

## Task 1

Use a weather forecast website, and utilize the psychrometric chart and the formula we went through in the class to determine the absolute humidity, the wet-bulb temperature and the mass of water vapor in the air in Classroom A (Aula A) of Piacenza campus in the moment that you are solving this exercise (provide the inputs that you utilized)

Umidità: Relative humidity, Pressione atmosferica: Air total pressure (1 hPa: 0.1 kPa), Temperatura effettiva: temperature to be utilized. tal pressure (1 hPa: 0.1 kPa), Temperatura effettiva: temperature to be utilized.

The weather today in Piacenza Monday, 16 December 2019		
	22:00	23:00
	 Light Rain	 Light Rain
Effective temperature	6 °C	7 °C
Perceived temperature	6 °C	7 °C
Rainfall	0 mm	0 mm
Humidity	96 %	95 %
Atmospheric pressure	1021 hPa	1020 hPa
Wind intensity	3 km / h	2 km / h
Wind direction		

Humidity  $\phi = 95\%$

The total air pressure  $P = 102 \text{ kPa}$

Effective temperature:  $7^\circ\text{C}$ , i.e., the temperature in Kelvin temperature scale  $T = 280 \text{ K}$

the absolute humidity  $\omega = 0.0055$

the web-bulb temperature  $T_{wb} = 6^\circ\text{C}$

$\omega = 0.622 P_v / P = 0.622 P_v / (P - P_v) = 0.0055$ ,  $P = 102 \text{ kPa}$

$$\omega = \frac{0.622 \times P_v}{P - P_v} \quad 0.0055 = \frac{0.622 \times P_v}{102 - P_v} \quad P_v \approx 0.893 \text{ kPa}$$

Classroom volume:  $300 \text{ m}^3$     Dimension  $5 \cdot 10 \cdot 6$

$R_v = 0.4615$

$$m_v = \frac{P_v V}{R_v T} \quad m_v = \frac{0.893 \times 300}{0.4615 \times 280} \approx 2.07 \text{ kg}$$

## Task 2

BRINDISI, Italy

WMO#: 163200

Lat: 40.65N Long: 17.95E Elev: 10 StdP: 101.2 Time Zone: 1.00 (EUW) Period: 86-10 WBAN: 99999

### Annual Heating and Humidification Design Conditions

Coldest Month	Heating DB		Humidification DP/MCDB and HR						Coldest month WS/MCDB				MCWS/PCWD to 99.6% DB	
			99.6%			99%			0.4%		1%			
	99.6%	99%	DP	HR	MCDB	DP	HR	MCDB	WS	MCDB	WS	MCDB	MCWS	PCWD
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)
2	2.9	4.1	-5.1	2.5	7.2	-3.0	3.0	7.4	13.4	10.2	12.4	10.6	3.4	250

### Annual Cooling, Dehumidification, and Enthalpy Design Conditions

(7)	Hottest Month	Hottest Month DB Range	Cooling DB/MCWB						Evaporation WBM/CDB						MCWS/PCWD to 0.4% DB		
			0.4%		1%		2%		0.4%		1%		2%				
			DB	MCWB	DB	MCWB	DB	MCWB	WB	MCDB	WB	MCDB	WB	MCDB	MCWS	PCWD	
	(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)	
	8	7.1	32.8	23.6	31.1	24.3	29.9	24.3	27.2	29.7	26.3	29.0	25.6	28.3	4.2	180	
	(2)																
(3)	Dehumidification DPM/CDB and HR												Enthalpy/MCDB				Hours 8 to 4 & 12.8/20.6
	0.4%			1%			2%			0.4%		1%		2%			
	DP	HR	MCDB	DP	HR	MCDB	DP	HR	MCDB	Enth	MCDB	Enth	MCDB	Enth	MCDB		
	(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)	
	26.3	21.8	29.2	25.4	20.7	28.5	24.7	19.7	27.9	86.0	30.1	82.2	29.1	78.5	28.3	1236	
	(2)																

