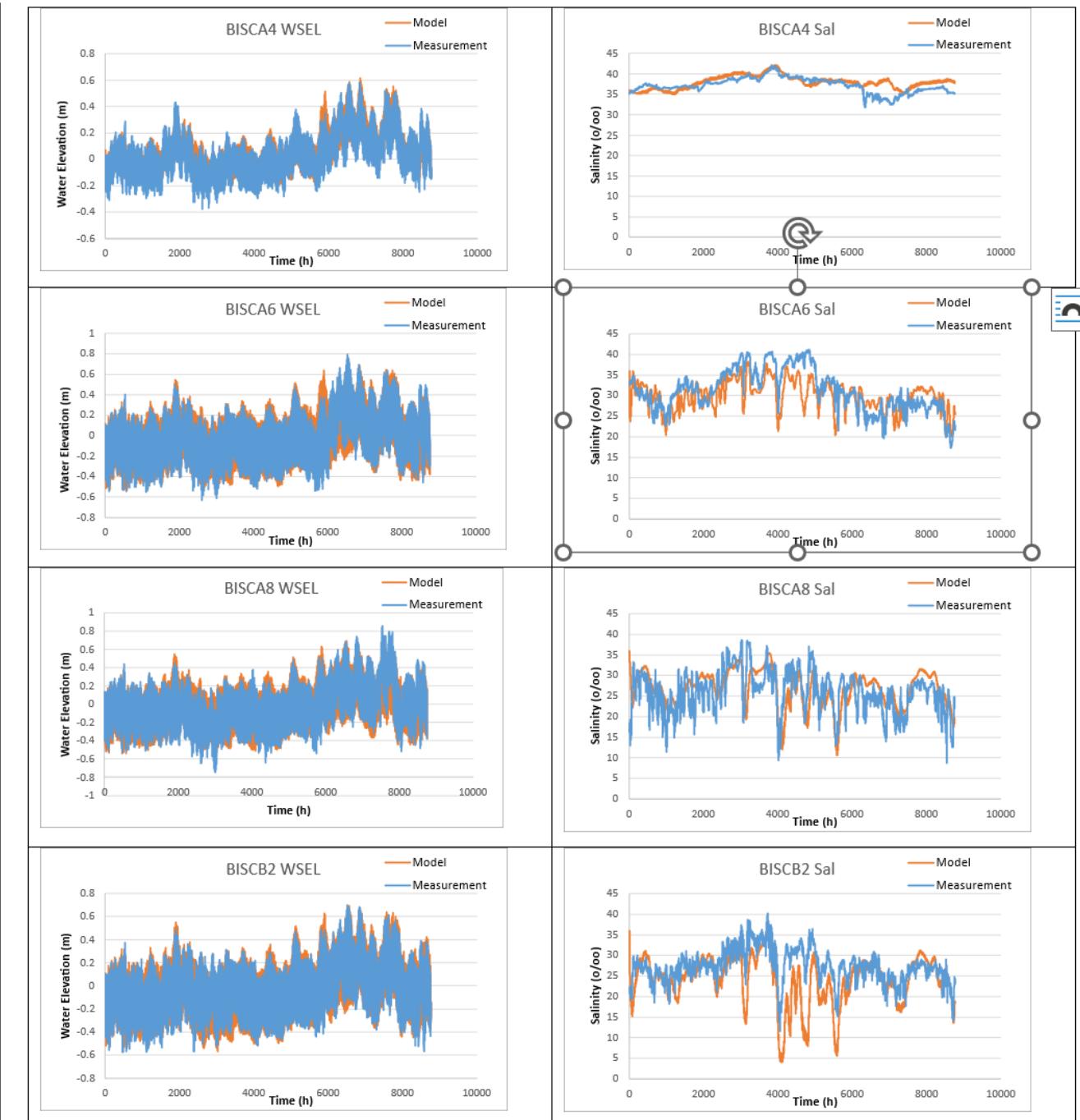


Figure 135 Water Surface elevations and salinities for stations BISCA4, BISCA6, BISCA8, and BISCB2. Comparison of model against measurements.

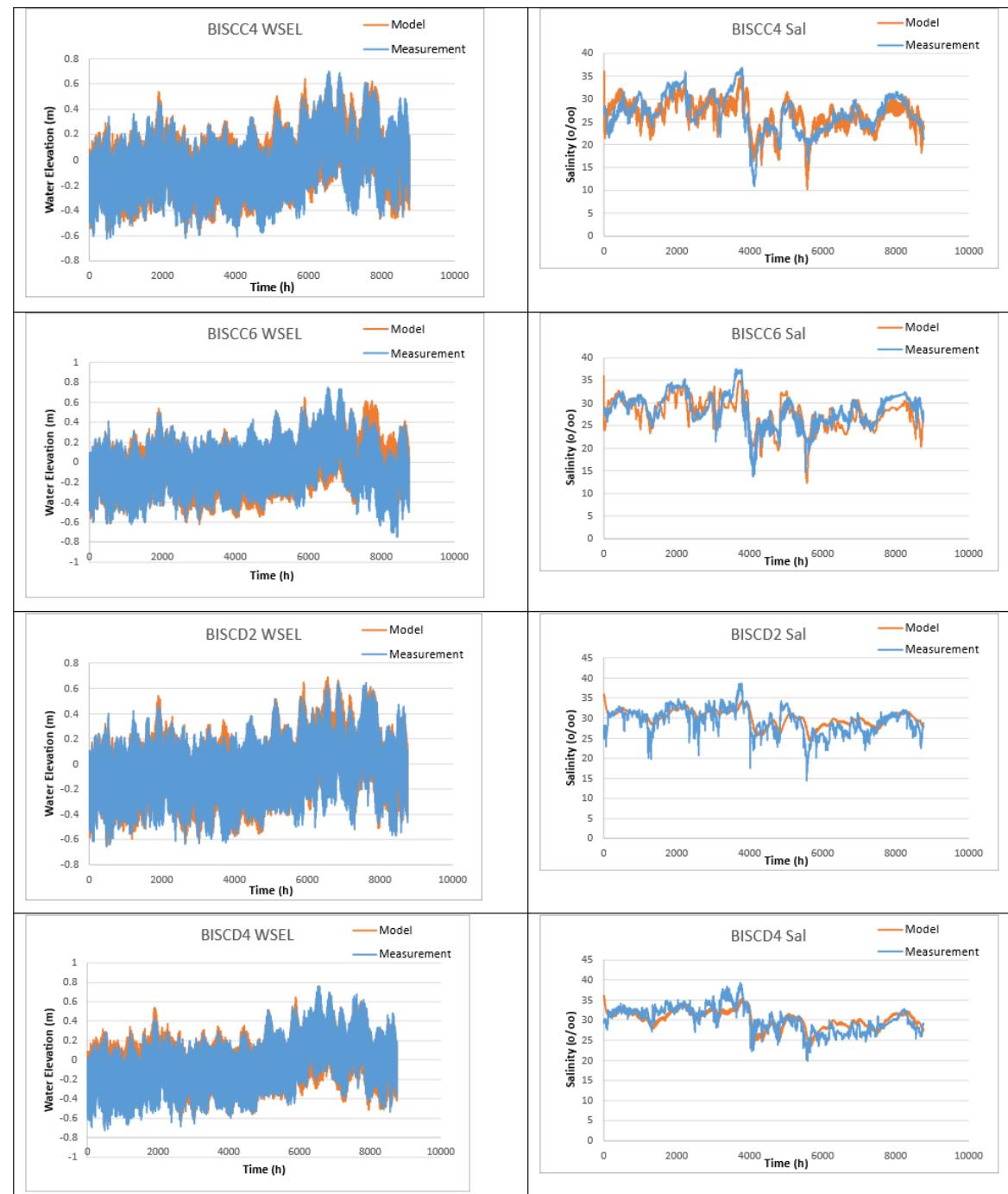


Figure 137 Water Surface elevations and salinities for stations BISCC4, BISCC6, BISCD2, and BISCD4. Comparison of model against measurements.

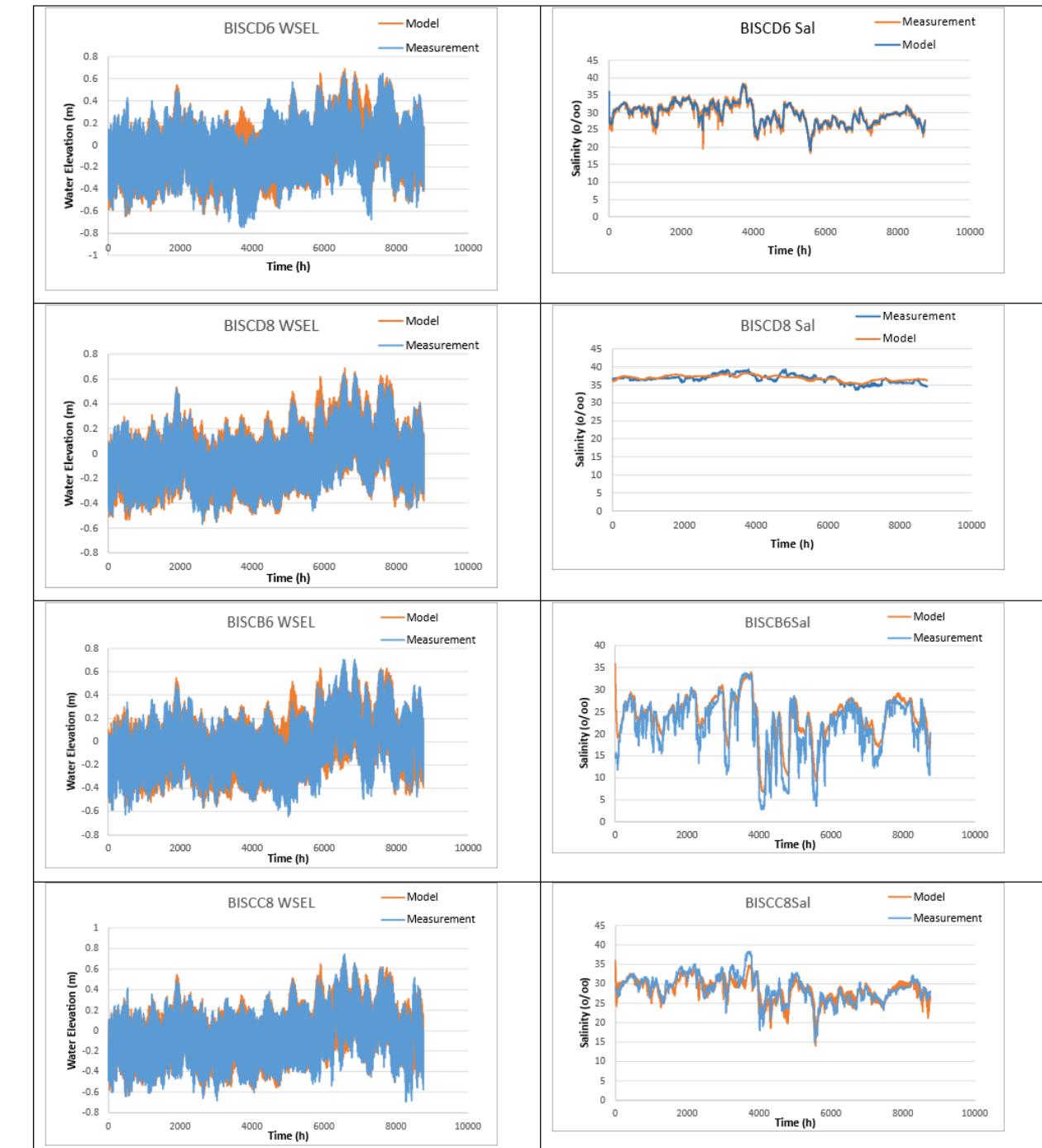


Figure 138 Water Surface elevations and salinities for stations BISCD6, BISCD8, BISCB6, and BISCC8. Comparison of model against measurements.

Table 4 Correlation Quality Indexes obtained for BBOM validation.

Station	Water Surface Elevation Correlation Index	Salinity Correlation Index
BISC10B	94.46	93.67
BISC12B	92.57	45.16
BISC14B	90.02	82.74
BISC16B	91.31	73.14
BISC18B	92.72	33.53
BISC20B	91.46	40.18
BISC22B	90.16	64.33
BISC26B	92.52	26.14
BISC28B	90.10	65.49
BISC32B	92.11	34.26
BISC34B	92.73	25.24
BISC36B	93.70	37.00
BISC40B	91.29	76.64
BISC44B	92.63	48.76
BISC46B	92.76	57.00
BISC48B	91.96	53.20
BISC52B	91.80	67.97
BISC60B	93.47	54.30
BISC62B	91.06	60.95
BISC64B	91.40	66.45
BISC66B	93.38	64.59
BISC68B	94.49	62.54
BISC70	94.34	61.57
BISCA2	93.55	37.30
BISCA4	92.90	62.99
BISCA6	90.79	66.33
BISCA8	89.68	56.24
BISCB2	92.10	51.30
BISCB4	91.99	76.00
BISCB8	91.06	72.76
BISCC2	89.17	61.45
BISCC4	91.58	72.12
BISCC6	88.59	70.70
BISCD2	91.07	68.96
BISCD4	91.85	75.16
BISCD6	88.70	96.60
BISCD8	93.72	76.81
BISC54B	89.42	91.60
BISC56B	91.31	84.23
BISC6	92.76	51.06
BISCC8	89.96	64.32

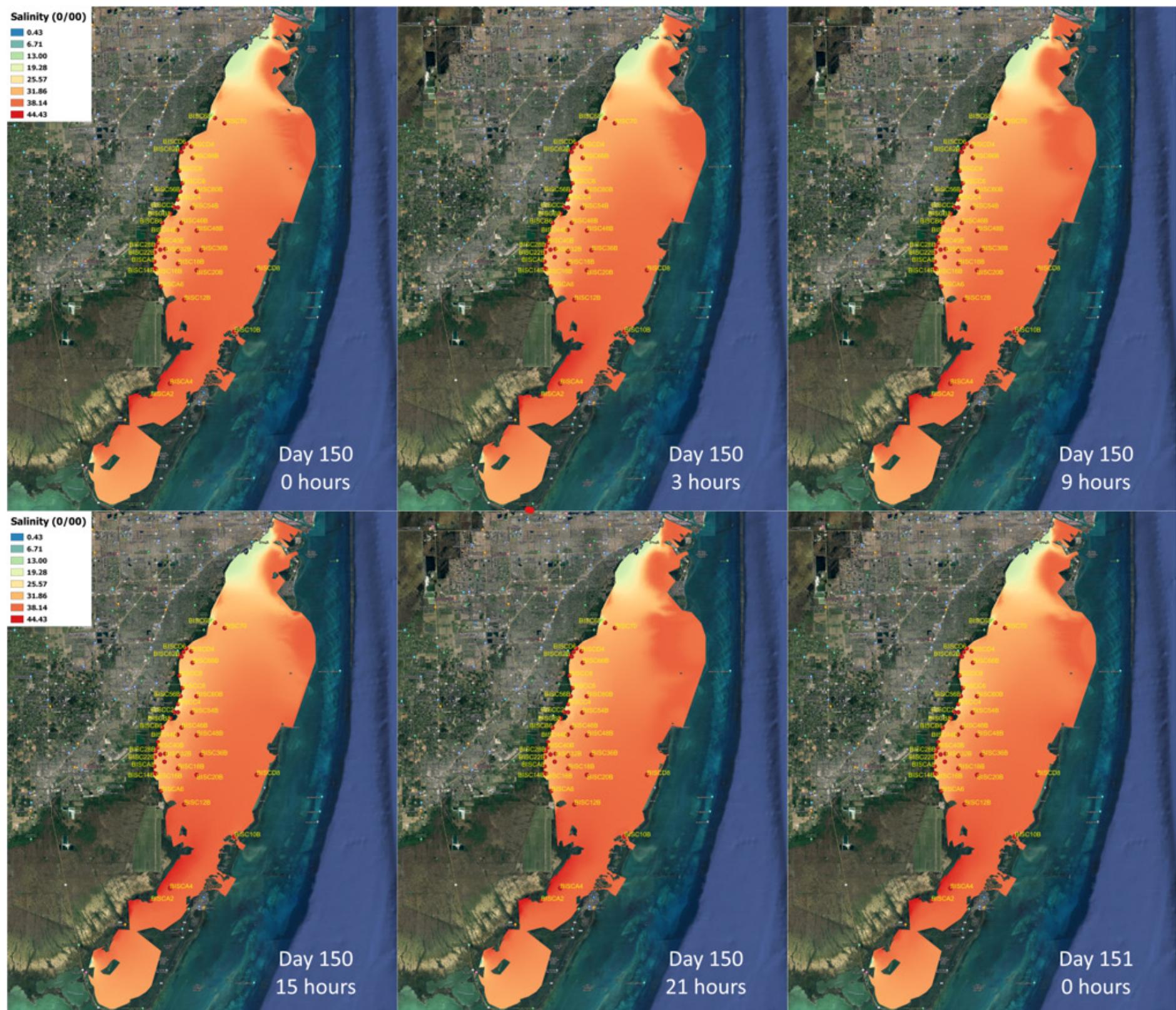
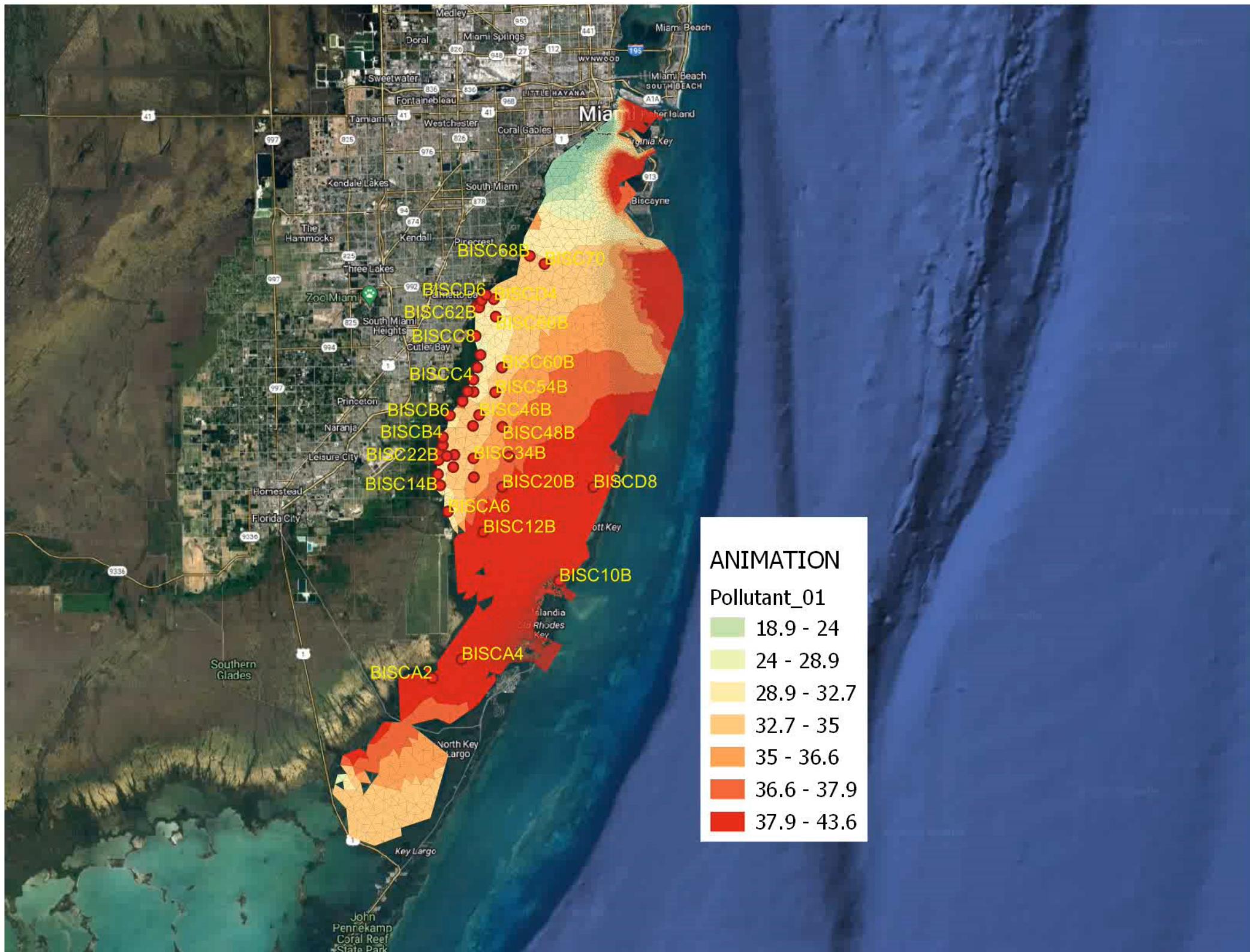


Figure 142 Salinity distribution at time 150 days, and 0, 3, 9, 15, and 21 hours.

Salinity Dynamics in Biscayne Bay [Day 150 to day 180] validation run. Feb. 2023.



BBOM Application Comments

- The results show that the model was able to reproduce measured and predicted water elevations and velocities in several Biscayne Bay locations with acceptable precision.
- Average Correlation Quality Indexes obtained during validation were for water elevations >90% and for salinity >71%.
- We found it essential to consider the combined effects of freshwater inflows from canals and groundwater, tidal forcing on the ocean boundaries, and wind stress on the water surface to be able to model water levels and salinities.
- BBOM triangular-mesh numerical engine can be adapted to irregular geometries and makes use of high-performance parallelized computations that run in multiple processor GPU hardware reducing significantly reducing runtimes of long-term scenarios.
- BBOM Graphical User Interface (GUI) based on the Open Source Geographical Information System QGIS provides a comprehensive and easy-to-use set model customization and visualization tools, including map rendering, and animations, facilitating the analysis of results.

GPU Acceleration (48h)

NVIDIA RTX 4090 GPU	
Memory	24 GB
Cores	16,384



Mesh	No. Cells	Intel CPU	RTX 4090	Max Speedup
Mesh 1	25,290	00:00:11:50	00:00:01:49	7x
Mesh 2	414,655	00:04:12:52	00:00:04:39	54x
Mesh 3	1,006,937	00:14:05:18	00:00:12:13	69x

HYDRONIA



Tony Hisgett / Wikimedia Commons / CC BY 2.0 • James T M Towill / CC BY-SA 2.0

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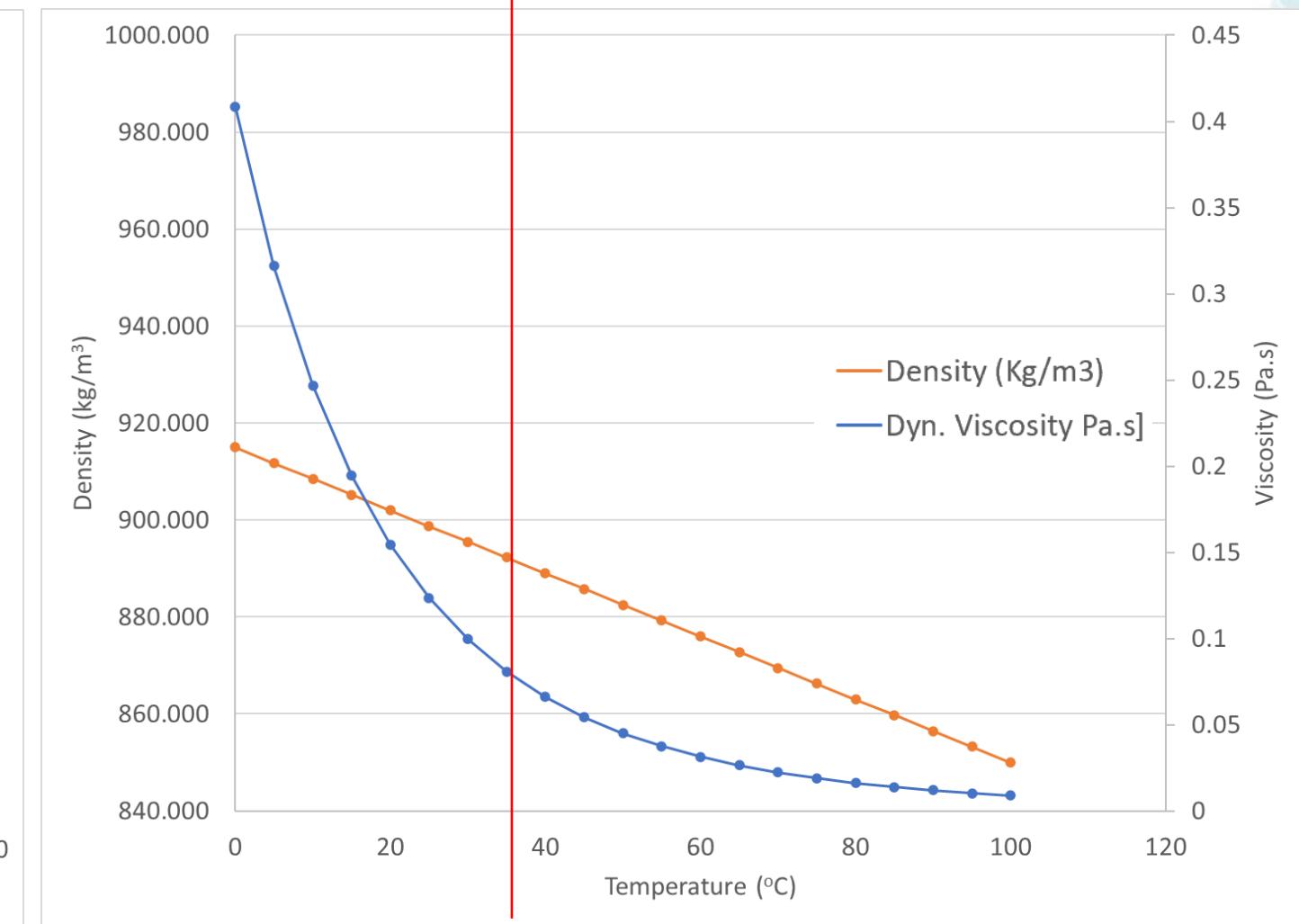
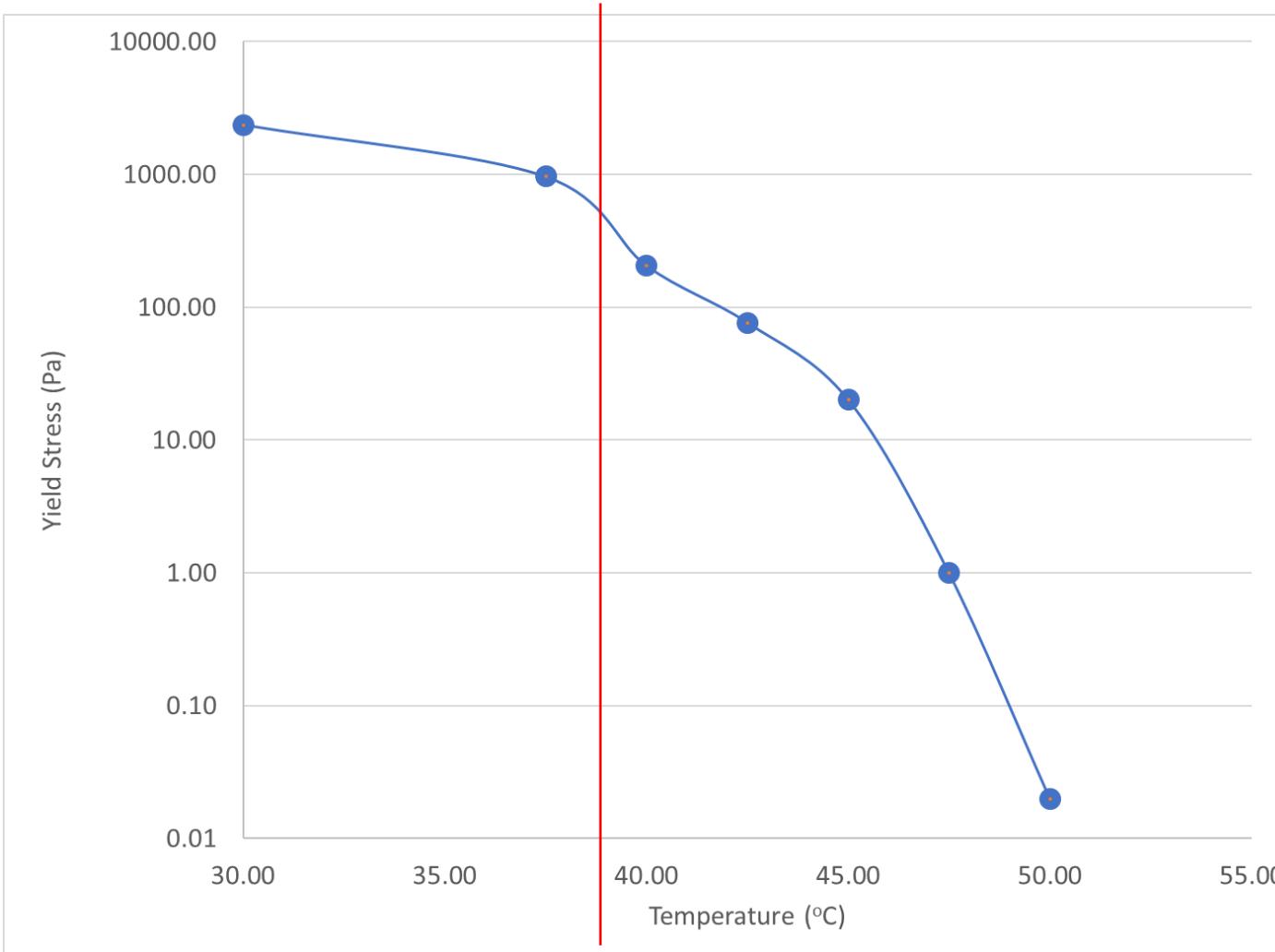
Oil Storage Tank Break and Oil Spills from Pipelines

