

材料力学 4回目

[1] (1) 温度上昇後の2つの材料の長さは等しいので、

$$\begin{cases} l' = l + \alpha_A l \Delta T_1 \\ l' = (l - \Delta l) + \alpha_B (l - \Delta l) \Delta T_1 \end{cases}$$

$$l + \alpha_A l \Delta T_1 = (l - \Delta l) + \alpha_B (l - \Delta l) \Delta T_1$$

$$\Delta T_1 \{ (\alpha_B - \alpha_A) l - \alpha_B \Delta l \} = \Delta l$$

$$\therefore \Delta T_1 = \frac{\Delta l}{(\alpha_B - \alpha_A) l - \alpha_B \Delta l}$$

$$l' = l + \alpha_A l \frac{\Delta l}{(\alpha_B - \alpha_A) l - \alpha_B \Delta l} = l \left\{ 1 + \frac{\alpha_A \Delta l}{(\alpha_B - \alpha_A) l - \alpha_B \Delta l} \right\}$$

(2) 軸力をPとすると、A、Bそれぞれの伸びは、

$$\lambda_A = \frac{R l' \alpha_A}{E_A S_A} + \alpha_A l' \Delta T_2, \quad \lambda_B = \frac{P l' \alpha_B}{E_B S_B} + \alpha_B l' \Delta T_2$$

$$\lambda_A = \lambda_B \text{ より,}$$

$$\frac{\alpha_A P l'}{E_A S_A} + \alpha_A l' \Delta T_2 = \frac{\alpha_B P l'}{E_B S_B} + \alpha_B l' \Delta T_2$$

$$\left(\frac{1}{E_A S_A} - \frac{1}{E_B S_B} \right) P = (\alpha_B - \alpha_A) \Delta T_2$$

$$P = - \frac{(\alpha_B - \alpha_A) \Delta T_2}{\frac{1}{E_A S_A} - \frac{1}{E_B S_B}} = - \frac{(\alpha_B - \alpha_A) \Delta T_2 E_A S_A E_B S_B}{E_B S_B - E_A S_A}$$

$$\therefore \sigma_A = \frac{P}{S_A} = - \frac{(\alpha_B - \alpha_A) E_A E_B S_B \Delta T_2}{E_A S_A - E_B S_B}$$

$$\sigma_B = \frac{P}{S_B} = - \frac{(\alpha_B - \alpha_A) E_A S_A E_B \Delta T_2}{E_A S_A - E_B S_B}$$

軸力: P_A, P_B

$$P_A + P_B = 0 \quad \text{2つ可}$$

力のつりあいより、

$$\sigma_A S_A + \sigma_B S_B = 0 \Rightarrow \sigma_B = - \frac{S_A}{S_B} \sigma_A$$

$$\left(\frac{1}{E_A} + \frac{S_A}{E_B S_B} \right) \sigma_A = (\alpha_B - \alpha_A) \Delta T_2$$

$$\sigma_A = \frac{(\alpha_B - \alpha_A) E_A E_B S_B \Delta T_2}{E_A S_A + E_B S_B}$$

$$\sigma_B = - \frac{S_A}{S_B} \sigma_A$$

$$= - \frac{(\alpha_B - \alpha_A) E_A S_A E_B \Delta T_2}{E_A S_A + E_B S_B}$$

$$\lambda_A = \frac{\alpha_A l'}{E_A} + \alpha_A l' \Delta T_2 = \frac{(\alpha_B - \alpha_A) E_B S_B \Delta T_2}{E_A S_A + E_B S_B} l' + \alpha_A l' \Delta T_2$$

$$= l' \Delta T_2 \left\{ \alpha_A + \frac{(\alpha_B - \alpha_A) E_B S_B}{E_A S_A + E_B S_B} \right\}$$

$$= l \Delta T_2 \left\{ 1 + \frac{\alpha_A \Delta l}{(\alpha_B - \alpha_A) l - \alpha_B \Delta l} \right\} \left\{ \frac{\alpha_A (E_A S_A + E_B S_B) + (\alpha_B - \alpha_A) E_B S_B}{E_A S_A + E_B S_B} \right\}$$

$$= l \Delta T_2 \left\{ 1 + \frac{\alpha_A \Delta l}{(\alpha_B - \alpha_A) l - \alpha_B \Delta l} \right\} \left(\frac{\alpha_A E_A S_A + \alpha_B E_B S_B}{E_A S_A + E_B S_B} \right)$$

[2] (1) $0 \leq x \leq l$ において,

$$M_x = R_A x - \frac{1}{2} w x^2 - M_A$$

(2) $\frac{d^2 \theta}{dx^2} = -\frac{M_x}{EI} \rightarrow EI \frac{d^2 \theta}{dx^2} = \frac{1}{2} w x^2 - R_A x + M_A$

$$EI \frac{d\theta}{dx} = \frac{1}{6} w x^3 - \frac{1}{2} R_A x^2 + M_A x + C_1$$

$$EI \theta = \frac{1}{24} w x^4 - \frac{1}{6} R_A x^3 + \frac{1}{2} M_A x^2 + C_1 x + C_2$$

