

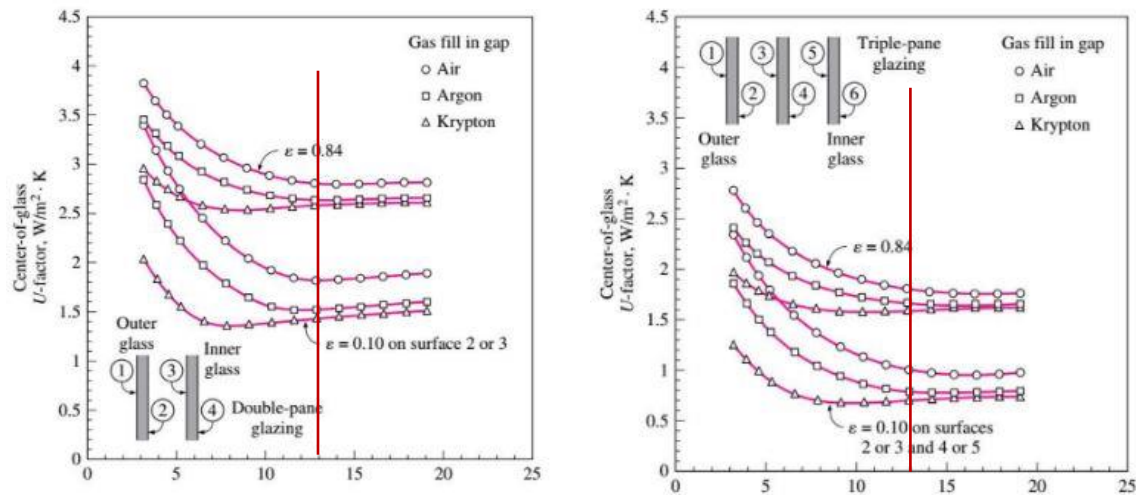
WEEKLY SUBMISSION - TASK 08

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1) Using the diagrams given in the presentation calculate how much (%) is the effect of applying different modifications (changing the gas, adding an extra pane, using a low emissivity coating) on the U value with respect to a benchmark case of double layer with air and no coating? (keep the gap thickness to be 13 mm)?



Soln: Benchmark:

With Double pane glazing ($\epsilon=0.84$) & gap thickness 13mm

U- Value of a double pane glazing window if the gap is filled with air is $2.8 \frac{W}{m^2 K}$

ϵ value	0.84		0.10			0.84			0.1		
No. of panes	2	2	2	2	2	3	3	3	3	3	3
Gas	Argon	Krypton	Air	Argon	Krypton	Air	Argon	Krypton	Air	Argon	krypton
U value	2.65	2.6	1.8	1.5	1.4	1.8	1.7	1.6	1	0.8	0.7
% of change	5.4	7.2	35.7	46.4	50	35.7	39.2	42.8	64.3	71.4	75

2) Consider the house that we analyzed in the last two examples, calculate the heating and cooling load of the other windows which are fixed 14.4 m² on the west, fixed 3.6 m² on the south and an operable 3.6 m² on the south (the same window and frame type). How much does the total value change if I change the frame of the window from wooden one to aluminum?

Sol:

PIACENZA, Italy

WMQ#: 160840

Lat: 44.92N Long: 9.73E Elev: 138 StdP: 99.68 Time Zone: 1.00 (EUW) Period: 89-10 WBAN: 99999

Annual Heating and Humidification Design Conditions

Coldest Month	Heating DB		Humidification DP/MCDB and HR						Coldest month WS/MCDB				MCWS/PCWD to 99.8% DB	
			99.6%			99%			0.4%		1%			
	99.6%	99%	DP	HR	MCDB	DP	HR	MCDB	WS	MCDB	WS	MCDB	MCWS	PCWD
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)
1	-6.2	-4.8	-11.6	1.4	3.1	-8.8	1.8	1.8	8.8	5.6	7.7	6.2	2.1	250

