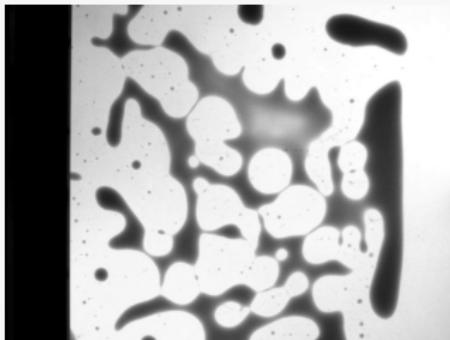


Phase change & Marangoni flows



Quentin **Magdelaine**

SVI – Saint-Gobain Research Paris, CNRS

Jean-Le-Rond d'Alembert Institute – Sorbonne Université, CNRS

Alban **Sauret**, Frédéric **Mondiot**

Jérémie **Teisseire**, Arnaud **Antkowiak**

I added a **slide (14)** with links toward **my sandbox**.

Introduction ► Wet coating

Applications



glass plates



glass fabrics

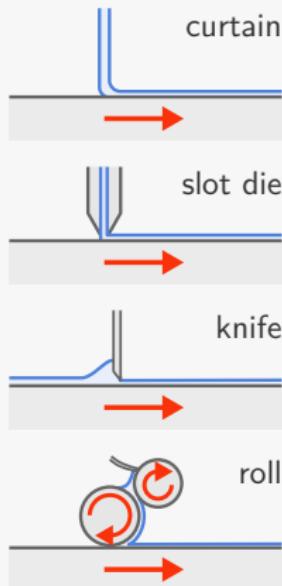


flexible substrates



wavy substrates
Planilaque

Deposition



Drying of liquid films

► relaxation or destabilization?



Polymer-based
protective coating

- $h \sim 2 - 10 \mu\text{m}$
- roughness: 150 nm

Paints, protective and functionalized layers:

defects limit the applications

► what do they have in common? ► **binary mixture**

Introduction ► Model experiments

Model system: water – propylene glycol



0 %
50 μm

x 6, 20 cm

Introduction ► Model experiments

Model system: water – propylene glycol



0 %
50 μm



87 %
50 μm

x 6, 20 cm

Introduction ► Model experiments

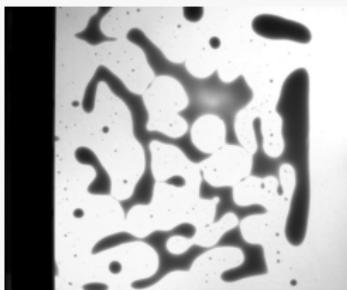
Model system: water – propylene glycol



0 %
50 µm



87 %
50 µm



50 %
50 µm

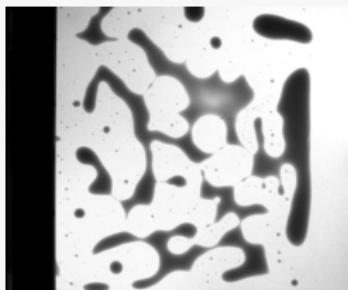
x 6, 20 cm

Introduction ► Model experiments

Model system: water – propylene glycol



0 %
50 µm



50 %
50 µm

x 6, 20 cm



87 %
50 µm

Model system

- **key ingredients:**
evaporation &
Marangoni stress
- set of **equations**

Introduction ► Equations

$$\rho_v \frac{d\mathbf{v}}{dt} + \rho_v \mathbf{v} \cdot \nabla \cdot \mathbf{v} = \rho_v \mathbf{g} + \eta_v \Delta \mathbf{v}$$

$$\frac{d\sigma_v}{dt} + \nabla \cdot (\sigma_v \mathbf{v}) = \nabla \cdot (D_v \nabla \sigma_v)$$

