1 MODEL SETUP

A bulk energy and mass balance model is used to calculate the amounts of ice, meltwater, water vapour and runoff water of the AIR every hour. This model consists of four modules which estimates the AIR, a) geometric evolution , b) energy balance, c) surface temperature and d) mass balance.

1.1 Geometric evolution

Radius r^i_{ice} and height h^i_{ice} define the dimensions of the AIR assuming its geometry to be a cone. The surface area A^i exposed to the atmosphere and volume V^i are:

$$A = \pi \cdot r_{ice} \cdot \sqrt{{r_{ice}}^2 + {h_{ice}}^2} \tag{1}$$

$$V = \pi/3 \cdot {r_{ice}}^2 \cdot h_{ice} \tag{2}$$

Note that we do not specify the time step superscript i of the shape variables A, V, r_{ice} and h_{ice} for brevity. The equations used henceforth display model time step superscript i only if it is different from the current time step.

With the mass of the AIR M_{ice}, its current volume can also be expressed as:

$$V = M_{ice}/\rho_{ice} \tag{3}$$

where ρ_{ice} is the density of ice (917 $kg\, m^{-3}$).

The influence of the AIR fountain is parameterised by the fountain water temperature T_w and its spray radius r_{spray}. The initial radius r_0 of the AIR is assumed to be r_{spray}. The initial height h_0 depends on the dome volume V_{dome} used to construct the AIR as follows:

$$h_0 = \Delta x + \frac{3 \cdot V_{dome}}{\pi r^2_{spray}} \tag{4}$$

where Δx is the surface layer thickness (defined in Section 1.2)

During subsequent time steps, the dimensions of the AIR evolve assuming a uniform ice formation and decay across its surface area with an invariant slope $s_{cone} = \frac{h_{ice}}{r_{ice}}$. During these time steps, the volume is parameterised using Eqn. 2 as:

$$V = \frac{\pi \cdot {r_{ice}}^3 \cdot s_{cone}}{3} \tag{5}$$

However, the Icestupa cannot outgrow the maximum range of the water droplets ($(r_{ice})_{max} = r_F$). Combining equations 2, 3 and 5, the geometric evolution of the Icestupa at each time step i can be determined by considering the following rules:

$$(r_{ice},\, h_{ice}) = \begin{cases} (r_{spray},\, h_0) & if\, i = 0 \\ (r^{i-1}_{ice},\, \frac{3 \cdot M_{ice}}{\pi \cdot \rho_{ice} \cdot (r^{i-1}_{ice})^2}) & if\, r^{i-1}_{ice} \geq r_F \text{ and } \Delta M_{ice} > 0 \text{ where } \Delta M_{ice} = M^{i-1}_{ice} - M^{i-2}_{ice} \\ (\frac{3 \cdot M_{ice}}{\pi \cdot \rho_{ice} \cdot s_{cone}})^{1/3} \cdot (1,\, s_{cone}) & otherwise \end{cases} \tag{6}$$

1.2 Energy Balance

The energy balance equation (Hock, 2005) for the AIR is formulated as follows:

$$q_{SW} + q_{LW} + q_L + q_S + q_F + q_G = q_{surf} \tag{7}$$

where q_{surf} is the surface energy flux in $[W\, m^{-2}]$; q_{SW} is the net shortwave radiation; q_{LW} is the net longwave radiation; q_L and q_S are the turbulent latent and sensible heat fluxes. q_F represents the heat exchange of the fountain water droplets with the AIR ice surface. q_G represents ground heat flux between Icestupa surface and Icestupa interior. Energy transferred in the direction of the ice surface is always denoted as positive and away as negative.

Equation 7 is usually referred to as the energy budget for “the surface”, but practically it must apply to a surface layer of ice with a finite thickness Δx. The energy flux acts upon the Icestupa surface layer which has an upper and a lower boundary defined by the atmosphere and the ice body of the Icestupa, respectively. The parameter selection for Δx is based on the following two arguments: (a) the ice thickness Δx should be small enough to represent the surface temperature variations every model time step Δt and (b) Δx should be large enough for these temperature variations to not reach the bottom of the surface layer. Therefore, we introduced a 20 mm thick surface layer for a model time step of 1 hour, over which the energy balance is calculated. A sensitivity analysis was later performed to understand the influence of this factor. Here, we define the surface temperature T_{ice} to be the modelled average temperature of the Icestupa surface layer and the energy flux q_{surf} is assumed to act uniformly across the Icestupa area A.