Modeling Oil Spills on Land Objectives

- Determine the affected area caused by crude oil spills
- Where and when...
- Assessing if the oil is going to hit high consequence zones
 - Urban areas
 - Sensitive ecosystems
 - Etc.
- Oil spills from
 - Well blowouts
 - Pipelines
 - Tanks
- *Considering the dependence of the Yield Stress, Viscosity and Density on Temperature, is crucial in estimating flow runout distance and general overland flow for some crude oils*



High Pour Point Crude Oils



Pour point: The temperature below which the liquid loses its flow feasibility.

Yield stress: The shear stress required to make the fluid flow possible.

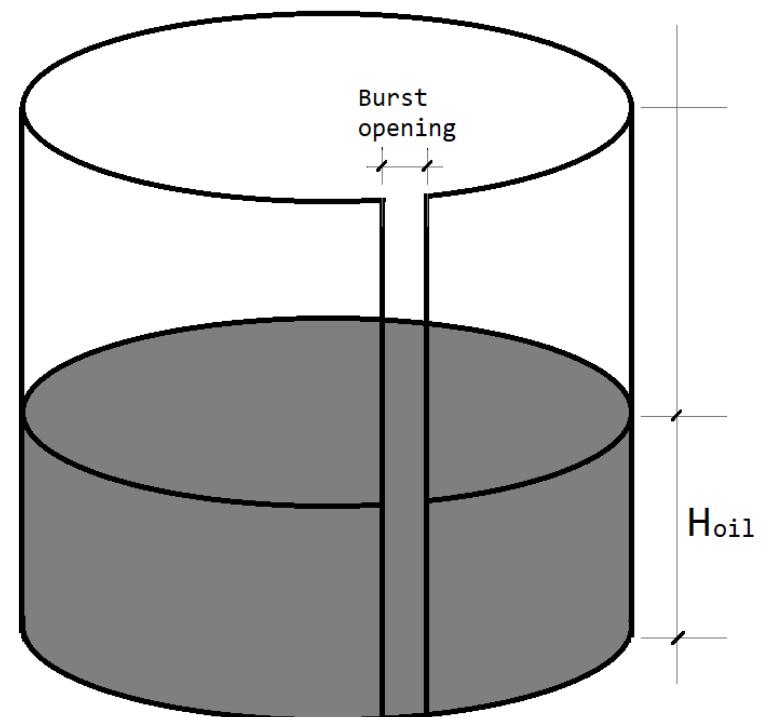
OilFlow2D Heat Transfer Model Assumptions

- Oil temperature, density, viscosity, yield stress vary in space and time (model calculated)
- Wind speed, Air temperature, and solar radiation can vary in time but are uniform in space
- Model allows different options to account for fluid properties as a function of temperature

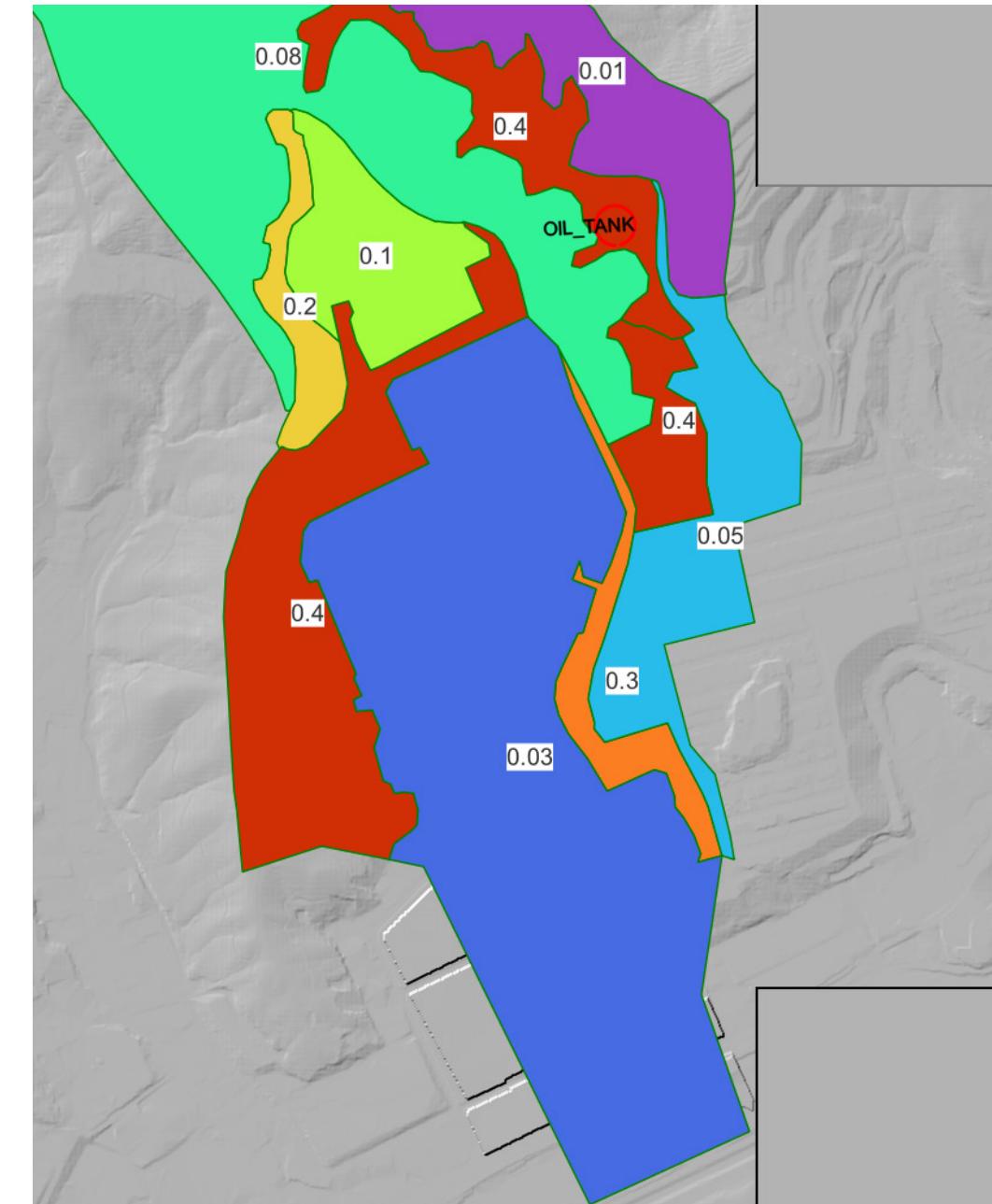
OilFlow2D Rheological Formulations

	τ_b	Parameters
Bingham	$2\tau_b^3 - 3 \left(\tau_y(T) + 2\mu(T) \frac{ \mathbf{u} }{h} \right) \tau_b^2 + \tau_y(T)^3 = 0$	μ, τ_y, ρ
Simplified Bingham	$\tau_b = \frac{3}{2} \tau_y + 3\mu_B \frac{ \mathbf{u} }{h}$	μ, τ_y, ρ
Quadratic	$\tau_b = \tau_y + \frac{k_0}{8} \mu_B \frac{ \mathbf{u} }{h} + \rho g_\psi \frac{n^2 \mathbf{u} ^2}{h^{1/3}}$	$\mu, \tau_y, \rho, \text{Manning's } n$

Tank burst application

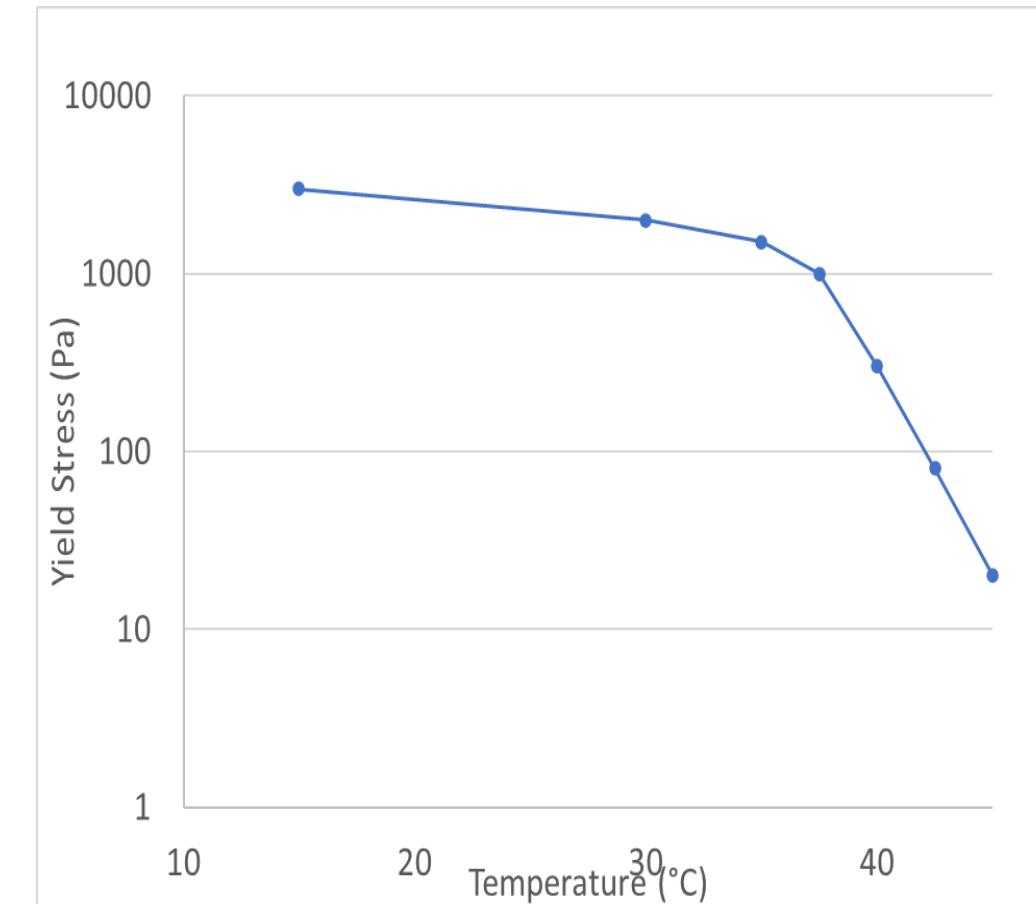


Digital Elevation Model & Manning's n Areas



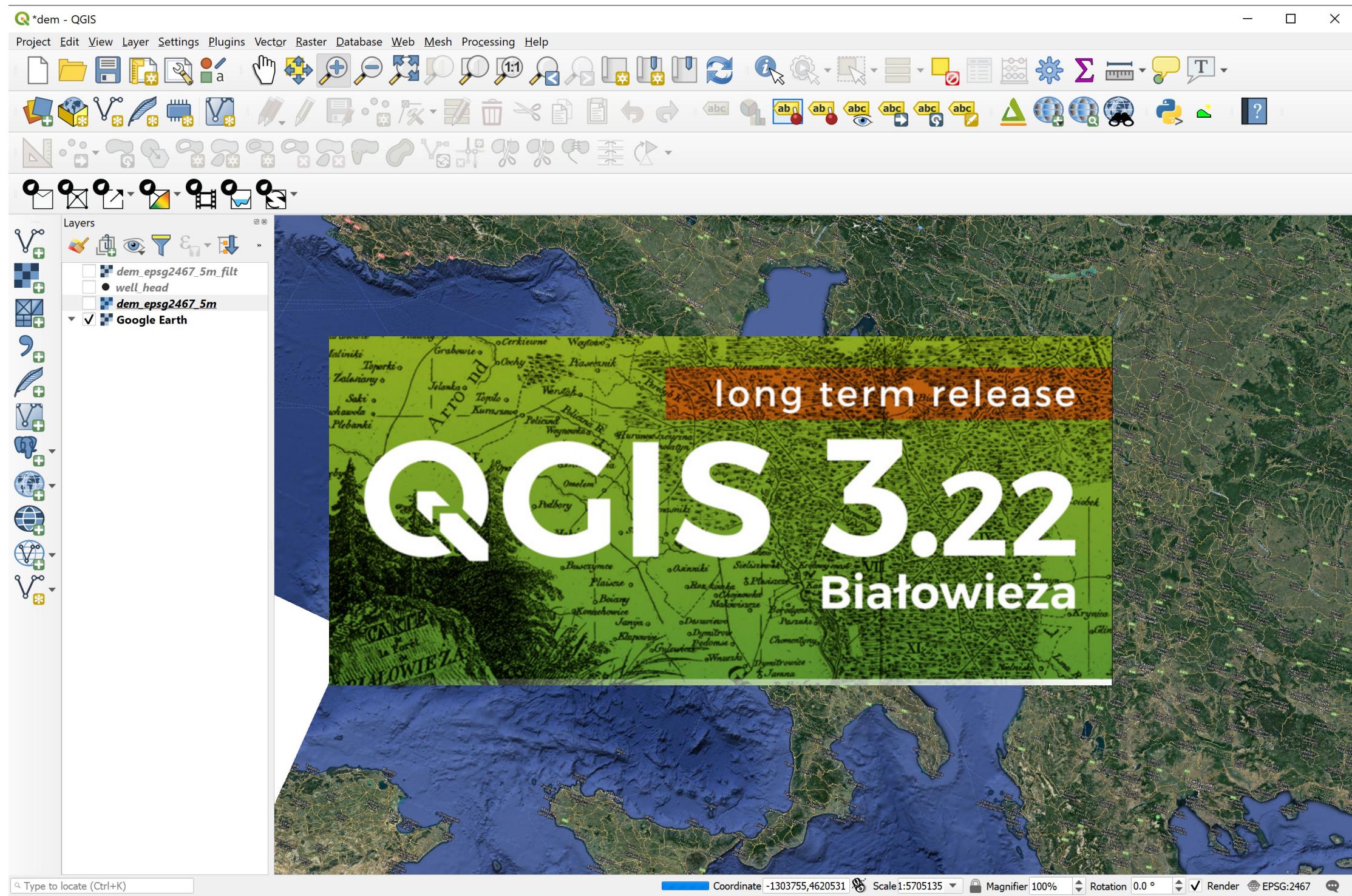
Data Summary

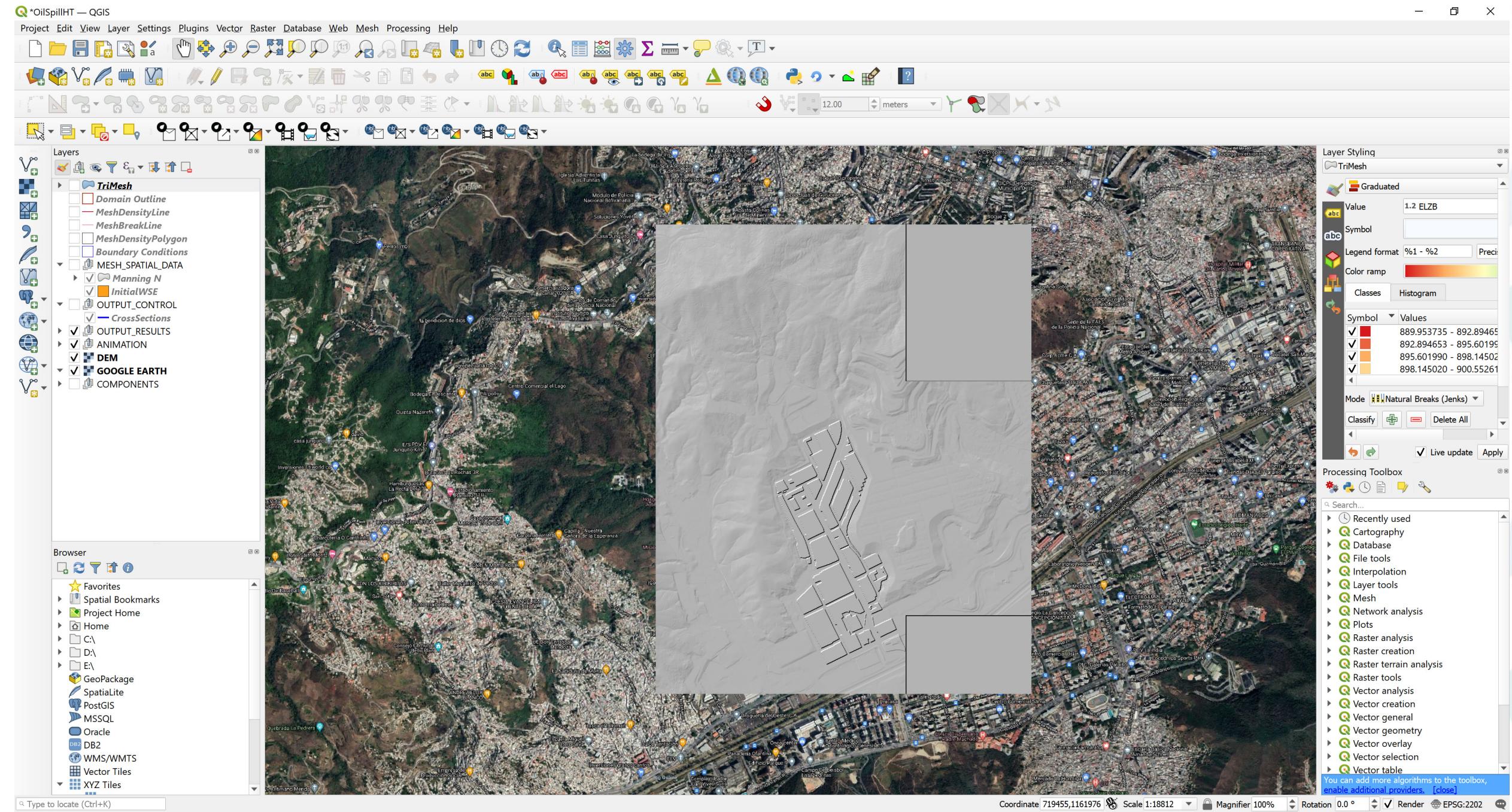
Parameter	Value
Initial oil temperature in tank	55 °C
Initial oil surface elevation in tank	910 m
Oil heat capacity Cp	1900 J/(kg·°C)
Reference density	912 kg/m ³
Density constant K	-0.627
Viscosity constant A _μ	2.6388 10 ⁻⁷
Viscosity constant B _μ	3893
Yield stress at 50 °C	0 Pa
Yield stress at 40 °C	300 Pa
Yield stress at 30 °C	2000 Pa
Ambient temperature	26 °C
Wind velocity	2-20 m/s
Solar radiation	1 W/m ²
Rheological formulation	Quadratic



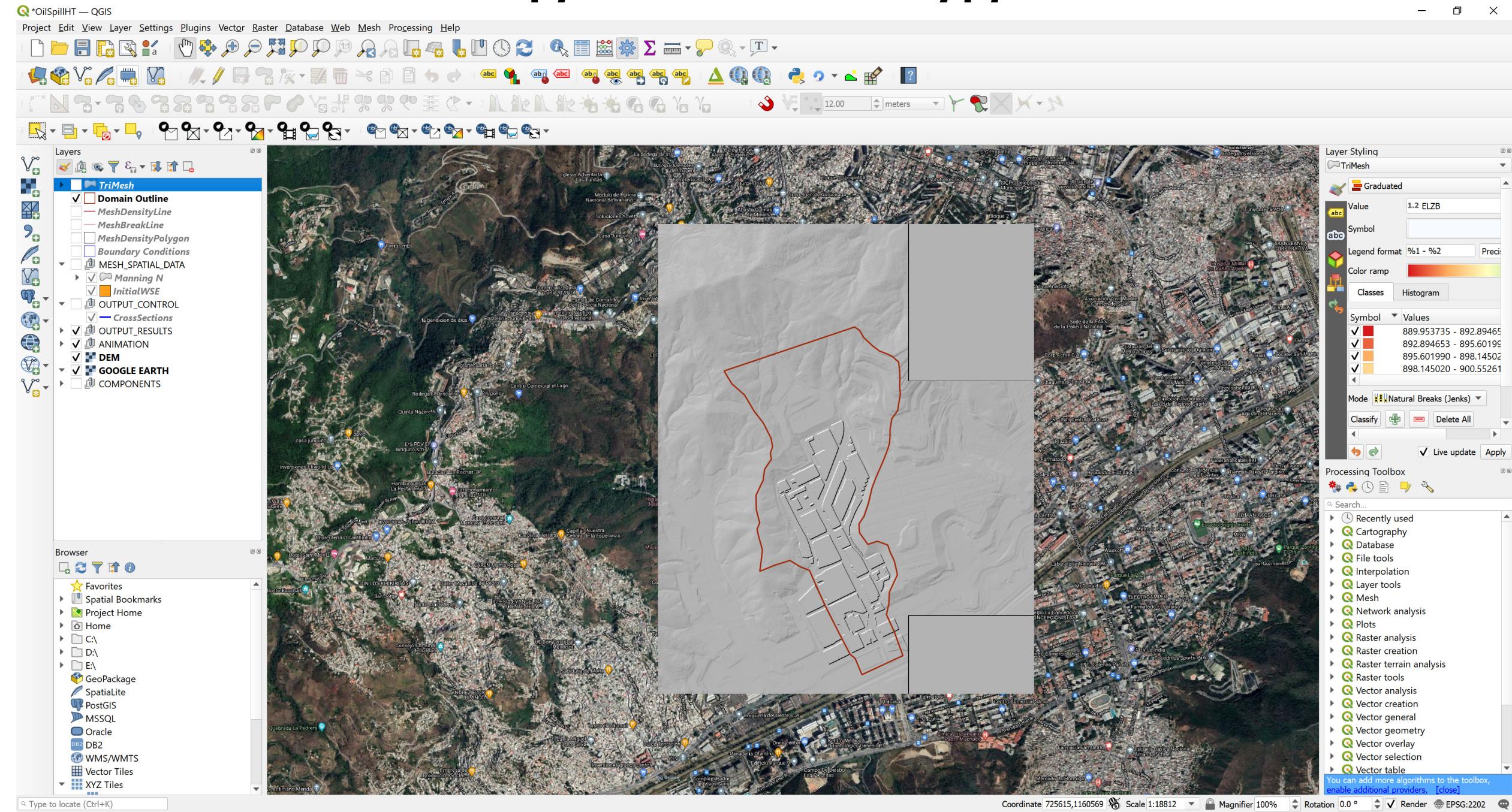
Yield stress f(t)