Introduction ► Equations

$$\rho_V \frac{d\mathbf{v}}{dt} + \rho_V \mathbf{v} \cdot \nabla \cdot \mathbf{v} = \rho_V \mathbf{g} + \eta_V \Delta \mathbf{v}$$

$$\frac{dc_V}{dt} + \nabla \cdot (c_V \mathbf{v}) = \nabla \cdot (D_V \nabla c_V)$$

$$\rho_L \frac{d\mathbf{v}}{dt} + \rho_L \mathbf{v} \cdot \nabla \cdot \mathbf{v} = \rho_L \mathbf{g} + \eta_L \Delta \mathbf{v}$$

$$\frac{dc_{L_1}}{dt} + \nabla \cdot (c_{L_1} \mathbf{v}) = \nabla \cdot (D_{L_1} \nabla c_{L_1})$$

$$\frac{dc_{L_2}}{dt} + \nabla \cdot (c_{L_2} \mathbf{v}) = \nabla \cdot (D_{L_2} \nabla c_{L_2})$$

Introduction ► Equations

$$\rho_V \frac{d\mathbf{v}}{dt} + \rho_V \mathbf{v} \cdot \nabla \cdot \mathbf{v} = \rho_V \mathbf{g} + \eta_V \Delta \mathbf{v}$$

$$1. \ c_V = c_s(c_{L_1})$$

$$\frac{dc_V}{dt} + \nabla \cdot (c_V \mathbf{v}) = \nabla \cdot (D_V \nabla c_V)$$



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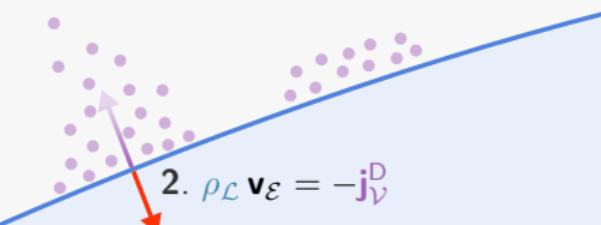
$$\frac{dc_{L_2}}{dt} + \nabla \cdot (c_{L_2} \mathbf{v}) = \nabla \cdot (D_{L_2} \nabla c_{L_2})$$

Introduction ► Equations

$$\rho_V \frac{dv}{dt} + \rho_V v \cdot \nabla \cdot v = \rho_V g + \eta_V \Delta v$$

$$\frac{dc_V}{dt} + \nabla \cdot (c_V v) = \nabla \cdot (D_V \nabla c_V)$$

$$1. c_V = c_s(c_{L_1})$$


$$2. \rho_L v_E = -j_V^D$$

$$\rho_L \frac{dv}{dt} + \rho_L v \cdot \nabla \cdot v = \rho_L g + \eta_L \Delta v$$

$$\frac{dc_{L_1}}{dt} + \nabla \cdot (c_{L_1} v) = \nabla \cdot (D_{L_1} \nabla c_{L_1})$$

$$\frac{dc_{L_2}}{dt} + \nabla \cdot (c_{L_2} v) = \nabla \cdot (D_{L_2} \nabla c_{L_2})$$

Introduction ► Equations

$$\rho_V \frac{dv}{dt} + \rho_V v \cdot \nabla \cdot v = \rho_V g + \eta_V \Delta v$$

$$\frac{dc_V}{dt} + \nabla \cdot (c_V v) = \nabla \cdot (D_V \nabla c_V)$$

$$1. c_V = c_s(c_{L_1})$$

$$3. j_{L_2}^D = 0$$

$$2. \rho_L v_E = -j_V^D$$

$$\rho_L \frac{dv}{dt} + \rho_L v \cdot \nabla \cdot v = \rho_L g + \eta_L \Delta v$$

$$\frac{dc_{L_1}}{dt} + \nabla \cdot (c_{L_1} v) = \nabla \cdot (D_{L_1} \nabla c_{L_1})$$

$$\frac{dc_{L_2}}{dt} + \nabla \cdot (c_{L_2} v) = \nabla \cdot (D_{L_2} \nabla c_{L_2})$$

