Hana Abou Baker

Task 1

Using the diagrams given in the presentation calculate how much (%) is the effect of applying different modifications (changing the gas, adding an extra pane, using a low emissivity coating) on the U value with respect to a benchmark case of double layer with air and no coating? (keep the gap thickness to be 13 mm)

$$U_{\text{window}} = \frac{U_{\text{center}} A_{\text{center}} + U_{\text{edge}} A_{\text{edge}} + U_{\text{fram}} U_{\text{fram}}}{A_{\text{window}}}$$

For double pan window, regardless of the thermal resistances of glass layers,

$$\frac{1}{U_{\text{double-pane(center region)}}} \approx \frac{1}{h_{i}} + \frac{1}{h_{\text{space}}} + \frac{1}{h_{o}}, h_{\text{space}} = h_{\text{rad,space}} + h_{\text{conv,space}}$$

 U_{center} , i.e. the h_{space} changes by changing the gas that fills the gap.

By changing the gas that fills the gap from air to argon, the U-value of the center of the glass decreases from $2.8 \frac{W}{m^2 K}$ to $2.65 \frac{W}{m^2 K}$, which means the u value decreases about 5.36%.

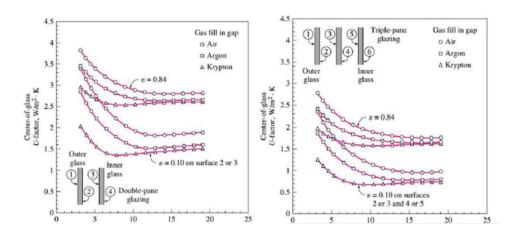
By changing the gas that fills the gap from air to Krypton, the U-value of the center of the glass decreases from $2.8 \frac{W}{m^2 K}$ to $2.6 \frac{W}{m^2 K}$, which means the u value decreases about 7.14%.

By adding an extra pane, the u-value of the center of the glass decreases $2.8 \frac{W}{m^2 K}$ to $1.8 \frac{W}{m^2 K'}$ which means the u value decreases about 35.71%.

Another way to change the U_{center} , is to coat the glass surfaces with a film that has a low emissivity.

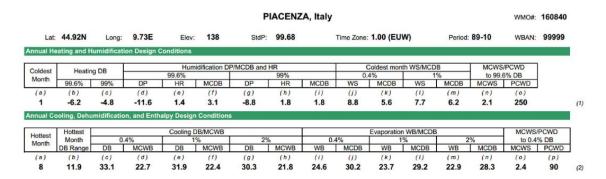
By coating the glass surfaces with a film that has the emissivity of 0.1, the U value of the center of the glass decreases from $2.8 \frac{W}{m^2 K}$ to $1.8 \frac{W}{m^2 K}$, which means the U value decreases about 35.71%

٤ value	0.84		0.10			0.84			0.10		
# of	2	2	2	2	2	3	3	3	3	3	3
panes											
Gas	Argon	Krypton	Air	Argon	Krypton	Air	Argon	Krypton	Air	Argon	krypton
U	2.65	2.6	1.8	1.5	1.4	1.8	1.7	1.6	1	0.8	0.75
value											
% of	5.36	7.14	35.71	46.42	50	35.71	39.2	42.85	64.28	71.4	73.21
change											



Task 2
Considering the house that we analyzed in the last two examples, calculate the heating and cooling load of the other windows which are fixed 14.4 sqm on the west, fixed 3.6 sqm on the south and an operable 3.6 sqm on the south (the same window and frame type). How much does the total value change if I change the frame of the window from wooden one to aluminum?

