# EE281 (Introduction to Electrical Engineering II) and EE285 (Electronics I) - Lecture 1

# Diodes (Two terminal semiconductor devices)

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### Intrinsic Semiconductor



#### Definition

A crystal of pure and regular lattice structure is called intrinsic semiconductor.

#### Materials

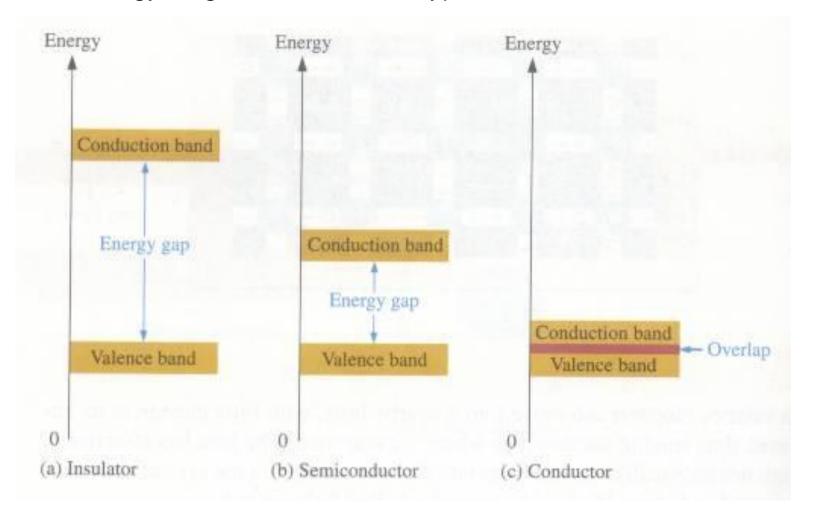
- Silicon---today's IC technology is based entirely on silicon
- Germanium---early used
- Gallium arsenide---used for microwave circuits

#### 10.1 Basic Diode Concepts

#### 10.1.1 Intrinsic Semiconductors

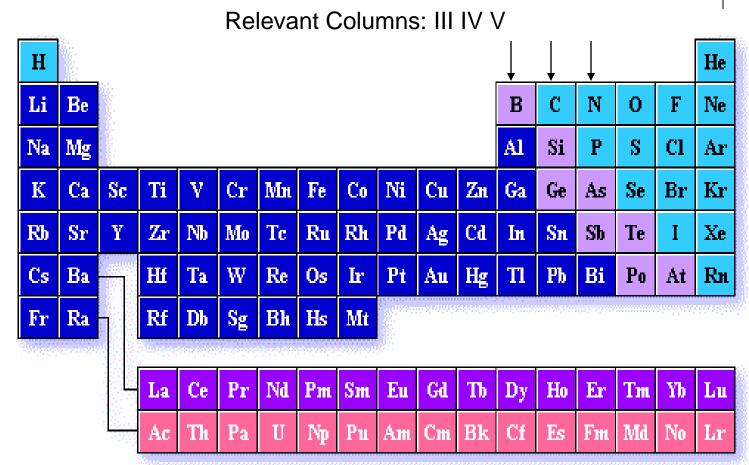
\* Energy Diagrams – *Insulator, Semiconductor, and Conductor* the energy diagram for the three types of solids



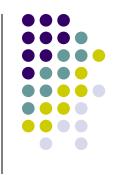


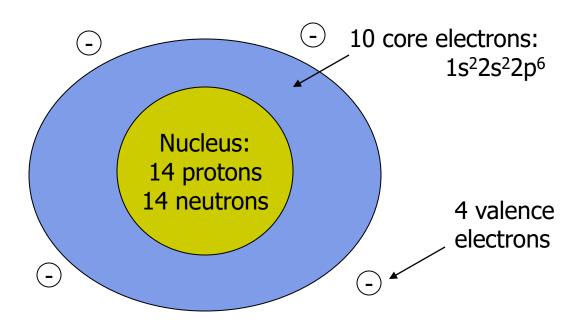
### **Periodic Table of Elements**





### **The Silicon Atom**



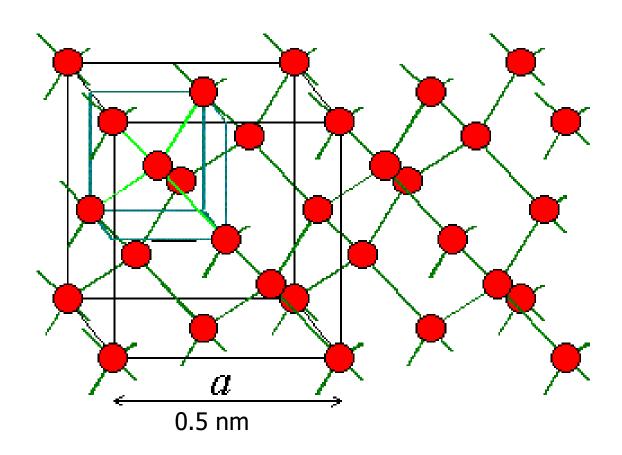


The 4 valence electrons are responsible for forming covalent bonds

### **Silicon Crystal**

**Each Si atom has <u>four</u> nearest neighbors — one for each valence electron** 

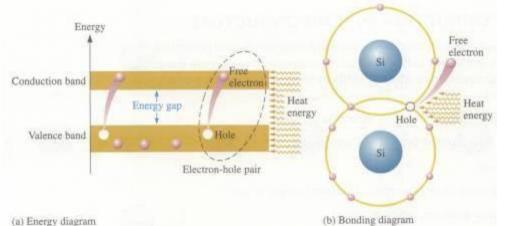


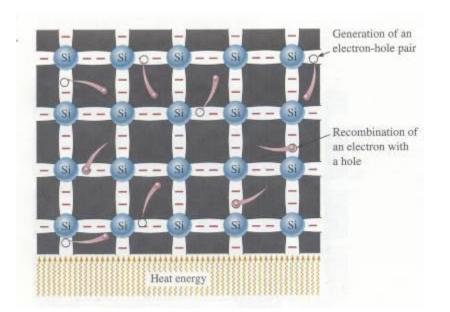


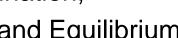
#### 10.1.1 Intrinsic Semiconductors

\* Intrinsic (pure) *Si* Semiconductor:

Thermal Excitation, Electron-Hole Pair, Recombination,







and Equilibrium

When equilibrium between excitation and recombination is reached:

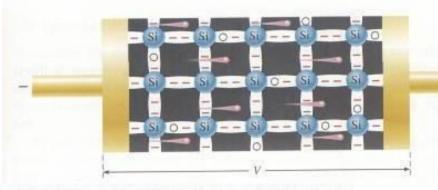
electron density = hole density $n_i = p_i = 1.5 \times 10^{10} \text{ cm}^{-3}$ for intrinsicSi crystal at 300 K ( Note: Si crystal atom density  $is \sim 5 \times 10^{22} \text{ cm}^{-3}$ 

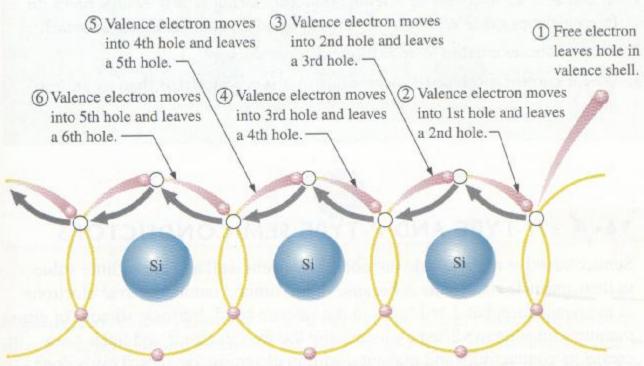


#### 10.1.1 Intrinsic Semiconductors

\*Apply a voltage across a piece of *Si:* 

electron current
and hole current

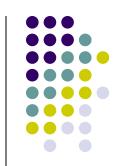


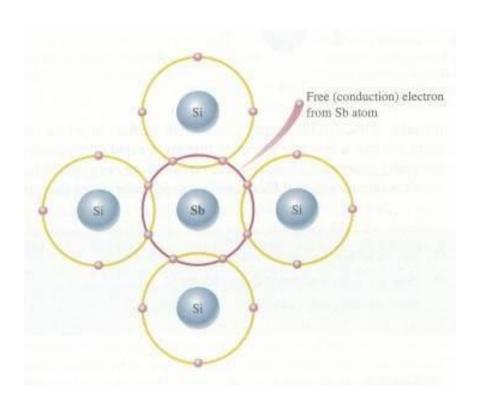


When a valence electron moves left to right to fill a hole while leaving another hole behind, a hole has effectively moved from right to left. Gray arrows indicate effective movement of a hole.

#### 10.1.2 N- and P- Type Semiconductors

- \* *Doping*: adding of impurities (i.e., dopants) to the intrinsic semiconductor material.
- \* N-type: adding Group V dopant (or donor) such as As, P, Sb,...





 $n \cdot p = constant \ for \ a \ semiconductor$ For  $Si \ at \ 300K$ 

$$n \cdot p = n_i^2 = p_i^2 = (1.5 \times 10^{10})^2$$

In n-type material

 $n \cong N_d$  the donor conceration

$$n = N_d \gg n_i$$
,  $p \ll p_i$ 

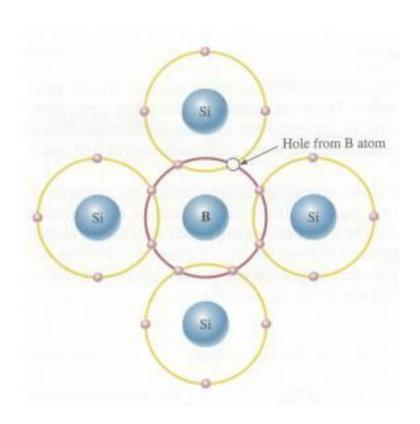
We call

electron the major charge carrier hole the minor cahage carrier

#### 10.1.2 N- and P- Type Semiconductors

- \* *Doping*: adding of impurities (i.e., dopants) to the intrinsic semiconductor material.
- \* P-type: adding Group III dopant (or acceptor) such as AI, B, Ga,...





