

# Heterogeneity & Effective Properties

- Today
  - Heterogeneity
  - Anisotropy
  - Effective Properties



## Heterogeneity: flow perpendicular to layers

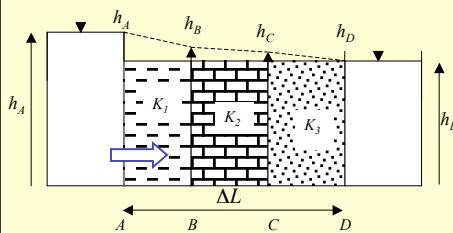
Discharge through each layer [L<sup>3</sup>/T]:

$$Q_1 = -K_1 A \frac{h_B - h_A}{b_1}$$

$$Q_2 = -K_2 A \frac{h_C - h_B}{b_2}$$

$$Q_3 = -K_3 A \frac{h_D - h_C}{b_3}$$

What can we say about the relationship between  $Q_1$ ,  $Q_2$  and  $Q_3$ ?



$$\begin{aligned} b_1 &= B - A, \\ b_2 &= C - B, \\ b_3 &= D - C. \end{aligned}$$

## Heterogeneity: flow perpendicular to layers

Solve for head drops and heads across system

$$Q_1 = -K_1 A \frac{h_B - h_A}{b_1} \quad h_B - h_A =$$

$$Q_2 = -K_2 A \frac{h_C - h_B}{b_2} \quad \longrightarrow \quad h_C - h_B =$$

$$Q_3 = -K_3 A \frac{h_D - h_C}{b_3} \quad h_D - h_C =$$

Layer-head drops all have the same  $Q$ .  
Layer-head drops  $\propto$  layer  $K$ , and  $1/\text{thickness}$

Heads:  $h_B = h_A - \frac{Qb_1}{K_1 A}$

$$h_C = h_B - \frac{Qb_2}{K_2 A} = h_A - \frac{Qb_1}{K_1 A} - \frac{Qb_2}{K_2 A}$$

$$h_D = h_C - \frac{Qb_3}{K_3 A} = h_A - \frac{Qb_1}{K_1 A} - \frac{Qb_2}{K_2 A} - \frac{Qb_3}{K_3 A}$$

To close the system (find the  $h$ 's),  
we need the discharge  $Q$ ; use  
effective property concept.

## Effective Conductivity: flow perpendicular to layers

Total discharge  $[L^3/T]$  written in terms of  $K_{eff}$ :

$$h_D - h_A = \bar{\phantom{x}}$$

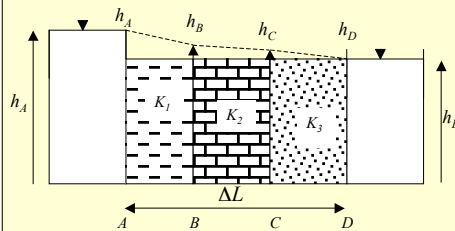
$$h_D - h_A = (h_B - h_A) + (h_C - h_B) + (h_D - h_C)$$

$$h_B - h_A = \frac{-Qb_1}{K_1 A}$$

$$h_C - h_B = \frac{-Qb_2}{K_2 A}$$

$$h_D - h_C = \frac{-Qb_3}{K_3 A}$$

Head drops vary.  
While gradient within a  
layer may be constant,  
it varies from layer to layer,  
depending on layer  
conductivity and thickness.



$$b_1 = B - A,$$

$$b_2 = C - B,$$

$$b_3 = D - C.$$

Area,  $A$ , is the same for all layers

## Effective Conductivity: flow perpendicular to layers

Equate the two terms:  $h_D - h_A = h_D - h_A$

$$\frac{-Q(b_1 + b_2 + b_3)}{K_{eff}A} = \left( \frac{-Qb_1}{K_1A} \right) + \left( \frac{-Qb_2}{K_2A} \right) + \left( \frac{-Qb_3}{K_3A} \right)$$

