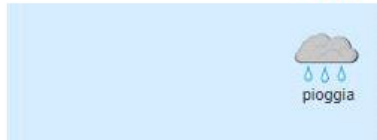


1 Use a weather forecast website and utilize the psychrometric chart and the formula to determine the absolute humidity, the wet-bulb temperature and the mass of water vapor in the air in Classroom A of Piacenza campus in the moment that you are solving this exercise (provide the inputs that you utilized).

Il tempo oggi in Piacenza
Domenica, 01 Dicembre 2019

19:00



Temperatura effettiva	7°C
Temperatura percepita	7°C
Precipitazioni	3 mm
Umidità	90 %
Pressione atmosferica	1018 hPa

dimensions classroom A:
length 20 m
width 6 m
weight 6 m

ABSOLUTE HUMIDITY

$$\omega = 0.0056 \frac{kg_{vapour}}{kg_{dryair}}$$

WET-BULB TEMPERATURE

$$T_{wb} = 6.24^{\circ}C$$

MASS OF WATER VAPOR

Assuming that at the moment that I am solving the exercise the internal temperature and the relative humidity of classroom A are the same as the external ones because on Sunday the campus is closed we have:

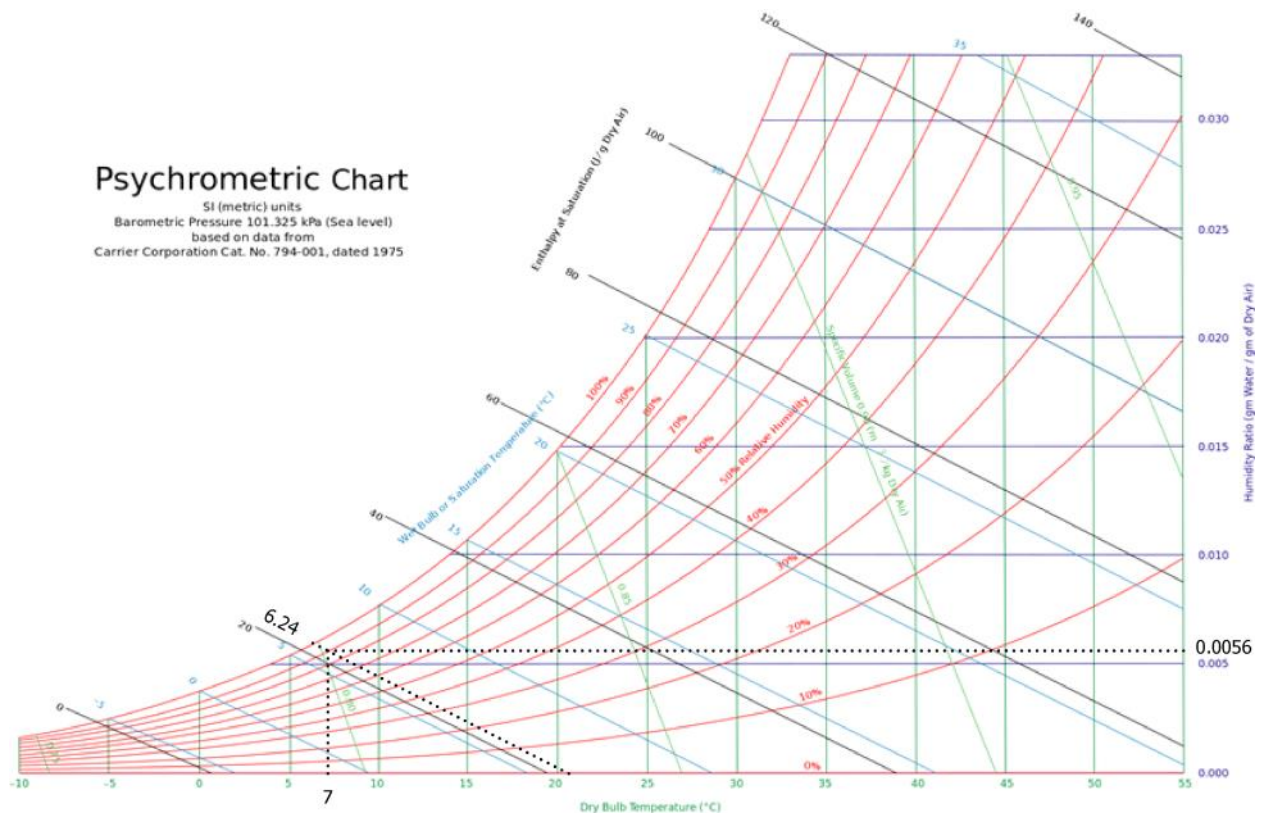
$$m_v = \frac{P_v \times V}{R_v \times T} = \frac{0.90 \times 720}{0.4615 \times (273 + 7)} = 5.01 \text{ Kg}$$

$$P_v = \phi P_g = \phi P_{sat}@7^{\circ}C = 0.90 \times 1 = 0.90 \text{ KPa}$$

$$V = 20 \text{ m} \times 6 \text{ m} \times 6 \text{ m} = 720 \text{ m}^3$$

Psychrometric Chart

SI (metric) units
Barometric Pressure 101.325 kPa (Sea level)
based on data from
Carrier Corporation Cat. No. 794-001, dated 1975



2 Utilize the same methodology we went through in the class and determine the sensible and latent load corresponding to internal gains, the ventilation, and the infiltration in a house with a **good** construction quality and with the same geometry as that of the example which is located in Brindisi, Italy.

