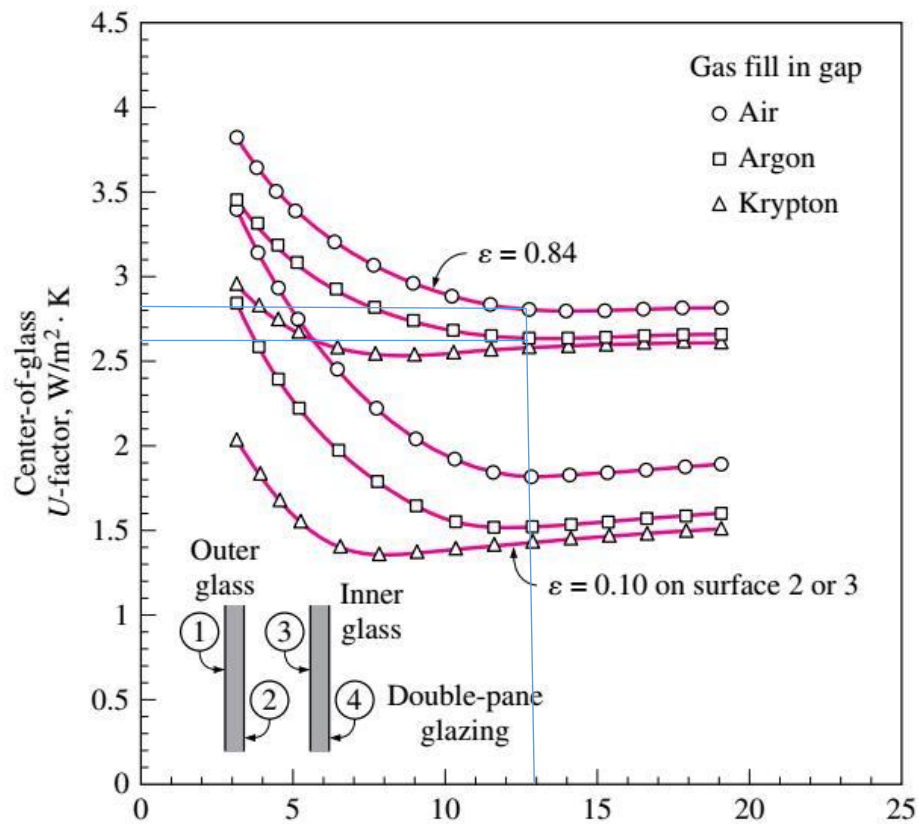
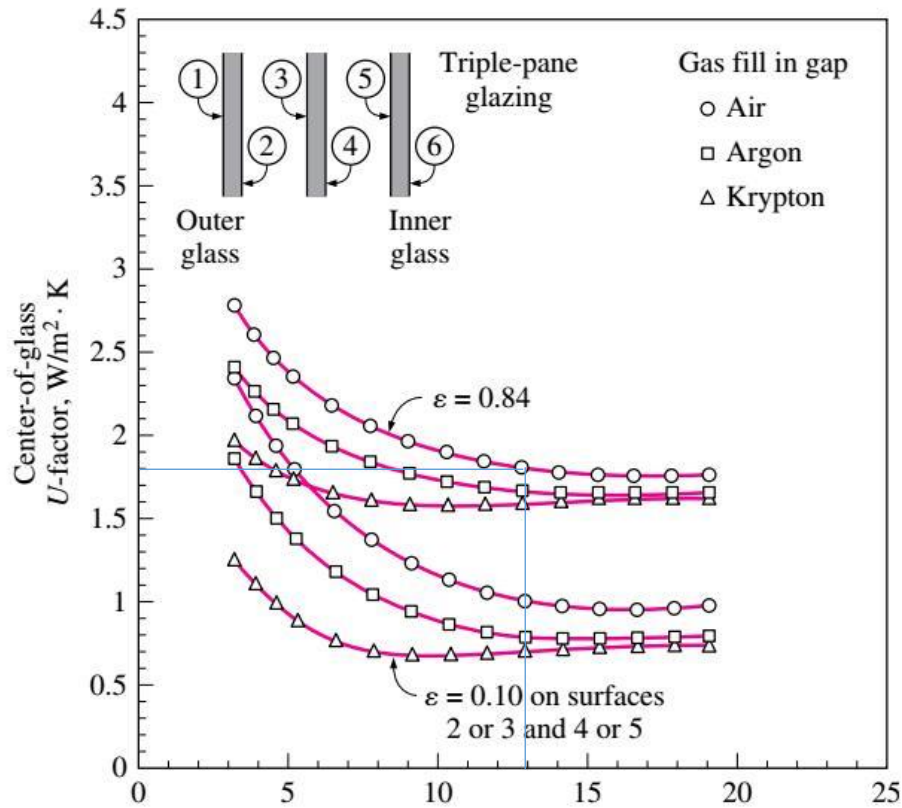


