WEEK 8

2019年11月27日 0:14

QUESTIONS

Task 1

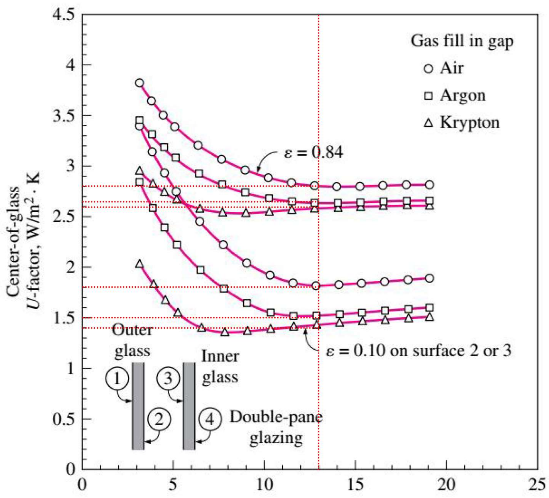
Using the diagrams given in the presentation calculate how much (%) is the effect of applying different modifications (changing the gas, adding an extra pane, using a low emissivity coating) on the U value with respect to a benchmark case of double layer with air and no coating ? (keep the gap thickenss to be 13 mm)

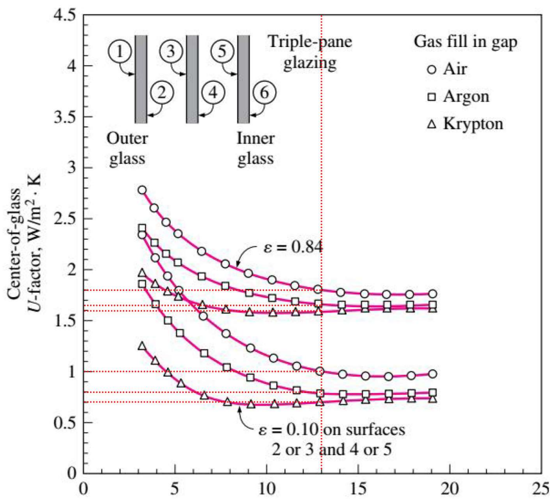
Task 2

Consider the house that we analyzed in the last two examples, calculate the heating and cooling load of the other windows which are fixed 14.4 m2 on the west, fixed 3.6 m2 on the south and an operable 3.6 m2 on the south (the same window and frame type). How much does the total value change if I change the frame of the window from wooden one to aluminum ?

ANSWERS

1. The benchmark is double-pane windows with 13mm air gap but no coating.





When $\epsilon = 0.84$ without coating, the U value are:

	Air	Argon	Krypton	Air	Argon	Krypton
Number of parallels	2	2	2	3	3	3
U-factor, (W/m^{2}K)	2.8	2.65	2.6	1.8	1.65	1.6
Changing percentage(%)	/	5.36	7.14	35.71	41.07	42.86

With coating ($\epsilon = 0.10$), the U value are:

	Air	Argon	Krypton	Air	Argon	Krypton
Number of parallels	2	2	2	3	3	3
U-factor, (W/m^{2}K)	1.8	1.5	1.4	1.0	0.8	0.7
Changing percentage(%)	35.71	46.43	50.00	64.29	71.43	39.29

2. Indoor Conditions.
   Based on ASHRAE Standard 55 typical practices are the following:
   ✓For cooling: 24°C db and a maximum of 50 to 65% rh.
   ✓For heating: 20°C db and 30% rh

PIACENZA, Italy WMO#: **160840**

Lat: **44.92N** Long: **9.73E** Elev: **138** StdP: **99.68** Time Zone: **1.00 (EUW)** Period: **89-10** WBAN: **99999**

Annual Heating and Humidification Design Conditions

Coldest Month	Heating DB		Humidification DP/MCDB and HR						Coldest month WS/MCDB				MCWS/PCWD to 99.6% DB		
			99.6%			99%			0.4%		1%				
	99.6%	99%	DP	HR	MCDB	DP	HR	MCDB	WS	MCDB	WS	MCDB	MCWS	PCWD	
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	
1	-6.2	-4.8	-11.6	1.4	3.1	-8.8	1.8	1.8	8.8	5.6	7.7	6.2	2.1	250	(1)