1.2.1 Net Shortwave Radiation q_{SW}

The net shortwave radiation q_{SW} is computed as follows:

$$q_{SW} = (1 - \alpha) \cdot (SW_{direct} \cdot f_{cone} + SW_{diffuse}) \tag{8}$$

where SW_{direct} and $SW_{diffuse}$ are the ERA5 direct and diffuse short wave radiation, α is the modelled albedo and f_{cone} is the area fraction of the ice structure exposed to the direct shortwave radiation.

We model the albedo using a scheme described in Oerlemans and Knap (1998). The scheme records the decay of albedo with time after fresh snow is deposited on the surface. δt records the number of time steps after the last snowfall event. After snowfall, albedo changes over a time step, δt , as

$$\alpha = \alpha_{ice} + (\alpha_{snow} - \alpha_{ice}) \cdot e^{(-\delta t)/\tau} \tag{9}$$

where α_{ice} is the bare ice albedo value (0.35), α_{snow} is the snow ice albedo value (0.85) and τ is a decay rate, which determines how fast the albedo of the ageing snow reaches this value. The decay rate τ is assumed to have a base value of 10 days similar to values obtained by Schmidt et al. (2017) for wet surfaces and its maximal value is set based on observations by Oerlemans and Knap (1998) as shown in Table 1.

Furthermore, the albedo α varies depending on the water source that formed the current Icestupa surface. Correspondingly, the albedo is reset to the value of bare ice albedo if the fountain is spraying water onto the current ice surface and to the value of fresh snow albedo if a snowfall event occurred. Snowfall events are assumed if the air temperature is below $T_{ppt} = 1°C$ (Fujita and Ageta, 2000).

The area fraction f_{cone} of the ice structure exposed to the direct shortwave radiation depends on the shape considered. The direct solar radiation incident on the AIR surface is first decomposed into horizontal and vertical components using the solar elevation angle θ_{sun}. For a conical shape, half of the total curved surface is exposed to the vertical component of the direct shortwave radiation and the projected triangle of the curved surface is exposed to the horizontal component of the direct shortwave radiation. The solar elevation angle θ_{sun} used is modelled using the parametrisation proposed by Woolf (1968). Accordingly, f_{cone} is determined as follows:

$$f_{cone} = \frac{(0.5 \cdot r_{ice} \cdot h_{ice}) \cdot cos\theta_{sun} + (\pi \cdot {r_{ice}}^2/2) \cdot sin\theta_{sun}}{\pi \cdot r_{ice} \cdot ({r_{ice}}^2 + {h_{ice}}^2)^{1/2}} \tag{10}$$

The ERA5 diffuse shortwave radiation is assumed to impact the conical Icestupa surface uniformly.

1.2.2 Net Longwave Radiation q_{LW}

The net longwave radiation q_{LW} is determined as follows:

$$q_{LW} = LW_{in} - \sigma \cdot \epsilon_{ice} \cdot (T_{ice} + 273.15)^4 \tag{11}$$

where T_a represents the measured air temperature, T_{ice} is the modelled surface temperature, both temperatures are given in [$°C$], $\sigma = 5.67 \cdot 10^{-8}\ Jm^{-2}s^{-1}K^{-4}$ is the Stefan-Boltzmann constant, LW_{in} denotes the incoming longwave radiation derived from the ERA5 dataset and ϵ_{ice} is the corresponding emissivity value for the Icestupa surface (see Table 1).

1.2.3 Turbulent sensible q_S and latent q_L heat fluxes

The turbulent sensible q_S and latent heat q_L fluxes are computed with the following expressions proposed by Garratt (1992):

$$q_S = c_a \cdot \rho_a \cdot p_a/p_{0,a} \cdot \frac{\kappa^2 \cdot v_a \cdot (T_a - T_{ice})}{(\ln \frac{h_{AWS}}{z_{ice}})^2} \tag{12}$$

$$q_L = 0.623 \cdot L_s \cdot \rho_a/p_{0,a} \cdot \frac{\kappa^2 \cdot v_a(p_{v,a} - p_{v,ice})}{(\ln \frac{h_{AWS}}{z_{ice}})^2} \tag{13}$$