 $n \cdot p = constant \ for \ a \ semiconductor$ For Si at 300K

$$n \cdot p = n_i^2 = p_i^2 = (1.5 \times 10^{10})^2$$

In p-type material

 $p \cong N_a$  the acceptor conceration

$$p = N_a \gg p_i$$
,  $n \ll n_i$ 

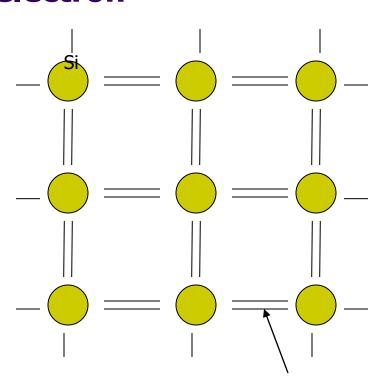
We call

hole the major charge carrier electron the minor cahage carrier

# **Two-dimensional Picture of Si**



*note:* each line ( —) represents a valence electron

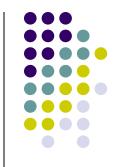


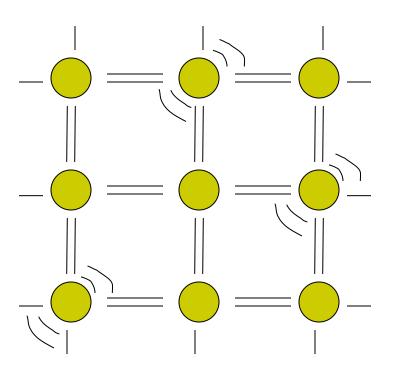
At T=0 Kelvin, all of the valence electrons are participating in covalent bonds

There are no "free" electrons, therefore no current can flow in the silicon → INSULATOR

covalent bond

### **Silicon at Room Temperature**

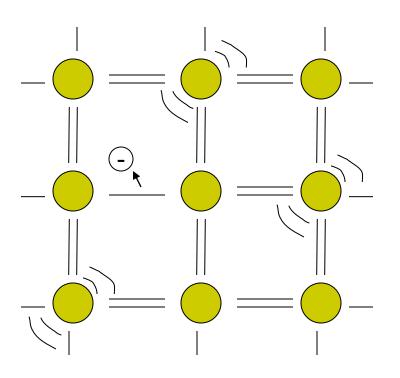




For T>0 K, the silicon atoms vibrate in the lattice. This is what we humans sense as "heat."

Occasionally, the vibrations cause a covalent bond to break and a valence electron is free to move about the silicon.

### Silicon at Room Temperature

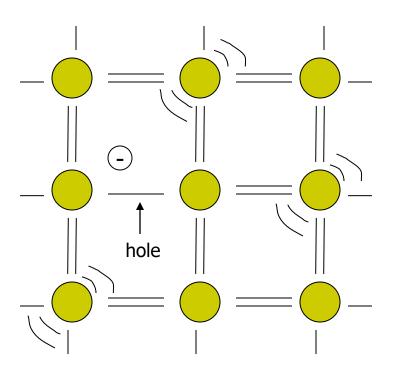


For T>0 K, the silicon atoms vibrate in the lattice. This is what we humans sense as "heat."

Occasionally, the vibrations cause a covalent bond to break and a valence electron is free to move about the silicon.

= free electron

### Silicon at Room Temperature



The broken covalent bond site is now *missing* an electron.

This is called a "hole"

The hole is a <u>missing negative</u> charge and has a charge of **+1**.

= a hole

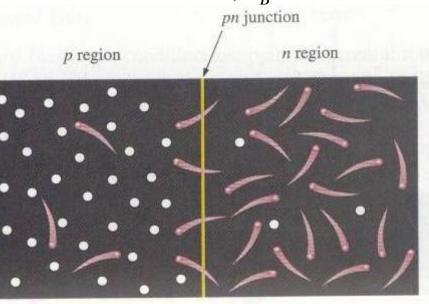


#### 10.1.3 The PN-Junction

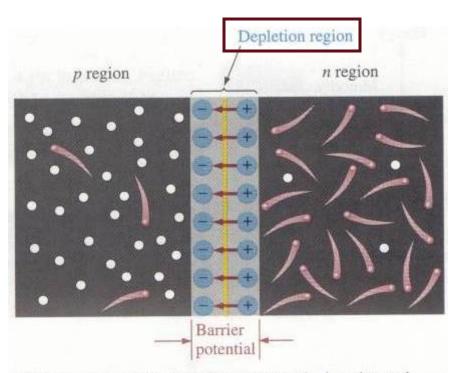
\* The interface in-between p-type and n-type material is called a *pn-junction*.

The barrier potential  $V_B \cong 0.6 - 0.7V$  for Si and 0.3V for Ge

at 300K: as  $T \uparrow, V_B \downarrow$ .



(a) At the instant of junction formation, free electrons in the n region near the pn junction begin to diffuse across the junction and fall into holes near the junction in the p region.



(b) For every electron that diffuses across the junction and combines with a hole, a positive charge is left in the n region and a negative charge is created in the p region, forming a barrier potential. This action continues until the voltage of the barrier repels further diffusion.

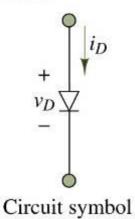


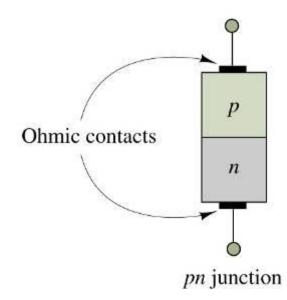
#### 10.1.4 Biasing the PN-Junction

- \* There is no movement of charge through a pn-junction at equilibrium.
- \* The pn-junction form a *diode*which allows current in only one
  direction and prevent the
  current in the other direction as
  determined by the *bias*.

The arrow in the circuit symbol for the diode indicates the direction of current flow when the diode is forward-biased.



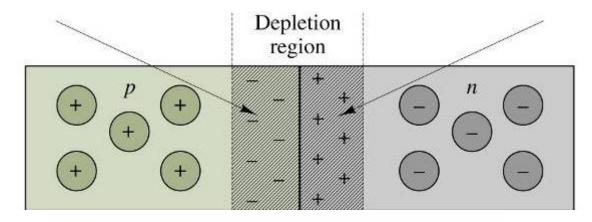


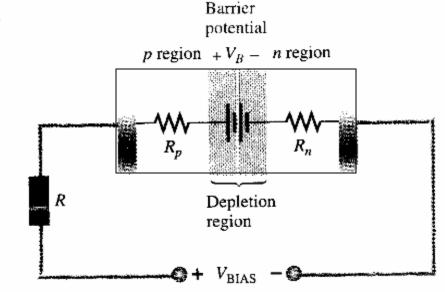


#### 10.1.4 Biasing the PN-Junction

\*Forward Bias: dc voltage positive terminal connected to the p region and negative to the n region. It is the condition that permits current through the pn-junction of a diode.



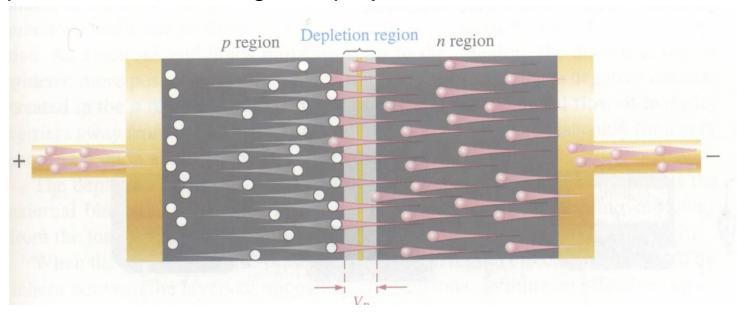


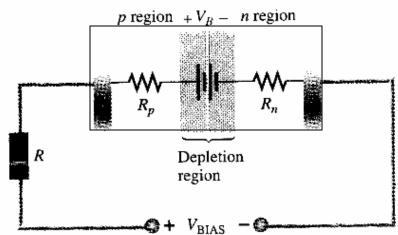


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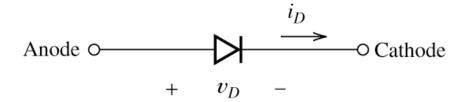


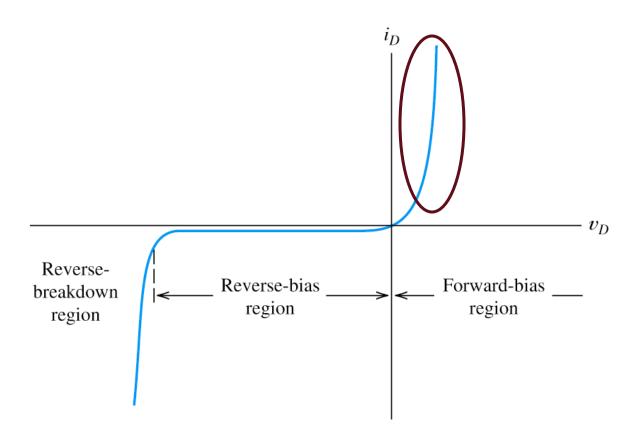




#### 10.1.4 Biasing the PN-Junction

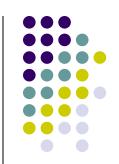
\*Forward Bias:

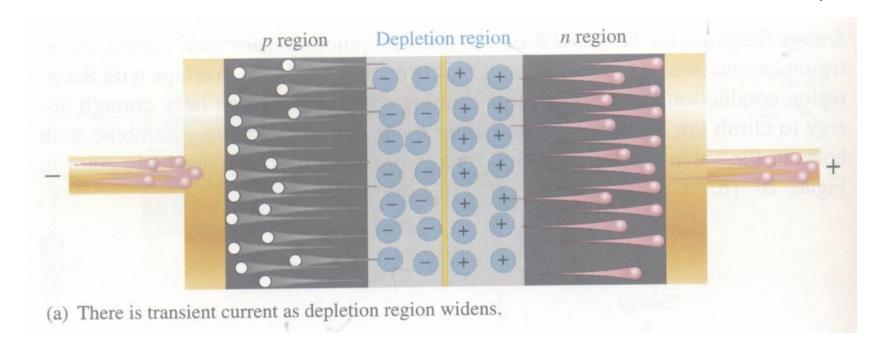






\*Reverse Bias: dc voltage negative terminal connected to the p region and positive to the n region. Depletion region widens until its potential difference equals the bias voltage, majority-carrier current ceases.

