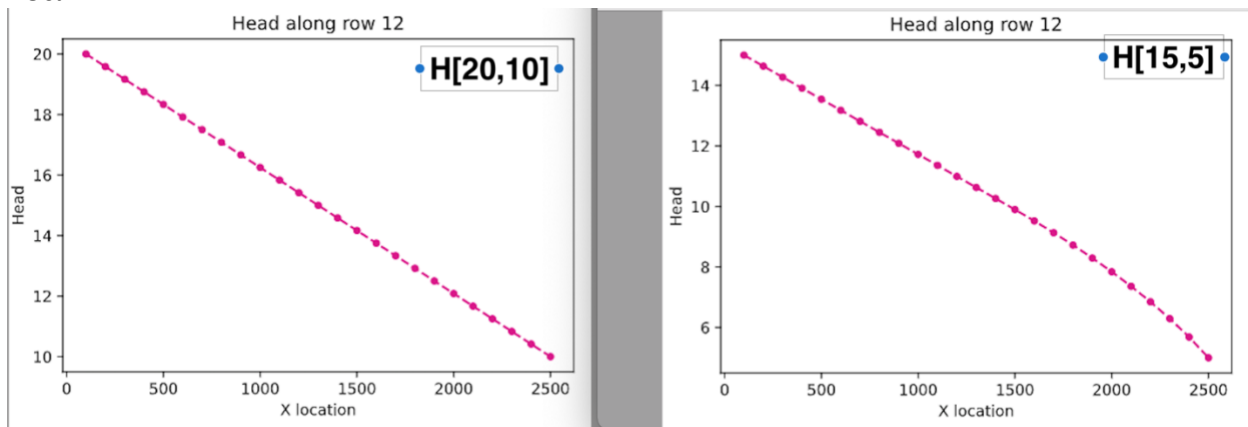


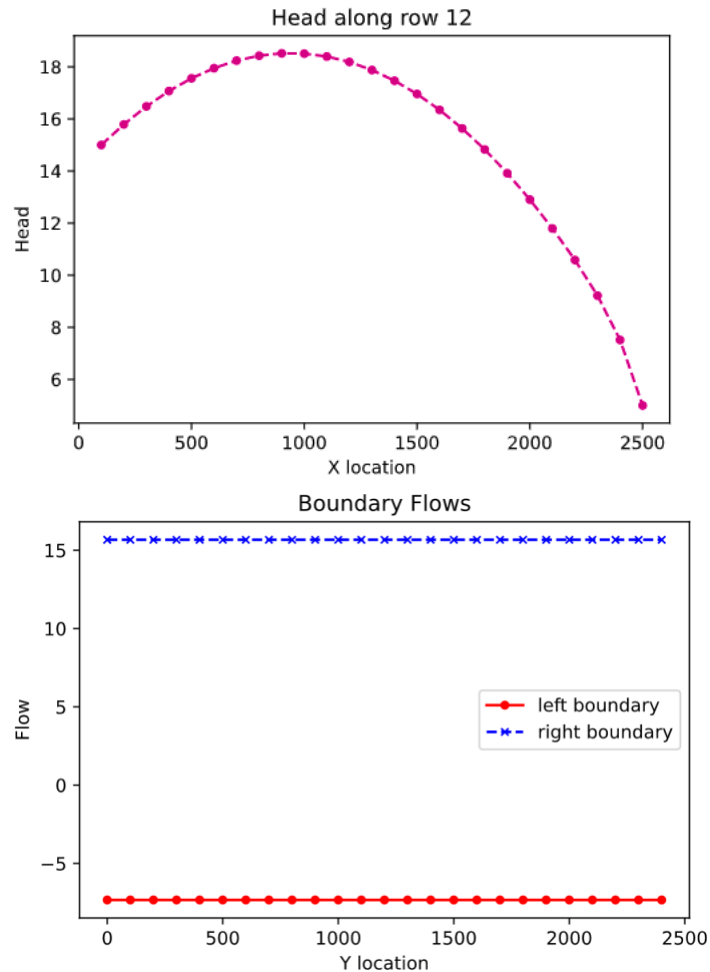
For the initial boundary head values and pumping and recharge rates, compare the head versus x distance - along a transect from the middle of one constant head boundary to the other - to the results for the BoxModel. Now reduce the boundary heads to 15 and 5. Compare this result and explain any observed differences. The overall gradient is the same, as is the K of the medium ... is the flow the same for both boundary conditions? Why or why not?



