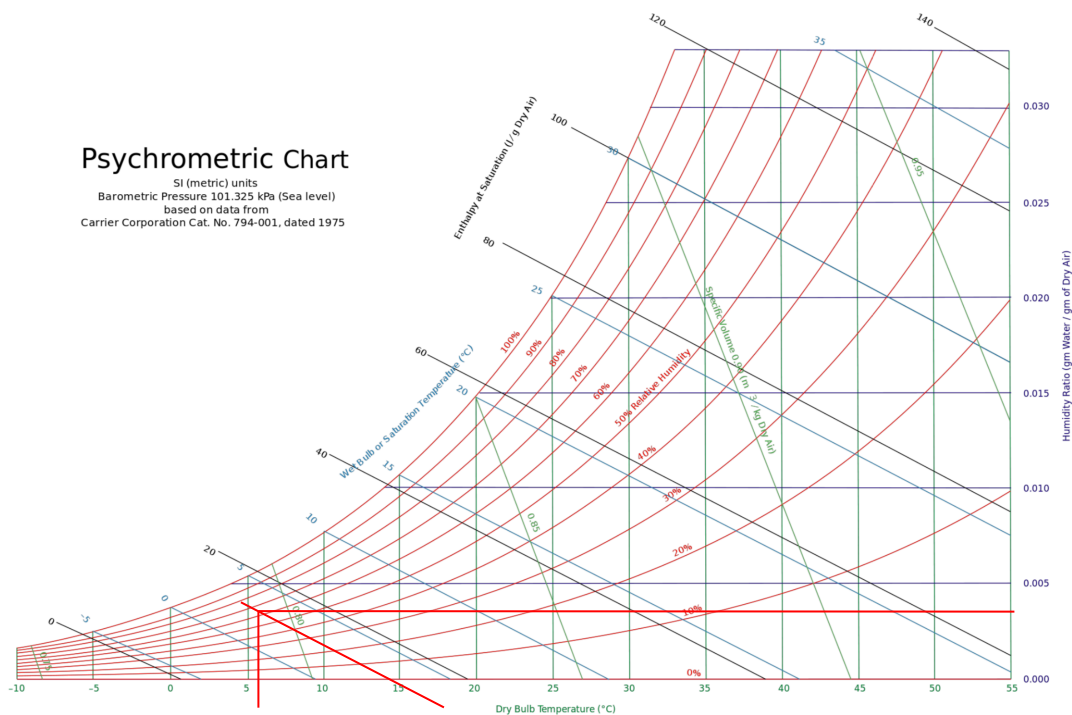


1. Use a weather forecast website, and utilize the psychrometric chart and the formula we went through in the class to determine the absolute humidity, the wet-bulb temperature and the mass of water vapour in the air in Classroom A (Aula A) of Piacenza campus in the moment that you are solving this exercise (provide the inputs that you utilized)

$$P = 1017 \text{ hPa} \rightarrow 101,7 \text{ KPa}$$

$$T = 6^\circ$$

$$\phi = 90\%$$



ABSOLUTE HUMIDITY

$$\omega = 0,0052 \frac{Kg_{water}}{Kg_{dry\ air}}$$

WET-BULB TEMPERATURE

$$T_{wb} = 5,2^\circ \text{C}$$

MASS OF WATER VAPOR

$$V_{room A} = 20 \cdot 20 \cdot 6 = 720 \text{ m}^3$$

$$P_v = \frac{P \cdot \omega}{0,622 + \omega} = \frac{101,7 \cdot 0,0052}{0,622 + 0,0052} = 0,84 \text{ Kg}$$

$$m_v = \frac{P_v \cdot V}{R_v \cdot T} = \frac{0,84 \cdot 720}{0,4615 \cdot (273 + 6)} = 4,7 \text{ Kg}$$

If I consider that when I am doing the exercise (Sunday), the Politecnico di Milano is closed, I assume as external temperature and humidity values for the calculation of the mass of vapor.

- Utilize the same methodology we went through in the class and determine the sensible and latent load corresponding to internal gains, the ventilation, and the infiltration in a house with a good construction quality and with the same geometry as that of the example which is located in Brindisi, Italy

BRINDISI, Italy														WMO#: 163200		
Lat: 40.65N		Long: 17.95E		Elev: 10		StdP: 101.2		Time Zone: 1.00 (EUW)		Period: 86-10		WBAN: 99999				
Annual Heating and Humidification Design Conditions																
Coldest Month	Heating DB		Humidification DP/MCDB and HR						Coldest month WS/MCDB				MCWS/PCWD to 99.6% DB			
	99.6%	99%	DP	HR	MCDB	DP	HR	MCDB	WS	MCDB	WS	MCDB	MCWS	PCWD		
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)		
2	2.9	4.1	-5.1	2.5	7.2	-3.0	3.0	7.4	13.4	10.2	12.4	10.6	3.4	250		
Annual Cooling, Dehumidification, and Enthalpy Design Conditions																
Hottest Month	Hottest Month DB Range	Cooling DB/MCWB						Evaporation WB/MCDB						MCWS/PCWD to 0.4% DB		
		0.4%		1%		2%		0.4%		1%		2%		MCWS	PCWD	
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)	
8	7.1	32.8	23.6	31.1	24.3	29.9	24.3	27.2	29.7	26.3	29.0	25.6	28.3	4.2	180	
Dehumidification DP/MCDB and HR												Enthalpy/MCDB			Hours 8 to 4 & 12.8/20.6	
0.4%		1%		2%		0.4%		1%		2%						
DP	HR	MCDB	DP	HR	MCDB	DP	HR	MCDB	Enth	MCDB	Enth	MCDB	Enth	MCDB	Enth	
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)	
26.3	21.8	29.2	25.4	20.7	28.5	24.7	19.7	27.9	86.0	30.1	82.2	29.1	78.5	28.3	1236	
Extreme Annual Design Conditions																
Extreme Annual WS			Extreme Max WB	Extreme Annual DB			n-Year Return Period Values of Extreme DB									
1%	2.5%	5%		Mean	Standard deviation		n=5 years		n=10 years		n=20 years		n=50 years			
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)	
11.3	9.9	8.7	31.4	0.4	37.3	1.4	3.0	-0.6	39.4	-1.4	41.1	-2.2	42.8	-3.2	44.9	

