Course Project: Implementation of MPPT in a CubeSat Electrical Power System Using STM32 and LabVIEW-based PIL Testing

AE 501: Virtual Instrumentation for Aerospace Engineers

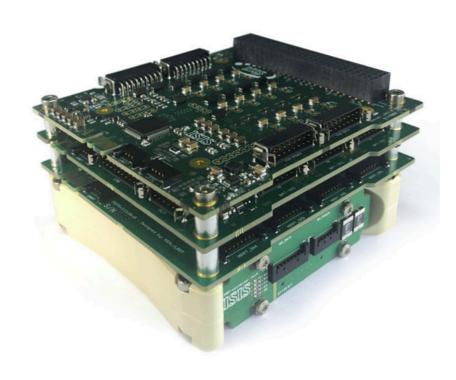
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Under the guidance of: Prof. T. Chandra Sekar



Electrical Power System (EPS): The Lifeline of a CubeSat

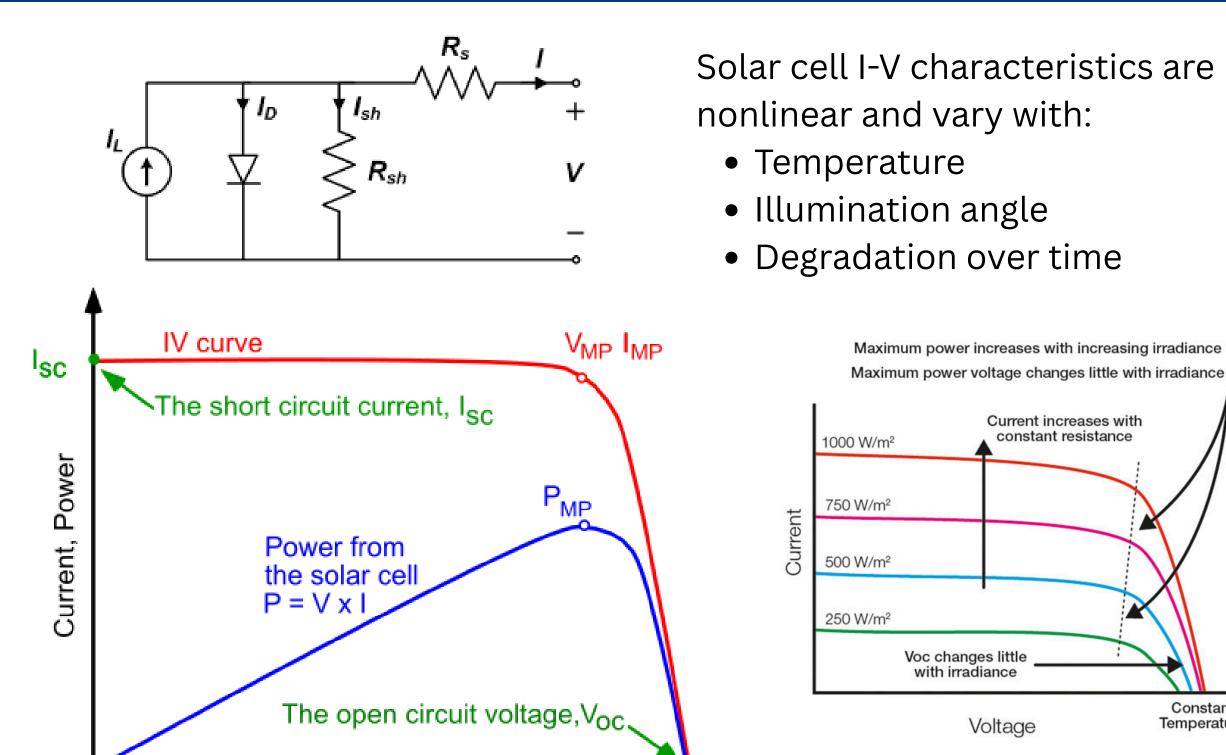




The EPS is crucial in CubeSats as it manages limited power within tight size and weight constraints, ensuring efficient energy use and reliable operation of all subsystems.

