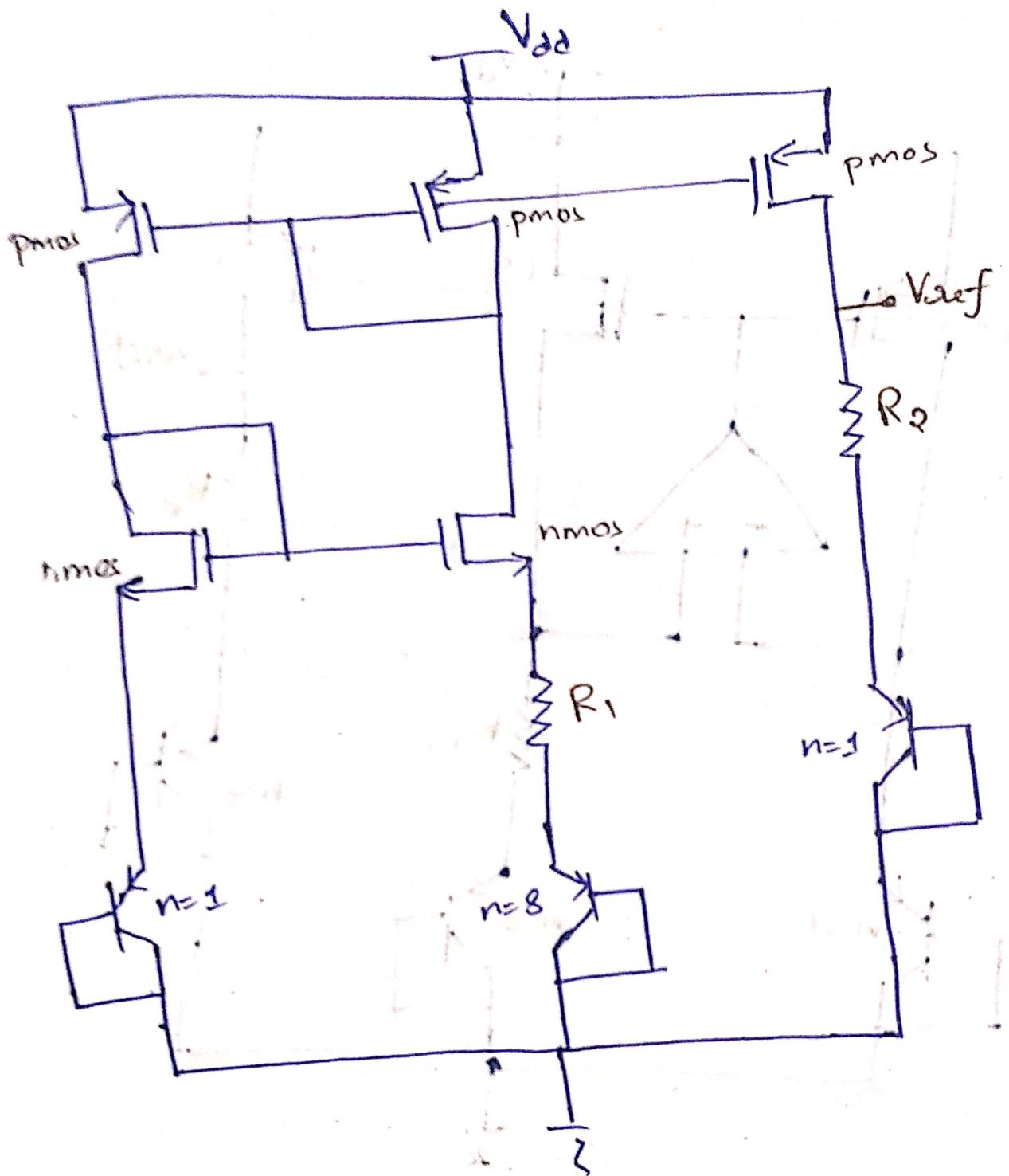


BGR with OP-amp

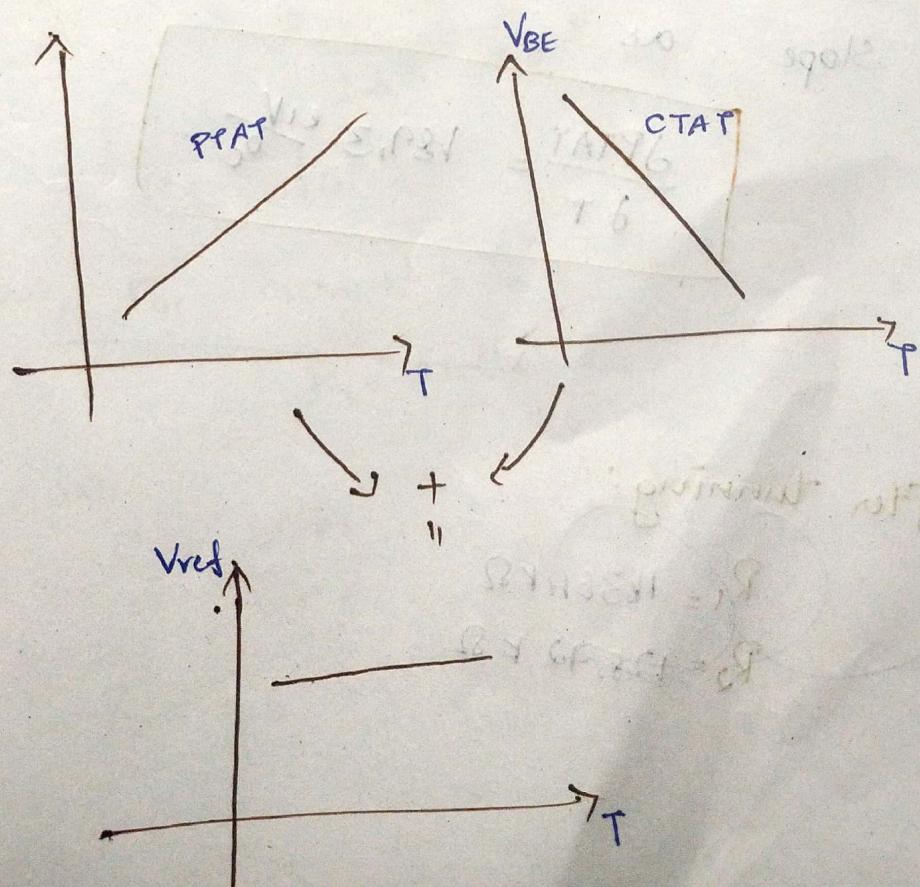


BGR with current mirror

Design:-

→ To achieve temperature independence, BGR circuit rely on two temperature-dependent voltage components.

- 1) PTAT:- This component increases linearly with temperature and is typically derived from the thermal voltage of BJT.
- 2) CTAT:- This component decreases linearly with temperature and is generated using the base-emitter voltage of BJT.



For CTAT slope :-

- The slope of CTAT is derived from simulating test circuit 1
- we are using Umc180 nm technology

$$\frac{\partial V_{BE}}{\partial T} = -1.938 \text{ mV/}^{\circ}\text{C}$$

For PTAT slope :-

- we have taken multiplier, n=5
- For this we have plotted $V_{BE} - V_{BEN}$ with varying temperature,
- From this we have found out the slope as

$$\frac{\partial PTAT}{\partial T} = 189.3 \text{ uV/}^{\circ}\text{C}$$

→ Now we need to adjust PTAT such that it gets cancelled with CTAT using R_1 , R_2 .

Now

$$V_{out} = \frac{R_2}{R_1} \underbrace{\ln n V_T}_{\text{PTAT}} + \underbrace{V_{BE}}_{\text{CTAT}}$$

diff w.r.t Temperature.

$$\frac{\partial V_{out}}{\partial T} \Rightarrow \cancel{\alpha_1} \frac{\partial P}{\partial T}$$

$$0 = \alpha_1 \frac{\partial \text{PTAT}}{\partial T} + \frac{\partial V_{BE}}{\partial T}$$

$$\alpha_1 = \frac{-\frac{\partial V_{BE}}{\partial T}}{\frac{\partial \text{PTAT}}{\partial T}}$$