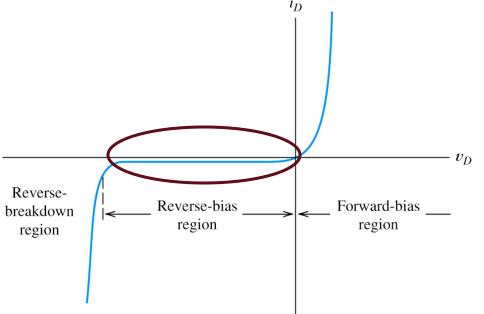


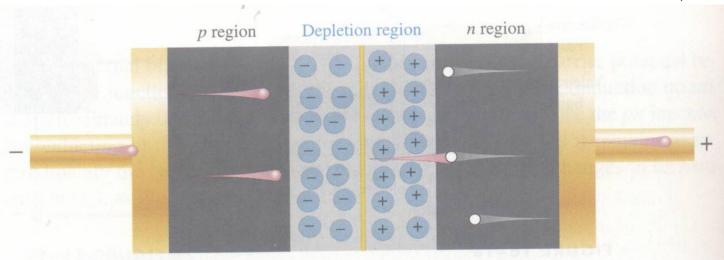


\*Reverse Bias:

majority-carrier current ceases.

\* However, there is still a very small current produced by minority carriers.



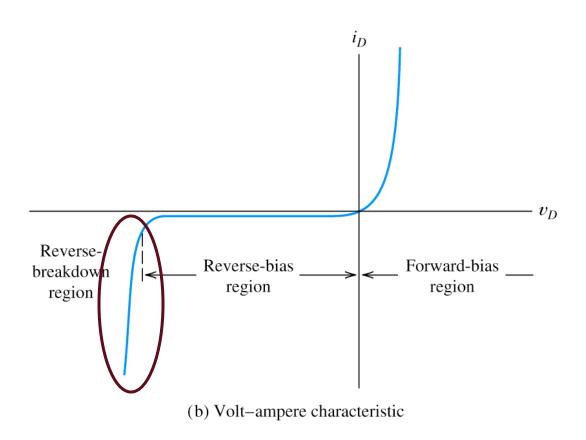


(b) Majority current ceases when barrier potential equals bias voltage. There is an extremely small reverse current due to minority carriers.

#### 10.1.4 Biasing the PN-Junction

\* Reverse Breakdown: As reverse voltage reach certain value, avalanche occurs and generates large current.





#### 10.1.5 The Diode Characteristic I-V Curve

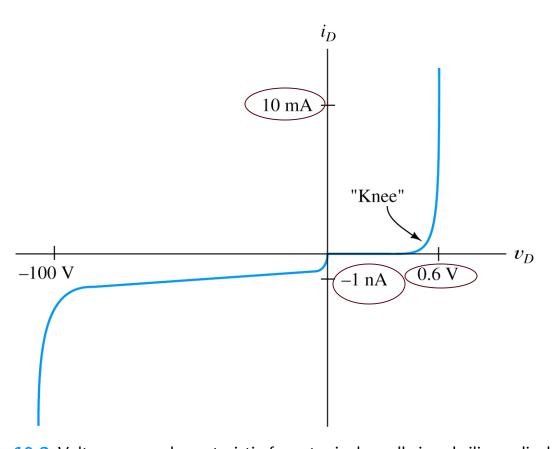
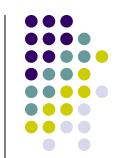


Figure 10.2 Volt–ampere characteristic for a typical small-signal silicon diode at a temperature of 300 K. Notice the change of scale for negative current and voltage.



### Two-terminal Devices with p-n Junction – Zener diode

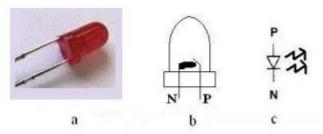


Two-terminal Devices with p-n Junction 1.3.a Zener Diode (ZD) (also referred as regulated diode) is a two terminal device that is widely used in voltage regulators. As shown in the characteristic curve of diode (Fig 1.5) (b) ), when the reverse bias, applied to the semiconductor, has reached to Vz, the current will be dramatically increased while the voltage keeps constant. The value of Vz can be controlled by changing the doping concentration. If the doping concentration is increased, the increased amount of impurity will decrease the value of Vz. The regulated values of the zener diode are thus distributed in the range from 3V to several hundreds of volts, whereas the power range is distributed 100W.

### **Light Emitting Diode (LED)**



Fig. 1.8 1.3.b Light Emitting Diode (LED) LED is one kind of p-n junction device made of galliumarsenic phosphide or gallium phosphide. When the electrons and holes of LED Are combined under the forward bias, the energy carried by free electrons will be transformed into light energy that is within the spectrum of visible light. If the silicon or germanium is used as material, the energy will be transformed into heat energy, but no visible light will be generated. Typically, the operating voltage of LED is around 1.7 V ~ 3.3 V, the power consumption is around 10 ~ 50 mW and the operating life is more than 100 thousand hours. The LEDs can generate visible lights with colors red, yellow, green..etc. depending on the selected materials. The LED will be illuminated if minimum 1.5V forward voltage is applied. If more than 1.5 V is continuously applied to LED, it will burn down. Moreover, as the breakdown voltage of LED is very low, the applied reverse voltage of LED should not exceed 3 V. Appearance (a and b) and symbol (c) of LED is given below.





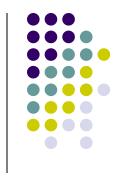
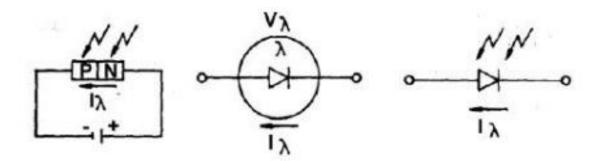


Photo-diode is one kind of junction type semiconductor device with operating region limited at the reverse bias region, that is, a photo is never applied forward bias. The reverse current of photo-diode is directly proportional to the strength of the light.



#### 10.1.6 Shockley Equation

\* The Shockley equation is a theoretical result under certain simplification:

$$i_D = I_s \left[ exp \left( \frac{v_D}{nV_T} \right) - 1 \right]$$

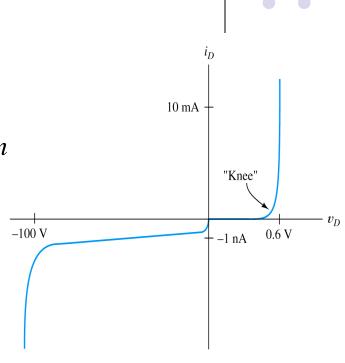
where  $I_s \cong 10^{-14}$  A at 300K is the (reverse) saturation current,  $n \cong 1$  to 2 is the emission coefficient,

$$V_T = \frac{kT}{q} \cong 0.026 V$$
 at 300K is the thermal voltage

*k is the Boltzman's constant, q* =  $1.60 \times 10^{-19}$  *C* 

when 
$$v_D \ge \approx 0.1V$$
,  $i_D \cong I_s exp\left(\frac{v_D}{nV_T}\right)$ 

This equation is not applicable when  $v_D < 0$ 



#### 10. Diodes – Load-Line Analysis of Diode Circuits

#### 10.2 Load-Line Analysis of Diode Circuit

We can use 
$$v = iR, i = C \frac{dv}{dt}, v = L \frac{di}{dt}, ...$$

but when there is a diode: 
$$i_D = I_s \left[ exp \left( \frac{v_D}{nV_T} \right) - 1 \right]$$

It is difficult to write KCL or KVL equations.

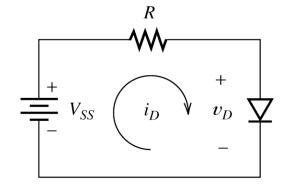


Figure 10.5 Circuit for load-line analysis.

For the circuit shown, KVL gives:

$$V_{SS} = R i_D + v_D$$

If the I - V curve of the diode is given, we can perform the

"Load - Line Analysis"

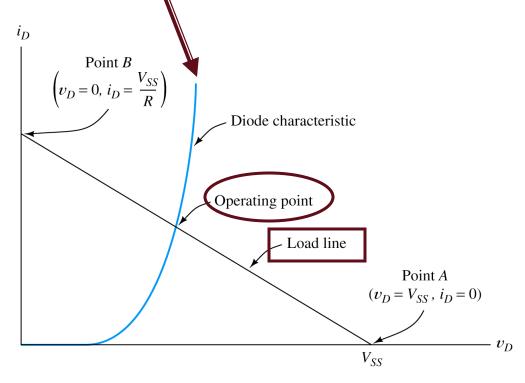


Figure 10.6 Load-line analysis of the circuit of Figure 10.5.

