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Faculty of Engineering

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Titans

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Steam Cycle

Steam cycle is used in steam power plants to generate a mechanical power from thermal energy that's produced from combustion, mechanical power is used to generate electricity by transferring the mechanical power to generators.

Simple steam cycle efficiency is always expected to be in range of 30-40 %, so modifications are used to increase this efficiency.

In this report, many methods will be discussed in detail with plots and tables to justify everything.

Simple Rankine Cycle

Consists of A boiler, condenser, pump, and a turbine.

Modifications expected to be used: Reheating and adding feed water heaters.

Feed water heaters have 2 kinds: Open feed water heaters and Closed feed water heaters.

OFWHs are usually used to rid of gases so it designed on a certain pressure in which these gases exit.

Advantages of Steam power station

Lower cost in built than other ones, low cost of used fuel compared to that used in nuclear and gaseous stations and getting higher electric energy from the fuel used in steam power station than from the same fuel quantity used in other stations.

Disadvantages

Environmental pollution, low efficiency because of continues losses in different level of operations, needs high quantity of cooling water, transporting fuel is a problem, steam power station must be built far from population areas and exhaustion of fuel by continues usage.

A) Reheat Rankine Cycle

Code

{Givens}

```
P_b=150;  
P_c=.1;  
T_max=500;  
T_r=T_max  
"P_r=P_c";  
eta_t=0.85 ; eta_p=0.95;
```

{Solution}

```
"P1"  
h_1=ENTHALPY(Steam,X=0,P=P_c)  
s_1=ENTROPY(Steam,X=0,P=P_c)  
"P2"  
h_2s=ENTHALPY(Steam,s=s_1,P=P_b)  
(h_2a - h_1)*eta_p=(h_2s - h_1)  
"P3"  
h_3=ENTHALPY(Steam,T=T_max,P=P_b)  
s_3=ENTROPY(Steam,T=T_max,P=P_b)  
"P4"  
h_4s=ENTHALPY(Steam,s=s_3,P=P_r)  
(h_3 - h_4s)*eta_t=(h_3 - h_4a)  
"P5"  
h_5=ENTHALPY(Steam,T=T_r,P=P_r)  
s_5=ENTROPY(Steam,T=T_r,P=P_r)  
"P6"  
h_6s=ENTHALPY(Steam,s=s_5,P=P_c)  
(h_5 - h_6s)*eta_t=(h_5 - h_6a)
```

"Requirements"

```
W_t=(h_3 - h_4a)+(h_5 - h_6a); W_p=h_2a - h_1;  
W_net = W_t - W_p  
Q_add = (h_3 - h_2a)+(h_5 - h_4a)  
eta_th= W_net / Q_add
```

ES Variable Information

Show array variables Show string variables

| Variable | Guess | Lower | Upper | Display | Units |
|----------|-------|------------|------------|---------|-------|
| P_r | 1 | 1.0000E-01 | 1.5000E+02 | A 0 N | bar |

OK **Print** **Update** **Cancel**

Varying Reheat Pressure using Max/min Tab

Calculations Completed

23 equations in 11 blocks - 20 iterations

Elapsed time = .2 sec
eta_th = 0.3696

Continue

| Independent Variable | Value | Best value |
|----------------------|-------|------------|
| P_r | 30.51 | 30.51 |

Optimum Reheat Pressure that maximizes efficiency= 30.51 bar

Maximum efficiency = 36.96%

Results tab for the maximum efficiency

Unit Settings: [kJ/C][bar/kg]/[degrees]
Maximization of eta_th(P_r) 20 iterations: Quadratic Approximations method

| | | | | | | | | |
|------------------------------|------------------|--------------------|-------------------------------|----------------------------------|----------------------------------|------------------------------|------------------|----------------------------------|
| $T_b = 0.95$ | $T_h = 0.85$ | $T_{h_0} = 0.3696$ | $h_1 = 191.7 \text{ [kJ/kg]}$ | $h_{2a} = 207.6 \text{ [kJ/kg]}$ | $h_{2b} = 206.8 \text{ [kJ/kg]}$ | $h_3 = 3309 \text{ [kJ/kg]}$ | $h_{4a} = 2953$ | $h_{4b} = 2890 \text{ [kJ/kg]}$ |
| $h_g = 3456 \text{ [kJ/kg]}$ | $h_{g_0} = 2464$ | $T_{max} = 500$ | $h_{g_1} = 2289$ | $T_f = 500$ | $P_b = 150 \text{ [bar]}$ | $P_c = 0.1 \text{ [bar]}$ | $Q_{add} = 3605$ | $q_1 = 0.6489 \text{ [kJ/kg-K]}$ |
| $s_0 = 7.226$ | | | $W_{net} = 1332$ | | $W_p = 15.89$ | $W_t = 1348$ | | $q_3 = 6.345 \text{ [kJ/kg-K]}$ |

Calculation time = .2 sec

Calculations Completed

23 equations in 11 blocks - 24 iterations

Optimum Reheat Pressure that maximizes work net = 2.984 bar

Elapsed time = .1 sec

W_{net} = 1421

 Continue

| Independent Variable | Value | Best value |
|----------------------|-------|------------|
| P _r | 2.984 | 2.984 |

Maximum Work net = 1421 kJ/kg

Results tab for maximum Work net

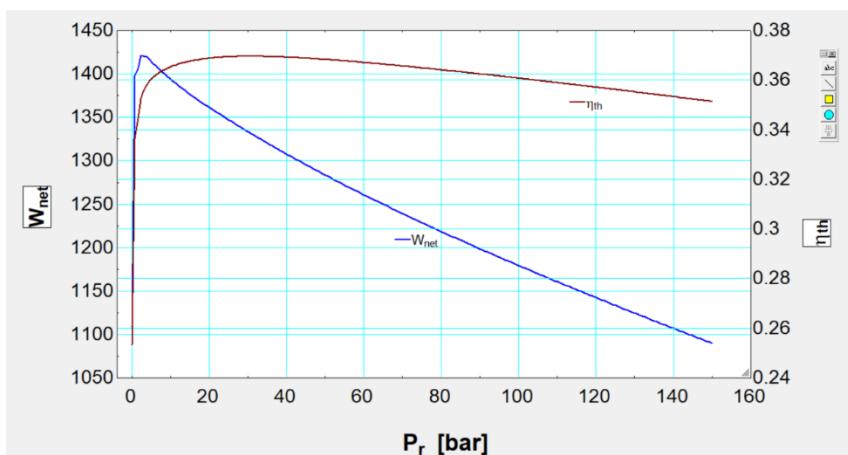
Unit Settings: [kJ][C]/[bar]/[kg]/[degrees]

Maximization of W_{net}(P_r) 24 iterations: Quadratic Approximations method

| | | | | | | | |
|------------------------------|-----------------|----------------------|-------------------------------|----------------------------------|------------------------------|----------------------------------|---------------------------------|
| $\eta_p = 0.95$ | $\eta_t = 0.85$ | $\eta_{lh} = 0.3553$ | $h_1 = 191.7 \text{ [kJ/kg]}$ | $h_{2s} = 207.6 \text{ [kJ/kg]}$ | $h_3 = 3309 \text{ [kJ/kg]}$ | $h_{4a} = 2588$ | $h_{4s} = 2461 \text{ [kJ/kg]}$ |
| $h_5 = 3486 \text{ [kJ/kg]}$ | $h_{6a} = 2770$ | $h_{6s} = 2644$ | $P_b = 150 \text{ [bar]}$ | $P_c = 0.1 \text{ [bar]}$ | $Q_{add} = 3999$ | $s_1 = 0.6489 \text{ [kJ/kg-K]}$ | $s_3 = 6.345 \text{ [kJ/kg-K]}$ |
| $s_5 = 0.328$ | $T_{max} = 500$ | $T_r = 500$ | $W_{net} = 1421$ | $W_p = 15.89$ | $W_f = 1437$ | | |

Calculation time = .1 sec

Reheat Pressure Plot against Work net and Efficiency



B) Varying P_b and getting Optimum P_r for each

Code

{Givens}

```
"P_b=120"  
P_c=.1;  
T_max=500;  
T_r=T_max  
"P_r=P_c";  
eta_t=0.85 ; eta_p=0.95;
```

{Solution}

```
"P1"  
h_1=ENTHALPY(Steam,X=0,P=P_c)  
s_1=ENTROPY(Steam,X=0,P=P_c)  
  
"P2"  
h_2s=ENTHALPY(Steam,s=s_1,P=P_b)  
(h_2a - h_1)*eta_p=(h_2s - h_1)  
  
"P3"  
h_3=ENTHALPY(Steam,T=T_max,P=P_b)  
s_3=ENTROPY(Steam,T=T_max,P=P_b)  
  
"P4"  
h_4s=ENTHALPY(Steam,s=s_3,P=P_r)  
(h_3 - h_4s)*eta_t=(h_3 - h_4a)
```

```
"P5"  
h_5=ENTHALPY(Steam,T=T_r,P=P_r)  
s_5=ENTROPY(Steam,T=T_r,P=P_r)
```

```
"P6"  
h_6s=ENTHALPY(Steam,s=s_5,P=P_c)  
(h_5 - h_6s)*eta_t=(h_5 - h_6a)
```

"Requirements"

```
W_t=(h_3 - h_4a)+(h_5 - h_6a); W_p=h_2a - h_1;  
W_net = W_t - W_p  
Q_add = (h_3 - h_2a)+(h_5 - h_4a)  
eta_th= W_net / Q_add  
R= P_r/P_b
```

