

# Week Assignment 9

## Question 1

Use a weather forecast website, and utilize the psychrometric chart and the formula we went through in the class to determine the absolute humidity, the wet-bulb temperature and the mass of water vapour in the air in Classroom A (Aula A) of Piacenza campus in the moment that you are solving this exercise (provide the inputs that you utilized)

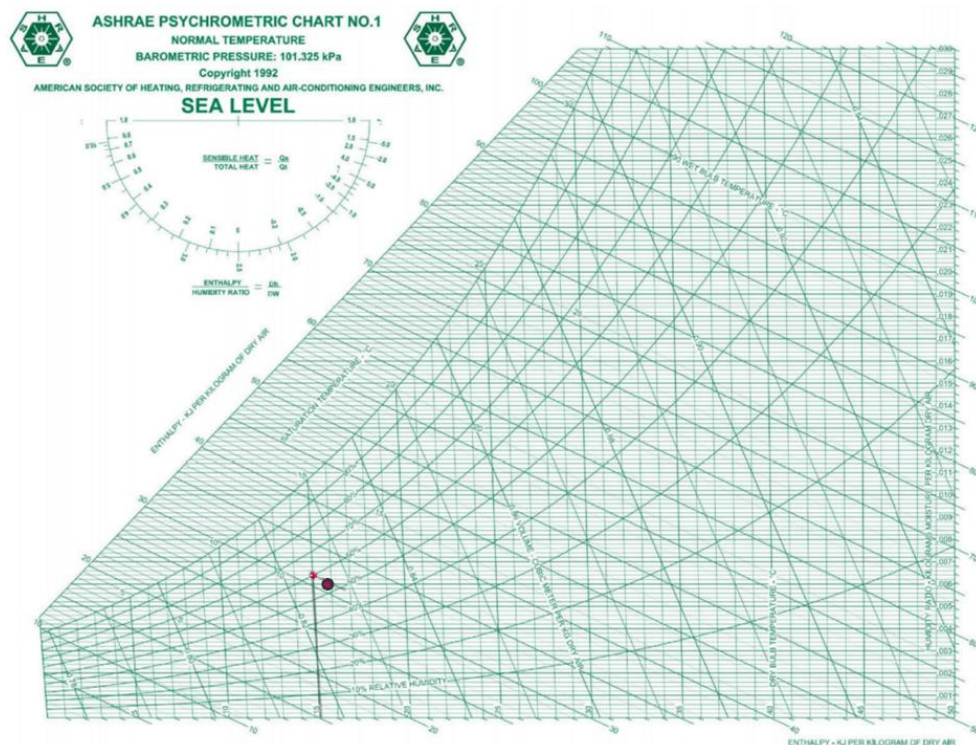
### Solution

On 2 December 2019, 10pm

Effective Temperature =  $8^{\circ}\text{C}$

Atmospheric Pressure = 102 kPa

Relative Humidity = 92%



$$\text{Absolute Humidity } (\omega) = 0.006 \left( \frac{\text{kg vapour}}{\text{kg dry air}} \right)$$

$$\text{Wet bulb temperature} = 7.2^{\circ}\text{C}$$

$$\text{Mass of water vapor, } m_v = \frac{P_v V_v}{R_v T}$$

$$\phi = \frac{m_v}{m_g} = \frac{P_v}{P_g}$$

At  $8^{\circ}\text{C}$ ,  $P_g = 1.07 \text{ kPa}$  (from steam table)