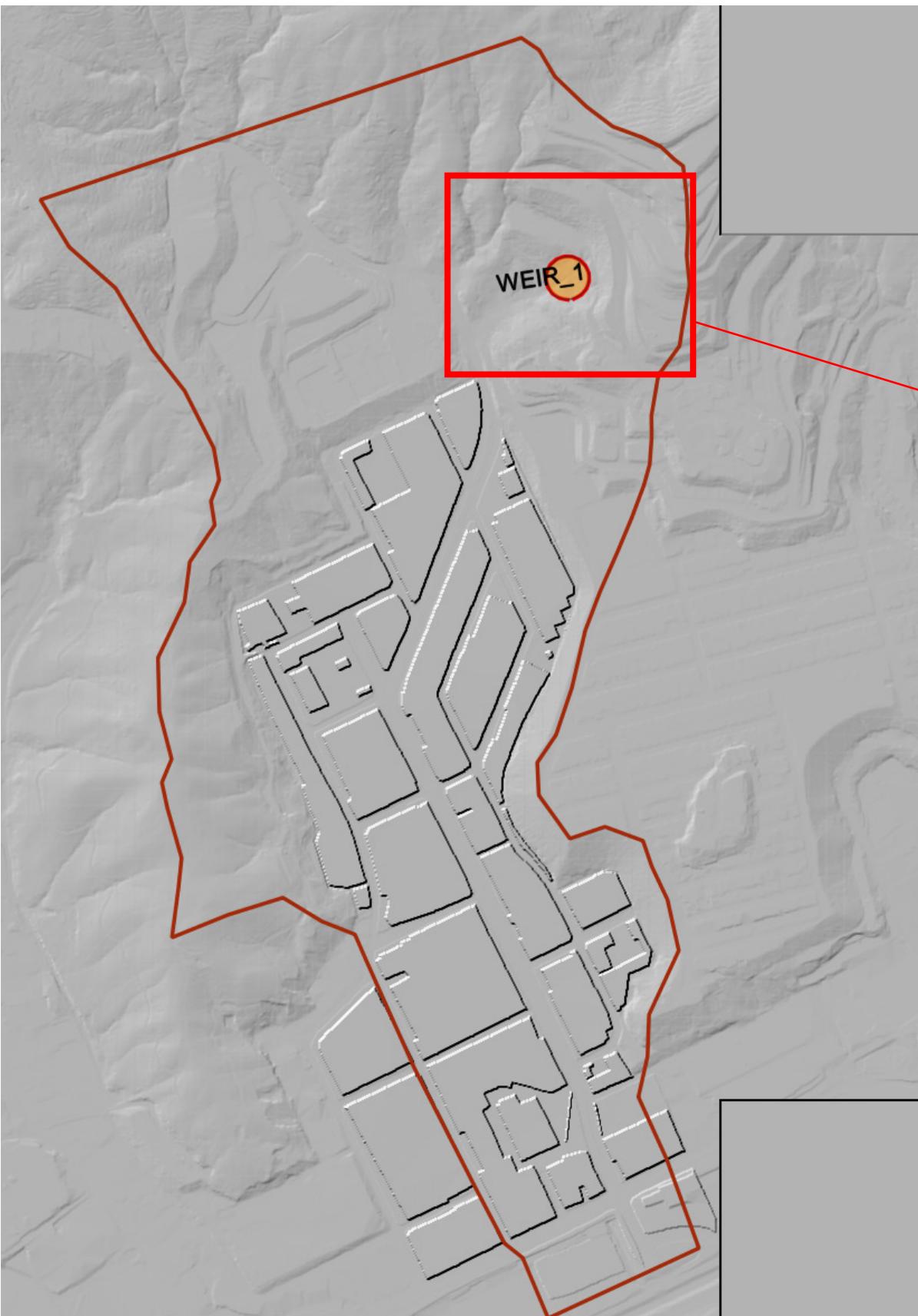
GUI: OilFlow2D –QGIS Integration





Create Modeling Limits: Polygon



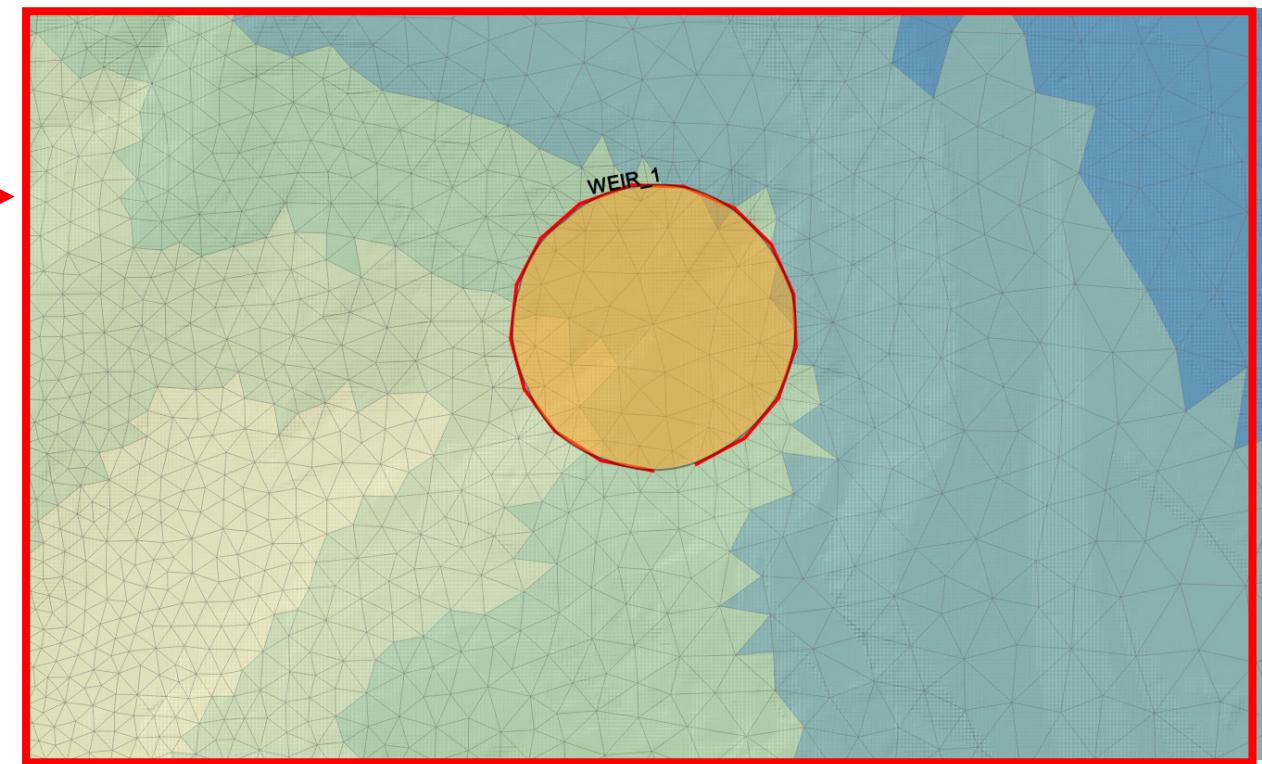
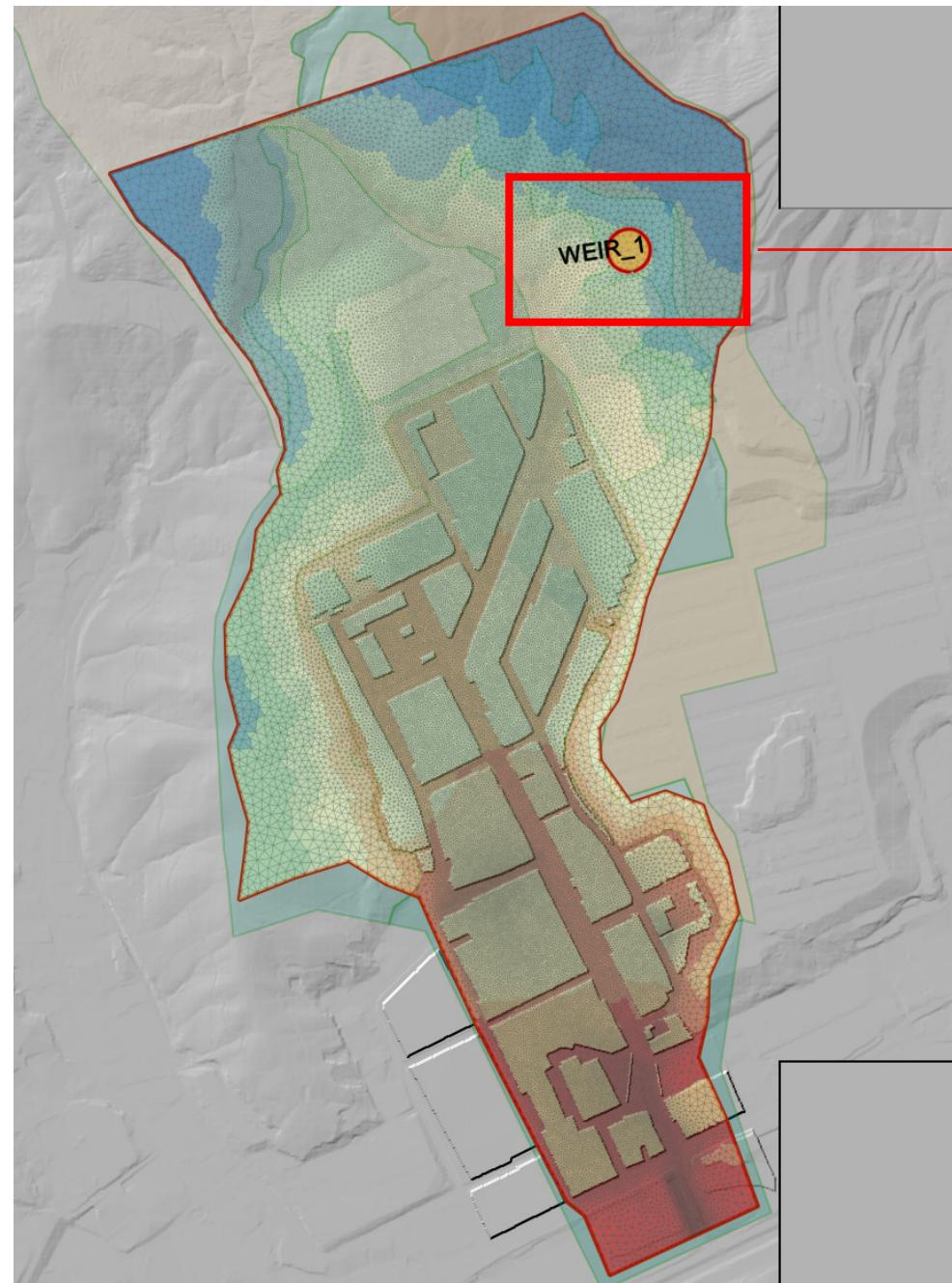


Oil Storage Tank

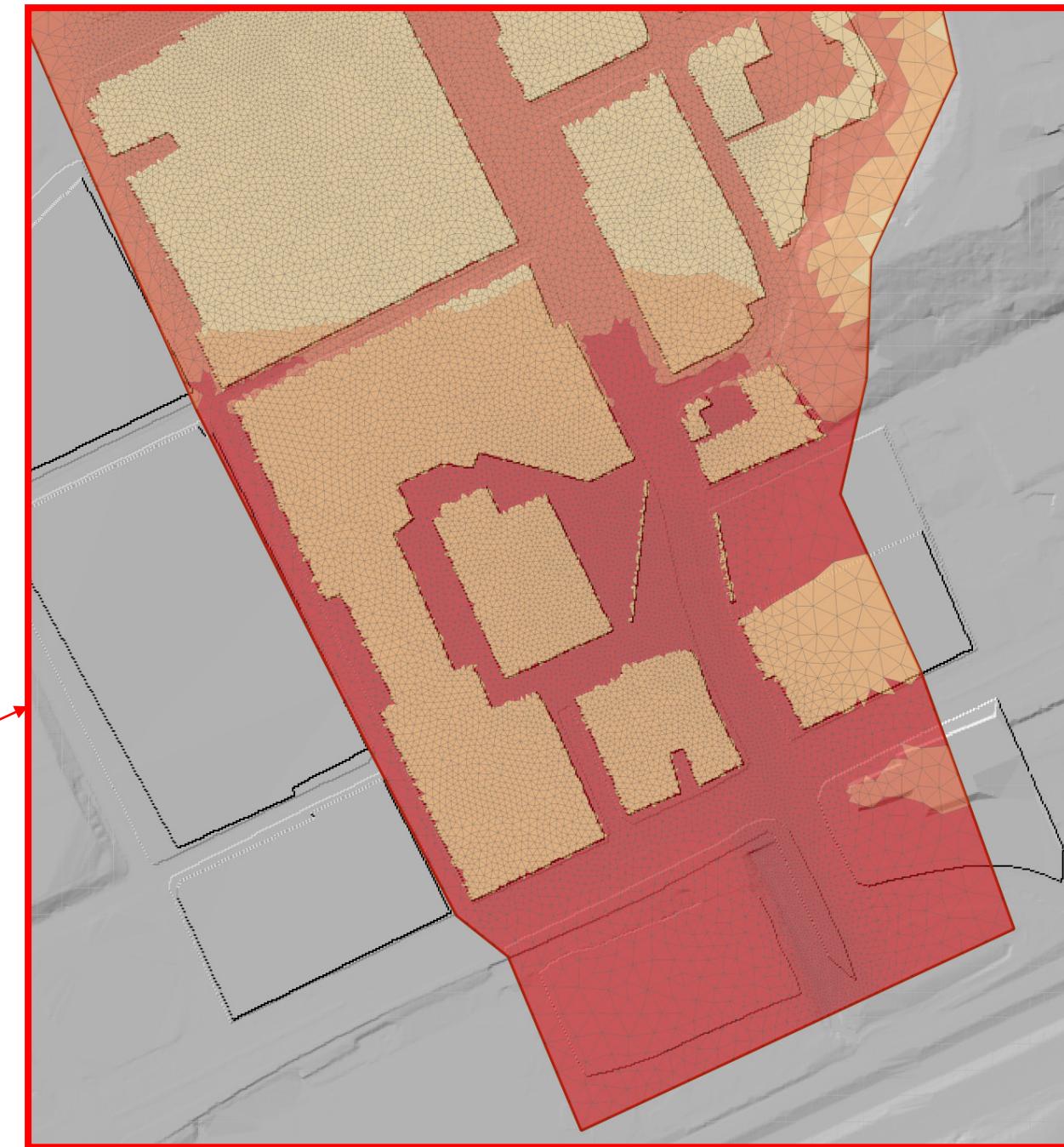
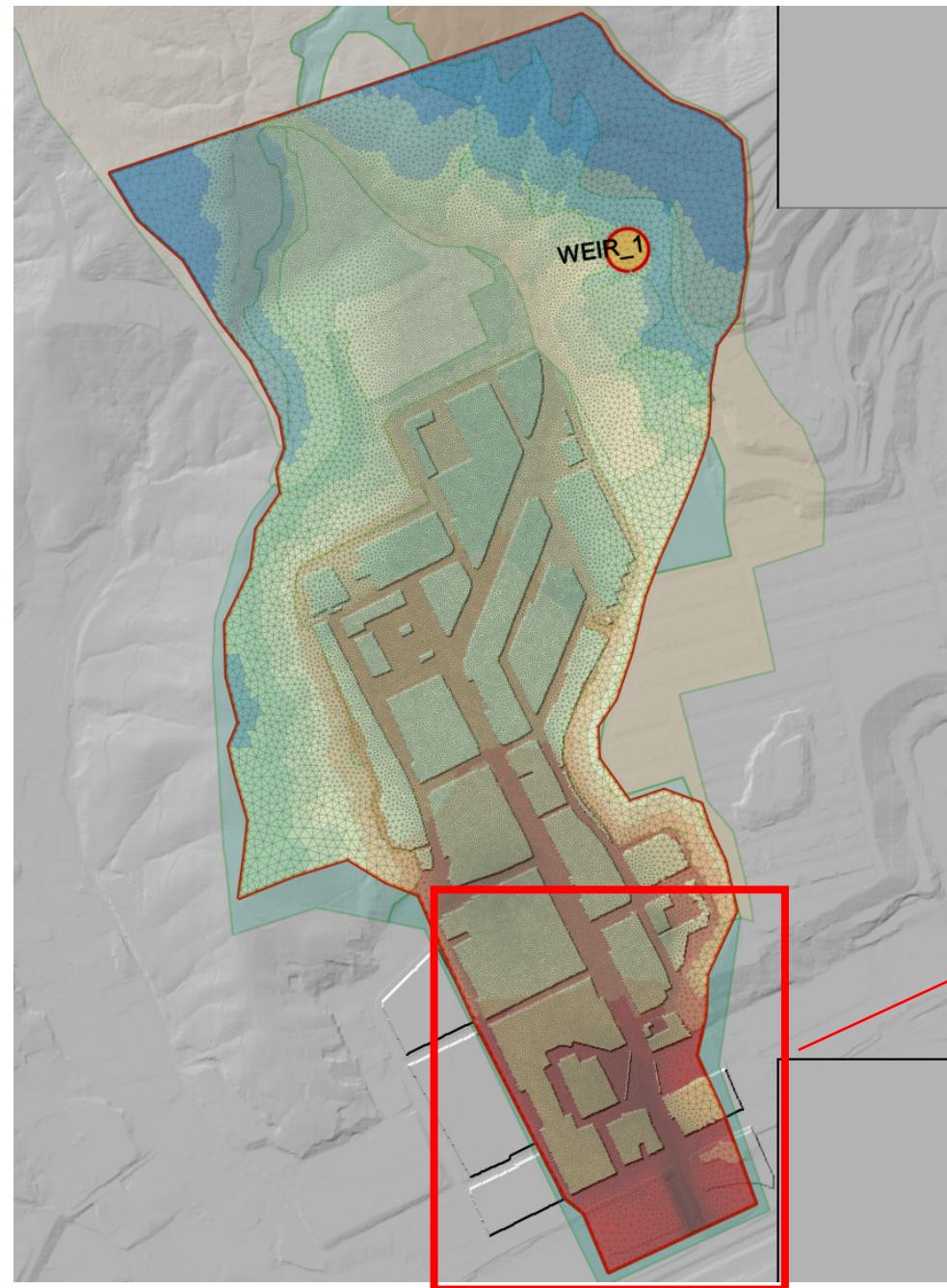


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Mesh: 89,388 elements



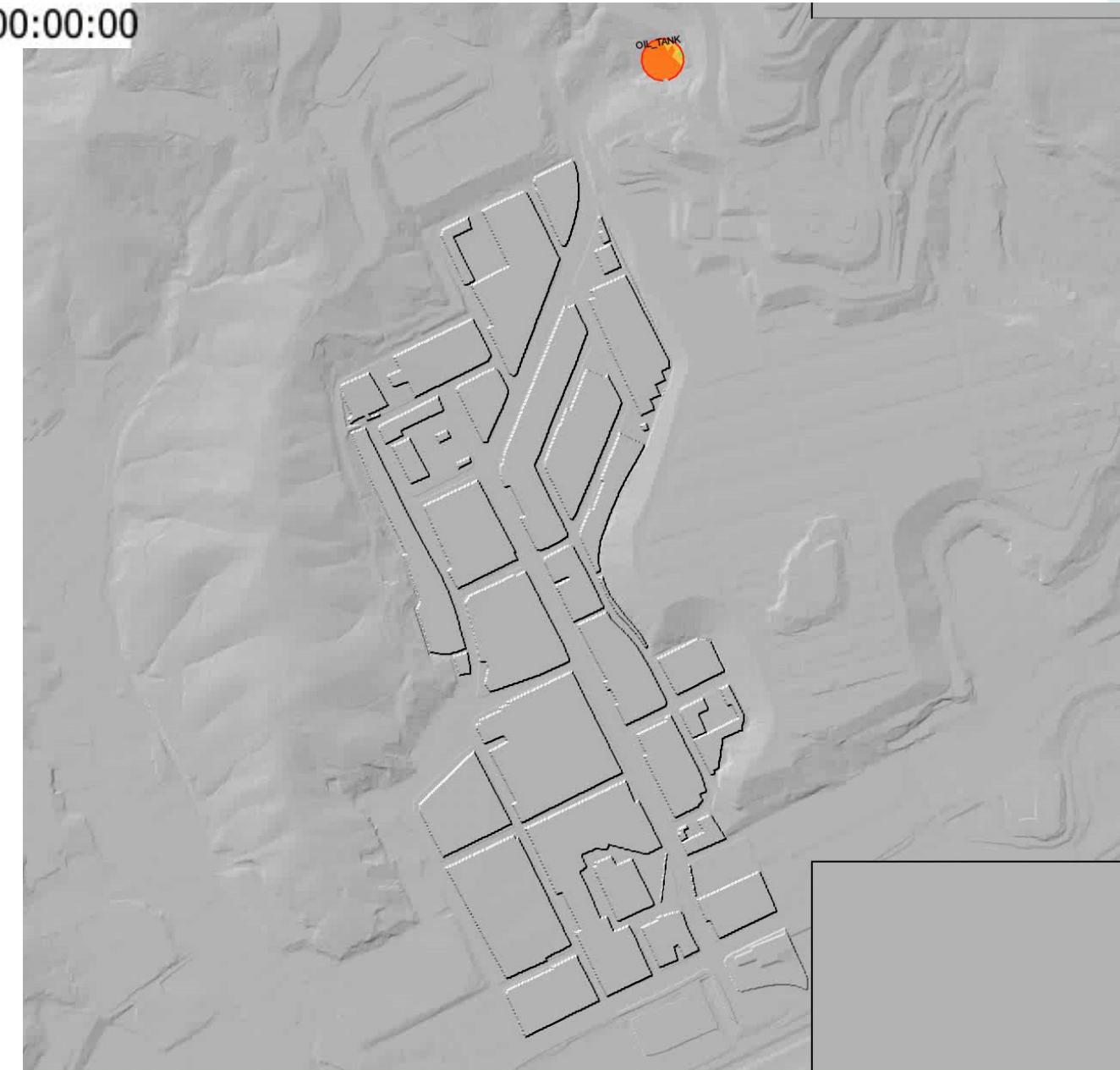
Mesh: Refinement at lower end



Spill Animations

Wind Speed 2 m/s

Wind Speed 20 m/s



Oil Depth

Wind Speed 2 m/s



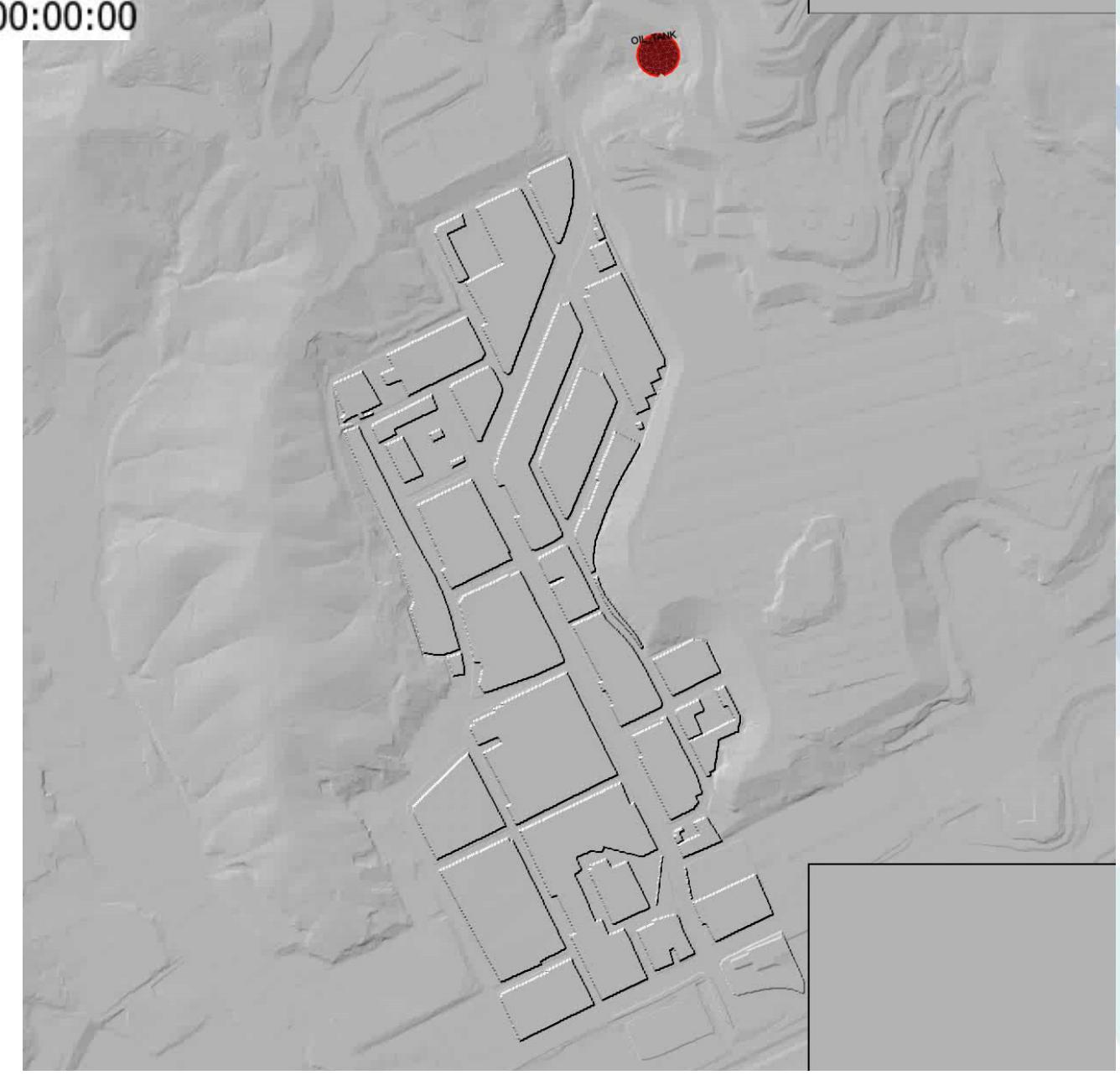
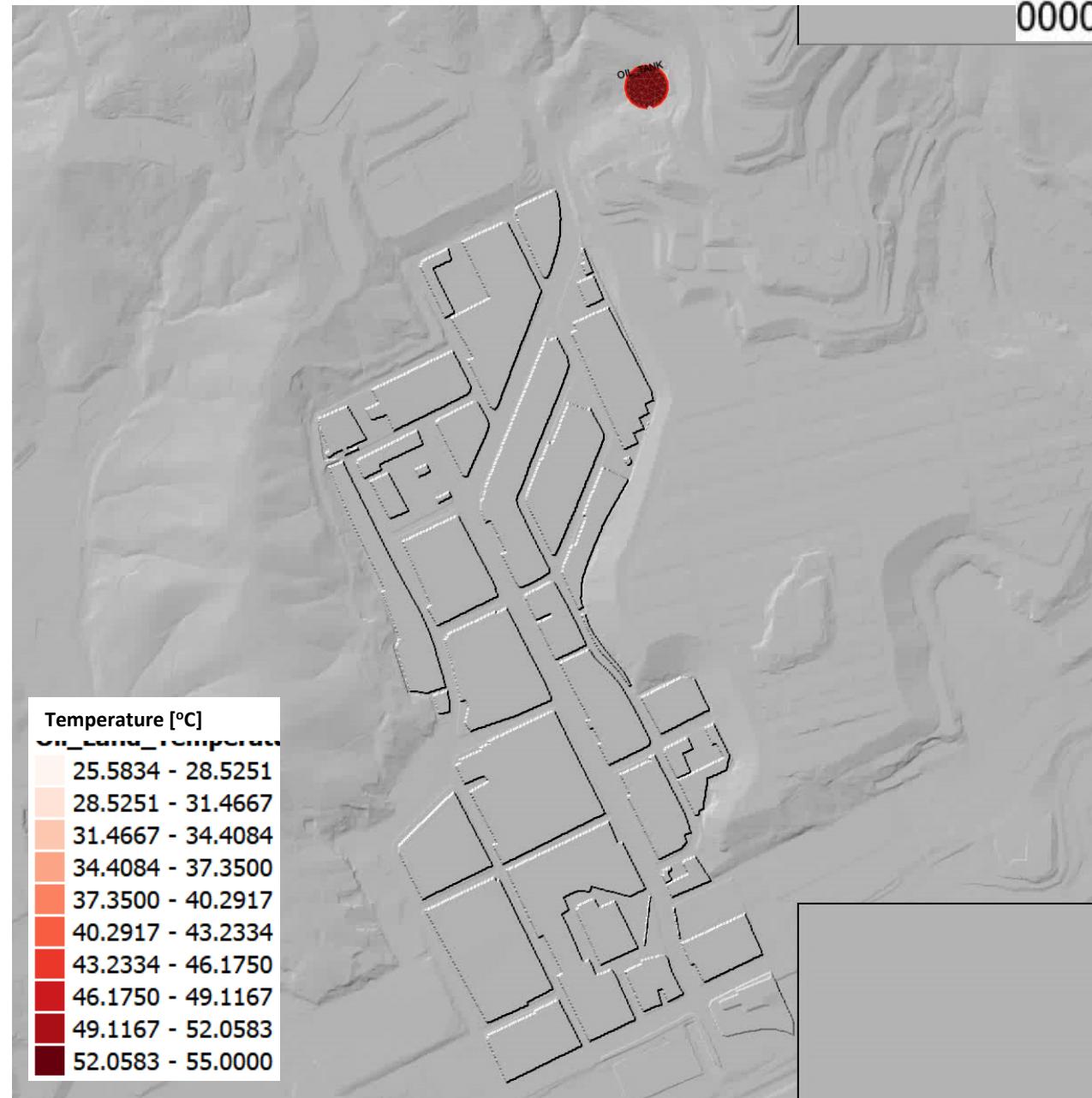
Wind Speed 20 m/s



