

ChE-381: Process Dynamics and Control

Simulation Session 6

Problem statement

Consider the three noninteracting tanks in series shown in Figure 1 with feedback control.

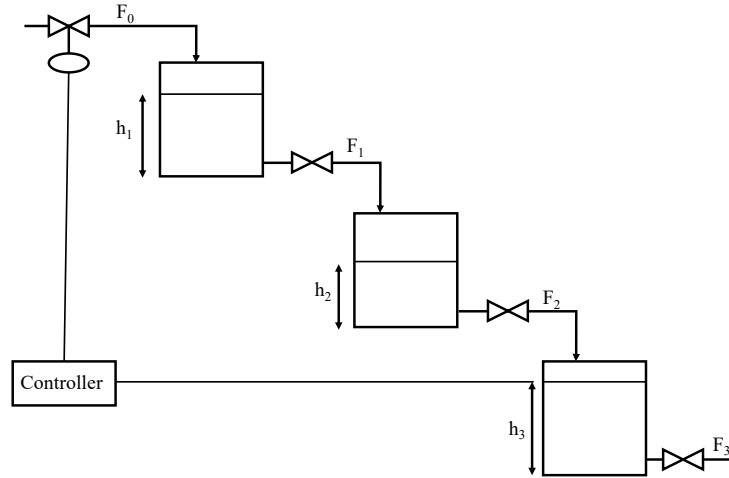


Figure 1. Three non-interacting tanks in series with feedback controller.

A linear model for the liquid level h_i of each tank will take the form:

$$\begin{aligned} A_1 \frac{dh_1}{dt} &= F_0 - c_1 h_1 \\ A_2 \frac{dh_2}{dt} &= c_1 h_1 - c_2 h_2 \\ A_3 \frac{dh_3}{dt} &= c_2 h_2 - c_3 h_3 \end{aligned}$$

where A_i and c_i represent the cross-section area and the outlet valve discharge constant for each tank. Defining deviation variables and taking Laplace transform, we get:

$$H'_3(s) = \frac{K}{(\tau_1 s + 1)(\tau_2 s + 1)(\tau_3 s + 1)} F'_0(s)$$

We observe that h_3 is measured and F_0 is adjusted by the controller. Assume that $K = 6$, $\tau_1 = 2$, $\tau_2 = 4$, and $\tau_3 = 6$.

- Tune PI controller using the following methods: robust response time, Skogestad IMC, and Zeigler-Nichols step response. Compute your performance metric used in lab 5 for the tuned PI controller. Which method performs the best in terms of performance metrics?
- Tune PI controller obtained using Skogestad IMC and Zeigler-Nichols further to reduce your performance metric while ensuring the poles of closed loop transfer function remains sufficiently in the left half plane.
- Show the response plot with the PI controller obtained in (b) and PID parameters obtained in the previous lab in the **same figure**. Ensure that the figure is well labeled, and legend is clear.

Submit a zipped folder containing a .txt file containing the solution of parts (a) and (b), and the simulink file for part (c). Name the folder as your roll number.