

TASK 1

Use a weather forecast website, and utilize the psychrometric chart and the formula we went through in the class to determine the absolute humidity, the wet-bulb temperature and the mass of water vapor in the air in Classroom A (Aula A) of Piacenza campus in the moment that you are solving this exercise (provide the inputs that you utilized)

ANSWER

At the time solving this exercise,

Temperature $T = 7^{\circ}\text{C}$

Relative Humidity $\phi = 90\%$

Air Total Pressure $P = 1019\text{hPa} = 101.9\text{kPa}$

Consider the dimensions of Aula A as follow:

$$V = d \times w \times h = 18 \times 6 \times 5 = 540\text{m}^3$$

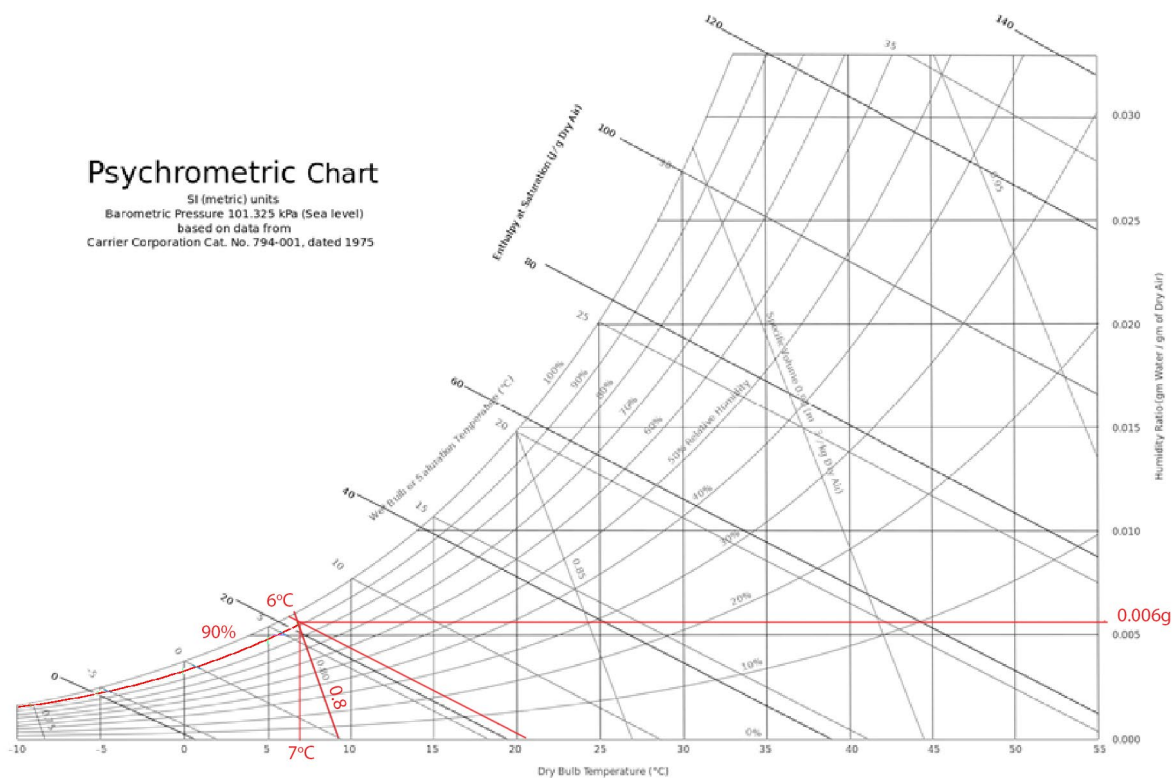
Using Psychrometric Chart,

Absolute Humidity $\omega = 0.006 \frac{\text{kg}_{\text{water}}}{\text{kg}_{\text{dryAir}}}$

Wet-bulb Temperature $T_{\text{wetbulb}} = 6^{\circ}\text{C}$

Specific volume $0.8\text{m}^3/\text{kg}_{\text{dryair}}$

Enthalpy $h = 21 \frac{\text{kJ}}{\text{kg}_{\text{dryAir}}}$



Using Formula,

$$\text{We have } \phi = \frac{m_v}{m_g} = \frac{P_v}{P_g}$$

The saturation pressure of water at 7°C $P_g = 1.002 \text{ kPa}$ (using Tetens' formula)