Oil Temperature

Wind Speed 2 m/s

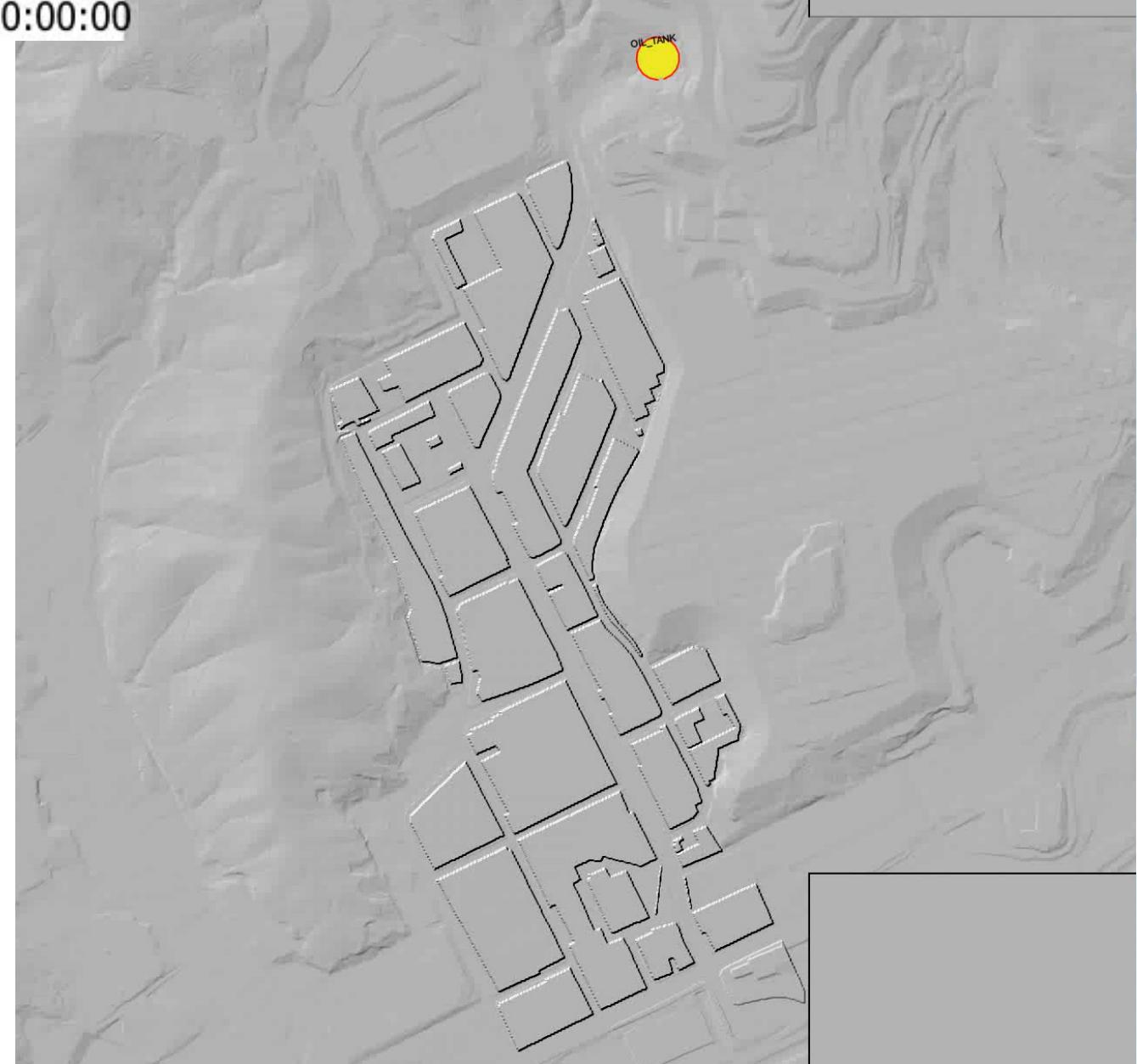
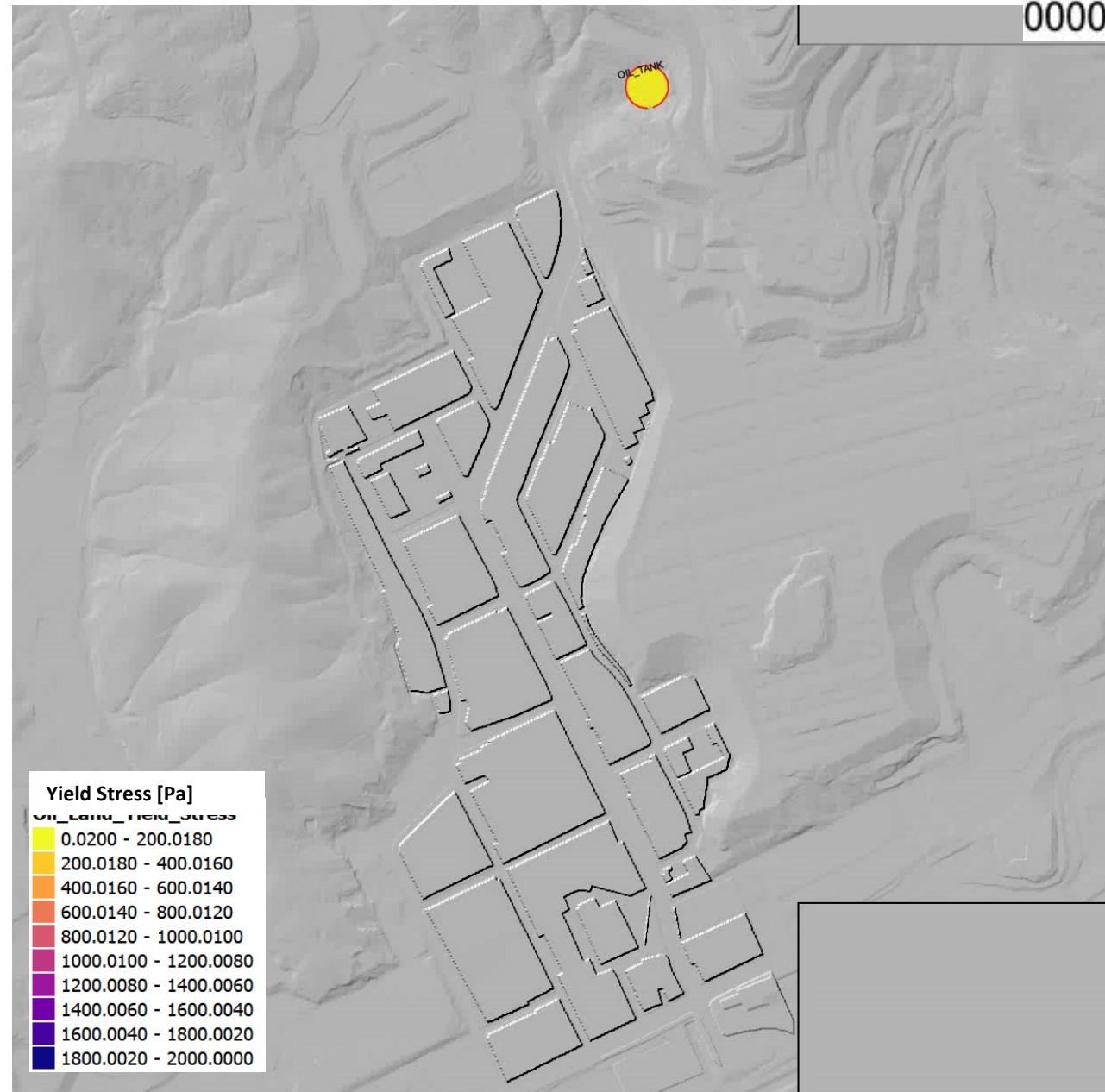
Wind Speed 20 m/s



Oil Yield Stress

Wind Speed 2 m/s

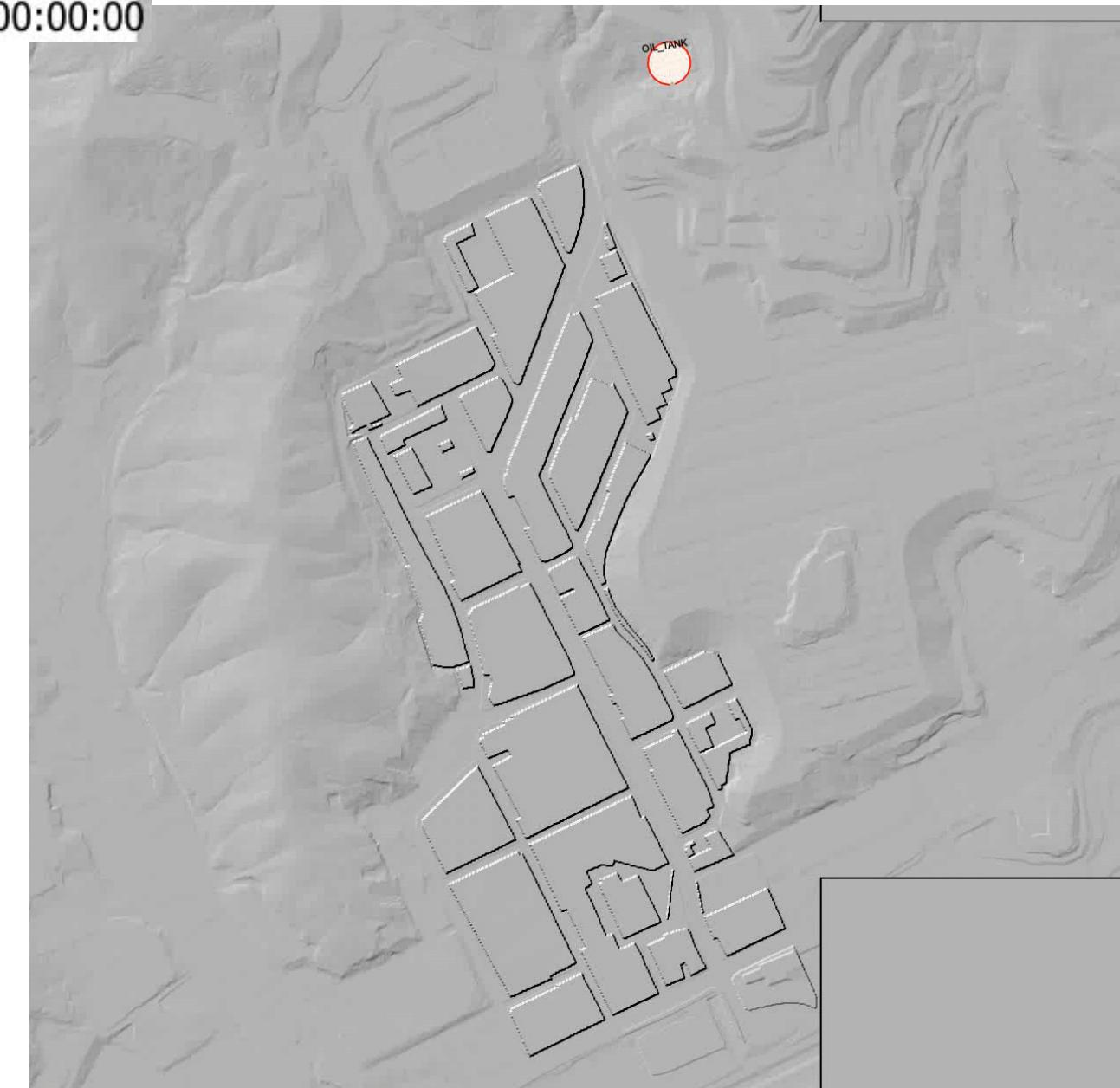
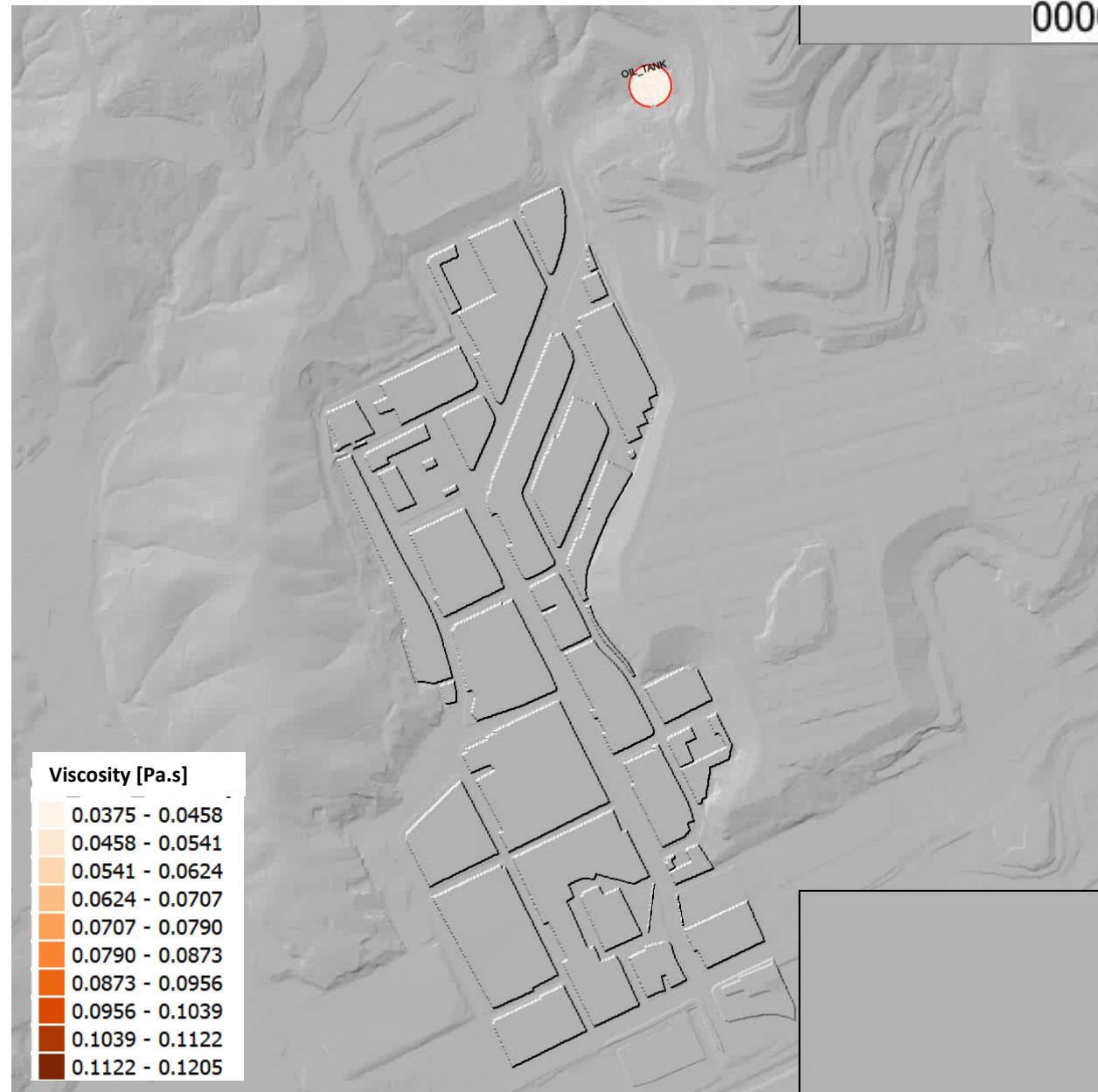
Wind Speed 20 m/s



Oil Viscosity

Wind Speed 2 m/s

Wind Speed 20 m/s



Comments

- Behaviour of some crude oils requires considering the variation of the fluid properties during spills.
- Modeling heat transfer in overland oil spill simulations can significantly improve the prediction of impacted areas.
- The OilFlow2D Heat Transfer Component is a practical model that can contribute to more realistic assessments of oil spill impacts.

THE ASHLAND OIL SPILL, FLOREFFE, PA

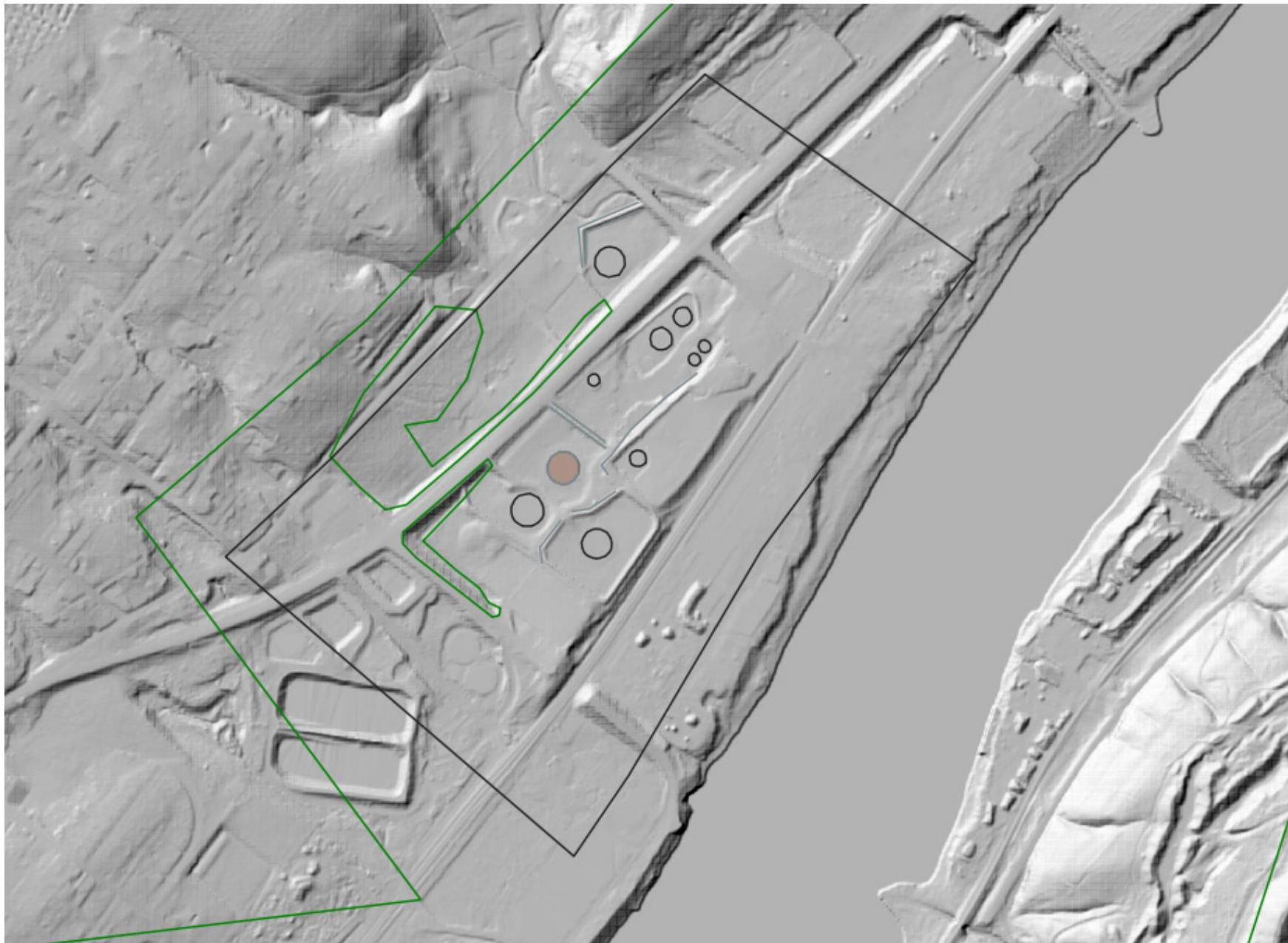
- Instantaneous and complete Diesel Fuel Storage Tank failure
- January 2, 1988
- Ashland Oil Terminal, Floreffe, Pennsylvania, near the Monongahela River 24 miles upstream of Pittsburgh
- Released 90,000 barrels ($\sim 15,000 \text{ m}^3$) of diesel oil
- Within hours, an estimated 18,000 barrels (3840 m^3) of diesel had entered the river.



