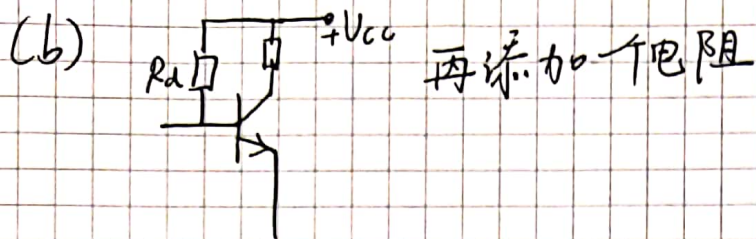


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2.1 (a) $-V_{CC}$ 变为 $+V_{CC}$



(c) ~~改为~~ ~~PNP型~~ $-V_{CC}$ 变为 $+V_{CC}$

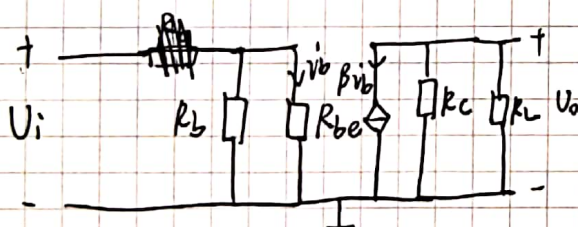
~~改~~ V_{BB} 反接, 并在 V_{BB} 与地之间加一个电阻或电容

(d) 在 V_{BB} 与地间加一个电阻, C_1 左边为+, $-V_{CC}$ 与 C 极间加一个电阻

2.5 $V_{CC} = U_{BEQ} + I_{BQ} \cdot R_b = 0.7 + 20 \times 10^{-6} \times 510 \times 10^3 \text{ V}$
 $= 0.7 + 10.2 = 10.9 \text{ V}$

$U_o = V_{CC} - I_{CQ} R_c = V_{CC} - \beta I_{BQ} R_c = 10.9 - 80 \times 20 \times 10^{-6} \times 510 \times 10^3$
 $= 2.9 \text{ V}$

动态时



$R_{be} = 1 \text{ k}\Omega$

$U_o = -\beta v_{be} (R_c \parallel R_L) = -80 \times 20 \times 10^{-6} \times 2.5 \times 10^3$
 $= -4 \text{ V}$

$\therefore A_u = \frac{-4 \text{ V}}{20 \text{ mV}} = -200$

$R_i = R_b \parallel R_{be} \approx 1 \text{ k}\Omega$

$R_o = R_c = 5 \text{ k}\Omega$

~~$R_i = R_b \parallel R_{be} \approx 1 \text{ k}\Omega$~~

$\frac{U_o R_i}{R_i + R_o} = U_i \therefore U_o = 60 \text{ mV}$

(1) X (2) X (3) X (4) ✓

(5) ✓ (6) X (7) X (8) ✓

(9) ✓ (10) X (11) X (12) ✓



2.6 测静态电位将 U_2 置 0

$$(1) I_{BQ} = \frac{V_{CC} - U_{BE}}{R_{b2}} - \frac{U_{BE}}{R_{b1}} \quad U_0 = V_{CC} - I_C R_C = V_{CC} - \beta I_{BQ} R_C$$

$$I_{BQ} = 0.0116 \text{ mA} \quad U_C \approx 7.9 \text{ V}$$

$$(2) U_{BE} = 0. \text{ T 截止 } U_C = 15 \text{ V}$$

$$(3) I_{BQ} = \frac{V_{CC} - U_{BE}}{R_{b2}} \quad U_C = V_{CC} - I_C R_C$$

$$\approx 0.174 \text{ mA}$$

$$\approx 0.024 \text{ mA}$$

$$\text{临界饱和基极电流 } I_{BS} = \frac{V_{CC} - U_{CES}}{\beta R_C} \approx 0.024 \text{ mA} < 0.174 \text{ mA}$$