Annual Cooling, Dehumidification, and Enthalpy Design Conditions

Hottest Month	Hottest Month DB Range	Cooling DB/MCWB						Evaporation WB/MCDB						MCWS/PCWD to 0.4% DB	
		0.4%		1%		2%		0.4%		1%		2%			
		DB	MCWB	DB	MCWB	DB	MCWB	WB	MCDB	WB	MCDB	WB	MCDB	MCWS	PCWD
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)
8	11.9	33.1	22.7	31.9	22.4	30.3	21.8	24.6	30.2	23.7	29.2	22.9	28.3	2.4	90

Latitude ≈ 45

$T_{cooling} = 24^{\circ}\text{C}$

$T_{heating} = 20^{\circ}\text{C}$

$\Delta T_{cooling} = 31.9^{\circ}\text{C} - 24^{\circ}\text{C} = 7.9^{\circ}\text{C}$

$\Delta T_{heating} = 20^{\circ}\text{C} - (-4.8)^{\circ}\text{C} = 24.8^{\circ}\text{C}$

From the table DR = 11.9 °C

FIXED WINDOW ON WEST SIDE

Area = 14.4 m²

COOLING LOAD

$$q_{west\ window} = A \times CF_{west\ window}$$

$$CF_{west\ window(heat\ transfer)} = U_{west\ window} (\Delta T_{cooling} - 0.46\ DR)$$

$$U_{west\ window} = 2.84 \frac{W}{m^2 K}$$

$$CF_{west\ window(heat\ transfer)} = 2.84 \frac{W}{m^2 K} (7.9\ K - 0.46 (11.9\ K))$$

$$\approx 6.89 \frac{W}{m^2}$$

Irradiation

$E_D = 559$

$E_d = 188$

$PXI_{west\ window} = E_D + E_d$

$$= 559 + 188 = 747$$

Since no internal shading, so IAC = 1

SHGC = 0.54

$FF_s = 0.56$

Glazing Type	Glazing Layers	ID ^b	Property ^{c,d}	Center of Glazing	Frame									
					Operable					Fixed				
					Aluminum	Aluminum with Thermal Break	Reinforced Vinyl/Aluminum	Wood/Vinyl	Insulated Fiberglass/Vinyl	Aluminum	Aluminum with Thermal Break	Reinforced Vinyl/Aluminum	Wood/Vinyl	Insulated Fiberglass/Vinyl
Clear	1	1a	U	5.91	7.24	6.12	5.14	5.05	4.61	6.42	6.07	5.55	5.55	5.35
			SHGC	0.86	0.75	0.75	0.64	0.64	0.64	0.78	0.78	0.75	0.75	0.75
	2	5a	U	2.73	4.62	3.42	3.00	2.87	5.83	3.61	3.22	2.86	2.84	2.72
			SHGC	0.76	0.67	0.67	0.57	0.57	0.57	0.69	0.69	0.67	0.67	0.67
	3	29a	U	1.76	3.80	2.60	2.25	2.19	1.91	2.76	2.39	2.05	2.01	1.93
			SHGC	0.68	0.60	0.60	0.51	0.51	0.51	0.62	0.62	0.60	0.60	0.60
Low-e, low-solar	2	25a	U	1.70	3.83	2.68	2.33	2.21	1.89	2.75	2.36	2.03	2.01	1.90
			SHGC	0.41	0.37	0.37	0.31	0.31	0.31	0.38	0.38	0.36	0.36	0.36
	3	40c	U	1.02	3.22	2.07	1.76	1.71	1.45	2.13	1.76	1.44	1.40	1.33
Low-e, high-solar			SHGC	0.27	0.25	0.25	0.21	0.21	0.21	0.25	0.25	0.24	0.24	0.24
	2	17c	U	1.99	4.05	2.89	2.52	2.39	2.07	2.99	2.60	2.26	2.24	2.13
			SHGC	0.70	0.62	0.62	0.52	0.52	0.52	0.64	0.64	0.61	0.61	0.61
	3	32c	U	1.42	3.54	2.36	2.02	1.97	1.70	2.47	2.10	1.77	1.73	1.66
			SHGC	0.62	0.55	0.55	0.46	0.46	0.46	0.56	0.56	0.54	0.54	0.54
Heat-absorbing	1	1c	U	5.91	7.24	6.12	5.14	5.05	4.61	6.42	6.07	5.55	5.55	5.35
			SHGC	0.73	0.64	0.64	0.54	0.54	0.54	0.66	0.66	0.64	0.64	0.64
	2	5c	U	2.73	4.62	3.42	3.00	2.87	5.83	3.61	3.22	2.86	2.84	2.72
			SHGC	0.62	0.55	0.55	0.46	0.46	0.46	0.56	0.56	0.54	0.54	0.54
	3	29c	U	1.76	3.80	2.60	2.25	2.19	1.91	2.76	2.39	2.05	2.01	1.93
			SHGC	0.34	0.31	0.31	0.26	0.26	0.26	0.31	0.31	0.30	0.30	0.30
Reflective	1	11	U	5.91	7.24	6.12	5.14	5.05	4.61	6.42	6.07	5.55	5.55	5.35
			SHGC	0.31	0.28	0.28	0.24	0.24	0.24	0.29	0.29	0.27	0.27	0.27
	2	5p	U	2.73	4.62	3.42	3.00	2.87	5.83	3.61	3.22	2.86	2.84	2.72
			SHGC	0.29	0.27	0.27	0.22	0.22	0.22	0.27	0.27	0.26	0.26	0.26
	3	29c	U	1.76	3.80	2.60	2.25	2.19	1.91	2.76	2.39	2.05	2.01	1.93
			SHGC	0.34	0.31	0.31	0.26	0.26	0.26	0.31	0.31	0.30	0.30	0.30