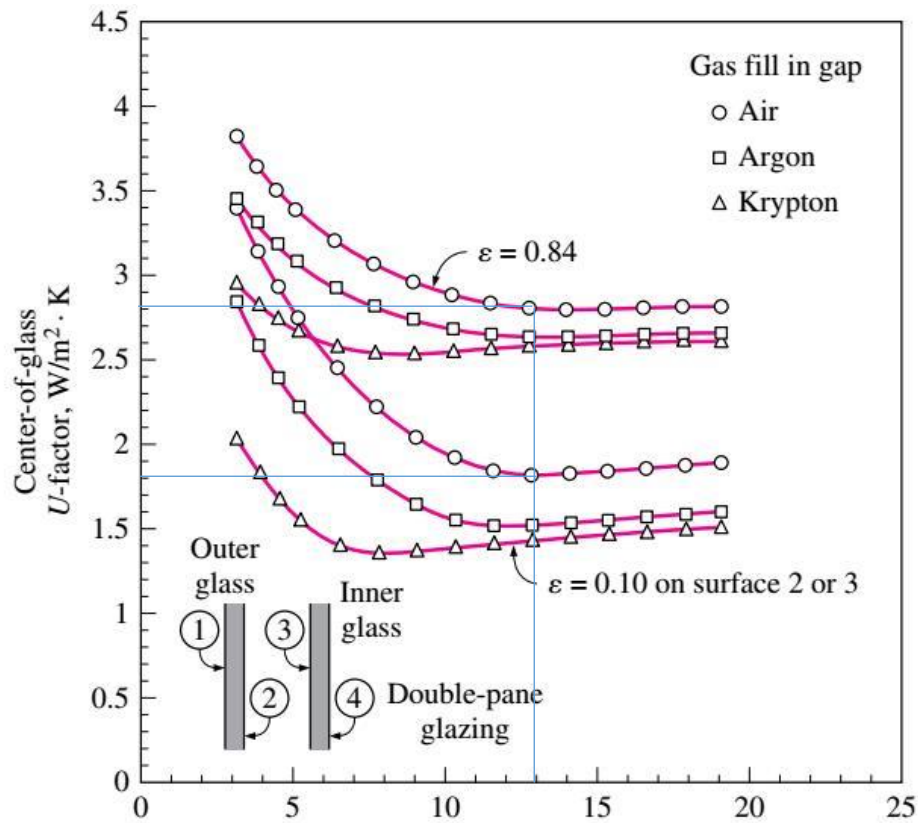
## Task 1:



- 1) Changing the gas:** When we change the gas from air to Argon, the Center-of-glass U-factor changes from 2.8  $W/m^2 \cdot K$  to 2.6  $W/m^2 \cdot K$ ,  $(2.8 - 2.6) / 2.8 = 7.1\%$ . So the U-factor decreased by 7.1%



- 2) **Adding an extra pane:** When we add an extra pane, the Center-of-glass U-factor changes from  $2.8 W/m^2 K$  to  $1.8 W/m^2 K$ ,  $(2.8-1.8)/2.8=35.7\%$ . So the U-factor decreased by 35.7%



- 3) **Using a low emissivity coating:** When we use a low emissivity coating (from  $\epsilon=0.84$  to  $\epsilon=0.1$ ), the Center-of-glass U-factor changes from  $2.8 W/m^2 K$  to  $1.8 W/m^2 K$ ,  $(2.8-1.8)/2.8=35.7\%$ . So the U-factor decreased by 35.7%

## Task 2:

### 1) The cooling load of the fixed 14.4 m<sup>2</sup> window on the West:

$$CF_{window_{west}heatTrasnferPart} = U_{window_{west}} (\Delta T_{cooling} - 0.46 DR)$$

$$= 2.84 (7.9 - 0.46 * 11.9) = 6.9 \frac{W}{m^2}$$

$$PXI_{window_{west}} = E_D + E_d = 559 + 188 = 747$$

$$SHGC = 0.54$$

No internal shading so IAC = 1

From the table for west window of a detached house FFs = 0.56

$$CF_{window_{west}IrradiationPart} = PXI \times SHGC \times IAC \times FF_s = 747 * 0.54 * 1 * 0.56$$

$$= 225.9 \frac{W}{m^2}$$

$$CF_{window_{west}} = CF_{window_{west}heatTrasnferPart} + CF_{window_{west}IrradiationPart} =$$

$$6.9 + 225.9 = 232.8 \frac{W}{m^2}$$

$$Q_{window_{west}} = CF_{window_{west}} \times A_{window_{west}} = 232.8 * 14.4 = 3352.3 W$$

### The heating load of the fixed 14.4 m<sup>2</sup> window on the West:

$$U_{window_{west}} = 2.84 \frac{W}{m^2 K}$$

$$HF_{window_{west}} = U_{window_{west}} \times \Delta T_{heating} = 2.84 * 24.8 = 70.4 \frac{W}{m^2}$$

$$Q_{window_{west}} = HF_{window_{west}} \times A_{window_{west}} = 70.4 * 14.4 = 1014.2 W$$