Introduction ► Equations

$$\rho_V \frac{dv}{dt} + \rho_V v \cdot \nabla \cdot v = \rho_V g + \eta_V \Delta v$$

$$\frac{dc_V}{dt} + \nabla \cdot (c_V v) = \nabla \cdot (D_V \nabla c_V)$$

$$1. c_V = c_s(c_{L_1})$$

$$3. j_{L_2}^D = 0$$

$$2. \rho_L v_\varepsilon = -j_V^D$$

$$4. j_{L_2}^c = c_{L_2} v_\varepsilon$$

$$\rho_L \frac{dv}{dt} + \rho_L v \cdot \nabla \cdot v = \rho_L g + \eta_L \Delta v$$

$$\frac{dc_{L_1}}{dt} + \nabla \cdot (c_{L_1} v) = \nabla \cdot (D_{L_1} \nabla c_{L_1})$$

$$\frac{dc_{L_2}}{dt} + \nabla \cdot (c_{L_2} v) = \nabla \cdot (D_{L_2} \nabla c_{L_2})$$

Introduction ► Equations

$$\rho_V \frac{dv}{dt} + \rho_V v \cdot \nabla \cdot v = \rho_V g + \eta_V \Delta v$$

$$\frac{dc_V}{dt} + \nabla \cdot (c_V v) = \nabla \cdot (D_V \nabla c_V)$$

$$f_s = \gamma \kappa n + \nabla s \gamma$$



$$1. c_V = c_s (c_{\mathcal{L}_1})$$

$$3. j_{\mathcal{L}_2}^D = 0$$

$$2. \rho_{\mathcal{L}} v_{\mathcal{E}} = -j_V^D$$

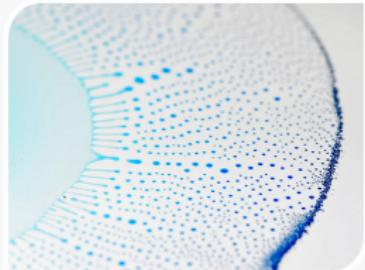
$$\rho_{\mathcal{L}} \frac{dv}{dt} + \rho_{\mathcal{L}} v \cdot \nabla \cdot v = \rho_{\mathcal{L}} g + \eta_{\mathcal{L}} \Delta v$$

$$\frac{dc_{\mathcal{L}_1}}{dt} + \nabla \cdot (c_{\mathcal{L}_1} v) = \nabla \cdot (D_{\mathcal{L}_1} \nabla c_{\mathcal{L}_1})$$

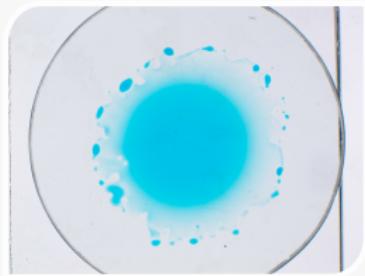
$$\frac{dc_{\mathcal{L}_2}}{dt} + \nabla \cdot (c_{\mathcal{L}_2} v) = \nabla \cdot (D_{\mathcal{L}_2} \nabla c_{\mathcal{L}_2})$$

Outline

Implementations in Basilisk



Instabilities in thin films



1. Saturation of the vapor: $c_v = c_s$

- **immersed Dirichlet** boundary condition
- **setpoint** in the diffusion equation

$$d_t c_v = \nabla \cdot (c_v \nabla c_v) + \frac{c_s - c_v}{\tau}$$

Implementations ► Evaporation of pure liquid

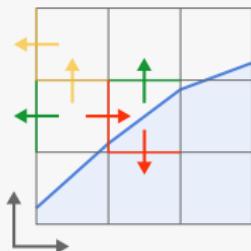
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2. Evaporation velocity

$$\rho_L \mathbf{v}_E = -\mathbf{j}_v^D = D_v \nabla c_v$$



Implementations ► Evaporation of pure liquid

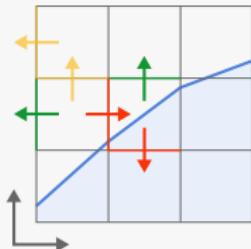
1. Saturation of the vapor: $c_v = c_s$

- **immersed Dirichlet** boundary condition
- **setpoint** in the diffusion equation