Partial pressure of vapor $P_v = P_g \times \phi = 1.002 \times 90\% = 0.902 \text{ kPa}$

Partial pressure of dry air $P_a = P - P_v = 101.9 - 0.9 = 101 \text{ kPa}$

Absolute Humidity $\omega = 0.622 \frac{P_v}{P_a} = 0.622 \frac{0.9}{101} = 0.0055 \frac{\text{kg water}}{\text{kg dry Air}}$

Mass of water vapor $m_v = \frac{P_v V}{R_v T} = \frac{0.9 \times 540}{0.4615 \times (273 + 7)} = 3.761 \text{ kg of water}$

Enthalpy of dry air $h_a = 1.005 \times T = 1.005 \times 7 = 7.035 \frac{\text{kJ}}{\text{kg dry Air}}$

Enthalpy of vapor $h_v = 2501.3 + 1.82 \times T = 2501.3 + 1.82 \times 7 = 2514.04 \frac{\text{kJ}}{\text{kg dry Air}}$

Total enthalpy

$$h_{total} = h_a + h_v \times \omega = 7.035 + 2514.04 \times 0.0055 = 20.86 \frac{\text{kJ}}{\text{kg dry Air}}$$

TASK 2

Utilize the same methodology we went through in the class and determine the sensible and latent load corresponding to internal gains, the ventilation, and the infiltration in a house with a good construction quality and with the same geometry (Height of 2.5 m, conditioned floor area of 200 m² and wall area is 144 m², two occupants and one bed room) located in Brindisi, Italy

BRINDISI, Italy														WMO#: 163200		
Lat: 40.65N		Long: 17.95E		Elev: 10		StdP: 101.2		Time Zone: 1.00 (EUW)		Period: 86-10		WBAN: 99999				
Annual Heating and Humidification Design Conditions																
Coldest Month	Heating DB			Humidification DP/MCDB and HR						Coldest month WS/MCDB				MCWS/PCWD to 99.6% DB		
				99.6%			99%			0.4%		1%				
	99.6%	99%		DP	HR	MCDB	DP	HR	MCDB	WS	MCDB	WS	MCDB	MCWS	PCWD	
	(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	
(1)	2	2.9	4.1	-5.1	2.5	7.2	-3.0	3.0	7.4	13.4	10.2	12.4	10.6	3.4	250	
Annual Cooling, Dehumidification, and Enthalpy Design Conditions																
Hottest Month	Hottest Month DB Range	Cooling DB/MCWB						Evaporation WB/MCDB						MCWS/PCWD to 0.4% DB		
		0.4%		1%		2%		0.4%		1%		2%				
		DB	MCWB	DB	MCWB	DB	MCWB	WB	MCDB	WB	MCDB	WB	MCDB	MCWS	PCWD	
		(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)
(2)	8	7.1	32.8	23.6	31.1	24.3	29.9	24.3	27.2	29.7	26.3	29.0	25.6	28.3	4.2	180
		Dehumidification DP/MCDB and HR						Enthalpy/MCDB						Hours		
		0.4%		1%		2%		0.4%		1%		2%		8 to 4 & 12.8/20.6		
		DP	HR	MCDB	DP	HR	MCDB	DP	HR	MCDB	Enth	MCDB	Enth	MCDB	Enth	MCDB
		(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)
(3)	26.3	21.8	29.2	25.4	20.7	28.5	24.7	19.7	27.9	86.0	30.1	82.2	29.1	78.5	28.3	1236
Extreme Annual Design Conditions																
Extreme Annual WS			Extreme Max WB	Extreme Annual DB				n-Year Return Period Values of Extreme DB								
				Mean		Standard deviation		n=5 years		n=10 years		n=20 years		n=50 years		
1%	2.5%	5%		Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)	
(4)	11.3	9.9	8.7	31.4	0.4	37.3	1.4	3.0	-0.6	39.4	-1.4	41.1	-2.2	42.8	-3.2	44.9