building height: 2.5m
conditioned floor area: 200 m²
wall area: 144 m²
number of occupants: 2
number of bedrooms: 2

out temperature: 31.1 °C
in temperature: 24
relative humidity: 50%

BRINDISI, Italy														WMO#: 163200	
Lat: 40.65N		Long: 17.95E		Elev: 10		StdP: 101.2		Time Zone: 1.00 (EUW)		Period: 86-10		WBAN: 99999			
Annual Heating and Humidification Design Conditions															
Coldest Month	Heating DB		Humidification DP/MCDB and HR						Coldest month WS/MCDB				MCWS/PCWD to 99.6% DB		
			99.6%			99%			0.4%		1%				
	99.6%	99%	DP	HR	MCDB	DP	HR	MCDB	WS	MCDB	WS	MCDB	MCWS	PCWD	
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	
2	2.9	4.1	-5.1	2.5	7.2	-3.0	3.0	7.4	13.4	10.2	12.4	10.6	3.4	250	
Annual Cooling, Dehumidification, and Enthalpy Design Conditions															
Hottest Month	Hottest Month DB Range	Cooling DB/MCWB						Evaporation WB/MCDB						MCWS/PCWD to 0.4% DB	
		0.4%		1%		2%		0.4%		1%		2%			
		DB	MCWB	DB	MCWB	WB	MCWB	WB	MCDB	WB	MCDB	WB	MCDB	MCWS	PCWD
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)
8	7.1	32.8	23.6	31.1	24.3	29.9	24.3	27.2	29.7	26.3	29.0	25.6	28.3	4.2	180
Dehumidification DP/MCDB and HR															
0.4%		1%		2%		0.4%		1%		2%		Hours 8 to 4 & 12.8/20.6			
DP	HR	MCDB	DP	HR	MCDB	DP	HR	MCDB	Enth	MCDB	Enth	MCDB	Enth	MCDB	Hours
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)
26.3	21.8	29.2	25.4	20.7	28.5	24.7	19.7	27.9	86.0	30.1	82.2	29.1	78.5	28.3	1236
Extreme Annual Design Conditions															
Extreme Annual WS			Extreme Max WB	Extreme Annual DB				n-Year Return Period Values of Extreme DB							
1%	2.5%	5%		Mean	Standard deviation		n=5 years		n=10 years		n=20 years		n=50 years		
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)
11.3	9.9	8.7	31.4	0.4	37.3	1.4	3.0	-0.6	39.4	-1.4	41.1	-2.2	42.8	-3.2	44.9

INTERNAL GAINS

$$\dot{Q}_{ig_{sensible}} = 136 + 2.2 * A_{cf} + 22 N_{oc} = 136 + 2.2 * 200 + 22 * 2 = 620 W$$

$$\dot{Q}_{ig_{latent}} = 20 + 0.22 * A_{cf} + 12 N_{oc} = 20 + 0.22 * 200 + 12 * 2 = 88 W$$

INFILTRATION

$$A_{ul} = 1.4 \frac{cm^2}{m^2} \quad (\text{good quality})$$

$$A_{es} = 200 + 144 = 344 m^2$$

$$A_L = A_{es} \times A_{ul} = 344 \times 1.4 = 481.6 cm^2$$

$$IDF_{heating} = 0.065 \frac{L}{s \cdot cm^2}$$

$$IDF_{cooling} = 0.032 \frac{L}{s \cdot cm^2}$$

$$\dot{V}_{infiltration_{heating}} = A_L \times IDF_{heating} = 481.6 * 0.065 = 31.30 \frac{L}{s}$$

$$\dot{V}_{infiltration_{cooling}} = A_L \times IDF_{cooling} = 481.6 * 0.032 = 15.41 \frac{L}{s}$$

VENTILATION

$$\dot{V}_{ventilation} = 0.05 A_{cf} + 3.5 (N_{br} + 1) = 0.05 * 200 + 3.5 * 2 = 17 \frac{L}{s}$$

$$\dot{V}_{infiltration-ventilation_{heating}} = \dot{V}_{infiltration_{heating}} + \dot{V}_{ventilation} = 31.30 + 17 = 48.30 \frac{L}{s}$$

$$\dot{V}_{infiltration-ventilation_{cooling}} = \dot{V}_{infiltration_{cooling}} + \dot{V}_{ventilation} = 15.41 + 17 = 32.41 \frac{L}{s}$$

$$C_{sensible} = 1.23$$

$$C_{latent} = 3010$$

$$\Delta T_{cooling} = 31.1 - 24 = 7.1 \text{ }^{\circ}\text{C}$$

$$\Delta T_{heating} = 20 - (4.1) = 15.9 \text{ }^{\circ}\text{C}$$

$$\dot{Q}_{inf-vent_{cooling_{sensible}}} = C_{sensible} \times \dot{V}_{inf-vent_{cooling}} \times \Delta T_{cooling} = 1.23 * 32.41 * 7.1 = 283.04 \text{ W}$$

$$\dot{Q}_{inf-vent_{heating_{sensible}}} = C_{sensible} \times \dot{V}_{inf-vent_{heating}} \times \Delta T_{heating} = 1.23 * 48.30 * 15.9 = 944.6 \text{ W}$$

$$\omega_{out} = 0.0143 \frac{kg_{water}}{kg_{dryAir}}$$

$$\omega_{in} = 0.0093 \frac{kg_{water}}{kg_{dryAir}}$$

$$\Delta \omega_{cooling} = \omega_{out} - \omega_{in} = 0.0143 - 0.0093 = 0.005 \frac{kg_{water}}{kg_{DryAir}}$$

$$\dot{Q}_{inf-vent_{cooling_{latent}}} = C_{latent} \times \dot{V}_{inf-vent_{cooling}} \times \Delta \omega_{cooling} = 3010 * 32.41 * 0.005 = 487.77 \text{ W}$$