Annual Cooling, Dehumidification, and Enthalpy Design Conditions

Hottest Month	Hottest Month DB Range	Cooling DB/MCWB						Evaporation WB/MCDB						MCWS/PCWD to 0.4% DB		
		0.4%		1%		2%		0.4%		1%		2%				
		DB	MCWB	DB	MCWB	DB	MCWB	WB	MCDB	WB	MCDB	WB	MCDB	MCWS	PCWD	
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)	
8	11.9	33.1	22.7	31.9	22.4	30.3	21.8	24.6	30.2	23.7	29.2	22.9	28.3	2.4	90	(2)

					Frame									
					Operable					Fixed				
Glazing Type	Glazing Layers	ID[b]	Property[c,d]	Center of Glazing	Aluminum	Aluminum with Thermal Break	Reinforced Vinyl/Aluminum Clad Wood	Wood/Vinyl	Insulated Fiberglass/Vinyl	Aluminum	Aluminum with Thermal Break	Reinforced Vinyl/Aluminum Clad Wood	Wood/Vinyl	Insulated Fiberglass/Vinyl
Clear	1	1a	U	5.91	7.24	6.12	5.14	5.05	4.61	6.42	6.07	5.55	5.55	5.35
			SHGC	0.86	0.75	0.75	0.64	0.64	0.64	0.78	0.78	0.75	0.75	0.75
	2	5a	U	2.73	4.62	3.42	3.00	2.87	5.83	3.61	3.22	2.86	2.84	2.72
			SHGC	0.76	0.67	0.67	0.57	0.57	0.57	0.69	0.69	0.67	0.67	0.67
	3	29a	U	1.76	3.80	2.60	2.25	2.19	1.91	2.76	2.39	2.05	2.01	1.93
			SHGC	0.68	0.60	0.60	0.51	0.51	0.51	0.62	0.62	0.60	0.60	0.60
Low-e, low-solar	2	25a	U	1.70	3.83	2.68	2.33	2.21	1.89	2.75	2.36	2.03	2.01	1.90
			SHGC	0.41	0.37	0.37	0.31	0.31	0.31	0.38	0.38	0.36	0.36	0.36
	3	40c	U	1.02	3.22	2.07	1.76	1.71	1.45	2.13	1.76	1.44	1.40	1.33
			SHGC	0.27	0.25	0.25	0.21	0.21	0.21	0.25	0.25	0.24	0.24	0.24
Low-e, high-solar	2	17c	U	1.99	4.05	2.89	2.52	2.39	2.07	2.99	2.60	2.26	2.24	2.13
			SHGC	0.70	0.62	0.62	0.52	0.52	0.52	0.64	0.64	0.61	0.61	0.61
	3	32c	U	1.42	3.54	2.36	2.02	1.97	1.70	2.47	2.10	1.77	1.73	1.66
			SHGC	0.62	0.55	0.55	0.46	0.46	0.46	0.56	0.56	0.54	0.54	0.54
Heat-absorbing	1	1c	U	5.91	7.24	6.12	5.14	5.05	4.61	6.42	6.07	5.55	5.55	5.35
			SHGC	0.73	0.64	0.64	0.54	0.54	0.54	0.66	0.66	0.64	0.64	0.64
	2	5c	U	2.73	4.62	3.42	3.00	2.87	2.53	3.61	3.22	2.86	2.84	2.72
			SHGC	0.62	0.55	0.55	0.46	0.46	0.46	0.56	0.56	0.54	0.54	0.54
	3	29c	U	1.76	3.80	2.60	2.25	2.19	1.91	2.76	2.39	2.05	2.01	1.93
			SHGC	0.34	0.31	0.31	0.26	0.26	0.26	0.31	0.31	0.30	0.30	0.30
Reflective	1	1l	U	5.91	7.24	6.12	5.14	5.05	4.61	6.42	6.07	5.55	5.55	5.35
			SHGC	0.31	0.28	0.28	0.24	0.24	0.24	0.29	0.29	0.27	0.27	0.27
	2	5p	U	2.73	4.62	3.42	3.00	2.87	2.53	3.61	3.22	2.86	2.84	2.72
			SHGC	0.29	0.27	0.27	0.22	0.22	0.22	0.27	0.27	0.26	0.26	0.26
	3	29c	U	1.76	3.80	2.60	2.25	2.19	1.91	2.76	2.39	2.05	2.01	1.93
			SHGC	0.34	0.31	0.31	0.26	0.26	0.26	0.31	0.31	0.30	0.30	0.30

