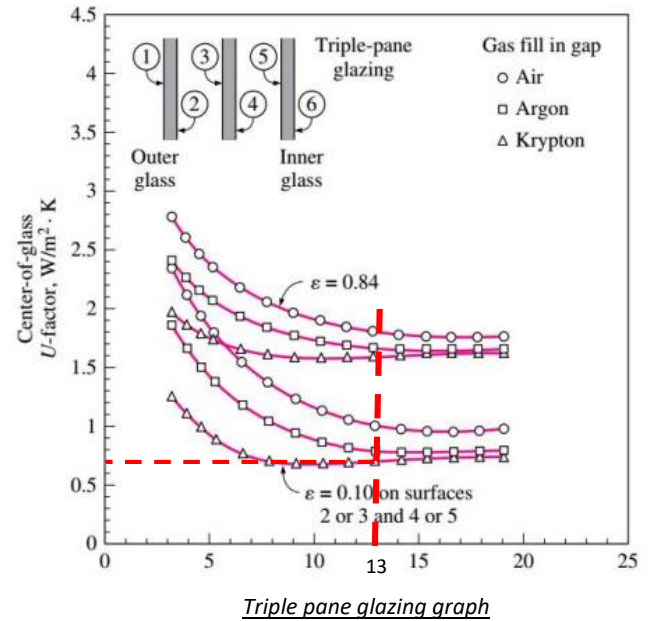
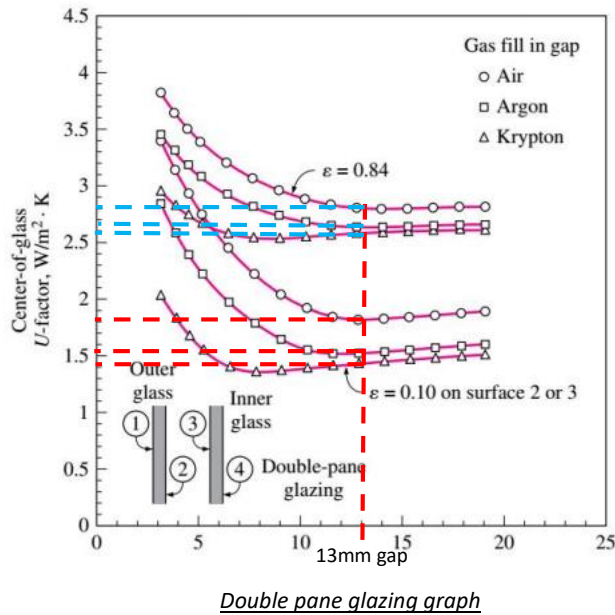


## Week 8

**Task 1** Using the diagrams given in the presentation calculate how much (%) is the effect of applying different modifications (changing the gas, adding an extra pane, using a low emissivity coating) on the U value with respect to a benchmark case of double layer with air and no coating?



| $\epsilon$        | 0.1     |       |       | 0.84    |       |     | 0.1     |       |       | 0.84    |       |       |
|-------------------|---------|-------|-------|---------|-------|-----|---------|-------|-------|---------|-------|-------|
| #Glazing          | 2       |       |       | 2       |       |     | 3       |       |       | 3       |       |       |
| Gas type          | Krypton | Argon | Air   | Krypton | Argon | Air | Krypton | Argon | Air   | Krypton | Argon | Air   |
| U Factor (W/m².K) | 1.4     | 1.5   | 1.8   | 2.6     | 2.65  | 2.8 | 0.7     | 0.8   | 1     | 1.6     | 1.7   | 1.8   |
| %                 | 50      | 46.42 | 35.71 | 7.14    | 5.36  | -   | 75      | 71.42 | 64.28 | 42.85   | 39.28 | 35.71 |

**Task 2** Consider the house that we analyzed in the last two examples, calculate the heating and cooling load of the other windows which are fixed 14.4 m<sup>2</sup> on the west, fixed 3.6 m<sup>2</sup> on the south and an operable 3.6 m<sup>2</sup> on the south (the same window and frame type). How much does the total value change if I change the frame of the window from wooden one to aluminum?

**Location:** Piacenza; **Latitude:** 44.92 N; **Longitudinal:** 9.73 E; **Elevation:** 138

T (heat)= 24°C; T (cool)= 20°C

Therefore,  $\Delta T_{\text{heating}} = 20 - (-4.8) = 24.8^\circ\text{C}$        $\Delta T_{\text{cooling}} = 31.9 - 24 = 7.9^\circ\text{C}$

DR= 11.9°C (from table)

1)

Calculating load of **fixed Wooden** window on the **WEST= 14.4 m<sup>2</sup>**:

a) Cooling

$$CF_{\text{ht}} = U(\Delta T_{\text{cooling}} - 0.46 \cdot DR) = 2.84 (7.9 - 0.46 \cdot 11.9) = 6.9 \text{ W/m}^2$$

$$CF_{\text{ip}} = \text{PXi} \cdot \text{SHGC} \cdot \text{IAC} \cdot \text{FF}_s = 747 \cdot 0.54 \cdot 1 \cdot 0.56 = 217.8 \text{ W/m}^2$$

$$CF(\text{total}) = 224.7 \text{ W/m}^2$$

$$\mathbf{Q(\text{cooling}) = CF(\text{total}) \cdot A = 224.7 \cdot 14.4 = 3235.7 \text{ W}}$$

b) Heating

$$HF = U \cdot \Delta T_{\text{heating}} = 2.84 \cdot 24.8 = 70.4 \text{ W/m}^2$$