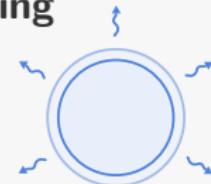
$$d_t c_v = \nabla \cdot (c_v \nabla c_v) + \frac{c_s - c_v}{\tau}$$

2. Evaporation velocity

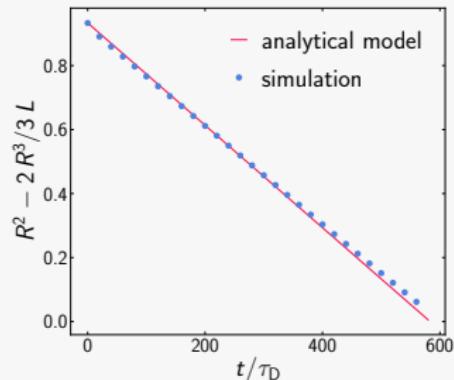
$$\rho_L \mathbf{v}_E = -\mathbf{j}_v^D = D_v \nabla c_v$$



Evaporating drop



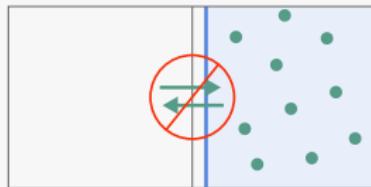
drop radius
in function of time



I. Langmuir, Phys. rev., 1918

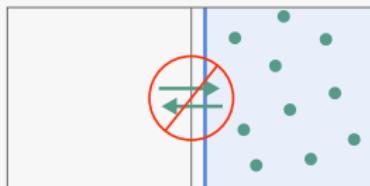
3. No flux condition at the interface:

$$\mathbf{j}_{\mathcal{L}_2}^D = D_{\mathcal{L}} \nabla c_{\mathcal{L}_2} = \mathbf{0}$$



3. No flux condition at the interface:

$$\mathbf{j}_{\mathcal{L}_2}^D = D_{\mathcal{L}} \nabla c_{\mathcal{L}_2} = \mathbf{0}$$



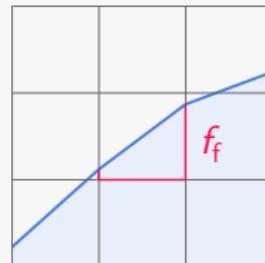
Diffusion equation

$$d_t c_{\mathcal{L}_2} = \nabla \cdot (D_{\mathcal{L}} \nabla c_{\mathcal{L}_2})$$

$$\text{& } \bar{c}_{\mathcal{L}_2} = \frac{1}{\Delta^2} \iint c_{\mathcal{L}_2} dS$$

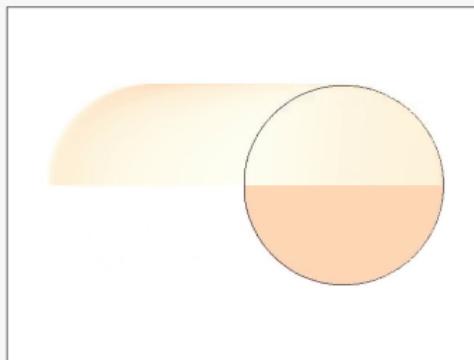
$$f d_t \bar{c}_{\mathcal{L}_2} = \nabla \cdot (f_f D_{\mathcal{L}} \nabla \bar{c}_{\mathcal{L}_2})$$

► **face value f_f**
of the liquid tracer f



3. No flux condition at the interface:

$$\mathbf{j}_{\mathcal{L}_2}^D = D_{\mathcal{L}} \nabla c_{\mathcal{L}_2} = \mathbf{0}$$



naive way: $f_f = (f_n + f_{n-1}) / 2$
 nice way: VOF reconstruction
 Thank Jose-Maria López Herrera

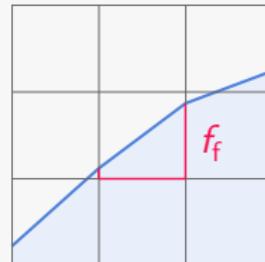
Diffusion equation

$$d_t c_{\mathcal{L}_2} = \nabla \cdot (D_{\mathcal{L}} \nabla c_{\mathcal{L}_2})$$