Parametric tables for varying P_b

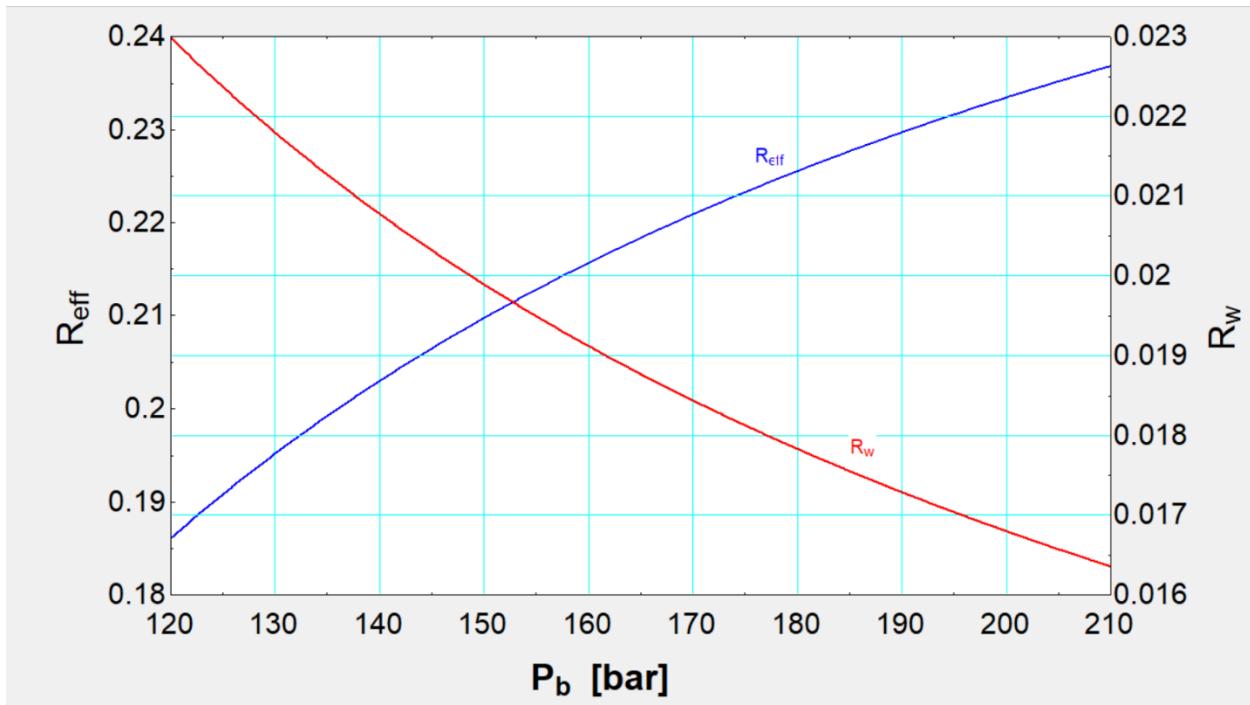
| 1 1..1000 | 2 P_r [bar] | 3 W_{net} | 4 P_b [bar] | 5 R |
|--------------|---------------------|----------------|---------------------|---------|
| Run 520 | 3.109 | 1425 | 166.8 | 0.01865 |
| Run 521 | 3.11 | 1425 | 166.8 | 0.01864 |
| Run 522 | 3.111 | 1425 | 166.9 | 0.01863 |
| Run 523 | 3.111 | 1425 | 167 | 0.01863 |
| Run 524 | 3.112 | 1425 | 167.1 | 0.01862 |
| Run 525 | 3.113 | 1425 | 167.2 | 0.01862 |
| Run 526 | 3.113 | 1425 | 167.3 | 0.01861 |
| Run 527 | 3.114 | 1425 | 167.4 | 0.0186 |
| Run 528 | 3.115 | 1425 | 167.5 | 0.0186 |
| Run 529 | 3.115 | 1425 | 167.6 | 0.01859 |
| Run 530 | 3.116 | 1425 | 167.7 | 0.01859 |
| Run 531 | 3.117 | 1425 | 167.7 | 0.01858 |
| Run 532 | 3.117 | 1425 | 167.8 | 0.01857 |
| Run 533 | 3.118 | 1425 | 167.9 | 0.01857 |
| Run 534 | 3.119 | 1425 | 168 | 0.01856 |
| Run 535 | 3.119 | 1425 | 168.1 | 0.01856 |
| Run 536 | 3.12 | 1425 | 168.2 | 0.01855 |
| Run 537 | 3.121 | 1425 | 168.3 | 0.01854 |
| Run 538 | 3.121 | 1425 | 168.4 | 0.01854 |
| Run 539 | 3.122 | 1425 | 168.5 | 0.01853 |
| Run 540 | 3.123 | 1425 | 168.6 | 0.01853 |
| Run 541 | 3.123 | 1425 | 168.6 | 0.01852 |
| Run 542 | 3.124 | 1425 | 168.7 | 0.01851 |
| Run 543 | 3.125 | 1425 | 168.8 | 0.01851 |
| Run 544 | 3.125 | 1425 | 168.9 | 0.0185 |
| Run 545 | 3.126 | 1425 | 169 | 0.0185 |
| Run 546 | 3.127 | 1425 | 169.1 | 0.01849 |
| Run 547 | 3.127 | 1425 | 169.2 | 0.01849 |
| Run 548 | 3.128 | 1425 | 169.3 | 0.01848 |
| Run 549 | 3.129 | 1425 | 169.4 | 0.01847 |
| Run 550 | 3.129 | 1425 | 169.5 | 0.01847 |

Varying P_b to get optimum P_r for max efficiency

| 1 1..1000 | 2 η_{th} | 3 P_r [bar] | 4 P_b [bar] | 5 R |
|--------------|------------------|---------------------|---------------------|--------|
| Run 368 | 0.37 | 32.4 | 153.1 | 0.2117 |
| Run 369 | 0.37 | 32.42 | 153.2 | 0.2117 |
| Run 370 | 0.37 | 32.45 | 153.2 | 0.2118 |
| Run 371 | 0.37 | 32.48 | 153.3 | 0.2118 |
| Run 372 | 0.37 | 32.51 | 153.4 | 0.2119 |
| Run 373 | 0.37 | 32.53 | 153.5 | 0.2119 |
| Run 374 | 0.37 | 32.56 | 153.6 | 0.212 |
| Run 375 | 0.37 | 32.59 | 153.7 | 0.212 |
| Run 376 | 0.3701 | 32.62 | 153.8 | 0.2121 |
| Run 377 | 0.3701 | 32.64 | 153.9 | 0.2121 |
| Run 378 | 0.3701 | 32.67 | 154 | 0.2122 |
| Run 379 | 0.3701 | 32.7 | 154.1 | 0.2122 |
| Run 380 | 0.3701 | 32.72 | 154.1 | 0.2123 |
| Run 381 | 0.3701 | 32.75 | 154.2 | 0.2124 |
| Run 382 | 0.3701 | 32.78 | 154.3 | 0.2124 |
| Run 383 | 0.3701 | 32.81 | 154.4 | 0.2125 |
| Run 384 | 0.3702 | 32.83 | 154.5 | 0.2125 |
| Run 385 | 0.3702 | 32.86 | 154.6 | 0.2126 |
| Run 386 | 0.3702 | 32.89 | 154.7 | 0.2126 |
| Run 387 | 0.3702 | 32.92 | 154.8 | 0.2127 |
| Run 388 | 0.3702 | 32.94 | 154.9 | 0.2127 |
| Run 389 | 0.3702 | 32.97 | 155 | 0.2128 |
| Run 390 | 0.3702 | 33 | 155 | 0.2128 |
| Run 391 | 0.3702 | 33.03 | 155.1 | 0.2129 |
| Run 392 | 0.3702 | 33.05 | 155.2 | 0.2129 |
| Run 393 | 0.3703 | 33.08 | 155.3 | 0.213 |
| Run 394 | 0.3703 | 33.11 | 155.4 | 0.213 |
| Run 395 | 0.3703 | 33.14 | 155.5 | 0.2131 |
| Run 396 | 0.3703 | 33.16 | 155.6 | 0.2132 |
| Run 397 | 0.3703 | 33.19 | 155.7 | 0.2132 |
| Run 398 | 0.3703 | 33.22 | 155.8 | 0.2133 |

Varying P_b to get optimum P_r for max work net

Plotting P_b against Pressure ratio for both efficiency and work net



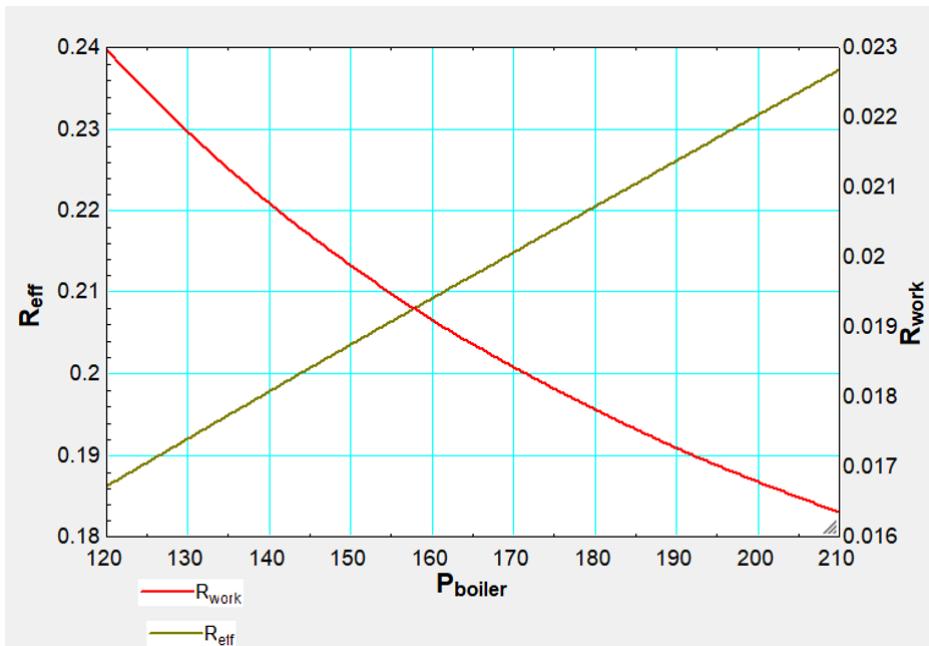
Note: method of using parametric tables has percentage of error as we assumed that the relation between the change of P_b and the change of P_r is linear.