境界条件より, $x=0$ において, $\frac{d\theta}{dx} = 0$, $\theta = 0$

$x=l$ において, $\frac{d\theta}{dx} = 0$, $\theta = 0$

$$EI \left(\frac{d\theta}{dx} \right)_{x=0} = 0 - 0 + 0 + C_1 \rightarrow C_1 = 0$$

$$EI \theta_{x=0} = 0 - 0 + 0 + 0 + C_2 = 0 \rightarrow C_2 = 0$$

$$EI \left(\frac{d\theta}{dx} \right)_{x=l} = \frac{1}{6} w l^3 - \frac{1}{2} R_A l^2 + M_A l = 0 \rightarrow M_A = \frac{1}{2} R_A l - \frac{1}{6} w l^2$$

$$EI \theta_{x=l} = \frac{1}{24} w l^4 - \frac{1}{6} R_A l^3 + \frac{1}{2} M_A l^2 = 0$$

$$\frac{1}{24} w l^4 - \frac{1}{6} R_A l^3 + \frac{1}{2} \left(\frac{1}{2} R_A l - \frac{1}{6} w l^2 \right) l^2 = 0$$

$$\frac{1}{12} R_A l = \frac{1}{24} w l^3 \rightarrow \therefore R_A = \frac{1}{2} w l$$

$$M_A = \frac{1}{4} w l^2 - \frac{1}{6} w l^2 = \frac{1}{12} w l^2$$

(3)

$$M_C = R_A l - M_A - \frac{1}{2} w l^2 = \frac{1}{2} w l^2 - \frac{1}{12} w l^2 - \frac{1}{2} w l^2 = -\frac{1}{12} w l^2$$

対称性より, $R_B = R_A = \frac{1}{2} w l$, $M_B = M_A = \frac{1}{12} w l^2$

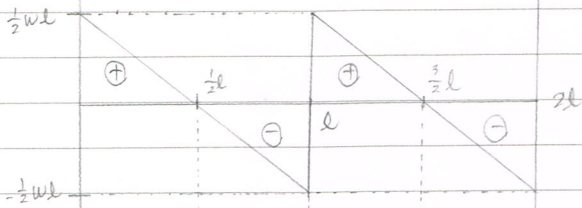
力のつりあいより,

$$R_A + R_B + R_C = 2 w l \rightarrow R_C = 2 w l - w l = w l$$

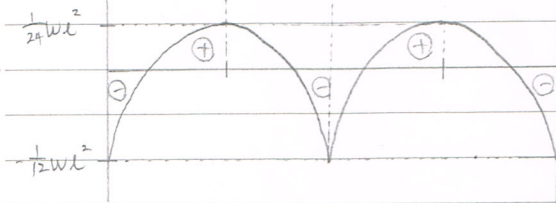
$$V_x - R_A + w x = 0 \rightarrow V_x = \frac{1}{2} w l - w x = w \left(\frac{1}{2} l - x \right)$$

$$M_x = -\frac{1}{2} w x^2 + \frac{1}{2} w l - \frac{1}{12} w l^2 = -\frac{1}{2} w \left(x^2 - l \right) - \frac{1}{12} w l^2 = -\frac{1}{2} w \left(x - \frac{l}{2} \right)^2 + \frac{1}{24} w l^2$$

SFD



BMD



$$[3] (1) \lambda_A = \frac{Pl}{EA} = \frac{4Pl}{\pi E d^2}$$

$$(2) A_B = \frac{\pi}{4} d^2 - \frac{\pi}{4} \left(\frac{d}{2}\right)^2 = \frac{3}{16} \pi d^2$$

$$\lambda_B = \frac{Pl}{EA_B} = \frac{16Pl}{3\pi E d^2}$$

$$(3) \frac{\lambda_B}{\lambda_A} = \frac{\frac{16}{3}}{4} = \frac{4}{3}$$

$$(4) T = GI_{PA} \theta_A, \quad I_{PA} = \int r^2 dA = \int_0^{\frac{d}{2}} r^2 \cdot 2\pi r dr = \frac{\pi}{2} \left[r^4 \right]_0^{\frac{d}{2}} = \frac{\pi}{32} d^4 \quad \text{ft},$$

$$\therefore T = \frac{\pi d^4 G \theta_A}{32}$$

$$(5) I_{PB} = \int r^2 dA = \frac{\pi}{2} \left[r^4 \right]_{\frac{d}{4}}^{\frac{d}{2}} = \frac{\pi}{2} \left(\frac{\pi}{16} d^4 - \frac{\pi}{256} d^4 \right) = \frac{15}{512} \pi d^4$$

$$\therefore T = GI_{PB} \theta_B = \frac{15 \pi d^4 G \theta_B}{512}$$

$$(6) \theta_A = 32T / \pi d^4 G, \quad \theta_B = 512T / 15 \pi d^4 G \quad \text{ft},$$

$$\frac{\theta_B}{\theta_A} = \frac{512/15}{32} = \frac{16 \cdot 2}{15 \cdot 2} = \frac{16}{15}$$