Table 11 Exterior Attachment Transmission

Attachment	T_x
None	1.0
Exterior insect screen	0.64 (see Chapter 15, Table 13G)
Shade screen	Manufacturer shading coefficient (SC) value, typically 0.4 to 0.6

Table 13 Fenestration Solar Load Factors FF_s

Exposure	Single Family Detached	Multifamily
North	0.44	0.27
Northeast	0.21	0.43
East	0.31	0.56
Southeast	0.37	0.54
South	0.47	0.53
Southwest	0.58	0.61
West	0.56	0.65
Northwest	0.46	0.57
Horizontal	0.58	0.73

Table 10 Peak Irradiance, W/m²

Exposure		Latitude 20°	25°	30°	35°	40°	45°	50°	55°	60°
North	E_D	125	106	92	84	81	85	96	112	136
	E_d	128	115	103	93	84	76	69	62	55
	E_t	253	221	195	177	166	162	164	174	191
Northeast/Northwest	E_D	460	449	437	425	412	399	386	374	361
	E_d	177	169	162	156	151	147	143	140	137
	E_t	637	618	599	581	563	546	529	513	498
East/West	E_D	530	543	552	558	560	559	555	547	537
	E_d	200	196	193	190	189	188	187	187	187
	E_t	730	739	745	748	749	747	742	734	724
Southeast/Southwest	E_D	282	328	369	405	436	463	485	503	517
	E_d	204	203	203	204	205	207	210	212	215
	E_t	485	531	572	609	641	670	695	715	732
South	E_D	0	60	139	214	283	348	408	464	515
	E_d	166	193	196	200	204	209	214	219	225
	E_t	166	253	335	414	487	557	622	683	740
Horizontal	E_D	845	840	827	806	776	738	691	637	574
	E_d	170	170	170	170	170	170	170	170	170
	E_t	1015	1010	997	976	946	908	861	807	744

$\therefore\ \Delta T_{heating} = 20 - (-4.8) = 24.8°C$

$\Delta T_{cooling} = 31.9 - 24 = 7.9°C$

$DR = 11.9°C$

1) 14.4m^2 fixed window on the west:

HEATING LOAD:

From the table of U and SHGC, we can see $U_{west\ fixed} = 2.84\ W/m^2K$,
$\therefore HF_{west\ fixed} = U_{west\ fixed} * \Delta T_{heating} = 2.84 * 24.8 = 70.44\ W/m^2$
$\dot{Q}_{west\ fixed} = HF_{west\ fixed} * A_{west\ fixed} = 70.44 * 14.4 \cong 1014.34\ W$

COOLING LOAD:

$CF_{west\ fixed} = U_{west\ fixed} * (\Delta T_{cooling} - 0.46 * DR) + PXI * SHGC * IAC * FF_s$
$\therefore CF_{west\ fixed,heat\ transfer} = U_{west\ fixed} * (\Delta T_{cooling} - 0.46 * DR)$
$= 2.84 * (7.9 - 0.46 * 11.9) = 6.9\ W/m^2$

If we assuming that there is no internal or external shading,
so IAC=1,

From the table of U and SHGC, we can see $SHGC_{west\ fixed} = 0.54$,

From the table 13, we can see $FF_s = 0.56$,

From the table 10, we can see $E_{D,west\ fixed} = 559, E_{d,west\ fixed} = 188$,
$PXI_{west\ fixed} = E_{D,west\ fixed} + E_{d,west\ fixed} = 559 + 188 = 747$

$\therefore CF_{west\ fixed,irradiation} = PXI * SHGC * IAC * FF_s$
$= 747 * 0.54 * 1 * 0.56 \cong 225.89\ W/m^2$
$\therefore CF_{west\ fixed} = 6.9 + 225.89 \cong 232.79\ W/m^2$
$\dot{Q}_{west\ fixed} = CF_{west\ fixed} * A_{west\ fixed} = 232.79 * 14.4 \cong 3352.18\ W$

If we change the frame into Aluminum

HEATING LOAD:

From the table of U and SHGC, we can see $U'_{west\ fixed} = 3.61\ W/m^2K$,
$\therefore HF'_{west\ fixed} = U'_{west\ fixed} * \Delta T_{heating} = 3.61 * 24.8 = 89.53\ W/m^2$
$\dot{Q}'_{west\ fixed} = HF'_{west\ fixed} * A_{west\ fixed} = 89.53 * 14.4 \cong 1289.23\ W$