- Powers all satellite subsystems: ADCS, OBC, Communications, Payload, etc.
- Limited surface area for solar panels → low power budget
- Must ensure autonomous, reliable, and efficient power regulation
- Failure of EPS = complete mission loss

Solar Cells

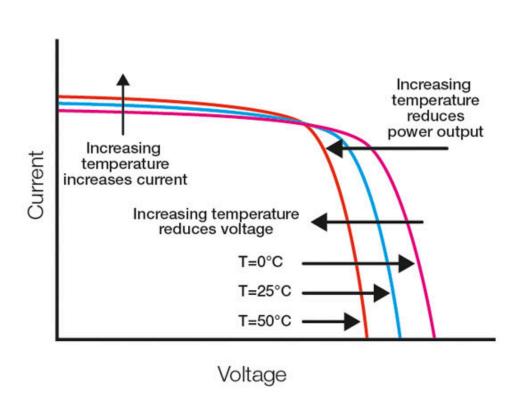


 V_{oc}

Voltage

Solar cell I-V characteristics are nonlinear and vary with:

- Illumination angle
- Degradation over time

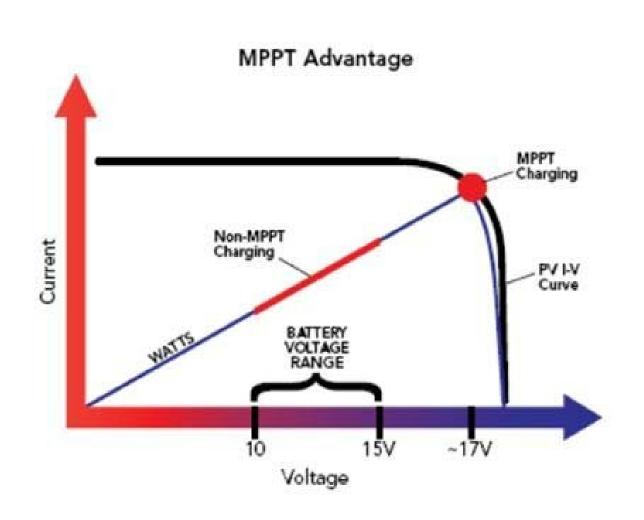


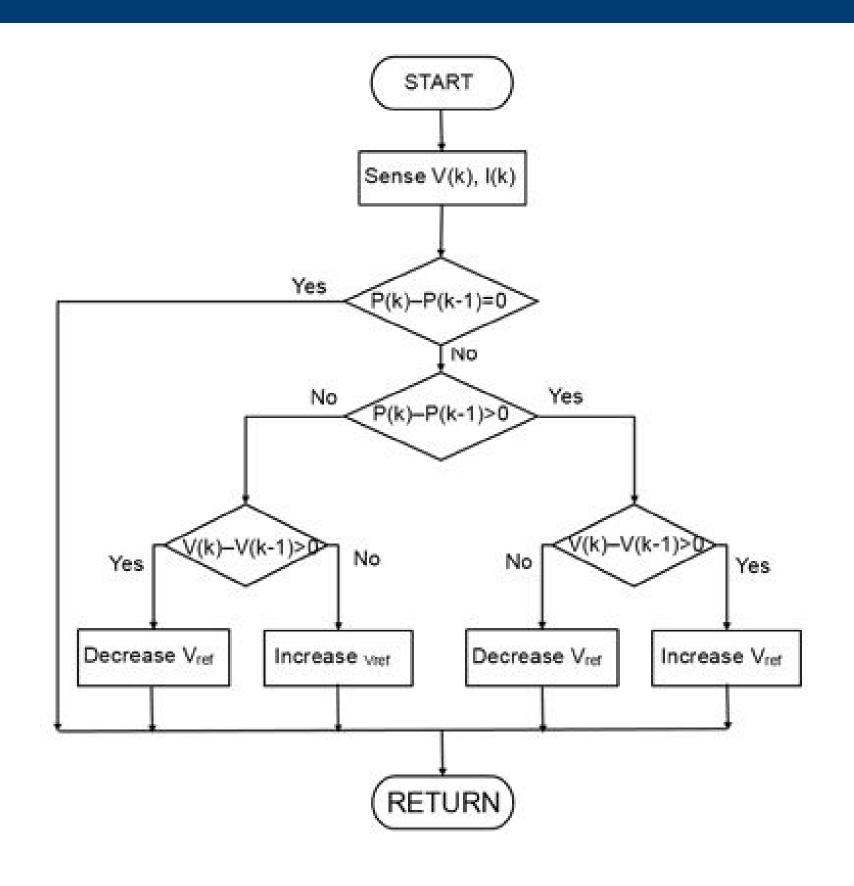
Constant

Temperature

Maximum Power Point Tracking (MPPT)

MPPT is a control technique used in power converters to dynamically adjust their operating point so that the solar panels always deliver the maximum possible power, regardless of environmental conditions