#### 10. Diodes – Load-Line Analysis of Diode Circuits

#### Example 10.1- Load-Line Analysis

For the circuit shown,

Given:  $V_{SS} = 2V, R = 1k\Omega$ ,

the I - V curve of the diode

Find: the diode current and voltage

at the operating point(Q - point)

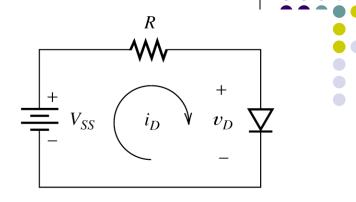


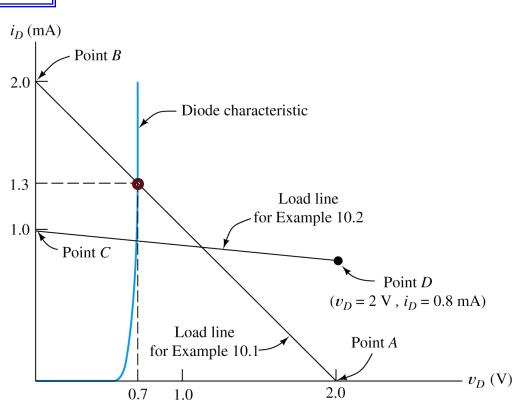
Figure 10.5 Circuit for load-line analysis.

$$V_{SS} = R i_D + v_D, i.e.,$$
  
 $2 = 1000 i_D + v_D$ 

 $\Rightarrow$  perform load - line analysis

 $\Rightarrow$  at the operating point

 $V_{DQ} \cong 0.70 \, V, \ i_{DQ} \cong 1.3 \, \text{mA}$ 



#### 10. Diodes – Load-Line Analysis of Diode Circuits

#### Example 10.2 - Load-Line Analysis

For the circuit shown,

Given: Vss = 10 V,  $R = 10 k\Omega$ ,

the I - V curve of the diode

Find: the diode current and voltage

at the operating point

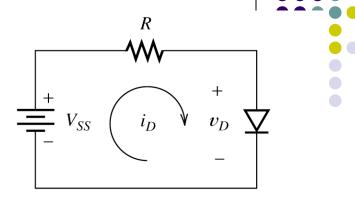
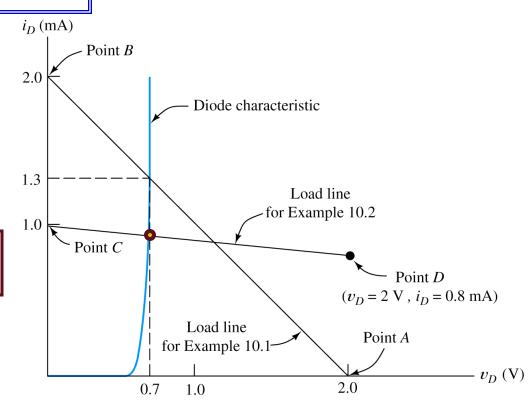


Figure 10.5 Circuit for load-line analysis.

$$V_{SS} = Ri_D + v_D$$
, i.e.,  
 $10 = 10k i_D + v_D$   
 $\Rightarrow perform load - line analysis$   
 $\Rightarrow at the operating point$ 

 $V_{DO} \cong 0.68 V$ ,  $i_{DO} \cong 0.93 mA$ 

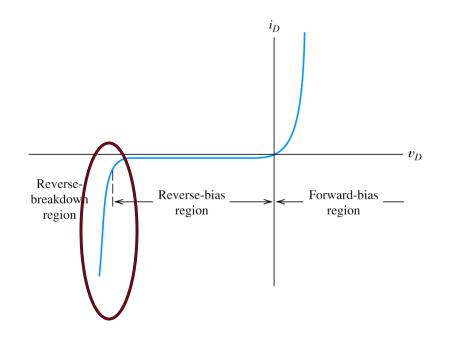


#### 10. Diodes – Zener Diode Voltage-Regulator Circuits

#### 10.3 Zener-Diode Voltage-Regulator Circuits

#### 10.3.1 The Zener Diode

- \* **Zener diode** is designed for operation in the reverse-breakdown region.
- \* The *breakdown voltage* is controlled by the doping level (-1.8 V to -200 V).
- \* The major application of Zener diode is to provide an output reference that is stable despite changes in input voltage power supplies, voltmeter,...



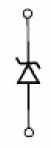


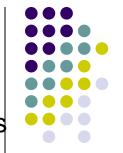
Figure 7.3 Zener diode symbol.



#### 10. Diodes – Zener-Diode Voltage-Regulator Circuits

#### 10.3.2 Zener-Diode Voltage-Regulator Circuits

\* Sometimes, a circuit that produces constant output voltage while operating from a variable supply voltage is needed. Such circuits are called *voltage regulator*.



- \* The Zener diode has a breakdown voltage equal to the desired output voltage.
- \* The resistor limits the diode current to a safe value so that Zener diode does not overheat.

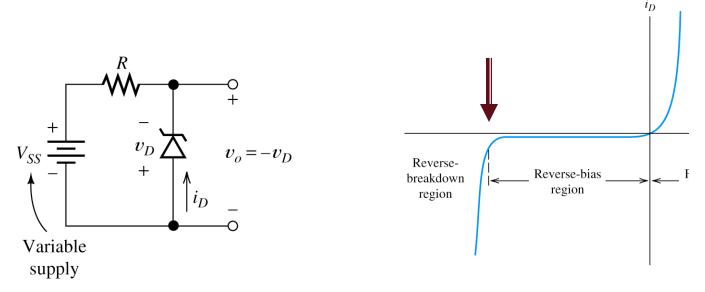


Figure 10.9 A simple regulator circuit that provides a nearly constant output voltage  $v_o$  from a variable supply voltage.

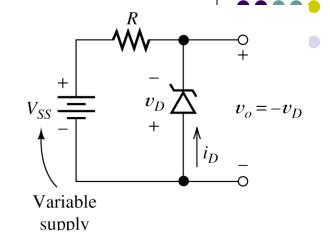
#### 10. Diodes – Zener-Diode Voltage-Regulator Circuits

#### Example 10.3 – Zener-Diode Voltage-Regulator Circuits

Given: the Zener diode I - V curve,  $R=1k\Omega$ 

Find: the output voltage for  $V_{SS} = 15 V$  and

$$V_{SS} = 20 V$$



#### KVL gives the load line:

$$V_{SS} + Ri_D + v_D = 0$$

From the Q - point we have:

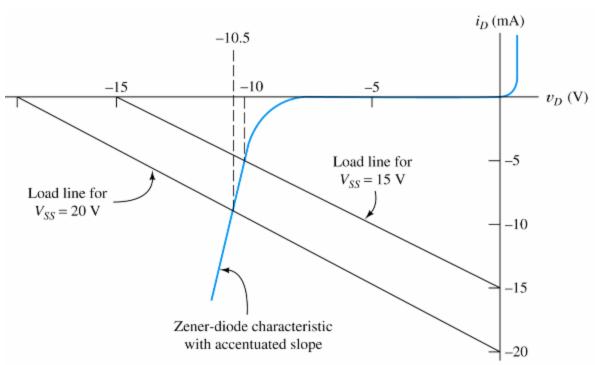
$$v_o = 10.0V \ for V_{SS} = 15V$$

$$v_o = 10.5V \text{ for } V_{SS} = 20V$$

5V change in input

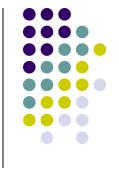
 $\Rightarrow$  0.5V change in  $v_o$ 

Actual Zener diode performs much better!



## 10. Diodes – Zener-Diode Voltage-Regulator Circuits 10.3.3 Load-Line Analysis of Complex Circuits

\* Use the Thevenin Equivalent



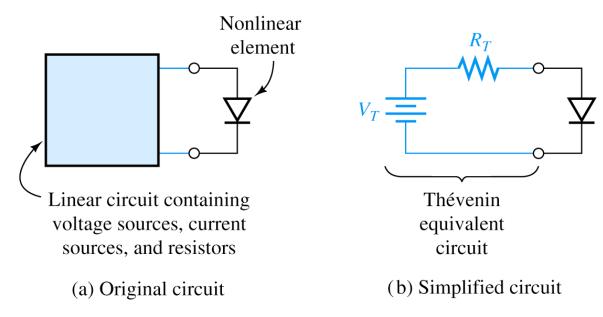
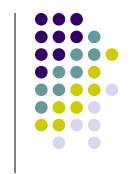


Figure 10.11 Analysis of a circuit containing a single nonlinear element can be accomplished by load-line analysis of a simplified circuit.

## 10. Diodes – Zener-Diode Voltage-Regulator Circuits Example 10.4 – Zener-Diode Voltage-Regulator with a Load

Given: Zener diode I - V curve,  $V_{SS}=24V, R=1.2k\Omega, R_L=6k\Omega$ 

Find: the load voltage  $v_L$  and source currents  $I_S$ 



Applying Thevenin Equivalent 
$$\Rightarrow V_T = V_{SS} \frac{R_L}{R + R_I} = 20V, R_T = \frac{RR_L}{R + R_I} = 1k\Omega$$

$$\Rightarrow V_T + R_T i_D + v_D = 0$$

$$\Rightarrow v_L = -v_D = 10.0V$$

$$I_S = (V_{SS} - v_L)/R = 11.67 \, mA$$

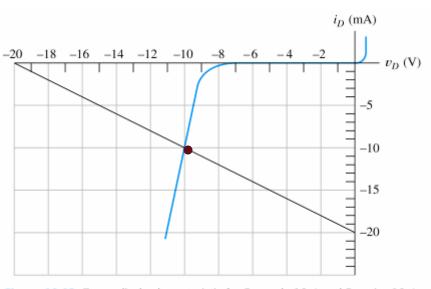


Figure 10.13 Zener-diode characteristic for Example 10.4 and Exercise 10.4.