where h_{AWS} is the measurement height above the ground surface of the AWS (in m), v_a is the wind speed in [$m\,s^{-1}$], c_a is the specific heat of air at constant pressure (1010 J $kg^{-1}K^{-1}$), ρ_a is the air density at standard sea level (1.29 kgm^{-3}), $p_{0,a}$ is the air pressure at standard sea level (1013 hPa), κ is the von Karman constant (0.4), L_s is the heat of sublimation (2848 $kJ\,kg^{-1}$) and z_{ice} (1.7 mm) denotes the roughness length of ice (momentum and scalar). The vapor pressures over air ($p_{v,a}$) and ice ($p_{v,ice}$) was obtained using the following formulation given in WMO (2018):

$$p_{v,a} = 6.107 \cdot 10^{(7.5 \cdot T_a/(T_a+237.3))}$$
$$p_{v,ice} = (1.0016 + 3.15 \cdot 10^{-6} \cdot p_a - 0.074 \cdot p_a^{-1}) \cdot (6.112 \cdot e^{(22.46 \cdot T_{ice}/(T_{ice}+272.62))}) \tag{14}$$

where p_a is the measured air pressure in $[hPa]$.

1.2.4 Fountain water heat flux q_F

The interaction between the fountain water and the ice surface is taken into account by assuming that the ice surface temperature remains constant at $0\ °C$ during time steps when the fountain is active. This process can be divided into two simultaneous steps: (a) the water temperature T_{water} is cooled to $0\ °C$ and (b) the ice surface temperature is warmed to $0\ °C$. Process (a) transfers the necessary energy for process (b) throughout the fountain runtime. We further assume that this process is instantaneous, i.e. the ice temperature is immediately set to $0\ °C$ within just one time step Δt when the fountain is switched on. Thus, the heat flux caused by the fountain water is calculated as follows:

$$q_F = \begin{cases} 0 & \textit{if}\ \Delta M_F = 0 \\ \frac{\Delta M_F \cdot c_{water} \cdot T_{water}}{\Delta t \cdot A} + \frac{\rho_{ice} \cdot \Delta x \cdot c_{ice} \cdot T_{ice}}{\Delta t} & \textit{if}\ \Delta M_F > 0 \end{cases} \tag{15}$$

with c_{ice} as the specific heat of ice.

1.2.5 Bulk Icestupa heat flux q_G

The bulk Icestupa heat flux q_G corresponds to the ground heat flux in normal soils and is caused by the temperature gradient between the surface layer (T_{ice}) and the ice body (T_{bulk}). It is expressed by using the heat conduction equation as follows:

$$q_G = k_{ice} \cdot (T_{bulk} - T_{ice})/l_{ice} \tag{16}$$

where k_{ice} is the thermal conductivity of ice ($2.123\ W\,m^{-1}\,K^{-1}$) , T_{bulk} is the mean temperature of the ice body within the Icestupa and l_{ice} is the average distance of any point in the surface to any other point in the ice body. T_{bulk} is initialised as $0\ °C$ and later determined from Eqn. 16 as follows:

$$T_{bulk}^{i+1} = T_{bulk} - (q_G \cdot A \cdot \Delta t)/(M_{ice} \cdot c_{ice}) \tag{17}$$

Since AIR's typically have conical shapes with $r_{ice} >> h_{ice}$, we assume that the center of mass of the ice body is near the base of the fountain. Thus, the distance of every point in the AIR surface layer from the ice body's center of mass is between h_{ice} and r_{ice}. So we calculate q_G here assuming $l_{ice} = (r_{ice} + h_{ice})/2$.

1.3 Surface temperature

The available energy q_{surf} can act on the surface of the AIR to a) change its temperature, b) melt ice or c) freeze ice. So Eqn. 7 can be rewritten as:

$$q_{surf} = q_{freeze/melt} + q_T \tag{18}$$

where q_T, q_{freeze} and q_{melt} represent energy associated with process (a), (b) and (c) respectively.

To distribute the surface energy flux into these three components, we categorize the model time steps as freezing or melting events. Freezing events can only occur if there is fountain water available and the

Table 1. Free parameters in the model categorised as constant, uncertain and site parameters. Base value (B) and uncertainty (U) were taken from the literature. For assumptions (assum.), the uncertainty was chosen to be relatively large (5 %). For measurements (meas.), the uncertainty due to parallax errors is chosen to be (1 %).