COOLING LOAD:

$CF'_{west\ fixed} = U'_{west\ fixed} * (\Delta T_{cooling} - 0.46 * DR) + PXI * SHGC' * IAC * FF_s$
$\therefore CF'_{west\ fixed,heat\ transfer} = U'_{west\ fixed} * (\Delta T_{cooling} - 0.46 * DR)$
$= 3.61 * (7.9 - 0.46 * 11.9) = 8.76\ W/m^2$

If we assuming that there is no internal or external shading,
so IAC=1,

From the table of U and SHGC, we can see $SHGC'_{west\ fixed} = 0.56$,

From the table 13, we can see $FF_s = 0.56$,

From the table 10, we can see $E_{D,west\ fixed} = 559, E_{d,west\ fixed} = 188$,
$PXI_{west\ fixed} = E_{D,west\ fixed} + E_{d,west\ fixed} = 559 + 188 = 747$

$\therefore CF'_{west\ fixed,irradiation} = PXI * SHGC * IAC * FF_s$
$= 747 * 0.56 * 1 * 0.56 \cong 234.26\ W/m^2$
$\therefore CF'_{west\ fixed} = 8.76 + 234.26 \cong 243.02\ W/m^2$
$\dot{Q}'_{west\ fixed} = CF'_{west\ fixed} * A_{west\ fixed} = 243.02 * 14.4 \cong 3499.49\ W$

2) $3.6m^2$ fixed window on the south:

HEATING LOAD:

From the table of U and SHGC, we can see $U_{south\ fixed} = 2.84\ W/m^2K$,
$\therefore HF_{south\ fixed} = U_{south\ fixed} * \Delta T_{heating} = 2.84 * 24.8 = 70.44\ W/m^2$
$\dot{Q}_{south\ fixed} = HF_{south\ fixed} * A_{south\ fixed} = 70.44 * 3.6 = 253.58\ W$

COOLING LOAD:

$CF_{south\ fixed} = U_{south\ fixed} * (\Delta T_{cooling} - 0.46 * DR) + PXI * SHGC * IAC * FF_s$
$\therefore CF_{south\ fixed,heat\ transfer} = U_{south\ fixed} * (\Delta T_{cooling} - 0.46 * DR)$
$= 2.84 * (7.9 - 0.46 * 11.9) = 6.9\ W/m^2$

If we assuming that there is no internal or external shading,
so IAC=1,

From the table of U and SHGC, we can see $SHGC_{south\ fixed} = 0.54$,

From the table 13, we can see $FF_s = 0.47$,

From the table 10, we can see $E_{D,south\ fixed} = 348, E_{d,south\ fixed} = 209$,
$PXI_{south\ fixed} = E_{D,south\ fixed} + E_{d,south\ fixed} = 348 + 209 = 557$

$\therefore CF_{south\ fixed,irradiation} = PXI * SHGC * IAC * FF_s$
$= 557 * 0.54 * 1 * 0.47 \cong 141.37\ W/m^2$
$\therefore CF_{south\ fixed} = 6.9 + 141.37 \cong 148.27\ W/m^2$
$\dot{Q}_{south\ fixed} = CF_{south\ fixed} * A_{south\ fixed} = 148.27 * 3.6 \cong 533.77\ W$

If we change the frame into Aluminum

HEATING LOAD:

From the table of U and SHGC, we can see $U'_{south\ fixed} = 3.61\ W/m^2K$,
$\therefore HF'_{south\ fixed} = U'_{south\ fixed} * \Delta T_{heating} = 3.61 * 24.8 = 89.53\ W/m^2$
$\dot{Q}'_{south\ fixed} = HF'_{south\ fixed} * A_{south\ fixed} = 89.53 * 3.6 = 322.31\ W$

COOLING LOAD:

$CF'_{south\ fixed} = U'_{south\ fixed} * (\Delta T_{cooling} - 0.46 * DR) + PXI * SHGC' * IAC * FF_s$
$\therefore CF'_{south\ fixed,heat\ transfer} = U'_{south\ fixed} * (\Delta T_{cooling} - 0.46 * DR)$
$= 3.61 * (7.9 - 0.46 * 11.9) = 8.76\ W/m^2$

If we assuming that there is no internal or external shading,
so IAC=1,

From the table of U and SHGC, we can see $SHGC'_{south\ fixed} = 0.56$, From the table 13, we can see $FF_s = 0.47$,

