






### Task1:

Use a weather forecast website, and utilize the psychrometric chart and the formula we went through in the class to determine the absolute humidity, the wet-bulb temperature and the mass of water vapour in the air in Classroom A (Aula A) of Piacenza campus in the moment that you are solving this exercise (provide the inputs that you utilized)

Umidità: Relative humidity, Pressione atmosferica: Air total pressure (1 hPa: 0.1 kPa), Temperatura effettiva: temperature to be utilized.

### ANSWER:

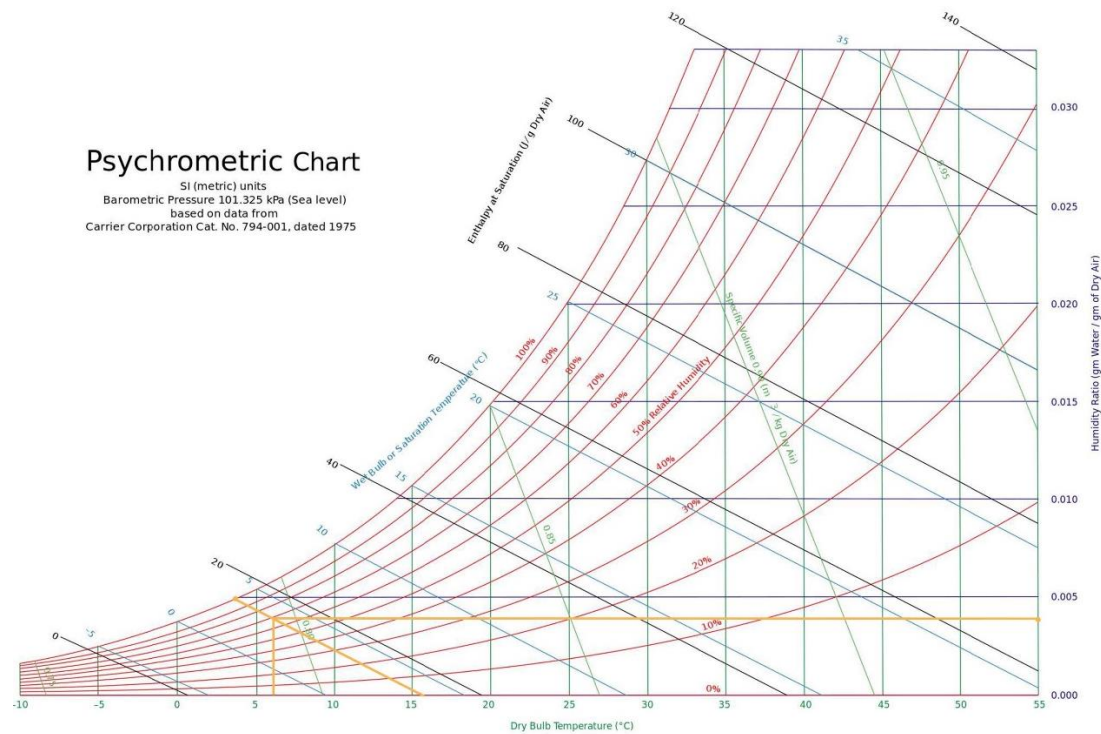
Il tempo oggi in Piacenza Martedì, 03 Dicembre 2019							
	13:00	14:00	16:00	18:00	20:00	21:00	22:00
	 LightCloud	 LightCloud	 PartlyCloud	 LightCloud	 Sun	 Sun	 Sun
Temperatura effettiva	9°C	10°C	8°C	6°C	4°C	2°C	2°C
Temperatura percepita	7°C	10°C	6°C	4°C	2°C	0°C	0°C
Precipitazioni	0 mm	0 mm	0 mm	0 mm	0 mm	0 mm	0 mm
Umidità	67 %	65 %	69 %	70 %	75 %	83 %	87 %
Pressione atmosferica	1025 hPa	1025 hPa	1025 hPa	1026 hPa	1027 hPa	1027 hPa	1028 hPa

