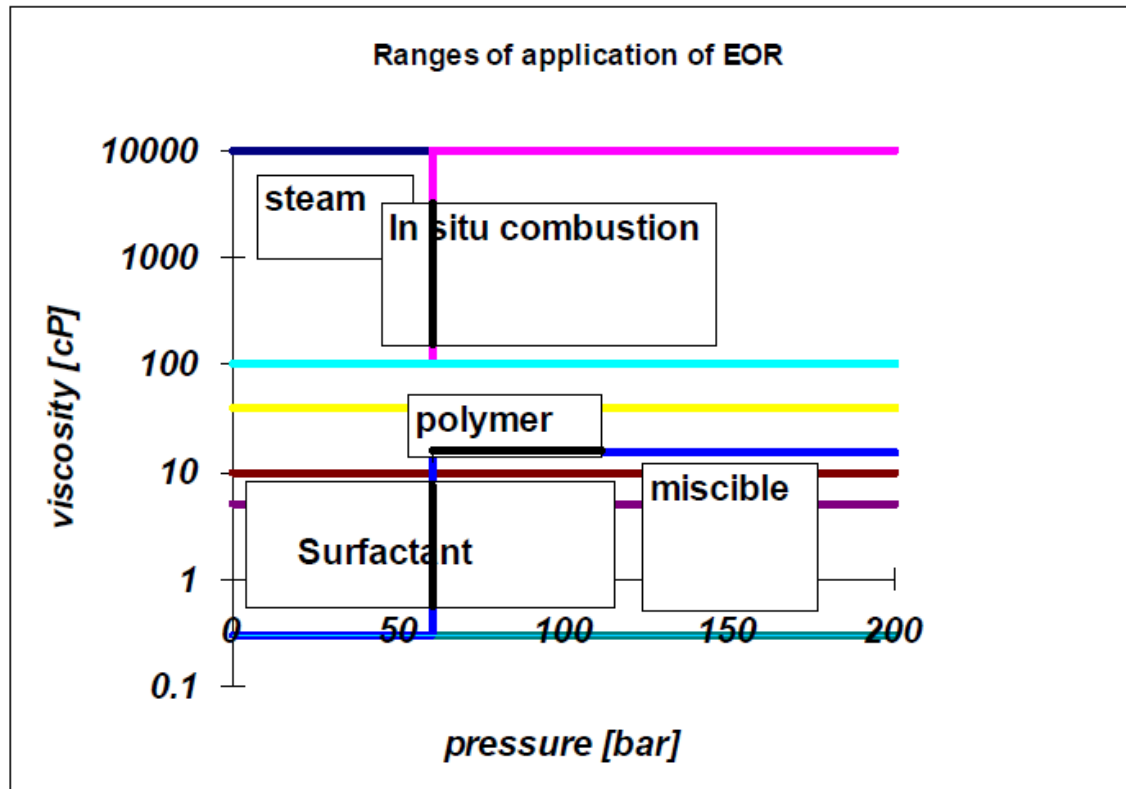


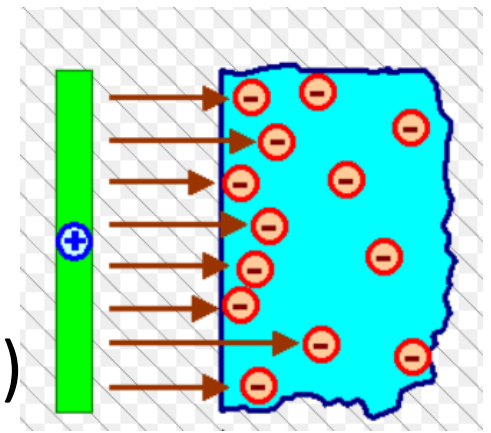
# **Geochemical Modeling of water flooding oil in calcite reservoirs at high carbon dioxide pressure**

Rouhi Farajzadeh, Dan Marchesin, Cor van Kruijsdijk, Wanderson Lambert, Hua Guo, Ali Akbar Eftekhari, Vitor Matos, Hamidreza Salimi, Amaury Alvarez Cruz

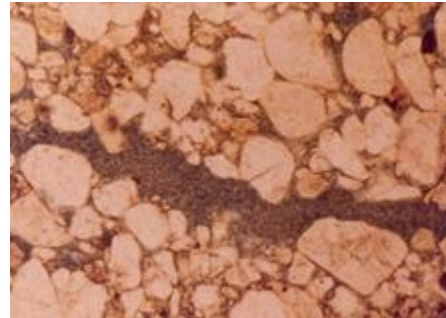
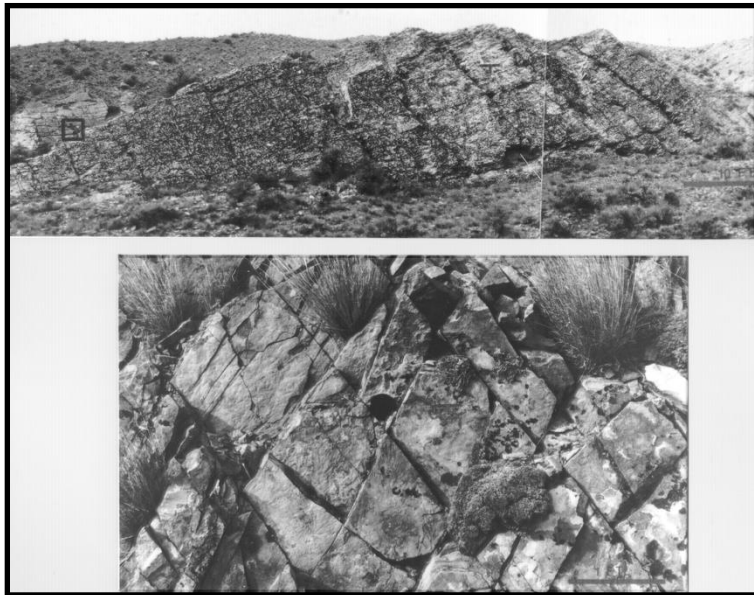


**RECOVERY OF OIL BECOMES INCREASINGLY CHALLENGING, WHAT ABOUT LOW/HIGH SALINITY WATER INJECTION?**

# Other challenges: Incorporate geochemistry

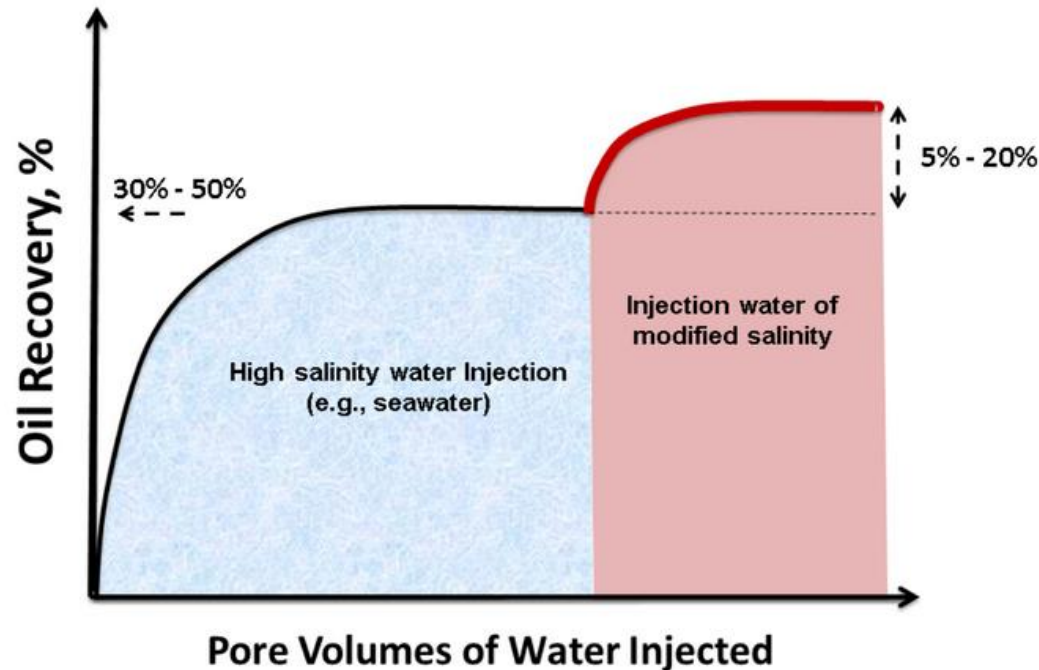


- High salinities (low-salinity water injection)
- Oil-wet- fractured calcite reservoirs
- High carbon dioxide content



$$\log_{10} \gamma_{\pm} = -\frac{Az_+z_-\sqrt{I}}{1+aB\sqrt{I}} + CI$$

**Before the turn of the century it was found by many researchers (Norman Morrow) that the water composition can effect oil recovery by some 10%**



- Yildiz, H.O., Valat, M., and Morrow, N.R.: "Effect of Brine Composition on Wettability and Oil Recovery of a Prudhoe Bay Crude Oil," J. Can. Pet. Tech, Jan. 1999, 38 (1) 26-31.
- Tang, G.Q. and Morrow, N.R.: "Salinity Temperature, Oil Composition and Oil Recovery by Waterflooding," SPE Reservoir Engineering, November 1997, 12, (4) 269-276.

# presal

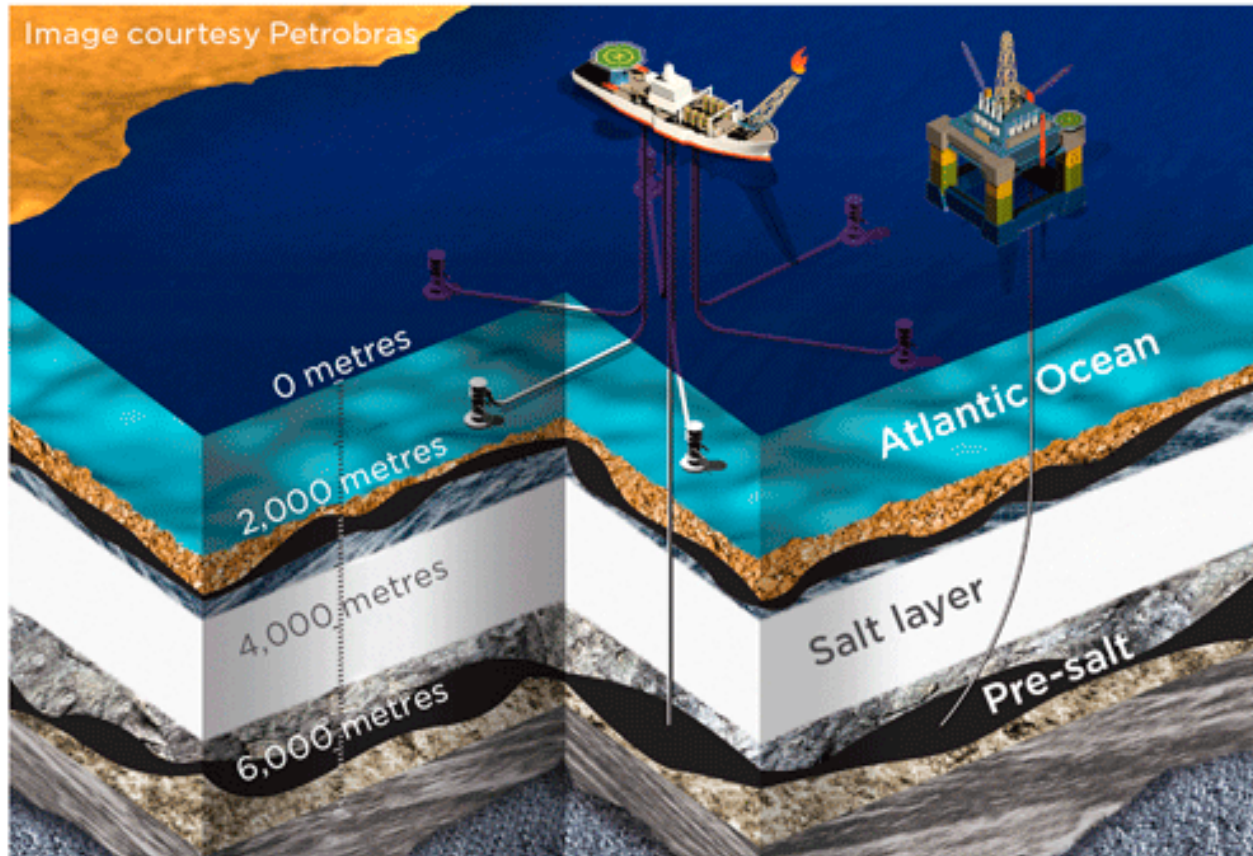
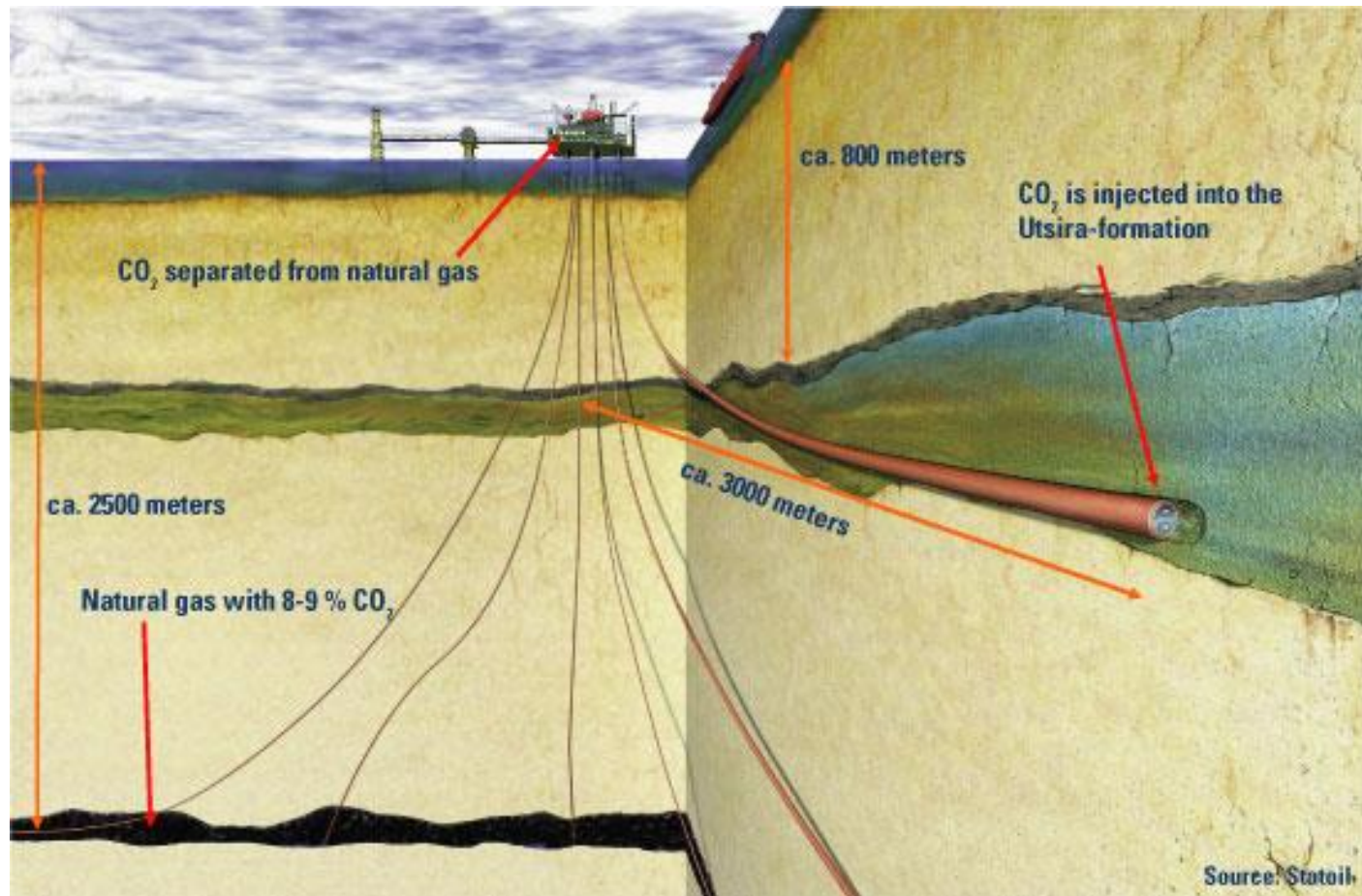