Another method “Manually”

| | 1..10 | P _{boiler} | P _{reheat1} | R _{eff} | P _{reheat2} | R _{work} |
|--------|-------|---------------------|----------------------|------------------|----------------------|-------------------|
| Run 1 | | 120 | 22.34 | 0.1862 | 2.756 | 0.02297 |
| Run 2 | | 130 | 24.96 | 0.192 | 2.833 | 0.02179 |
| Run 3 | | 140 | 27.69 | 0.1978 | 2.908 | 0.02077 |
| Run 4 | | 150 | 30.53 | 0.2035 | 2.983 | 0.01989 |
| Run 5 | | 160 | 33.47 | 0.2092 | 3.057 | 0.01911 |
| Run 6 | | 170 | 36.53 | 0.2149 | 3.132 | 0.01842 |
| Run 7 | | 180 | 39.69 | 0.2205 | 3.207 | 0.01782 |
| Run 8 | | 190 | 42.96 | 0.2261 | 3.281 | 0.01727 |
| Run 9 | | 200 | 46.34 | 0.2317 | 3.357 | 0.01679 |
| Run 10 | | 210 | 49.82 | 0.2372 | 3.433 | 0.01635 |

Here we've calculated optimum P_r at each P_b

Plotting P_b against the pressure ratio for each efficiency and work net



(C) Using the reheat pressure that maximized the efficiency in (1),

Varying the pressure of the OPWH from the P_c to the P_b to construct the maximum efficiency

1-Taking the pressure from the high-pressure turbine:

code

{Givens}

$P_b=150$

$P_c=0.1$

$T_{max}=500$

$\eta_t=0.85$

$\eta_p=0.95$

$P_r=30.51$

" $P_{ofwh}=0$ "

{Point 1}

$h_1=\text{Enthalpy(Steam},x=0,P=P_c)$

$s_1=\text{Entropy(Steam},x=0,P=P_c)$

{Point 2}

$s_2=s_1$

$h_{2s}=\text{Enthalpy(Steam},s=s_2,p=P_{ofwh})$

$(h_{2s}-h_1)*\eta_p=(h_{2s}-h_1)$

{Point 3}

$h_3=\text{Enthalpy(Steam},x=0,P=P_{ofwh})$

s_3=Entropy(Steam,x=0,P=P_ofwh)

{Point 4}

s_4=s_3

h_4s=Enthalpy(Steam,s=s_4,p=P_b)

(h_4-h_3)*eta_p=(h_4s-h_3)

{Point 5}

h_5=Enthalpy(Steam,p=P_b,T=T_max)

s_5=Entropy(Steam,p=P_b,T=T_max)

{Point 6}

s_6=s_5

h_6s=Enthalpy(Steam,s=s_6,p=P_ofwh)

eta_t=(h_5-h_6)/(h_5-h_6s)

{Point 7}

s_7=s_5

h_7s=Enthalpy(Steam,s=s_7,p=P_r)

eta_t=(h_5-h_7)/(h_5-h_7s)

{Point 8}

h_8=Enthalpy(Steam,p=P_r,t=T_max)

s_8=Entropy(Steam,p=P_r,t=T_max)

{Point 9}

$$s_9 = s_8$$

$$h_{9s} = \text{Enthalpy(Steam}, s=s_9, p=P_c)$$

$$\eta_t = (h_8 - h_9) / (h_8 - h_{9s})$$

{HB on ofwh}

$$m = (h_3 - h_2) / (h_6 - h_2)$$

{Calculations}

$$w_t = (h_5 - h_6) + (h_6 - h_7) * (1-m) + (h_8 - h_9) * (1-m)$$

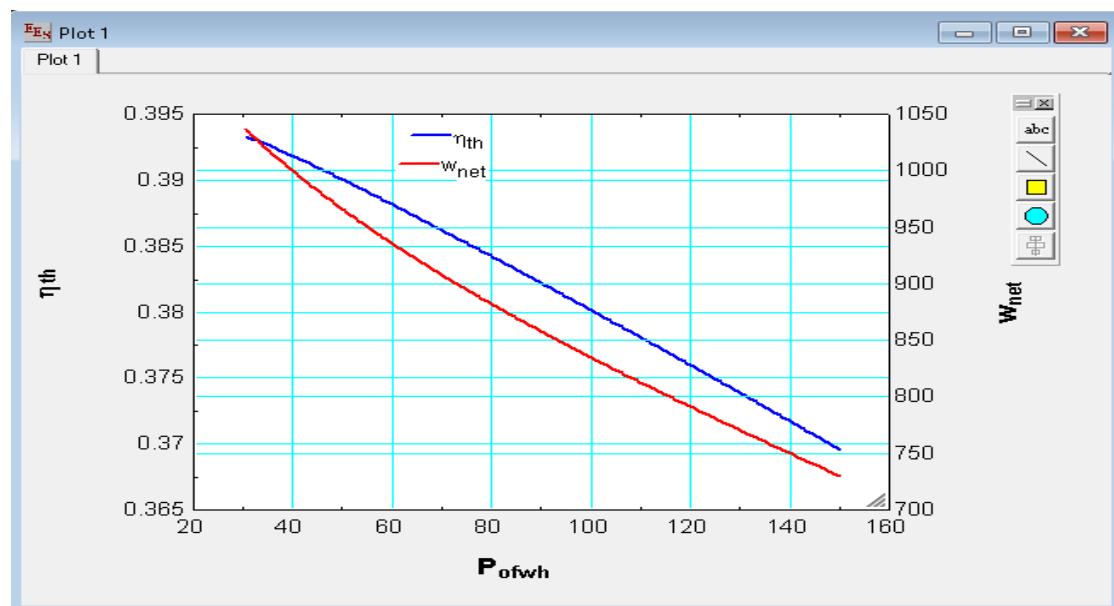
$$w_p = (h_2 - h_1) * (1-m) + (h_4 - h_3)$$

$$w_{net} = w_t - w_p$$

$$q_{add} = h_5 - h_4 + (h_8 - h_7) * (1-m)$$

$$\eta_{th} = w_{net} / q_{add}$$

The OFWH pressure (varies from P_c to P_b) against the thermal efficiency and the net work



The OFWH pressure that maximized work net

Calculations Completed

35 equations in 16 blocks - 37 iterations

Elapsed time = 1.9 sec

w_net = 1037



| Independent Variable | Value | Best value |
|----------------------|-------|------------|
| P_ofwh | 30.51 | 30.51 |