$$\therefore \text{T 饱和 } U_C = U_{CES} = 0.5 \text{ V}$$

$$(4) R_{b2} \text{ 开路, T 截止, } U_C = 15 \text{ V}$$

$$(5) R_{b2} \text{ 短路, T 损坏, 若 } b-e \text{ 断路则 } U_C = 15 \text{ V}$$

$$\text{若 } b-e \text{ 短路, 则 } U_C \text{ 未知.}$$

$$(6) \text{ 若 } R_C \text{ 短路, 则 } U_C = 15 \text{ V.}$$

$$2.7 R \rightarrow \infty \text{ 计算静态工作点 } I_{BQ} = \frac{V_{CC} - U_{BEQ}}{R_b} - \frac{U_{BEQ}}{R_s}$$

$$I_{CQ} = \beta I_{BQ} \approx 1.76 \text{ mA}$$

$$\approx 22 \mu\text{A}$$

$$U_{CEQ} = V_{CC} - \beta I_{BQ} R_C \approx 6.2 \text{ V}$$

$$b-e \text{ 间动态电阻 } Y_{be} = Y_{be'} + \beta \frac{U_T}{I_{CQ}} = 100 + \frac{26 \text{ mV}}{22 \mu\text{A}} \approx 1.3 \text{ k}\Omega$$

$$\dot{A}_u = -\frac{\beta R_C}{j_b Y_{be}} = -\frac{\beta R_C}{Y_{be}} \approx -308 \quad R_i = R_b // Y_{be} \approx 1.3 \text{ k}\Omega$$

$$R_o = R_C = 5 \text{ k}\Omega$$

$$R_L = 3 \text{ k}\Omega \quad Q \text{ 点不变 } I_{BQ} \approx 22 \mu\text{A} \quad I_{CQ} \approx 1.76 \text{ mA} \quad Y_{be} \approx 1.3 \text{ k}\Omega$$

$$\dot{A}_u = -\frac{\beta (R_C // R_L)}{Y_{be}} \approx -115 \quad R_i = R_b // Y_{be} \approx 1.3 \text{ k}\Omega$$

$$R_o = R_C = 5 \text{ k}\Omega$$



$$2.9 (1) \frac{V_{CC} - U_{CEQ}}{\beta R_C} = I_{BQ} \quad R_b = \frac{V_{CC} - U_{BEQ}}{I_{BQ}} \quad \text{得 } R_b = 565 \text{ k}\Omega$$

$$(2) A_u > 220 \quad A_u = - \frac{\beta(R_L // R_C)}{r_{be}} = - \frac{100 \times (R_C // 15 \text{ k}\Omega)}{1 \text{ k}\Omega} > 220$$

$$\therefore R_C' > 2200 \quad \frac{R_C // 15 \text{ k}}{R_C // 15 \text{ k}} > 2200 \quad R_C > 3928.6 \Omega$$

$\therefore R_C$ 至少为 3928.6Ω .

2.11 (1) 静态时 等效电路为

$$I_{BQ} = \frac{V_{BB} - U_{BEQ}}{R_b' + (1+\beta)(R_f + R_e)}$$

$$\text{得 } I_{BQ} \approx 10 \mu\text{A}$$

$$I_{CQ} \approx 1 \text{ mA}$$

$$U_{CEQ} = V_{CC} - I_C(R_C) - I_E \times (R_f + R_e) = 5.7 \text{ V}$$

$$\text{动态分析} \quad r_{be} = r_{bb'} + \beta \frac{U_T}{I_{CQ}} = 100 + 100 \times \frac{26 \text{ mV}}{1 \text{ mA}} = 2700 \Omega$$

$$A_u = - \frac{\beta(R_C // R_L)}{r_{be} + (1+\beta)R_f} \approx -7.6$$

$$R_i = R_{b1} // R_{b2} // (r_{be} + (1+\beta)R_f) \approx 3.7 \text{ k}\Omega$$

$$R_o = R_C = 5 \text{ k}\Omega$$

(2) 因为 $U_{EQ} = U_{BQ} - U_{BEQ}$ 基本不变

$$\text{因为 } I_{EQ} = \frac{(V_{BB} - U_{BEQ})(1+\beta)}{R_b' + (1+\beta)(R_f + R_e)} = \frac{V_{BB} - U_{BEQ}}{\frac{R_b'}{1+\beta} + R_f + R_e} \quad \text{因为 } \frac{R_b'}{1+\beta} \ll R_f + R_e$$

