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Task: 01

Use a weather forecast website, and utilize the psychrometric chart and the formula we went through in the class to determine the absolute humidity, the wet-bulb temperature and the mass of water vapour in the air in Classroom A (Aula A) of Piacenza campus in the moment that you are solving this exercise (provide the inputs that you utilized)

Umidità: Relative humidity, Atmospheric temperature : Air total pressure (1 hPa: 0.1 kPa), Effective Temperature : temperature to be utilized.

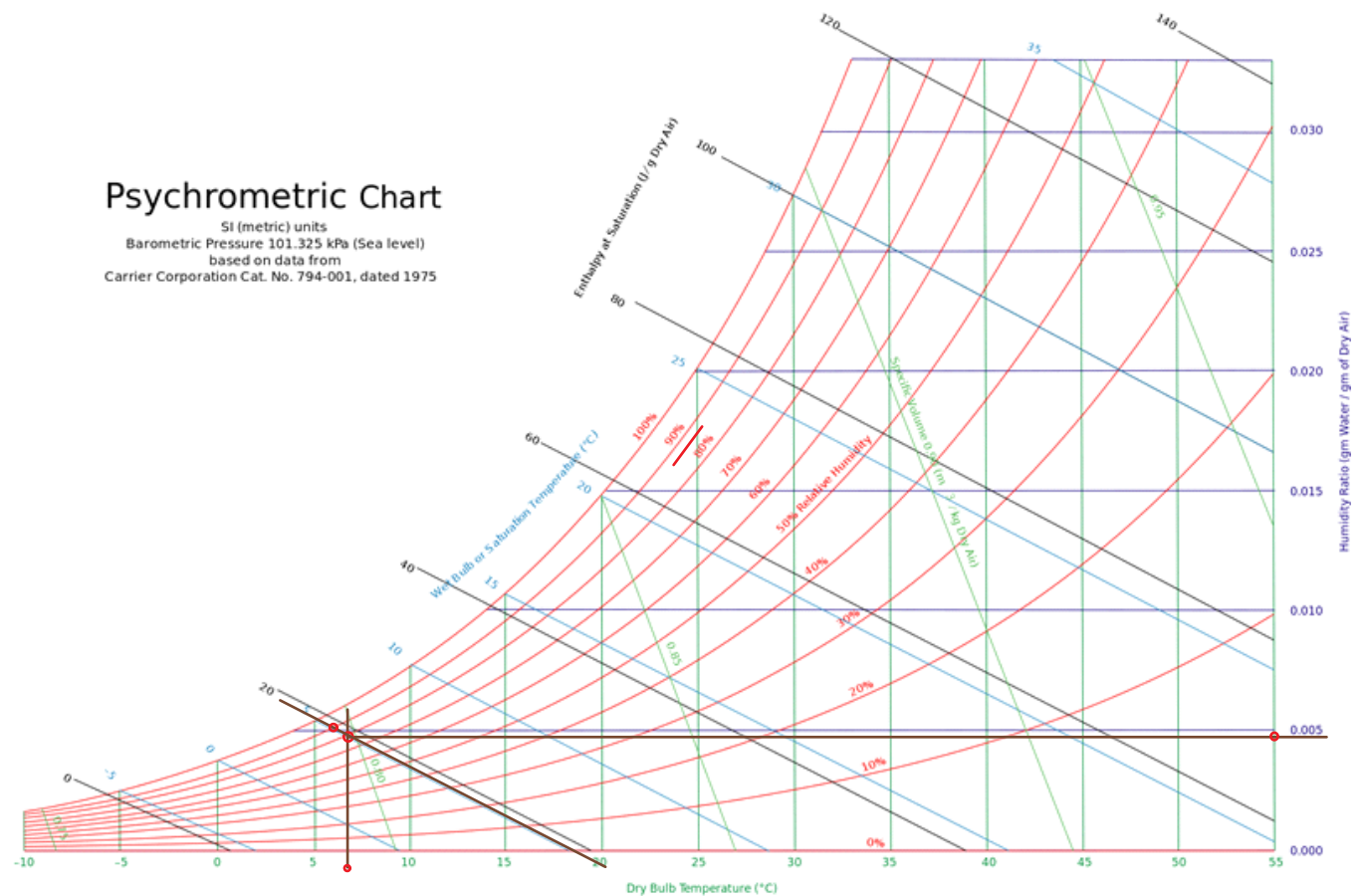
| Il tempo oggi in Piacenza Lunedì, 02 Dicembre 2019 | | | | | | | |
|---|--|--|---|---|--|--|--|
| | 13:00 | 14:00 | 16:00 | 18:00 | 20:00 | 21:00 | 22:00 |
| |  PartlyCloud |  PartlyCloud |  LightCloud |  LightCloud |  PartlyCloud |  Cloud |  PartlyCloud |
| Temperatura effettiva | 10°C | 10°C | 9°C | 6°C | 7°C | 7°C | 8°C |
| Temperatura percepita | 10°C | 10°C | 8°C | 5°C | 7°C | 6°C | 7°C |
| Precipitazioni | 0 mm | 0 mm | 0 mm | 0 mm | 0 mm | 0 mm | 0 mm |
| Umidità | 79 % | 77 % | 89 % | 90 % | 90 % | 92 % | 91 % |
| Pressione atmosferica | 1016 hPa | 1015 hPa | 1016 hPa | 1017 hPa | 1019 hPa | 1019 hPa | 1020 hPa |