Constant Parameters	Symbol	Value		References
Van Karman constant	κ	0.4		B: Cuffey and Paterson
Stefan Boltzmann constant	σ	$5.67 \cdot 10^{-8} W\, m^{-2}\, K^{-4}$		B: Cuffey and Paterson
Air pressure at sea level	$p_{0,a}$	1013 hPa		B: Mölg and Hardy
Density of water	ρ_w	1000 $kg\, m^{-3}$		B: Cuffey and Paterson
Density of ice	ρ_{ice}	917 $kg\, m^{-3}$		B: Cuffey and Paterson
Density of air	ρ_a	1.29 $kg\, m^{-3}$		B: Mölg and Hardy
Specific heat of ice	c_{ice}	2097 $J\, kg^{-1}\, {}^{\circ}C^{-1}$		B: Cuffey and Paterson
Specific heat of water	c_w	4186 $J\, kg^{-1}\, {}^{\circ}C^{-1}$		B: Cuffey and Paterson
Specific heat of air	c_a	1010 $J\, kg^{-1}\, {}^{\circ}C^{-1}$		B: Mölg and Hardy
Thermal conductivity of ice	k_{ice}	2.123 $W\, m^{-1}\, K^{-1}$		B: Bonales et al.
Latent Heat of Sublimation	L_s	2848 $kJ\, kg^{-1}$		B: Cuffey and Paterson
Latent Heat of Fusion	L_f	334 $kJ\, kg^{-1}$		B: Cuffey and Paterson
Uncertain Parameters			**Range**	
Precipitation Temperature threshold	T_{ppt}	1 °C	$\pm\, 1\, {}^{\circ}C$	B + U: Fujita and Ageta, Zhou et al.
Ice Emissivity	ϵ_{ice}	0.95	[0.949,0.993]	B: Cuffey and Paterson; U: Hori et al.
Ice Albedo	α_{ice}	0.35	± 5 %	B: Cuffey and Paterson; U: assum.
Snow Albedo	α_{snow}	0.85	± 5 %	B: Cuffey and Paterson; U: assum.
Albedo Decay Rate	τ	10 days	$[1, 22]\, days$	B: Schmidt et al.; U: Oerlemans and Knap
Surface layer thickness	Δx	20 mm	$[1, 10]\, mm$	assum.
Fountain Parameters			**Range**	
Spray Radius	r_{spray}		± 5 %	
Water temperature	T_{water}	$1 {}^{\circ}C$	$[0, 5]\, {}^{\circ}C$	

surface energy flux is negative. But just these two conditions are not sufficient as the latent heat energy can only contribute to temperature fluctuations. So to prevent latent heat energy from turning a melting event into a freezing event an additional condition namely $(q_{surf} - q_L) < 0$ is required. Thus, freezing and melting events are identified as follows:

$$q_{freeze/melt} = \begin{cases} q_{freeze} & \textit{if } \Delta M_F > 0 \textit{ and } q_{surf} < 0 \textit{ and } (q_{surf} - q_L) < 0 \\ q_{melt} & \textit{otherwise} \end{cases} \tag{19}$$

During a freezing event, the available energy $(q_{surf} - q_L)$ can either be sufficient or insufficient to freeze the fountain water available. If insufficient, the additional energy further cools down the surface temperature. So the surface energy flux distribution during a freezing event can be represented as:

$$(q_{freeze}, q_T) = \begin{cases} (q_{surf} - q_L, q_L) & \mathit{if}\ \Delta M_F \geq -\frac{(q_{surf}-q_L)A\cdot\Delta t}{L_f} \\ (\frac{\Delta M_F\cdot L_f}{A\cdot\Delta t}, q_{surf} + \frac{\Delta M_F\cdot L_f}{A\cdot\Delta t}) & \mathit{if}\ \Delta M_F < -\frac{(q_{surf}-q_L)A\cdot\Delta t}{L_f} \end{cases} \tag{20}$$

During a melting event, the surface energy flux (q_{surf}) is first used to change the surface temperature to T_{temp} calculated as:

$$T_{temp} = \frac{q_{surf}\cdot\Delta t}{\rho_{ice}\cdot c_{ice}\cdot\Delta x} + T_{ice} \tag{21}$$