$$= \frac{1.938 \times 10^{-3}}{1.893 \times 10^{-6}}$$

$$\alpha_1 = 10.23$$

now, For current, $I_0 = 5 \mu A$

$$R_1 = 11.36 k\Omega$$

now,

$$R_2 = \frac{\alpha_1 R_1}{\ln 8} = \frac{11.36 \times 10.23}{\ln 8}$$

$$R_2 = 128.72 k\Omega$$

After tuning :-

For current mirror based BGR :-

$$R_1 = 13.22 \text{ k}\Omega$$

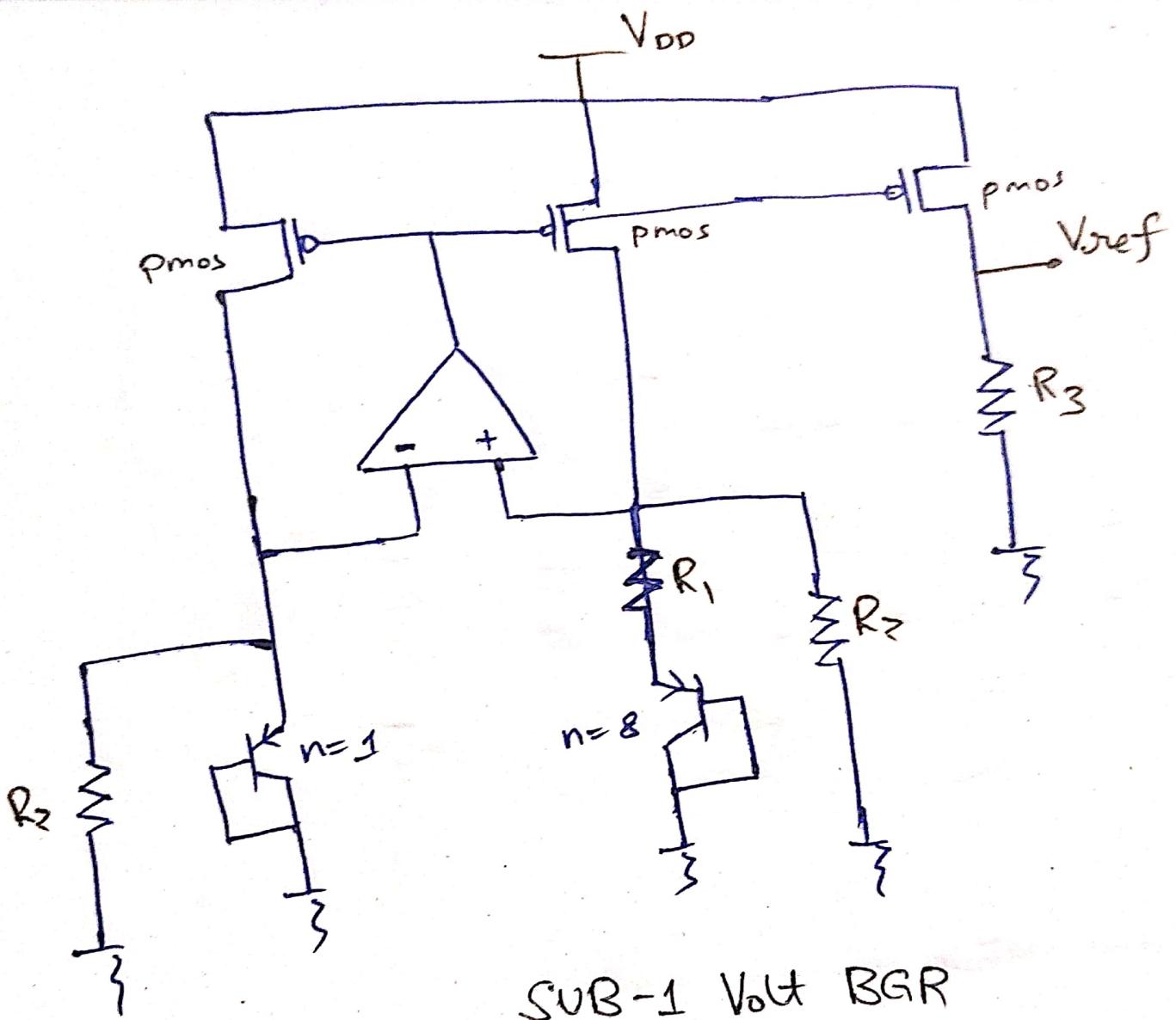
$$R_2 = 118.87 \text{ k}\Omega$$

For op-amp based BGR :-

$$R_1 = 11.36 \text{ k}\Omega$$

$$R_2 = 110.9 \text{ k}\Omega$$





SUB-1 Volt BGR

Design of Sub 1 Volt BGR using op-amp based BGR:-

For normal opamp based BGR

$$V_{out} = V_{BE} + \frac{R_2}{R_1} V_T \ln(n).$$

For Sub 1 Volt BGR,

$$V_{out} = \frac{R_3}{R_2} \left(V_{BE} + \frac{R_2}{R_1} V_T \ln(n) \right).$$

$$= \frac{R_3}{R_2} V_{out} \Big|_{op-amp}$$

For $V_{out} = 0.75V$

$$0.75 = \frac{R_3}{R_2} (1.25)$$

$$R_3 = \frac{0.75}{1.25} \times 110.9 \text{ k}\Omega$$

$$R_3 = 66.54 \text{ k}\Omega$$

After tuning :-

$$R_1 = 12 \text{ k}\Omega$$

$$R_2 = 111.2 \text{ k}\Omega$$

$$R_3 = 68 \text{ k}\Omega$$