**SATURATED STEAM - TEMPERATURE TABLE**

|         | Spec. vol.<br>m <sup>3</sup> =kg |   | Int. Ener.<br>kJ/kg            |                                | Enthalpy<br>kJ/kg              |                                | Entropy<br>kJ=(kg°K)           |                                |                                |
|---------|----------------------------------|---|--------------------------------|--------------------------------|--------------------------------|--------------------------------|--------------------------------|--------------------------------|--------------------------------|
| T<br>°C | P<br>bar                         | Sat.<br>liq.<br>v <sub>f</sub><br>X1000 | Sat.<br>vap.<br>v <sub>g</sub> | Sat.<br>liq.<br>u <sub>f</sub> | Sat.<br>vap.<br>u <sub>g</sub> | Sat.<br>liq.<br>h <sub>f</sub> | Sat.<br>vap.<br>h <sub>g</sub> | Sat.<br>liq.<br>s <sub>f</sub> | Sat.<br>vap.<br>s <sub>g</sub> |
| 0.01    | 0.0061                           | 1.0002                                  | 206.1                          | 0.01                           | 2376                           | 0.01                           | 2501                           | 0                              | 9.156                          |
| 4       | 0.0081                           | 1.0001                                  | 157.2                          | 16.79                          | 2381                           | 16.79                          | 2509                           | 0.061                          | 9.051                          |
| 5       | 0.0087                           | 1.0001                                  | 147.1                          | 21.00                          | 2383                           | 21                             | 2511                           | 0.0762                         | 9.026                          |
| 6       | 0.0093                           | 1.0001                                  | 137.7                          | 25.21                          | 2384                           | 25.21                          | 2512                           | 0.0912                         | 9.000                          |
| 8       | 0.0107                           | 1.0001                                  | 120.9                          | 33.61                          | 2387                           | 33.61                          | 2516                           | 0.1212                         | 8.950                          |
| 10      | 0.0123                           | 1.0001                                  | 106.4                          | 42.01                          | 2389                           | 42.01                          | 2520                           | 0.151                          | 8.901                          |
| 11      | 0.0131                           | 1.0007                                  | 99.86                          | 46.19                          | 2391                           | 46.19                          | 2522                           | 0.1658                         | 8.876                          |
| 12      | 0.0140                           | 1.0007                                  | 93.79                          | 50.40                          | 2392                           | 50.4                           | 2523                           | 0.1806                         | 8.852                          |

$$P_v = \phi \times P_g = 0.92 \times 1.07 = 0.9844 \text{ kPa}$$

$$R_v = 0.4615$$

$$\text{Volume (Aula A)} = 10 \times 20 \times 3 = 600 \text{ m}^3$$

$$m_v = \frac{0.9844 \times 600}{0.4615 \times 281} = 4.55 \text{ kg}$$

## Question 2

Utilize the same methodology we went through in the class and determine the sensible and latent load corresponding to internal gains, the ventilation, and the infiltration in a house with a *good* construction quality and with the same geometry as that of the example which is located in Brindisi, Italy

BRINDISI, Italy

WMO#: 163200

Lat: 40.65N Long: 17.95E Elev: 10 StdP: 101.2 Time Zone: 1.00 (EUW) Period: 86-10 WBAN: 99999

Annual Heating and Humidification Design Conditions

| Coldest Month | Heating DB |     |      | Humidification DP/MCDB and HR |     |      |     |      |      | Coldest month WS/MCDB |      |      |     | MCWS/PCWD to 99.6% DB |  |
|---------------|------------|-----|------|-------------------------------|-----|------|-----|------|------|-----------------------|------|------|-----|-----------------------|--|
|               |            |     |      | 99.6%                         |     |      | 99% |      |      | 0.4%                  |      | 1%   |     |                       |  |
|               | DP         | HR  | MCDB | DP                            | HR  | MCDB | WS  | MCDB | WS   | MCDB                  | MCWS | PCWD |     |                       |  |
| (a)           | (b)        | (c) | (d)  | (e)                           | (f) | (g)  | (h) | (i)  | (j)  | (k)                   | (l)  | (m)  | (n) | (o)                   |  |
| 2             | 2.9        | 4.1 | -5.1 | 2.5                           | 7.2 | -3.0 | 3.0 | 7.4  | 13.4 | 10.2                  | 12.4 | 10.6 | 3.4 | 250                   |  |

Annual Cooling, Dehumidification, and Enthalpy Design Conditions

| Hottest Month | Hottest Month DB Range | Cooling DB/MCWB |      |      |      |      |      | Evaporation WB/MCDB |      |      |      |      |      | MCWS/PCWD to 0.4% DB |      |
|---------------|------------------------|-----------------|------|------|------|------|------|---------------------|------|------|------|------|------|----------------------|------|
|               |                        | 0.4%            |      | 1%   |      | 2%   |      | 0.4%                |      | 1%   |      | 2%   |      |                      |      |
|               |                        | DB              | MCWB | DB   | MCWB | DB   | MCWB | WB                  | MCDB | WB   | MCDB | WB   | MCDB | MCWS                 | PCWD |
| (a)           | (b)                    | (c)             | (d)  | (e)  | (f)  | (g)  | (h)  | (i)                 | (j)  | (k)  | (l)  | (m)  | (n)  | (o)                  | (p)  |
| 8             | 7.1                    | 32.8            | 23.6 | 31.1 | 24.3 | 29.9 | 24.3 | 27.2                | 29.7 | 26.3 | 29.0 | 25.6 | 28.3 | 4.2                  | 180  |