From the table 10, we can see $E_{D,south\ fixed} = 348, E_{d,south\ fixed} = 209$,
$PXI_{south\ fixed} = E_{D,south\ fixed} + E_{d,south\ fixed} = 348 + 209 = 557$

$$\therefore CF'_{south\ fixed,irradiation} = PXI * SHGC' * IAC * FF_s$$
$$= 557 * 0.56 * 1 * 0.47 \cong 146.60\ W/m^2$$
$$\therefore CF'_{south\ fixed} = 8.76 + 146.60 = 155.36\ W/m^2$$
$$\dot{Q}'_{south\ fixed} = CF'_{south\ fixed} * A_{south\ fixed} = 155.36 * 3.6 \cong 559.30\ W$$

3) $3.6m^2$ operable window on the south:

HEATING LOAD:

From the table of U and SHGC, we can see $U_{south,operable} = 2.87\ W/m^2K$,
$$\therefore HF_{south,operable} = U_{south,operable} * \Delta T_{heating} = 2.87 * 24.8 \cong 71.18\ W/m^2$$
$$\dot{Q}_{south,operable} = HF_{south,operable} * A_{south,operable} = 71.18 * 3.6 \cong 256.25\ W$$

COOLING LOAD:

$$CF_{south,operable} = U_{south,operable} * (\Delta T_{cooling} - 0.46 * DR) + PXI * SHGC * IAC * FF_s$$
$$\therefore CF_{south,operable,heat\ transfer} = U_{south,operable} * (\Delta T_{cooling} - 0.46 * DR)$$
$$= 2.87 * (7.9 - 0.46 * 11.9) = 7.0\ W/m^2$$

If we assuming that there is no internal or external shading,
so IAC=1,

From the table of U and SHGC, we can see $SHGC_{south,operable} = 0.46$,

From the table 13, we can see $FF_s = 0.47$,

From the table 10, we can see $E_{D,south,operable} = 348, E_{d,south,operable} = 209$,
$PXI_{south,operable} = E_{D,south,operable} + E_{d,south,operable} = 348 + 209 = 557$

$$\therefore CF_{south,operable,irradiation} = PXI * SHGC * IAC * FF_s$$
$$= 557 * 0.46 * 1 * 0.47 \cong 120.42\ W/m^2$$
$$\therefore CF_{south,operable} = 7.0 + 120.42 = 127.42\ W/m^2$$
$$\dot{Q}_{south,operable} = CF_{south,operable} * A_{south,operable} = 127.42 * 3.6 \cong 458.71\ W$$

If we change the frame into Aluminum

HEATING LOAD:

From the table of U and SHGC, we can see $U'_{south,operable} = 4.62\ W/m^2K$,
$$\therefore HF'_{south,operable} = U'_{south,operable} * \Delta T_{heating} = 4.62 * 24.8 \cong 114.58\ W/m^2$$
$$\dot{Q}'_{south,operable} = HF'_{south,operable} * A_{south,operable} = 114.58 * 3.6 \cong 412.49\ W$$

COOLING LOAD:

$$CF'_{south,operable} = U'_{south,operable} * (\Delta T_{cooling} - 0.46 * DR) + PXI * SHGC' * IAC * FF_s$$
$$\therefore CF'_{south,operable,heat\ transfer} = U'_{south,operable} * (\Delta T_{cooling} - 0.46 * DR)$$
$$= 4.62 * (7.9 - 0.46 * 11.9) = 11.21\ W/m^2$$

If we assuming that there is no internal or external shading,
so IAC=1,

From the table of U and SHGC, we can see $SHGC'_{south,operable} = 0.55$,

From the table 13, we can see $FF_s = 0.47$,

From the table 10, we can see $E_{D,south,operable} = 348, E_{d,south,operable} = 209$,
$PXI_{south,operable} = E_{D,south,operable} + E_{d,south,operable} = 348 + 209 = 557$

$$\therefore CF'_{south,operable,irradiation} = PXI * SHGC' * IAC * FF_s$$
$$= 557 * 0.55 * 1 * 0.47 \cong 143.98\ W/m^2$$
$$\therefore CF'_{south,operable} = 11.21 + 143.98 = 155.19\ W/m^2$$
$$\dot{Q}'_{south,operable} = CF'_{south,operable} * A_{south,operable} = 155.19 * 3.6 \cong 558.68\ W$$