*The time is 18:23 now, we can see from the chart that:*

*Relative humidity:  $\phi = 70\%$*

*Air total pressure:  $P = 1026\text{hPa} = 102.6\text{kPa}$*

*Temperature:  $T = 6^\circ\text{C}$*



We can see from above chart that:

(1) The absolute humidity  $\omega = 0.004 \frac{Kg_{vapour}}{kg_{dryAir}}$

(2) The wet-bulb temperature  $T_{wb} = 4^\circ C$

(3)  $\omega = 0.622 \frac{P_v}{P_a} = 0.622 \frac{P_v}{P - P_v} = 0.004 \frac{Kg_{vapour}}{kg_{dryAir}} ; P = 102.6 kPa$

So,  $P_v = 0.66 kPa$

$m = \frac{PV}{R_{sp}T} ; R_{sp} = \frac{R_{global}}{M_{gas}} \rightarrow$  We can find it in Tables  $R_v = 0.4615$

$m_v = \frac{0.66 \times V_{Aula A}}{0.4615 \times (273 + 6)} = 0.005 V_{Aula A} = 0.005 \times (15 \times 6 \times 6) = 2.7 kg$

## Task 2:

Utilize the same methodology we went through in the class and determine the sensible and latent load corresponding to internal gains, the ventilation, and the infiltration in a house with a *good* construction quality and with the same geometry as that of the example which is located in Brindisi, Italy.

**ANSWER:**

# BRINDISI, Italy

WMO#: 163200

Lat: 40.65N Long: 17.95E Elev: 10 StdP: 101.2 Time Zone: 1.00 (EUW) Period: 86-10 WBAN: 99999

## Annual Heating and Humidification Design Conditions

Coldest Month	Heating DB		Humidification DP/MCDB and HR						Coldest month WS/MCDB				MCWS/PCWD to 99.6% DB		
			99.6%			99%			0.4%		1%				
	DP	HR	MCDB	DP	HR	MCDB	WS	MCDB	WS	MCDB					
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	
(1)	2	2.9	4.1	-5.1	2.5	7.2	-3.0	3.0	7.4	13.4	10.2	12.4	10.6	3.4	250

## Annual Cooling, Dehumidification, and Enthalpy Design Conditions

(2)	Hottest Month	Hottest Month DB Range	Cooling DB/MCWB						Evaporation WB/MCDB						MCWS/PCWD to 0.4% DB		(2)
			0.4%		1%		2%		0.4%		1%		2%		MCWS	PCWD	
			DB	MCWB	DB	MCWB	DB	MCWB	WB	MCDB	WB	MCDB	WB	MCDB			
	(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)	
	8	7.1	32.8	23.6	31.1	24.3	29.9	24.3	27.2	29.7	26.3	29.0	25.6	28.3	4.2	180	

(3)	Dehumidification DP/MCDB and HR									Enthalpy/MCDB						Hours 8 to 4 & 12.8/20.6	(3)
	0.4%			1%			2%			0.4%		1%		2%			
	DP	HR	MCDB	DP	HR	MCDB	DP	HR	MCDB	Enth	MCDB	Enth	MCDB	Enth	MCDB		
	(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)	
	26.3	21.8	29.2	25.4	20.7	28.5	24.7	19.7	27.9	86.0	30.1	82.2	29.1	78.5	28.3	1236	

## Extreme Annual Design Conditions

Extreme Annual WS			Extreme Max WB	Extreme Annual DB				n-Year Return Period Values of Extreme DB								
1%	2.5%	5%		Mean		Standard deviation		n=5 years		n=10 years		n=20 years		n=50 years		
				Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	
(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)	
(4)	11.3	9.9	8.7	31.4	0.4	37.3	1.4	3.0	-0.6	39.4	-1.4	41.1	-2.2	42.8	-3.2	44.9

$$\Delta T_{cooling} = 31.1 - 24 = 7.1 \text{ }^{\circ}\text{C}$$

$$\Delta T_{heating} = 20 - 4.1 = 15.9 \text{ }^{\circ}\text{C}$$

$$H_{building} = 2.5m$$

$$A_{roof} = 200m^2$$

$$A_{wall} = 144m^2$$

Two occupants

One bedroom

Internal gains:

$$\dot{Q}_{ig_{sensible}} = 136 + 2.2 \times A_{cf} + 22 N_{oc} = 136 + 2.2 \times 200 + 22 \times 2 = 620 \text{ W}$$

$$\dot{Q}_{ig_{latent}} = 20 + 0.22 \times A_{cf} + 12 N_{oc} = 20 + 0.22 \times 200 + 12 \times 2 = 88 \text{ W}$$