Illustration of oil extraction from Brazil's pre-salt reservoirs



# Sleipner field

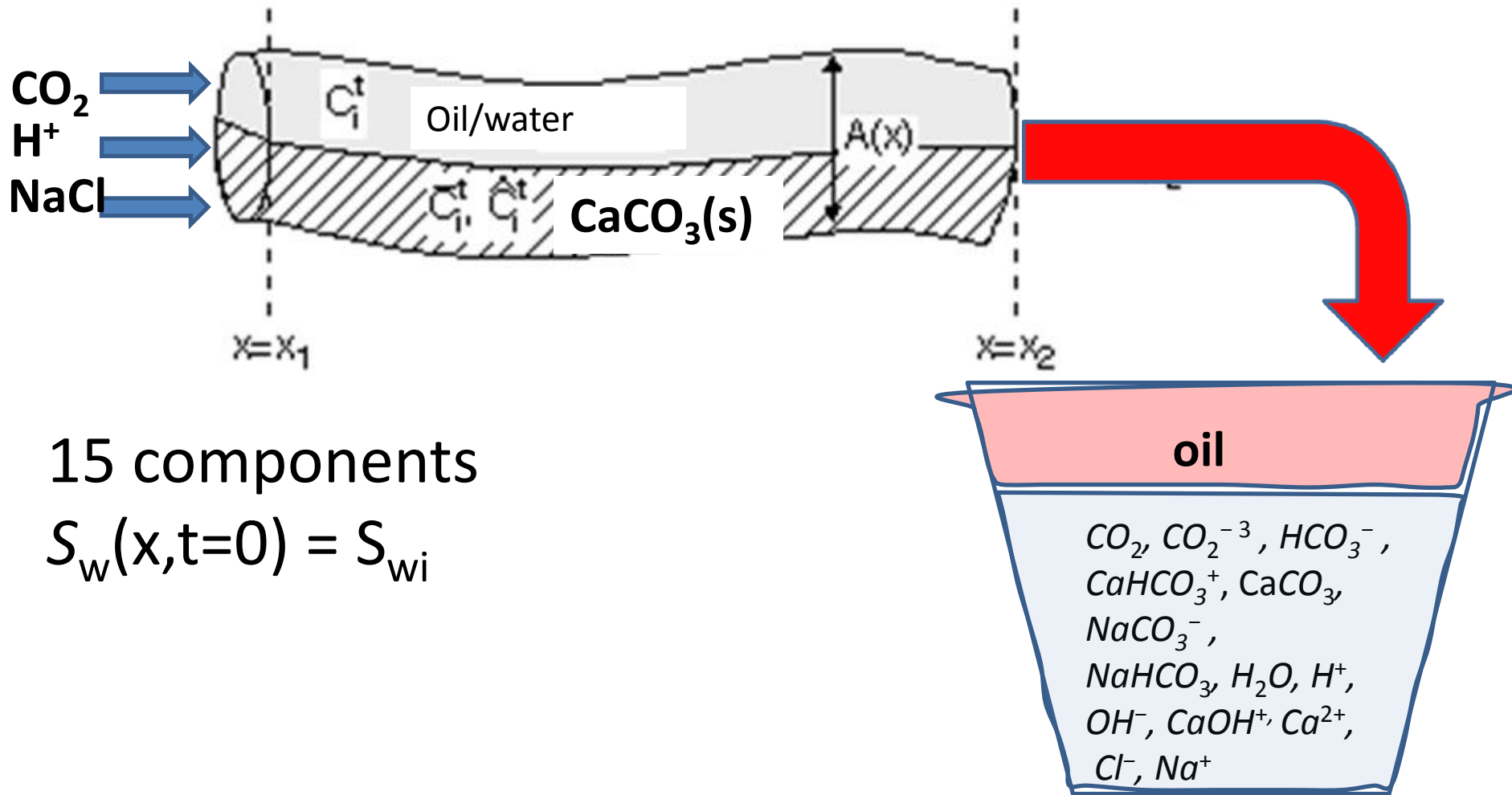


# Hypotheses

- **1-Geochemistry can be incorporated in multiphase flow simulators by**
  - a- Use of geochemical software to create look-up tables or regression formula and use of EUREQA statistical software
  - b- Simultaneous solution of all relevant equations
- **2- Oil recovery predictions require full incorporation of geochemistry**
  - a- e.g.: Aqueous Carbon dioxide dissolution depends on ionic strength
  - b- Wetting behaviour depends on surface charges and thus on adsorption of surface complexes
  - Positive effect on relative permeabilities not clear
- **The main challenge for petroleum engineers is to understand geochemistry, which is facilitated with the help of existing free software**
  - PHREEQC, MINTEQ
- **Dissolved Carbon dioxide, analogously to gaseous CO<sub>2</sub>, main contributor to enhance oil recovery**

# Low salinity water injection: 1-D setting

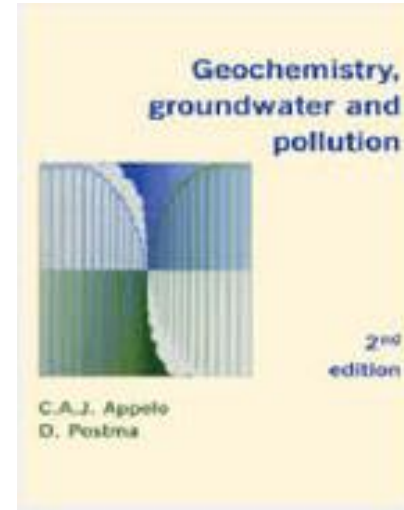
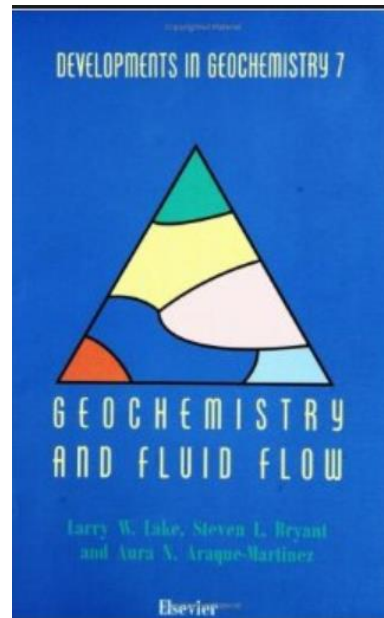
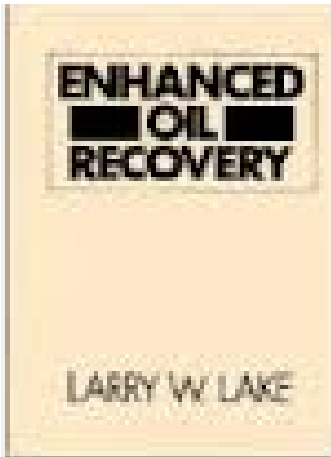
Figure adapted from geochemistry and fluid flow



15 components

$$S_w(x, t=0) = S_{wi}$$





Traditional approach using geochemical software for “flash” calculation  
MORES and PHREEQC (ETH))

# MODELING MULTIPHASE FLOW INCLUDING GEOCHEMISTRY

# Main step in creation of look-up table

## Determine # of equations and unknowns

- **Assumption of local thermodynamic equilibrium: number of degrees of freedom  $N_f$  can be derived with extended Gibbs phase rule:  $N_f = N_s - N_r - N_c - p + 2 = \# \text{ species} - \# \text{ reactions} - \# \text{ constraints} - \# \text{ phases} + (T,P) = 15-8-2-3 = 2 + (T,P \text{ pm})$** 
  - $N_c = 2$  for charge balance equation and NaCl equation,  $p = 3$
  - We choose  $H^+$  and  $Cl^-$*
- **For surface species  $N_s - N_r - N_c = 0 = \# \text{ surface species} - \# \text{ reactions} - \# \text{ constraints}$  (number of species – number of reactions – number of constraints = zero; see below)**

(1) C Anthony J Appelo and Dieke Postma. *Geochemistry, groundwater and pollution*. Taylor & Francis, 2005.

(2) David L Parkhurst and CAJ Appelo. *Description of Input and Examples for PHREEQC* US Geological Survey Denver, 2013.

Activities

# **EQUILIBRIUM RELATIONS**

# Eight equilibrium equations (page 87 of EOR)

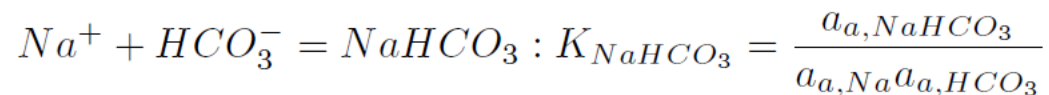
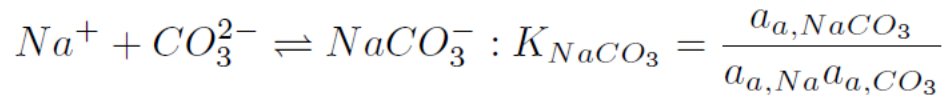
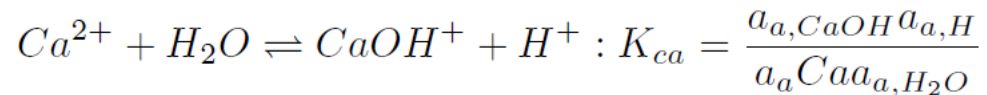
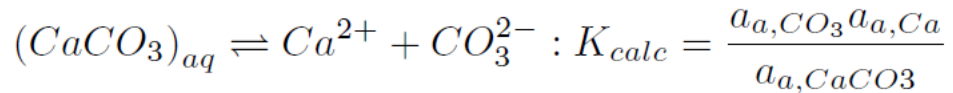
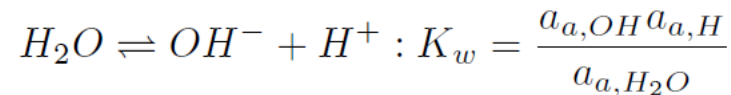
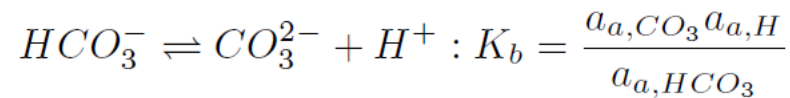
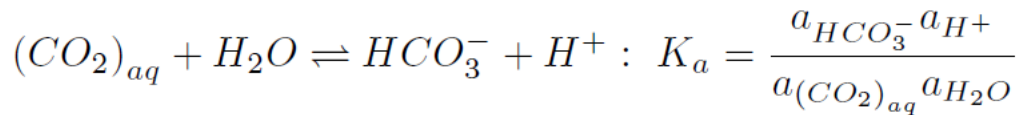
**TABLE 3-7** SELECTED SOLUBILITY DATA AT 298 K FOR AQUEOUS AND SOLID SPECIES IN NATURALLY OCCURRING PERMEABLE MEDIA (ADAPTED FROM DRIA ET AL., 1988)