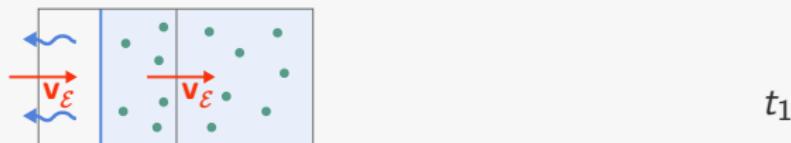
& $\bar{c}_{\mathcal{L}_2} = \frac{1}{\Delta^2} \iint c_{\mathcal{L}_2} dS$

$$f d_t \bar{c}_{\mathcal{L}_2} = \nabla \cdot (f_f D_{\mathcal{L}} \nabla \bar{c}_{\mathcal{L}_2})$$

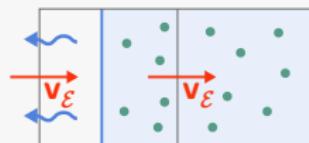
► **face value f_f**
 of the liquid tracer f



4. Tracer advection: the **net** allegory



4. Tracer advection: the **net** allegory



t_1

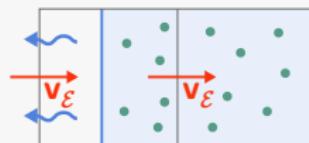
Advectiong c_{L_2} along
with f with v_E .



t_2

We concentrate the
solute in the **next**
cell. v_E is **not** a flow.

4. Tracer advection: the **net** allegory

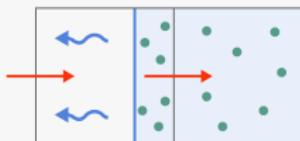


t_1

Advectiong c_{L_2} along
with f with v_E .



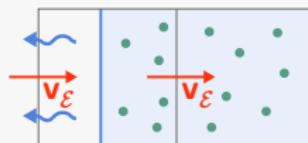
The interface is more
acting as a **net**.



t_2

We concentrate the
solute in the **next**
cell. v_E is **not** a flow.

4. Tracer advection: the **net** allegory



t_1

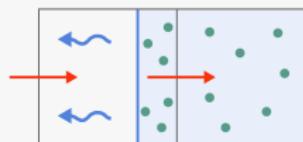
Advectioning c_{L_2} along with f with v_E .



t_2

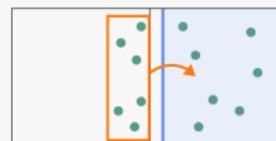
We concentrate the solute in the **next** cell. v_E is **not** a flow.

The interface is more acting as a **net**.



t_3

Redistribution of the solute of the **dry** cells.



t_3

Implementations ► Evaporation of mixtures

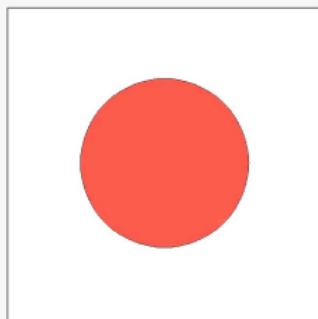
Raoult law

$$c_V = c_s (c_{\mathcal{L}_1}) = c_s \frac{c_{\mathcal{L}_1}}{\rho_{\mathcal{L}}}$$