The time now is 20:00, from the data given in this website, <https://www.meteo-oggi.it/italia/regione-emilia-romagna/tempo-piacenza/>

Humidity is 90%, i.e. $t = \text{The relative Humidity } \phi = 90\%$

Atmospheric Pressure (P)= 1019hPa.=101.9kPa

Effective temperature= 7°C, i.e. Kelvin temperature scale $T = 7^\circ\text{C} + 273.15 = 230.15\text{K}$



From the Psychrometric chart we can see,

The humidity ratio i.e. The absolute humidity $\omega = 0.0055$

The wet bulb temperature $T_{wb} = 6 \text{ }^{\circ}\text{C}$

$$\omega = 0.622 \cdot \frac{P_v}{P_a} \quad , \quad 0.0055 = \frac{0.622 P_v}{101.9 - P_v}$$

(by taking $P = 101.9 \text{ kPa}$ in equation) $P_v = 0.89 \text{ kPa}$

$$\phi = \frac{m_v}{m_g} = 90\%$$

For ideal gas, $m = \frac{PV}{R_{sp} \cdot T}$, we know, $R_{sp} = 0.4615$, Pressure of Water vapour

$P_v = 0.893 \text{ Kpa}$ and definite volume of Aula A is 'V'

$$m_v = \frac{0.893}{0.4615 \cdot 230} = 8.41 \cdot 10^{-3} V$$

$$\text{Maximum water vapour, } m_g = \frac{m_v}{90\%} = 9.34 \cdot 10^{-3} V$$

Task: 02

Utilize the same methodology we went through in the class and determine the sensible and latent load corresponding to internal gains, the ventilation, and the infiltration in a house with a good construction quality and with the same geometry as that of the example which is located in Brindisi, Italy

Lat: 40.65N Long: 17.95E Elev: 10 StdP: 101.2 Time Zone: 1.00 (EUW) Period: 86-10 WBAN: 99999

Annual Heating and Humidification Design Conditions

| Coldest Month | Heating DB | | Humidification DPM/CDB and HR | | | | | | Coldest month WS/MCDB | | | | MCWS/PCWD to 99.6% DB | |
|---------------|------------|-----|-------------------------------|-----|------|------|-----|------|-----------------------|------|------|------|-----------------------|------|
| | 99.6% | 99% | DP | HR | MCDB | DP | HR | MCDB | WS | MCDB | WS | MCDB | MCWS | PCWD |
| (a) | (b) | (c) | (d) | (e) | (f) | (g) | (h) | (i) | (j) | (k) | (l) | (m) | (n) | (o) |
| (1) 2 | 2.9 | 4.1 | -5.1 | 2.5 | 7.2 | -3.0 | 3.0 | 7.4 | 13.4 | 10.2 | 12.4 | 10.6 | 3.4 | 250 |