Aqueous species or complexes		Log $K_r$	$\Delta H^\circ$ J/kg-mole
$\text{OH}^-$	$= \text{H}_2\text{O} - \text{H}^+$	14.00	-133.5
$\text{CaOH}^+$	$= \text{Ca}^{2+} + \text{H}_2\text{O} - \text{H}^+$	12.70	-173.2
$\text{Ca}(\text{OH})_2$	$= \text{Ca}^{2+} + 2\text{H}_2\text{O} - 2\text{H}^+$	27.92	-267.2
$\text{CaCO}_3$	$= \text{Ca}^{2+} + \text{CO}_3^{2-}$	-3.23	44.1
$\text{CaHCO}_3^+$	$= \text{Ca}^{2+} + \text{CO}_3^{2-} + \text{H}^+$	-11.23	45.0
$\text{Ca}(\text{HCO}_3)_2$	$= \text{Ca}^{+2} + 2\text{CO}_3^{2-} + 2\text{H}^+$	-20.73	66.8
$\text{HCO}_3^-$	$= \text{CO}_3^{2-} + \text{H}^+$	-8.84	35.5
$\text{CO}_2(\text{dissolved})$	$= \text{CO}_3^{2-} - \text{H}_2\text{O} + 2\text{H}^+$	-16.68	53.8

# Equilibrium reactions: PHREEQC (US-geological survey)

## input concentrations: NaCl, CO<sub>2</sub> equilibrate with calcite

### (Appelo / Parkhurst)



$$(CaCO_3)_r = (CaCO_3)_{aq}$$

$$(CO_2)_o = (CO_2)_{aq}$$

USGS Software determines:

- (1) 15 Relevant species
- (2) 10 Equilibrium reactions
- (3) Equilibrium calculations
- (4) Equilibrium compositions

Eureqa software determines  
convenient regression  
expressions; choice between  
accuracy and simplicity

# Some theory to obtain activity coefficients ( $a = \gamma c$ )

- The chemical potential of a component does not depend on whether the concentrations are measured in molar, molal or mole fractions.
- $\mu = \mu_{0x} + RT \ln (\gamma_x X) = \mu_{0m} + RT \ln (\gamma_m m) = \mu_{0c} + RT \ln (\gamma_c c) = \mu_0 + RT \ln a$   
where  $\mu_{0x}$  is the chemical potential of pure solute having the properties of an infinitely dilute solution,  $\mu_{0m}$  is the chemical potential of the solute in the ideal one molal solution and  $\mu_{0c}$  is the chemical potential of the ideal one molar solution.
- Anderson and Crerar show that difference between the activity coefficients  $\gamma$  except for very high concentrations are extremely small, e.g.,  
$$\ln \gamma_x = \ln \gamma_m + \Gamma = \ln \gamma_m + \ln (1 + 0.0180153m)$$
- Greg M Anderson and David A Crerar. *Thermodynamics in geochemistry: The equilibrium model*. Oxford University Press, USA, 1993.



## Activity coefficients

- The chemical potential does not depend on whether the concentrations are expressed in mole fractions  $X$ , molalities  $m$ , or molarities  $c$  or activities  $a$ .
- The equations require a reference concentration:  $X=1$ , concentration / sum of concentrations,  $m =$  *concentration of one mol / kg-water (molal) or one mol / liter solution (molar)*

$$\begin{aligned}\mu &= \mu_X^0 + RT \ln (\gamma_{H,x} X) \\ &= \mu_m^0 + RT \ln (\gamma_{H,m} m) \\ &= \mu_c^0 + RT \ln (\gamma_{H,c} c) \\ &= \mu^0 + RT \ln a\end{aligned}$$

The reference activity is the activity of one molal of substance if it were to behave ideally.

$$\ln \gamma_{H,x} = \ln \gamma_{H,m} + \Gamma = \ln \gamma_{H,m} + \ln (1 + 0.0180153m)$$

# Activity coefficients $\gamma = a / c$

The extended Debye-Hückel theory for calculating the activity coefficient  $\gamma_j(\mu)$  of an ion reads ( $A = 1.1709$ ,  $B = 0.3281$ ,

ionic strength =  $\mu = \frac{1}{2} \sum c_i z_i^2 = \frac{1}{2} \sum a_i \gamma_i(\mu) z_i^2$ )

$$\ln \gamma_j(\mu) = -A z_j^2 \sqrt{\mu} / (1 + B a_j \sqrt{\mu}) + b_j \mu$$

In the absence of data for the ionic radius  $a_j$  and the activity fraction coefficient  $b_j$ , the formula of Davies is often used

$$\ln \gamma_j(\mu) = -A z_j^2 \sqrt{\mu} / (1 + B \sqrt{\mu}) + 0.3 \mu$$

Equilibrium constants are expressed in activities not concentrations

## Activity coefficients

There is a variety of models for the activity coefficient. Data difficult to find

Debye-Huckel model:

$$\ln \gamma_j (\mu) = -Az_j^2 \nu \mu / (1 + B^\circ a_j \nu \mu) + b_j \mu$$

$$B_\gamma = (8\pi N_A q_e^2 \rho_0 / 1000 \epsilon_r k_B T)^{1/2} =$$

$$50.29158649 \rho_0^{1/2} / (\epsilon_r T)^{1/2}$$

$$A_\gamma = (2\pi N_A q_e^6 \rho_0 / (1000 (\epsilon_r RT)^3))^{1/2} =$$

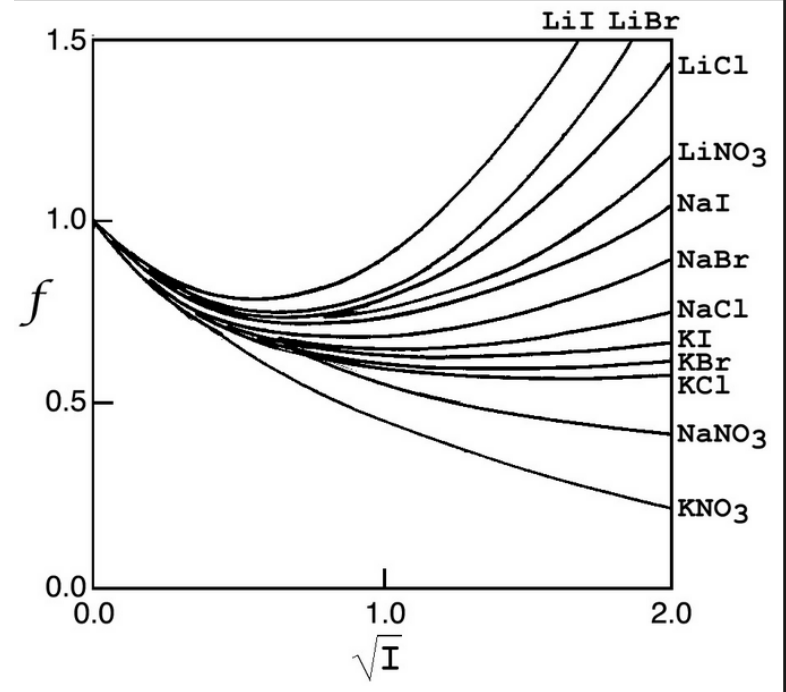
$$= 1824829.238 \rho_0^{1/2} / (\epsilon_r T)^{3/2}$$

[mol/kg]<sup>1/2</sup>,  $a_j$  in Angstrom

at where  $A = 1.1708$ ,  $B = 0.3281$

Davies made an equation that does not require ion specific data

$$\ln \gamma_j (\mu) = -Az_j^2 \nu \mu / (1 + \nu \mu) + 0.3 \mu,$$



$$[\alpha_{Ca^{2+}}][\alpha_{CO_3^{2-}}] = K_{sp} = 4.47 \times 10^{-9}$$

$$[Ca^{2+}]\gamma_{Ca^{2+}}[CO_3^{2-}]\gamma_{CO_3^{2-}} = K_{sp} = 4.47 \times 10^{-9}$$

$$[Ca^{2+}](0.405)[CO_3^{2-}](0.37) = 4.47 \times 10^{-9}$$

$$X^2 = \frac{4.47 \times 10^{-9}}{(0.405)(0.37)} = 2.98 \times 10^{-8}$$

$$X = \sqrt{2.98 \times 10^{-8}} = 1.73 \times 10^{-4}$$

# Activity coefficients for neutral molecules

The Setch'elow coefficient  $k_s$  relates the activity coefficient of interest to the ionic strength of the solution, e.g., for carbon dioxide

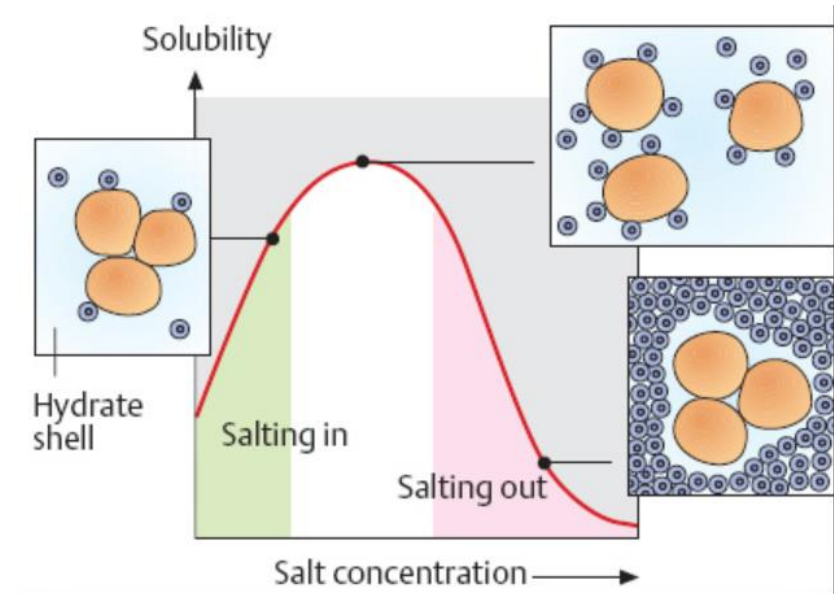
$$\log \gamma_{CO2(aq)} = k_s \mu,$$

where the logarithm has base ten. Similar relations hold for the other noncharged components.

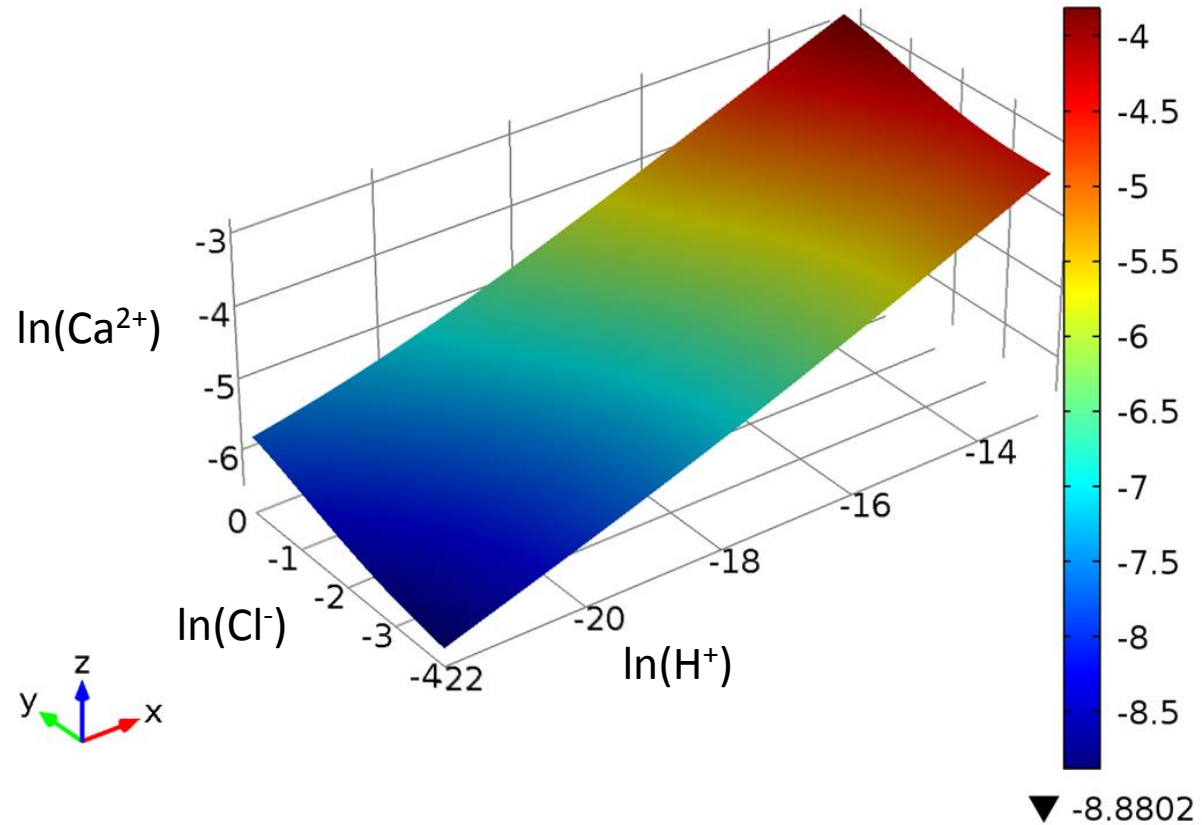
For single salt solutions, values can be found in [98]. Byrne et al. [21] use the equation

$$\log m_0 / m_s = \sum k_{m,i} \mu$$

where  $m$  and  $m_0$  are the solubilities in salt solutions and distilled water