### When we change the frame of the window from wooden to aluminum:

$$U_{window_{west}} = 3.61 \frac{W}{m^2}, SHGC = 0.54$$

$$\text{Cooling load } Q_{window_{west}} = CF_{window_{west}} \times A_{window_{west}} = 3499.5 W$$

$$\text{Heating load } Q_{window_{west}} = HF_{window_{west}} \times A_{window_{west}} = 1289.2 W$$

**2) The cooling load of the fixed 3.6 m<sup>2</sup> window on the South:**

$$CF_{window_{south}heatTrasnferPart} = U_{window_{south}} (\Delta T_{cooling} - 0.46 DR)$$

$$= 2.84 (7.9 - 0.46 * 11.9) = 6.9 \frac{W}{m^2}$$

$$PXI_{window_{south}} = E_D + E_d = 348 + 209 = 557$$

$$SHGC = 0.55$$

No internal shading so IAC = 1

$$FFs = 0.47$$

$$CF_{window_{south}IrradiationPart} = PXI \times SHGC \times IAC \times FF_S = 557 * 0.55 * 1 * 0.47$$

$$= 144.0 \frac{W}{m^2}$$

$$CF_{window_{south}} = CF_{window_{south}heatTrasnferPart} + CF_{window_{south}IrradiationPart} =$$

$$6.9 + 144.0 = 150.9 \frac{W}{m^2}$$

$$Q_{window_{south}} = CF_{window_{south}} \times A_{window_{south}} = 150.9 * 3.6 = 543.2 W$$

**The heating load of the fixed 3.6 m<sup>2</sup> window on the South:**

$$U_{window_{south}} = 2.84 \frac{W}{m^2 K}$$

$$HF_{window_{south}} = U_{window_{south}} \times \Delta T_{heating} = 2.84 * 24.8 = 70.4 \frac{W}{m^2}$$

$$Q_{window_{south}} = HF_{window_{south}} \times A_{window_{south}} = 70.4 * 3.6 = 253.4 W$$

**When we change the frame of the window from wooden to aluminum:**

$$U_{window_{south}} = 3.61 \frac{W}{m^2}, SHGC = 0.56$$

$$\text{Cooling load } Q_{window_{south}} = CF_{window_{south}} \times A_{window_{south}} = 559.4 W$$

$$\text{Heating load } Q_{window_{south}} = HF_{window_{south}} \times A_{window_{south}} = 322.3 W$$

### 3) The cooling load of the operable 3.6 m<sup>2</sup> window on the South:

$$CF_{window_{south}heatTrasnferPart} = U_{window_{south}} (\Delta T_{cooling} - 0.46 DR)$$

$$= 2.87 (7.9 - 0.46 * 11.9) = 7.0 \frac{W}{m^2}$$

$$PXI_{window_{south}} = E_D + E_d = 348 + 209 = 557$$

$$SHGC = 0.46$$

No internal shading so IAC = 1

$$FFs = 0.47$$

$$CF_{window_{south}IrradiationPart} = PXI \times SHGC \times IAC \times FF_S = 557 * 0.46 * 1 * 0.47$$

$$= 120.4 \frac{W}{m^2}$$

$$CF_{window_{south}} = CF_{window_{south}heatTrasnferPart} + CF_{window_{south}IrradiationPart} =$$

$$7.0 + 120.4 = 127.4 \frac{W}{m^2}$$

$$Q_{window_{south}} = CF_{window_{south}} \times A_{window_{south}} = 127.4 * 3.6 = 458.6 W$$

### The heating load of the operable 3.6 m<sup>2</sup> window on the South:

$$U_{window_{south}} = 2.87 \frac{W}{m^2 K}$$

$$HF_{window_{south}} = U_{window_{south}} \times \Delta T_{heating} = 2.87 * 24.8 = 71.2 \frac{W}{m^2}$$

$$Q_{window_{south}} = HF_{window_{south}} \times A_{window_{south}} = 71.2 * 3.6 = 256.3 W$$

### When we change the frame of the window from wooden to aluminum:

$$U_{window_{south}} = 4.62 \frac{W}{m^2}, SHGC = 0.55$$

$$\text{Cooling load } Q_{window_{south}} = CF_{window_{south}} \times A_{window_{south}} = 558.7 W$$

$$\text{Heating load } Q_{window_{south}} = HF_{window_{south}} \times A_{window_{south}} = 412.5 W$$

4) **The total value change:**

Cooling load:

$$Q_{wood\ frame} = 3352.3 + 543.2 + 458.6 = 4354.1\ W$$

$$Q_{aluminum\ frame} = 3499.5 + 559.4 + 558.7 = 4,617.6\ W$$

$$Q_{wood\ frame} - Q_{aluminum\ frame} = 4354.1 - 4,617.6 = -263.5\ W$$

Heating load:

$$Q_{wood\ frame} = 1014.2 + 253.4 + 256.3 = 1,523.9\ W$$

$$Q_{aluminum\ frame} = 1289.2 + 322.3 + 412.5 = 2024\ W$$

$$Q_{wood\ frame} - Q_{aluminum\ frame} = 1,523.9 - 2024 = -500.1\ W$$