Eliminate common elements:

$$\frac{(b_1 + b_2 + b_3)}{K_{eff}} = \left( \frac{b_1}{K_1} \right) + \left( \frac{b_2}{K_2} \right) + \left( \frac{b_3}{K_3} \right)$$

Solve for the effective conductivity :  $K_{eff} =$

The “effective conductivity” is the equivalent homogenous  $K$  that results in the same discharge. It’s the result of “upscaling” or “spatial averaging” over the heterogeneities.  
In general, for flow perpendicular to layers:

## Heterogeneity: flow perpendicular to layers

Heads from:

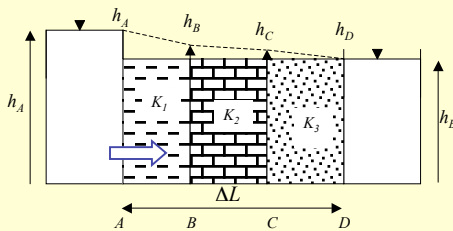
$$K_{eff} = \frac{b_1 + b_2 + b_3}{\left( \frac{b_1}{K_1} \right) + \left( \frac{b_2}{K_2} \right) + \left( \frac{b_3}{K_3} \right)} \longrightarrow Q = -K_{eff}A \frac{h_D - h_A}{b_1 + b_2 + b_3}$$

$$\downarrow$$

$$h_B = h_A - \frac{Qb_1}{K_1A}$$

$$h_C = h_B - \frac{Qb_2}{K_2A} = h_A - \frac{Qb_1}{K_1A} - \frac{Qb_2}{K_2A}$$

$$h_D = h_C - \frac{Qb_3}{K_3A} = h_A - \frac{Qb_1}{K_1A} - \frac{Qb_2}{K_2A} - \frac{Qb_3}{K_3A}$$



Then linearly interpolate heads between A, B, C, and D to get  $h(x)$ .

# Heterogeneity: flow perpendicular to layers

What is the rate of specific discharge and seepage velocity in each layer?  
How long would it take a non-reactive tracer to move from A to B across all layers?

Discharge in layer  $i$  [ $L^3/T$ ]:

$$Q_i = Q = -K_{eff} A \frac{h_D - h_A}{b_1 + b_2 + b_3}$$

where  $i=1,2,3$ :

Specific discharge in layer  $i$  [ $L/T$ ]:

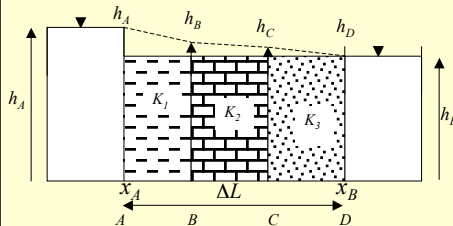
$$q_i = \frac{Q_i}{A} = \frac{Q}{A} = q =$$

Seepage velocity in layer  $i$  [ $L/T$ ]:

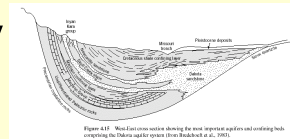
$$v_i =$$

Travel time A to B [T]:

$$t = \int_{x_A}^{x_B} \frac{1}{v_i} dx =$$



## Effective Conductivity for layered systems



- The “effective conductivity” is the equivalent homogenous  $K$  that results in the same discharge.
- It’s the result of “upscaling” or “spatial averaging” over the heterogeneities.

- In general,

– for flow parallel to layers:

- Use the
- which is weighted towards

$$K_{eff} = K_A = \frac{\sum K b}{\sum b}$$

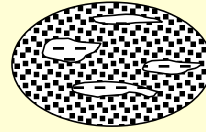
– for flow perpendicular to layers:

- use a
- which is weighted towards the

$$K_{eff} = K_H = \frac{\sum b}{\sum \frac{b}{K}}$$

# Effective Conductivity for more complex heterogeneities

When averaging over any spatial arrangement of discrete K values, the upscaling or averaging result depends on orientation of the arrangement relative to the direction of the hydraulic head gradient:



- Arithmetic mean: highest effective value  $K_{eff} = K_A = \frac{\sum K_i V_i}{\sum V_i}$
- Harmonic mean: lowest effective value  $K_{eff} = K_H = \frac{\sum V_i}{\sum \frac{V_i}{K_i}}$
- Geometric mean: yields an intermediate effective value between arithmetic and harmonic means,  $\ln K_{eff} = \ln K_G =$

$$K_H \leq$$

$V_i$  = volume of  $i$ th volume fraction

Averaging or upscaling  
heterogeneity leads to (upscaled) anisotropy



# Snell's Law

- Flow lines refract when crossing an abrupt boundary between two homogeneous units:

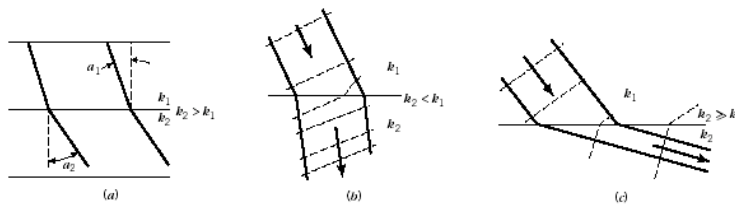
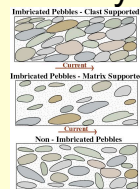


Figure 3.11 Diagrams of flow line refraction and conditions at the boundaries between materials of differing permeability (from Domenico and Schwartz, 1998, *Physical and chemical hydrogeology*). Copyright © 1998 by John Wiley & Sons, Inc. Reprinted by permission of John Wiley & Sons, Inc.

SZ2005

# Anisotropy

- Typical causes of anisotropy in natural systems?
  - Imbricated grains
    - Upscaling at the grain, or Darcy scale

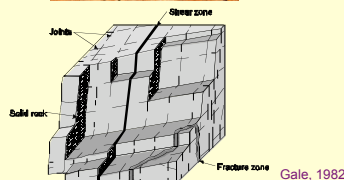


U of Montana, 2005

- Bedding in sedimentary systems
  - Upscaling over the beds

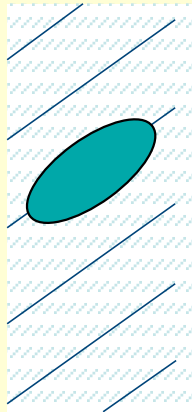


- Fracture networks
  - With preferred orientation and connectivity of fractures
  - Upscaling over the network



Gale, 1982

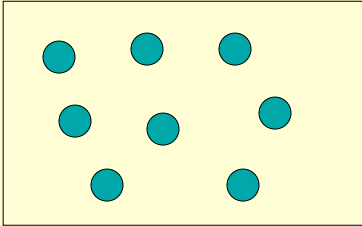
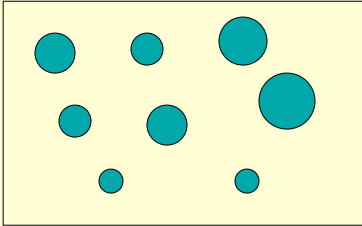

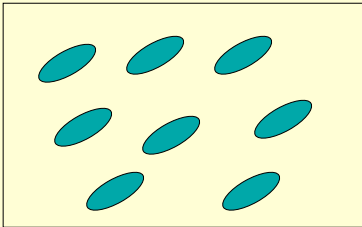
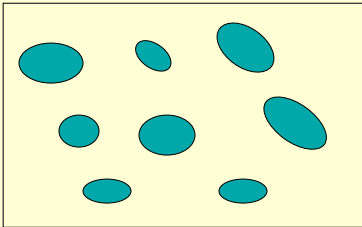