### Extreme Annual Design Conditions

Extreme Annual WS			Extreme Max WB	Extreme Annual DB				n-Year Return Period Values of Extreme DB							
				Mean	Standard deviation	Min	Max	n=5 years		n=10 years		n=20 years		n=50 years	
1%	2.5%	5%						Min	Max	Min	Max	Min	Max	Min	Max
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)
11.3	9.9	8.7	31.4	0.4	37.3	1.4	3.0	-0.6	39.4	-1.4	41.1	-2.2	42.8	-3.2	44.9

$$q_{ig}, s = 136 + 2.2A_{cf} + 22N_{oc} = 136 + 2.2 \cdot 200 + 22 \cdot 2 = 620 \text{ W}$$

$$q_{ig}, l = 20 + 0.22A_{cf} + 12N_{oc} = 20 + 0.22 \cdot 200 + 12 \cdot 2 = 88 \text{ W}$$

for a house with a good construction quality, unit leakage area  $A_{ul} = 1.4 \text{ cm}^2/\text{m}^2$   
 and the exposed surface  $A_{es} = A_{wall} + A_{roof} = 200 + 144 = 344 \text{ m}^2$   
 thus,  $AL = A_{es} \cdot A_{ul} = 344 \cdot 1.4 = 481.6 \text{ cm}^2$

cooling temperature  $T_{cooling} = 24^\circ\text{C}$ , and heating temperature  $T_{heating} = 20^\circ\text{C}$

$$\Delta T_{cooling} = 31.1^\circ\text{C} - 24^\circ\text{C} = 7.1^\circ\text{C} = 7.1 \text{ K}$$

$$\Delta T_{heating} = 20^\circ\text{C} - (-4.1^\circ\text{C}) = 24.1^\circ\text{C} = 24.1 \text{ K}$$

$$DR = 7.1^\circ\text{C} = 7.1 \text{ K}$$

Given that  $IDF_{heating} = 0.073 \text{ L/s} \cdot \text{cm}^2$ ,

$$IDF_{cooling} = 0.033 \text{ L/s} \cdot \text{cm}^2,$$

Calculate infiltration airflow rate,

$$Q_{i, \text{heating}} = AL \cdot IDF_{heating} = 481.6 \cdot 0.073 \approx 35.157 \text{ L/s}$$

$$Q_{i, \text{cooling}} = AL \cdot IDF_{cooling} = 481.6 \cdot 0.033 \approx 15.893 \text{ L/s}$$

The required minimum whole-building ventilation rate is

$$Q_v = 0.05A_{cf} + 3.5(N_{br} + 1) = 0.05 \cdot 200 + 3.5 \cdot (1 + 1) = 17 \text{ L/s}$$

$$Q_{i-v, \text{heating}} = Q_{i, \text{heating}} + Q_v \approx 35.157 + 17 = 52.157 \text{ L/s}$$

$$Q_{i-v, \text{cooling}} = Q_{i, \text{cooling}} + Q_v \approx 15.893 + 17 = 32.893 \text{ L/s}$$

Given that  $C_{sensible} = 1.23$ ,  $C_{latent} = 3010$ ,  $\Delta\omega_{cooling} = 0.0039$

$$q_{inf-v, \text{cooling sensible}} = C_{sensible} Q_{i-v, \text{cooling}} \Delta T_{cooling} \approx 1.23 \cdot 32.893 \cdot 7.1 \approx 287.25 \text{ W}$$

$$q_{inf-v, \text{cooling latent}} = C_{latent} Q_{i-v, \text{cooling}} \Delta\omega_{cooling} \approx 3010 \cdot 32.893 \cdot 0.0039 \approx 386.13 \text{ W}$$

$$q_{inf-v, \text{heating sensible}} = C_{sensible} Q_{i-v, \text{heating}} \Delta T_{heating} \approx 1.23 \cdot 52.157 \cdot 24.1 \approx 1546.09 \text{ W}$$