We can see the difference when changing the head to 15,5 the behavior seems to become nonlinear in the second half of the cross section. This is true because the domain is 10m thick and the head is only 5m at the RHS we have a section of the domain that is unsaturated. It is much harder for water to flow through unsaturated medium than saturated medium you can think of the different like lowering the hydraulic conductivity. For the figure on the right the gradient towards the right half of the domain has to be steeper to account for the same flow. Since K has effectively been reduced by dewatering the domain the head gradient has to steepen in order to let the same flow through the domain.

We can see the non-linear behavior once the head drops below 10m, the ONLY reason for this is that the domain has become dewatered or not fully saturated. This means the cells in MODFLOW have now converted from a confined aquifer to an unconfined aquifer. MODFLOW models this by altering the transmissivity because it takes more energy for water to flow through unsaturated conditions. This unsaturated flow DOES NOT 'really' exist in MODFLOW it just alters the transmissivity to simulate this property. In MODFLOW head is based upon water levels in the cells. If you reduce the water level in the cells you are reducing the water flow area in the cells. MODFLOW tries to solve this by using a circular solution where everything is dependent on everything else and this makes this non-linear solution computationally heavy. The best way to describe non-linearity in a model is the properties of the model depend on the state of the model, but you CANT define the state without knowing the properties and you CANT define the properties without knowing the state. You can see how this could become a problem.

Now add recharge at a constant rate of $1\text{e-}4$ m/day over the entire top boundary. Explain the head transect and boundary flows. Is flow in this system 2D or 3D? Is it represented as 2D or 3D? Explain what you mean by your answers.

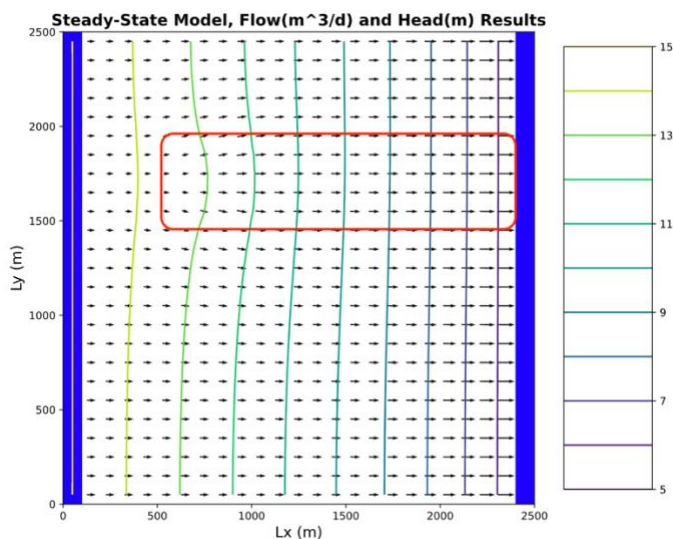


In the head transect we can see some very interesting things when adding uniform recharge over the top boundary. The shape of the head versus x-location looks like it does because the transmissivity of the domain decreases as we move away from the center of the domain. We can see that we created a groundwater divide and actually reversed the gradient of the domain. We made a groundwater mound in the middle of the domain which reversed the direction water flows through part of the domain. We can see that around 1000 m into the domain is the crested or maximum head in the domain. Remember water flows from higher to lower heads. We can see that now if put a molecule just to the right of that groundwater divide it flows to the right boundary but if you put a water molecule to the left of the groundwater divide it flows back to the left boundary. This can also be seen in the boundary flows graph below. The flow through the LHS is a negative value. This does not mean that there is negative flow the negative sign represents the direction of flow. You can also see that we didn't dewater the domain till about 2250 m. The gradient is so steep in the right hand section of the groundwater divide because now our flow out of the domain is greater than our inflow into the domain. The flow in

the system is still represented as 2D because the recharge in our system is a uniform distribution.

There is no vertical flow component in this model even with recharge. We can think of this whole 10m domain and a single cell in the model. MODFLOW models recharge water by just adding it into the cell it doesn't add it from any real direction it just magically sort of appears. Due to MODFLOW considering this a 1 layer model therefore flow can only happen in 2D. When adding the uniform recharge we can see the head change is again non-linear. We can see from about 900-2500m that the gradient becomes more and more as you go closer to the edge. The reason for the non-linearity here is 2 fold whereas in question one there is only 1 explanation. One reason again is because the domain does become dewatered below 10m and it becomes harder to flow water through a unsaturated domain. The second reason is due to what I call compounding. As we go further and further to the right we keep adding more and more flow that needs to "escape" the center of the domain towards the edges. As water compounds the model must move more water to the exits quicker and therefore increases the gradient. This is also related the boundary conditions we have set on the model. On the RHS the BC is constant head. We can think of this constant head like a pump or a lake that is just constantly removing water from our model, if our model was a different boundary than constant head we may see different behavior in our gradient.

