熱力学 4回目

[1] (1) 開いた系のエネルギ式かり、  $E_{I} = m \left( h_{I} + \frac{1}{2} W_{I}^{2} + \theta Z_{I} \right)$ 

- (2)  $m(\hat{h}_{I} + \frac{1}{2}w_{z}^{2} + \vartheta z_{1}) Q_{L} = m(\hat{h}_{I} + \frac{1}{2}w_{x}^{2} + \vartheta z_{x}) + W_{t}$ :  $W_t = m \{ (h_I - h_I) + \frac{1}{2} (W_I^2 - W_I^2) + \theta (Z_I - Z_I) \}^2 - Q_L$
- (3) 絞り前後ではエニタルピの変化はないので、はこの  $dt = C_P dT + [V - T(\partial V/\partial T)P] dP = 0$  $\frac{\partial T}{\partial P} = -\frac{1}{C_P} \left\{ V - T \left( \frac{\partial V}{\partial T} \right)_P \right\}$

ュール・トムリン効果り、逆転運度の際には  $M = \frac{dT}{dp} = 0$ 

$$V - T\left(\frac{\partial V}{\partial T}\right)_{P} = 0$$

PV = aRPT - bT + CP  $V = \alpha R \vec{1} - \frac{h}{P} T + C - 2$ (ar)= 2aRT - b

3 =1,

$$aRT^{2} - pT + C - 2aRT^{2} + pT = 0$$

 $\alpha RT^2 = C$ 

$$T = \begin{bmatrix} C \\ aR \end{bmatrix}$$

(4) 等エンタルピ変化より、 ま=0  $dh = CpdT + [V - T(\partial V/\partial T)p] dP = 0$ 

$$\frac{dT}{dP} = \frac{1}{C_P} \left\{ V - T \left( \frac{\partial V}{\partial T} \right)_P \right\} = 0$$

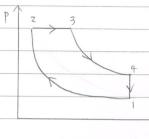
理想気体の状態方程式が、PV=RT→ V=RT/P

#E, 
$$PN - E + 5 | F|$$
,  $\left(\frac{\partial V}{\partial T}\right)_{P} = \frac{R}{P}$ 

dT = 1 (RT TR)=0 > 温度変化なしり

[2] (1)

No.



(2)・2-73;定圧変化が,かり=0

de=dh-vdP to, de=dh=cpdT

:,吸熱量: Q23=),mBTdT= 1mB(T3-T2)

· 4 -> 1;定客変化的, dv = 0

d8 = dutpou +1, d8 = du = crdT

:、放熱量; QH= 5+mxTdT= = 12mx(Ti-T4)

·374;断熟变化的

·172;断熱変化制,

Q34 = [0]

Q12 = 0

(3)·定压变化の2±,如=0

 $d\theta = dR - vdp + \eta$ ,  $d\theta = dR$ 

dq = Tds x),

ds = de dk cpdT =mBdT

S=MBT + So

S= 0 or= , T= To F),

S=mBTo+So= 0 -> So=mBTo

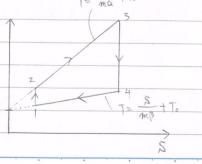
 $: S = m\beta T - m\beta T_0 \rightarrow : T = \frac{S}{m\beta} + T_0$ 

,定客变化も同様(2,

S=MOT-MOTO -> : T= S + To

 $(4) (3) \xi'), T = \frac{8}{m\beta} + T_0$  $T = \frac{s}{m\alpha} + T_o$ 

 $C_{\nu} < C_{\rho} \not\models i), \quad \alpha < \beta \rightarrow \frac{1}{\alpha} > \frac{1}{\beta}$ 





エントロピ変化量は等しいので、

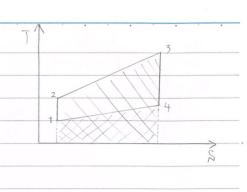
エトロピ変化量をARとおくと

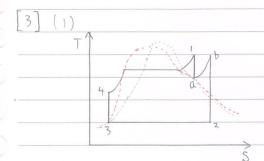
$$Q_1 = \left(T_2 + T_3\right) \cdot \Delta S \cdot \frac{1}{2} = \frac{1}{2} \Delta S \left(T_2 + T_3\right)$$

$$Q_2 = (T_1 + T_4) \cdot \Delta S \cdot \frac{1}{2} = \frac{1}{2} \Delta S (T_1 + T_4)$$

$$\mathcal{N} = \frac{\mathcal{Q}}{\mathcal{Q}} = \frac{Q_1 - Q_2}{Q_1} = \frac{\frac{1}{2}\Delta S \left(T_1 + T_2\right)}{\frac{1}{2}\Delta S \left(T_2 + T_3\right)}$$

$$= 1 - \frac{T_1 + T_4}{T_2 + T_3}$$





(2) 
$$\& = (h_1 - h_4) - (h_b - h_a) = h_1 - h_4 + h_a - h_b$$
  
 $\& = -(h_3 - h_2) = h_2 - h_3$ 

(3) 
$$\chi_{\alpha} = \frac{w}{8_1} = \frac{8_1 - 8_2}{8_1} = \frac{8_2}{8_1} = \frac{1 - \frac{1}{8_2} - \frac{1}{8_3}}{\frac{1}{8_1} - \frac{1}{8_4} + \frac{1}{8_4} - \frac{1}{8_b}}$$

$$f_{12} = f_{12}' + \chi_2 r = f_{13} + \chi_2 r$$

$$\hbar_c = \hbar_c' + \chi_{cr} = \hbar_3 + \chi_{cr}$$

$$8'_1 = h_1 - h_4$$
,  $8'_2 = h_c - h_3$ 

$$N_{b} = \frac{W}{8_{1}} = \frac{9_{1}' - 8_{2}}{9_{1}'} = \frac{9_{2}'}{9_{1}'} = \frac{1}{9_{2}'} = \frac{1}{1} + \frac{1}{1} +$$

れる フれらのとき

$$\frac{f_2-f_3}{f_1-f_4+f_6-f_6} > \frac{f_6-f_3}{f_1-f_4}$$