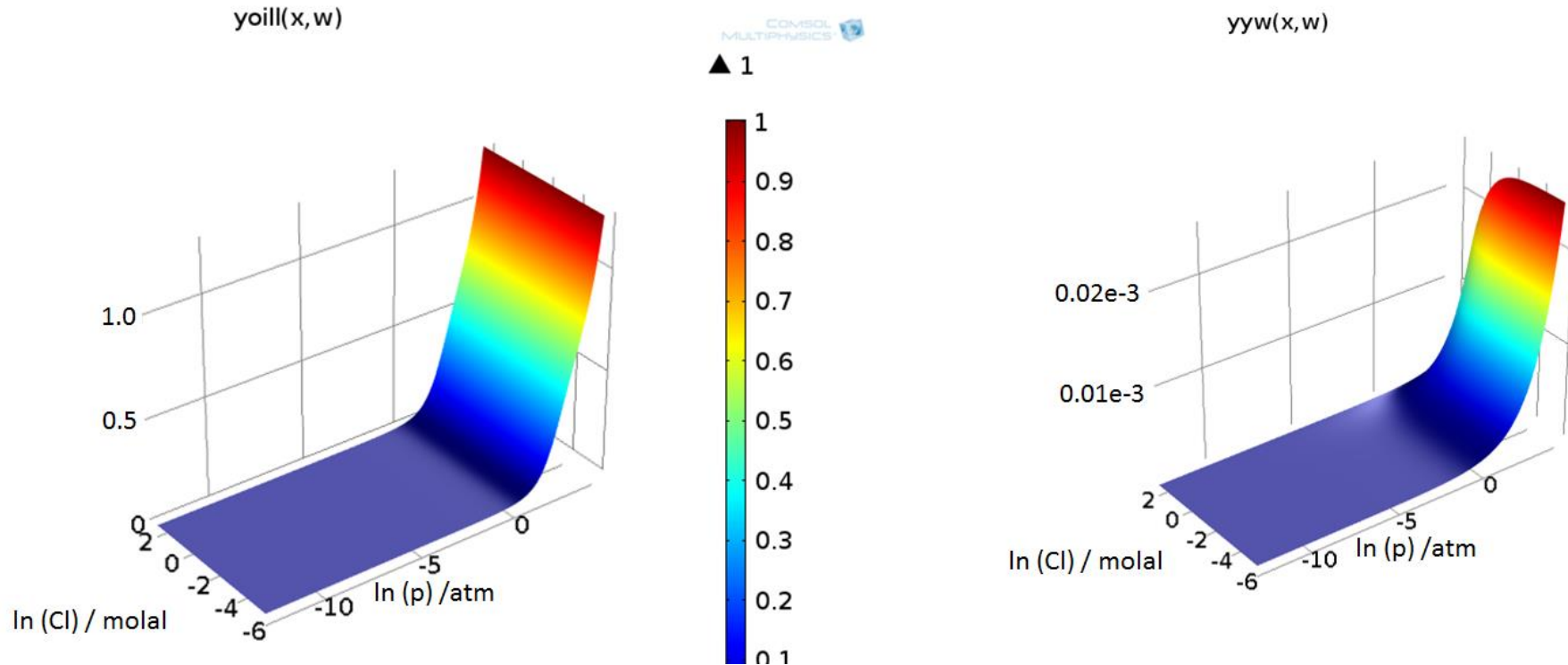


$\ln(\text{Ca}^{2+})$  (hp = x =  $\ln(\text{H}^+)$ , cl = y =  $\ln \text{Cl}^-$ )



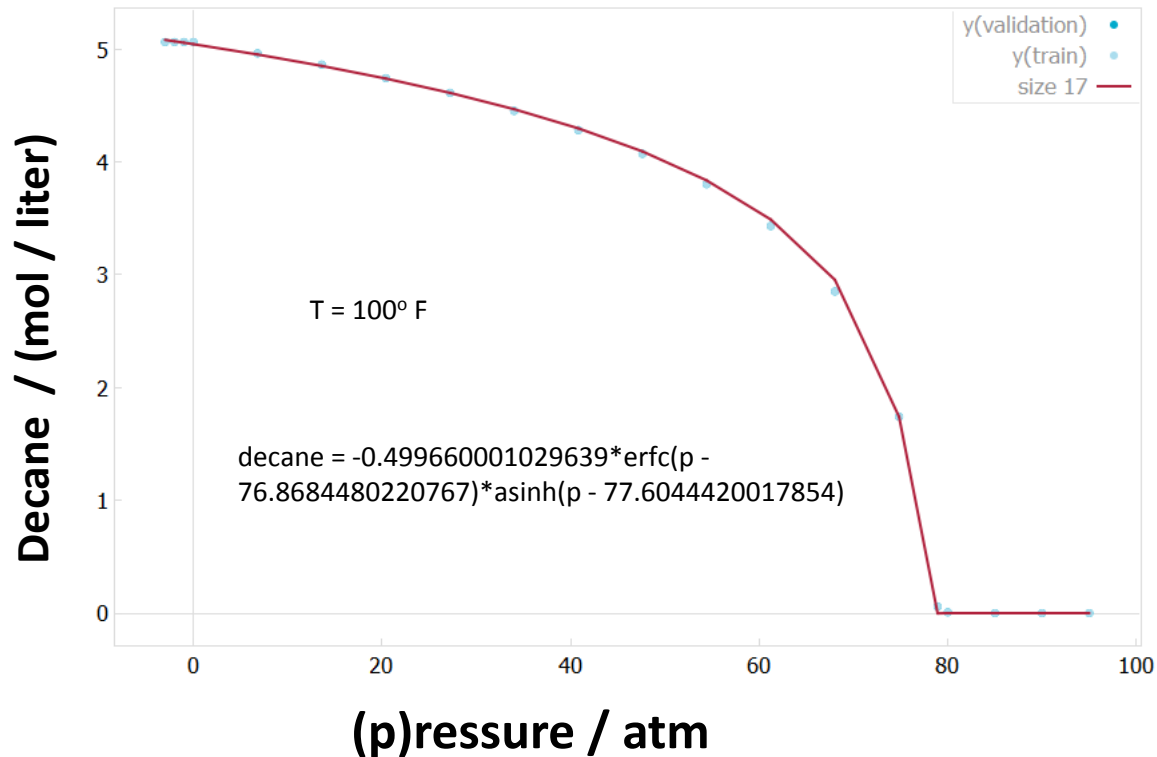
$$\ln(\text{Ca}^{2+}) = 1.93 + 0.467 \ln(\text{H}^+) - 0.00927 \ln(\text{H}^+) \ln(\text{Cl}^-) - 0.0893 \ln(\text{Cl}^-) (\text{Cl}^-)$$

# Comparison of carbon dioxide dissolution in oil and water

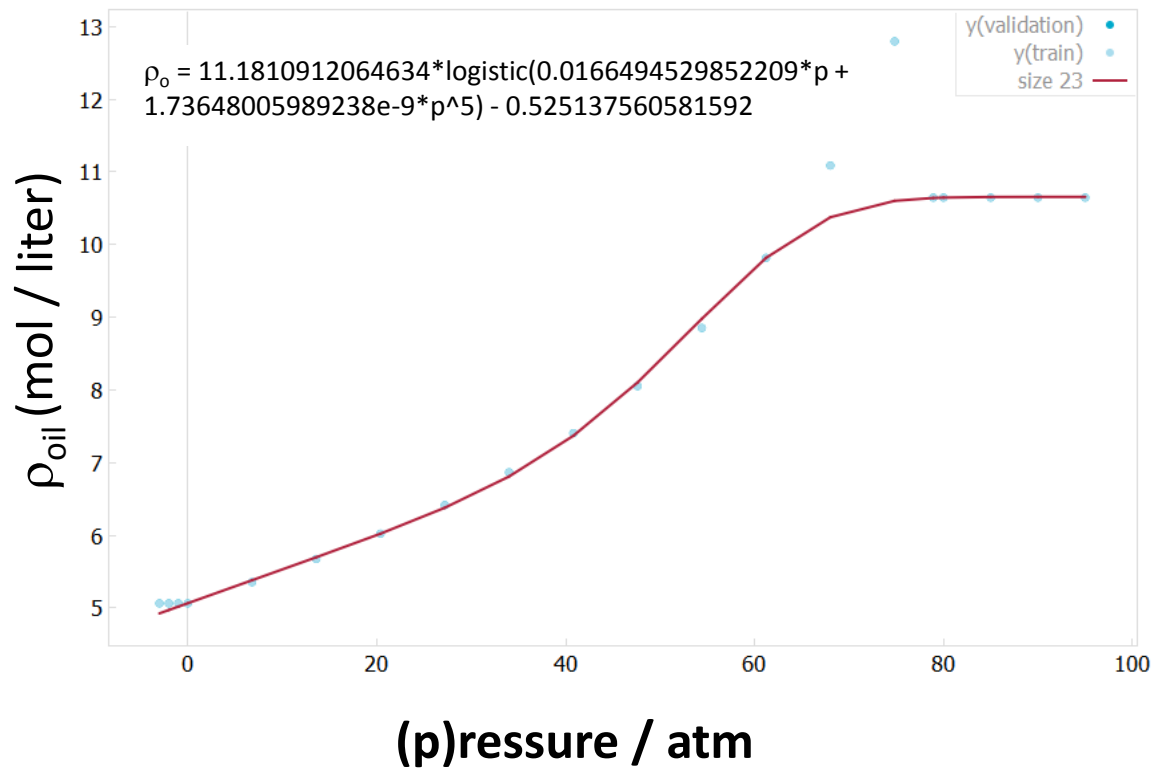




# Decane versus pressure



# Oleic phase density versus pressure



Example necessity of incorporation of geochemistry

# **CARBON DIOXIDE DISSOLUTION DEPENDS ON IONIC STRENGTH**

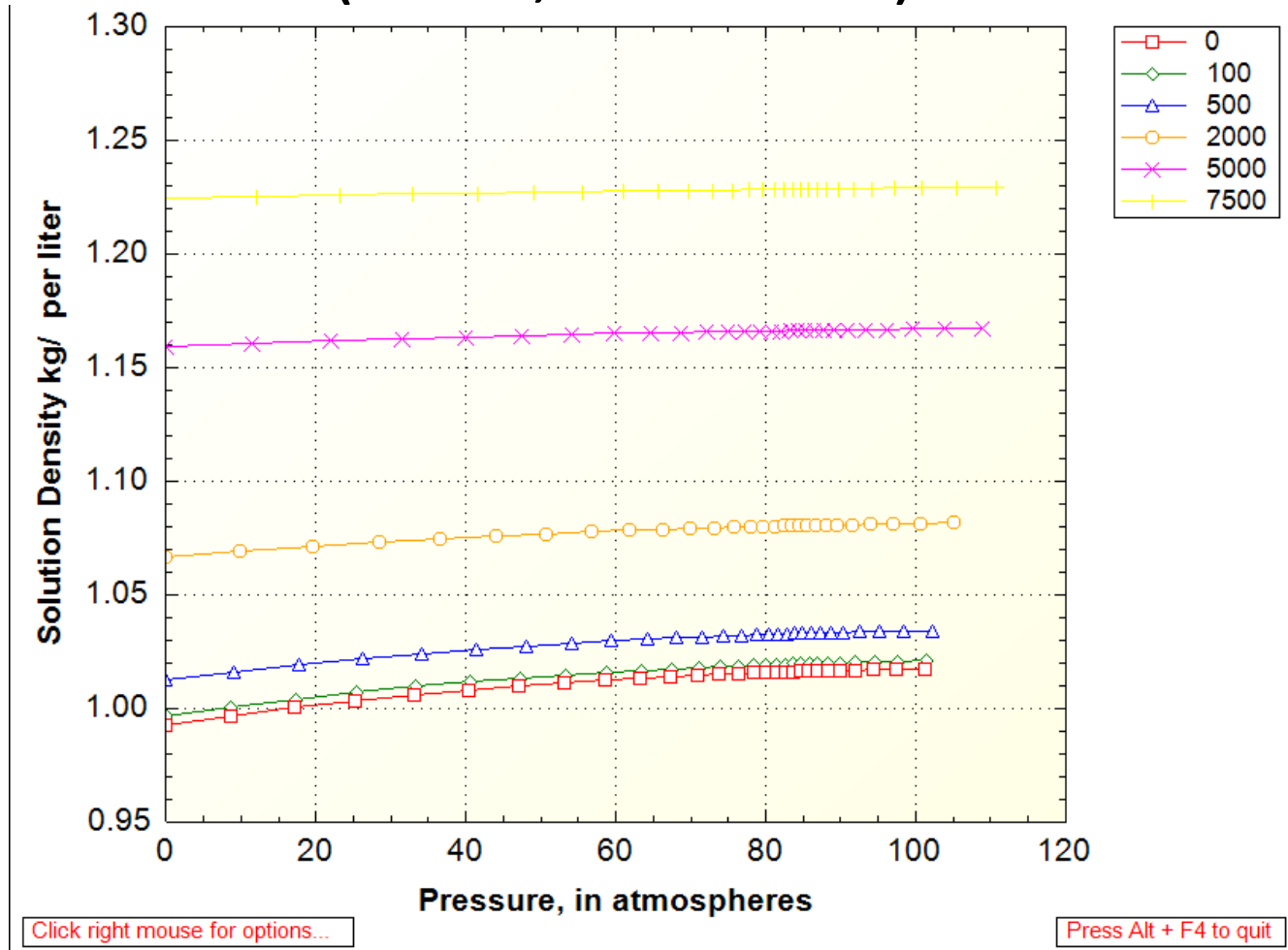
# Carbon dioxide dissolution

At this boundary we use Henry's law to relate the gas pressure to the carbon dioxide concentration in the liquid, i.e.,