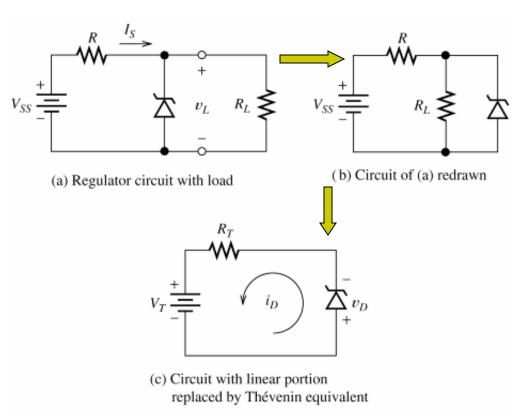


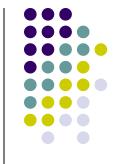
Figure 10.12 See Example 10.4.

#### 10. Diodes – Zener-Diode Voltage-Regulator Circuits

#### Quiz - Exercise 10.5

Given: the circuit and the Zener doide I - V curve as shown.

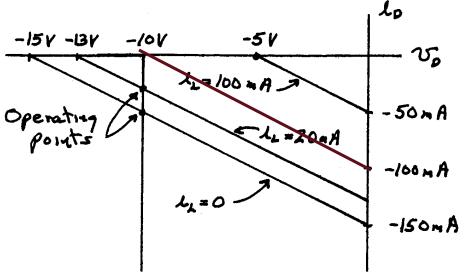
Find: the output voltage  $v_o$  for  $i_L = 0$ ,  $i_L = 20$ mA, and  $i_L = 100$ mA



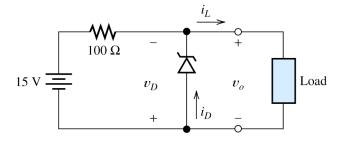
Writing a KVL equation for the loop consisting of the source, the resistor, and the load, we obtain:

$$15 = 100(i_L - i_D) - v_D$$

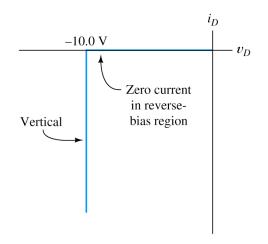
The corresponding load lines for the three specified values of  $i_L$  are shown:



At the intersections of the load lines with the diode characteristic, we find (a)  $v_o = -v_D = 10 \text{ V}$ ; (b)  $v_o = -v_D = 10 \text{ V}$ ; (c)  $v_o = -v_D = 5 \text{ V}$ . Notice that the regulator is effective only for values of load current up to 50 mA.



(a) Circuit diagram



(b) Zener-diode characteristic

#### 10.4 Ideal-Diode Model

- \* Graphical load-line analysis is too cumbersome for complex circuits.
- \* We may apply "Ideal-Diode Model" to simplify the analysis:
- (1) in forward direction: short-circuit assumption, zero voltage drop;
- (2) in reverse direction: open-circuit assumption.
- \* The ideal-diode model can be used when the forward voltage drop and reverse currents are negligible.

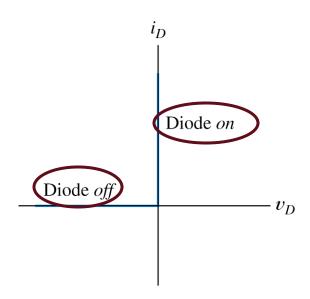
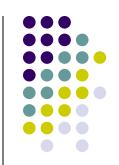
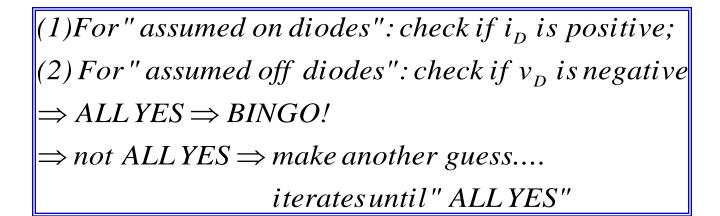


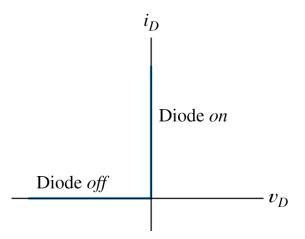
Figure 10.15 Ideal-diode volt–ampere characteristic.

#### 10.4 Ideal-Diode Model

- \* In analysis of a circuit containing diodes, we may not know in advance which diodes are on and which are off.
- \* What we do is first to make a guess on the state of the diodes in the circuit:



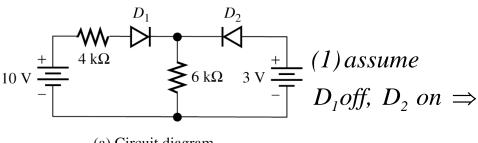




## Example 10.5 – Analysis by Assumed Diode States

## Analysis the circuit by assuming $D_1$ is off and $D_2$ on



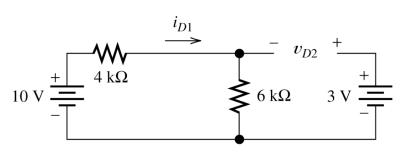


(a) Circuit diagram

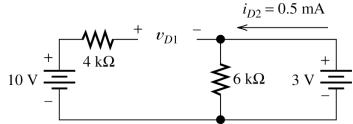


(2) assume

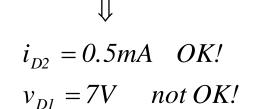
$$D_1$$
 on,  $D_2$  off



(c) Equivalent circuit assuming  $D_1$  on and  $D_2$  off (this is the correct assumption since  $i_{D1}$  turns out to be a positive value and  $v_{D2}$  turns out negative)



(b) Equivalent circuit assuming  $D_1$  off and  $D_2$  on (since  $v_{D1} = +7$  V, this assumption is not correct)



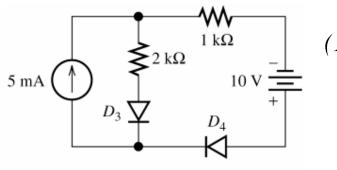
$$\Rightarrow i_{D1} = 1 \, mA \quad OK!$$

$$v_{D2} = -3 \, V \quad OK!$$

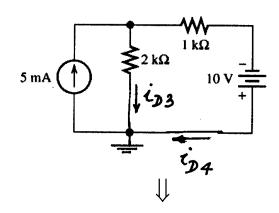
### Quiz - Exercise 10.8c

\* Find the diode states by using ideal-diode model. Starting by assuming both diodes are on.

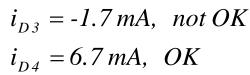


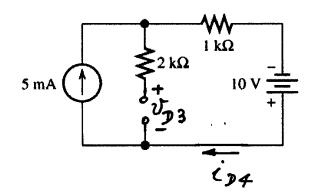


 $\begin{array}{ccc} (1) \, assume & \\ D_3 \, \, on & \Rightarrow \\ D_4 \, \, on & \end{array}$ 



(2) assume  $D_3$  off and  $D_4$  on



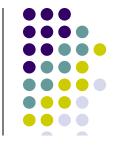


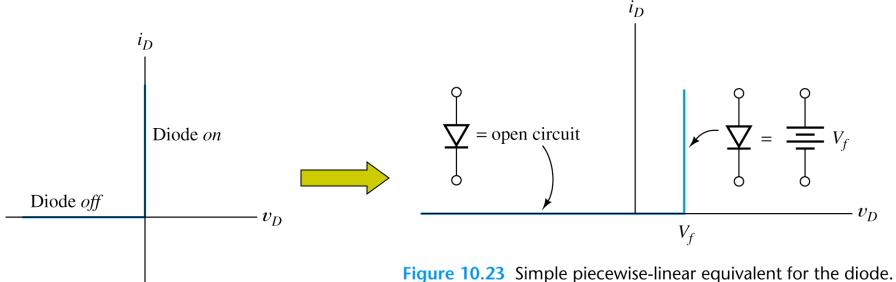
$$\Rightarrow i_{D4} = 5 \text{ mA}, \quad OK$$
$$v_{D3} = -5 V, \quad OK$$

### 10. Diodes – Piecewise-Linear Diode Models

#### 10.5 Piecewise-Linear Diode Models

### 10.5.1 Modified Ideal-Diode Model

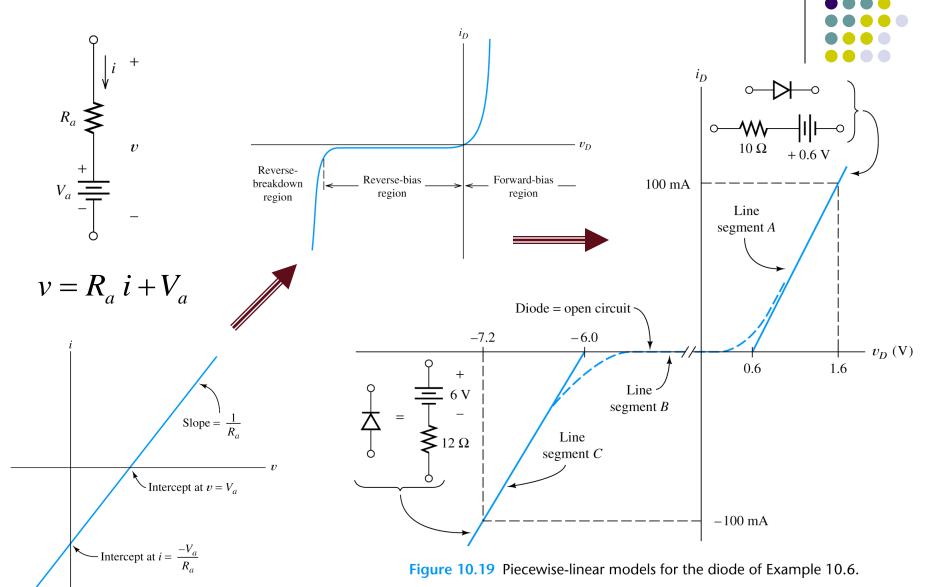




\* This modified ideal-diode model is usually accurate enough in most of the circuit analysis.