THE ASHLAND OIL SPILL, FLOREFFE, PA

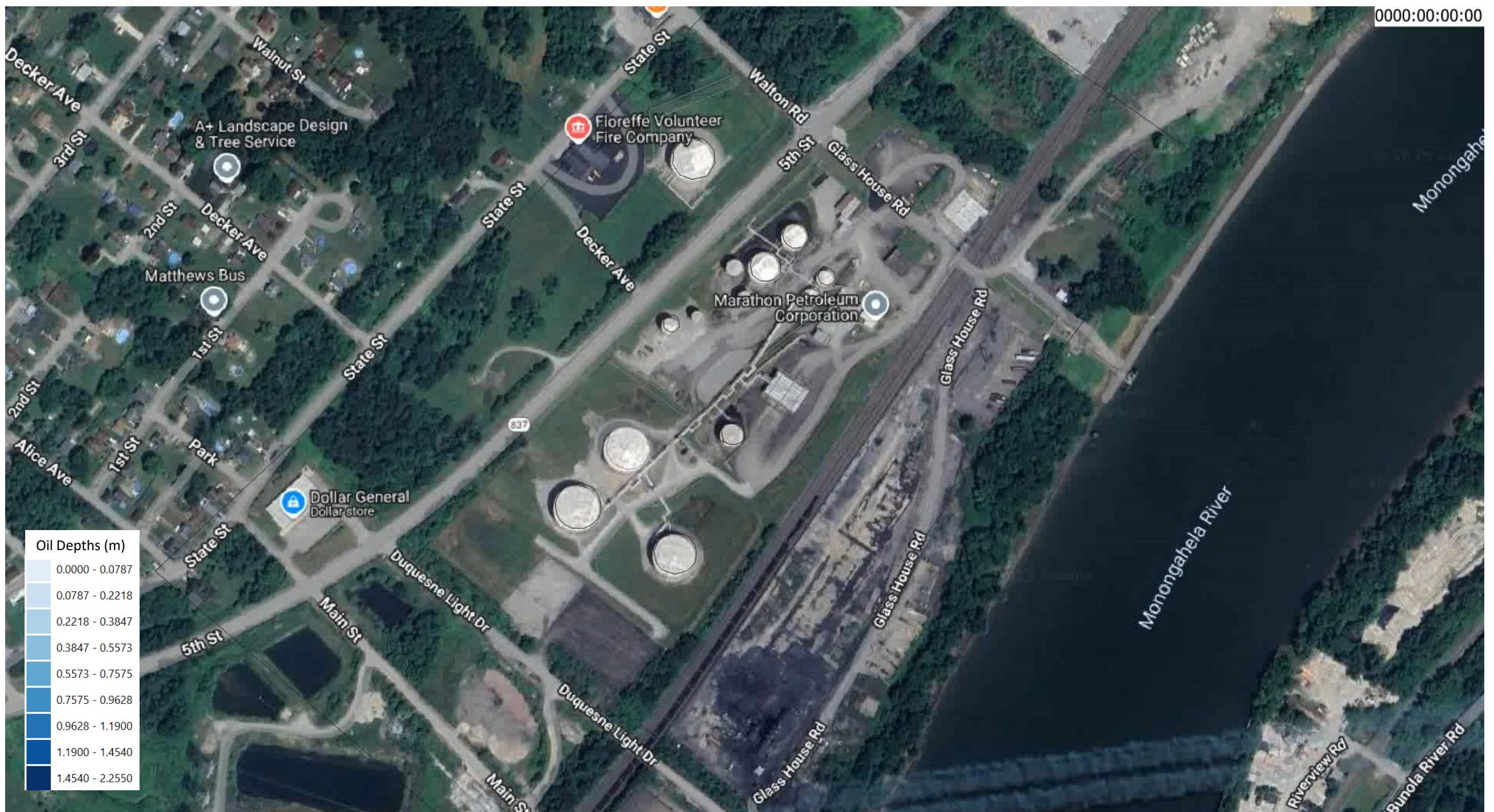


THE ASHLAND OIL SPILL, FLOREFFE, PA

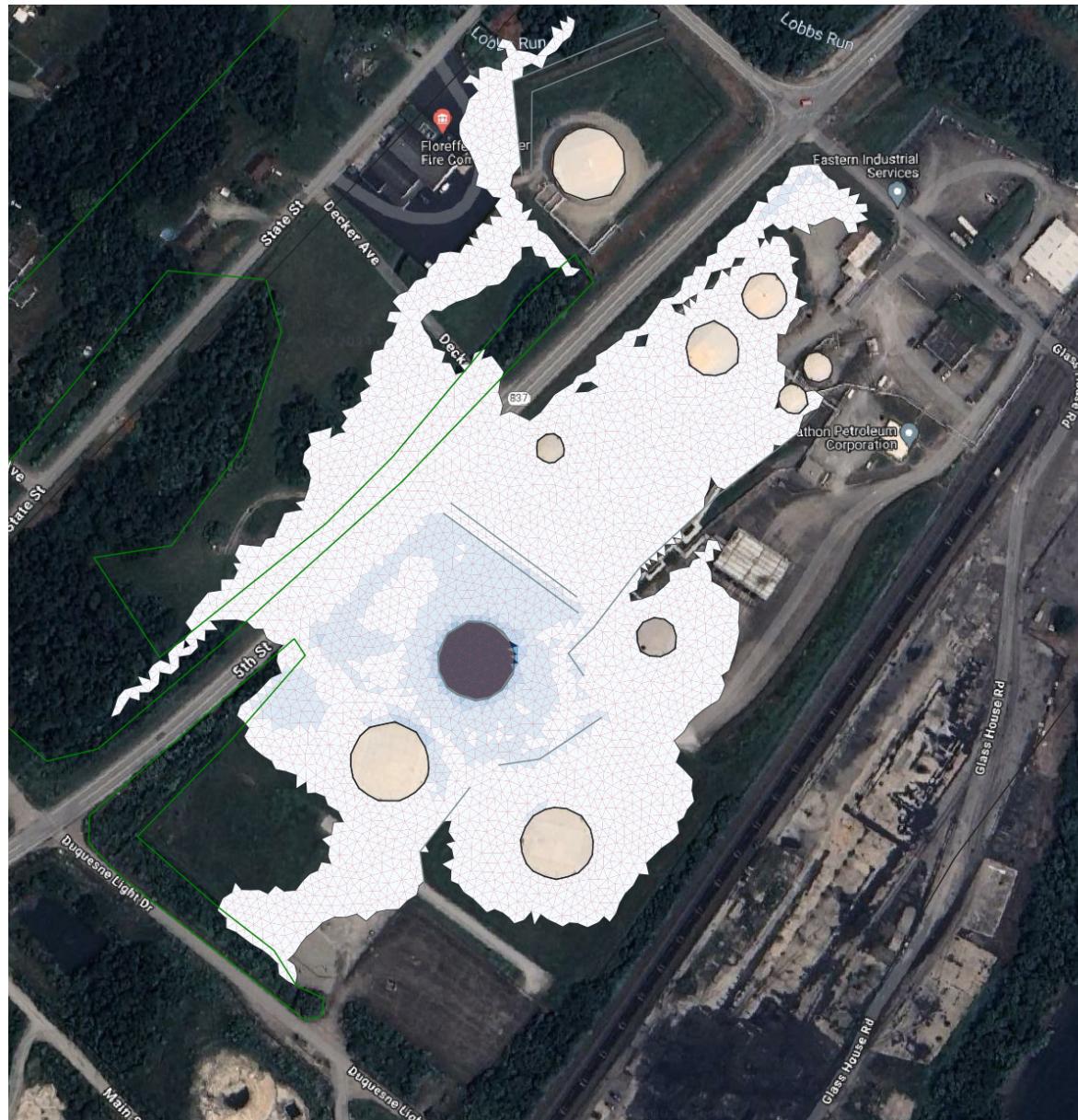


THE ASHLAND OIL SPILL, FLOREFFE, PA

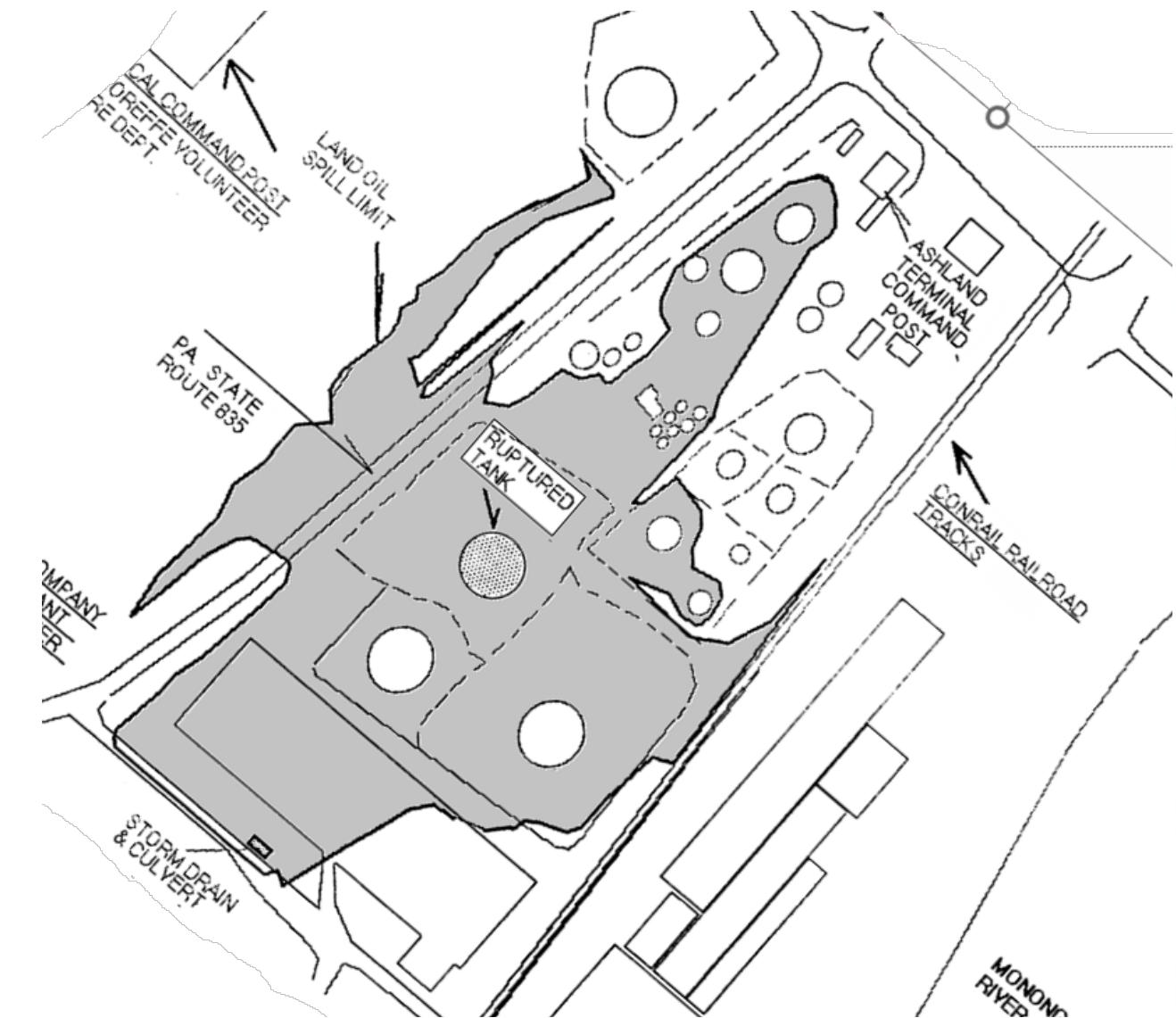




THE ASHLAND OIL SPILL, FLOREFFE, PA

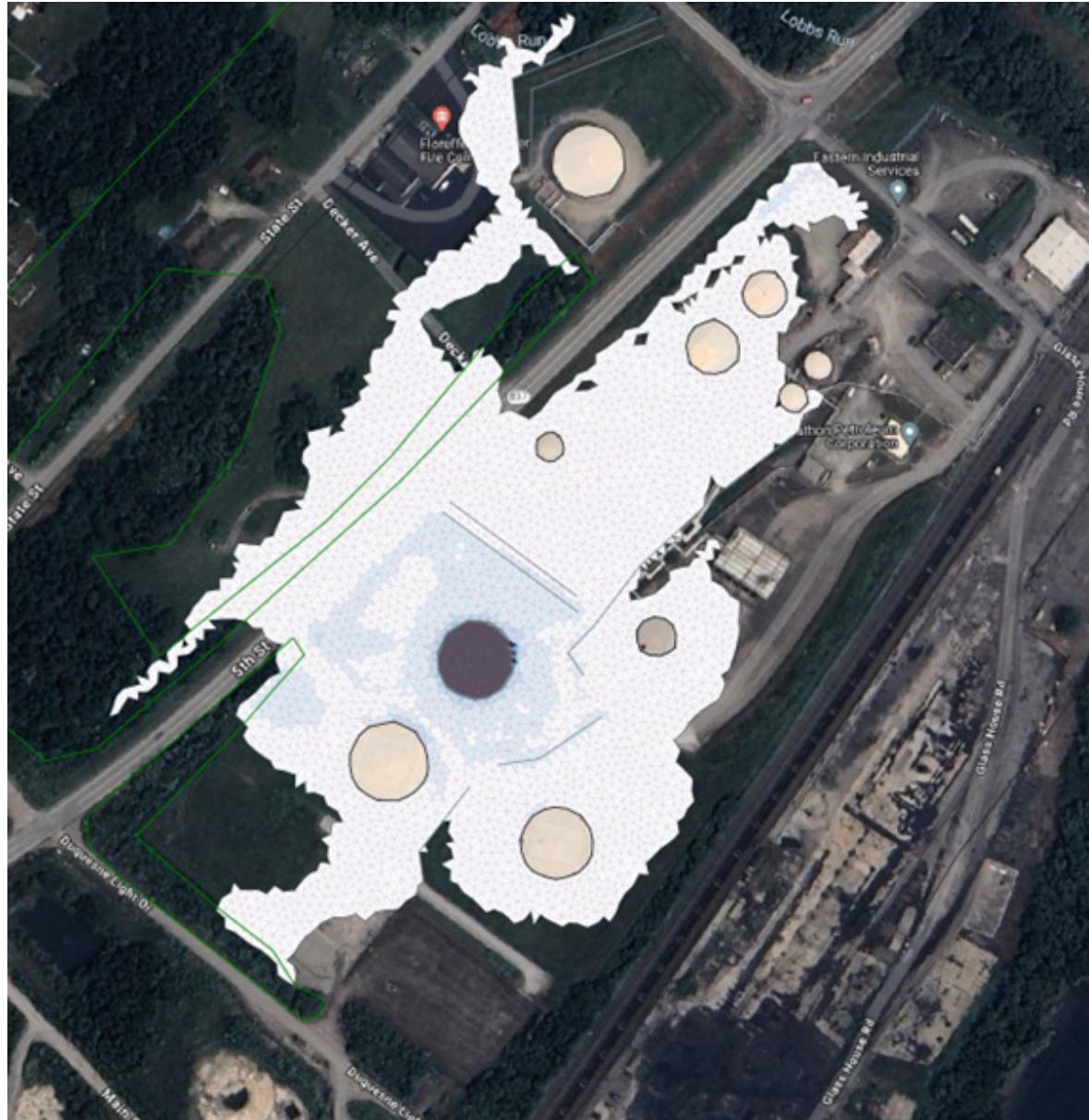


OilFlow2D Impacted Area

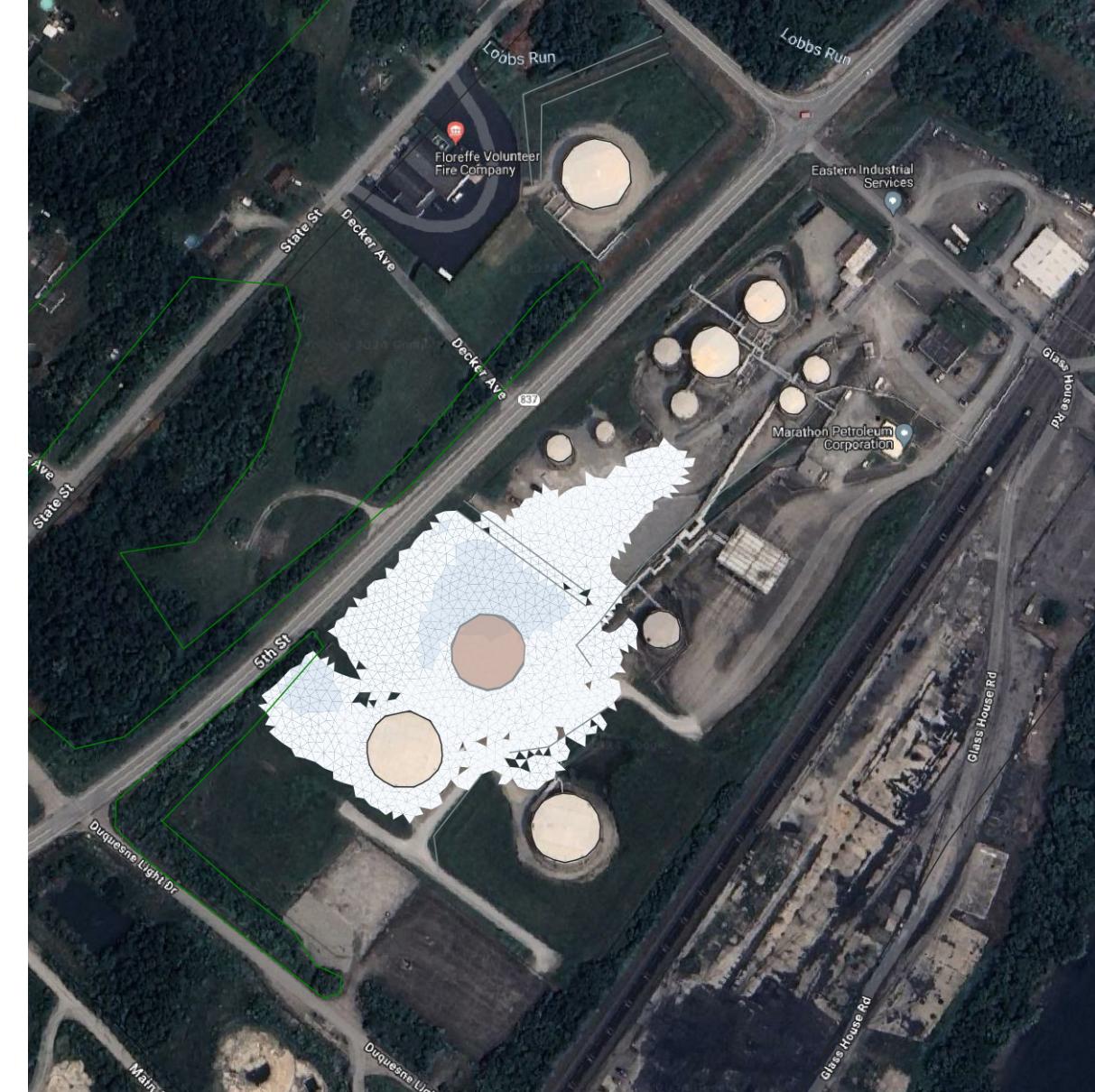


Impacted Area Reported

Impacted areas as a function of Oil Properties

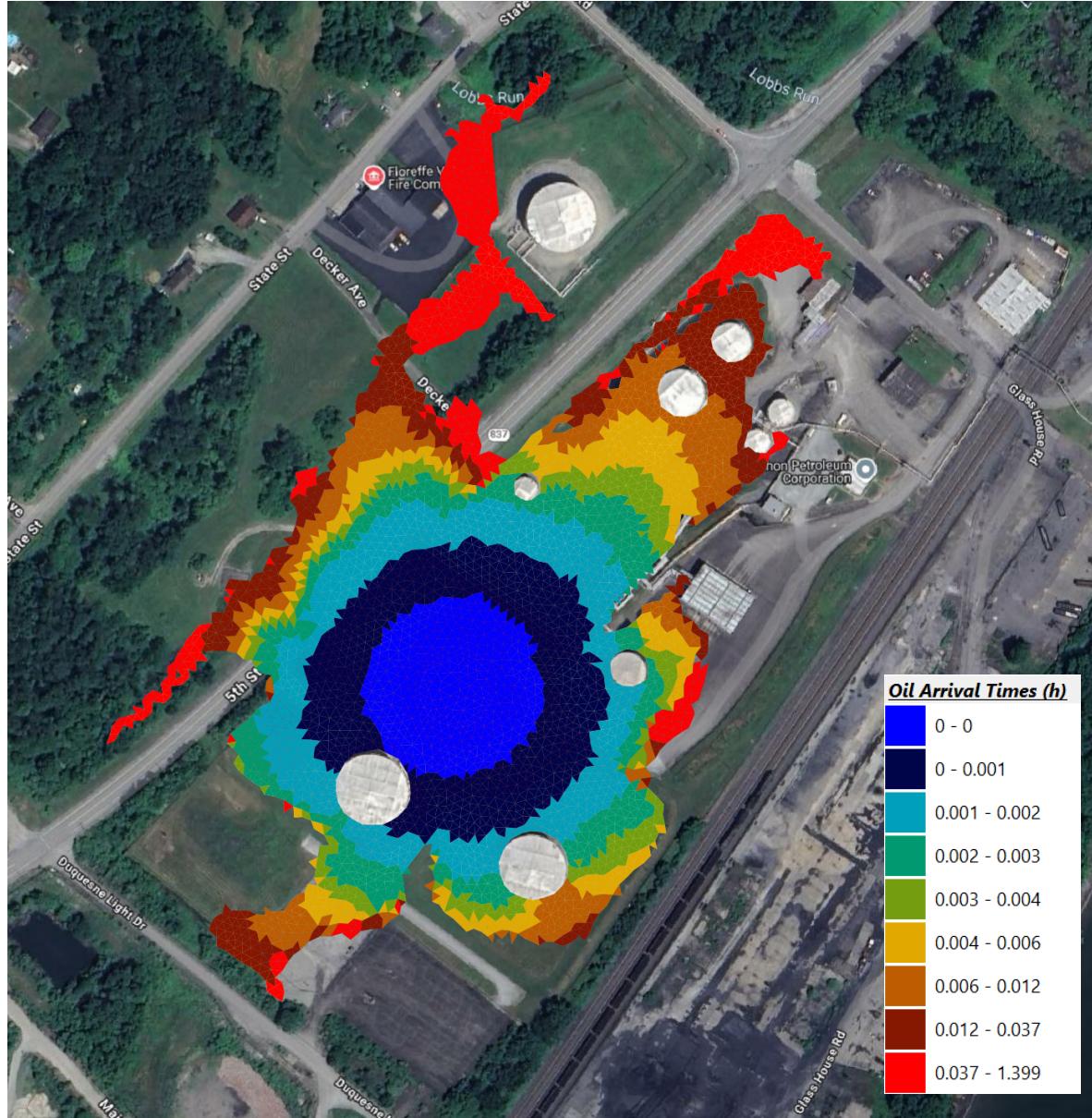


No-heat transfer low viscosity

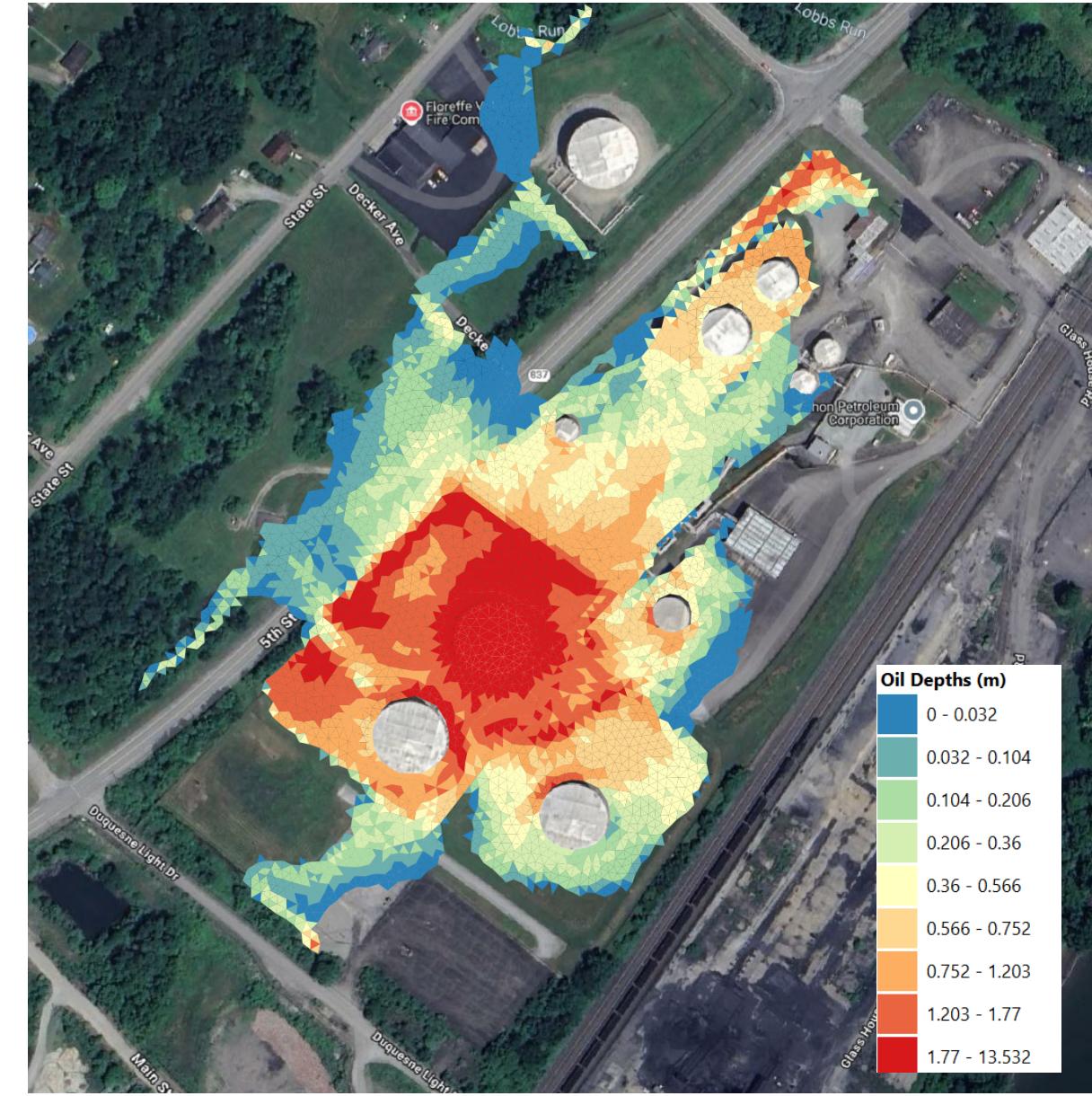


Higher viscosity by cooling

Oil arrival times and maximum depths



Oil Arrival Times



Oil Depths

GPU Acceleration

NVIDIA RTX 4090 GPU	
Memory	24 GB
Cores	16,384



Mesh	No. Cells	RTX 4090			Speedup
		Intel CPU (16 cores)	(16,384 cores)	Max	
Mesh 1	22,345	00:00:02:51	00:00:00:36	5x	
Mesh 2	508,362	00:02:24:20	00:00:06:45	21x	
Mesh 3	1,118,866	00:09:16:56	00:00:18:42	30x	

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Oil Pipeline Spill Modeling

Or why GPU Brute Force is not always the first option

Oil Spills From Pipeline Bursts



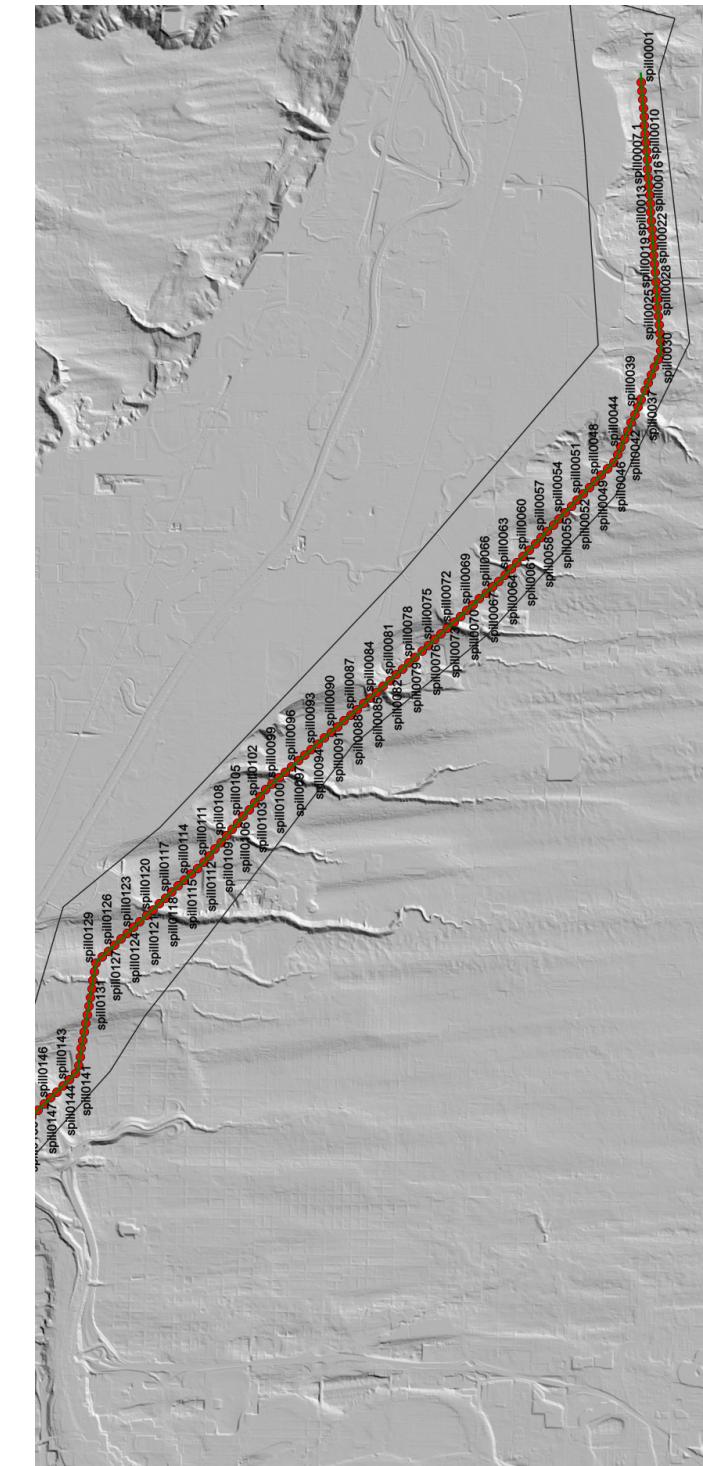
Tony Hisgett / Wikimedia Commons / CC BY 2.0 • James T M Towill / CC BY-SA 2.0

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Some country requirements

- Pipeline Spill risk assessment
- Thousands of spills along the pipeline
- Brute-force approach is seldom the best approach
- Also requires optimizing post processing to make it practical



Oil Pipeline Module

Pre-processing

- Allows entering a pipeline polyline and multiple spill points.
- Automatic creation of the sources layer for batch processing of the overland oil spills.
- Computation of the steady state initial pressure distribution along the pipeline given the oil flow rate and pressure head.
- Considers the closing time of block valves.
- Calculates the output flow rates from leaks of any diameter in two stages: The period between the initial time and valve closing and the period between the closing of valves and the final oil drainage from the pipeline during depressurization.
- The pipeline polyline can contain elevations, or the program can assign elevations from the Digital Terrain Model raster.

