

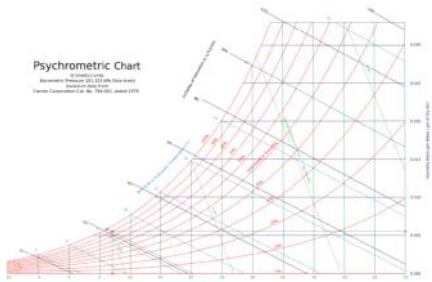
Task 1 Use a weather forecast website, and utilize the psychrometric chart and the formula we went through in the class to determine the absolute humidity, the wet-bulb temperature and the mass of water vapour in the air in Classroom A (Aula A) of Piacenza campus in the moment that you are solving this exercise (provide the inputs that you utilized)

Weather Forecast Website example

Umidità: Relative humidity, Pressione atmosferica: Air total pressure (1 hPa: 0.1 kPa), Temperatura effettiva: temperature to be utilized.

Il tempo oggi in Piacenza							
Lunedì, 02 Dicembre 2019							
	13:00	14:00	16:00	18:00	20:00	21:00	22:00
Temperatura effettiva	10°C	10°C	9°C	6°C	7°C	7°C	8°C
Temperatura percepita	10°C	10°C	8°C	5°C	7°C	6°C	7°C
Precipitazioni	0 mm	0 mm	0 mm	0 mm	0 mm	0 mm	0 mm
Umidità	79 %	77 %	89 %	90 %	90 %	92 %	91 %
Pressione atmosferica	1016 hPa	1018 hPa	1016 hPa	1017 hPa	1019 hPa	1019 hPa	1020 hPa

The time now is 8 pm from the data given in the website :
relative humidity is +90%
Total air pressure = 101.9 kPa
Temperture in kelvin scale T= 230 K



absolte humidity $w = 0.0055$
bulb temperature $T_{wb} = 6^{\circ}C$
$$w = \frac{0.622 P_v}{P_a} = \frac{0.622 P_v}{P - P_v} = 0.0055$$

introduce $P = 101.9 kPa$
 $P_v \approx 0.893 kPa$
airtem $\phi = \frac{m_v}{m_g} = 90\%$
for any Ideal gas \Rightarrow water vapour, $R_{sp} = 0.4615$
 $P_v = 0.893 kPa$
 $m_v = \frac{0.893 V}{0.4615 \times 230} \approx 8.41 \times 10^{-3}$
 $m_g = \frac{m_v}{90\%} \approx 9.34 \times 10^{-3}$

Task 2 Utilize the same methodology we went through in the class and determine the sensible and latent load corresponding to internal gains, the ventilation, and the infiltration in a house with a good construction quality and with the same geometry as that of the example which is located in Brindisi, Italy

BRINDISI, Italy										WMO# 163200				
Lat: 40.63N		Long: 17.95E		Elev: 10		SeaP: 161.2		Time Zone: 1.00 (EUT)		Period: 06-10				
										HDD: 99999				
Climate Analysis and Meteorological Design Conditions														
Calendar Month	Heating DB				Neutralization (SPRINKLER and DB)				Cooling DB (SUMMER)				MICROSPOND	
	DB	WB	WBP	WBR	DB	WB	WBP	WBR	DB	WB	WBP	WBR	DB	WB
(A)	18.2	14.2	12.7	12.1	27.2	24.2	22.7	22.1	18.2	14.2	12.7	12.1	18.2	14.2
(B)	2	2.9	4.4	-5.1	2.5	7.2	-3.0	3.0	7.4	13.4	10.2	12.4	10.4	3.4
(C)	2	2.9	4.4	-5.1	2.5	7.2	-3.0	3.0	7.4	13.4	10.2	12.4	10.4	3.4
Annual Cooling, Dehumidification, and Entropy Design Conditions														
Calendar Month	Heating DB				Cooling DB (SUMMER)				Cooling DB (SUMMER)				MICROSPOND	
	DB	WB	WBP	WBR	DB	WB	WBP	WBR	DB	WB	WBP	WBR	DB	WB
(A)	18.2	14.2	12.7	12.1	27.2	24.2	22.7	22.1	18.2	14.2	12.7	12.1	18.2	14.2
(B)	8	7.1	32.8	23.6	31.1	24.3	29.9	24.3	27.2	29.7	26.3	29.9	25.6	38.3
(C)	8	7.1	32.8	23.6	31.1	24.3	29.9	24.3	27.2	29.7	26.3	29.9	25.6	38.3
Extreme Annual Design Conditions														
Calendar Month	Heating DB				Cooling DB (SUMMER)				Cooling DB (SUMMER)				MICROSPOND	
	DB	WB	WBP	WBR	DB	WB	WBP	WBR	DB	WB	WBP	WBR	DB	WB
(A)	18.2	14.2	12.7	12.1	27.2	24.2	22.7	22.1	18.2	14.2	12.7	12.1	18.2	14.2
(B)	21.8	20.9	25.4	20.7	28.5	24.7	19.7	27.9	68.0	30.5	62.2	28.1	75.5	25.3
(C)	21.8	20.9	25.4	20.7	28.5	24.7	19.7	27.9	68.0	30.5	62.2	28.1	75.5	25.3
Extreme Annual Design Conditions														
Calendar Month	Extreme Max				Extreme Annual DB				Extreme Max				Extreme Max	
	DB	WB	WBP	WBR	DB	WB	WBP	WBR	DB	WB	WBP	WBR	DB	WB
(A)	35.3	33.0	34.2	34.2	24.7	19.2	19.2	19.2	24.7	19.2	19.2	19.2	24.7	19.2
(B)	35.3	33.0	34.2	34.2	24.7	19.2	19.2	19.2	24.7	19.2	19.2	19.2	24.7	19.2
(C)	35.3	33.0	34.2	34.2	24.7	19.2	19.2	19.2	24.7	19.2	19.2	19.2	24.7	19.2