The OFWH pressure that maximized the thermal efficiency

Calculations Completed

35 equations in 16 blocks - 37 iterations

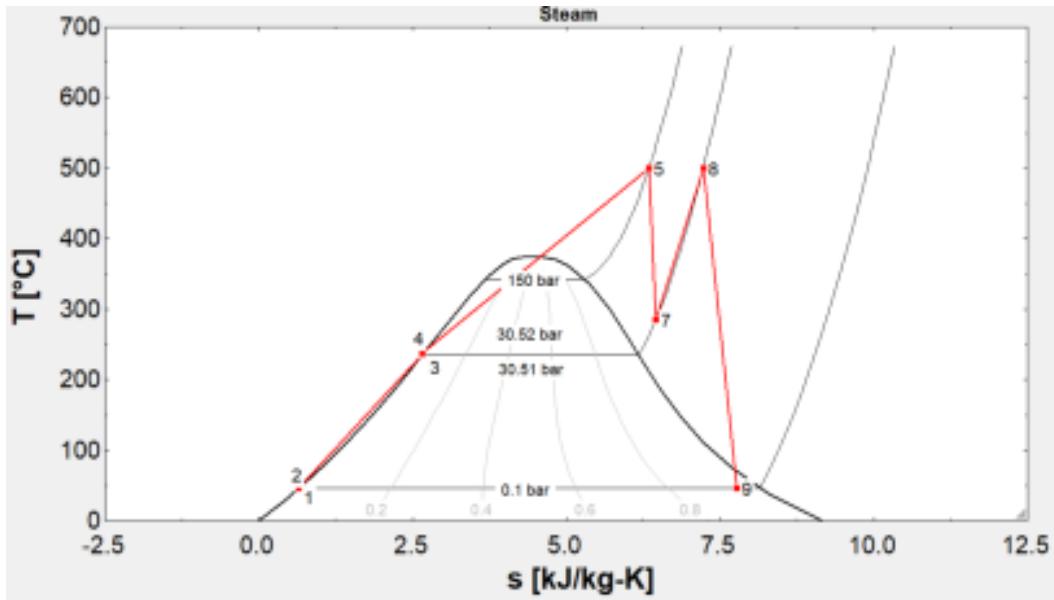
Elapsed time = 1.7 sec

eta_th = 0.3933

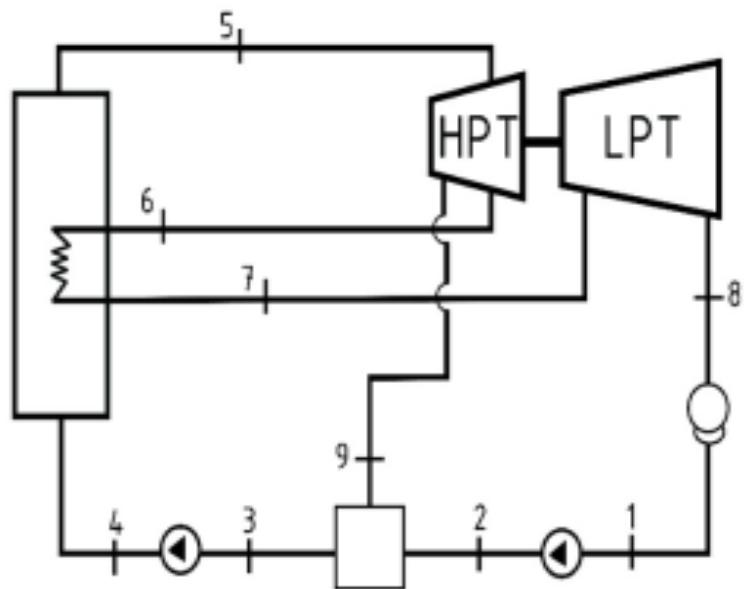


| Independent Variable | Value | Best value |
|----------------------|-------|------------|
| P_ofwh | 30.51 | 30.51 |

T-s diagram



Flow diagram for this case



Note: After connecting the open feed water heater intake to the high pressure turbine and set the limits from boiler and reheat pressure we deduce that that $P_{ofwh}=P_r$ (it's not important to try the cases of connecting the open feed water heater into the reheat pressure).

2- Taking the pressure from the low pressure turbine:

code

{Givens}

P_b=150

P_c=0.1

T_max=500

eta_t=0.85

eta_p=0.95

P_r=30.51

"P_ofwh=0"

{Point 1}

h_1=Enthalpy(Steam,x=0,P=P_c)

s_1=Entropy(Steam,x=0,P=P_c)

{Point 2}

s_2=s_1

h_2s=Enthalpy(Steam,s=s_2,p=P_ofwh)

(h_2s-h_1)*eta_p=(h_2s-h_1)

{Point 3}

h_3=Enthalpy(Steam,x=0,P=P_ofwh)

s_3=Entropy(Steam,x=0,P=P_ofwh)

{Point 4}

s_4=s_3

h_4s=Enthalpy(Steam,s=s_4,p=P_b)

(h_4-h_3)*eta_p=(h_4s-h_3)

{Point 5}

h_5=Enthalpy(Steam,p=P_b,T=T_max)

s_5=Entropy(Steam,p=P_b,T=T_max)

{Point 6}

s_6s=s_8

h_6s=Enthalpy(Steam,s=s_6s,p=P_ofwh)

(h_8-h_6)=(h_8-h_6s)*eta_t

s_6=Entropy(Steam,h=h_6,p=P_ofwh)

{Point 7}

s_7=s_5

h_7s=Enthalpy(Steam,s=s_7,p=P_r)

eta_t=(h_5-h_7)/(h_5-h_7s)

{Point 8}

h_8=Enthalpy(Steam,p=P_r,t=T_max)

s_8=Entropy(Steam,p=P_r,t=T_max)

{Point 9}

$$s_9 = s_6$$

$$h_{9s} = \text{Enthalpy(Steam, } s=s_9, p=P_c)$$

$$\eta_t * (h_6 - h_{9s}) = (h_6 - h_9)$$

{HB on ofwh}

$$m = (h_3 - h_2) / (h_6 - h_2)$$

{Calculations}

$$w_t = (h_5 - h_7) + (h_8 - h_6) + (h_6 - h_9) * (1 - m)$$

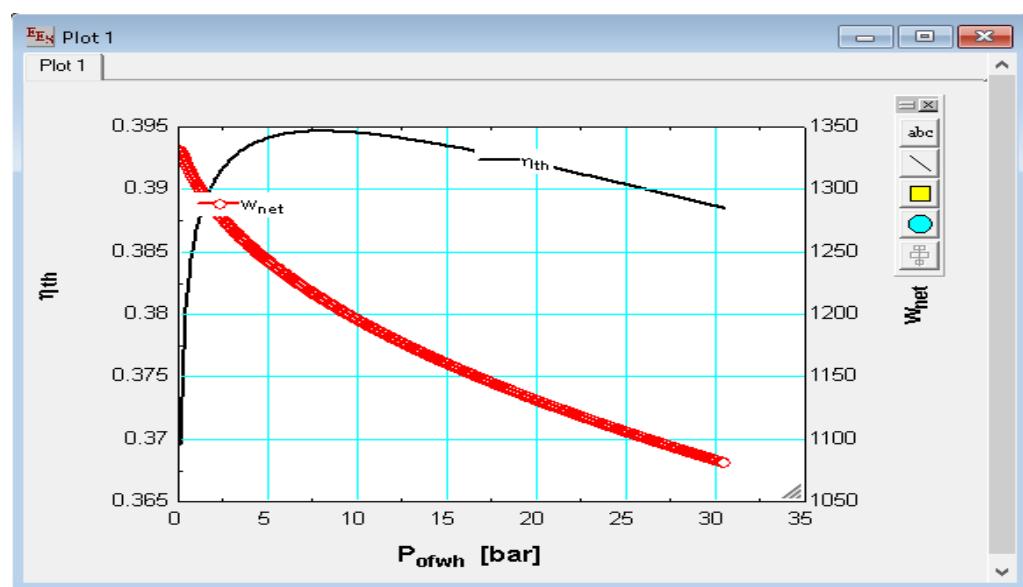
$$w_p = (h_2 - h_1) * (1 - m) + (h_4 - h_3)$$

$$w_{net} = w_t - w_p$$

$$q_{add} = h_5 - h_4 + h_8 - h_7$$

$$\eta_{th} = w_{net} / q_{add}$$

The open feed water pressure (varies from P_c to P_r) against the thermal efficiency and the net work



The open feed water pressure that maximizes the efficiency

Calculations Completed

35 equations in 16 blocks - 37 iterations

Elapsed time = 1.7 sec

eta_th = 0.3933

 Continue

| Independent Variable | Value | Best value |
|----------------------|-------|------------|
| P_ofwh | 30.51 | 30.51 |

The open feed water pressure that maximizes the work net

Calculations Completed

36 equations in 20 blocks - 28 iterations

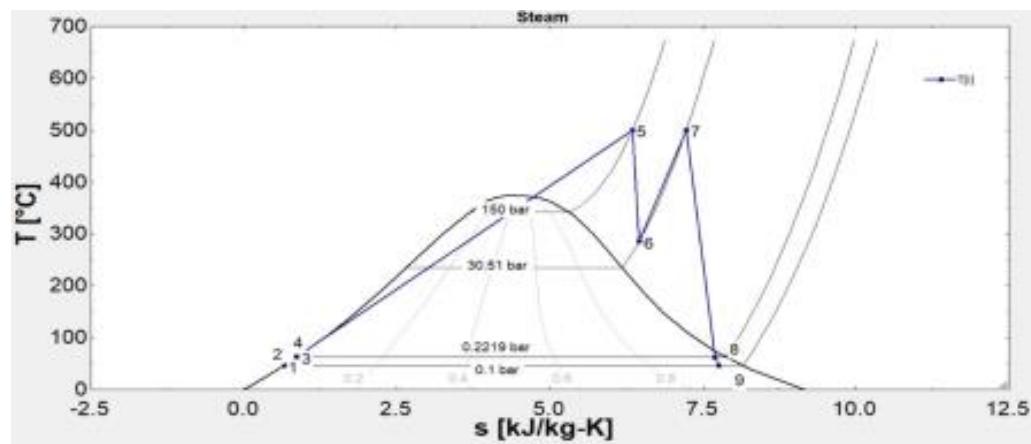
Elapsed time = 1.6 sec

w_net = 1336

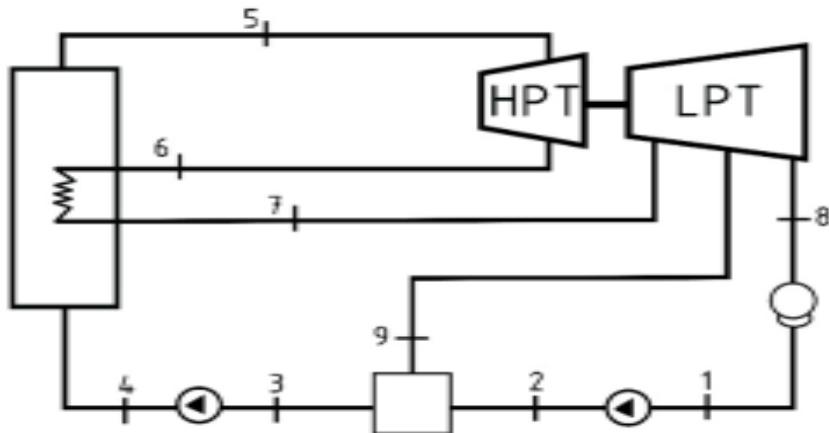
 Continue

| Independent Variable | Value | Best value |
|----------------------|--------|------------|
| P_ofwh | 0.2219 | 0.2219 |

T-s diagram



Flow diagram for this case:



3-Taking the pressure from the upper reheat line

Code

{Givens}

$$P_b = 150$$

$$P_c = 0.1$$

$$T_{max} = 500$$

$$\eta_t = 0.85$$

$$\eta_p = 0.95$$

$$P_r = 30.51$$

$$P_{ofwh} = P_r$$

{Point 1}

$$h_1 = \text{Enthalpy(Steam, } x=0, P=P_c)$$

$$s_1 = \text{Entropy(Steam, } x=0, P=P_c)$$

{Point 2}

s_2=s_1

h_2s=Enthalpy(Steam,s=s_2,p=P_ofwh)

(h_2-h_1)*eta_p=(h_2s-h_1)

{Point 3}

h_3=Enthalpy(Steam,x=0,P=P_ofwh)

s_3=Entropy(Steam,x=0,P=P_ofwh)

{Point 4}

s_4=s_3

h_4s=Enthalpy(Steam,s=s_4,p=P_b)

(h_4-h_3)*eta_p=(h_4s-h_3)

{Point 5}

h_5=Enthalpy(Steam,p=P_b,T=T_max)

s_5=Entropy(Steam,p=P_b,T=T_max)

{Point 6}

s_6=s_5

h_6s=Enthalpy(Steam,s=s_6,p=P_ofwh)

eta_t=(h_5-h_6)/(h_5-h_6s)

{Point 7}

h_7=Enthalpy(Steam,p=P_r,t=T_max)

$s_7 = \text{Entropy}(\text{Steam}, p=P_r, t=T_{\max})$

{Point 8}

$s_7 = s_8$

$h_{8s} = \text{Enthalpy}(\text{Steam}, s=s_8, p=P_c)$

$\eta_{\text{t}} = (h_7 - h_{8s}) / (h_7 - h_2)$

{HB on ofwh}

$m = (h_3 - h_2) / (h_6 - h_2)$

{Calculations}

$w_t = (h_5 - h_6) + (h_7 - h_8) * (1 - m)$

$w_p = (h_2 - h_1) * (1 - m) + (h_4 - h_3)$

$w_{\text{net}} = w_t - w_p$

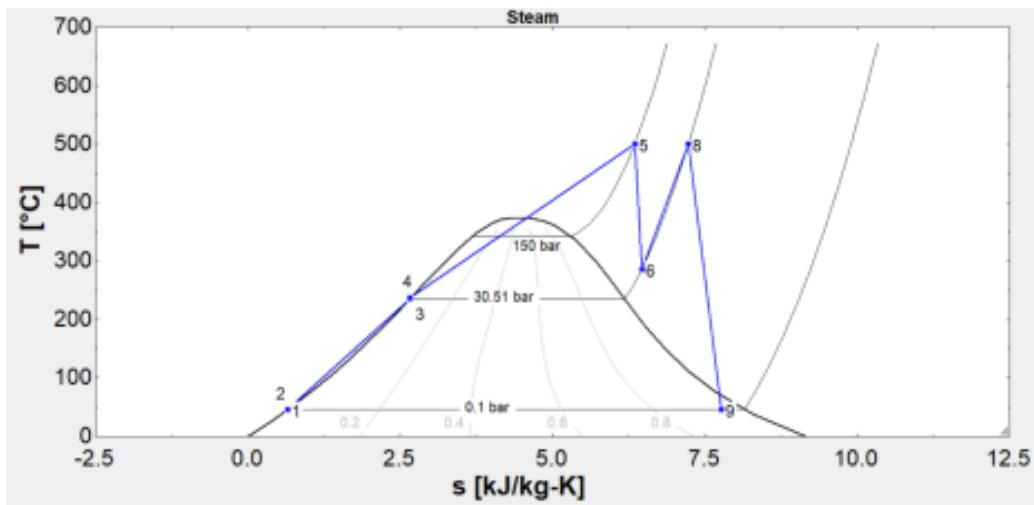
$q_{\text{add}} = h_5 - h_4 + (h_7 - h_6) * (1 - m)$

$\eta_{\text{th}} = w_{\text{net}} / q_{\text{add}}$

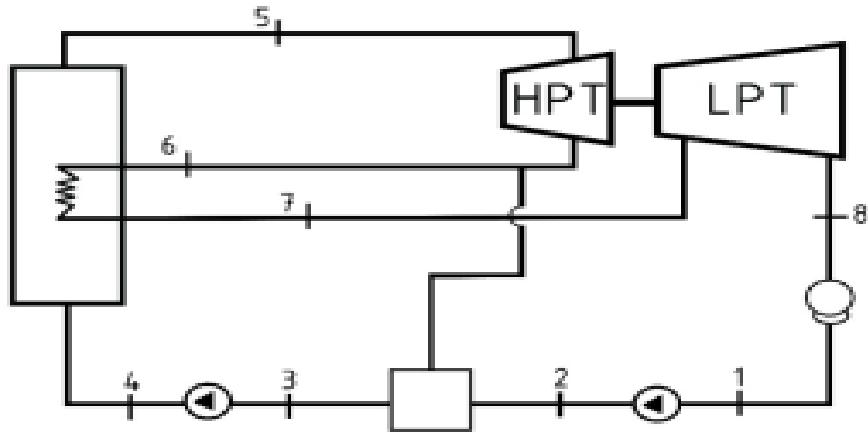
Results Tab

| Unit Settings: [kJ]/[C]/[bar]/[kg]/[degrees] | | | | | |
|--|----------------------------------|---------------------------------|---------------------------------|---------------------------------|----------------------------------|
| $\eta_p = 0.95$ | $\eta_t = 0.85$ | $\eta_{\text{lb}} = 0.3933$ | $h_1 = 191.7 \text{ [kJ/kg]}$ | $h_2 = 195$ | $h_{2s} = 194.8 \text{ [kJ/kg]}$ |
| $h_4 = 1028$ | $h_{4s} = 1027 \text{ [kJ/kg]}$ | $h_5 = 3309 \text{ [kJ/kg]}$ | $h_6 = 2953$ | $h_{6s} = 2890 \text{ [kJ/kg]}$ | $h_3 = 1013 \text{ [kJ/kg]}$ |
| $h_{8s} = 2289 \text{ [kJ/kg]}$ | $m = 0.2965$ | $P_b = 150$ | $P_c = 0.1$ | $P_{\text{ofwh}} = 30.51$ | $h_7 = 3456 \text{ [kJ/kg]}$ |
| $s_1 = 0.6489 \text{ [kJ/kg-K]}$ | $s_2 = 0.6489 \text{ [kJ/kg-K]}$ | $s_3 = 2.654 \text{ [kJ/kg-K]}$ | $s_4 = 2.654 \text{ [kJ/kg-K]}$ | $s_5 = 6.345 \text{ [kJ/kg-K]}$ | $h_8 = 2464$ |
| $s_6 = 7.226$ | $T_{\max} = 500$ | $w_{\text{net}} = 1037$ | $w_p = 17.53$ | $w_t = 1054$ | $q_{\text{add}} = 2635$ |
| Calculation time = .0 sec | | | | | |

T-s diagram



Flow diagram



4-Taking the pressure from the lower reheat line:

code

{Givens}

$P_b=150$

$P_c=0.1$

$T_{max}=500$

$\eta_t=0.85$

$\eta_p=0.95$

P_r=30.51

P_ofwh=P_r

{Point 1}

h_1=Enthalpy(Steam,x=0,P=P_c)

s_1=Entropy(Steam,x=0,P=P_c)

{Point 2}

s_2=s_1

h_2s=Enthalpy(Steam,s=s_2,p=P_ofwh)

(h_2-h_1)*eta_p=(h_2s-h_1)

{Point 3}

h_3=Enthalpy(Steam,x=0,P=P_ofwh)

s_3=Entropy(Steam,x=0,P=P_ofwh)

{Point 4}

s_4=s_3

h_4s=Enthalpy(Steam,s=s_4,p=P_b)

(h_4-h_3)*eta_p=(h_4s-h_3)

{Point 5}

h_5=Enthalpy(Steam,p=P_b,T=T_max)

s_5=Entropy(Steam,p=P_b,T=T_max)

{Point 6}

s_6=s_5

h_6s=Enthalpy(Steam,s=s_6,p=P_ofwh)

eta_t=(h_5-h_6)/(h_5-h_6s)

{Point 7}

h_7=Enthalpy(Steam,p=P_r,t=T_max)

s_7=Entropy(Steam,p=P_r,t=T_max)

{Point 8}

s_7=s_8

h_8s=Enthalpy(Steam,s=s_8,p=P_c)

eta_t=(h_7-h_8)/(h_7-h_8s)

{HB on ofwh}

m=(h_3-h_2)/(h_7-h_2)

{Calculations}

w_t=(h_5-h_6)+(h_7-h_8)*(1-m)