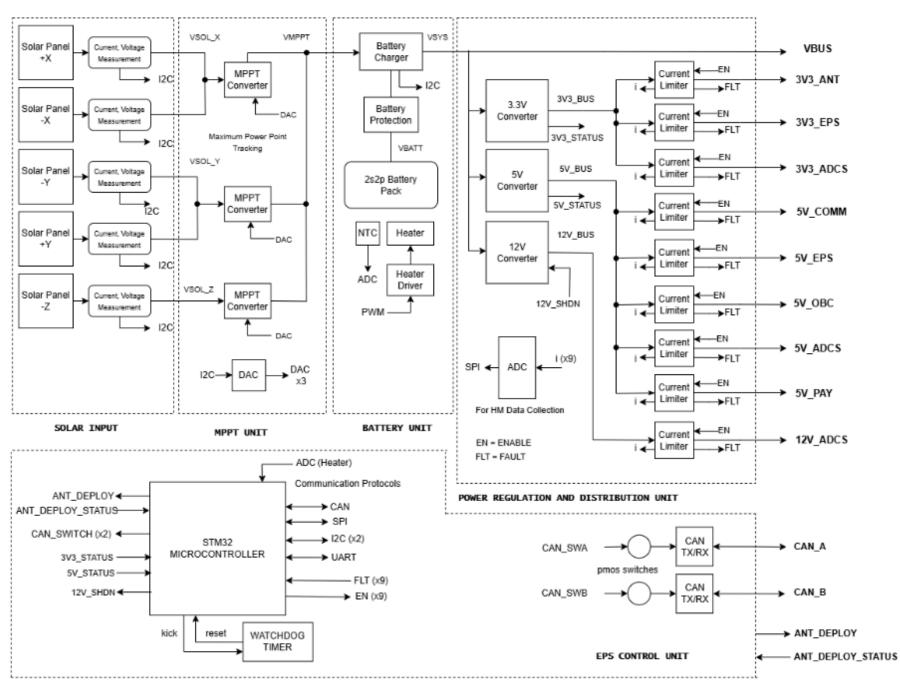


Our Problem

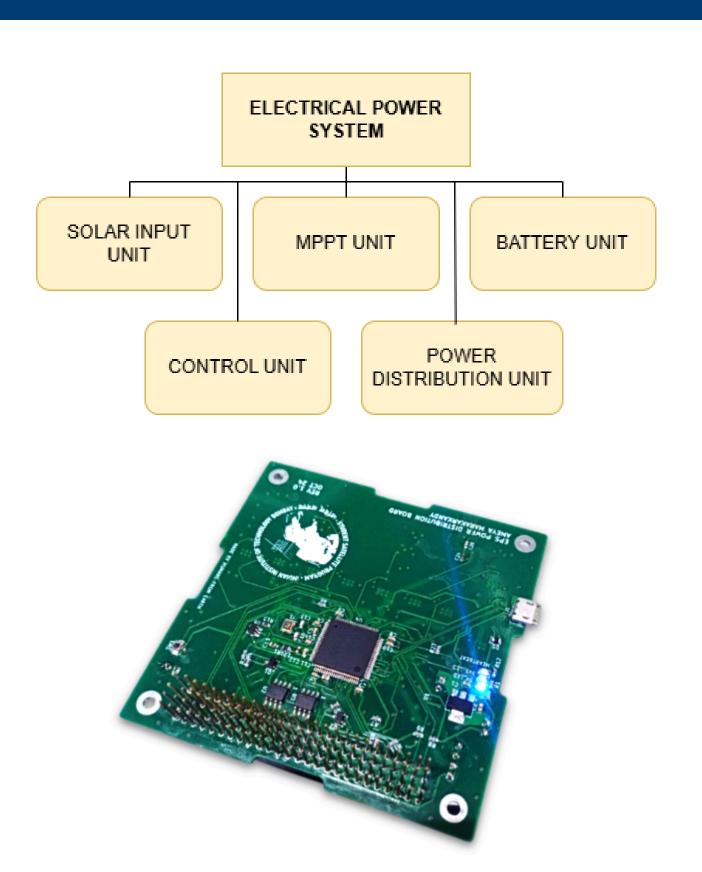
The EPS is crucial in CubeSats as it manages limited power within tight size and weight constraints, ensuring efficient energy use and reliable operation of all subsystems. Orbital conditions cause rapid fluctuations in solar irradiance and temperature, significantly affecting power output. The Maximum Power Point Tracking (MPPT) algorithm optimizes energy extraction from solar arrays under these dynamic conditions. Testing MPPT algorithms directly onboard a satellite introduces significant risks and high costs, necessitating reliable ground-based testing methods.

Processor-In-the-Loop Simulation (PILS) offers a solution by **virtually simulating** orbital conditions or utilizing real sensor data, enabling thorough and cost-effective validation of EPS systems without the risks of physical deployment.