Oil Pipeline Module

Post-processing

- Numeric output includes for each spill point:
 - The outflow hydrograph (oil discharge vs time),
 - Total oil volume drained from upstream and downstream of the spill point.
 - Oil volume drained from upstream and downstream of the spill point before valve closure.
 - Oil volume drained from upstream and downstream of the spill point after valve closure.
- Pressure head along the pipeline for the initial conditions.
- General table of hydrographs for all spills.
- Map batch processing to generate depth and affected area maps for all spills.
- Spill ID stamp for shape files.
- Integrated map in a single shape file for all spills.

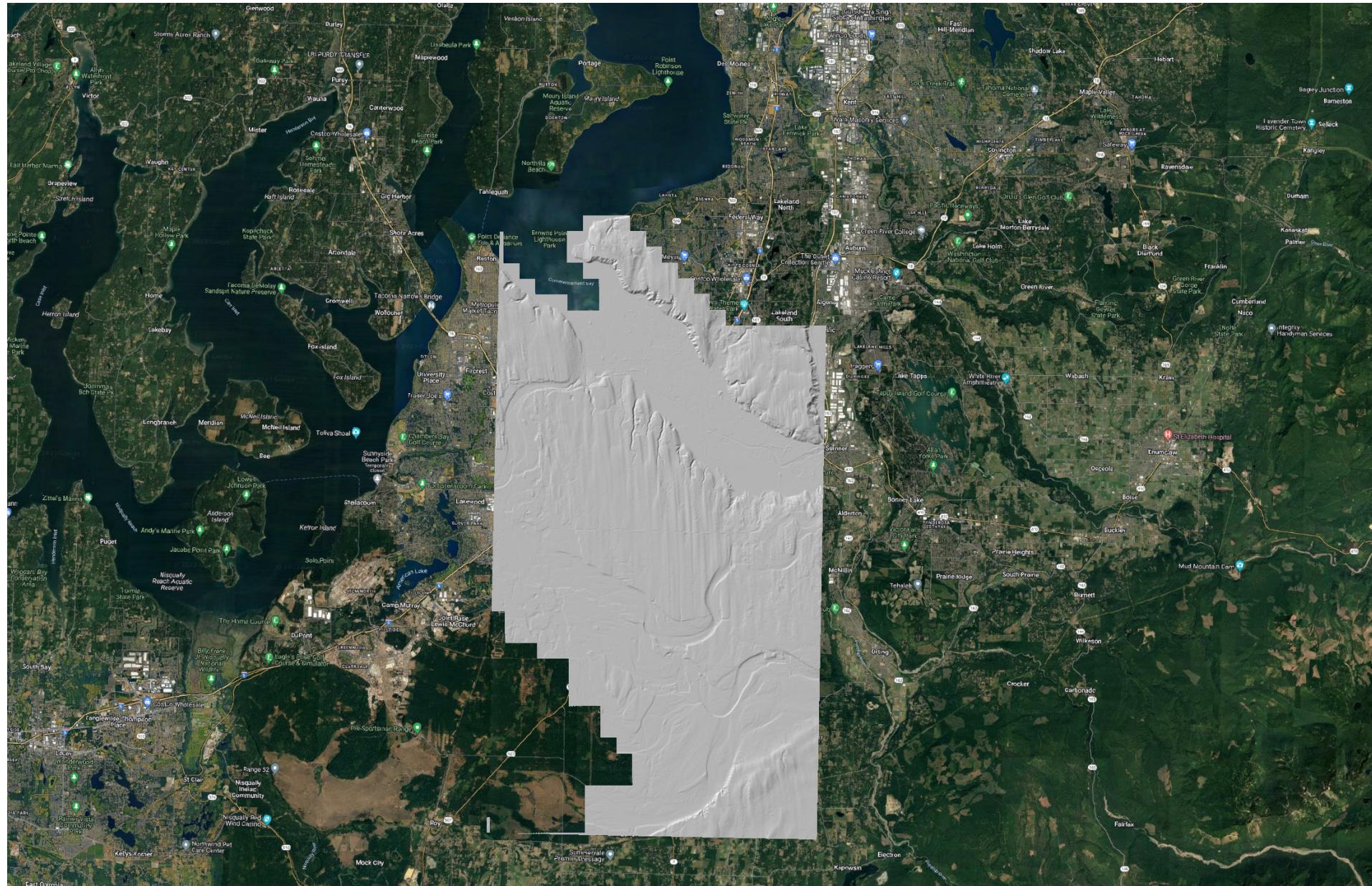
OilPipeline Application Workflow

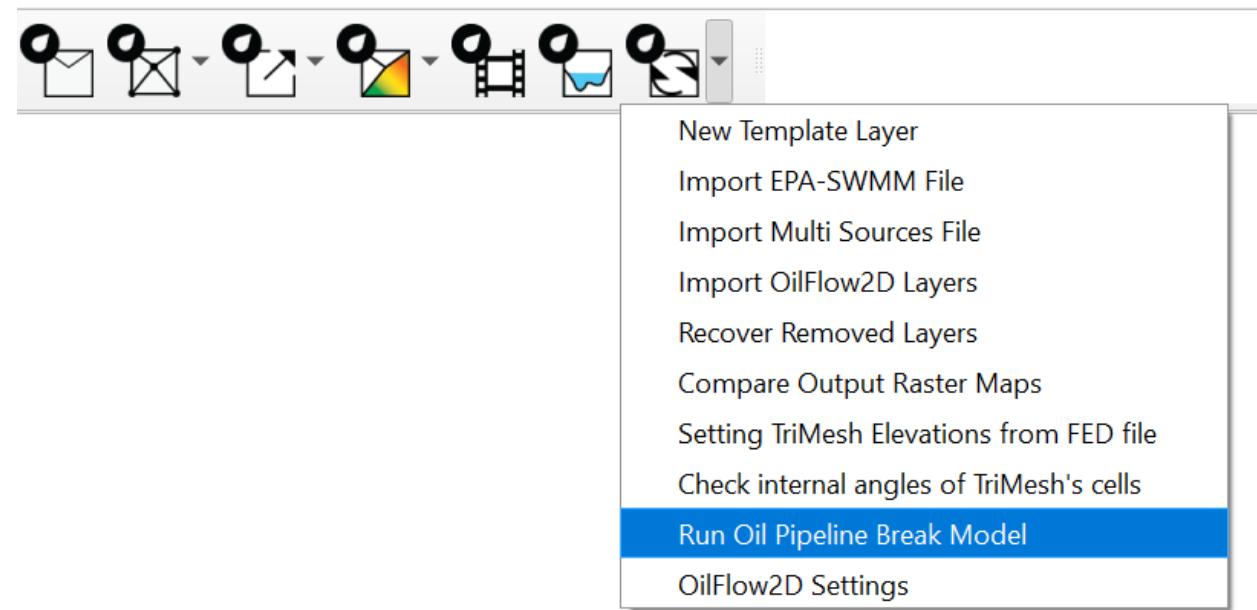
1. Open QGIS
2. Create a new OilFlow2D Project
3. Load Terrain Elevations (DEM)
4. Create empty *OilPipeline* and *Valves* layers
5. Enter pipe polyline
6. Enter Valve location points
7. Run the program to calculate Q vs time for each spill and generate *Sources* layer



Terrain Elevations: USGS

<https://apps.nationalmap.gov/downloader/#/>





Oil Pipeline Break Model

Calculation interval (seconds) :

Distance between spill points [Delta X] (m) :

Leak diameter (m) : Discharge coeff.(0-1) :

Friction coeff. :

Oil Properties

Density (kg/m³) :

Kinematic Viscosity (m²/s) :

Basic Model Heat Transfer Model Output Oil Temp (°C) :

Initial pressure head at pipe end (m) :

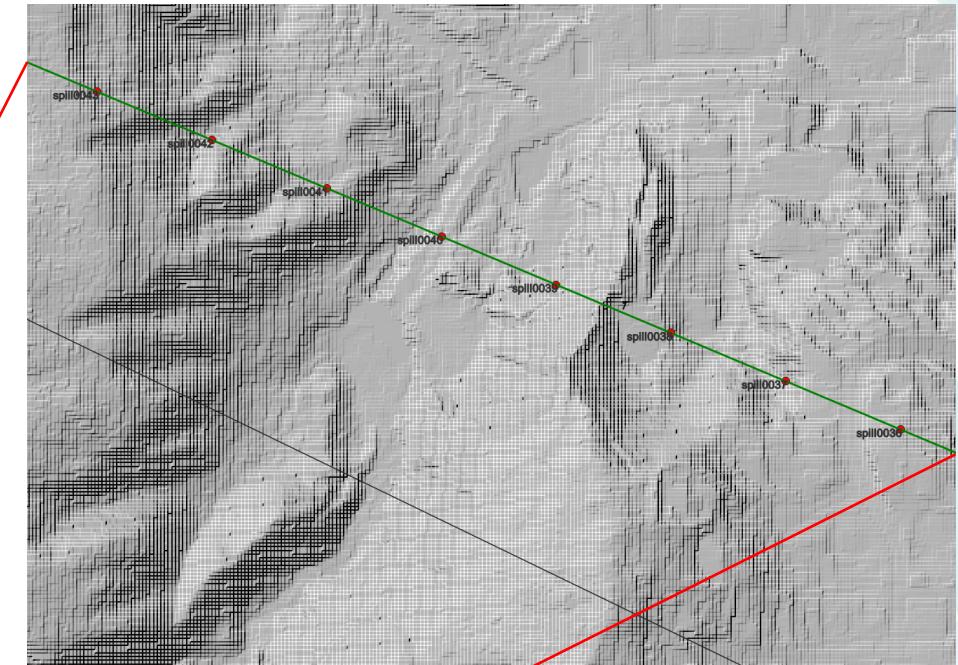
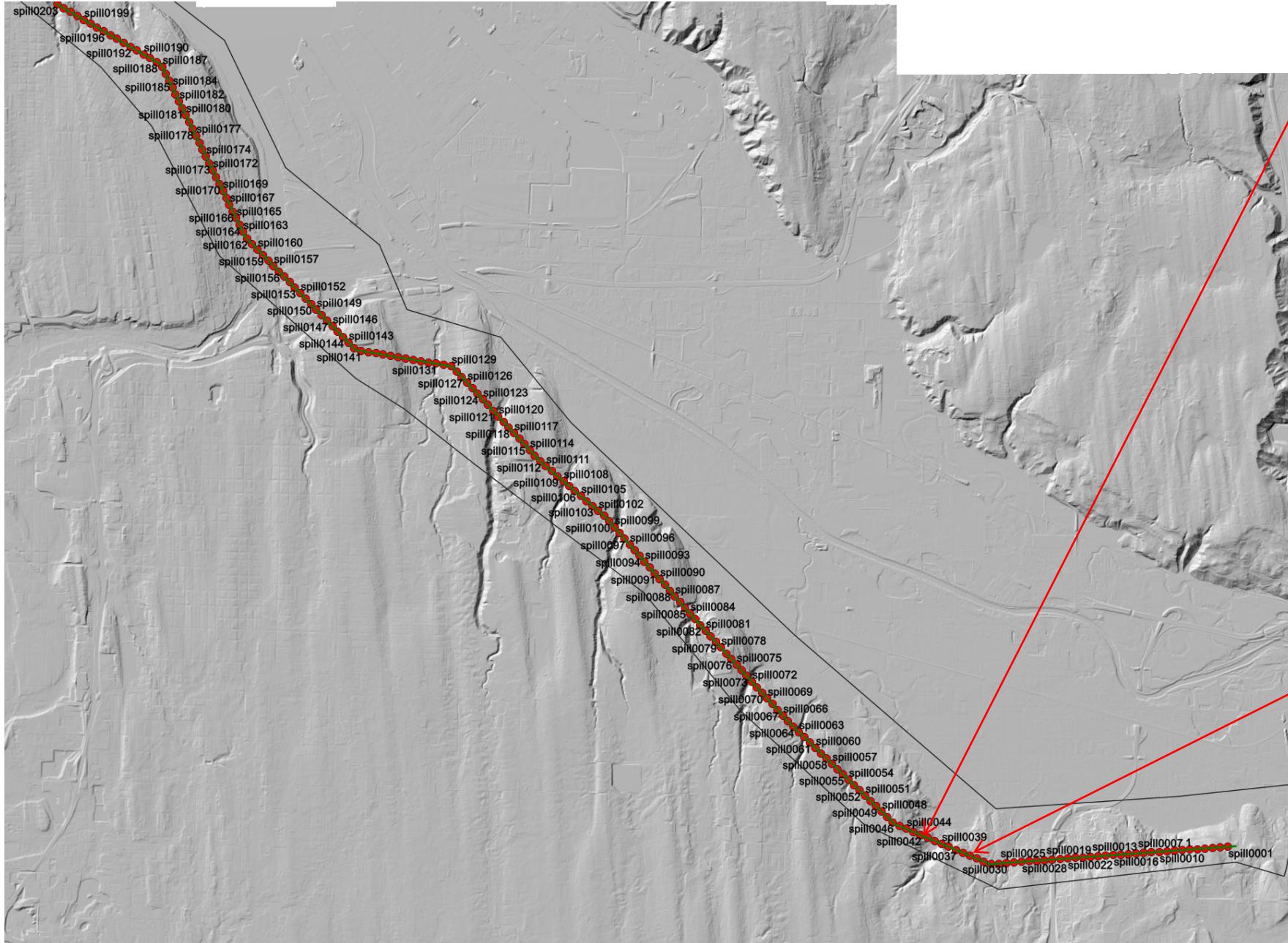
Initial flowrate (m³/s) :

Valve closing time (seconds) :

Assign elevations to spill points from:

OilPipeline nodes
 DEM layer DEM12Merged Offset (m) :
 Get elevations from Multiple DEM Boundaries
 Using local mesh Cell Size : H/V Size (m) :

Automatic Generation of Spill Sources

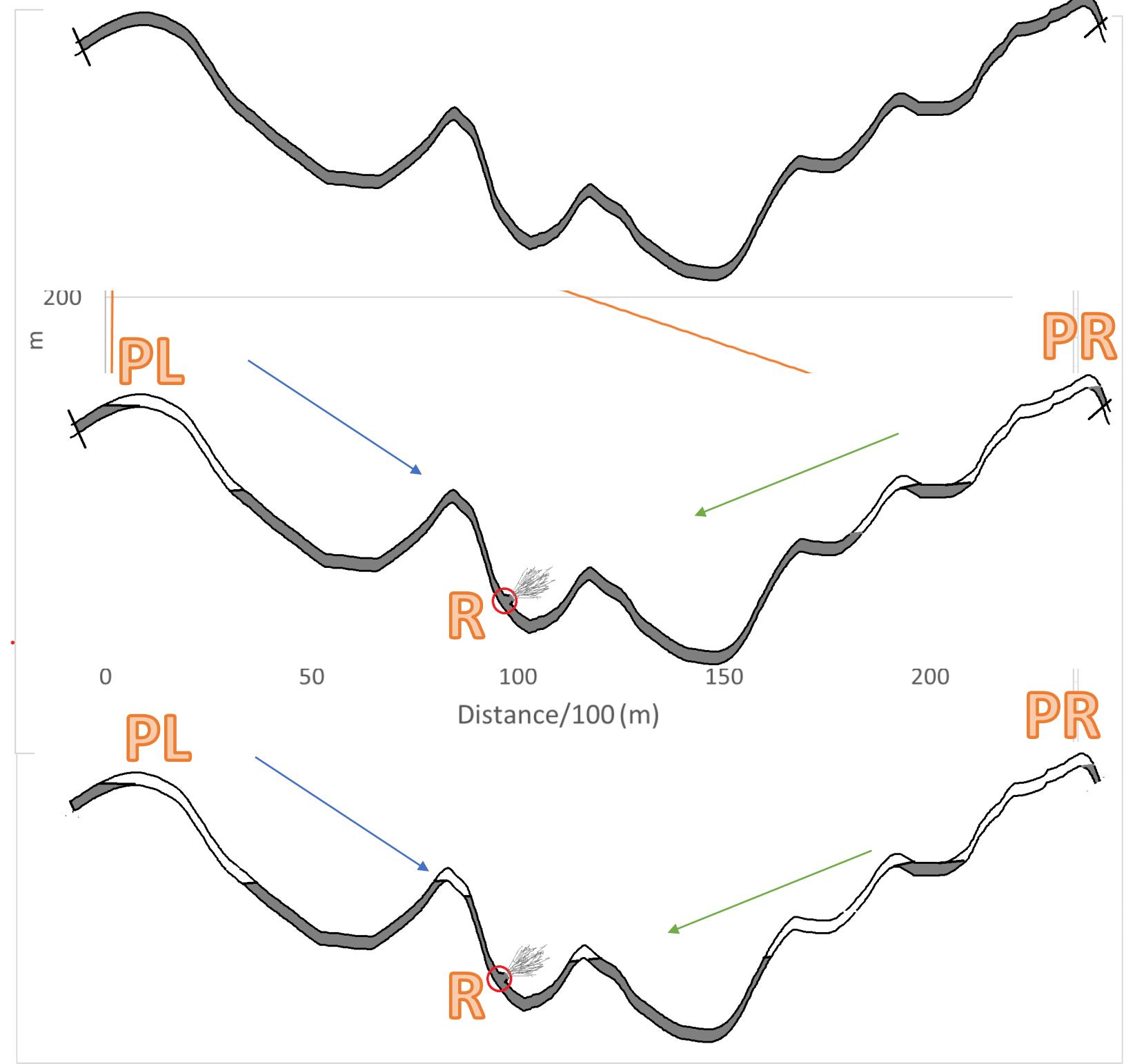




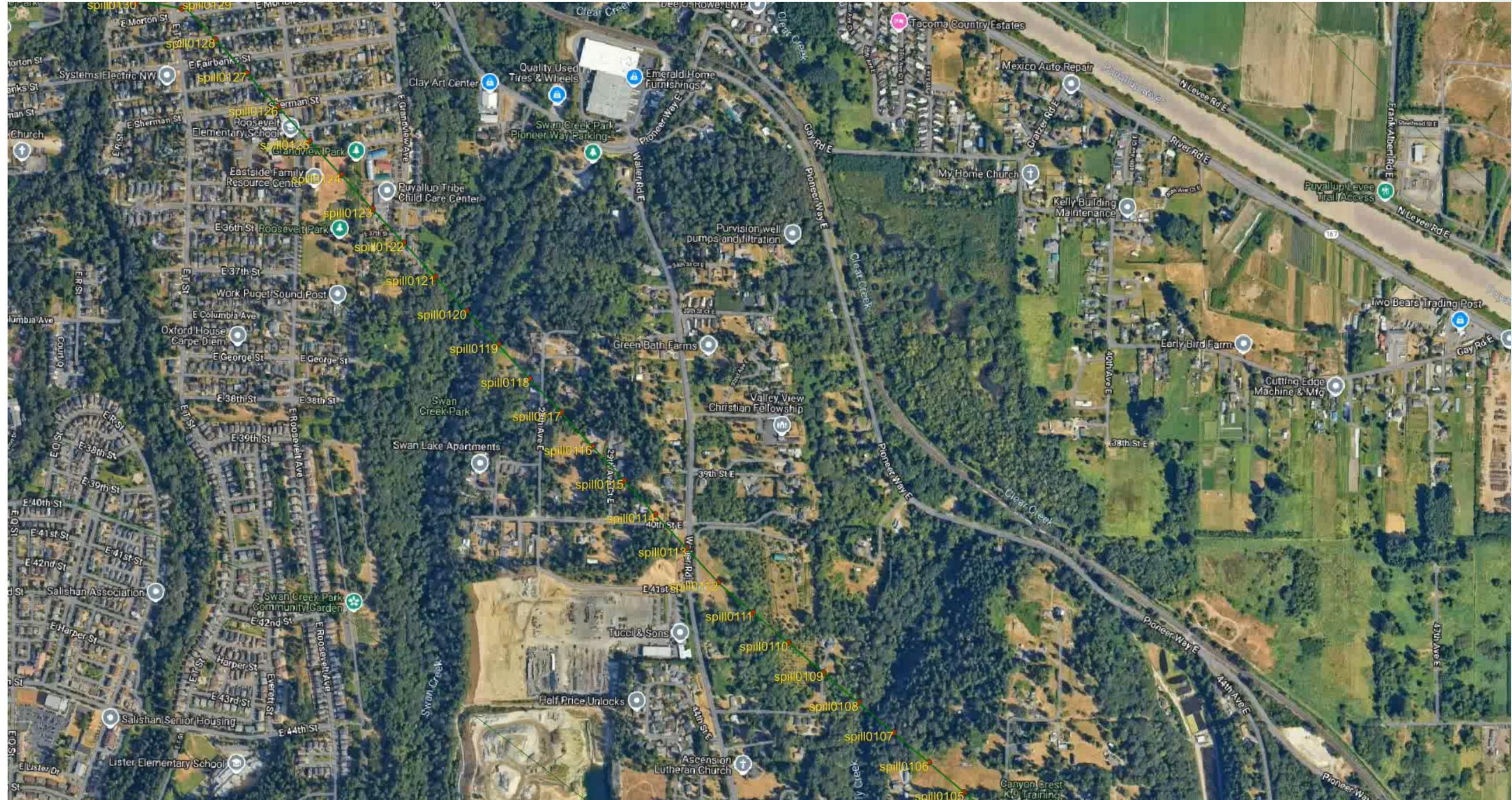
Oil leak discharge Calculation

- Initial steady state: Q, Pressure
- For each leak point
 - From PL to R and from PR to R apply Quasi-Unsteady 1D Continuity and Energy equations
 - Export Q vs *time* table for each leak point