If $T_{temp} > 0°C$, then energy is reallocated from q_T to q_{melt} to maintain surface temperature at melting point. So the surface energy flux distribution during a melting event can be represented as:

$$(q_{melt}, q_T) = \begin{cases} (0, q_{surf}) & \mathit{if}\ T_{temp} < 0 \\ (\frac{T_{temp}\cdot\rho_{ice}\cdot c_{ice}\cdot\Delta x}{\Delta t}, q_{surf} - \frac{T_{temp}\cdot\rho_{ice}\cdot c_{ice}\cdot\Delta x}{\Delta t}) & \mathit{if}\ T_{temp} > 0 \end{cases} \tag{22}$$

1.4 Mass Balance

The mass balance equation for an AIR is represented as:

$$\frac{\Delta M_F + \Delta M_{ppt} + \Delta M_{dep}}{\Delta t} = \frac{\Delta M_{ice} + \Delta M_{water} + \Delta M_{sub} + \Delta M_{runoff}}{\Delta t} \tag{23}$$

where M_F is the discharge of the fountain; M_{ppt} is the cumulative precipitation; M_{dep} is the cumulative accumulation through water vapour deposition; M_{ice} is the cumulative mass of ice; M_{water} is the cumulative mass of melt water; M_{sub} represents the cumulative water vapor loss by sublimation and M_{runoff} represents the fountain discharge runoff that did not interact with the AIR. The LHS of equation 23 represents the rate of mass input and the RHS represents the rate of mass output for an AIR.

Precipitation input is calculated as shown in equation 24a where ρ_w is the density of water (1000 $kg\,m^{-3}$), ppt is the measured precipitation rate in $[m\,s^{-1}]$ and T_{ppt} is the temperature threshold below which precipitation falls as snow. Here, snowfall events were identified using T_{ppt} as $1°C$. Snow mass input is calculated by assuming a uniform deposition over the entire circular footprint of the Icestupa.

The latent heat flux is used to estimate either the evaporation and condensation processes or sublimation and deposition processes as shown in equation 24b. During time steps at which surface temperature is below 0 $°C$ only sublimation and deposition can occur, but if the surface temperature reaches 0 $°C$, evaporation and condensation can also occur. As the differentiation between evaporation and sublimation (and condensation and deposition) when the air temperature reaches 0 $°C$ is challenging, we assume that negative (positive) latent heat fluxes correspond only to sublimation (deposition), i.e. no evaporation (condensation) is calculated.

Since we have categorized every time step as a freezing and melting event, we can determine the meltwater and ice generated using the associated energy fluxes as shown in equations 24c and 24d. Having calculated all the other mass components the fountain wastewater generated every time step can be calculated using equation 24e.

$$\frac{\Delta M_{ppt}}{\Delta t} = \begin{cases} \pi \cdot {r_{ice}}^2 \cdot \rho_w \cdot ppt & \textit{if}\, T_a < T_{ppt} \\ 0 & \textit{if}\, T_a \geq T_{ppt} \end{cases} \tag{24a}$$

$$(\frac{\Delta M_{dep}}{\Delta t}, \frac{\Delta M_{sub}}{\Delta t}) = \begin{cases} \frac{q_L \cdot A}{L_s} \cdot (1, 0) & \textit{if}\, q_L \geq 0 \\ \frac{q_L \cdot A}{L_s} \cdot (0, -1) & \textit{if}\, q_L < 0 \end{cases} \tag{24b}$$

$$\frac{\Delta M_{water}}{\Delta t} = \frac{q_{melt} \cdot A}{L_f} \tag{24c}$$

$$\frac{\Delta M_{ice}}{\Delta t} = \frac{q_{freeze} \cdot A}{L_f} + \frac{\Delta M_{ppt}}{\Delta t} + \frac{\Delta M_{dep}}{\Delta t} - \frac{\Delta M_{sub}}{\Delta t} - \frac{\Delta M_{melt}}{\Delta t} \tag{24d}$$

$$\frac{\Delta M_{runoff}}{\Delta t} = \frac{\Delta M_F - \Delta M_{ice}}{\Delta t} \tag{24e}$$

Considering AIRs as water reservoirs, we can quantify their potential through the amount of water they store (storage quantity) and the length of time they store it (storage duration). Another means of comparing different Icestupas is through their water storage efficiency defined accordingly as:

$$\textit{Storage Efficiency} = \frac{M_{water}}{(M_F + M_{ppt} + M_{dep})} \cdot 100 \tag{25}$$

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