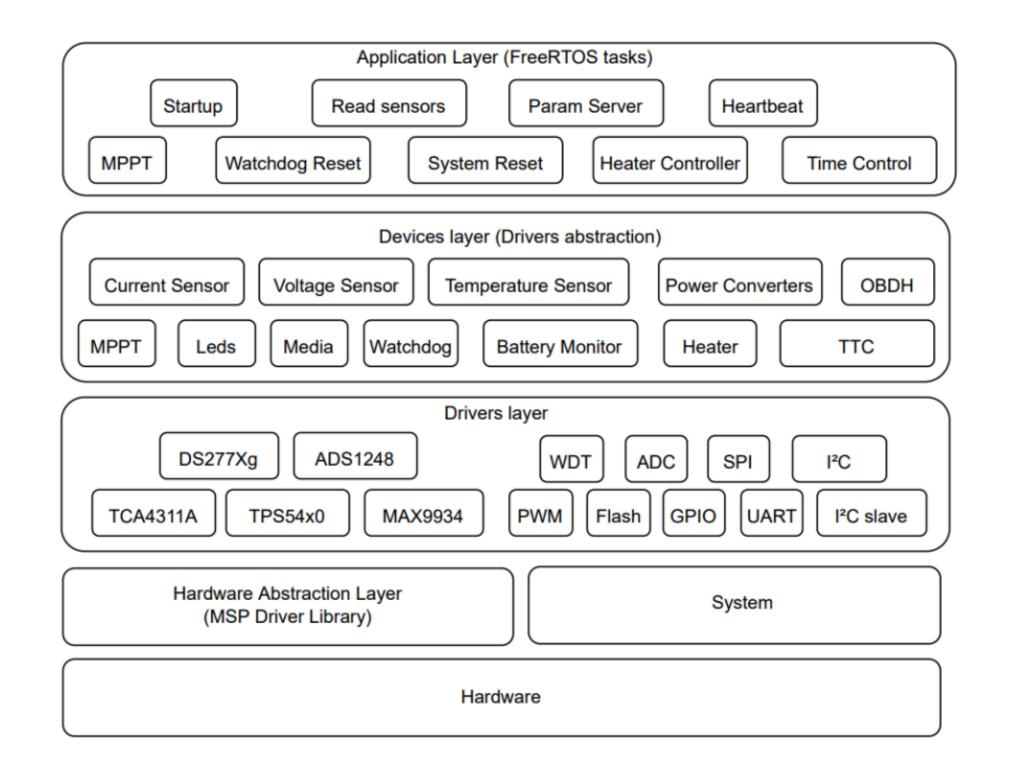
Hardware Architecture



ELECTRICAL POWER SYSTEM ARCHITECTURE



EPS Control Unit



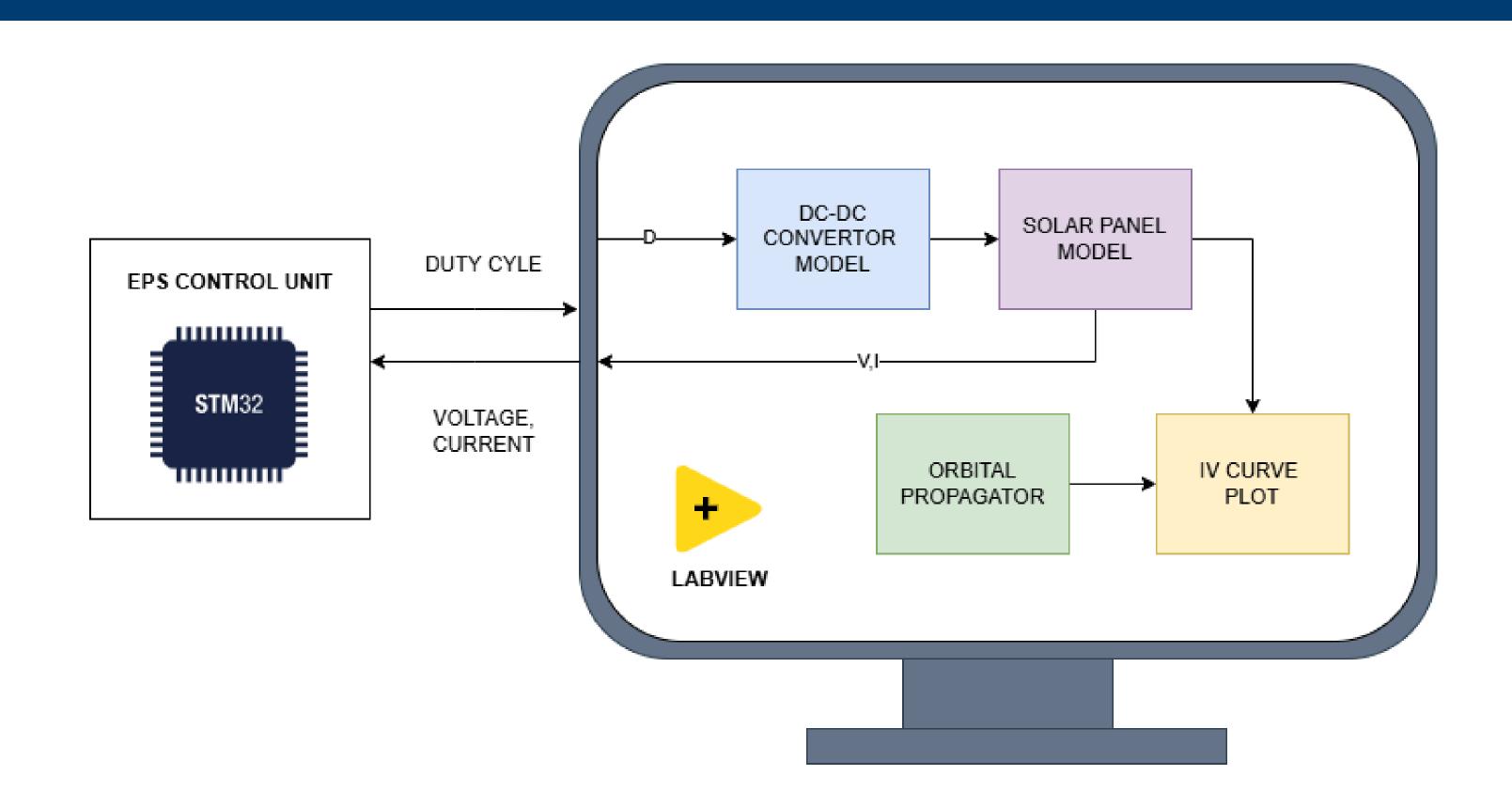
STM32L4767VET6 microcontroller Embedded programming in C/C++ FreeRTOS real time operating system Watchdog timer, RTC, CAN Transceiver, I2C Buffer and other components