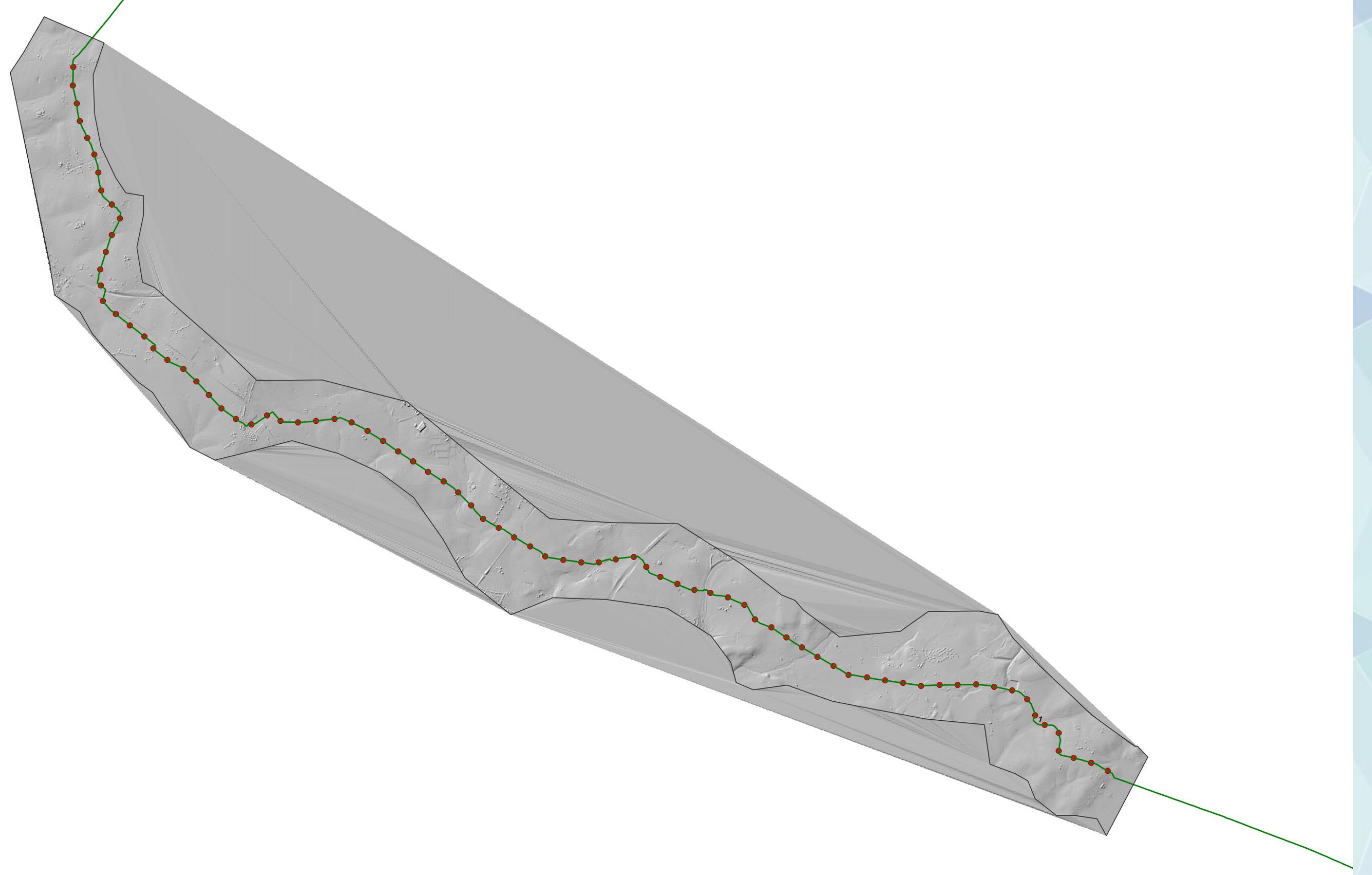
Time (s)	Time (h)	spill0001 (m ³ /s)	spill0002 (m ³ /s)	spill0003 (m ³ /s)	spill0004 (m ³ /s)	spill0005 (m ³ /s)	spill0006 (m ³ /s)	spill0007 (m ³ /s)
0	0	1.9755	1.9678	0	0.1769	1.6717	2.2839	2.387
1.0008	0.000278	1.9666	1.952	0	0.175	0.2971	2.2667	2.37
2.0016	0.000556	1.9577	1.9362	0	0.173	0.2944	2.2493	2.354
2.9988	0.000833	1.9488	1.3188	0	0.1711	0.2917	2.2318	2.338
3.9996	0.001111	1.9397	0	0	0.1692	0.289	2.2142	2.322
5.0004	0.001389	1.9306	0	0	0.1672	0.2863	2.1965	2.305
6.0012	0.001667	1.9214	0	0	0.1653	0.2835	2.1787	2.288
6.9984	0.001944	0.6228	0	0	0.1633	0.2808	1.7053	2.272
7.9992	0.002222	0	0	0	0.1613	0.278	0.5512	2.255
9	0.0025	0	0	0	0.1593	0.2752	0.543	2.238
10.0008	0.002778	0	0	0	0.1573	0.2724	0.5348	1.935
11.0016	0.003056	0	0	0	0.1553	0.2696	0.5265	0.611
11.9988	0.003333	0	0	0	0.1532	0.2667	0.5182	0.603
12.9996	0.003611	0	0	0	0.1512	0.2639	0.5098	0.595
14.0004	0.003889	0	0	0	0.1491	0.261	0.5014	0.588
15.0012	0.004167	0	0	0	0.147	0.2581	0.4929	0.580
15.9984	0.004444	0	0	0	0.145	0.2552	0.4843	0.572
16.9992	0.004722	0	0	0	0.1429	0.2523	0.4757	0.564
18	0.005	0	0	0	0.1407	0.2493	0.4671	0.556
19.0008	0.005278	0	0	0	0.1386	0.2464	0.4584	0.548
20.0016	0.005556	0	0	0	0.1365	0.2434	0.4496	0.539
20.9988	0.005833	0	0	0	0.1343	0.2404	0.4408	0.531
21.9996	0.006111	0	0	0	0.1322	0.2374	0.4319	0.523
23.0004	0.006389	0	0	0	0.13	0.2343	0.423	0.515
24.0012	0.006667	0	0	0	0.1278	0.2313	0.414	0.506
24.9984	0.006944	0	0	0	0.1256	0.2282	0.405	0.498
25.9992	0.007222	0	0	0	0.1234	0.2252	0.3959	0.489
27	0.0075	0	0	0	0.1212	0.222	0.3868	0.481
28.0008	0.007778	0	0	0	0.1189	0.2189	0.3775	0.472
29.0016	0.008056	0	0	0	0.1167	0.2158	0.3683	0.464
29.9988	0.008333	0	0	0	0.1144	0.2126	0.3589	0.455
30.9996	0.008611	0	0	0	0.1121	0.2094	0.3495	0.446
32.0004	0.008889	0	0	0	0.1098	0.2063	0.3401	0.438



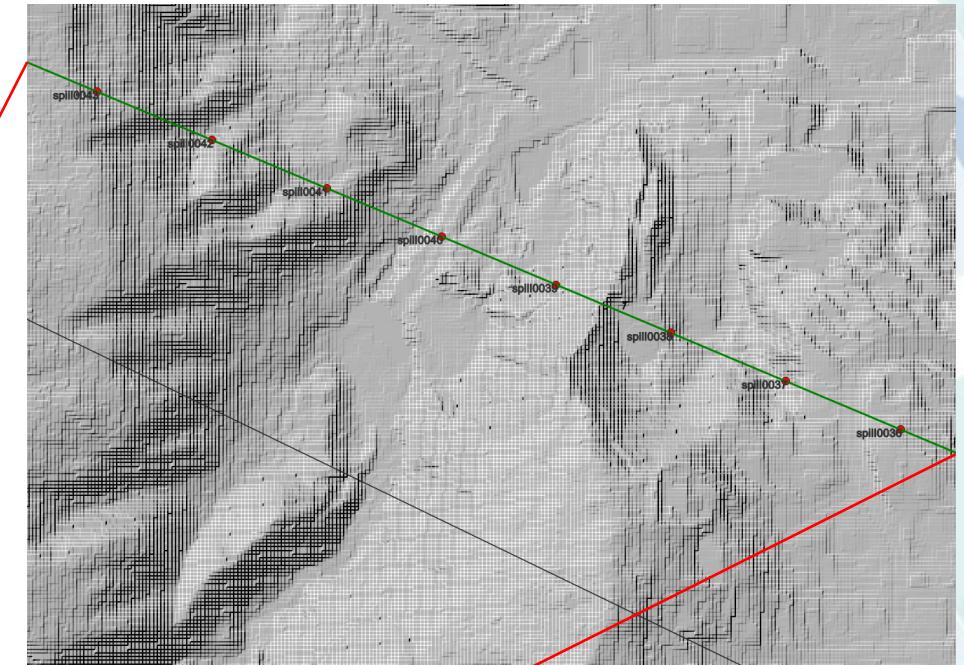
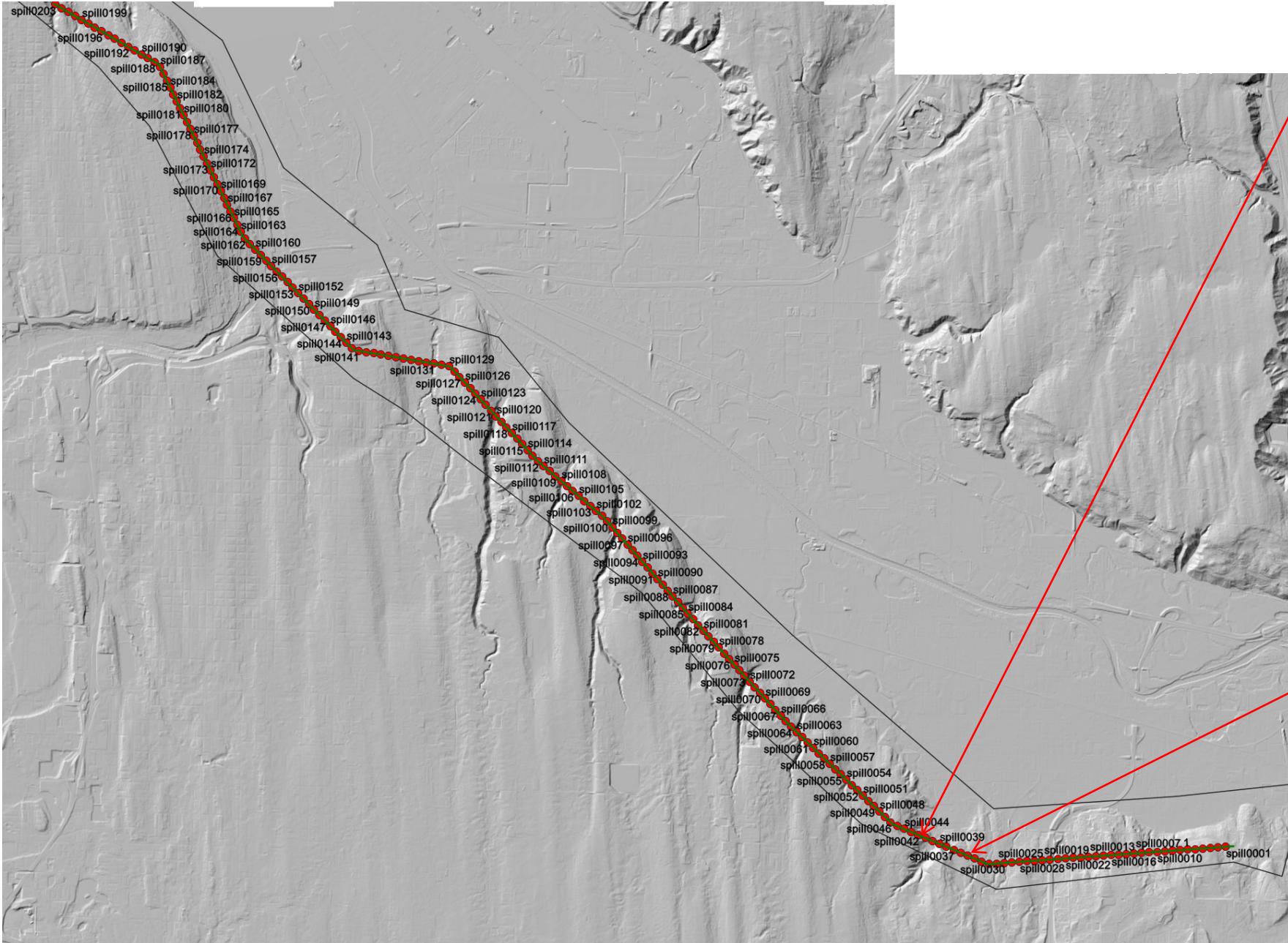
Oil Spill Spreading Animation for Spill 116



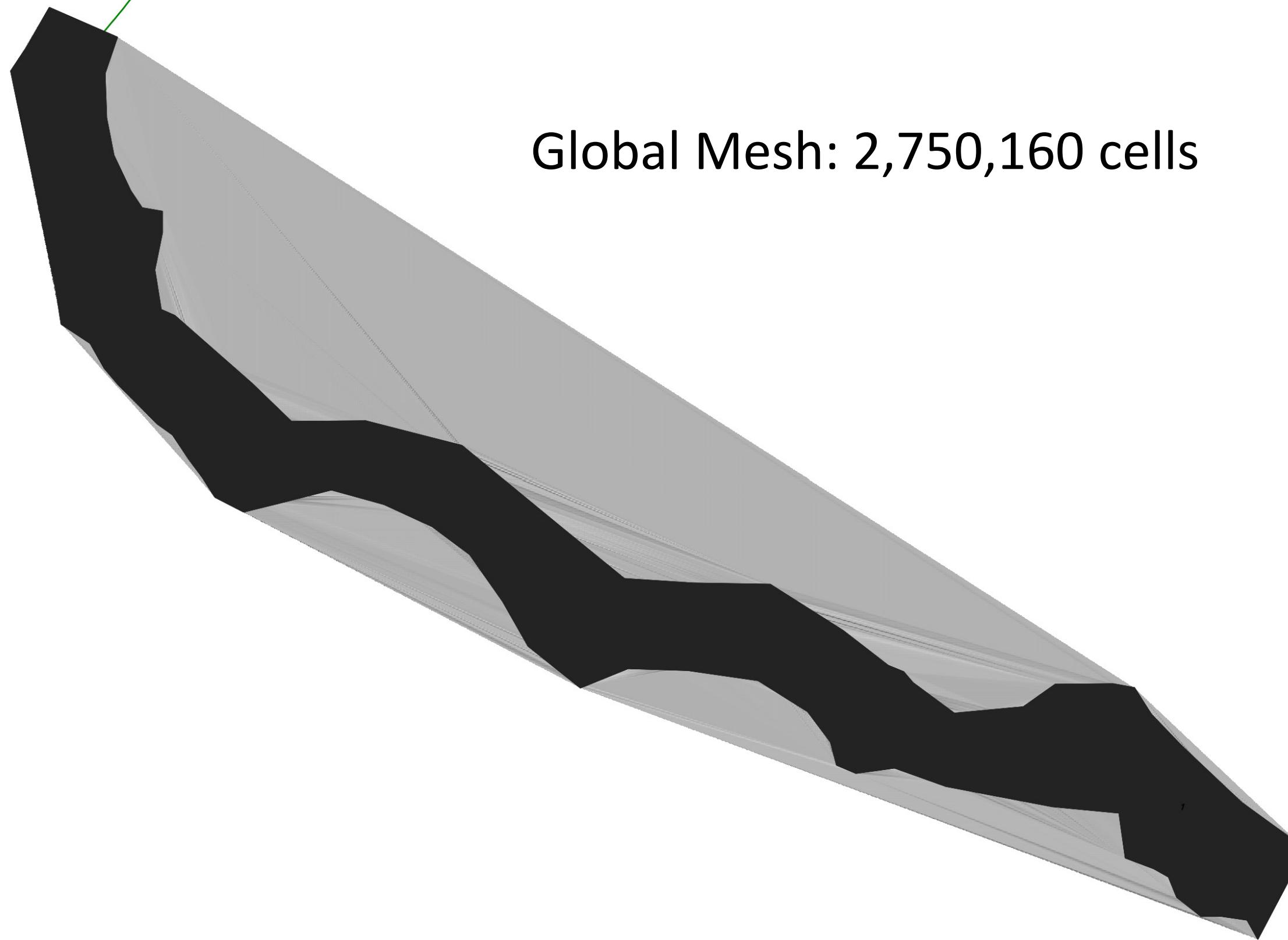
HYDRONIA

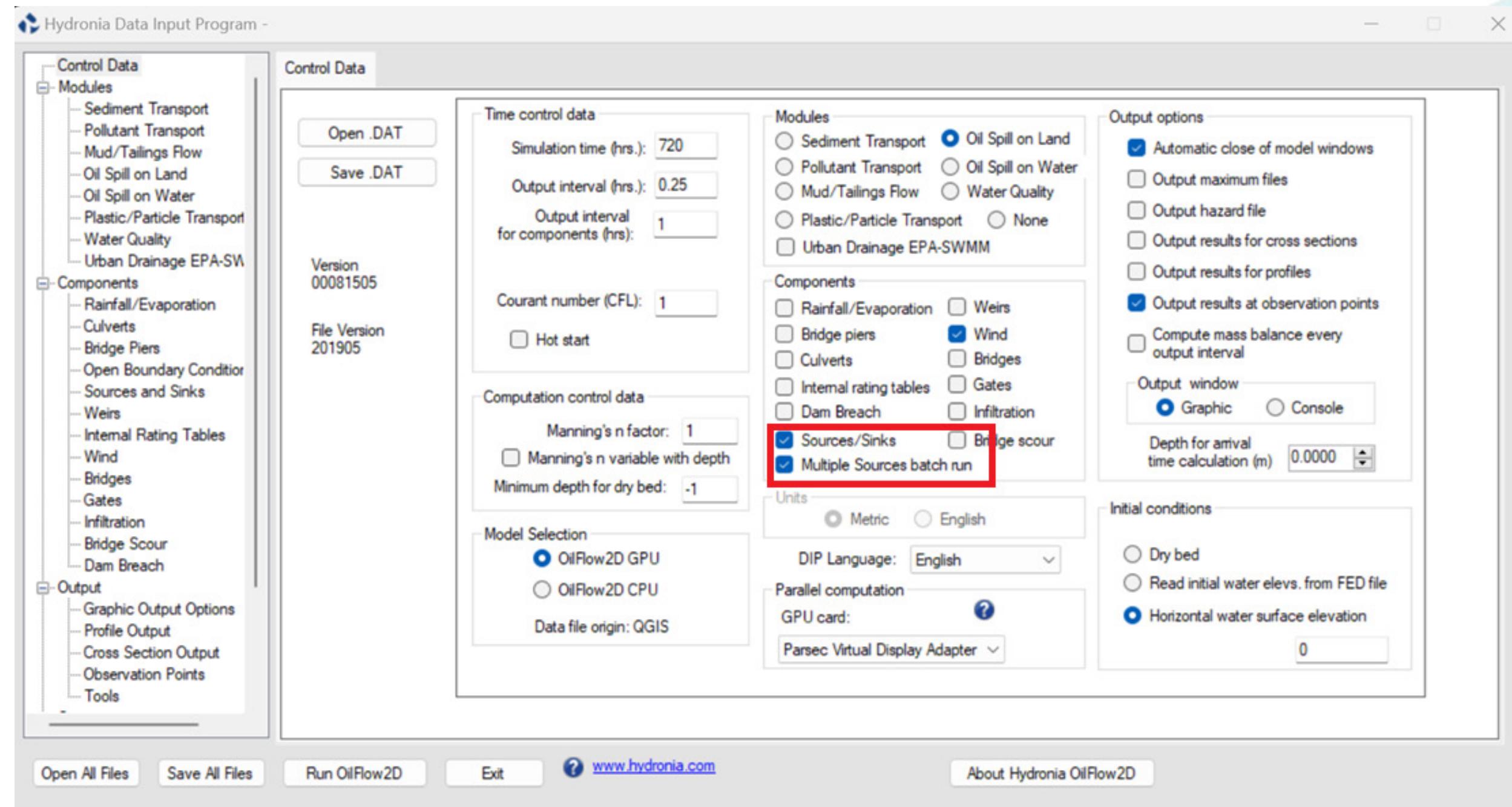


User Defined Spill Sources



Global Mesh: 2,750,160 cells



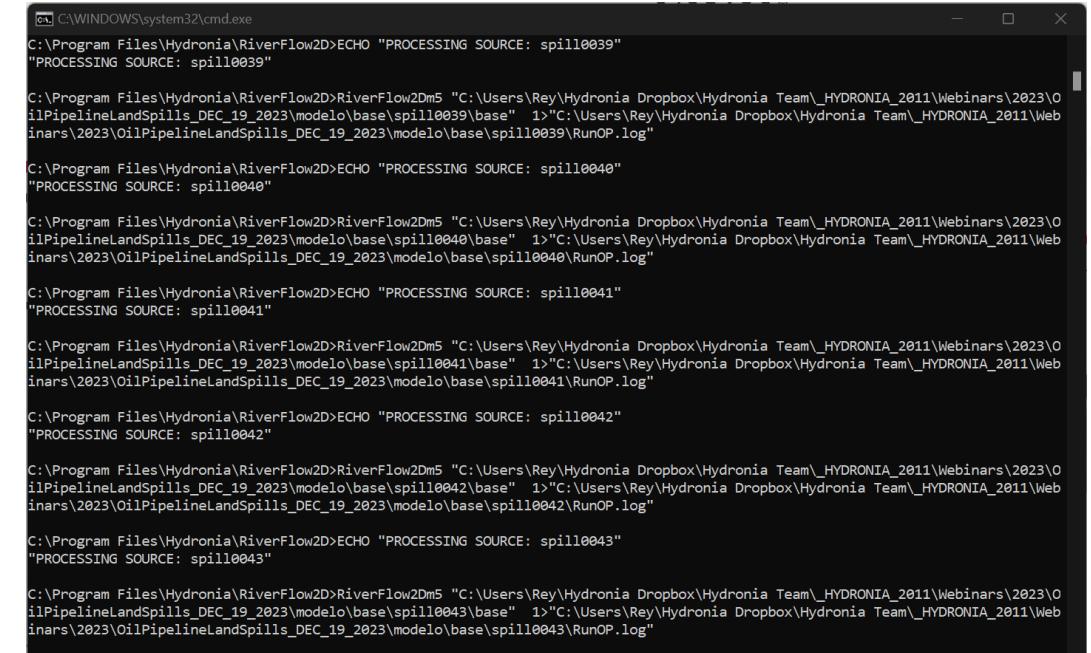


Batch Run of All Spills

- Automate running thousands of spills

- Little user action required

- Results for each spill are written in separate directories



```
C:\WINDOWS\system32\cmd.exe
C:\Program Files\Hydronia\RiverFlow2D>ECHO "PROCESSING SOURCE: spill0039"
"PROCESSING SOURCE: spill0039"

C:\Program Files\Hydronia\RiverFlow2D>RiverFlow2Dm5 "C:\Users\Rey\Hydronia Dropbox\Hydronia Team\_HYDRONIA_2011\Webinars\2023\OilPipelineLandSpills_DEC_19_2023\modelo\base\spill0039\base" 1>"C:\Users\Rey\Hydronia Dropbox\Hydronia Team\_HYDRONIA_2011\Webinars\2023\OilPipelineLandSpills_DEC_19_2023\modelo\base\spill0039\RunOP.log"

C:\Program Files\Hydronia\RiverFlow2D>ECHO "PROCESSING SOURCE: spill0040"
"PROCESSING SOURCE: spill0040"

C:\Program Files\Hydronia\RiverFlow2D>RiverFlow2Dm5 "C:\Users\Rey\Hydronia Dropbox\Hydronia Team\_HYDRONIA_2011\Webinars\2023\OilPipelineLandSpills_DEC_19_2023\modelo\base\spill0040\base" 1>"C:\Users\Rey\Hydronia Dropbox\Hydronia Team\_HYDRONIA_2011\Webinars\2023\OilPipelineLandSpills_DEC_19_2023\modelo\base\spill0040\RunOP.log"

C:\Program Files\Hydronia\RiverFlow2D>ECHO "PROCESSING SOURCE: spill0041"
"PROCESSING SOURCE: spill0041"

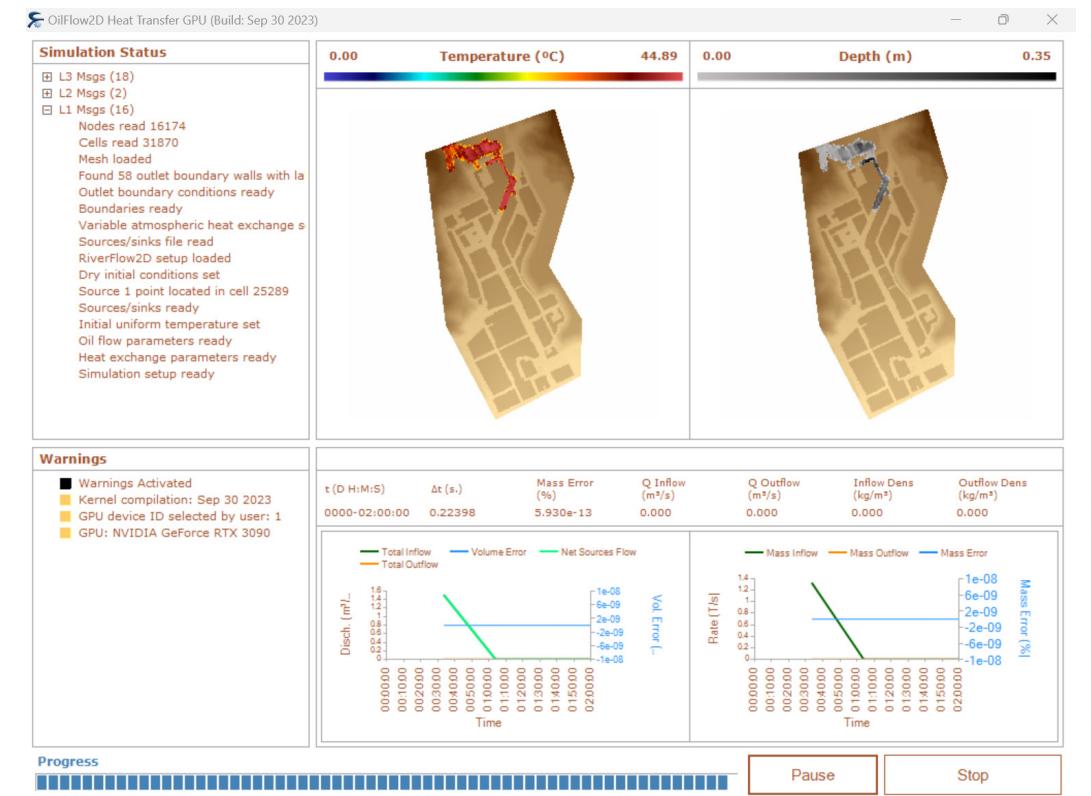
C:\Program Files\Hydronia\RiverFlow2D>RiverFlow2Dm5 "C:\Users\Rey\Hydronia Dropbox\Hydronia Team\_HYDRONIA_2011\Webinars\2023\OilPipelineLandSpills_DEC_19_2023\modelo\base\spill0041\base" 1>"C:\Users\Rey\Hydronia Dropbox\Hydronia Team\_HYDRONIA_2011\Webinars\2023\OilPipelineLandSpills_DEC_19_2023\modelo\base\spill0041\RunOP.log"

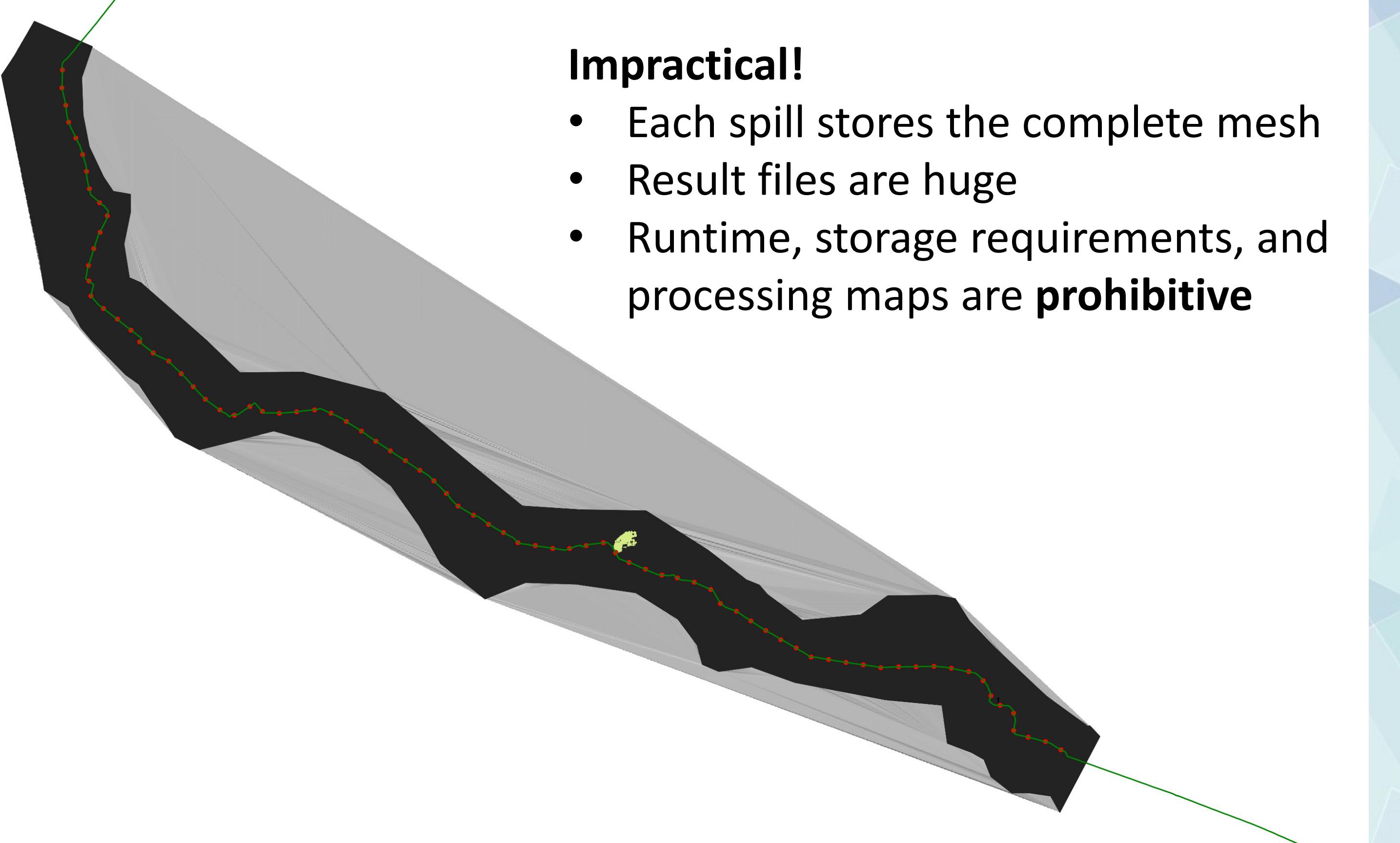
C:\Program Files\Hydronia\RiverFlow2D>ECHO "PROCESSING SOURCE: spill0042"
"PROCESSING SOURCE: spill0042"

C:\Program Files\Hydronia\RiverFlow2D>RiverFlow2Dm5 "C:\Users\Rey\Hydronia Dropbox\Hydronia Team\_HYDRONIA_2011\Webinars\2023\OilPipelineLandSpills_DEC_19_2023\modelo\base\spill0042\base" 1>"C:\Users\Rey\Hydronia Dropbox\Hydronia Team\_HYDRONIA_2011\Webinars\2023\OilPipelineLandSpills_DEC_19_2023\modelo\base\spill0042\RunOP.log"

C:\Program Files\Hydronia\RiverFlow2D>ECHO "PROCESSING SOURCE: spill0043"
"PROCESSING SOURCE: spill0043"

C:\Program Files\Hydronia\RiverFlow2D>RiverFlow2Dm5 "C:\Users\Rey\Hydronia Dropbox\Hydronia Team\_HYDRONIA_2011\Webinars\2023\OilPipelineLandSpills_DEC_19_2023\modelo\base\spill0043\base" 1>"C:\Users\Rey\Hydronia Dropbox\Hydronia Team\_HYDRONIA_2011\Webinars\2023\OilPipelineLandSpills_DEC_19_2023\modelo\base\spill0043\RunOP.log"
```





Impractical!