# Anisotropy

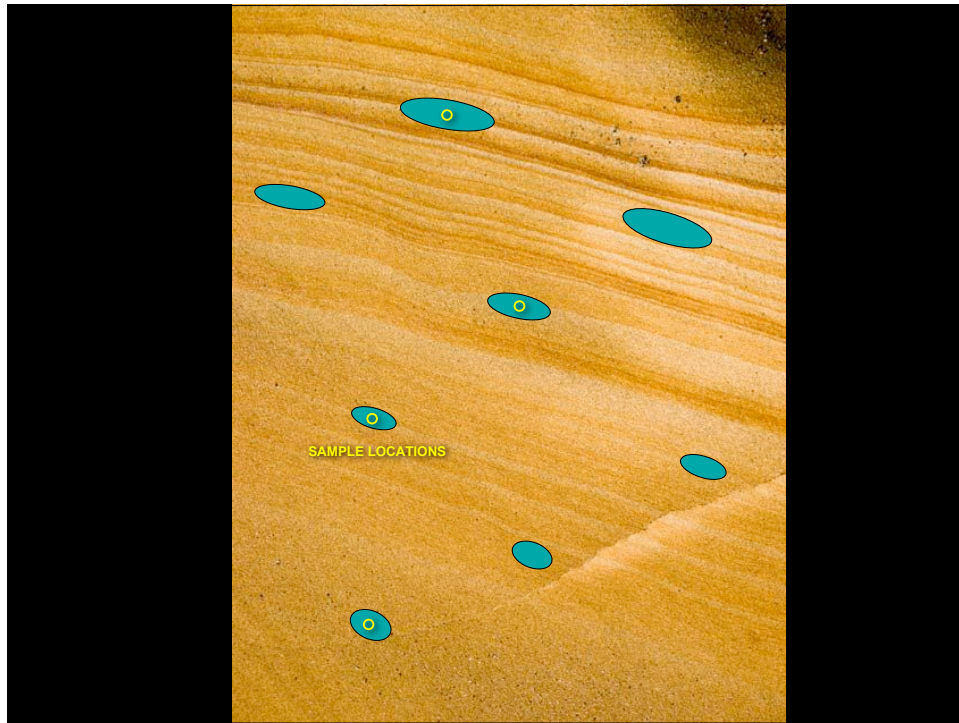


The variation of  $K$  with direction forms an ellipse. In 3-D it forms an ellipsoid.

The **principal axes** of the ellipsoid point in the directions of greatest and least resistance.

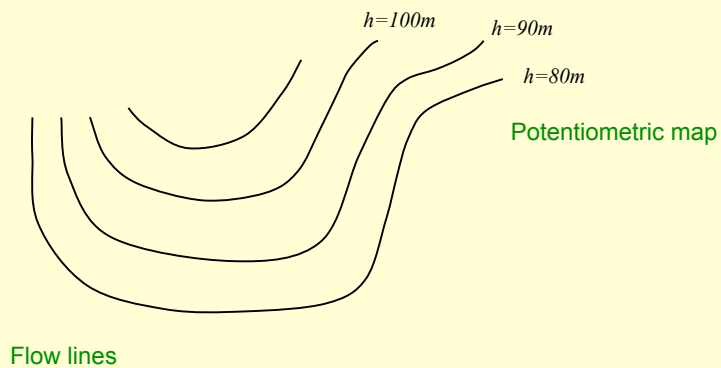
## Properties as functions of location and direction

	HOMOGENEOUS	HETEROGENEOUS	
ISOTROPIC			Property <u>constant</u> with <u>direction</u> 
			Property <u>changes</u> with <u>direction</u> 
	Property <u>constant</u> with <u>location</u>	Property <u>changes</u> with <u>location</u>	