|      | Dehumidification DP/MCDB and HR |      |      |      |      |      | Enthalpy/MCDB |      |      |      |      |      | Hours 8 to 4 & 12.8/20.6 |      |      |      |  |    |
|------|---------------------------------|------|------|------|------|------|---------------|------|------|------|------|------|--------------------------|------|------|------|--|----|
|      | 0.4%                            |      |      | 1%   |      |      | 2%            |      |      | 0.4% |      |      |                          |      | 1%   |      |  | 2% |
|      | DP                              | HR   | MCDB | DP   | HR   | MCDB | DP            | HR   | MCDB | Enth | MCDB | Enth | MCDB                     | Enth | MCDB | Enth |  |    |
| (a)  | (b)                             | (c)  | (d)  | (e)  | (f)  | (g)  | (h)           | (i)  | (j)  | (k)  | (l)  | (m)  | (n)                      | (o)  | (p)  |      |  |    |
| 26.3 | 21.8                            | 29.2 | 25.4 | 20.7 | 28.5 | 24.7 | 19.7          | 27.9 | 86.0 | 30.1 | 82.2 | 29.1 | 78.5                     | 28.3 | 1236 |      |  |    |

Extreme Annual Design Conditions

| Extreme Annual WS |      |     | Extreme Max WB | Extreme Annual DB |      |                    |     | n-Year Return Period Values of Extreme DB |      |            |      |            |      |            |      |
|-------------------|------|-----|----------------|-------------------|------|--------------------|-----|---|------|------------|------|------------|------|------------|------|
|                   |      |     |                | Mean              |      | Standard deviation |     | n=5 years                                 |      | n=10 years |      | n=20 years |      | n=50 years |      |
| 1%                | 2.5% | 5%  |                | Min               | Max  | Min                | Max | Min                                       | Max  | Min        | Max  | Min        | Max  | Min        | Max  |
| (a)               | (b)  | (c) | (d)            | (e)               | (f)  | (g)                | (h) | (i)                                       | (j)  | (k)        | (l)  | (m)        | (n)  | (o)        | (p)  |
| 11.3              | 9.9  | 8.7 | 31.4           | 0.4               | 37.3 | 1.4                | 3.0 | -0.6                                      | 39.4 | -1.4       | 41.1 | -2.2       | 42.8 | -3.2       | 44.9 |

### Solution

Room height,  $h=2.5\text{m}$

Good construction quality – 2 occupants, 1 bedroom

Conditioned floor area =  $200\text{ m}^2$

Wall Area =  $144\text{ m}^2$

### Internal Gains

$$\dot{Q}ig_{sensible} = 136 + 2.2 \times A_{cf} + 22N_{oc} = 136 + 2.2(200) + 22(2) = 620\text{ W}$$

$$\dot{Q}ig_{latent} = 20 + 0.22 \times A_{cf} + 12N_{oc} = 20 + 0.22(200) + 12(2) = 88\text{ W}$$

### Infiltration

$$A_{es} \text{ (exposed surface area)} = 200 + 144 = 344\text{ m}^2$$

$$A_{ul} \text{ (unit leakage area for good quality construction)} = 1.4 \frac{\text{cm}^2}{\text{m}^2}$$

**Table 3 Unit Leakage Areas**

| Construction | Description  | $A_{ul}, \text{cm}^2/\text{m}^2$ |
|--------------|--|----------------------------------|
| Tight        | Construction supervised by air-sealing specialist      | 0.7                              |
| Good         | Carefully sealed construction by knowledgeable builder | 1.4                              |
| Average      | Typical current production housing                     | 2.8                              |
| Leaky        | Typical pre-1970 houses                                | 5.6                              |
| Very leaky   | Old houses in original condition                       | 10.4                             |

$$A_L \text{ (Leakage area)} = A_{es} \times A_{ul} = 344 \times 1.4 = 481.6\text{ cm}^2$$

