















## Task 1

Use a weather forecast website, and utilize the psychrometric chart and the formula we went through in the class to determine the absolute humidity, the wet-bulb temperature and the mass of water vapor in the air in Classroom A (Aula A) of Piacenza campus in the moment that you are solving

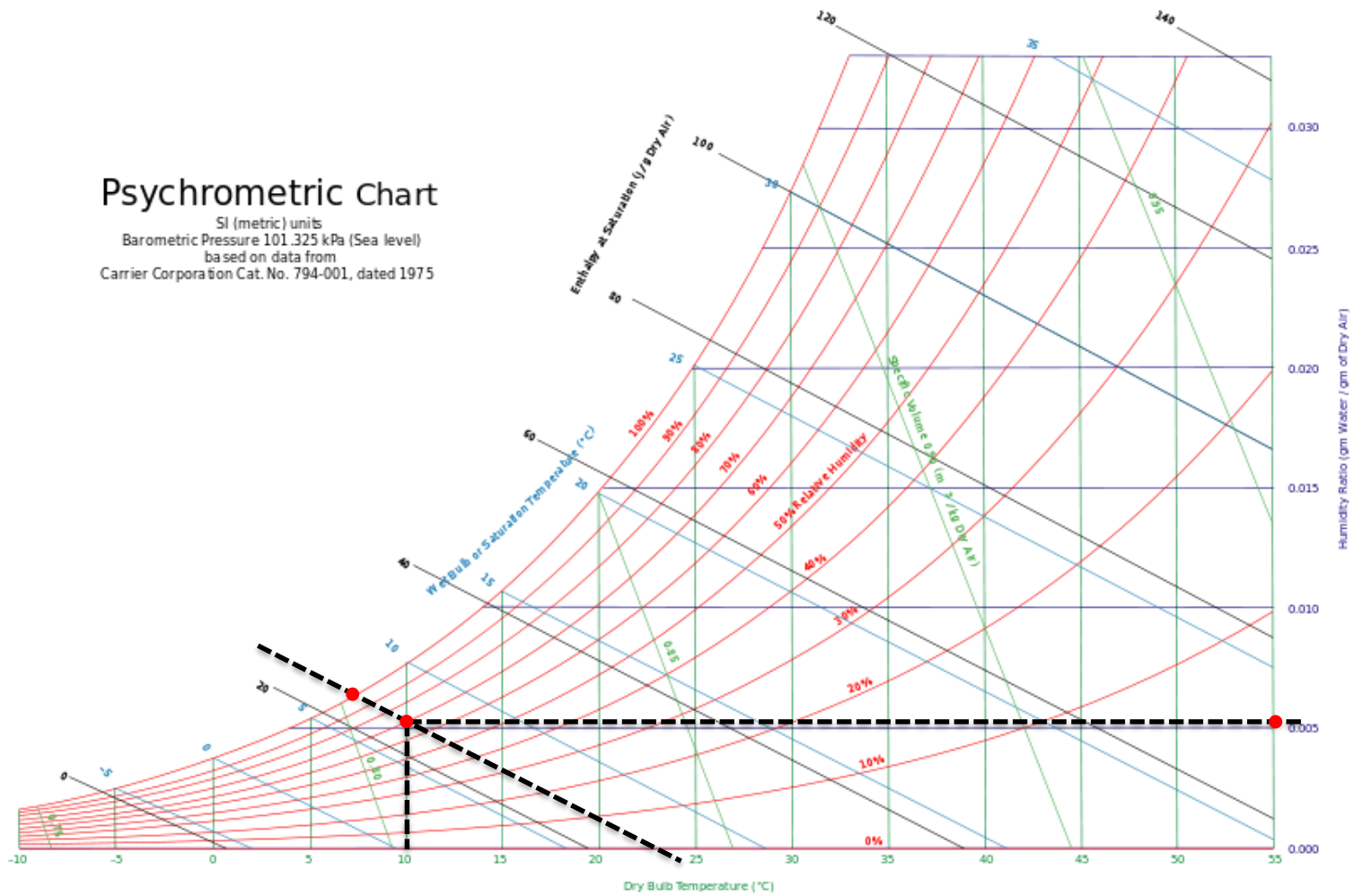
Umidità: Relative humidity, Pressione atmosferica: Air total pressure (1 hPa: 0.1 kPa), Temperature effettiva: temperature to be utilized.

