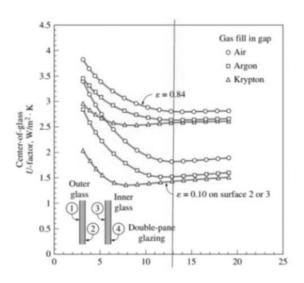
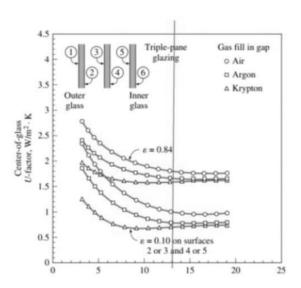
Task 1

Panel with air gap 13mm	U-Value	Effect %
D-Pg air between N-	2.80	0%
coating		
D-P argon N-coating	2.65	5%
D-P krypton N-coating	2.60	7%
D-P air coating IP	1.80	36%
D-P argon coating IP	1.55	45%
D-P krypton coating IP	1.40	50%
T-P air no-coating	1.80	36%
T-P argon no-coating	1.65	41%
T-P krypton no-coating	1.53	45%
T-P air coating IP	1.00	64%
T-P argon coating IP	0.8	71%
T-P air coating IP	1.00	64%
T-P argon coating IP	0.8	71%
T-P krypton coating IP	0.70	75%





Task 2

 $Q_{heating_window_{west}} = HF_{window_{west}} \times A_{window_{west}}$

 $HF_{window_{west}} = U_{window_{west}} \times \Delta T_{heating} = 2.84 \times 24.8 \approx 70.44 \frac{W}{m2}$

 $Q_{heating_window_{west}} = 70.44 \times 14.4 \approx 1014.34 W$

 $Q_{cooling_window_{west}} = \mathit{CF}_{window_{west}} \times A_{window_{west}}$

 $CF_{window_{west}} = U_{window_{west}} \left(\Delta T_{cooling} - 0.46DR \right) + PXI_{window_{west}} \times SHGC_{window_{west}} \times IAC_{window_{west}} \times FF_{3\ window_{west}} \right)$

= 2.84 (7.9 - 0.46 × 11.9) + 747 × 0.54 × 1 × 0.56
$$\approx$$
 226 $\frac{W}{m2}$
$$Q_{cooling} = 190 \times 14.4 \approx 3255 W$$

$$Q_{heating_window_{south-f}} = HF_{window_{south-f}} \times A_{window_{south-f}}$$

$$HF_{window south-f} = U_{window south-f} \times \Delta T_{heating}$$

$$= 2.84 \times 24.8 \approx 70.44 \frac{W}{m2}$$

$$Q_{heating_window_{south-f}} = 70.44 \times 3.6 \approx 254 W$$

$$Q_{cooling_window_{south-f}} = CF_{window_{south-f}} \times A_{window_{south-f}}$$

$$CF_{window_{south-f}} = U_{window_{south-f}} (\Delta T_{cooling} - 0.46DR) +$$

$$PXI_{window_{south-f}} \times SHGC_{window_{south-f}} \times IAC_{window_{south-f}} \times$$

FF₃
$$window_{south-f} = 2.84 (7.9 - 0.46 \times 11.9) + 557 \times 0.54 \times 1 \times 0.47 \approx 149 \frac{W}{m2}$$

 $Q_{cooling} = 149 \times 3.6 = 536.4 W$

$$Q_{heating_window_{south-o}} = HF_{window_{south-o}} \times A_{window_{south-o}}$$

$$HF_{window_{south-o}} = U_{window_{south-o}} \times \Delta T_{heating} = 2.87 \times 24.8 \approx 71.2 \frac{W}{m^2}$$

$$Q_{heating_window_{south-f}} = 71.2 \times 3.6 \approx 257 W$$

$$Q_{cooling_window_{south-o}} = CF_{window_{south-o}} \times A_{window_{south-o}}$$

$$CF_{window\,south-o} = U_{window\,south-o} \left(\Delta T_{cooling} - 0.46DR \right) + PXI_{window\,south-o} \times SHGC_{window\,south-o} \times IAC_{window\,south-o} \times FF_{3\,window\,south-o} \right)$$

$$= 2.87 \left(7.9 - 0.46 \times 11.9 \right) + 557 \times 0.46 \times 1 \times 0.47 \approx 127.43 \frac{w}{m^2} \qquad Q_{cooling} = 127.43 \times 3.6 = 458.8 \, W$$