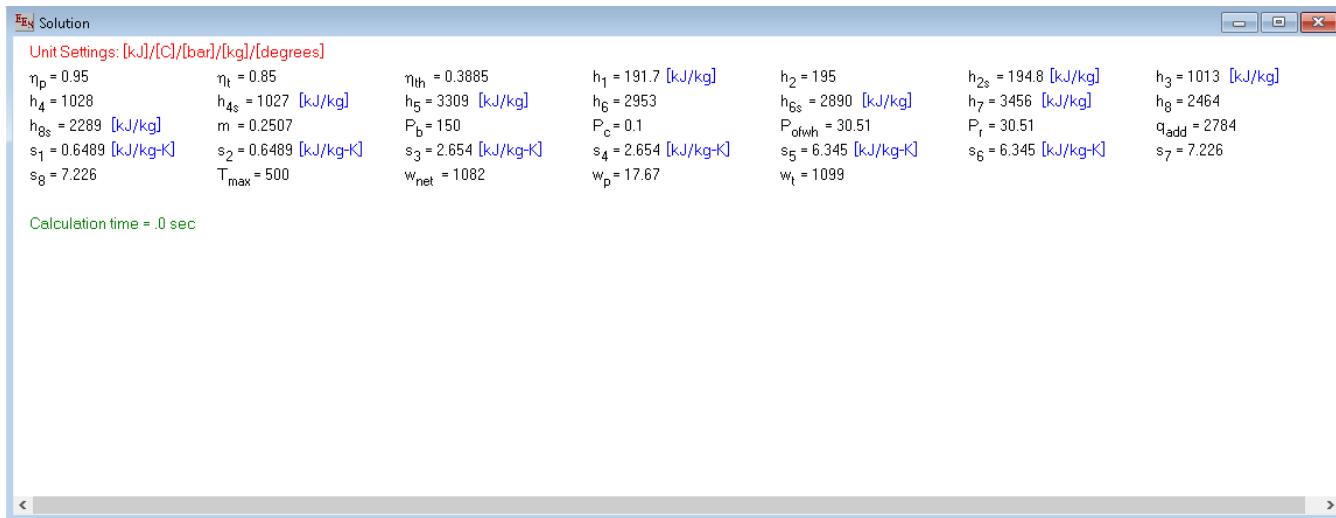
w_p=(h_2-h_1)*(1-m) + (h_4-h_3)

w_net=w_t-w_p

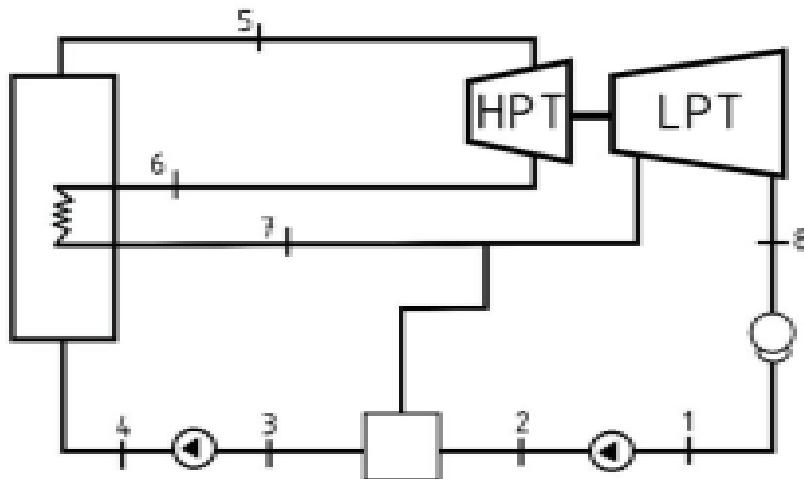
q_add=h_5-h_4+(h_7-h_6)

eta_th=w_net/q_add

Results Tab



Flow diagram



From 1,2,3,4 we deduce that the maximum efficiency can be extracted when we intake the pressure to the open feed water from **the low pressure turbine**.

-Maximum efficiency=0.4013 at $P_{ofwh}=5.913$

-Maximum work net=1336 at $P_{ofwh}=0.2219$

(D) Adding feed water heaters to modify the cycle

D.1

"From low LP Turbine"

{Givens}

P_b=150

P_c=0.1

T_max=500

eta_t=0.85

eta_p=0.95

P_r=30.51

"P_ofwh=0"

{Point 1}

h_1=Enthalpy(Steam,x=0,P=P_c)

s_1=Entropy(Steam,x=0,P=P_c)

{Point 2}

s_2=s_1

h_2s=Enthalpy(Steam,s=s_2,p=P_ofwh)

(h_2s-h_1)*eta_p=(h_2s-h_1)

{Point 3}

h_3=Enthalpy(Steam,x=0,P=P_ofwh)

s_3=Entropy(Steam,x=0,P=P_ofwh)

{Point 4}

$$s_4=s_3$$

$h_{4s}=\text{Enthalpy(Steam}, s=s_4, p=P_b)$

$$(h_4-h_3)*\eta_p=(h_{4s}-h_3)$$

{Point 5}

$h_5=\text{Enthalpy(Steam}, p=P_b, T=T_{max})$

$s_5=\text{Entropy(Steam}, p=P_b, T=T_{max})$

{Point 6}

$$s_6=s_8$$

$h_{6s}=\text{Enthalpy(Steam}, s=s_6, p=P_{ofwh})$

$$(h_8-h_6)=(h_8-h_{6s})*\eta_t$$

$s_6=\text{Entropy(Steam}, h=h_6, p=P_{ofwh})$

{Point 7}

$$s_7=s_5$$

$h_{7s}=\text{Enthalpy(Steam}, s=s_7, p=P_r)$

$$\eta_t=(h_5-h_7)/(h_5-h_{7s})$$

{Point 8}

$h_8=\text{Enthalpy(Steam}, p=P_r, t=T_{max})$

$s_8=\text{Entropy(Steam}, p=P_r, t=T_{max})$

{Point 9}

s_9=s_6

h_9s=Enthalpy(Steam,s=s_9,p=P_c)

eta_t*(h_6-h_9s)=(h_6-h_9)

{HB on ofwh}

m=(h_3-h_2)/(h_6-h_2)

{Calculations}

w_t=(h_5-h_7)+(h_8-h_6)+(h_6-h_9)*(1-m)

w_p=(h_2-h_1)*(1-m) + (h_4-h_3)

w_net=w_t-w_p

q_add=h_5-h_4+h_8-h_7

eta_th=w_net/q_add

Calculations

Calculations Completed

36 equations in 20 blocks - 19 iterations

Elapsed time = 1.1 sec

eta_th = 0.4013



| Independent Variable | Value | Best value |
|----------------------|-------|------------|
| P_ofwh | 5.913 | 5.913 |

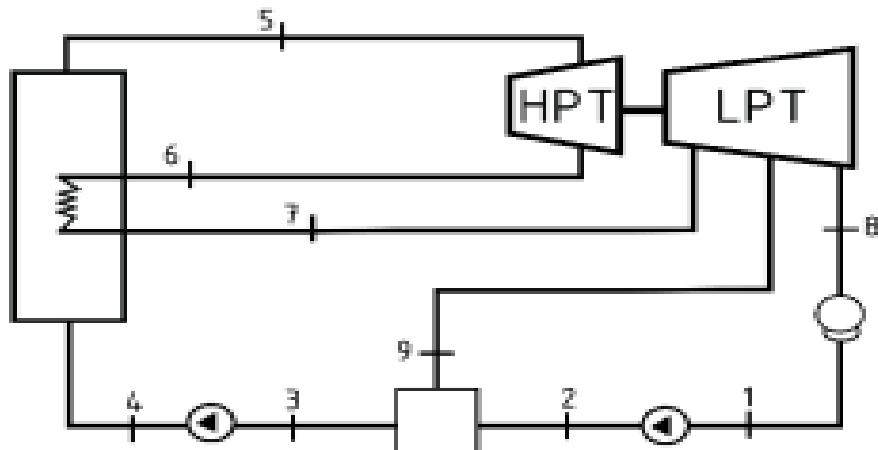
Optimum OFWH Pressure = 5.913 bar

Maximum efficiency = 40.13%

Results Tab

| EES Solution | | | | | | |
|--|------------------|----------------------------------|----------------------------------|-----------------|------------------|----------------------------------|
| Unit Settings: [kJ]/[C]/[bar]/[kg]/[degrees] | | | | | | |
| Maximization of $\eta_{th}(P_{ofwh}, P_r)$ 95 iterations: Variable Metric method | | | | | | |
| $\eta_p = 0.95$ | $\eta_t = 0.85$ | $\eta_{th} = 0.4013$ | $h_1 = 191.7 \text{ [kJ/kg]}$ | $h_2 = 192.3$ | $h_{2s} = 192.3$ | $h_3 = 671.3$ |
| $h_4 = 687.9$ | $h_{4s} = 687.1$ | $h_5 = 3309 \text{ [kJ/kg]}$ | $h_6 = 3053$ | $h_{6s} = 2981$ | $h_7 = 2953$ | $h_{7s} = 2890$ |
| $h_g = 3456$ | $h_g = 2439$ | $h_{9s} = 2330$ | $m = 0.1675$ | $P_b = 150$ | $P_c = 0.1$ | $P_{ofwh} = 6.024 \text{ [bar]}$ |
| $P_r = 30.51$ | $q_{add} = 3124$ | $s_1 = 0.6489 \text{ [kJ/kg-K]}$ | $s_2 = 0.6489 \text{ [kJ/kg-K]}$ | $s_3 = 1.933$ | $s_4 = 1.933$ | $s_5 = 6.345 \text{ [kJ/kg-K]}$ |
| $s_p = 7.355$ | $s_{6s} = 7.226$ | $s_7 = 6.345 \text{ [kJ/kg-K]}$ | $s_8 = 7.226$ | $s_9 = 7.355$ | $T_{max} = 500$ | $w_{net} = 1254$ |
| $w_t = 17.14$ | $w_t = 1271$ | | | | | |
| Calculation time = 6.9 sec | | | | | | |