The weather today in Piacenza Tuesday, 03 December 2019							
	1:00 pm	14:00	4:00 pm	18:00	8:00 pm	21:00	22:00
							
	LightCloud	LightCloud	PartlyCloud	LightCloud	Sun	Sun	Sun
Effective temperature	9 °C	10 °C	8 °C	6 °C	4 °C	2 °C	2 °C
Perceived temperature	7 °C	10 °C	6 °C	4 °C	2 °C	0 °C	0 °C
Rainfall	0 mm	0 mm	0 mm	0 mm	0 mm	0 mm	0 mm
Humidity	67 %	65 %	69 %	70 %	75 %	83 %	87 %
Atmospheric pressure	1025 hPa	1025 hPa	1025 hPa	1026 hPa	1027 hPa	1027 hPa	1028 hPa
Wind intensity	15 km / h	14 km / h	9 km / h	9 km / h	7 km / h	8 km / h	8 km / h
Wind direction							

The hour at the moment is 14:30. According to the weather forecast shown above we know that there is no chances of rainfall, effective temperature 9°C ( $T = 282.15$  Kelvin), the humidity is 65% (relative humidity  $\phi = 65\%$ ), and the atmospheric pressure 1025 hPa (total air pressure  $P = 102.5$  kPa)

# Psychrometric Chart

SI (metric) units  
Barometric Pressure 101.325 kPa (Sea level)  
based on data from  
Carrier Corporation Cat. No. 794-001, dated 1975



Utilize the psychrometric chart, we can see, the humidity ratio, i.e., the absolute humidity  $\omega=0.0052$

The web-bulb temperature  $T_{wb} = 10^{\circ}\text{C}$

Therefore  $\omega = \frac{0.622 P_v}{P_a} = \frac{0.622 P_v}{P - P_v} = 0.0052$ , introduce  $P = 102.5$  KPa into this equation, and solve it.

$$\frac{0.622 P_v}{102.5 - P_v} = 0.0052$$

$$P_v = 0.8498 \text{ KPa}$$

$$\text{Autem, } \phi = \frac{m_v}{m_g} = 70\% \dots\dots (1)$$

For any ideal gas,  $m = \frac{P_v}{R_{sp} T}$ , during the class we were told that for water vapor,  $R_{sp} = 0.4615$

Introduce the pressure of water vapor  $P_v = 0.8498$  KPa, and define the volume of Aula A is

$$V: m_v = \frac{0.8498 V}{0.4615 \cdot 282.15} = 130.212225 \text{ V}$$

Subordinate this value to equation number (1)

Calculate the maximum water vapor  $m_g = \frac{mv}{70\%} = 9.34 \times 10^{-3}V$

## Task 2

Utilize the same methodology we went through in the class and determine the sensible and latent load corresponding to internal gains, the ventilation, and the infiltration in a house with a *good* construction quality and with the same geometry as that of the example which is located in Brindisi, Italy

BRINDISI, Italy														WMO#: 163200		
Lat: 40.65N		Long: 17.95E		Elev: 10		StdP: 101.2		Time Zone: 1.00 (EUW)				Period: 86-10		WBAN: 99999		
Annual Heating and Humidification Design Conditions																
Coldest Month	Heating DB		Humidification DP/MCDB and HR						Coldest month WS/MCDB				MCWS/PCWD to 99.6% DB			
			99.6%			99%			0.4%		1%					
	99.6%	99%	DP	HR	MCDB	DP	HR	MCDB	WS	MCDB	WS	MCDB	MCWS	PCWD		
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)		
(1) 2	2.9	4.1	-5.1	2.5	7.2	-3.0	3.0	7.4	13.4	10.2	12.4	10.6	3.4	250	(1)	
Annual Cooling, Dehumidification, and Enthalpy Design Conditions																
Hottest Month	Hottest Month DB Range		Cooling DB/MCWB						Evaporation WB/MCDB						MCWS/PCWD to 0.4% DB	
			0.4%		1%		2%		0.4%		1%		2%			
	DB	MCWB	DB	MCWB	DB	MCWB	WB	MCDB	WB	MCDB	WB	MCDB	MCWS	PCWD		
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)	
(2) 8	7.1	32.8	23.6	31.1	24.3	29.9	24.3	27.2	29.7	26.3	29.0	25.6	28.3	4.2	180	(2)
	Dehumidification DP/MCDB and HR								Enthalpy/MCDB						Hours 8 to 4 & 12.8/20.6	
	0.4%		1%		2%		0.4%		1%		2%					
	DP	HR	MCDB	DP	HR	MCDB	DP	HR	MCDB	Enth	MCDB	Enth	MCDB	Enth	MCDB	
(3) 26.3	21.8	29.2	25.4	20.7	28.5	24.7	19.7	27.9	86.0	30.1	82.2	29.1	78.5	28.3	1236	(3)
Extreme Annual Design Conditions																
Extreme Annual WS			Extreme Max WB	Extreme Annual DB				n-Year Return Period Values of Extreme DB								
				Mean		Standard deviation		n=5 years		n=10 years		n=20 years		n=50 years		
1%	2.5%	5%		Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)	
(4) 11.3	9.9	8.7	31.4	0.4	37.3	1.4	3.0	-0.6	39.4	-1.4	41.1	-2.2	42.8	-3.2	44.9	(4)