ANSWER

Internal Gain

$$\dot{Q}_{ig_{sensible}} = 136 + 2.2 * A_{cf} + 22 N_{oc} = 136 + 2.2 * 200 + 22 * 2 = 620 \text{ W}$$

$$\dot{Q}_{ig_{latent}} = 20 + 0.22 * A_{cf} + 12 N_{oc} = 20 + 0.22 * 200 + 12 * 2 = 88 \text{ WDR} = 11.9 \text{ }^{\circ}\text{C}$$

Infiltration and Ventilation

Table 3 Unit Leakage Areas

Construction	Description	$A_{ul}, \text{ cm}^2/\text{m}^2$
Tight	Construction supervised by air-sealing specialist	0.7
Good	Carefully sealed construction by knowledgeable builder	1.4
Average	Typical current production housing	2.8
Leaky	Typical pre-1970 houses	5.6
Very leaky	Old houses in original condition	10.4

Good Construction quality $\rightarrow A_{ul}=1.4\text{cm}^2/\text{m}^2$

$$\text{Total leakage Area } A_L = A_{es} \times A_{ul} = (200 + 144) \times 1.4 = 481.6\text{cm}^2$$

From Brindisi Weather Design Condition and table 5, typical IDF values,

$$\text{Heating design temperature } 4.1^{\circ}\text{C} \rightarrow IDF_{heating} = 0.065 \frac{L}{s \cdot \text{cm}^2}$$

$$\text{Cooling design temperature } 31.1^{\circ}\text{C} \rightarrow IDF_{cooling} = 0.032 \frac{L}{s \cdot \text{cm}^2}$$

Table 5 Typical IDF Values, $L/(s \cdot \text{cm}^2)$

$H, \text{ m}$	Heating Design Temperature, $^{\circ}\text{C}$					Cooling Design Temperature, $^{\circ}\text{C}$			
	-40	-30	-20	-10	0	10	30	35	40
2.5	0.10	0.095	0.086	0.077	0.069	0.060	0.031	0.035	0.040
3	0.11	0.10	0.093	0.083	0.072	0.061	0.032	0.038	0.043
4	0.14	0.12	0.11	0.093	0.079	0.065	0.034	0.042	0.049
5	0.16	0.14	0.12	0.10	0.086	0.069	0.036	0.046	0.055
6	0.18	0.16	0.14	0.11	0.093	0.072	0.039	0.050	0.061
7	0.20	0.17	0.15	0.12	0.10	0.075	0.041	0.051	0.068
8	0.22	0.19	0.16	0.14	0.11	0.079	0.043	0.058	0.074

$$\dot{V}_{infiltration_{heating}} = A_L \times IDF_{heating} = 486.1 \times 0.065 = 31.60 \frac{L}{s}$$

$$\dot{V}_{infiltration_{cooling}} = A_L \times IDF_{cooling} = 486.1 \times 0.032 = 15.56 \frac{L}{s}$$

$$\dot{V}_{ventilation} = 0.05 A_{cf} + 3.5 (N_{br} + 1) = 0.05 \times 200 + 3.5 \times (1 + 1) = 17 \frac{L}{s}$$

$$\text{For } C_{sensible} = 1.23, C_{latent} = 3010$$

$$\dot{Q}_{inf-vent_{heating_{sensible}}} = C_{sensible} \dot{V}_{inf-vent} \Delta T_{heating} = 1.23 \times (31.6 + 17) \times (20 - 4.1) = 950.5 \text{ W}$$

$$\dot{Q}_{inf-vent_{cooling_{sensible}}} = C_{sensible} \dot{V}_{inf-vent} \Delta T_{cooling} = 1.23 \times (15.56 + 17) \times (31.1 - 24) = 284.3 \text{ W}$$

Using Psychrometric Chart, at 50% relative humidity,

$$\text{At } 31.1^\circ\text{C}, \omega_{outside} = 0.0132 \frac{kg_{water}}{kg_{dryAir}}$$

$$\text{At } 24^\circ\text{C}, \omega_{inside} = 0.0093 \frac{kg_{water}}{kg_{dryAir}}$$

$$\rightarrow \Delta \omega_{cooling} = 0.0132 - 0.0093 = 0.0039$$

$$\dot{Q}_{inf-vent_{cooling_{latent}}} = C_{latent} \dot{V}_{inf-vent} \Delta \omega_{cooling} = 3010 \times (31.6 + 17) \times 0.0039 = 570.5 \text{ W}$$