Flight software modified for PILS to take sensor reading from serial port instead of INA232 and send duty cycle back to Labview model





PILS ARCHITECTURE



Array Generations for Graph

VOITAGE ARRAY

$$V_i = rac{V_{oc}}{N-1} imes i \quad ext{for } i=0 ext{ to } N-1$$

Where:

- N = number of voltage points (e.g., 100)
- i = current index in the For Loop

Automatically handled in labview using ramp pattern.vi

Array Generations for Graph

- CURRENT CALCULATION
- ullet Case 1: For $V \leq V_{mp}$

$$I(V) = I_{sc} + \left(rac{I_{mp} - I_{sc}}{V_{mp}}
ight) \cdot V$$

ullet Case 2: For $V>V_{mp}$

$$I(V) = I_{mp} + \left(rac{0-I_{mp}}{V_{oc}-V_{mp}}
ight) \cdot (V-V_{mp})$$

• POWER CALCULATION

$$P(V) = V \cdot I(V)$$

Orbital Solar Panel Simulation

• ASSUMPTIONS & GIVEN VALUES

Parameter	Value	Explanation
G_STC	1367 W/m^2	Solar constant (irradiance at standard test conditions)
T_STC	301 K	Cell temperature at STC
β (Beta angle)	O°	Orbit normal is perpendicular to sun vector (simplifies θ calculation)
T_base	260 K	Base satellite cell temperature in shadow
ΔT (rise at full sunlight)	40 K	Estimated heating from full irradiance
α_I	+0.0005 /K	Current temperature coefficient
β_V	-0.0022 V/K	Voltage temperature coefficient

Parameter	Value	Explanation
n	1.2	Diode ideality factor
k	1.380649×10−23 J/K	Boltzmann constant
q	1.602×10 −19 C	Charge of electron
Earth Radius (R_E)	6.371 x 10^6 m	
G (Gravitational Constant)	6.674 x 10^-11	
M (Earth Mass)	5.972 x 10^24	

Orbital Solar Panel Simulation

• ORBITAL PERIOD

$$T=2\pi\sqrt{rac{(R_E+h)^3}{GM}}$$

• SATELLITE SUN ANGLE (θ) OVER TIME

$$heta(t) = \left(rac{360 imes t}{T}
ight) \mod 360$$

$$heta_{
m rad} = heta_{
m deg} imes rac{\pi}{180}$$

• PROJECTED SOLAR IRRADIANCE

Only valid when Sun is in view (i.e., $\theta \in [0^{\circ}, 90^{\circ}] \cup [270^{\circ}, 360^{\circ}]$):

$$G_{ ext{eff}} = G_{ ext{STC}} imes \cos(heta_{ ext{rad}})$$

Otherwise:

$$G_{
m eff}=0$$
 (Eclipse)

Orbital Solar Panel Simulation

• SOLAR CELL TEMPERATURE

$$T_{
m cell} = T_{
m base} + \Delta T \left(rac{G_{
m eff}}{G_{
m STC}}
ight)$$

• IV CHARACTERESTICS

$$I_{sc}(G,T) = I_{sc, ext{STC}} imes \left(rac{G_{ ext{eff}}}{G_{ ext{STC}}}
ight) \left[1 + lpha_I (T_{ ext{cell}} - T_{ ext{STC}})
ight]$$

$$V_{oc}(G,T) = V_{oc, ext{STC}} + eta_V(T_{ ext{cell}} - T_{ ext{STC}}) + rac{nkT_{ ext{cell}}}{q} \ln \left(rac{G_{ ext{eff}}}{G_{ ext{STC}}}
ight)$$

$$I_{mp}(G,T)pprox I_{mp, ext{STC}} imes rac{I_{sc}(G,T)}{I_{sc, ext{STC}}}$$

$$V_{mp}(G,T)pprox V_{mp, ext{STC}} imes rac{V_{oc}(G,T)}{V_{oc, ext{STC}}}$$

Labview Program