Table 10 Peak Irradiance, W/m²

Exposure		Latitude										
		20°	25°	30°	35°	40°	45°	50°	55°	60°		
North	E_D	125	106	92	84	81	85	96	112	136		
	E_d	128	115	103	93	84	76	69	62	55		
	E_t	253	221	195	177	166	162	164	174	191		
Northeast/Northwest	E_D	460	449	437	425	412	399	386	374	361		
	E_d	177	169	162	156	151	147	143	140	137		
	E_t	637	618	599	581	563	546	529	513	498		
East/West	E_D	530	543	552	558	560	559	555	547	537		
	E_d	200	196	193	190	189	188	187	187	187		
	E_t	730	739	745	748	749	747	742	734	724		
Southeast/Southwest	E_D	282	328	369	405	436	463	485	503	517		
	E_d	204	203	203	204	205	207	210	212	215		
	E_t	485	531	572	609	641	670	695	715	732		
South	E_D	0	60	139	214	283	348	408	464	515		
	E_d	166	193	196	200	204	209	214	219	225		
	E_t	166	253	335	414	487	557	622	683	740		
Horizontal	E_D	845	840	827	806	776	738	691	637	574		
	E_d	170	170	170	170	170	170	170	170	170		
	E_t	1015	1010	997	976	946	908	861	807	744		

Table 13 Fenestration Solar Load Factors FF_s

Exposure	Single Family Detached	Multifamily
North	0.44	0.27
Northeast	0.21	0.43
East	0.31	0.56
Southeast	0.37	0.54
South	0.47	0.53
Southwest	0.58	0.61
West	0.56	0.65
Northwest	0.46	0.57
Horizontal	0.58	0.73

$$CF_{\text{west window(irradiation)}} = PXI \times SHGC \times IAC \times FF_s$$

$$= 747 \times 0.54 \times 1 \times 0.56 = 225.89$$

$$q_{\text{west window}} = A \times CF_{\text{west window}} = A \times (CF_{\text{west window(heat transfer)}} + (CF_{\text{west window(irradiation)}}))$$

$$= 14.4 \text{ m}^2 \times (6.89 + 225.89) \frac{\text{W}}{\text{m}^2} = 3352.07 \text{ W}$$

HEATING LOAD

$$q_{\text{west window}} = A \times HF_{\text{west window}} = A \times U_{\text{west window}} \times \Delta T_{\text{heating}}$$

$$= 14.4 \text{ m}^2 \times 2.84 \frac{\text{W}}{\text{m}^2 \text{K}} \times 24.8 \text{ K} = 1014.22 \text{ W}$$