Here,



Temperature difference

$$\Delta T_{\text{cooling}} = 31.9 - 24 = 7.9 \,^{\circ}\text{C}$$

 $\Delta T_{\text{heating}} = 20 - (-4.8) = 24.8 \,^{\circ}\text{C}$
DR = 11.9 $^{\circ}\text{C}$

WEST WINDOW (FIXED)

Cooling Load: Wooden Frame

$$A = 14.4 \text{ m}^2$$

 $\dot{q}_{windowwest} = A \times CF_{windowwest}$

So,
$$CF_{windowwest} = CF_{windowwest_heattransfer} + CF_{windowwest_irridiation} = U(\Delta T - 0.46DR) + PXI x SHGC x IAC x FF_s$$

Here, U = 2.84, DR= 11.9, $\Delta T_{cooling} = 7.9$, SHGC = 0.54, IAC = 1 , FF_s = 0.56
PXI = $E_D - E_d = 559 + 188 = 747$
 $CF_{windowwest} = 2.84(7.9 - 0.46*11.9) + 747*0.54*1*0.56 = 232.78 \frac{W}{m^2}$
 $\dot{q}_{windowwest} = 14.4 \times 232.78 = 3352.07 \text{ W}$

Cooling Load: Aluminum Frame

$$A = 14.4 \text{ m}^2$$

 $\dot{q}_{windowwest} = A \times CF_{windowwest}$

So,
$$CF_{windowwest} = CF_{windowwest_heattransfer} + CF_{windowwest_irridiation} = U(\Delta T - 0.46DR) + PXI x SHGC x IAC x FF_s$$

Here, U = 3.61, DR= 11.9, $\Delta T_{cooling} = 7.9$, SHGC = 0.56, IAC = 1 , FF_s = 0.56
PXI = $E_D - E_d = 559 + 188 = 747$
 $CF_{windowwest} = 3.61(7.9 - 0.46*11.9) + 747*0.56*1*0.56 = 243.02 \frac{W}{m^2}$
 $\dot{q}_{windowwest} = 14.4 \times 243.02 = 3499.47 W$

Heating Load: Wooden Frame

$$A = 14.4 \text{ m}^2$$

$$\begin{split} \dot{q}_{windowwest} &= A \times CF_{windowwest} \\ HF_{windowwest} &= U_{windowwest} \times \Delta T_{heating} = 2.84 \times 24.8 = 70.43 \ \frac{W}{m^2} \\ \dot{q}_{windowwest} &= A \times HF_{windowwest} = 14.4 \times 70.43 = 1014.22 \ W \end{split}$$

Heating Load: Aluminum Frame

$$A = 14.4 \text{ m}^2$$

 $\begin{array}{l} \dot{q}_{windowwest} \ = \ A \ x \ CF_{windowwest} \\ HF_{windowwest} \ = \ U_{windowwest} \ x \ \Delta T_{heating} \ = \ 3.61 \ x \ 24.8 \ = \ 89.53 \ \frac{W}{m^2} \\ \dot{q}_{windowwest} \ = \ A \ x \ HF_{windowwest} \ = \ 14.4 \ x \ 89.53 \ = \ 1289.20 \ W \\ \end{array}$

So, The cooling load difference = 3499.47- 3352.07 = 147.4 W The heating load difference = 1289.20 - 1014.22 = 274.98 W

SOUTH WINDOW (FIXED)

Cooling Load: Wooden Frame

$$A = 3.6 \text{ m}^2$$

$$\begin{split} \dot{q}_{windowsouth} &= \text{A x CF}_{windowsouth} \\ \text{So,} \\ \text{CF}_{windowsouth} &= \text{CF}_{windowsouth_heattransfer} \, + \, \text{CF}_{windowsouth_irridiation} \\ &= \text{U}(\Delta \text{T} - 0.46 \text{DR}) + \text{PXI x SHGC x IAC x FF}_s \\ \text{Here, U = 2.84, DR= 11.9, } \Delta \text{T}_{cooling} &= 7.9, \text{ SHGC = 0.54, IAC = 1, FF}_s \, = \, 0.47 \\ \text{PXI = E}_D \, - \, \text{E}_d \, = \, 348 + 209 \, = \, 557 \\ \text{CF}_{windowsouth} \, = \, 2.84 (7.9 - 0.46*11.9) + 557*0.54*1*0.47 = 148.26 \, \frac{\text{W}}{\text{m}^2} \\ \dot{q}_{windowsouth} \, = \, 3.6 \, \, \text{x } \, 148.26 \, = \, 533.74 \, \, \text{W} \end{split}$$