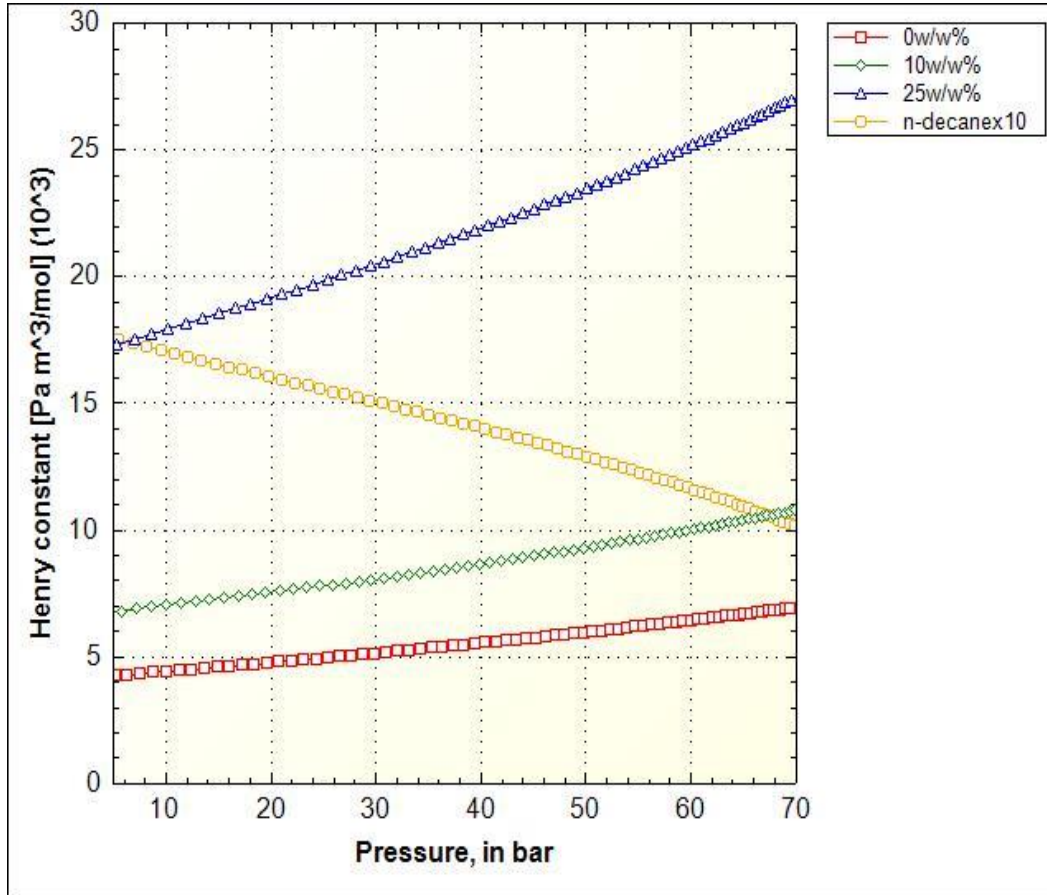
$$K_{w-g}^H = a_{w,CO_2} / a_{g,CO_2} = m_{w,CO_2} \gamma_{w,CO_2} / f_{g,CO_2} \quad , \quad 6$$

where  $m_{w,CO_2}$  is the molality of carbon dioxide in the water phase,  $\gamma_{w,CO_2}$  the activity coefficient, and  $f_{g,CO_2(g)}$  is the fugacity of carbon dioxide in the gas phase. We use PHREEQC ([Parkhurst and Appelo, 2013](#)) for the computations. The procedure to get activities in neutral molecules is given in ([Randall and Failey, 1927](#))

# Density of carbon dioxide solutions (ex 22, PHREEQC)



# Henry coefficient $P=Hc$



$$K_H = a_{\text{CO}_2(g)} / a_{\text{CO}_2(aq)} = f_{\text{CO}_2(g)} / c_{\text{CO}_2(aq)} \gamma_{\text{CO}_2(aq)}$$

$$K = a_{\text{CO}_2(aq)} / a_{\text{CO}_2(g)} \text{ and } \text{fresh/salt} = K / K_s = \gamma$$

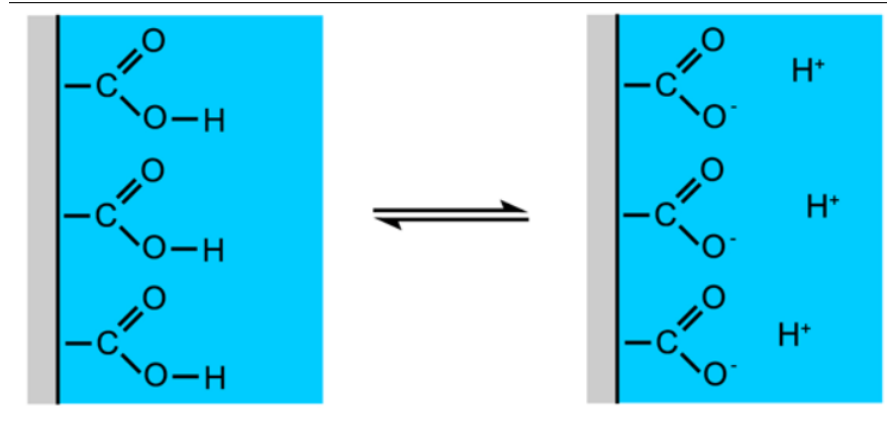
**Setchenov-coefficients  $C$**

$$\log_{10} \gamma_{\pm} = - \frac{A z_+ z_- \sqrt{I}}{1 + a B \sqrt{I}} + C I$$



- Adsorbed species determine surface charge

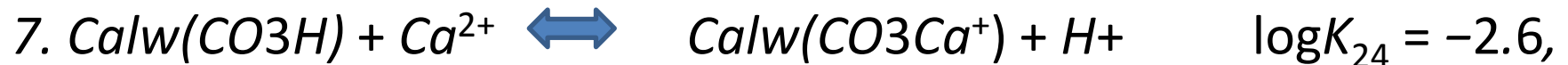
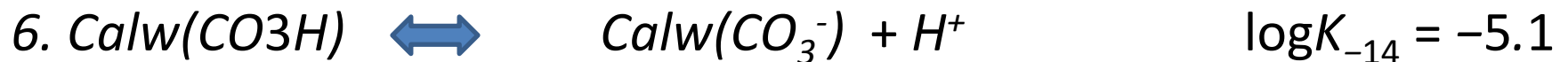
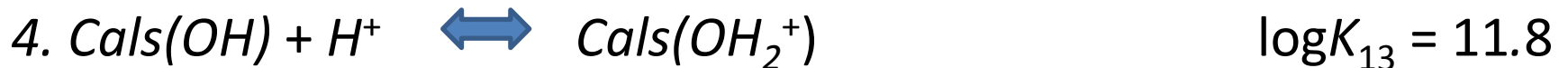
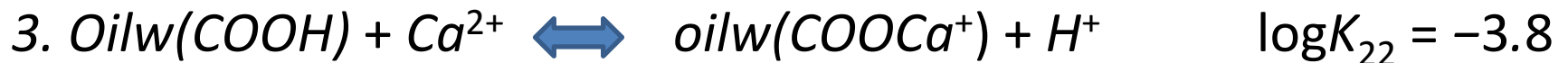
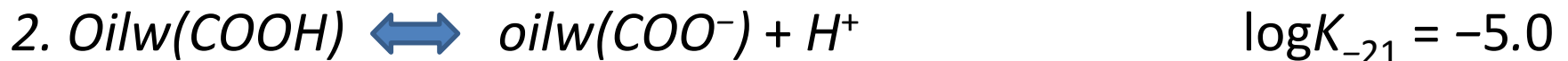
Charge on calcite and oil surface  
can be obtained with phreeqc



- **Importance of surface complexes**

Wetting behaviour depends on surface charges and thus on adsorption of surface complexes

# Surface complexes (after Brady)



## 4- Constraints

$$oil_s(NH^+) + oil_s(N) = x_1 c_1$$

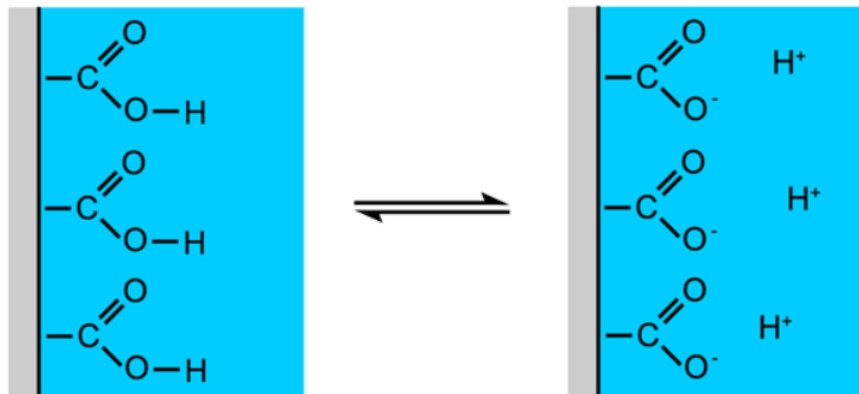
$$Oil_w(COOH) + oil_w(COO^-) + oil_w(COOCa^+) = x_2 c_2$$

$$Cal_s(OH) + Cal_s(OH_2^+) + Cal_s(CO_3^-) = x_3 c_3$$

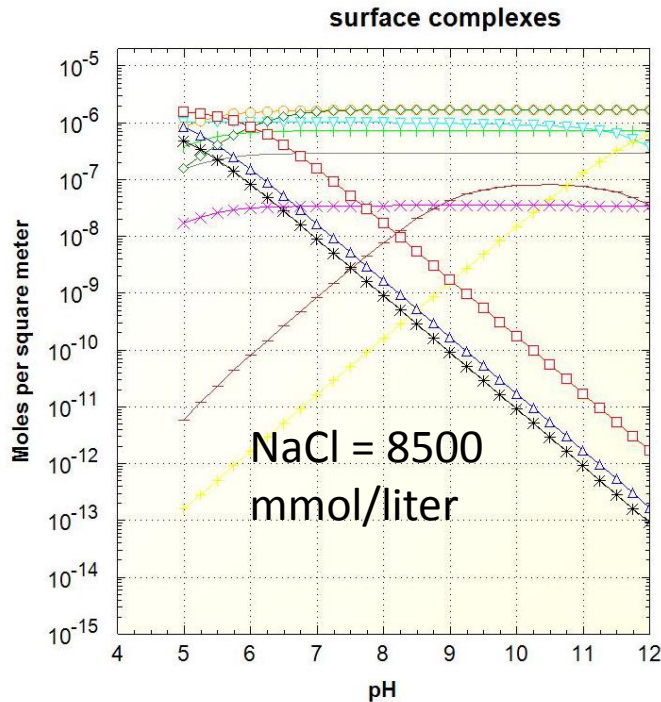
$$Cal_w(CO_3H) + Cal_w(CO_3^-) + Cal_w(CO_3Ca^+) = x_4 c_4$$

# Calculation of charge densities

- The charge density in the domain of fixed ions is given by  $\sigma = F/(AS) \sum_s (c_s v_s)$ ,  $F$  = Faraday constant,  $c_s$ ,  $v_s$  = concentration and charge of surface species. Solid concentration  $S = \text{g/L}$ ,  $A[\text{m}^2/\text{g}]$
- $\sigma = \text{sign}(\psi_0) \sqrt{(4000RT\epsilon_r\epsilon_0) \sum_i S_{\text{bulk};i} (\exp -z_i F\psi_0 / (RT) - 1)} \rightarrow \psi_0$
- $\Delta G_{0\text{Total}} = \Delta G_{0\text{intrinsic}} + \Delta G_{0\text{Coulombic}} = \Delta G_{0\text{intrinsic}} + \Delta ZF\psi_0$
- $K_{\text{app}} = \exp(-\Delta G_{0\text{intrinsic}} + \Delta ZF\psi_0 / (RT)) := K_{\text{int}} \exp(\Delta ZF\psi_0 / RT)$