$$\mathbf{Q(\text{heating}) = HF \cdot A = 70.4 \cdot 14.4 = 1013.8 \text{ W}}$$

Calculating load of **fixed Aluminum** window on the **WEST= 14.4 m<sup>2</sup>**:

a) Cooling

$$CF_{\text{ht}} = U(\Delta T_{\text{cooling}} - 0.46 \cdot DR) = 3.61 (7.9 - 0.46 \cdot 11.9) = 8.8 \text{ W/m}^2$$

$$CF_{\text{ip}} = \text{PXi} \cdot \text{SHGC} \cdot \text{IAC} \cdot \text{FF}_s = 747 \cdot 0.56 \cdot 1 \cdot 0.56 = 234.3 \text{ W/m}^2$$

$$CF(\text{total}) = 243.1 \text{ W/m}^2$$

$$\mathbf{Q(\text{cooling}) = CF(\text{total}) \cdot A = 243.1 \cdot 14.4 = 3500.64 \text{ W}}$$

b) Heating

$$HF = U \cdot \Delta T_{\text{heating}} = 3.61 \cdot 24.8 = 89.5 \text{ W/m}^2$$

$$\mathbf{Q(\text{heating}) = HF \cdot A = 89.5 \cdot 14.4 = 1288.8 \text{ W}}$$

2)

Calculating load of **fixed Wooden** window on the **SOUTH= 3.6 m<sup>2</sup>**:

a) Cooling

$$CF_{\text{ht}} = U(\Delta T_{\text{cooling}} - 0.46 \cdot DR) = 2.84 (7.9 - 0.46 \cdot 11.9) = 6.9 \text{ W/m}^2$$

$$CF_{\text{ip}} = \text{PXi} \cdot \text{SHGC} \cdot \text{IAC} \cdot \text{FF}_s = 557 \cdot 0.54 \cdot 1 \cdot 0.47 = 141.4 \text{ W/m}^2$$

$$CF(\text{total}) = 148.3 \text{ W/m}^2$$

$$\mathbf{Q(\text{cooling}) = CF(\text{total}) \cdot A = 148.3 \cdot 3.6 = 533.9 \text{ W}}$$

b) Heating

$$HF = U \cdot \Delta T_{\text{heating}} = 2.84 \cdot 24.8 = 70.4 \text{ W/m}^2$$

$$\mathbf{Q(\text{heating}) = HF \cdot A = 70.4 \cdot 3.6 = 253.4 \text{ W}}$$

Calculating load of **fixed Aluminum** window on the **SOUTH= 3.6 m2**:

a) Cooling

$$CF_{ht} = U (\Delta T_{cooling} - 0.46 \cdot DR) = 3.61 (7.9 - 0.46 \cdot 11.9) = 8.8 \text{ W/m}^2$$

$$CF_{ip} = PXI \cdot SHGC \cdot IAC \cdot FF_s = 557 \cdot 0.56 \cdot 1 \cdot 0.47 = 146.6 \text{ W/m}^2$$

$$CF \text{ (total)} = 155.4 \text{ W/m}^2$$

$$\mathbf{Q \text{ (cooling)} = CF \text{ (total)} \cdot A = 155.4 \cdot 3.6 = 559.4 \text{ W}}$$

b) Heating

$$HF = U \cdot \Delta T_{heating} = 3.61 \cdot 24.8 = 89.5 \text{ W/m}^2$$

$$\mathbf{Q \text{ (heating)} = HF \cdot A = 89.5 \cdot 3.6 = 322.2 \text{ W}}$$

3)

Calculating load of **operable Wooden** window on the **SOUTH= 3.6 m2**:

a) Cooling

$$CF_{ht} = U (\Delta T_{cooling} - 0.46 \cdot DR) = 2.87 (7.9 - 0.46 \cdot 11.9) = 6.96 \text{ W/m}^2$$

$$CF_{ip} = PXI \cdot SHGC \cdot IAC \cdot FF_s = 557 \cdot 0.46 \cdot 1 \cdot 0.47 = 120.4 \text{ W/m}^2$$

$$CF \text{ (total)} = 127.4 \text{ W/m}^2$$

$$\mathbf{Q \text{ (cooling)} = CF \text{ (total)} \cdot A = 127.4 \cdot 3.6 = 458.6 \text{ W}}$$

b) Heating

$$HF = U \cdot \Delta T_{heating} = 2.87 \cdot 24.8 = 71.2 \text{ W/m}^2$$

$$\mathbf{Q \text{ (heating)} = HF \cdot A = 71.2 \cdot 3.6 = 256.3 \text{ W}}$$

Calculating load of **operable Aluminum** window on the **SOUTH= 3.6 m2**:

a) Cooling

$$CF_{ht} = U (\Delta T_{cooling} - 0.46 \cdot DR) = 4.62 (7.9 - 0.46 \cdot 11.9) = 11.2 \text{ W/m}^2$$

$$CF_{ip} = PXI \cdot SHGC \cdot IAC \cdot FF_s = 557 \cdot 0.55 \cdot 1 \cdot 0.47 = 143.98 \text{ W/m}^2$$

$$CF \text{ (total)} = 155.2 \text{ W/m}^2$$

$$\mathbf{Q \text{ (cooling)} = CF \text{ (total)} \cdot A = 155.2 \cdot 3.6 = 558.7 \text{ W}}$$

b) Heating

$$HF = U \cdot \Delta T_{heating} = 4.62 \cdot 24.8 = 114.6 \text{ W/m}^2$$

$$\mathbf{Q \text{ (heating)} = HF \cdot A = 114.6 \cdot 3.6 = 412.6 \text{ W}}$$