Annual Cooling, Dehumidification, and Enthalpy Design Conditions

| Hottest Month | Hottest Month DB Range | Cooling DB/MCWB | | | | | | Evaporation WB/MCDB | | | | | | MCWS/PCWD to 0.4% DB | |
|---------------|------------------------|-----------------|------|------|------|------|------|---------------------|------|------|------|------|------|----------------------|------|
| | | 0.4% | 1% | 2% | 0.4% | 1% | 2% | WB | MCDB | WB | MCDB | WB | MCDB | MCWS | PCWD |
| (a) | (b) | (c) | (d) | (e) | (f) | (g) | (h) | (i) | (j) | (k) | (l) | (m) | (n) | (o) | (p) |
| (2) 8 | 7.1 | 32.8 | 23.6 | 31.1 | 24.3 | 29.9 | 24.3 | 27.2 | 29.7 | 26.3 | 29.0 | 25.6 | 28.3 | 4.2 | 180 |

| Dehumidification DPM/CDB and HR | | | | | | | | | Enthalpy/MCDB | | | | | | Hours 8 to 4 & 12.8/20.6 | |
|---------------------------------|------|------|------|------|------|------|------|------|---------------|------|------|------|------|------|--------------------------------|-----|
| 0.4% | | | 1% | | | 2% | | | 0.4% | | 1% | | 2% | | | |
| DP | HR | MCDB | DP | HR | MCDB | DP | HR | MCDB | Enth | MCDB | Enth | MCDB | Enth | MCDB | | |
| (a) | (b) | (c) | (d) | (e) | (f) | (g) | (h) | (i) | (j) | (k) | (l) | (m) | (n) | (o) | | |
| (3) 26.3 | 21.8 | 29.2 | 25.4 | 20.7 | 28.5 | 24.7 | 19.7 | 27.9 | 86.0 | 30.1 | 82.2 | 29.1 | 78.5 | 28.3 | 1236 | (4) |

Extreme Annual Design Conditions

| Extreme Annual WS | | | Extreme Max WB | Extreme Annual DB | | | | n-Year Return Period Values of Extreme DB | | | | | | | |
|-------------------|------|-----|----------------|-------------------|--------------------|-----|-----|---|------|------------|------|------------|------|------------|------|
| 1% | 2.5% | 5% | | Mean | Standard deviation | Min | Max | n=5 years | | n=10 years | | n=20 years | | n=50 years | |
| (a) | (b) | (c) | (d) | (e) | (f) | (g) | (h) | (i) | (j) | (k) | (l) | (m) | (n) | (o) | (p) |
| (4) 11.3 | 9.9 | 8.7 | 31.4 | 0.4 | 37.3 | 1.4 | 3.0 | -0.6 | 39.4 | -1.4 | 41.1 | -2.2 | 42.8 | -3.2 | 44.9 |

Internal gains

$$\dot{Q}_{\text{igensible}} = 136 + 2.2 \cdot A_{\text{cf}} + 22 N_{\text{oc}} = 136 + 2.2 \cdot 200 + 22 \cdot 2 = 620 \text{ W}$$

$$\dot{Q}_{\text{iglatent}} = 20 + 0.22 \cdot A_{\text{cf}} + 12 N_{\text{oc}} = 20 + 0.22 \cdot 200 + 12 \cdot 2 = 88 \text{ W}$$

$$\text{Average quality} \rightarrow A_{\text{ul}} = 1.4 \frac{\text{cm}^2}{\text{m}^2}$$

$$\text{Exposed surface} = \text{Wall area} + \text{roof area}$$

$$A_{\text{es}} = 200 + 144 = 344 \text{ m}^2$$

$$A_{\text{L}} = A_{\text{es}} \times A_{\text{ul}} = 344 \times 1.4 = 481.6 \text{ cm}^2$$