Height= 2.5 m; Floor area= 200 m<sup>2</sup>; Wall area= 144 m<sup>2</sup>

Internal Gains:

Sensible cooling load from internal gains,

$$q_{ig,sensible} = 136 + 2.2A_{cr} + 22N_{oc} = 136 + 2.2 \cdot 200 + 22 \cdot 2 = 620W$$

Latent cooling load from internal gains,

$$q_{ig,latent} = 20 + 0.22A_{cr} + 12N_{oc} = 20 + 0.22 \cdot 200 + 12 \cdot 2 = 88W$$

Infiltration:

$$\text{Unit leakage area } A_{ul} = 1.4 \text{ cm}^2/\text{m}^2$$

$$\text{Exposed surface } A_L = A(\text{wall}) + A(\text{roof}) = 200 + 144 = 344\text{m}^2$$

$$\text{So, } A_L = A_{es} \cdot A_{ul} = 344 \cdot 1.4 = 481.6 \text{ cm}^2$$

Define the cooling temperature  $T_{cooling} = 24^\circ\text{C}$ , and heating temperature  $T_{heating} = 20^\circ\text{C}$  in Brindisi,

$$\Delta T_{cooling} = 31.1 - 24 = 7.1^\circ\text{C} = 7.1 \text{ K}$$

$$\Delta T_{\text{heating}} = 20^{\circ}\text{C} - (-4.1^{\circ}\text{C}) = 24.1^{\circ}\text{C} = 24.1 \text{ K}$$

$$\text{DR} = 7.1^{\circ}\text{C} = 7.1 \text{ K}$$

$$\text{Given: IDF (heating)} = 0.073 \frac{\text{L}}{\text{s} \cdot \text{cm}^2}$$

$$\text{IDF (cooling)} = 0.033 \frac{\text{L}}{\text{s} \cdot \text{cm}^2}$$

Calculate infiltration airflow rate,

$$Q_{i, \text{heating}} = A_L * \text{IDF}_{\text{heating}} = 481.6 * 0.073 = 35.157 \frac{\text{L}}{\text{s}}$$

$$Q_{i, \text{cooling}} = A_L * \text{IDF}_{\text{cooling}} = 481.6 * 0.033 = 15.893 \frac{\text{L}}{\text{s}}$$

The required minimum whole building ventilation rate is

$$Q_v = 0.05 A_{cf} + 3.5 (N_{br} + 1) = 0.05 * 200 + 3.5 * (1+1) = 17 \frac{\text{L}}{\text{s}}$$

Thus,

$$Q_{i-v, \text{heating}} = Q_{i, \text{heating}} + Q_v = 35.157 + 17 = 52.157 \frac{\text{L}}{\text{s}}$$

$$Q_{i-v, \text{cooling}} = Q_{i, \text{cooling}} + Q_v = 15.893 + 17 = 32.893 \frac{\text{L}}{\text{s}}$$

Given that  $C_{\text{sensible}} = 1.23$ ,  $C_{\text{latent}} = 3010$ ,  $\Delta \omega_{\text{cooling}} = 0.0039$

$$\dot{q}_{\text{inf-ventilation (cooling sensible)}} = C_{\text{sensible}} Q_{i-v, \text{cooling}} \Delta T_{\text{cooling}} = 1.23 * 32.893 * 7.1 = 287.25 \text{ W}$$

$$\dot{q}_{\text{inf-ventilation (cooling latent)}} = C_{\text{latent}} Q_{i-v, \text{cooling}} \Delta \omega_{\text{cooling}} = 3010 * 32.893 * 0.0039 = 386.13 \text{ W}$$

$$\dot{q}_{\text{inf-ventilation (heating sensible)}} = C_{\text{sensible}} Q_{i-v, \text{heating}} \Delta T_{\text{heating}} = 1.23 * 52.157 * 24.1 = 1546.09 \text{ W}$$