## Later we'll see that ...

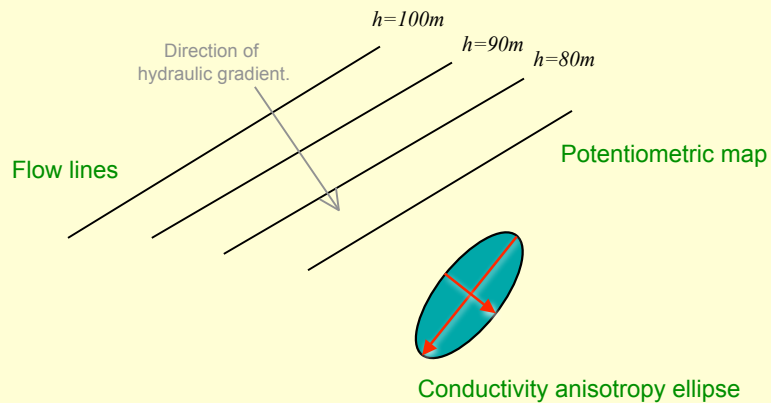
Water always seeks the most efficient way to move, so in an isotropic, homogenous medium it will always flow parallel to the hydraulic gradient, i.e., perpendicular to the potentiometric contours.





## However ...

In an anisotropic medium flow is at an angle to the potentiometric contours, an angle that depends on the amount of anisotropy.



## Anisotropy and Effective Conductivity

Because of its directional dependence Hydraulic Conductivity is a tensor quantity:

$$\begin{bmatrix} K_{xx} & K_{xy} & K_{xz} \\ K_{yx} & K_{yy} & K_{yz} \\ K_{zx} & K_{zy} & K_{zz} \end{bmatrix}$$

The tensor is symmetric, with off diagonals:

$$K_{yx} = K_{xy}, \quad K_{zx} = K_{xz}, \quad K_{zy} = K_{yz}.$$

The tensor is like a matrix.

What does each entry in the tensor represent?

$$\begin{bmatrix} K_{xx} & K_{xy} & K_{xz} \\ K_{yx} & K_{yy} & K_{yz} \\ K_{zx} & K_{zy} & K_{zz} \end{bmatrix}$$

$K_{xx}$  = specific discharge in the  $x$  direction due to a unit hydraulic gradient in the  $x$  direction

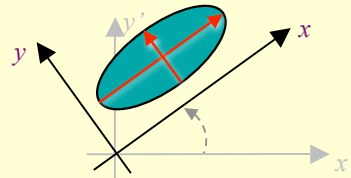
$K_{xy}$  = specific discharge in the  $y$  direction due to a unit hydraulic gradient in the  $x$  direction

# Anisotropy and Effective Conductivity

If your coordinate system is selected to lie in the principal directions of anisotropy, the tensor is diagonal

The off diagonals are:

$$\begin{bmatrix} K_{xx} & & \\ & K_{yy} & \\ & & K_{zz} \end{bmatrix}$$

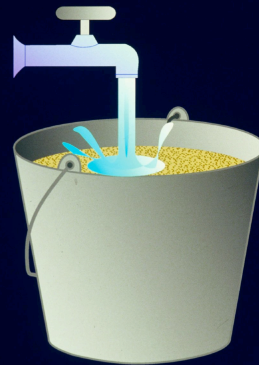


Simply rotate coordinate system to align with principal directions.  
Only works if principal directions are homogeneous  
(don't change with position).

## Storage

- Today
  - Aquifer Storage
  - Storativity
  - Specific Yield

Only two quarts of water in a  
2-gallon bucket full of sand?  
How about only 1/40<sup>th</sup> of an ounce!



# Groundwater Balance

## Change in storage

$$= \text{Recharge} - \text{Pumping} - \text{GW Discharge}$$

$$- ET_{GW} \pm \text{Underflow} = \text{Forcings}$$

### Hydraulic Conductivity:

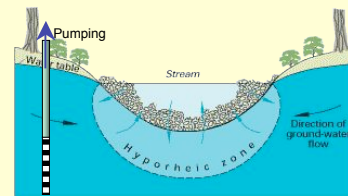
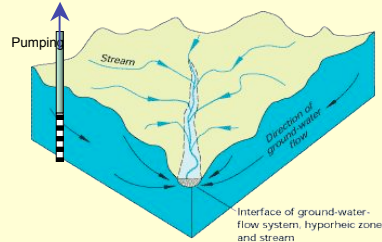
- influences each of the RHS forcings, or how the system responds to these forcings.