In Brindisi,

$$\Delta T_{\text{cooling}} = 31.1^\circ\text{C} - 24^\circ\text{C} = 7.1^\circ\text{C} = 7.1\text{K}$$

$$\Delta T_{\text{heating}} = 20^\circ\text{C} - (-4.1)^\circ\text{C} = 24.1^\circ\text{C} = 24.1\text{K}$$

$$\text{DR} = 7.1^\circ\text{C} = 7.1\text{K}$$

Given,

$$\text{IDF}_{\text{heating}} = 0.073 \frac{\text{L}}{\text{s} \cdot \text{cm}^2} \quad \text{IDF}_{\text{cooling}} = 0.033 \frac{\text{L}}{\text{s} \cdot \text{cm}^2}$$

Table 5 Typical IDF Values, L/(s·cm²)

| H, m | Heating Design Temperature, °C | | | | | Cooling Design Temperature, °C | | | | |
|---------------|--------------------------------|-------|-------|-------|-------|--------------------------------|-------|-------|-------|--|
| | -40 | -30 | -20 | -10 | 0 | 10 | 30 | 35 | 40 | |
| 2.5 | 0.10 | 0.095 | 0.086 | 0.077 | 0.069 | 0.060 | 0.031 | 0.035 | 0.040 | |
| 3 | 0.11 | 0.10 | 0.093 | 0.083 | 0.072 | 0.061 | 0.032 | 0.038 | 0.043 | |
| 4 | 0.14 | 0.12 | 0.11 | 0.093 | 0.079 | 0.065 | 0.034 | 0.042 | 0.049 | |
| 5 | 0.16 | 0.14 | 0.12 | 0.10 | 0.086 | 0.069 | 0.036 | 0.046 | 0.055 | |
| 6 | 0.18 | 0.16 | 0.14 | 0.11 | 0.093 | 0.072 | 0.039 | 0.050 | 0.061 | |
| 7 | 0.20 | 0.17 | 0.15 | 0.12 | 0.10 | 0.075 | 0.041 | 0.051 | 0.068 | |
| 8 | 0.22 | 0.19 | 0.16 | 0.14 | 0.11 | 0.079 | 0.043 | 0.058 | 0.074 | |

Calculate infiltration air-flow rate,

$$\dot{V}_{\text{infiltration heating}} = A_{\text{L}} \times \text{IDF} = 481.6 \cdot 0.073 = 35.15 \frac{\text{L}}{\text{s}}$$

$$\dot{V}_{\text{infiltration cooling}} = A_{\text{L}} \times \text{IDF} = 481.6 \cdot 0.033 = 15.89 \frac{\text{L}}{\text{s}}$$

The required minimum whole building ventilation rate is,

$$\dot{V}_{\text{ventilation}} = 0.05 A_{\text{cf}} + 3.5 (N_{\text{br}} + 1) = 0.05 \cdot 200 + 3.5 \cdot (1+1) = 17 \text{ L/S}$$

$$\text{Thus, } \dot{V}_{\text{inf-ventilation heating}} = \dot{V}_{\text{infiltration heating}} + \dot{V}_{\text{ventilation}} = 35.15 + 17 = 52.157 \frac{\text{L}}{\text{s}}$$

$$\text{Given that, } C_{\text{Sensible}} = 1.23, C_{\text{Latent}} = 3010, \Delta\omega_{\text{Cooling}} = 0.0039$$

$$q_{\dot{V}_{\text{inf-Ventilation cooling sensible}}} = C_{\text{sensible}} \cdot \dot{V}_{\text{infiltration cooling}} \cdot \Delta T_{\text{cooling}} = 1.23 * 32.893 * 7.1 = 287.25 \text{ W}$$

$$q_{\dot{V}_{\text{inf-Ventilation cooling latent}}} = C_{\text{latent}} \cdot \dot{V}_{\text{infiltration cooling}} \cdot \Delta\omega_{\text{cooling}} = 3010 * 32.893 * 0.0039 = 386.13 \text{ W}$$

$$q_{\dot{V}_{\text{inf-Ventilation heating sensible}}} = C_{\text{sensible}} \cdot \dot{V}_{\text{infiltration cooling}} \cdot \Delta T_{\text{heating}} = 1.23 * 52.157 * 24.1 = 1546.09 \text{ W}$$