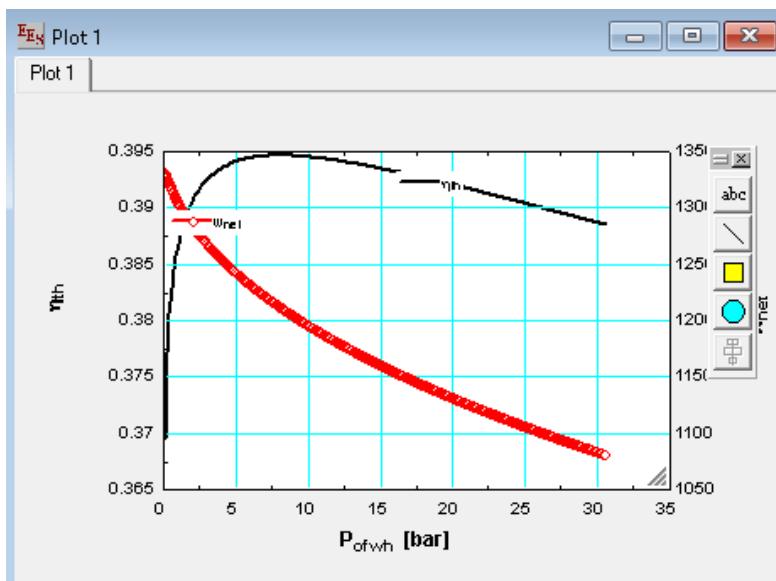
Flow Diagram



| 1..1000 | 1 η_{th} | 2 P_{ofwh} [bar] | 3 W_{net} |
|----------|------------------|--------------------------|----------------|
| Run 975 | 0.3888 | 29.75 | 1085 |
| Run 976 | 0.3887 | 29.78 | 1085 |
| Run 977 | 0.3887 | 29.81 | 1085 |
| Run 978 | 0.3887 | 29.84 | 1085 |
| Run 979 | 0.3887 | 29.87 | 1085 |
| Run 980 | 0.3887 | 29.9 | 1084 |
| Run 981 | 0.3887 | 29.93 | 1084 |
| Run 982 | 0.3887 | 29.96 | 1084 |
| Run 983 | 0.3887 | 29.99 | 1084 |
| Run 984 | 0.3887 | 30.02 | 1084 |
| Run 985 | 0.3887 | 30.05 | 1084 |
| Run 986 | 0.3886 | 30.08 | 1084 |
| Run 987 | 0.3886 | 30.11 | 1083 |
| Run 988 | 0.3886 | 30.14 | 1083 |
| Run 989 | 0.3886 | 30.18 | 1083 |
| Run 990 | 0.3886 | 30.21 | 1083 |
| Run 991 | 0.3886 | 30.24 | 1083 |
| Run 992 | 0.3886 | 30.27 | 1083 |
| Run 993 | 0.3886 | 30.3 | 1083 |
| Run 994 | 0.3886 | 30.33 | 1083 |
| Run 995 | 0.3885 | 30.36 | 1082 |
| Run 996 | 0.3885 | 30.39 | 1082 |
| Run 997 | 0.3885 | 30.42 | 1082 |
| Run 998 | 0.3885 | 30.45 | 1082 |
| Run 999 | 0.3885 | 30.48 | 1082 |
| Run 1000 | 0.3885 | 30.51 | 1082 |

Parametric Table for P_{ofwh} with efficiency and work net

Plotting P_{ofwh} against efficiency and work net



Using Duplicate

eta_p=0.95

P_c=0.1

P_b=150

P_r=30.51

T_max=500

eta_t=0.85

Duplicate i=1,30

P_ofwh[i]=(1)+(i-1)*(30-1)/30

h_2s[i]=enthalpy(Steam,s=s_2,P=P_ofwh[i])

h_2[i]=((h_2s[i]-h_1)/eta_p)+h_1

h_3[i]=enthalpy(Steam,x=0,P=P_ofwh[i])

s_3[i]=entropy(Steam,x=0,P=P_ofwh[i])

s_4[i]=s_3[i]

h_4s[i]=enthalpy(Steam,s=s_4[i],P=P_b)

h_4[i]=(h_4s[i]-h_3[i])/eta_p+h_3[i]

h_6s[i]=enthalpy(Steam,s=s_6s,P=P_ofwh[i])

h_6[i]=h_8-((h_8-h_6s[i])*eta_t)

s_6[i]=entropy(Steam,h=h_6[i],P=P_ofwh[i])

s_9[i]=s_6[i]

h_9s[i]=enthalpy(Steam,s=s_9[i],P=P_c)

h_9[i]=h_6[i]-((h_6[i]-h_9s[i])*eta_t)

m[i]=(h_3[i]-h_2[i])/(h_6[i]-h_2[i])

w_t[i]=(h_5-h_7)+(h_8-h_6[i])+(h_6[i]-h_9[i])*(1-m[i])

w_p[i]=(h_2[i]-h_1)*(1-m[i]) + (h_4[i]-h_3[i])

q_add[i]=h_5-h_4[i]+h_8-h_7

w_net[i]=w_t[i]-w_p[i]

eta_th[i]=w_net[i]/q_add[i]

End

h_1=enthalpy(Steam,x=0,P=0.1)

s_1=entropy(Steam,x=0,P=0.1)

s_2=s_1

{Point 5}

h_5=enthalpy(Steam,P=P_b,T=T_max)

s_5=entropy(Steam,P=P_b,T=T_max)

{Point 8}

h_8=enthalpy(Steam,P=P_r,T=T_max)

s_8=entropy(Steam,P=P_r,T=T_max)

s_6s=s_8

{Point 7}

s_7=s_5

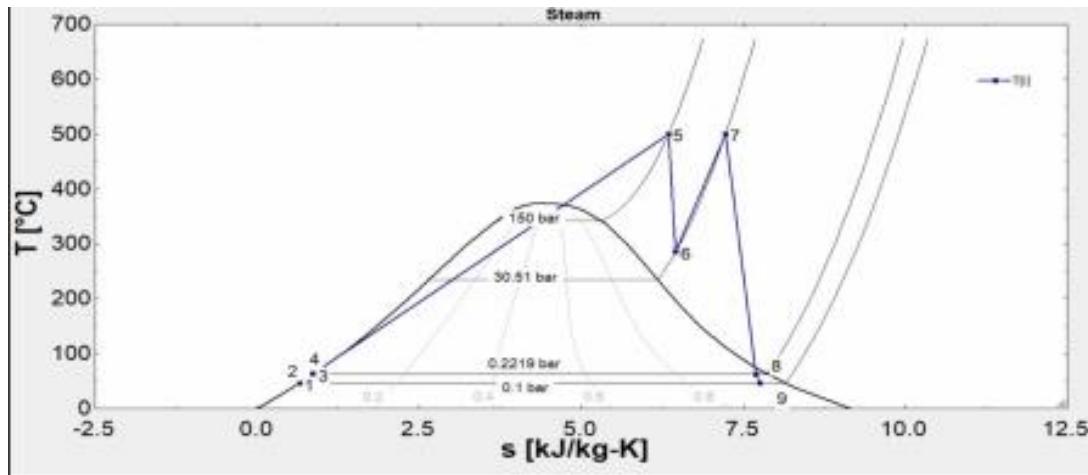
h_7s=enthalpy(Steam,s=s_7,P=P_r)

eta_t=(h_5-h_7)/(h_5-h_7s)