# Surface concentrations; effect of ionic strength (PHREEQC)

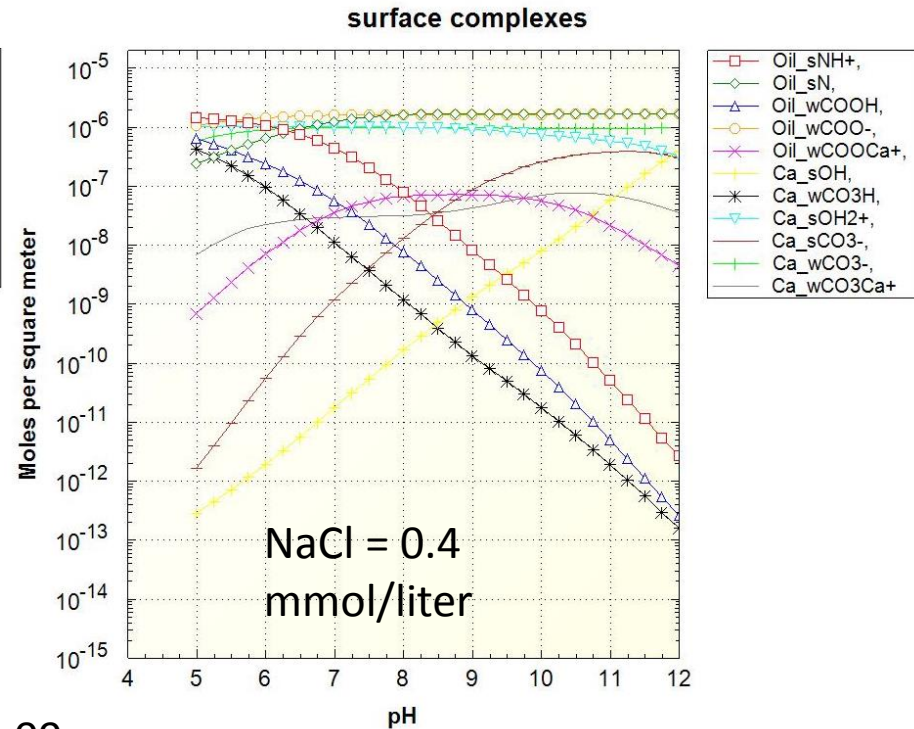


Oil\_sNH+ 1.67e-6 600. 0.09

Oil\_wCOOH 1.67e-6

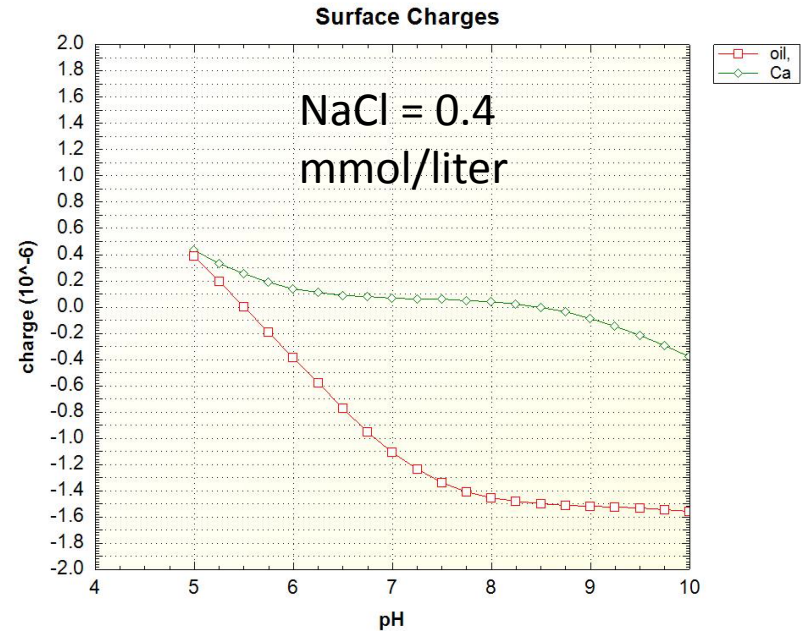
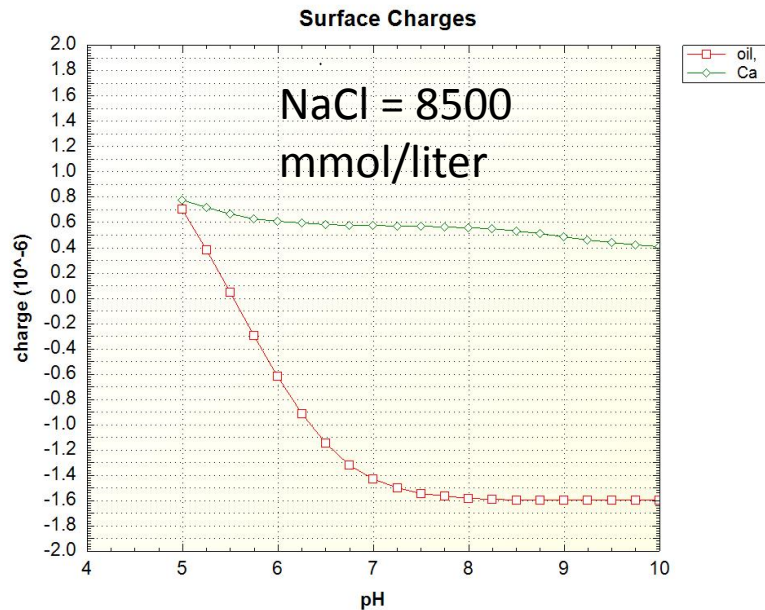
Ca\_sOH 1.0e-6 600. 0.09

Ca\_wCO3H 1.0e-6





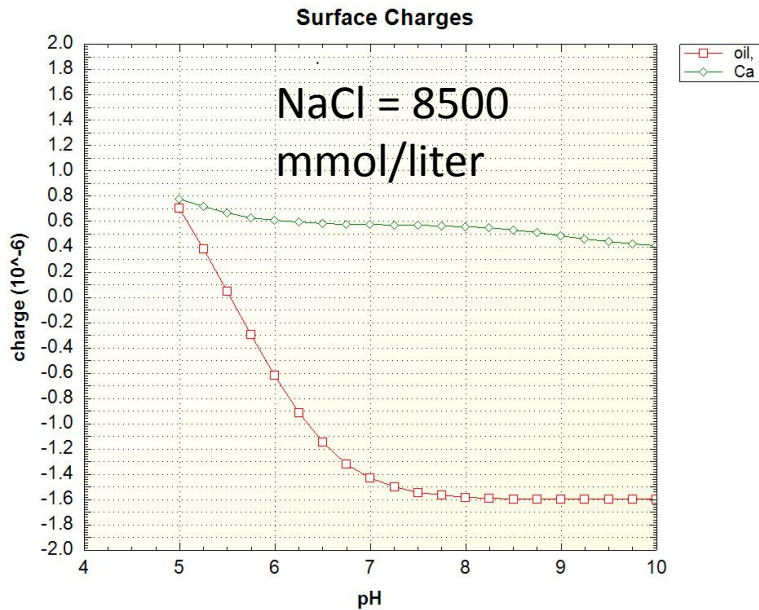
# Surface charge



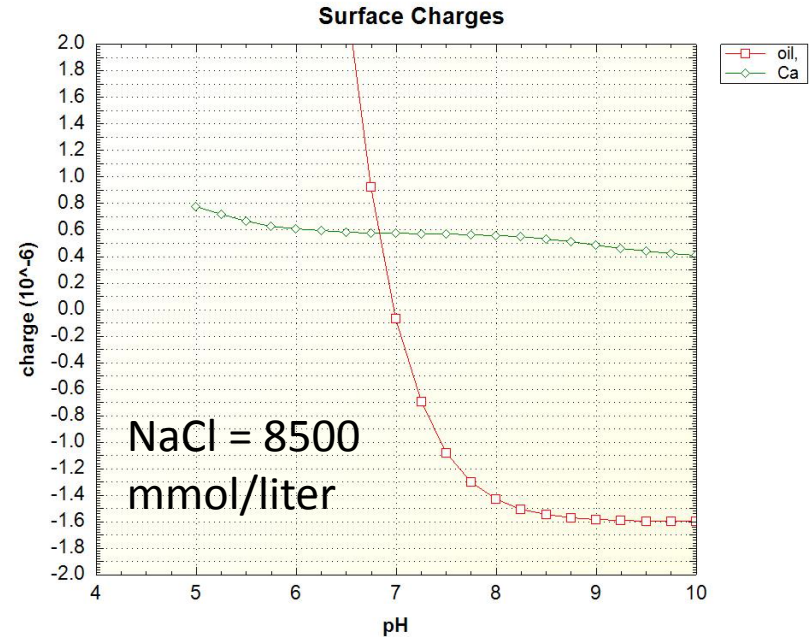
Oil\_sNH+ 1.67e-6 600. 0.09  
 Oil\_wCOOH 1.67e-6  
 Ca\_sOH 1.0e-6 600. 0.09  
 Ca\_wCO3H 1.0e-6

# Surface charge

independent of amount of oil; depends on fraction active sites



Oil\_sNH+ 1.67e-6 600. 0.009  
 Oil\_wCOOH 1.67e-6  
 Ca\_sOH 1.0e-6 600. 0.009  
 Ca\_wCO3H 1.0e-6



Oil\_sNH+ 1.67e-5 600. 0.09  
 Oil\_wCOOH 1.67e-6  
 Ca\_sOH 1.0e-6 600. 0.09  
 Ca\_wCO3H 1.0e-6

## Interface interaction (SPE 17367, Hirasaki)

### *Van der Waals attraction*

$$A_z = \frac{3}{4} kT (\epsilon_1 - \epsilon_3) (\epsilon_2 - \epsilon_3) / ((\epsilon_1 + \epsilon_3) (\epsilon_2 + \epsilon_3) 12 \pi D^2) + \text{high frequency terms}$$

### *Double layer repulsion*

$$P(\kappa D \gg 1) \rightarrow (\epsilon_0 \epsilon)^{-1} \sigma_1 \sigma_2 e^{-\kappa D}$$

$$\kappa = 0.304 \text{ e-9} / \sqrt{I} \text{ (mol/liter)}$$

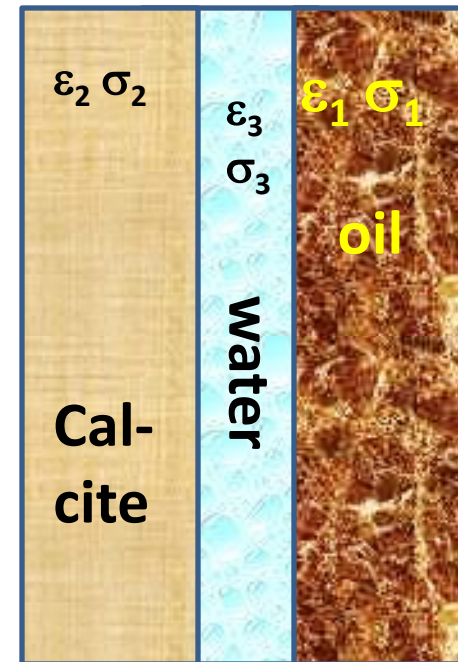
### *Hydration forces*

(Repulsive or attractive, very small range)

### *Disjoining pressure $\Pi$*

$\Pi = \partial_r U$  ;  $P_c = \Pi - 2 H \gamma$ ,  $H$  = curvature  
Unstable water films at high  $P_c$

## • Calcite-H<sub>2</sub>O-oil



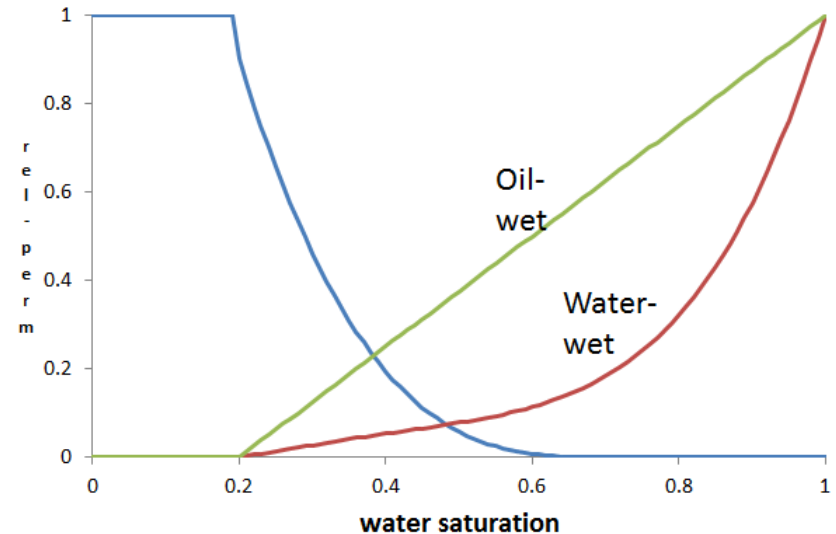
Repulsion is requirement for stability of water-film  
Water film is requirement for water-wet behavior

Charges on surface complexes

# **EFFECT ON RELATIVE PERMEABILITIES?**

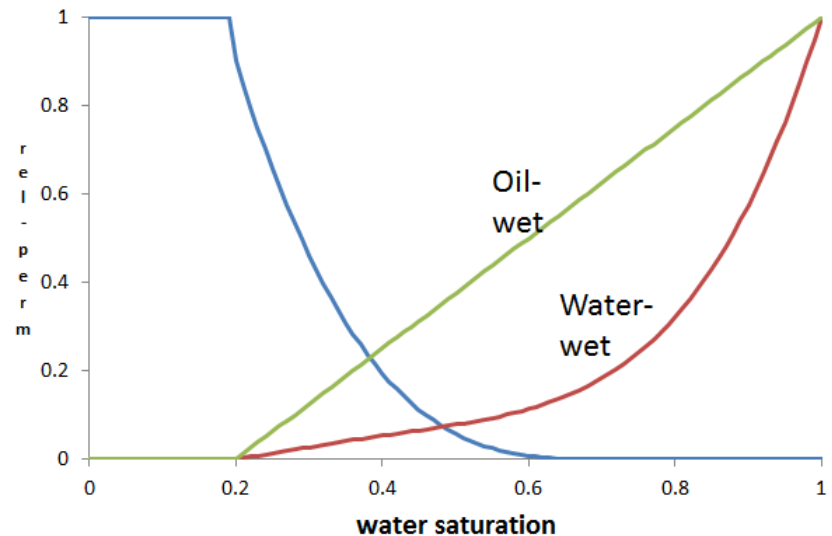
# Relative permeabilities

- Relative oil permeabilities of strongly water-wet systems remain close to one, when the oil saturation is 5-10% above one minus connate water saturation
- At residual oil saturation  $S_{or} \approx 0.25$  the relative permeability to water can be 10% of the single phase permeability.
- The cross-over point, i.e. the saturation at which the relative oil permeability and relative water permeability are equal is above 50% water saturation.