Infiltration:

Table 3 Unit Leakage Areas

Construction	Description	$A_{ul}$ , cm <sup>2</sup> /m <sup>2</sup>
Tight	Construction supervised by air-sealing specialist	0.7
Good	Carefully sealed construction by knowledgeable builder	1.4
Average	Typical current production housing	2.8
Leaky	Typical pre-1970 houses	5.6
Very leaky	Old houses in original condition	10.4

$$A_{es} = A_{wall} + A_{roof}$$

$$= 200 + 144 = 344 \text{ m}^2$$

$$A_L = A_{es} \times A_{ul}$$

$$= 344 \times 1.4 = 481.6 \text{ cm}^2$$

Table 5 Typical IDF Values, L/(s·cm <sup>2</sup> )									
H, m	Heating Design Temperature, °C					Cooling Design Temperature, °C			
	-40	-30	-20	-10	0	10	30	35	40
2.5	0.10	0.095	0.086	0.077	0.069	0.060	0.031	0.035	0.040
3	0.11	0.10	0.093	0.083	0.072	0.061	0.032	0.038	0.043
4	0.14	0.12	0.11	0.093	0.079	0.065	0.034	0.042	0.049
5	0.16	0.14	0.12	0.10	0.086	0.069	0.036	0.046	0.055
6	0.18	0.16	0.14	0.11	0.093	0.072	0.039	0.050	0.061
7	0.20	0.17	0.15	0.12	0.10	0.075	0.041	0.051	0.068
8	0.22	0.19	0.16	0.14	0.11	0.079	0.043	0.058	0.074

$$IDF_{heating} = 0.065 \frac{L}{s \cdot cm^2}$$

$$IDF_{cooling} = 0.032 \frac{L}{s \cdot cm^2}$$

$$Q_{infiltration_{heating}} = A_L \times IDF_{heating} = 481.6 \times 0.065$$

$$= 31.30 \frac{L}{s}$$

$$Q_{infiltration_{cooling}} = A_L \times IDF_{cooling} = 481.6 \times 0.032$$

$$= 15.41 \frac{L}{s}$$

### Ventilation:

$$Q_v = 0.05 A_{cf} + 3.5 (N_{br} + 1) = 0.05 \times 200 + 3.5 \times 2 = 17 \frac{L}{s}$$

$$Q_{inf-ventilation_{heating}} = Q_{infiltration_{heating}} + Q_v = 31.30 + 17 = 48.30 \frac{L}{s}$$

$$Q_{inf-ventilation_{cooling}} = Q_{infiltration_{cooling}} + Q_v = 15.41 + 17 = 32.41 \frac{L}{s}$$

$$C_{sensible} = 1.23, C_{latent} = 3010$$

$$\begin{aligned} \dot{Q}_{inf-ventilation_{cooling_{sensible}}} &= C_{sensible} Q_{inf-ventilation_{cooling}} \Delta T_{cooling} \\ &= 1.23 \times 32.41 \times 7.1 = 283.04 W \end{aligned}$$

$$\begin{aligned} \dot{Q}_{inf-ventilation_{heating_{sensible}}} &= C_{sensible} Q_{infiltration_{heating}} \Delta T_{heating} \\ &= 1.23 \times 48.30 \times 15.9 = 944.60 W \end{aligned}$$

$$\Delta \omega = \omega_{out} - \omega_{in} = 0.0132 - 0.0093 = 0.0039 \frac{kg_{water}}{kg_{DryAir}}$$

$$\begin{aligned} \dot{Q}_{inf-ventilation_{cooling_{latent}}} &= C_{latent} Q_{inf-ventilation_{cooling}} \Delta \omega_{cooling} \\ &= 3010 \times 32.41 \times 0.0039 = 380.46 W \end{aligned}$$