The values for Aluminum frames:

$$Q_{heating_window_{west}} = HF_{window_{west}} \times A_{window_{west}}$$

$$HF_{window_{west}} = U_{window_{west}} \times \Delta T_{heating} = 3.61 \times 24.8 \approx 90 \frac{w}{m^2}$$

$$Q_{heating_window_{west}} = 90 \, \times 14.4 \approx 1300 \, W$$

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Q_{cooling\_window_{west}} = CF_{window_{west}} \times A_{window_{west}}
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$$CF_{window_{west}} = U_{window_{west}}$$
 ($\Delta T_{cooling}$ - 0.46DR) + $PXI_{window_{west}} \times SHGC_{window_{west}} \times IAC_{window_{west}} \times FF_{3\ window_{west}}$

= 3.61 (7.9 - 0.46 × 11.9) + 747 × 0.56 × 1 × 0.56
$$\approx$$
 243 $\frac{W}{m^2}$

$$Q_{cooling} = 190~\times 14.4 \approx 3500~W$$

$$Q_{heating_window_{south-f}} = HF_{window_{south-f}} \times A_{window_{south-f}}$$

$$HF_{window_{south-f}} = U_{window_{south-f}} \times \Delta T_{heating}$$

$$= 3.61 \times 24.8 \approx 90 \frac{W}{m^2}$$

$$Q_{heating_window_{south-f}} = 90 \times 3.6 \approx 324 W$$

$$Q_{cooling_window_{south-f}} = CF_{window_{south-f}} \times A_{window_{south-f}}$$

$$CF_{window\,south-f} = U_{window\,south-f} \left(\Delta T_{cooling} \text{- 0.46DR} \right) + PXI_{window\,south-f} \times SHGC_{window\,south-f} \times IAC_{window\,south-f} \times \text{FF}_{3\,\,window\,south-f} \times \text{FF}_{3\,\,window\,south-$$

= 3.61 (7.9 - 0.46 × 11.9) + 557 × 0.56 × 1 × 0.47
$$\approx$$
 155.4 $\frac{W}{m2}$

$$Q_{cooling} = 155.4 \times 3.6 \approx 560 \; W$$

$$Q_{heating_window_{south-o}} = \mathit{HF}_{window_{south-o}} \times A_{window_{south-o}}$$

$$HF_{window_{south-o}} = U_{window_{south-o}} \times \Delta T_{heating}$$

$$= 4.62 \times 24.8 \approx 114.58 \frac{W}{m2}$$

$$Q_{heating_window_{south-f}} = 114.58 \times 3.6 \approx 413 W$$

$$Q_{cooling_window_{south-o}} = CF_{window_{south-o}} \times A_{window_{south-o}}$$

$$CF_{window\,south-o} = U_{window\,south-o} \left(\Delta T_{cooling} \text{- } 0.46DR \right) + \\ PXI_{window\,south-o} \times SHGC_{window\,south-o} \times IAC_{window\,south-o} \times \text{FF}_{3\,\,window\,south-o} \right) + \\ PXI_{window\,south-o} \times SHGC_{window\,south-o} \times IAC_{window\,south-o} \times \text{FF}_{3\,\,window\,south-o} \times \text$$

= 4.62 (7.9 - 0.46 × 11.9) + 557 × 0.55 × 1 × 0.47
$$\approx$$
 155.21 $\frac{W}{m^2}$

$$Q_{cooling} = 155.21 \times 3.6 = 559 W$$