Raoult law

$$c_V = c_s (c_{L_1}) = c_s \frac{c_{L_1}}{\rho_L}$$

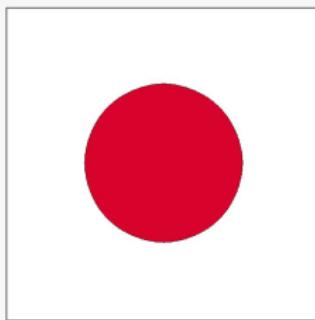
Fast diffusion



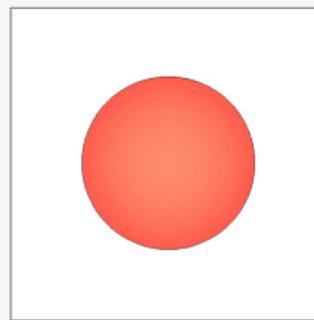
Raoult law

$$c_v = c_s (c_{L_1}) = c_s \frac{c_{L_1}}{\rho_L}$$

Fast diffusion



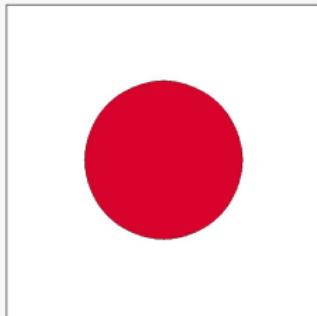
Moderate



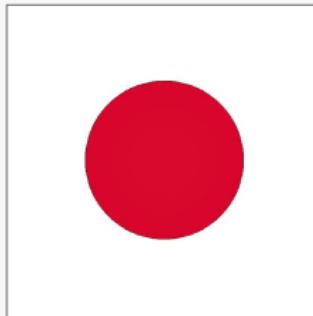
Raoult law

$$c_V = c_s (c_{L_1}) = c_s \frac{c_{L_1}}{\rho_L}$$

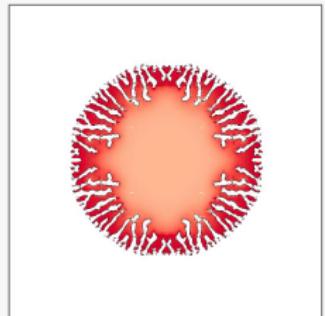
Fast diffusion



Moderate



Slow



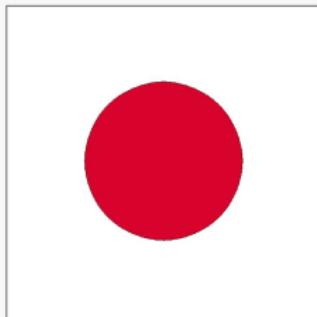
no surface tension

Implementations ► Evaporation of mixtures

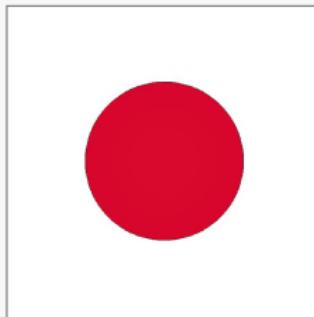
Raoult law

$$c_V = c_s (c_{L_1}) = c_s \frac{c_{L_1}}{\rho_L}$$

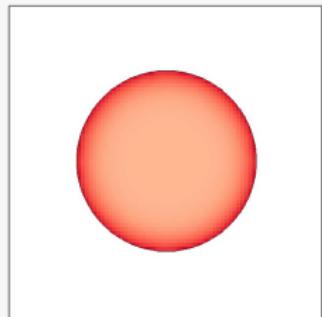
Fast diffusion



Moderate



Slow



surface tension

Implementations ► Evaporation of mixtures

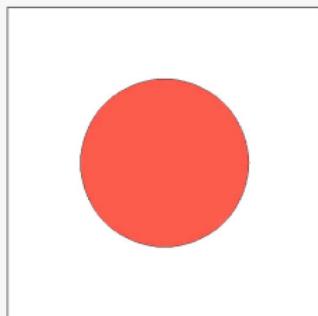
Raoult law

$$c_v = c_s (c_{\mathcal{L}_1}) = c_s \frac{c_{\mathcal{L}_1}}{\rho_{\mathcal{L}}}$$

Péclet number

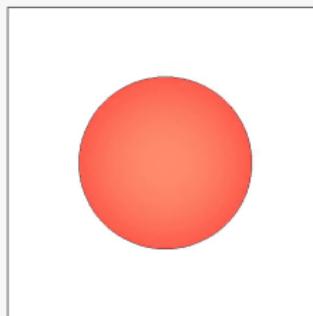
$$Pe_{\mathcal{E}} = \frac{v_{\mathcal{E}} R}{D_{\mathcal{L}}}$$