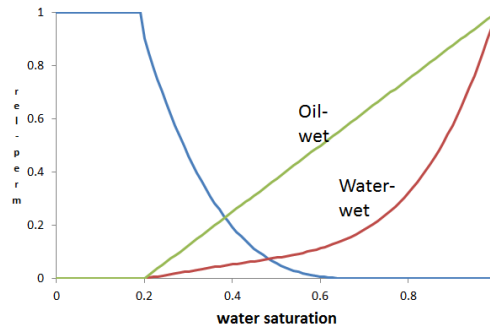
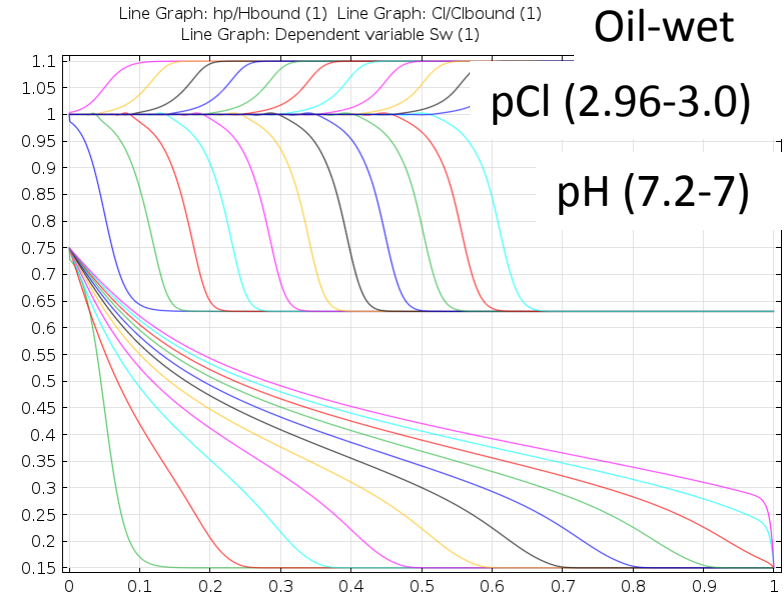
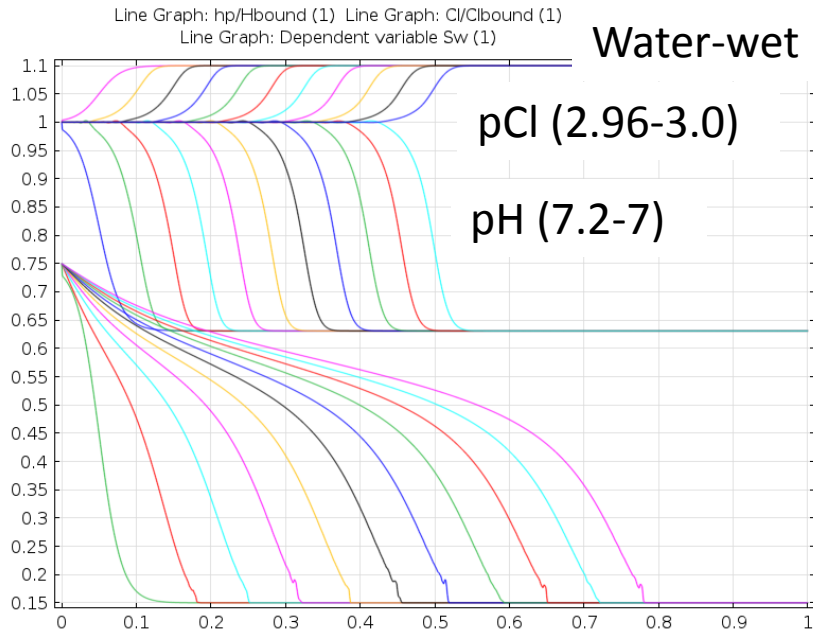


# Relative permeabilities

- For strongly oil-wet systems the oil permeability starts to reduce when the water saturation becomes higher than the connate water saturation.
- The relative permeability of water at residual oil saturation is greater than 50% and approaching 100%.
- The cross-over point when water and oil permeability are equal is less than 50%.



# Water-wet/ oil wet



Conservation of master species

# **DERIVATION OF MODEL EQUATIONS**



# Enumeration of master species, (Consult geochemical software, e.g. Appelo)

- Master species are C(+ 4), C(-4), H(1), O(-2), Ca(2), Na(1), Cl(-1)
  - C(4) = {CO<sub>2</sub>+ HCO<sub>3</sub> ,etc.}, C(-4) = C<sub>7</sub> H<sub>16</sub>
  - H(1) = {H<sup>+</sup>+ H<sub>2</sub>O, etc}
  - O(-2) = {CO<sub>2</sub>+ HCO<sub>3</sub> ,etc.}
  - Ca(2) = {Ca<sup>2+</sup> + CaOH<sup>+</sup> , etc}
  - Na(1) = {Na<sup>+</sup> + Na<sub>2</sub>CO<sub>3</sub> + NaHCO<sub>3</sub><sup>-</sup>}
  - Cl(-1) = {Cl<sup>-</sup>}
  - C(-4) = {C<sub>10</sub>H<sub>22</sub>}
- $\varphi \sum_{\alpha} \left( \partial_t (c_{\alpha} x_{\alpha i} S_{\alpha} + \partial_x (u c_{\alpha} x_{\alpha i} f_{\alpha}) \right) = \text{diffusion terms,}$   
i=1..N<sub>c</sub>) (EOR, pp 29)

# Equations

We are trying to find the solution of the total inorganic carbon equation

$$\partial_t (\varphi S_w c_{a,C(4).}) + \partial_t (\varphi S_o c_{o,CO_2.}) + \partial_x (u f_w c_{a,C(4).}) + \partial_x (u f_o c_{o,CO_2.}) = 0, \quad (42)$$

the total hydrogen equation

$$\partial_t (\varphi S_w c_{a,H(1).}) + \partial_x (u f_w c_{a,H(1).}) = 0, \quad (43)$$

the total oxygen equation

$$\partial_t (\varphi S_w c_{a,O(2).}) + 2\partial_t (\varphi S_o c_{o,CO_2.}) + \partial_x (u f_w c_{a,O(2).}) + 2\partial_x (u f_o c_{o,CO_2.}) = 0, \quad (44)$$

and the organic carbon equation

$$\partial_t (\varphi S_o c_{o,C(-4).}) + \partial_x (u f_o c_{o,C(-4).}) = 0, \quad (45)$$

where  $c_{w,j}$  and  $c_{o,j}$  are the mole fractions times the molar density  $\bar{\rho}_w$  in the water and  $\bar{\rho}_o$  oleic phase respectively. The molar density of water is given by

$$\bar{\rho}_w = \frac{1}{\sum_{i=1}^6 x_i \bar{V}_i}, \quad (46)$$

where  $x_i$  is the mole fraction in the solution of component  $i$ , and  $\bar{V}_i$  is the molar volume of component  $i$ .

## Partial molar volume $V_i$ and molar concentration $c$

The partial molar volume is a mol-based ( $n_i$ ) average of the partial molar volume ( $V_i$ ) of each *constituent*.

$$V_A = \partial V / \partial n_A; V_B = \partial V / \partial n_B$$

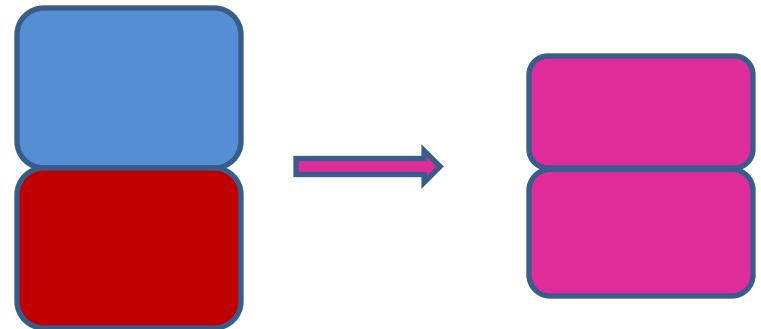
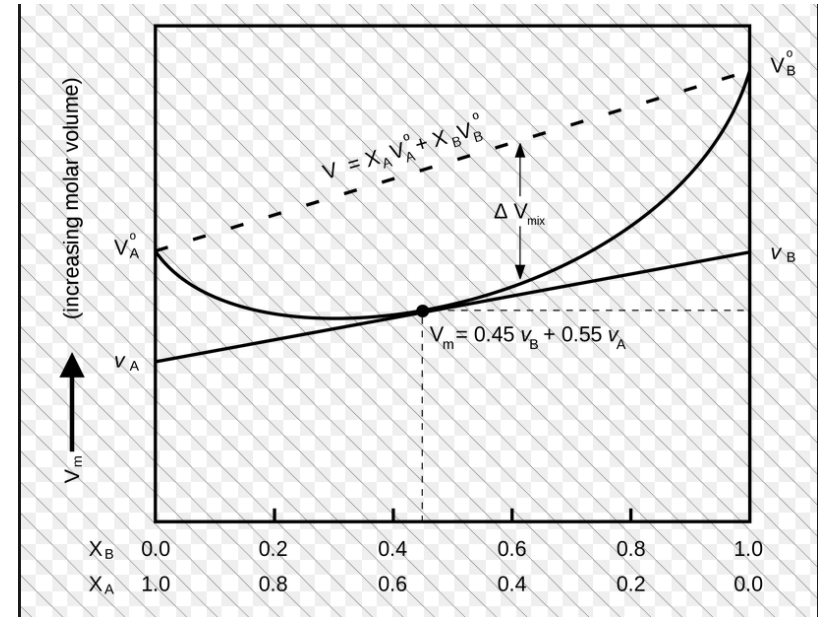
$$dV = \partial V / \partial n_A dn_A + \partial V / \partial n_B dn_B$$

*Gibbs-Duhem:*  $V = V_A n_A + V_B n_B$

$$1 = V_A c_A + V_B c_B = c (V_A x_A + V_B x_B) \rightarrow$$

$$c = 1 / (V_A x_A + V_B x_B)$$

*Generalized:*  $c = 1 / (\sum_i x_i V_i)$



**Partial molar volume  $V_i$**   
**HKF model (see PHREEQC data base)**  
 (Helgeson, Kirkham, Flowers)

There are regression expressions for the partial molar volume of ions in water.  
 At infinite dilution

$$V_i^0 = 41.84 (a_1/10 + 100a_2 / (2600 + P_b) - WQ_{Born} + a_3 / (T_K - 228) + 10000a_4 / ((2600 + Pb) (T_K - 228)))$$

The parameters  $a_i$ ,  $i_i$  are to be found in the data base of Phreeqc, Born constant:  $Q_{Born} = -\partial_p (1/\epsilon_r) = -0.615 \text{e-}06 (\text{/bar})$ .

$$V_k(\mu) - V_k^0 = Z_i^2 A_V \sqrt{\mu} / (1 + {}^\circ a B_\gamma \sqrt{\mu}) + \beta_i \mu^{i4},$$

where  $\mu$  is the ionic strength, and  ${}^\circ a$  is the ionic radius (Angstrom)