### 10. Diodes – Piecewise-Linear Diode Models

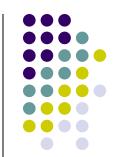
### 10.5.2 Piecewise-Linear Diode Models



### 10. Diodes - Rectifier Circuits

#### 10.6 Rectifier Circuits

- \* Rectifiers convert ac power to dc power.
- \* Rectifiers form the basis for electronic power suppliers and battery charging circuits.



#### 10.6.1 Half-Wave Rectifier

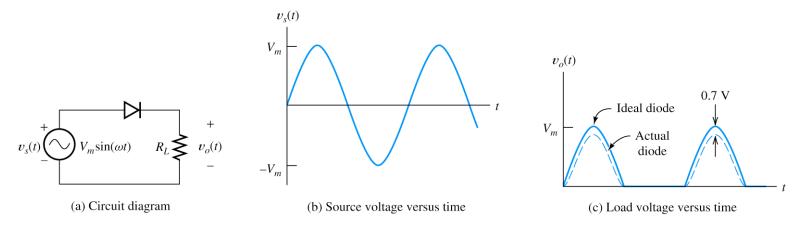
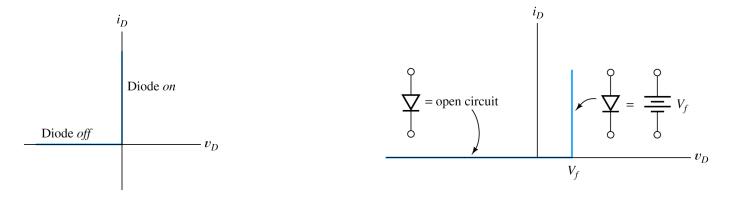


Figure 10.24 Half-wave rectifier with resistive load.



### 10. Diodes - Rectifier Circuits

## \* Battery-Charging Circuit

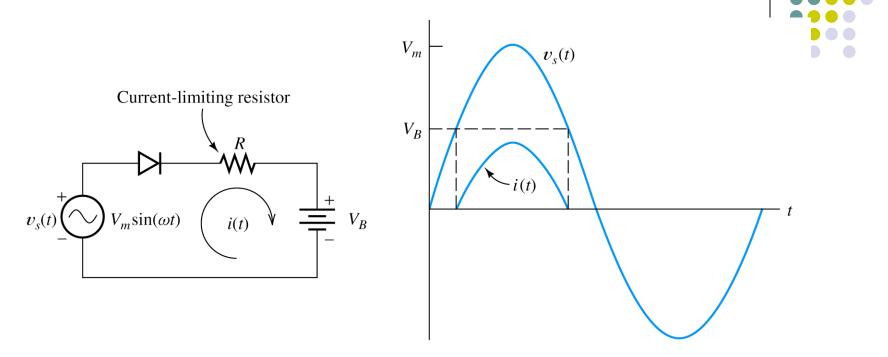
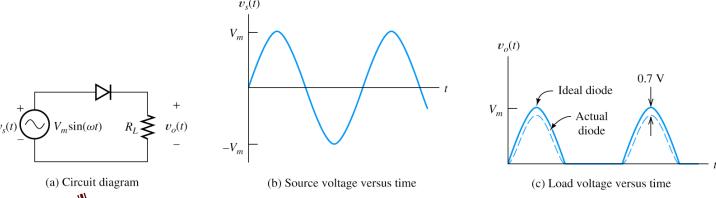


Figure 10.25 Half-wave rectifier used to charge a battery.

\* The current flows only in the direction that charges the battery.

### 10. Diodes - Rectifier Circuits

### \* Half-Wave Rectifier with Smoothing Capacitor



\* To place large capacitance across the output terminals:

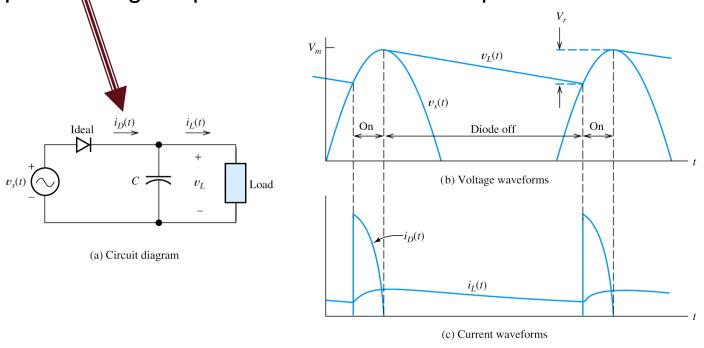
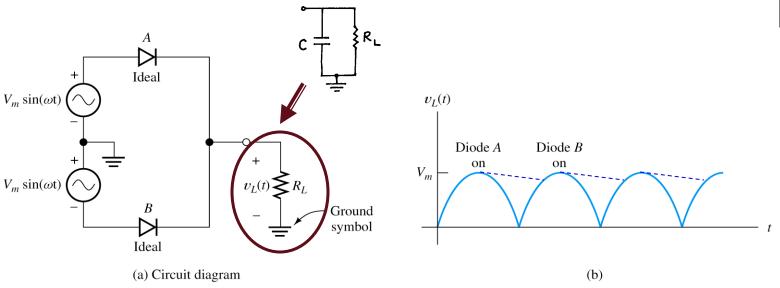


Figure 10.26 Half-wave rectifier with smoothing capacitor.



#### 10. Diodes – Rectifier Circuits

#### 10.6.2 Full-Wave Rectifier Circuits





- \* Center-Tapped Full-Wave Rectifier two half-wave rectifier with out-ofphase source voltages and a common ground.
- \* When upper source supplies "+" voltage to diode A, the lower source supplies "-" voltage to diode B; and vice versa.
- \* We can also smooth the output by using a large capacitance.



### 10. Diodes – Rectifier Circuits

### 10.6.2 Full-Wave Rectifier Circuits

\* The *Diode-Bridge Full-Wave Rectifier*.

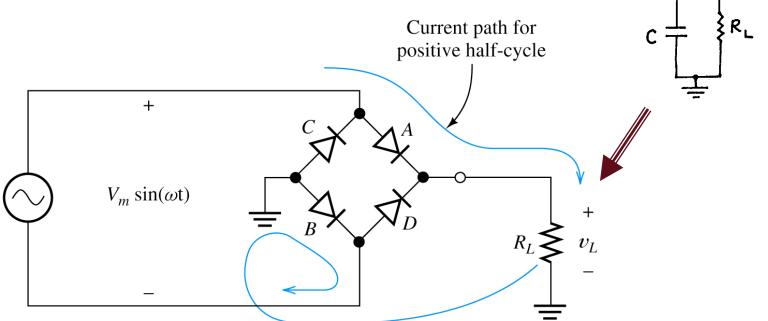
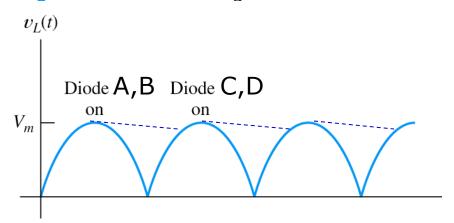


Figure 10.28 Diode-bridge full-wave rectifier.





## Clipping (Limiting) circuits



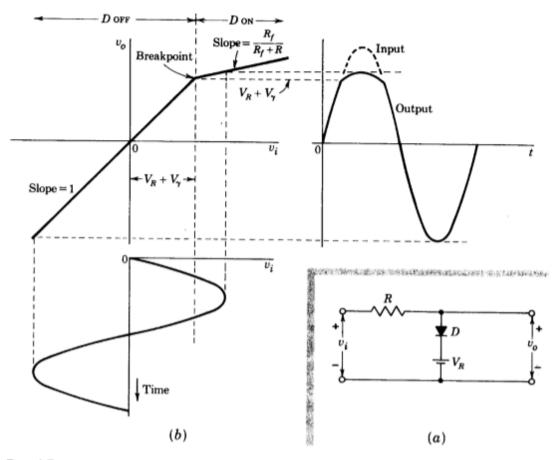


Fig. 4-7 (a) A diode clipping circuit which transmits that part of the waveform more negative than  $V_R + V_\gamma$ . (b) The piecewise linear transmission characteristic of the circuit. A sinusoidal input and the clipped output are shown.





Consider the circuit of Fig. 4-7a. Using the piecewise linear model, the transfer characteristic of Fig. 4-7b is obtained, as may easily be verified. For example, if D is off, the diode voltage  $v < V_{\gamma}$  and  $v_i < V_{\gamma} + V_R$ . How-

ever, if D is off, there is no current in R and  $v_o = v_i$ . This argument justifies the linear portion (with slope unity) of the transmission characteristic extending from arbitrary negative values to  $v_i = V_R + V_{\gamma}$ . For  $v_i$  larger than  $V_R + V_{\gamma}$ , the diode conducts, and it behaves as a battery  $V_{\gamma}$  in series with a resistance  $R_f$ , so that increments  $\Delta v_i$  in the input are attenuated and appear at the output as increments  $\Delta v_o = \Delta v_i R_f / (R_f + R)$ . This verifies the linear portion of slope  $R_f / (R_f + R)$  for  $v_i > V_R + V_{\gamma}$  in the transfer curve. Note that the transmission characteristic is piecewise linear and continuous and has a break point at  $V_R + V_{\gamma}$ .

Figure 4-7b shows a sinusoidal input signal of amplitude large enough so that the signal makes excursions past the break point. The corresponding output exhibits a suppression of the positive peak of the signal. If  $R_f \ll R$ , this suppression will be very pronounced, and the positive excursion of the output will be sharply limited at the voltage  $V_R + V_{\gamma}$ . The output will appear as though the positive peak had been "clipped off" or "sliced off."