Fast diffusion



$$Pe_{\mathcal{E}} = 10^{-3}$$

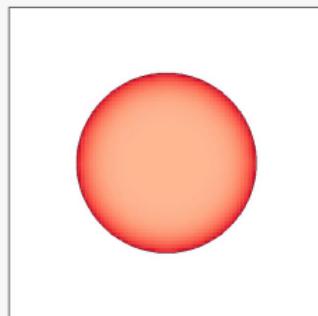
Moderate



$$Pe_{\mathcal{E}} = 2$$

water – ethanol

Slow



$$Pe_{\mathcal{E}} = 10^2$$

paint

Capillary force

$$d\mathbf{F}_\ell = (\gamma \mathbf{t})(s) - (\gamma \mathbf{t})(s + ds)$$

$$\mathbf{f}_S = ds(\gamma \mathbf{t})$$

$$\mathbf{f}_S = \gamma \kappa \mathbf{n} + d_s \gamma \mathbf{t}$$

generalized in 3D:

$$\mathbf{f}_S = \gamma \kappa \mathbf{n} + \nabla_S \gamma$$



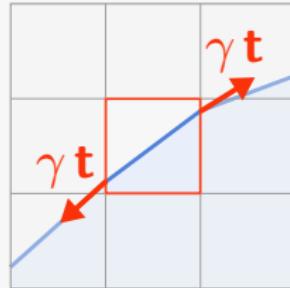
Laplace pressure
Marangoni stress

Implementations ► Marangoni stress

Capillary force, two formulations

$$\mathbf{F}_\ell = (\gamma \mathbf{t})(s) - (\gamma \mathbf{t})(s + \Delta s)$$

$$\mathbf{f}_S = \gamma \kappa \mathbf{n} + \nabla_S \gamma$$



Brackbill formulation

Brackbill, Kothe, Zemach, 1992

Seric, Afkhami, Kondic, 2017

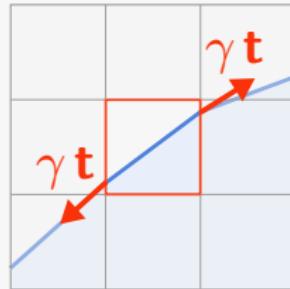
- δ_S is added to make it volumetric
- not easy to evaluate the surface gradient ∇_S

Implementations ► Marangoni stress

Capillary force, two formulations

$$\mathbf{F}_\ell = (\gamma \mathbf{t})(s) - (\gamma \mathbf{t})(s + \Delta s)$$

$$\mathbf{f}_S = \gamma \kappa \mathbf{n} + \nabla_S \gamma$$



Brackbill formulation

Brackbill, Kothe, Zemach, 1992

Seric, Afkhami, Kondic, 2017

- δ_S is added to make it volumetric
- not easy to evaluate the surface gradient ∇_S

Integral formulation

Abu-Al-Saul, Popinet and Tchelepi, 2018

- already **discrete**
- **well-balanced** and **momentum conservative**

Instabilities ► Simulations & lubrication

Evaporation of a liquid mixture layer with Marangoni stress

Instabilities ► Simulations & lubrication

Evaporation of a liquid mixture layer with Marangoni stress



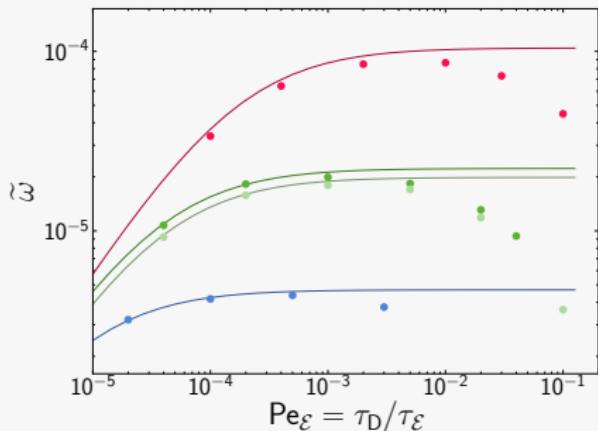
horizontal velocity

Evaporation of a liquid mixture layer with Marangoni stress



horizontal velocity

Growth rate ω in function of $\text{Pe}_{\mathcal{E}} = \tau_D/\tau_{\mathcal{E}}$



