

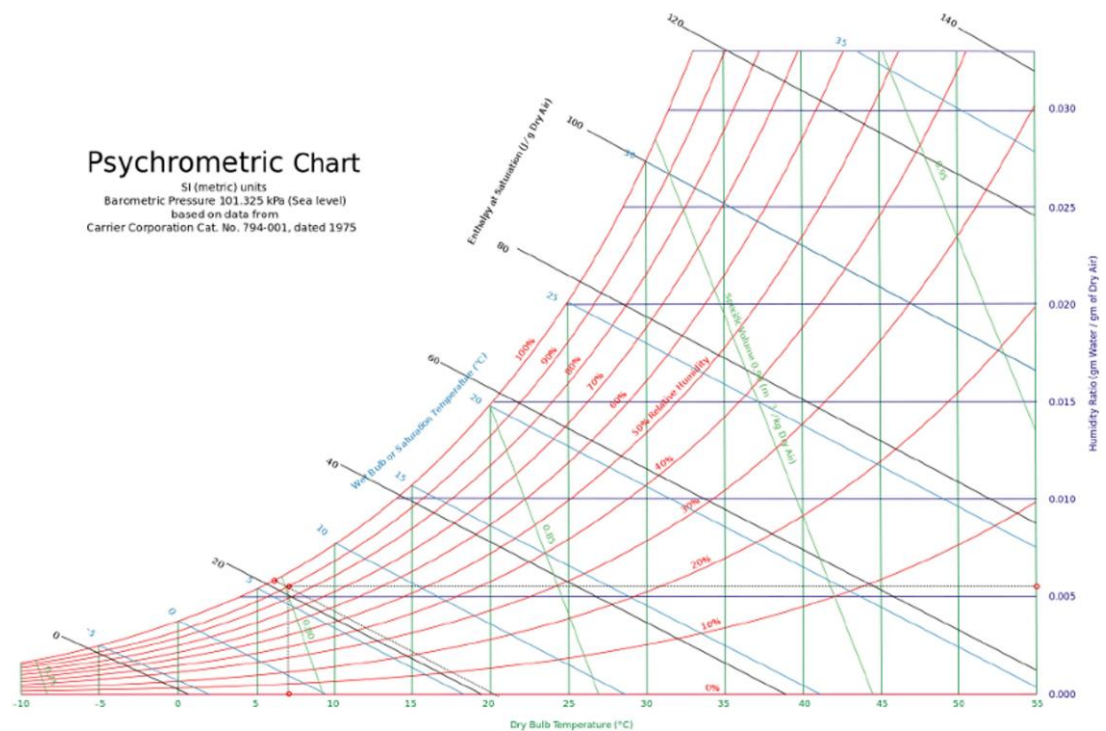
Practice No1

The time now is 20:00, from the data given in the website <https://www.meteo-oggi.it/italia/regione-emilia-romagna/tempo-piacenza/>

umidità: 90%, i.e., the relative humidity
 ϕ
 $\phi = 90\%$;

pressione atmosferica: 1019 hPa, i.e., the total air pressure $P = 101.9 \text{ kPa}$;

temperatura effettiva: 7
 t_{eff}
 t_{eff} , i.e., the temperature in Kelvin temperature scale $T = 230 \text{ K}$



Utilize the psychrometric chart, we can see,

the humidity ratio, i.e., the absolute humidity
 w
 $w = 0.0055$

the wet-bulb temperature
 $T_{\text{wb}} = 6 \text{ }^{\circ}\text{C}$

$w=0.622P_v/P_a=0.622P_v/P-P_v=0.0055$, introduce $P=101.9$ kPa into this equation, and solve it,

$$P_v = 0.893 \text{ kPa}$$

$$\text{autem, } \phi = m_v/m_g = 90\% \quad (1)$$

for any ideal gas, $m = P_v R_{sp} T$, during the class we were told that for water vapor, $R_{sp} = 0.4615$

introduce the pressure of water vapor

$P_v = 0.893$ kPa, and define the volume of aula A is V , here we have:

$$m_v = 0.893 V / 0.4615 \times 230 = 8.41 \times 10^{-3} V$$

subordinate this value to (1), calculate the maximum water vapor m_g ,

$$m_g = m_v / 90\% = 9.34 \times 10^{-3} V$$

Practice No 2

Internal gains,

Calculate the sensible cooling load from internal gains,

$$q_{ig, s} = 136 + 2.2 A_{cf} + 22 N_{oc} = 136 + 2.2 \times 200 + 22 \times 2 = 620 \text{ W}$$

Calculate the latent cooling load from internal gains,

$$q_{ig, l} = 20 + 0.22 A_{cf} + 12 N_{oc} = 20 + 0.22 \times 200 + 12 \times 2 = 88 \text{ W}$$

Infiltration,

for a house with a good construction quality, unit leakage area

$$A_{ul} = 1.4 \text{ cm}^2/\text{m}^2$$

and the exposed surface

$$A_{es} = A_{wall} + A_{roof} = 200 + 144 = 344 \text{ m}^2$$

thus,

$$A_L = A_{es} \times A_{ul} = 344 \times 1.4 = 481.6 \text{ cm}^2$$

Define the cooling temperature $T_{cooling}=24\text{ }^{\circ}\text{C}$, and
heating temperature $T_{heating}=20\text{ }^{\circ}\text{C}$

in Brindisi,
[Equazione]

$$O T_{cooling}=31.1\text{ }^{\circ}\text{C}-24\text{ }^{\circ}\text{C}=7.1\text{ }^{\circ}\text{C}=7.1\text{ K}$$

$$O T_{heating}=20\text{ }^{\circ}\text{C}-(-4.1\text{ }^{\circ}\text{C})=24.1\text{ }^{\circ}\text{C}=24.1\text{ K}$$

$$DR = 7.1\text{ }^{\circ}\text{C}=7.1\text{ K}$$

Given that IDF heating= $0.073\text{ Ls}\times\text{cm}^2$,

$$\text{IDF cooling}=0.033\text{ Ls}\times\text{cm}^2 ,$$

Calculate infiltration airflow rate,

$$Q_{i, \text{ heating}}=AL\times\text{IDF heating}=481.6\times0.073=35.157\text{ Ls}$$

$$Q_{i, \text{ cooling}}=AL\times\text{IDF cooling}=481.6\times0.033=15.893\text{ Ls}$$

The required minimum whole-building ventilation rate is

$$Q_v=0.05A_{cf}+3.5(N_{br}+1) = 0.05\times200+3.5\times(1+1)=17\text{ Ls}$$

Thus ,

$$Q_{i-v, \text{ heating}} = Q_{i, \text{ heating}}+Q_v=35.157+17=52.157\text{ Ls}$$

$$Q_{i-v, \text{ cooling}}=Q_{i, \text{ cooling}}+Q_v=15.893+17=32.893\text{ Ls}$$

Given that

$$C_{sensible}=1.23 , C_{latent}=3010, O_w\text{Cooling}=0.0039$$

$$q_{inf-ventilation\text{cooling}sensible}=C_{sensible}Q_{i-v, \text{ cooling}} O T_{cooling}=1.23 \times 32.893 \times 7.1=287.25\text{ W}$$

$$q_{inf-ventilation\text{cooling}latent} = C_{latent}Q_{i-v, \text{ cooling}} O_w\text{Cooling}=3010 \times 32.893 \times 0.0039=386.13\text{ W}$$

$$q_{inf-ventilation\text{heating}sensible}=C_{sensible}Q_{i-v, \text{ heating}} O T_{heating}=1.23 \times 52.157 \times 24.1=1546.09\text{ W}$$