If the frame is aluminium

$$U'_{\text{west window}} = 3.61 \frac{\text{W}}{\text{m}^2 \text{K}}$$

$$SHGC' = 0.56$$

Cooling load

$$CF'_{\text{west window(heat transfer)}} = U'_{\text{west window}} (\Delta T_{\text{cooling}} - 0.46 \text{ DR})$$

$$= 3.61 \frac{\text{W}}{\text{m}^2 \text{K}} (7.9 \text{ K} - 0.46 \times 11.9 \text{ K}) = 8.76 \frac{\text{W}}{\text{m}^2}$$

$$CF'_{\text{west window(irradiation)}} = PXI \times SHGC' \times IAC \times FF_s$$

$$= 747 \times 0.56 \times 1 \times 0.56 = 234.26$$

$$q'_{\text{west window}} = A \times (CF'_{\text{west window(heat transfer)}} + (CF'_{\text{west window(irradiation)}}))$$

$$= 14.4 \text{ m}^2 \times (8.76 + 234.26) \frac{\text{W}}{\text{m}^2} = 3499.48 \text{ W}$$

Heating load

$$q'_{\text{west window}} = A \times HF'_{\text{west window}} = A \times U'_{\text{west window}} \times \Delta T_{\text{heating}}$$

$$= 14.4 \text{ m}^2 \times 3.61 \frac{\text{W}}{\text{m}^2 \text{K}} \times 24.8 \text{ K} = 1289.20 \text{ W}$$

FIXED WINDOW ON SOUTH SIDE

$$\text{Area} = 3.6 \text{ m}^2$$

COOLING LOAD

$$q_{\text{south window}} = A \times CF_{\text{south window}}$$

$$CF_{\text{south window(heat transfer)}} = U_{\text{south window}} (\Delta T_{\text{cooling}} - 0.46 \text{ DR})$$

$$U_{\text{south window}} = 2.84 \frac{\text{W}}{\text{m}^2 \text{K}}$$

$$CF_{\text{south window(heat transfer)}} = 2.84 \frac{\text{W}}{\text{m}^2 \text{K}} (7.9 \text{ K} - 0.46 (11.9 \text{ K})) \approx 6.89 \frac{\text{W}}{\text{m}^2}$$

Irradiation

$$E_D = 348$$

$$E_d = 209$$

$$P_{XI \text{ west window}} = E_D + E_d = 348 + 209 = 557$$

Since no internal shading, so IAC = 1

$$SHGC = 0.54$$

$$FF_s = 0.47$$

$$CF_{\text{south window(irradiation)}} = P_{XI} \times SHGC \times IAC \times FF_s = 557 \times 0.54 \times 1 \times 0.47 = 141.36$$

$$\begin{aligned} q_{\text{south window}} &= A \times CF_{\text{south window}} = A \times (CF_{\text{south window(heat transfer)}} + (CF_{\text{south window(irradiation)}})) \\ &= 3.6 \text{ m}^2 \times (6.89 + 141.36) \frac{\text{W}}{\text{m}^2} = 533.72 \text{ W} \end{aligned}$$

HEATING LOAD

$$\begin{aligned} q_{\text{south window}} &= A \times HF_{\text{south window}} = A \times U_{\text{south window}} \times \Delta T_{\text{heating}} \\ &= 3.6 \text{ m}^2 \times 2.84 \frac{\text{W}}{\text{m}^2 \text{K}} \times 24.8 \text{ K} = 253.56 \text{ W} \end{aligned}$$

If the frame is aluminum

$$U'_{\text{south window}} = 3.61 \frac{\text{W}}{\text{m}^2 \text{K}}$$

$$SHGC' = 0.56$$

Cooling load

$$\begin{aligned} CF'_{\text{south window(heat transfer)}} &= U'_{\text{south window}} (\Delta T_{\text{cooling}} - 0.46 \text{ DR}) \\ &= 3.61 \frac{\text{W}}{\text{m}^2 \text{K}} (7.9 \text{ K} - 0.46 \times 11.9 \text{ K}) = 8.76 \frac{\text{W}}{\text{m}^2} \end{aligned}$$

$$CF'_{\text{south window(irradiation)}} = P_{XI} \times SHGC' \times IAC \times FF_s = 557 \times 0.56 \times 1 \times 0.47 = 146.6$$

$$\begin{aligned} q'_{\text{south window}} &= A \times (CF'_{\text{south window(heat transfer)}} + (CF'_{\text{south window(irradiation)}})) \\ &= 3.6 \text{ m}^2 \times (8.76 + 146.60) \frac{\text{W}}{\text{m}^2} = 559.30 \text{ W} \end{aligned}$$