internal gains:

calculate the sensible cooling load from internal gains:

$$Q_{igs} = 136 + 2.2 A_{cf} + 22 N_{oc} = 136 + 2.2 \times 22 \times 200 + 22 \times 2 = 620 \text{ W}$$

calculate cooling of int gains.

$$Q_{igl} = 20 + 0.22 A_{cf} + 12 N_{oc} = 20 + 0.22 \times 200 + 12 \times 2 = 88 \text{ W}$$

infiltration:

$$A_{ul} = 1.4 \text{ cm}^2/\text{m}^2$$

$$A_{eg} = A_{wall} + A_{roof} = 200 + 144 = 344 \text{ m}^2$$

$$\text{thus, } A_L = A_{eg} \times A_{ul} = 344 \times 1.4 = 481.6 \text{ cm}^2$$

$$T_{cooling} = 24^\circ\text{C} \quad T_{heating} = 20^\circ\text{C}$$

$$\Delta T_{cooling} = 31.1^\circ\text{C} - 24^\circ\text{C} = 7.1^\circ\text{C} = 7.1 \text{ K}$$

$$\Delta T_{heating} = 20^\circ\text{C} - (-4.1^\circ\text{C}) = 24.1^\circ\text{C} = 24.1 \text{ K}$$

$$DR = 7.1^\circ\text{C} = 7.1 \text{ K}$$

$$IDF_{heating} = 0.1073 \frac{\text{L}}{\text{s} \times \text{cm}^2}$$

$$IDF_{cooling} = 0.033 \frac{\text{L}}{\text{s} \times \text{cm}^2}$$

air flow rate:

$$Q_{i,heating} = A_L \times IDF_{heating} = 481.6 \times 0.1073 \approx 35.157 \frac{\text{L}}{\text{s}}$$

$$Q_{i,cooling} = A_L \times IDF_{cooling} = 481.6 \times 0.033 \approx 15.893 \frac{\text{L}}{\text{s}}$$

min whole building ventilation:

$$Q_v = 0.05 A_{cf} + 3.5 (N_{br} + 1) = 0.05 \times 200 + 3.5 \times (1+1) = 17 \frac{\text{L}}{\text{s}}$$

$$Q_{i-v,heating} = Q_{i,heating} + Q_v \approx 35.157 + 17 = 52.157 \frac{\text{L}}{\text{s}}$$

$$Q_{i-v,cooling} = Q_{i,cooling} + Q_v \approx 15.893 + 17 = 32.893 \frac{\text{L}}{\text{s}}$$

Given that $C_{sensible} = 1.23$, $C_{latent} = 3010$, $\Delta W_{cooling} = 0.0039$

$$Q_{inf-v,es} = C_s Q_{i-v} \Delta T_c \approx 1.23 \times 32.893 \times 7.1 = 287.25 \text{ W}$$

$$Q_{inf-v,cf} = C_L Q_{i-v} \Delta W_c \approx 3010 \times 32.893 \times 0.0039 = 386.13 \text{ W}$$

$$Q_{inh-vhs} = C_s Q_{i-vh} \Delta T_{heating} = 1,23 \times 52,157 \times 24,1 = 1546,09 W$$