$$h_{\text{building}} = 2,5 \text{ m}$$

$$A_{\text{floor}} = 200 \text{ m}^2$$

$$A_{\text{wall}} = 144 \text{ m}^2$$

$$N^{\circ} \text{ occupants} = 2$$

$$N^{\circ} \text{ bedroom} = 1$$

INTERNAL GAINS

$$\dot{Q}_{ig_{sensible}} = 136 + 2.2 \cdot A_{cf} + 22 N_{oc} = 136 + 2.2 \cdot 200 + 22 \cdot 2 = 620 \text{ W}$$

$$\dot{Q}_{ig_{latent}} = 20 + 0.22 \cdot A_{cf} + 12 N_{oc} = 20 + 0.22 \cdot 200 + 12 \cdot 2 = 88 \text{ W}$$

INFILTRATION

$$A_{ul} = 1.4 \frac{\text{cm}^2}{\text{m}^2} \quad (\text{good quality})$$

$$A_{es} = A_{wall} + A_{roof}$$

$$A_{es} = 200 + 144 = 344 \text{ m}^2$$

$$A_L = A_{es} \times A_{ul} = 344 \times 1.4 = 481.6 \text{ cm}^2$$

$$IDF_{heating} = 0.065 \frac{L}{s \cdot \text{cm}^2}$$

$$IDF_{cooling} = 0.032 \frac{L}{s \cdot \text{cm}^2}$$

$$\dot{V}_{infiltration_{heating}} = A_L \times IDF_{heating} = 481.6 \cdot 0.065 = 31.30 \frac{L}{s}$$

$$\dot{V}_{infiltration_{cooling}} = A_L \times IDF_{cooling} = 481.6 \cdot 0.032 = 15.41 \frac{L}{s}$$

VENTILATION

$$\dot{V}_{ventilation} = 0.05 A_{cf} + 3.5 (N_{br} + 1) = 0.05 \cdot 200 + 3.5 \cdot 2 = 17 \frac{L}{s}$$

$$\begin{aligned} \dot{V}_{infiltration-ventilation_{heating}} &= \dot{V}_{infiltration_{heating}} + \dot{V}_{ventilation} = 31.30 + 17 \\ &= 48.30 \frac{L}{s} \end{aligned}$$

$$\begin{aligned} \dot{V}_{infiltration-ventilation_{cooling}} &= \dot{V}_{infiltration_{cooling}} + \dot{V}_{ventilation} = 15.41 + 17 \\ &= 32.41 \frac{L}{s} \end{aligned}$$

$$C_{sensible} = 1.23$$

$$C_{latent} = 3010$$

$$\Delta T_{cooling} = 31.1 - 24 = 7.1 \text{ }^{\circ}C$$

$$\Delta T_{heating} = 20 - (4.1) = 15.9 \text{ }^{\circ}C$$

$$\begin{aligned}\dot{Q}_{inf-vent_{cooling_{sensible}}} &= C_{sensible} \times \dot{V}_{inf-vent_{cooling}} \times \Delta T_{cooling} \\ &= 1.23 \cdot 32.41 \cdot 7.1 = 283.04 \text{ } W\end{aligned}$$

$$\begin{aligned}\dot{Q}_{inf-vent_{heating_{sensible}}} &= C_{sensible} \times \dot{V}_{inf-vent_{heating}} \times \Delta T_{heating} \\ &= 1.23 \cdot 48.30 \cdot 15.9 = 944.6 \text{ } W\end{aligned}$$

$$\omega_{out} = 0.0143 \frac{kg_{water}}{kg_{dryAir}}$$

$$\omega_{in} = 0.0093 \frac{kg_{water}}{kg_{dryAir}}$$

$$\Delta \omega_{cooling} = \omega_{out} - \omega_{in} = 0.0143 - 0.0093 = 0.005 \frac{kg_{water}}{kg_{DryAir}}$$

$$\begin{aligned}\dot{Q}_{inf-vent_{cooling_{latent}}} &= C_{latent} \times \dot{V}_{inf-vent_{cooling}} \times \Delta \omega_{cooling} \\ &= 3010 \cdot 32.41 \cdot 0.005 = 487.77 \text{ } W\end{aligned}$$