Conductivity doesn't influence the LHS term, involving the rate of change of storage.

### Storage Parameters:

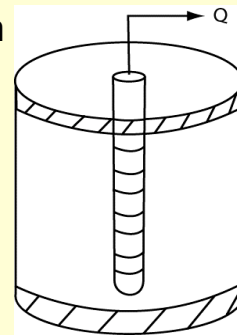
- Control the LHS, rate of change of storage
- Two types of storage, due to:

- Parameters, respectively



# Aquifer Storage

- Consider a pumping well located in an infinite confined aquifer.
  - aquifer is bounded above and below by aquicludes
  - well is fully penetrating
  - well is pumping at a constant volumetric-flow rate,  $Q$



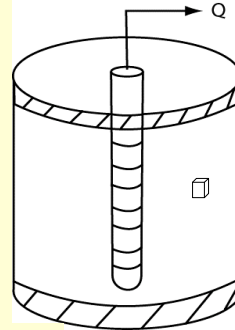
- Where does the water come from?

$$\text{Pumping} = - \text{Change in storage} + \text{Recharge} - \text{GW Discharge}$$

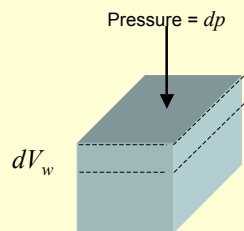
$$- ET_{GW} \pm \text{Underflow}$$

# Aquifer Storage

- Where does the water come from?
  - Head drops as well is pumped.
  - Elevation is not changing, so then
  - pressure must be changing.
  - As pressure is released
    - water comes out of storage.
  - How?

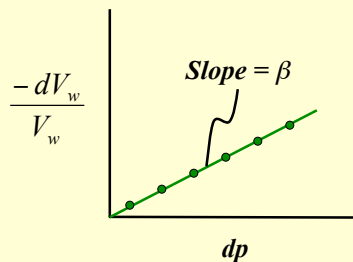


# Water Compressibility



Control volume of pure water,  
volume =  $V_w$

In response to the increase in pressure  $dp$ ,  
the volume of water decreases (compresses)  
by the amount  $dV_w$



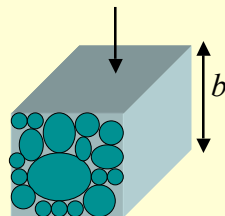
# Water Compressibility

$$\beta = \frac{1}{V_w} \frac{-dV_w}{dp}$$

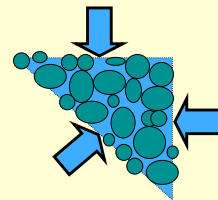
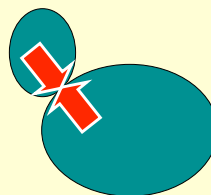
- Dividing by  $V_w$  normalizes the data  
if we only had  $-dV_w$  on the y axis, compressing different volumes of water would yield different slopes
- This is for a cube of pure water, where  $V_w = V_{total} = V_t$
- What happens in an aquifer?

# Matrix Compressibility

Overburden Stress =  $\sigma$



Control volume of aquifer



Total stress  $\sigma$  is balance by:

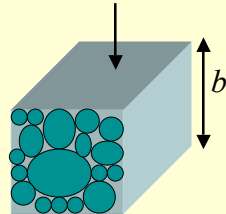
-the transmitted through the matrix  
(e.g., due to grain-to-grain contacts),

and by

-the

## Matrix Compressibility

Overburden Stress =  $\sigma$



Control volume of aquifer

Total stress  $\sigma$  is balance by:

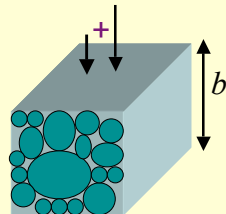
-the **effective stress**  $\sigma_e$  transmitted through the matrix  
(e.g., due to grain-to-grain contacts),

and by

-the **water pressure**,  $p$ , transmitted through the pore space

## Matrix Compressibility

Add to overburden stress by amount  $d\sigma$



Control volume of aquifer

If the total stress  $\sigma$  increases by  $d\sigma$ , say due to a new building