I_{EQ} 基本不变 $\therefore U_{EQ}$ 基本不变 但 $I_{BQ} \approx \frac{V_{BB} - U_{BEQ}}{(1+\beta)(R_f + R_e)}$ 明显减小

约为 $5 \mu\text{A}$

(3) 若 C_e 开路 则 $R_i = R_{b1} // R_{b2} // (r_{be} + (1+\beta)(R_f + R_e)) \approx 4.1 \text{ k}\Omega$

$$A_u = - \frac{\beta(R_C // R_L)}{r_{be} + R_f + R_e(1+\beta)} \approx -1.92$$



2.12 (1) 静态时

$$V_{CC} = I_{BQ} R_b + (1+\beta) I_{BQ} R_e + U_{BEQ}$$

$$\text{得 } I_{BQ} = \frac{V_{CC} - U_{BEQ}}{R_b + (1+\beta) R_e} = \frac{32.76 \text{ V}}{32.76 \text{ k}\Omega} = 32.78 \mu\text{A}$$

$$I_{CQ} = \beta I_{BQ} \approx 2.58 \text{ mA}$$

$$U_{CEQ} = V_{CC} - (1+\beta) I_{BQ} R_e \approx 7.14 \text{ V}$$

(2) $R_L = \infty$

$$\dot{A}_u = \frac{(1+\beta) R_e}{r_{be} + (1+\beta) R_e} \approx 0.996$$

$$R_i = R_b // [r_{be} + (1+\beta) R_e] \approx 110 \text{ k}\Omega$$

$$R_o = R_e = 3 \text{ k}\Omega$$

$$R_L = 3 \text{ k}\Omega \quad \dot{A}_u = \frac{(1+\beta)(R_e // R_L)}{r_{be} + (1+\beta)(R_e // R_L)} \approx 0.992$$

$$R_i = R_b // [r_{be} + (1+\beta)(R_e // R_L)] \approx 76 \text{ k}\Omega$$

输出电阻与负载无关 $R_o = R_e // \frac{R_s // R_b + r_{be}}{1+\beta} \approx 37 \Omega$

2.13 (1) 静态时

$$I_{BQ} = \frac{V_{CC} - U_{BEQ}}{R_b + (1+\beta) R_e} \approx 31 \mu\text{A}$$

$$I_{CQ} = \beta I_{BQ} \approx 1.86 \text{ mA}$$

$$U_{CEQ} \approx V_{CC} - I_{CQ} (R_c + R_e) = 4.56 \text{ V}$$

动态时 $\dot{A}_u = - \frac{\beta (R_c // R_L)}{r_{be} + (1+\beta) R_e} \approx -96 \quad r_{be} = r_{be0} + \beta \frac{U_T}{I_{CQ}}$

$$R_i = R_b // r_{be} \approx 939 \Omega$$

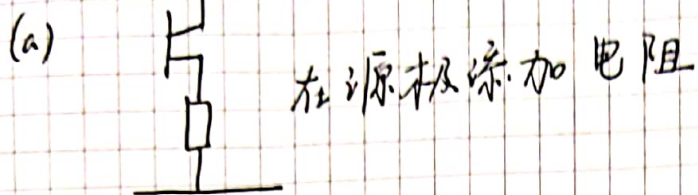
$$R_o = R_c = 3 \text{ k}\Omega$$

(2) 求 U_i $U_i = \frac{U_s R_i}{R_s + R_i} = 3.2 \text{ mV} \quad U_o = |\dot{A}_u| U_i = 307 \text{ mV}$