## Clipping (Limiting) circuits



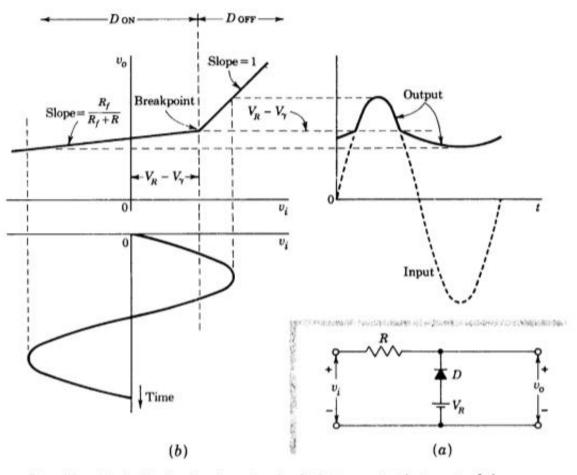


Fig. 4-8 (a) A diode clipping circuit which transmits that part of the waveform more positive than  $V_R-V_\gamma$ . (b) The piecewise linear transmission characteristic of the circuit. A sinusoidal input and the clipped output are shown.

## Clipping (Limiting) circuits



In Fig. 4-8a the clipping circuit has been modified in that the diode in Fig. 4-7a has been reversed. The corresponding piecewise linear representation of the transfer characteristic is shown in Fig. 4-8b. In this circuit, the portion of the waveform more positive than  $V_R - V_{\gamma}$  is transmitted without attenuation, but the less positive portion is greatly suppressed.

In Figs. 4-7b and 4-8b we have assumed  $R_r$  arbitrarily large in comparison with R. If this condition does not apply, the transmission characteristics must be modified. The portions of these curves which are indicated as having unity slope must instead be considered to have a slope  $R_r/(R_r + R)$ .

In a transmission region of a diode clipping circuit we require that  $R_r \gg R$ , for example, that  $R_r = kR$ , where k is a large number. In the attenuation region, we require that  $R \gg R_f$ , for example, that  $R = kR_f$ . From these two equations we deduce that  $R = \sqrt{R_f R_r}$  and that  $k = \sqrt{R_r/R_f}$ . On this basis we conclude that it is reasonable to select R as the geometrical mean of  $R_r$  and  $R_f$ . And we note that the ratio  $R_r/R_f$  may well serve as a figure of merit for diodes used in the present application.

## **Additional clipping circuits**



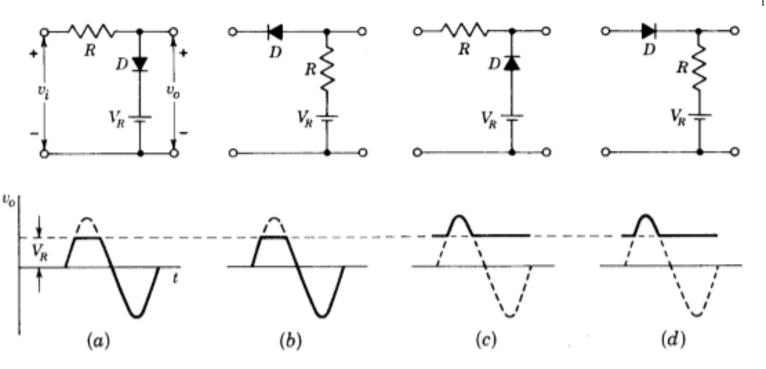


Fig. 4-9 Four diode clipping circuits. In (a) and (c) the diode appears as a shunt element. In (b) and (d) the diode appears as a series element. Under each circuit appears the output waveform (solid) for a sinusoidal input. The clipped portion of the input is shown dashed.

## **Clipping circuits**

$Input \ v_i$	$Output\ v_o$	$Diode\ states$
$v_i \leq V_{R1}$	$v_o = V_{R1}$	D1 on, $D2$ off
$V_{R1} < v_i < V_{R2}$	$v_o = v_i$	D1 off, $D2$ off
$v_i \geq V_{R2}$	$v_o = V_{R2}$	D1 off, $D2$ on

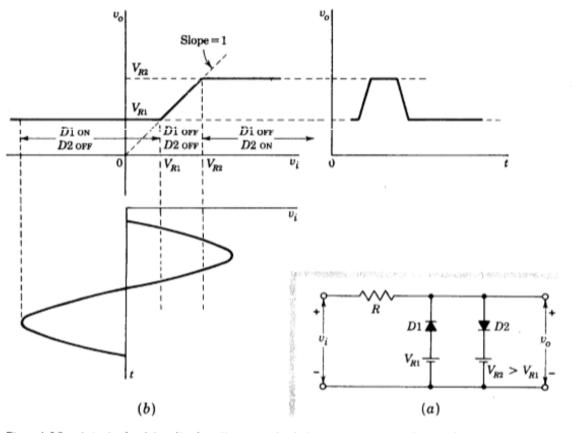


Fig. 4-10 (a) A double-diode clipper which limits at two independent levels. (b) The piecewise linear transfer curve for the circuit in (a). The doubly clipped output for a sinusoidal input is shown.



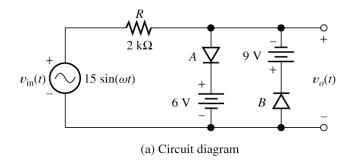
### 10. Diodes – Wave-Shaping Circuits

### 10.7 Wave-Shaping Circuits

### 10.7.1 Clipper Circuits

\* A portion of an input signal waveform is "clipped" off.





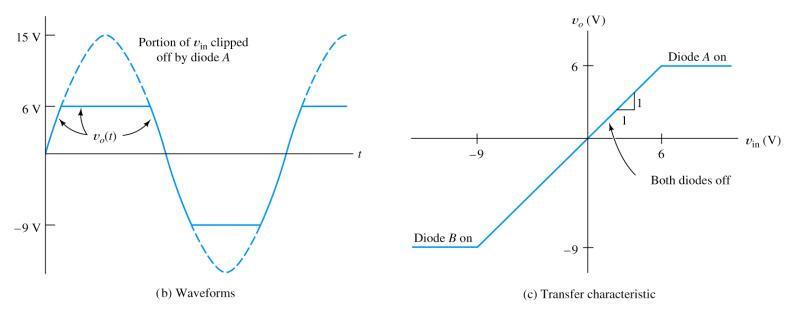


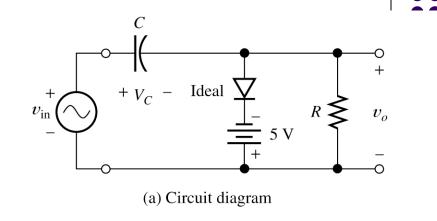
Figure 10.29 Clipper circuit.

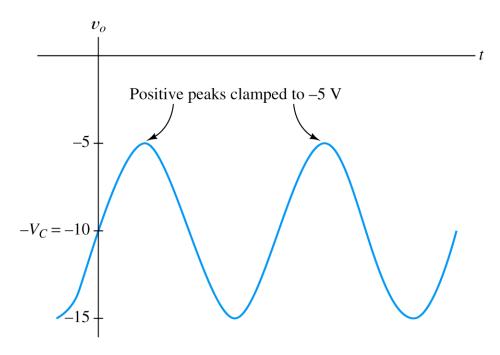
## 10. Diodes – Wave-Shaping Circuits

## 10.7 Wave-Shaping Circuits

## 10.7.2 Clamper Circuits

\* Clamp circuits are used to add a dc component to an ac input waveform so that the positive (or negative) peaks are "clamped" to a specified voltage value.





(b) Output waveform for  $v_{in} = 5 \sin(\omega t)$ 

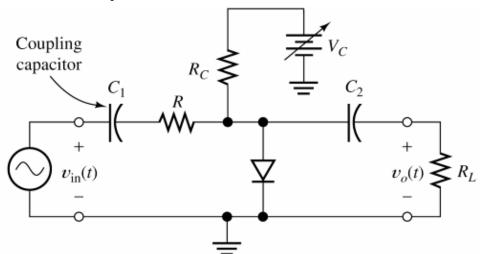
Figure 10.33 Example clamp circuit.

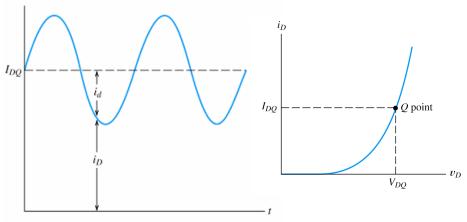
## 10. Diodes – Linear Small-Signal Equivalent Circuits

### 10.8 Linear Small-Signal Equivalent Circuits

\* In most of the electronic circuits, dc supply voltages are used to bias a nonlinear device at an operating point and a small signal is injected into the circuits.







- Figure 10.39 Illustration of diode currents.
- \* We often split the analysis of such circuit into two parts:
- (1) Analyze the dc circuit to find operating point,
- (2) Analyze the small signal (by using the "linear small-signal equivalent circuit".)

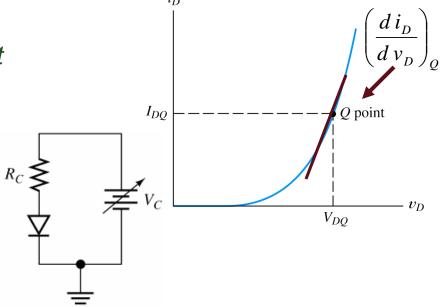
## 10. Diodes – Linear Small-Signal Equivalent Circuits

## 10.8 Linear Small-Signal Equivalent Circuits

- \* A diode in linear small-signal equivalent circuit is simplified to a resistor.
- \* We first determine the *operating point* (or the "*quiescent point*" or *Q point*) by dc bias.
- \* When small ac signal injects, it swings the Q point slightly up and down.
- \* If the signal is small enough, the characteristic is straight.

$$\Delta i_D \cong \left(\frac{d i_D}{d v_D}\right)_O \Delta v_D$$

 $\Delta i_D$  is the small change in diode current  $\Delta v_D$  is the small change in diode voltage



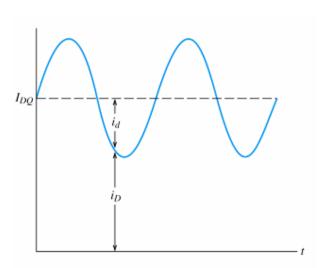


Figure 10.39 Illustration of diode currents.