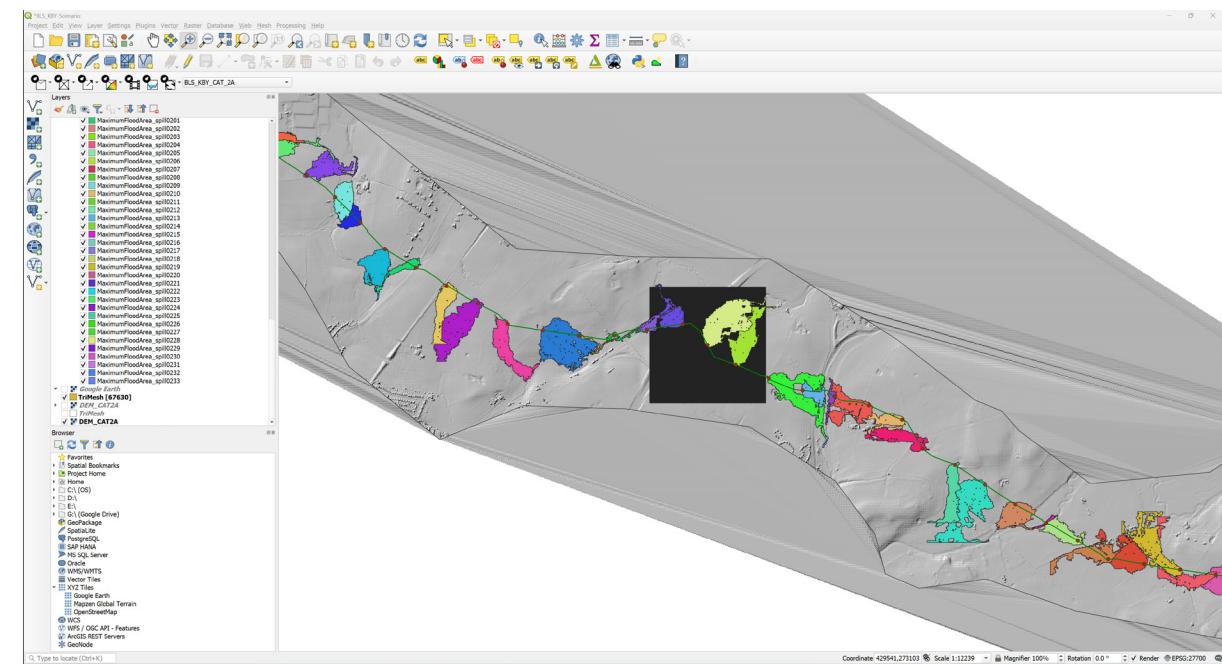
- Each spill stores the complete mesh
- Result files are huge
- Runtime, storage requirements, and processing maps are **prohibitive**

Alternative: Local Mesh Optimization

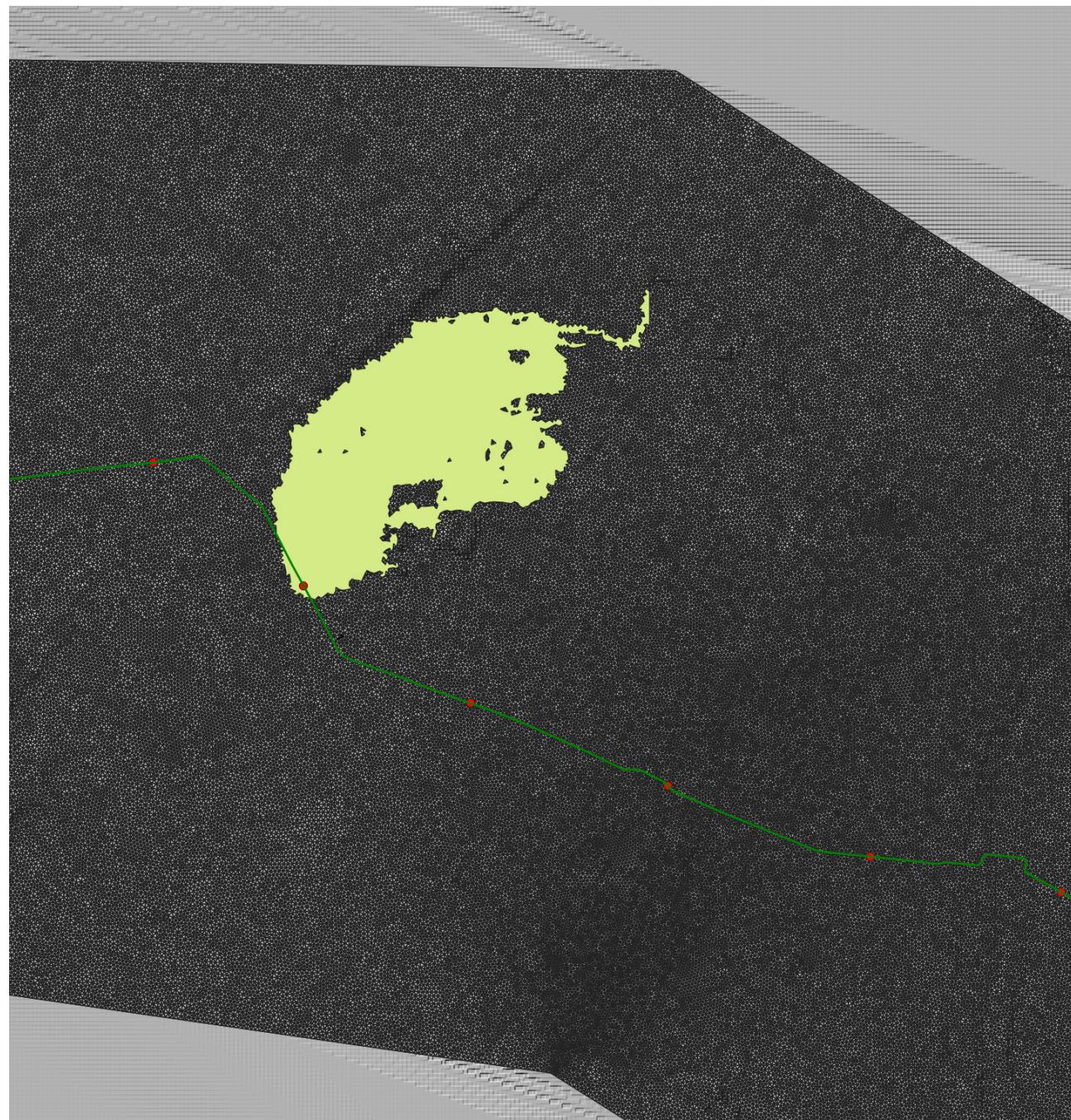
- Local meshes are automatically generated for each spill
- Global mesh is not required
- If the oil impacts the mesh boundary for a given spill, the domain is automatically extended and a new run is performed
- The process finalizes when all spills are contained within their respective domains.

Advantages

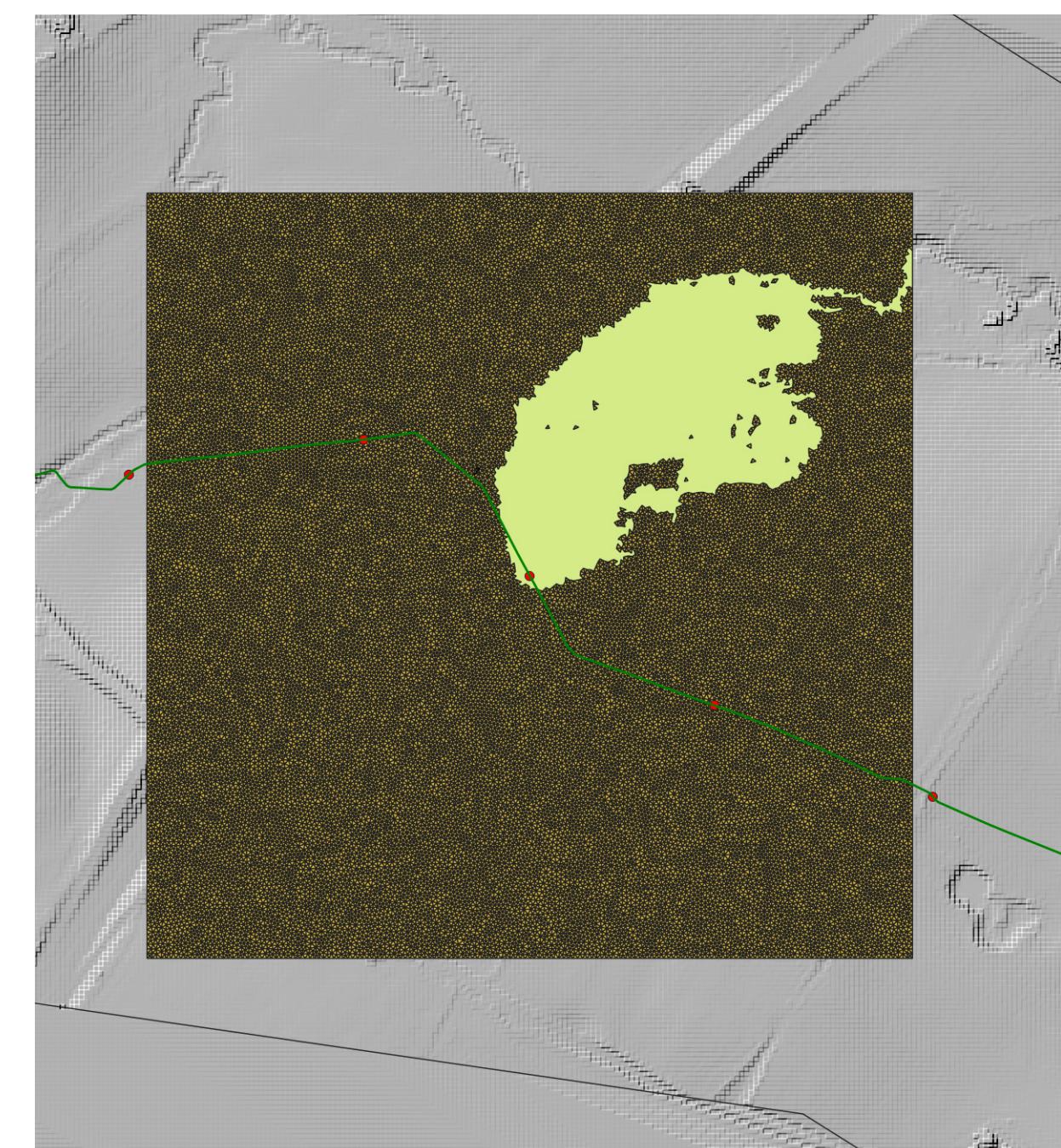
- Minimum user intervention
- Global mesh is not required
- Much smaller meshes
 - Increased local resolution
 - Shorter runtimes
 - Smaller file sizes
 - Shorter map generation times



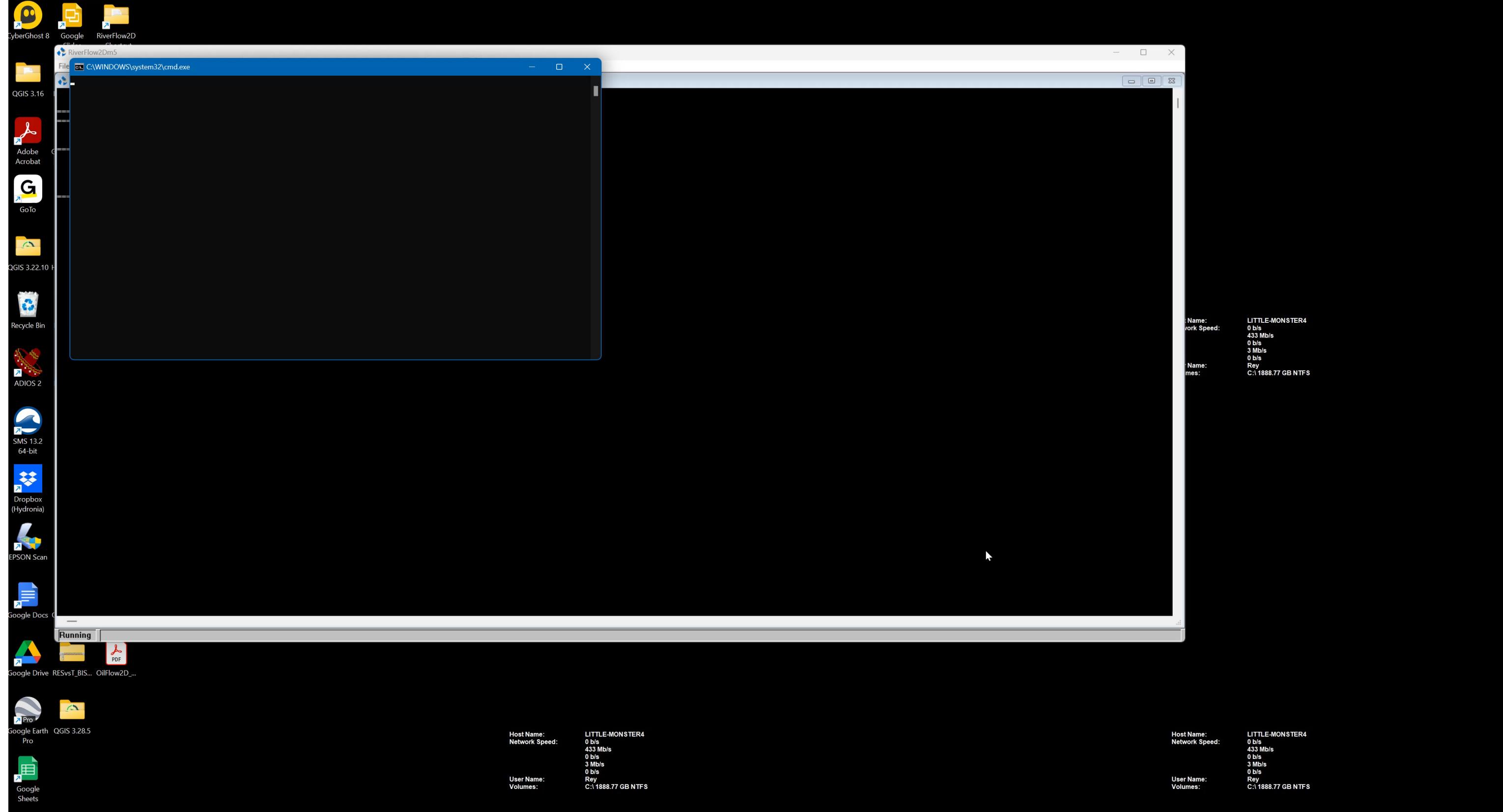
Global Mesh: 2,750,168 cells

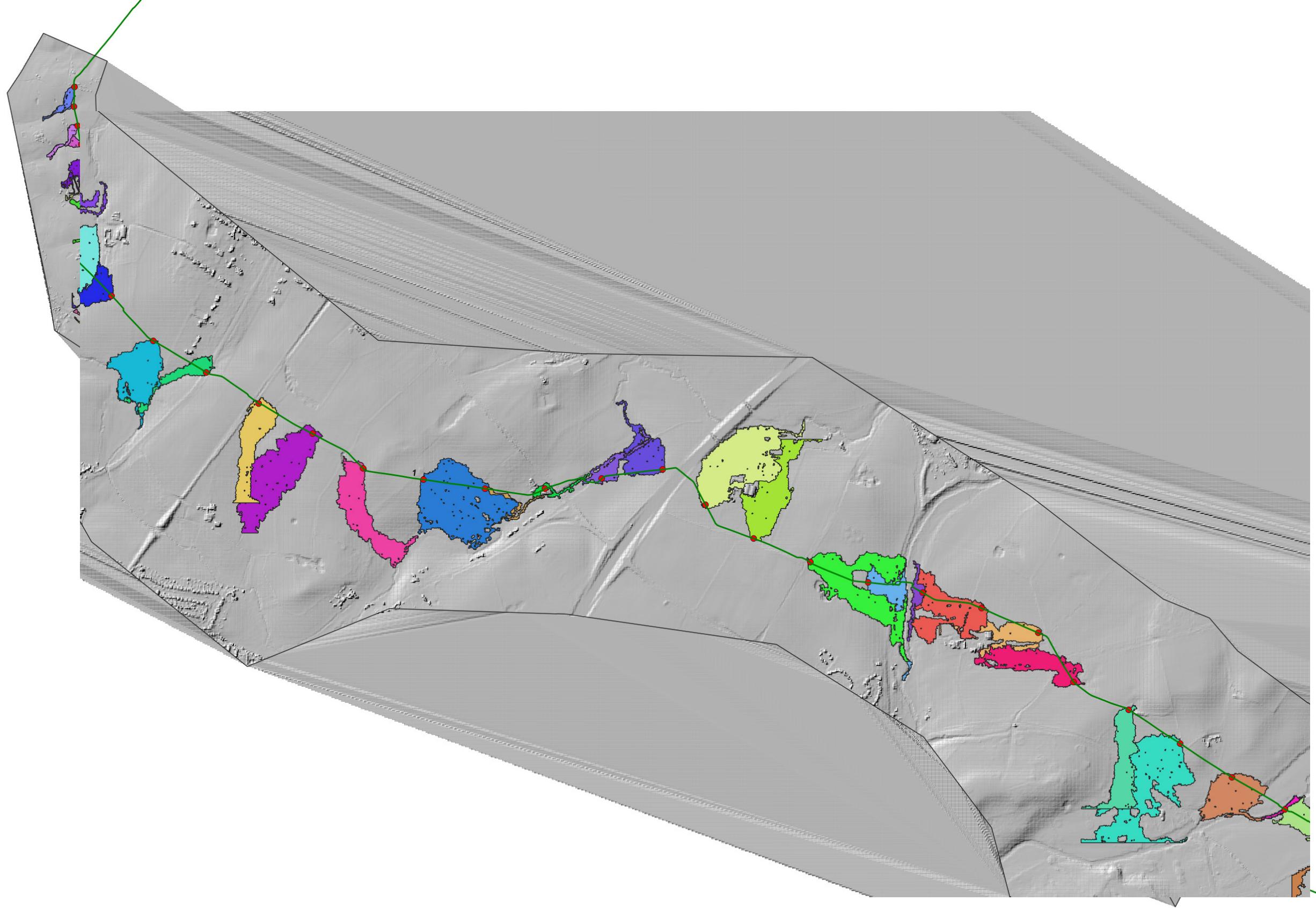


Local Mesh 67,630 cells



HYDRONIA



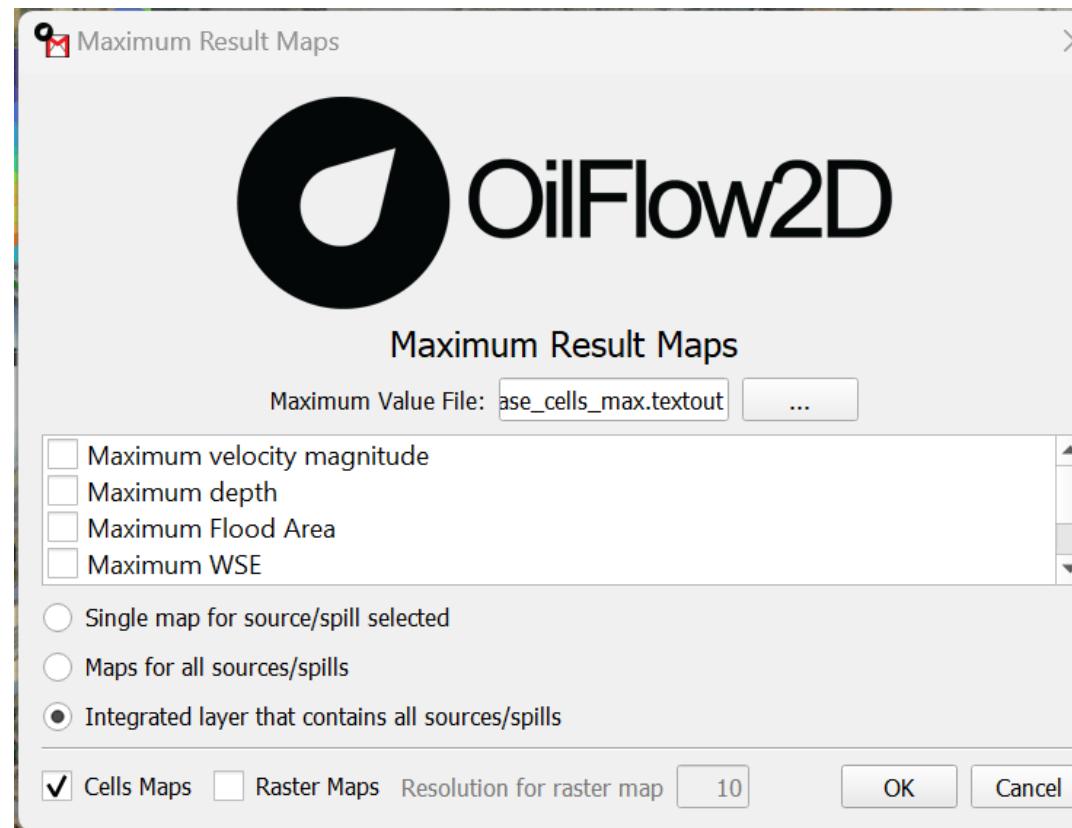


Optimized Algorithm Improvements

	Global Mesh	Local Meshes
Number of cells	2.7 M	67k
Run time (81 spills)	8 hours	1.5 hours
Project size	1.39 TB	36 GB
Map processing time	4 hours	3 minutes

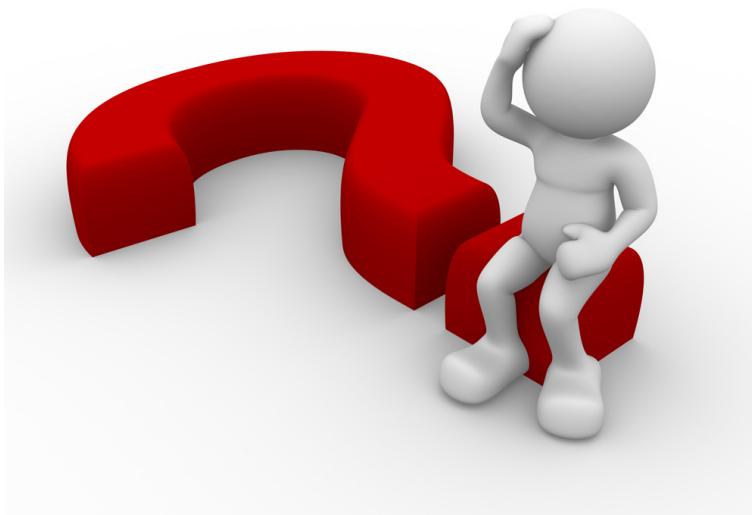
Maps/Shapefiles Generation Automation

- All spills map with a single click



Final Thought

- *Often you should stop programming for a moment and try to see the big picture*



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