Now model a system with zero recharge except for a farm located in [6:10, 6:10] - in python terms. Recharge beneath the farm is $1\text{e-}4$ m/day due to excess irrigation. First, calculate the annual excess irrigation, in meters, that has been applied to the farm. Second, assuming that the crop is cotton, it is located in southern Arizona, and cotton is grown all year (for simplicity), calculate the total irrigation rate on the farm that would be associated with this amount of excess irrigation. Finally, identify the area within the domain that might be subject to contamination if the recharge water was somehow tainted.



Calculate excess irrigation:

Domain = 4 cells x 4 cells = 16 cells x 100 x long x 100 m wide = 160,000 m²
 160,000 m² * 1e-4 m/day * 365 days = 5840 m³/yr
 5840 m³/year / 160,000m²=0.0365m/year

Calculate total irrigation:

Cotton water requirement in southern AZ= 5 ft/ year = 1.5 m/yr / 365 days = 0.0041 m/day

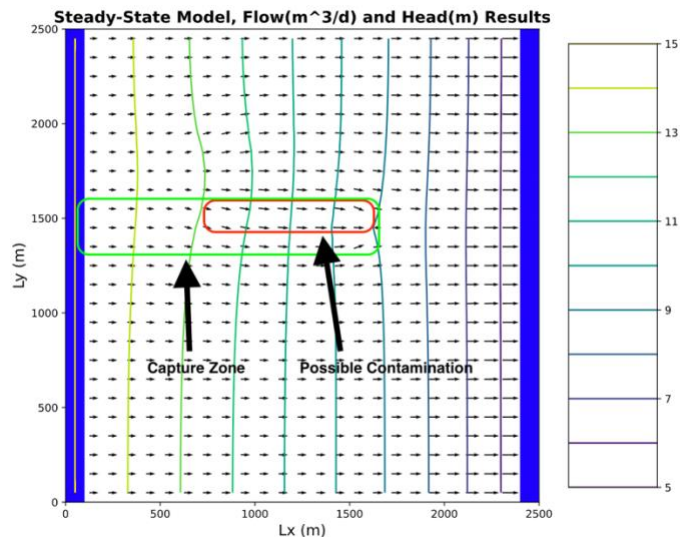
Total irrigation rate on farm: 1e-4 m/day + 0.004 m/day = 0.0041 m/day

0.0041 m/day is what the irrigation rate would have to be for the cotton on the farm to get that excess irrigation rate.

SOURCE:

(<https://www.pimafoodalliance.org/696/#:~:text=Over%20the%20course%20of%20a,water%20for%20cotton%20per%20year.>)

Lastly, start the well pumping at a rate of 8 m³/day. Using one color, identify the capture zone of the well. Using a second color, show the area that might be contaminated by the irrigated farm fields. Comment on the impact of the well on the pattern of potential contamination.



Part of the contamination zone is also included in the well capture zone. This means at a recharge rate of 1e-4 m/day and a pumping rate of 8 m³/day the contamination would travel from the recharge area and be captured in the well. If you were to change the recharge rate or change the pumping rate then this statement may change. Also this is a steady state model where none of the background conditions are changing. If you changed other conditions such as hydraulic conductivity or transmissivity or the recharge was transient and changed over time the contamination may not be part of the well capture zone. Overall there are so many factors

that influence the well capture zone even in this simple model. It is daunting to think about how hard it is to predict contaminant capture in a real life groundwater system.

One of the main things discussed in class was what would the concentration be at the well if the concentration of the made up pollution was 1 that was spilled and recharged into our GW domain. If we look at the green box or capture zone of the well we can see that our source of water that is going into the well is coming from the left boundary. This water is non polluted and has a concentration of 0. As the water travels from that boundary it is “picking u” or mixing with polluted water that has infiltrated above our farm. This is a simple system and we are assuming no dispersion, advection, or diffusion. Since the contaminated water from the recharge area is mixing with clean water inflow from the boundary the concentration of the pollutant at the well must be between 0-1. A mass balance for the well water shows

$$Q(\text{well}) = Q(\text{Left boundary}) + Q(\text{farm})$$

$$Q(\text{Left boundary}) = 6.17 \text{ (flow that comes to the well from the left boundary summed from Python)}$$

$$8 \text{ m/day} = (3.07 + 3.10) + Q(\text{farm})$$

$$Q(\text{farm}) = 1.83 \text{ m/day}$$

$$\text{Concentration Well} = (Q(\text{Left boundary}) * C(\text{left boundary}) + Q(\text{farm}) * C(\text{farm})) / Q_{\text{total}}$$

$$\text{Concentration Well} = ((6.17) * 0 + (1.83) * 1) / 8$$

$$\text{Concentration Well} = 0.23$$

I think the concentration would be 0.23 at the well.