WEEK 8:

Michibane

TASK 1:

Using the diagrams given in the presentation calculate how much (%) is the effect of applying different modifications (changing the gas, adding an extra pane, using a low emissivity coating) on the U value with respect to a benchmark case of double layer with air and no coating? (keep the gap thickenss to be 13 mm)

The U value of a window:

Uwindow = (Ucenter*Acenter + Uedge*Aedge + Uframe*Aframe)/Awindow

1/Udoublepanecenter = 1/hi + 1/hspace + 1/ho; hspace = hradiationspace +hconvectionspace

=>U and h change according to the type of gas

According to the diagrams given in the presentation:

- Gap thickness is 13 mm
- Type of gas:ARGON
- In this case, the U value of the center of the glass decreases from 2,8 w/m²k to 2,65 w/m²k
- percentage: 5,3 %
- Gap thickness is 13 mm
- Type of gas:KRYPTON
- In this case, the U value of the center of the glass decreases from 2,8 w/m²k to 2,6 w/m²k
- percentage : 7,1 %

=>U and h change when we add an extra pane

- In case of 13mm of tickness, gas: air, an extra pane:
- the U value decreases from 2,8 to 1,8
- percentage : 35,7 %
- In case of 13mm of tickness, gas: air, an extra pane + a coating film that has an emmisivity of 0,1:
- the U value decreases from 2,8 to 1,8
- percentage: 35,7 %

TASK 2:

Consider the house that we analysed in the alst two examples, calculate the heating and cooling load of the other windows which are fixed 14.4 m2 on the west, fixed 3.6 m2 on the south and an operable 3.6 m2 on the south (the same window and frame type). How much does the total value change if I change the frame of the window from wooden one to aluminium?

CASE 1: FIXED WINDOW ON WEST:

1.1 Cooling load:

```
Frame: wood  \label{eq:qwindowW} Frame: wood \\ qwindowW = A*CFwindowW \; ; A=14,4 \; m^2 \\ CfwindowWheattransfer = UwindowW \; ($\Delta$Tcooling-0,46 DR ) = 2,84*(7,9-0,46*11,9 ) \\ CfwindowWheattransfer = 6,89 \; w/m^2 \\ PXIwindowW = ED+Ed=559+188=747 \; ; SHGC=0,54 \qquad ; \quad IAC=1 \quad ; \quad Ffs=0,56 \\ CfwindowWirradiation = PXI*SHGC*IAC*FFs=747*0,54*1*0,56 \\ CfwindowWirradiation = 225,9 \\ qwindowW = A*CFwindowW = A*(CFwindowWheattransfer + CFwindowWirradiation )= 14,4*(6,89+225,9) \\ qwindowW = 3352,17 \; W
```

1.2 Heating load:

```
Frame: aluminium qwindowW = A*HFwindowW = A*UwindowW \Delta Theating = 14,4*2,84*24,8 \\ \textbf{qwindowW} = \textbf{1014,22} \ W UwindowW = 3,61 \ ; \ HSGC=0,56 CF'windowWheattransfer = \ U'windowW *(( \Delta Tcooling-0,46 \ DR ) = 3,61*(7,9-0,46*11,9) \\ \textbf{CF'windowWheattransfer} = \textbf{8,76} \textbf{Cooling load:}
```

```
 \label{eq:continuous} $q'$window$W = A*CF'$window$W = A*(CF'$window$W$heattransfer + CF'$window$W$irradiation ) $=14,4* ( 8,76+234,26) $ $q'$window$W = 3499,49 $ $W$ $
```

Heating load:

```
\label{eq:window} \begin{aligned} & \textbf{q'windowW} = A*HF'windowW &= A*U'windowW* \ \Delta Theating = 14,4*3,61*24,8 \\ & \textbf{q'windowW} = \textbf{1289,2} \ \textbf{W} \end{aligned}
```

CASE 2: FIXED WINDOW ON SOUTH:

1.1 Cooling load:

Frame: wood

CfwindowSheattransfer = 6,89 w/m²

PXIwindowS = ED+Ed = 348+209=557; SHGC = 0.56; IAC = 1; Ffs = 0.47

CfwindowSirradiation = PXI*SHGC*IAC*FFs = 557*0,56*1*0,47 CfwindowSirradiation = 146,60

qwindowS = A*CF windowS = A*(CF windowSheattransfer + CF windowSirradiation)= 3,6 * (6,89+146,60) **qwindowW** = **552,56 W**

1.2 Heating load:

Frame: aluminium

qwindowS = A*HFwindowS= A*UwindowS \triangle Theating = 3,6*2,84*24,8 **qwindowW** = 253,56 **W**

UwindowS = 3.61; HSGC=0.56

CF'windowSheattransfer = U'windowS *((Δ Tcooling-0,46 DR) =3,61*(7,9-0,46*11,9) CF'windowWheattransfer = 8,76 W/m²

Cooling load:

 $\label{eq:qwindows} \begin{subarray}{l} q' windowS = A^*CF' windowS = $A^*(CF'$ windowS heattransfer + CF' windowS irradiation) = 3,6* (8,76+146,60) \\ \begin{subarray}{l} q' windowS = $559,3$ W \\ \end{subarray}$

Heating load:

```
\mathbf{q'}windowS = A*HF'windowS = A*U'windowS* \DeltaTheating = 3,6*3,61*24,8 \mathbf{q'}windowW = 322,3 W
```

CASE 3: OPERABLE WINDOW ON SOUTH:

COOLING LOAD FOR THE OPERABLE:

qwindowS = A*CFwindowS; $A=3.6 \text{ m}^2$

```
CfwindowSheattransfer = UwindowS ( \DeltaTcooling-0,46 DR ) = 2,87*(7,9-0,46*11,9) CfwindowSheattransfer =6,96 w/m<sup>2</sup>
```

PXIwindowS = ED+Ed =
$$348+209=557$$
; SHGC = $0,46$; IAC = 1 ; Ffs = $0,47$

CfwindowSirradiation = PXI*SHGC*IAC*FFs = 557*0,46*1*0,47

CfwindowSirradiation = 120,42

qwindowS = A*CFwindowS = A*(CFwindowSheattransfer + CFwindowSirradiation)= 3,6 * (6,96+141,36) **qwindowS** = **533,97** W

HEATING LOAD (fixed window):

qwindowS =
$$A*HFwindowS=A*UwindowS$$
 $\triangle Theating = 3,6*2,87*24,8$ **qwindowW = 256,23 W**

with aluminium frame:

UwindowS = 3,61; HSGC=0,56

CF'windowSheattransfer = U'windowS *((Δ Tcooling-0,46 DR) =4,62*(7,9-0,46*11,9) CF'windowWheattransfer = 11,21 W/m²

Cooling load:

$$\label{eq:qwindows} \begin{aligned} &q'windowS = A*CF'windowS = A*(CF'windowSheattransfer + CF'windowSirradiation~) = 3,6* (~11,21+143,98) \\ &\textbf{q'windowS=558,7} \text{ W} \end{aligned}$$

Heating load:

```
q'windowS = A*HF'windowS = A*U'windowS* \Delta Theating = 3,6*4,62*24,8

q'windowS=412,47 W
```