Cooling Load: Aluminum Frame

$$A = 3.6 \text{ m}^2$$

Heating Load: Wooden Frame

$$A = 3.6 \text{ m}^2$$

$$\dot{q}_{windowsouth} = A \times HF_{windowsouth}$$

$$HF_{windowsouth} = U_{windowsouth} \times \Delta T_{heating} = 2.84 \times 24.8 = 70.43 \times \frac{W}{m^2}$$

$$\dot{q}_{windowsouth} = A \times HF_{windowsouth} = 3.6 \times 70.43 = 253.08 \times W$$

Heating Load: Aluminum Frame

$$A = 3.6 \text{ m}^2$$

 $\dot{q}_{windowsouth} = A x HF_{windowsouth}$

 $HF_{windowsouth} = U_{windowsouth} \times \Delta T_{heating} = 3.61 \times 24.8 = 89.53 \frac{W}{m^2}$

 $\dot{q}_{windowsouth} = A x HF_{windowsouth} = 3.6 x 89.53 = 322.31 W$

So, The cooling load difference = 559.30- 533.74 = 25.56 W The heating load difference = 322.31 - 253.08 = 69.23 W

SOUTH WINDOW (OPERABLE)

Cooling Load: Wooden Frame

 $A = 3.6 \text{ m}^2$

 $\dot{q}_{windowsouth} = A x CF_{windowsouth}$

So,

 $CF_{windowsouth} = CF_{windowsouth_heattransfer} + CF_{windowsouth_irridiation}$

= $U(\Delta T - 0.46DR) + PXI \times SHGC \times IAC \times FF_s$

Here, U = 2.87, DR= 11.9, $\Delta T_{cooling} = 7.9$, SHGC = 0.46, IAC = 1 , FF $_{s} = 0.47$

 $PXI = E_D - E_d = 348 + 209 = 557$

 $CF_{windowwest} = 2.87(7.9 - 0.46*11.9) + 557*0.46*1*0.47 = 127.38 \frac{W}{m^2}$

 $\dot{q}_{windowwest} = 3.6 \text{ x } 127.38 = 458.57 \text{ W}$

Cooling Load: Aluminum Frame

 $A = 3.6 \text{ m}^2$

 $\dot{q}_{windowsouth} = A x CF_{windowsouth}$

So,

 $CF_{windowsouth} = CF_{windowsouth_heattransfer} \ + \ CF_{windowsouth_irridiation}$

= $U(\Delta T - 0.46DR) + PXI \times SHGC \times IAC \times FF_s$

Here, U = 4.62, DR= 11.9, $\Delta T_{cooling} = 7.9$, SHGC = 0.55, IAC = 1 , FF $_{s} = 0.47$

 $PXI = E_D - E_d = 348 + 209 = 557$

 $CF_{windowwest} = 4.62(7.9 - 0.46*11.9) + 557*0.55*1*0.47 = 155.19 \frac{W}{m^2}$

 $\dot{q}_{windowwest} = 3.6 \text{ x } 155.19 = 558.68 \text{ W}$

Heating Load: Wooden Frame

$A = 3.6 \text{ m}^2$

 $\begin{array}{l} \dot{q}_{windowsouth} \; = \; A \; x \; HF_{windowsouth} \\ HF_{windowsouth} \; = \; U_{windowsouth} \; x \; \Delta T_{heating} = 2.87 \; x \; 24.8 = 71.18 \; \frac{W}{m^2} \\ \dot{q}_{windowsouth} \; = \; A \; x \; HF_{windowsouth} \; = \; 3.6 \; x \; 71.18 = 256.23 \; W \\ \end{array}$

Heating Load: Aluminum Frame

 $A = 3.6 \text{ m}^2$

So, The cooling load difference = 558.68- 458.57 = 100.11 W The heating load difference = 412.47 - 256.23 = 156.243 W