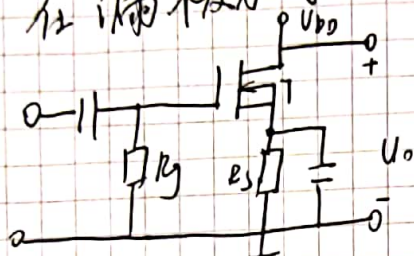
若 C_3 开路 $\dot{A}_u = - \frac{\beta (R_c // R_L)}{r_{be} + (1+\beta) R_e} \approx -1.45 \quad U_i = \frac{R_i U_s}{R_s + R_i} \approx 9.6 \text{ mV} \quad U_o = |\dot{A}_u| U_i \approx 14 \text{ mV}$



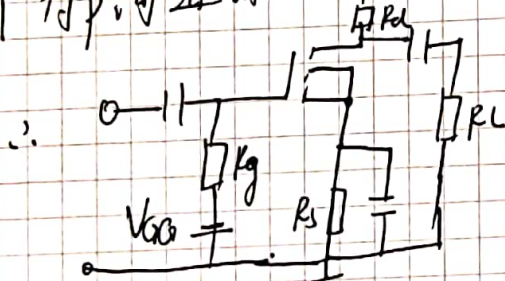
2.14



(b) 在漏极加电阻 R_d , 在输入端加耦合电容

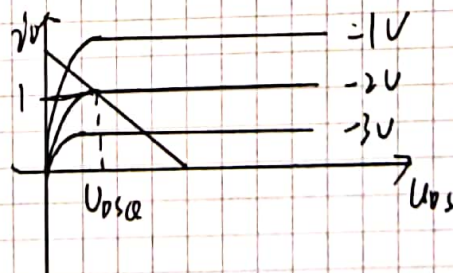
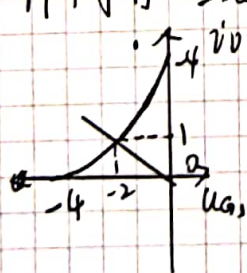


(c) Γ 为 p 沟道增强型管 $\therefore U_{GS} < 0, U_{DS} < 0$
 $+U_{DD}$ 变为 $-V_{DD}$
 加个电源 V_{GG}

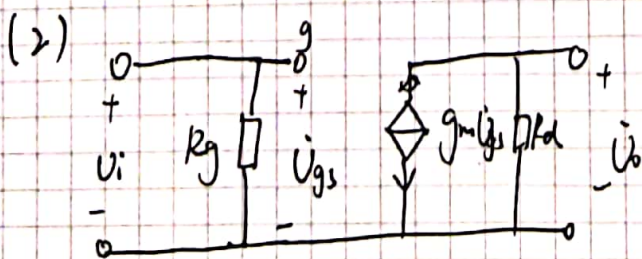


2.15 (1) 静态时该电路自给偏压 $U_{GS} = -I_{DQ} R_S \therefore I_{DQ} = -\frac{1}{R_S} U_{GS}$

作图得 $I_{DQ} = 1\text{mA}$ $U_{GSQ} = -2\text{V}$



$$U_{DS} = V_{DD} - I_D (R_d + R_s) \therefore U_{DSQ} \approx 3\text{V}$$



$$A_u = \frac{U_o}{U_i} = -\frac{g_m U_{GS} R_d}{U_{GS}} = -g_m R_d$$

$$g_m = \frac{-2}{(U_{GS(off)})} \sqrt{I_{DQ} I_{DSS}} = 1\text{ms}$$

$$\therefore A_u = -5 \quad R_i = R_g = 1\text{M}\Omega$$

$$R_o = R_d = 5\text{k}\Omega$$



2.17 (1) 若底部失真, 则应降低 U_{GS} , 则增大 R_1, R_2 , 降低 R_2, R_d 。
若顶部失真, 则应升高 U_{GS} , 则增大 R_2, R_d , 减小 R_1, R_s 。

(2) 可减小 R_1, R_s , 增大 R_2 来增大 U_{GS} 从而
增大 I_{DQ} , 从而增大 g_m , 或增大 R_d 。