Heating load

$$\begin{aligned} q'_{\text{south window}} &= A \times HF'_{\text{south window}} = A \times U'_{\text{south window}} \times \Delta T_{\text{heating}} \\ &= 3.6 \text{ m}^2 \times 3.61 \frac{\text{W}}{\text{m}^2 \text{K}} \times 24.8 \text{ K} = 322.30 \text{ W} \end{aligned}$$

OPERABLE WINDOW ON SOUTH SIDE

$$\text{Area} = 3.6 \text{ m}^2$$

COOLING LOAD

$$q_{\text{south window}} = A \times CF_{\text{south window}}$$

$$CF_{\text{south window(heat transfer)}} = U_{\text{south window}} (\Delta T_{\text{cooling}} - 0.46 \text{ DR})$$

$$U_{\text{south window}} = 2.87 \frac{\text{W}}{\text{m}^2 \text{K}}$$

$$CF_{\text{south window(heat transfer)}} = 2.87 \frac{\text{W}}{\text{m}^2 \text{K}} (7.9 \text{ K} - 0.46 (11.9 \text{ K})) \approx 6.96 \frac{\text{W}}{\text{m}^2}$$

Irradiation

$$E_D = 348$$

$$E_d = 209$$

$$P_{\text{XI south window}} = E_D + E_d = 348 + 209 = 557$$

Since no internal shading, so IAC = 1

$$\text{SHGC} = 0.46$$

$$FF_s = 0.47$$

$$CF_{\text{south window(irradiation)}} = P_{\text{XI}} \times \text{SHGC} \times \text{IAC} \times FF_s = 557 \times 0.46 \times 1 \times 0.47 = 120.42$$

$$\begin{aligned} q_{\text{south window}} &= A \times CF_{\text{south window}} = A (CF_{\text{south window(heat transfer)}} + (CF_{\text{south window(irradiation)}})) \\ &= 3.6 \text{ m}^2 \times (6.96 + 120.42) \frac{\text{W}}{\text{m}^2} = 458.58 \text{ W} \end{aligned}$$

HEATING LOAD

$$\begin{aligned} q_{\text{south window}} &= A \times HF_{\text{south window}} = A \times U_{\text{south window}} \times \Delta T_{\text{heating}} \\ &= 3.6 \text{ m}^2 \times 2.87 \frac{\text{W}}{\text{m}^2 \text{K}} \times 24.8 \text{ K} = 256.23 \text{ W} \end{aligned}$$

If the frame is aluminium

$$U'_{\text{south window}} = 4.62 \frac{\text{W}}{\text{m}^2 \text{K}}$$

$$\text{SHGC}' = 0.55$$

Cooling load

$$\begin{aligned} CF'_{\text{south window(heat transfer)}} &= U'_{\text{south window}} (\Delta T_{\text{cooling}} - 0.46 \text{ DR}) \\ &= 4.62 \frac{\text{W}}{\text{m}^2 \text{K}} (7.9 \text{ K} - 0.46 \times 11.9 \text{ K}) = 11.21 \frac{\text{W}}{\text{m}^2} \end{aligned}$$

$$CF'_{\text{west window(irradiation)}} = P_{\text{XI}} \times \text{SHGC}' \times \text{IAC} \times FF_s = 557 \times 0.55 \times 1 \times 0.47 = 143.98$$

$$\begin{aligned} q'_{\text{west window}} &= A \times (CF'_{\text{west window(heat transfer)}} + (CF'_{\text{west window(irradiation)}})) \\ &= 3.6 \text{ m}^2 \times (11.21 + 143.98) \frac{\text{W}}{\text{m}^2} = 558.70 \text{ W} \end{aligned}$$

Heating load

$$\begin{aligned} q'_{\text{south window}} &= A \times HF'_{\text{south window}} = A \times U'_{\text{south window}} \times \Delta T_{\text{heating}} \\ &= 3.6 \text{ m}^2 \times 4.62 \frac{\text{W}}{\text{m}^2 \text{K}} \times 24.8 \text{ K} = 412.47 \text{ W} \end{aligned}$$