**Table 5 Typical IDF Values,  $\text{L}/(\text{s} \cdot \text{cm}^2)$**

| $H,$<br>m | Heating Design<br>Temperature, °C |       |       |       |       | Cooling Design<br>Temperature, °C |       |       |       |
|-----------|-----------------------------------|-------|-------|-------|-------|-----------------------------------|-------|-------|-------|
|           | -40                               | -30   | -20   | -10   | 0     | 10                                | 30    | 35    | 40    |
| 2.5       | 0.10                              | 0.095 | 0.086 | 0.077 | 0.069 | 0.060                             | 0.031 | 0.035 | 0.040 |
| 3         | 0.11                              | 0.10  | 0.093 | 0.083 | 0.072 | 0.061                             | 0.032 | 0.038 | 0.043 |
| 4         | 0.14                              | 0.12  | 0.11  | 0.093 | 0.079 | 0.065                             | 0.034 | 0.042 | 0.049 |
| 5         | 0.16                              | 0.14  | 0.12  | 0.10  | 0.086 | 0.069                             | 0.036 | 0.046 | 0.055 |
| 6         | 0.18                              | 0.16  | 0.14  | 0.11  | 0.093 | 0.072                             | 0.039 | 0.050 | 0.061 |
| 7         | 0.20                              | 0.17  | 0.15  | 0.12  | 0.10  | 0.075                             | 0.041 | 0.051 | 0.068 |
| 8         | 0.22                              | 0.19  | 0.16  | 0.14  | 0.11  | 0.079                             | 0.043 | 0.058 | 0.074 |

Heating Design Temperature =  $4.1\text{ }^\circ\text{C}$

Cooling Design Temperature =  $31.1\text{ }^\circ\text{C}$

## Volume

$$V_{infiltration_{heating}} = A_L \times IDF_{heating} = 481.6 \times 0.065 = 31.304 \frac{L}{s}$$

$$V_{infiltration_{cooling}} = A_L \times IDF_{cooling} = 481.6 \times 0.0317 = 15.266 \frac{L}{s}$$

## Ventilation

$$\dot{v}_v = 0.05 A_{cf} + 3.5 (N_{br} + 1) = 0.05(200) + 3.5(1+1) = 17 \frac{L}{s}$$

$$\dot{Q}_{infiltration_{heating}} = 31.304 + 17 = 48.304 \frac{L}{s}$$

$$\dot{Q}_{infiltration_{cooling}} = 15.266 + 17 = 32.266 \frac{L}{s}$$

$$\dot{Q}_{inf-ventilation_{heating_{sensible}}} = C_{sensible} \dot{v} \Delta T_{heating} = 1.23 \times 48.304 \times (20 - 4.1) = 944.681 \text{ W}$$

$$\dot{Q}_{inf-ventilation_{cooling_{sensible}}} = C_{sensible} \dot{v} \Delta T_{cooling} = 1.23 \times 32.266 \times (31.1 - 24) = 281.779 \text{ W}$$

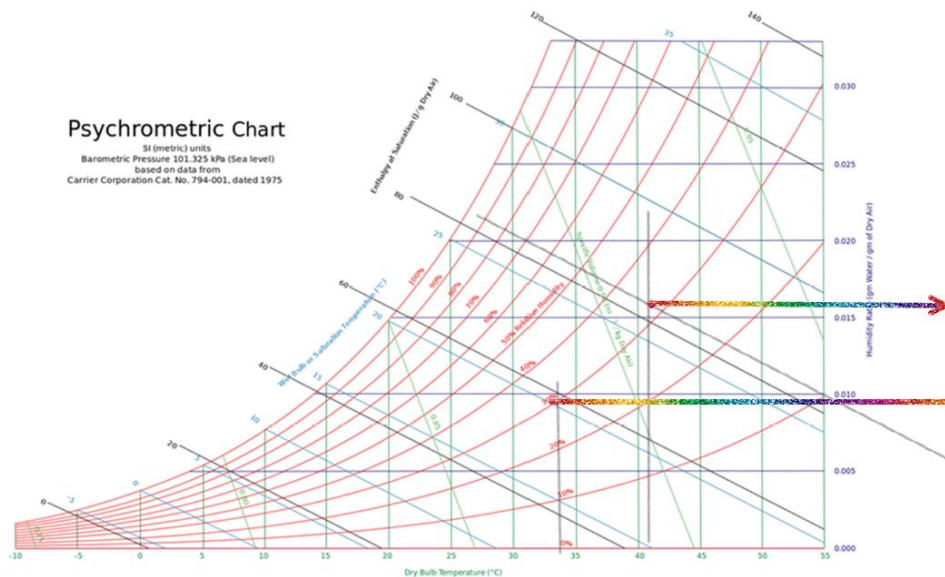
For latent load calculation, we need  $\Delta\omega_{cooling}$

Refer to psychrometric chart (DB = 31.1°C, WB = 24.3°C)

$$\omega_{out} = 0.016$$

$$\omega_{in} = 0.0093$$

$$\Delta\omega_{cooling} = 0.0067$$



Therefore,

$$\dot{Q}_{inf-ventilation_{cooling_{latent}}} = C_{latent} \dot{v} \Delta\omega_{cooling} = 3010 \times 32.266 \times 0.0067 = 650.708 \text{ W}$$