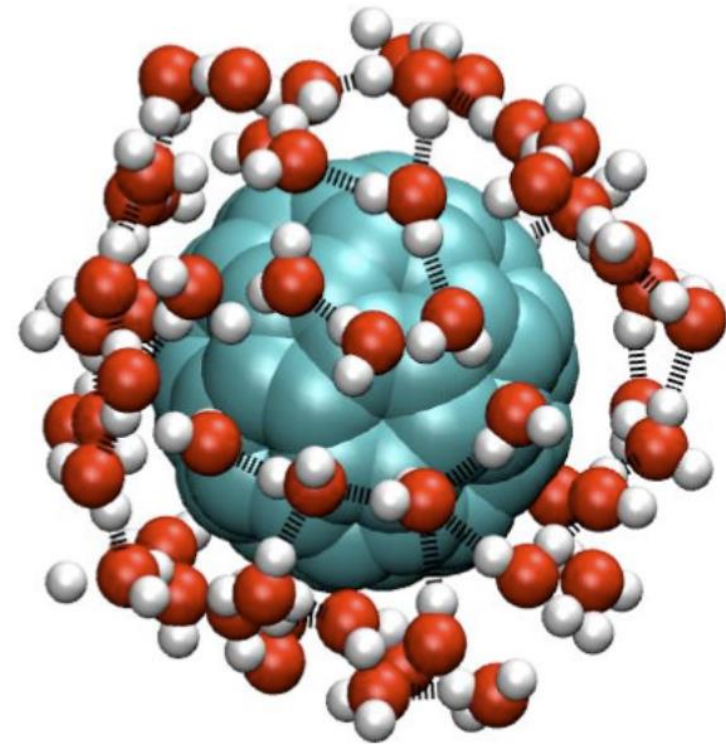
The Debye Limiting slope  $A_V$

$$A_V = (8\pi N_A^4 q_e^6 \rho_0 / (\epsilon_r^3 RT))^{1/2} (\partial_p \ln \epsilon_r - \kappa_0 / 3)$$

$$\beta_i = i_1 + i_2 / (T_K - 228) + i_3 (T_K - 228)$$

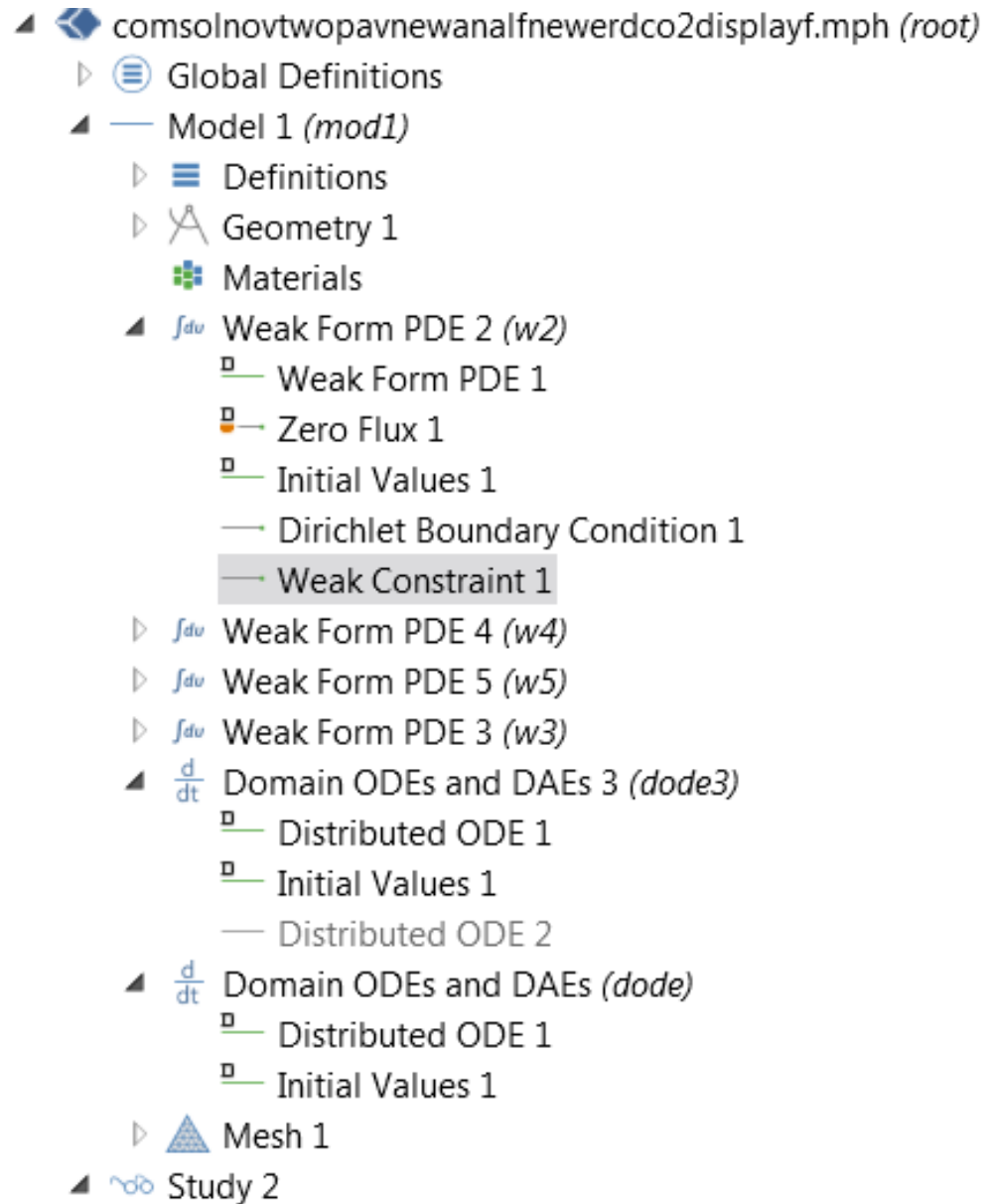
$$B_\gamma = (8\pi N_A q_e^2 \rho_0 / 1000 \epsilon_r k_B T)^{1/2} = 50.29158649 \rho_0^{1/2} / (\epsilon_r T)^{1/2}$$

$N_A$  = Avogadro number,  $q_e = 4.803 \text{e-}10$  is charge of electron (esu),  $\epsilon_r$  relative dielectric constant of water,  $\rho_0$  density of pure water,  $P$  pressure in atm and  $\kappa_0$  is compressibility of pure water



**Use equation based  
software to solve pde's  
and algebraic equations**

- (a) Define constants
- (b) Define concentrations  
with regression  
expressions
- (c) Formulate eqs. in  
weak form
- (d) IC's and BC's
- (e) Define mesh
- (f) Study = solve



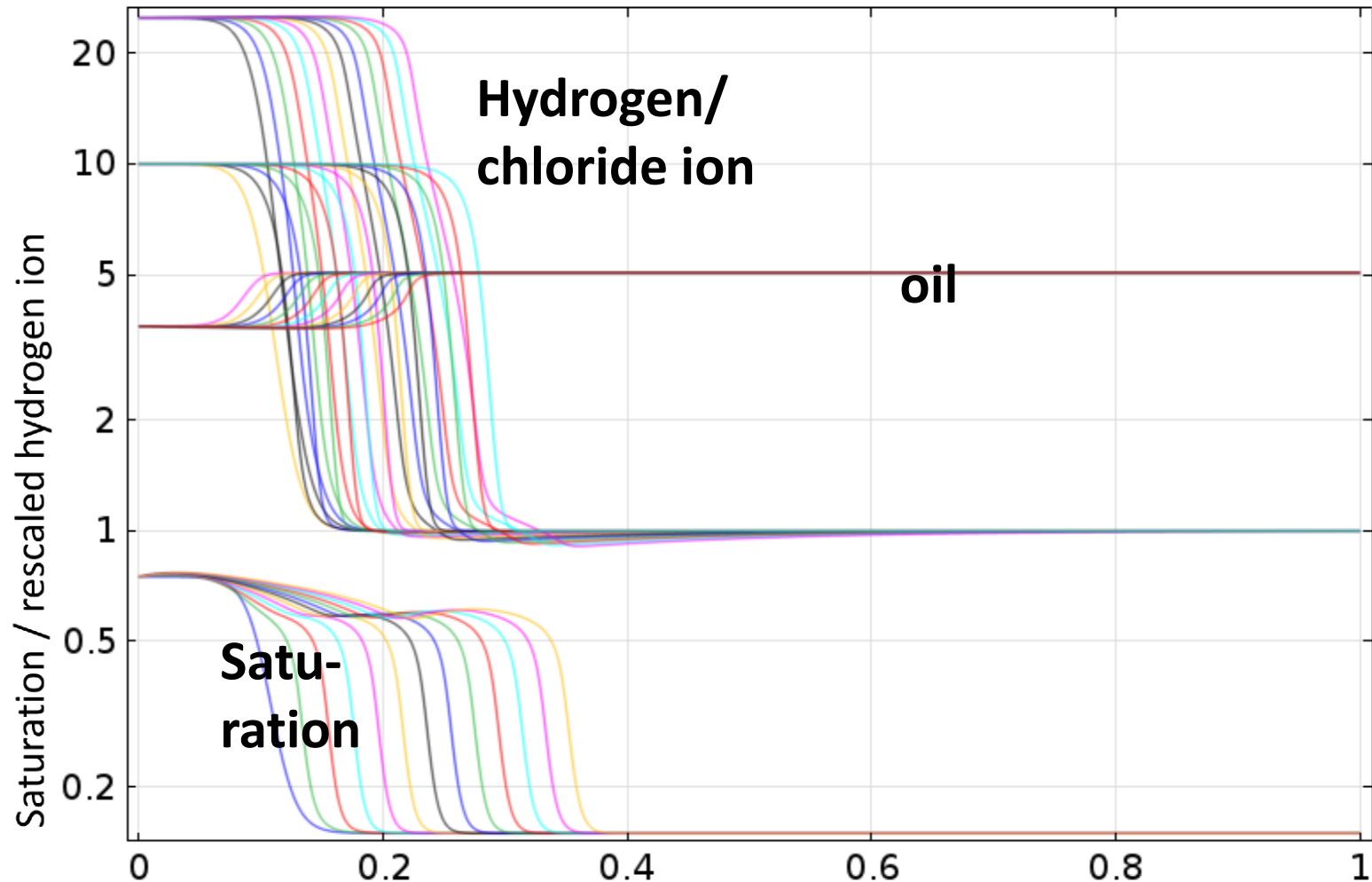
# Eigenvalue analysis

- When we perform an eigenvalue analysis we observe that  $\lambda=0$  is one of the characteristic speeds
- Determination of the eigenvector shows that the corresponding eigenvector is associated with the porosity  $\phi$
- We can conclude that the porosity wave travels with zero speed, i.e. stays at the entrance and therefore a porosity change does not need to be considered.

# Procedure of solving equations

- Determine activities from the equilibrium equations ( $N_f = N_s (=15) - N_r (=8) - N_c (=1) - p (=3) = 3$  (and we use  $[Na] = [Cl]$  as constraint)
- (a) Determine ionic strength from  $\mu = 1/2 \sum c_i z_i^2 = 1/2 \sum a_i / \gamma_i(\mu) z_i^2$ , which is a non-linear algebraic equation
- (b) Express charge equation in terms of concentrations, which is a non-linear algebraic equation
- All concentrations now depend on  $CO_3^{2-}$ ,  $Cl^-$

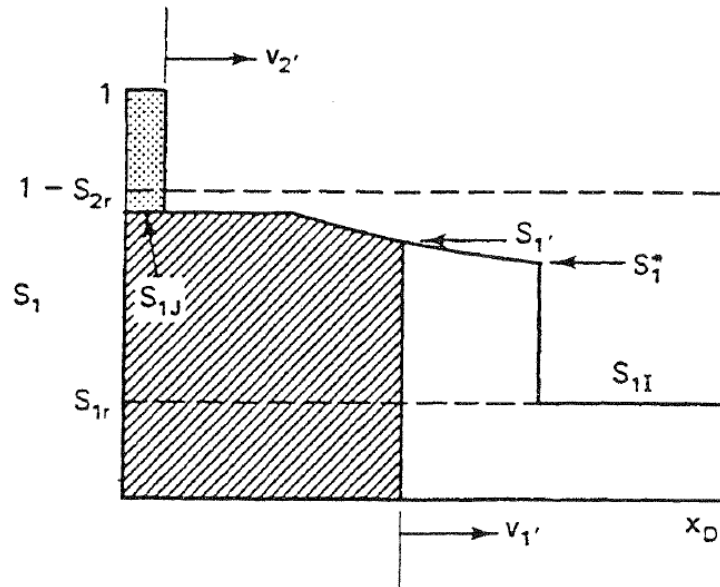
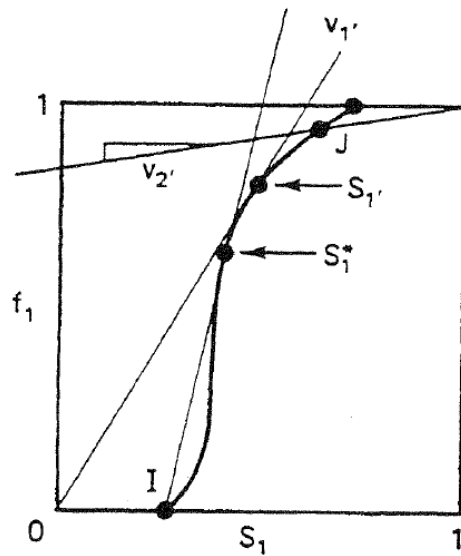
Line Graph: Dependent variable Sw (1)  
Line Graph: AH/(3.0e-5) (1) Line Graph: Cl/2e-5 (1)  
Line Graph: rhomoldecane(log(AH))





# Fractional flow computations

## EOR pp 155



# Conclusions

- **1-Geochemistry can be accounted for by**
  - a- Use of geochemical software to create look-up tables or regression formula; but solutions appear to be unstable
  - b- Simultaneous solution of all relevant equations; appears to have much better performance but validation needed
- **2- Oil recovery predictions require full incorporation of geochemistry**
  - a- Carbon dioxide dissolution depends on ionic strength; geochemical behaviour essential for understanding Low salinity waterflood
  - b- Wetting behaviour depends on surface charges and thus on adsorption of surface complexes and can be found with PHREEQC
    - Ionic strength not the only wetting modifying characteristic
    - Surfactants modify surface behaviour (carboxylic acids)
    - Virtue of water-wet relative permeabilities is not clear
- **3- CO<sub>2</sub> presence is important reason for enhancing oil recovery**
- **Understanding geochemistry is facilitated with the help of the books “EOR” and “Geochemistry and Fluid flow”**
  - The main problem is understanding fluid flow with geochemistry; not the programming

end

**QUESTIONS?**