## 10. Diodes - Linear Small-Signal Equivalent Circuits

## 10.8 Linear Small-Signal Equivalent Circuits

Define the dynamic resistance of the diode as:

$$r_d \cong \left[ \left( \frac{d i_D}{d v_D} \right)_O \right]^{-1}$$
 We will have:

$$\Delta i_D \cong \left(\frac{d i_D}{d v_D}\right)_O \Delta v_D \implies \Delta i_D \cong \frac{\Delta v_D}{r_d}$$

Replace  $\Delta i_D$  and  $\Delta v_D$  by  $i_d$  and  $v_d$  denoting small changes, we have for ac signals:

$$i_d = \frac{v_d}{r_d}$$

Furthermore, by applying the Shockley equation,

we have: 
$$r_d = \frac{nV_T}{I_{DQ}}$$

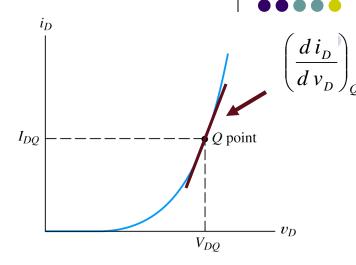


Figure 10.37 Diode characteristic, illustrating the Q point

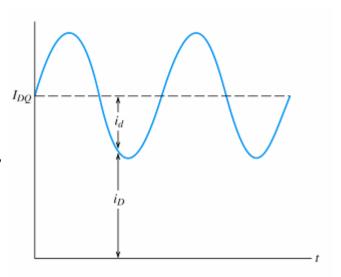


Figure 10.39 Illustration of diode currents.

## 10. Diodes – Linear Small-Signal Equivalent Circuits

## 10.8 Linear Small-Signal Equivalent Circuits

$$i_d = \frac{v_d}{r_d}, \quad r_d = \frac{nV_T}{I_{DQ}}$$

- \* By using these two equations, we can *treat* diode simply as a linear resistor in small ac signal analysis.
- \* Note: An ac voltage of fixed amplitude produces different ac current change at different Q point.

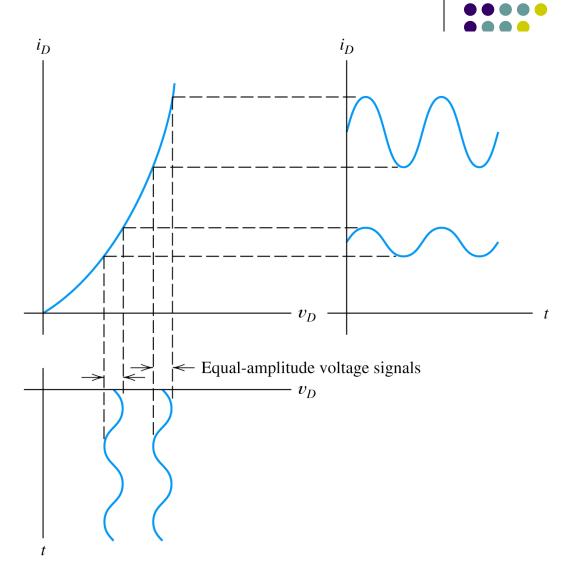
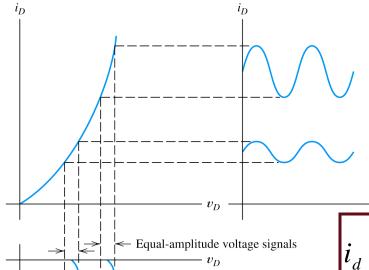


Figure 10.38 As the Q point moves higher, a fixed-amplitude ac voltage produces an ac current of larger amplitude.

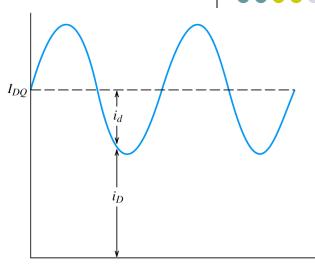
## 10. Diodes – Linear Small-Signal Equivalent Circuits 10.8 Linear Small-Signal Equivalent Circuits

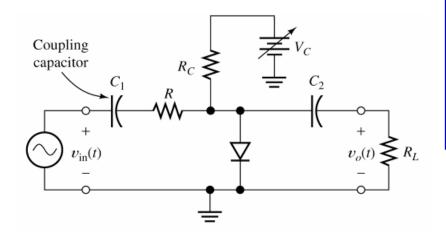




$$D_D = I_{DQ} + i_d$$
$$D_D = V_{DQ} + v_d$$

$$i_d = \frac{v_d}{r_d}, \quad r_d = \frac{nV_T}{I_{DQ}}$$

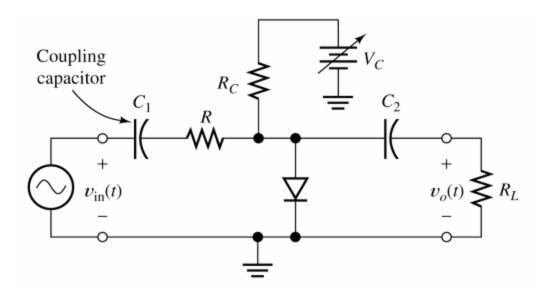




- $(1)V_{DQ}$  and  $I_{DQ}$  represent the dc signals at the Q point.
- (2)  $v_d$  and  $i_d$  represent the small sc signals.
- $(3) v_D$  and  $i_D$  represent the total instantaneous diode voltage and current.

## 10. Diodes – Linear Small-Signal Equivalent Circuits

## Voltage-Controlled Attenuator



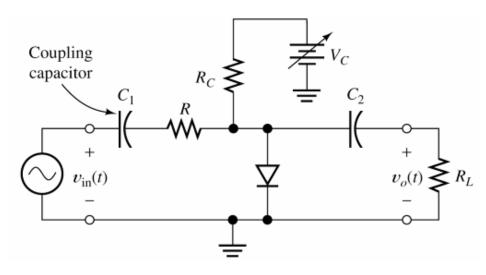


- \* The function of this circuit is to produce an output signal that is a variable fraction of the ac input signal.
- \* Two large *coupling capacitors*: behave like short circuit for ac signal and open circuit for dc, thus the Q point of the diode is unaffected by the ac input and the load.

$$Z_C = \frac{1}{j\omega C}$$

## 10. Diodes – Linear Small-Signal Equivalent Circuits

**Voltage-Controlled Attenuator** 



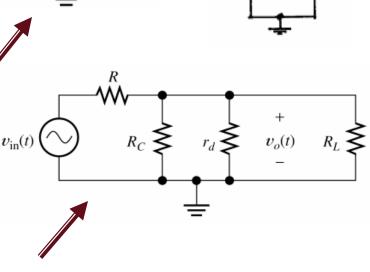
First apply dc analysis to find the diode Q point,

determine 
$$I_{DQ}$$
, then the  $r_d$  of the diode:  $r_d = \frac{nV_T}{I_{DQ}}$ 

Next, we perform small ac signal analysis:

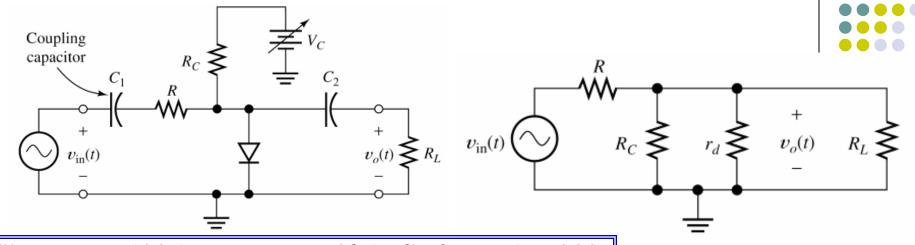
(note: the dc voltage source has an ac component of current but no ac voltage, the dc voltage source is equivalent to a short circuit for ac signal.)

$$R_p = \frac{1}{1/R_C + 1/R_L + 1/r_d}$$
, based on voltage divider:  $A_v = \frac{v_o}{v_{in}} = \frac{R_p}{R + R_o}$ 



## 10. Diodes - Linear Small-Signal Equivalent Circuits

## Exercise 10.20 - Voltage-Controlled Attenuator



Given:  $R = 100 \Omega$ ,  $R_C = R_L = 2k\Omega$ , diode n = 1 at 300K

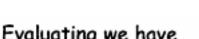
Find : the Q - point values assuming  $V_f = 0.6V$  and  $A_v$  for  $V_C = 1.6$  and 10.6V

First apply dc analysis to find the diode Q point,

$$I_{DQ} = \frac{V_C - 0.6}{R_C}, \quad r_d = \frac{nV_T}{I_{DO}} \quad with V_T = 0.026V$$

Next, we perform small ac signal analysis:

$$R_p = \frac{1}{1/R_C + 1/R_L + 1/r_d}, \quad A_v = \frac{v_o}{v_{in}} = \frac{R_p}{R + R_p}$$



Evaluating we have		
<i>V<sub>c</sub></i> (V)	1.6	10.6
$I_{DQ}$ (mA)	0.5	5.0
$r_d(\Omega)$	52	5.2
$R_p(\Omega)$	49.43	5.173
A <sub>v</sub>	0.3308	0.04919

# Thank you