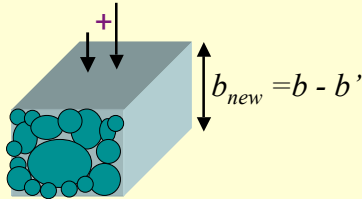
-- initially the **water pressure**,  $p$ , increases

-- if the water is allowed to drain off, the stress is slowly  
transmitted to the matrix, and effective stress  $\sigma_e$  increases

# Matrix Compressibility

*What happens after the water drains off and  $dp = 0$  ...*

Add to overburden stress by amount  $d\sigma$



Control volume of aquifer

If the total stress  $\sigma$  increases by  $d\sigma$ , say due to a new building

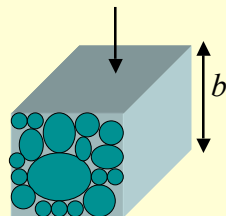


-- initially the water pressure,  $p$ , increases

-- if the water is allowed to drain off, the stress is slowly transmitted to the matrix, and effective stress  $\sigma_e$  increases

# Matrix Compressibility

Overburden Stress =  $\sigma$



$$\sigma = \sigma_e + p$$

Control volume of aquifer

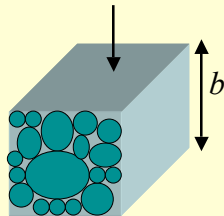
In groundwater hydrology we usually assume that the overburden or total stress  $\sigma$  is fixed:  $d\sigma = 0$ .

Instead we are concerned with what happens to effective stress and thickness  $b$  when the water pressure,  $p$ , changes -due to pumping or injection or ...

# Matrix Compressibility

*In groundwater hydrology  $d\sigma = 0$  ...*

Overburden Stress  $\sigma$



Control volume of aquifer

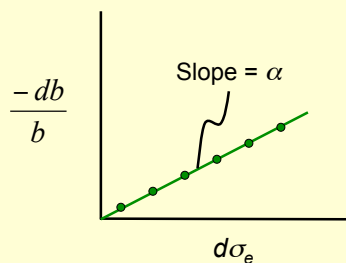
In groundwater hydrology we usually assume that the overburden or total stress  $\sigma$  is fixed:  $d\sigma = 0$ .

Instead we are concerned with what happens to effective stress and thickness  $b$  when the water pressure,  $p$ , changes -due to pumping or injection or ...

# Matrix Compressibility

Suppose effective stress increases  
-due to increase in total stress or  
-decrease of pressure,  
then the control volume will compress.

Measure that compression as a function of effective stress, normalize, and plot. The slope is the matrix compressibility:





## Matrix Compressibility

$$\alpha = \frac{-db}{b} \frac{1}{d\sigma_e} =$$

$$\alpha = -\frac{1}{V_t} \frac{dV_t}{d\sigma_e} \longrightarrow$$

We usually consider the rock material (eg, grains) incompressible, so changes in the volume of voids (& therefore volume of water) must account for changes in the volume of the aquifer control volume.

Relates change in water volume, due to matrix compressibility, to change in aquifer effective stress.

## Matrix Compressibility

Recall that in hydrology applications,  $d\sigma \cong 0$ :

$$d\sigma_e =$$

$$dV_w =$$

Relates change in water volume, due to matrix compressibility, to change in aquifer water pressure.

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The matrix model is due to Karl Terzaghi (1883-1963). It's a principal model of geotechnical engineering and groundwater hydrology. The major assumption is that compression is vertical (no horizontal movement). Secondary assumptions include no compression of grains. Also, to account for irreversible consolidation you need to augment the model or use a more sophisticated model (e.g., Biot's theory). Ralph Peck, one of Terzaghi's main disciples and famous in his own right, is almost 90 and lives in Albuquerque. He still travels the world as a geotechnical consultant.