high $v_{\mathcal{E}}$
moderate $v_{\mathcal{E}}$
low $v_{\mathcal{E}}$

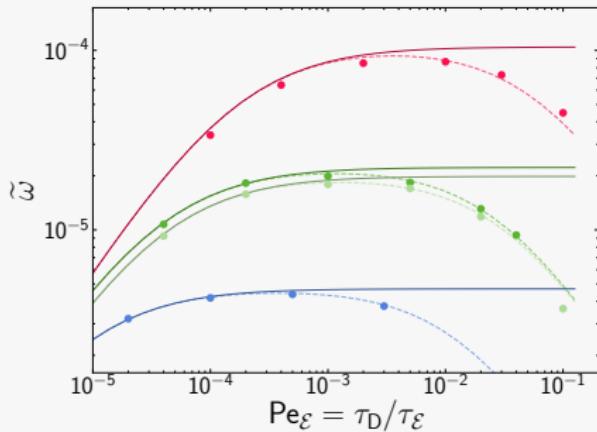
- agreement at small Péclet

Evaporation of a liquid mixture layer with Marangoni stress



horizontal velocity

Growth rate ω in function of $\text{Pe}_{\mathcal{E}} = \tau_D / \tau_{\mathcal{E}}$



high $v_{\mathcal{E}}$
moderate $v_{\mathcal{E}}$
low $v_{\mathcal{E}}$

- agreement at small Péclet
- **cross-diffusion limited** at high Péclet: $\tau_{\mathcal{I}} = \tau_D + \tau_{\mathcal{I},\text{th}}$
dashed line

Phase change

- header file for **pure liquid**
- examples: **static**, **oscillating**, **falling**, and **blown** drops
- additional header file for **mixtures**
- mwe: **diffusion** in a domain, **advection** with respect to a phase change velocity
- example: **digitations** at slow solute diffusion

Marangoni stress

- header files: **straight line** or **circle arc** extrapolations
- **capwave** mwe
- contact angles with **straight line** or **circle arc** extrapolations
- mwe with **adaptive mesh**
- **Marangoni flow** example

Phase change

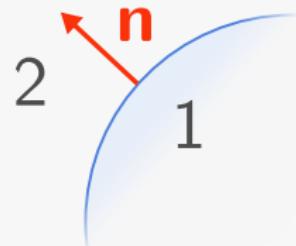
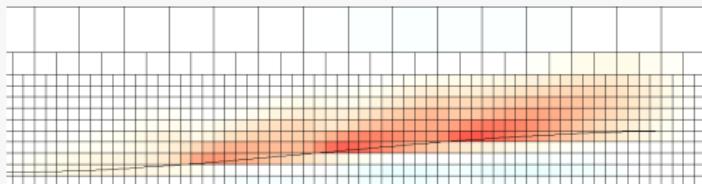
- **Stefan flow** and recoil pressure
 - ▶ Cécile Lalanne & Jose-Maria Fullana
- **Embedded boundaries** would ensure more precise conditions
 - ▶ Alexandre Limare & Christophe Josserand

Marangoni stress

- switch between height functions
- extend to **3D**
- jump of the **tangential viscous stress**

Conclusion ► Viscous stress jump

Close up on a simulation
horizontal velocity



$$[A] = A_2 - A_1$$

$\underline{\underline{\sigma}}$: stress tensor

Tangential stress continuity: $[\mathbf{t} \underline{\underline{\sigma}} \mathbf{n}] = \nabla_S \gamma \cdot \mathbf{t}$

$$\blacktriangleright \partial_t \gamma = \mu_2 (\partial_t u_n|_2 + \partial_n u_t|_2) - \mu_1 (\partial_t u_n|_1 + \partial_n u_t|_1)$$

Normal stress continuity: $[\mathbf{n} \underline{\underline{\sigma}} \mathbf{n}] = \gamma \kappa$