Results tab for Duplicate

| ¹ h _{2,i} | ² h _{2s,i} | ³ P _{ofwh,i} | ⁴ h _{3,i} | ⁵ s _{3,i} | ⁶ $\eta_{lh,i}$ | ⁷ h _{4,i} | ⁸ h _{4s,i} | ⁹ h _{6,i} | ¹⁰ h _{6s,i} | ¹¹ h _{9,i} | ¹² h _{9s,i} | ¹³ m _i | ¹⁴ q _{add,i} | ¹⁵ s _{4,i} | ¹⁶ s _{6,i} |
|----------------------------------|-----------------------------------|-------------------------------------|----------------------------------|----------------------------------|-------------------------------|----------------------------------|-----------------------------------|----------------------------------|------------------------------------|-----------------------------------|------------------------------------|---------------------------------|-------------------------------------|-----------------------------------|-----------------------------------|
| 192 | 192 | 1.967 | 502.5 | 1.524 | 0.3971 | 518.9 | 518.1 | 2851 | 2744 | 2441 | 2368 | 0.1168 | 3294 | 1.524 | 7.47 |
| 192.1 | 192.1 | 2.933 | 558.2 | 1.664 | 0.3995 | 574.7 | 573.9 | 2917 | 2822 | 2438 | 2354 | 0.1343 | 3239 | 1.664 | 7.42 |
| 192.2 | 192.2 | 3.9 | 600.7 | 1.767 | 0.4006 | 617.3 | 616.5 | 2968 | 2882 | 2438 | 2345 | 0.1472 | 3196 | 1.767 | 7.39 |
| 192.3 | 192.3 | 4.867 | 635.7 | 1.85 | 0.4011 | 652.3 | 651.5 | 3010 | 2932 | 2439 | 2338 | 0.1573 | 3161 | 1.85 | 7.37 |
| 192.4 | 192.4 | 5.833 | 665.6 | 1.92 | 0.4012 | 682.2 | 681.4 | 3047 | 2974 | 2439 | 2332 | 0.1658 | 3131 | 1.92 | 7.3 |
| 192.5 | 192.5 | 6.8 | 691.9 | 1.98 | 0.4011 | 708.5 | 707.7 | 3078 | 3012 | 2440 | 2328 | 0.173 | 3105 | 1.98 | 7.34 |
| 192.6 | 192.6 | 7.767 | 715.5 | 2.034 | 0.4009 | 732.1 | 731.3 | 3107 | 3045 | 2441 | 2324 | 0.1794 | 3081 | 2.034 | 7.33 |
| 192.7 | 192.7 | 8.733 | 737 | 2.082 | 0.4006 | 753.5 | 752.7 | 3133 | 3076 | 2442 | 2321 | 0.1851 | 3060 | 2.082 | 7.32 |
| 192.8 | 192.8 | 9.7 | 756.7 | 2.125 | 0.4002 | 773.2 | 772.4 | 3157 | 3104 | 2444 | 2318 | 0.1902 | 3040 | 2.125 | 7.31 |
| 192.9 | 192.9 | 10.67 | 775 | 2.165 | 0.3998 | 791.5 | 790.7 | 3179 | 3130 | 2445 | 2315 | 0.1949 | 3022 | 2.165 | 7.30 |
| 193 | 193 | 11.63 | 792.1 | 2.203 | 0.3993 | 808.6 | 807.8 | 3199 | 3154 | 2446 | 2313 | 0.1993 | 3005 | 2.203 | 7.29 |
| 193.1 | 193.1 | 12.6 | 808.2 | 2.237 | 0.3988 | 824.6 | 823.8 | 3219 | 3177 | 2447 | 2311 | 0.2033 | 2989 | 2.237 | 7.29 |
| 193.2 | 193.2 | 13.57 | 823.4 | 2.27 | 0.3983 | 839.8 | 839 | 3237 | 3198 | 2448 | 2309 | 0.2071 | 2973 | 2.27 | 7.28 |
| 193.3 | 193.3 | 14.53 | 837.8 | 2.3 | 0.3978 | 854.2 | 853.4 | 3254 | 3218 | 2449 | 2307 | 0.2106 | 2959 | 2.3 | 7.28 |
| 193.4 | 193.4 | 15.5 | 851.6 | 2.329 | 0.3972 | 867.9 | 867.1 | 3270 | 3237 | 2450 | 2306 | 0.2139 | 2945 | 2.329 | 7.27 |
| 193.5 | 193.5 | 16.47 | 864.7 | 2.357 | 0.3967 | 881 | 880.1 | 3286 | 3256 | 2451 | 2304 | 0.217 | 2932 | 2.357 | 7.27 |
| 193.6 | 193.6 | 17.43 | 877.3 | 2.383 | 0.3961 | 893.5 | 892.7 | 3301 | 3273 | 2452 | 2303 | 0.22 | 2920 | 2.383 | 7.26 |
| 193.7 | 193.7 | 18.4 | 889.4 | 2.408 | 0.3956 | 905.5 | 904.7 | 3315 | 3290 | 2453 | 2301 | 0.2229 | 2908 | 2.408 | 7.26 |
| 193.8 | 193.8 | 19.37 | 901.1 | 2.432 | 0.395 | 917.1 | 916.3 | 3328 | 3306 | 2454 | 2300 | 0.2256 | 2896 | 2.432 | 7.2 |
| 194 | 193.8 | 20.33 | 912.3 | 2.455 | 0.3944 | 928.3 | 927.5 | 3342 | 3321 | 2455 | 2299 | 0.2282 | 2885 | 2.455 | 7.25 |
| 194.1 | 193.9 | 21.3 | 923.2 | 2.477 | 0.3938 | 939.1 | 938.3 | 3354 | 3336 | 2456 | 2298 | 0.2307 | 2874 | 2.477 | 7.25 |
| 194.2 | 193.9 | 22.3 | 933.7 | 2.499 | 0.3932 | 950.0 | 949.2 | 3366 | 3349 | 2457 | 2297 | 0.2331 | 2864 | 2.499 | 7.24 |

T-S diagram



D.2 One OFWH & CFWH were added to the reheat cycle

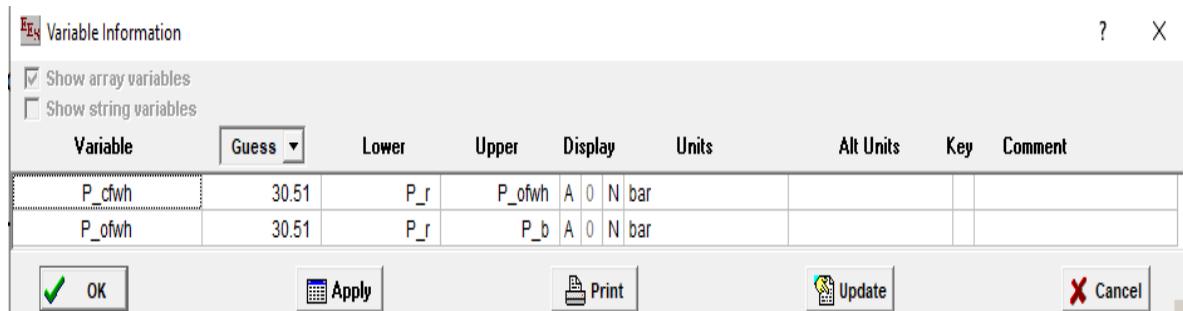
After the Reheat Pressure

```
{Take p_ofwh&p_cfw from HT turbine}  
{given}  
P_b=150  
P_c=0.1  
P_r=30.51  
T_max=500  
eta_p=0.95  
eta_t=0.85  
{point1}  
h_1=enthalpy(Steam,x=0,P=P_c)  
s_1=entropy(Steam,x=0,P=P_c)  
{point2}  
s_2s=s_1  
h_2s=enthalpy(Steam,s=s_2s,P=P_ofwh)  
eta_p=(h_2s-h_1)/(h_2-h_1)  
{point11}  
h_11=enthalpy(Steam,x=0,P=P_cfw)  
T_sat11=t_sat(Steam,P=P_cfw)  
{point12}  
h_12=h_11  
{point3}  
T_3=T_sat11  
h_3=4.18*T_3  
{point4}  
h_4=enthalpy(Steam,x=0,P=P_ofwh)  
s_4=entropy(Steam,x=0,P=P_ofwh)  
{point5}  
s_5s=s_4  
h_5s=enthalpy(Steam,s=s_5s,P=P_b)  
eta_p=(h_5s-h_4)/(h_5-h_4)  
{point6}  
h_6=enthalpy(Steam,T=T_max,P=P_b)  
s_6=entropy(Steam,T=T_max,P=P_b)
```

```

{point9}
s_9s=s_6
h_9s=enthalpy(Steam,s=s_9s,P=P_ofwh)
eta_t=(h_6-h_9)/(h_6-h_9s)
s_9=entropy(Steam,h=h_9,P=P_ofwh)
{point10}
s_10s=s_9
h_10s=enthalpy(Steam,s=s_10s,P=P_cfh)
eta_t=(h_9-h_10)/(h_9-h_10s)
s_10=entropy(Steam,h=h_10,P=P_cfh)
{point7}
s_7s=s_10
h_7s=enthalpy(Steam,s=s_7s,P=P_r)
eta_t=(h_10-h_7)/(h_10-h_7s)
s_7=entropy(Steam,h=h_7,P=P_r)
{point8}
h_8=enthalpy(Steam,T=T_max,P=P_r)
s_8=entropy(Steam,T=T_max,P=P_r)
{point13}
s_13s=s_8
h_13s=enthalpy(Steam,s=s_13s,P=P_c)
eta_t=(h_8-h_13)/(h_8-h_13s)
s_13=entropy(Steam,h=h_13,P=P_c)
x_13=quality(Steam,s=s_13,P=P_c)
{HB OFWH}
m_1=(h_4-h_3)/(h_9-h_3)
{HB CFWH}
(m_2*h_10)+(1-m_1)*h_2=(m_2*h_11)+(1-m_1)*h_3
{calculation}
w_t=(h_6-h_9)+(h_9-h_10)*(1-m_1)+(h_10-h_7)*(1-m_1-m_2)+(h_8-h_13)*(1-m_1-m_2)
w_p=(h_2-h_1)*(1-m_1)+(h_5-h_4)
w_net=w_t-w_p
q_add=(h_6-h_5)+(h_8-h_7)*(1-m_1-m_2)
eta_th=w_net/q_add

```



Calculations Completed

49 equations in 31 blocks - 38 iterations

Elapsed time = 2.2 sec

eta_th = 0.3629



| Independent Variable | Value | Best value |
|----------------------|-------|------------|
| P_cfwh | 30.51 | 30.51 |
| P_ofwh | 72.75 | 72.75 |

Optimum OFWH pressure = 72.75bar

Optimum CFWH pressure = 30.51bar

Max thermal efficiency = 0.3629 bar

Results tab

Unit Settings: SI C bar kJ mass deg

Maximization of eta_th(P_cfwh,P_ofwh) = 0.3629 38 iterations: Variable Metric method

| | | | | |
|--------------------------|---------------------|----------------------|-----------------|------------------|
| $\eta_p = 0.95$ | $\eta_t = 0.85$ | $\eta_{th} = 0.3629$ | $h_1 = 191.8$ | $h_{10} = 2949$ |
| $h_{13s} = 2290$ | $h_2 = 199.5$ | $h_{2s} = 199.1$ | $h_3 = 981.4$ | $h_4 = 1281$ |
| $h_7s = 2949$ | $h_8 = 3457$ | $h_9 = 3133$ | $h_{9s} = 3102$ | $m_1 = 0.1395$ |
| $P_{ofwh} = 72.75$ [bar] | $P_r = 30.51$ | $q_{add} = 2279$ | $s_1 = 0.6492$ | $s_{10} = 6.454$ |
| $s_4 = 3.146$ | $s_{5s} = 3.146$ | $s_6 = 6.348$ | $s_7 = 6.454$ | $s_{7s} = 6.454$ |
| $T_{max} = 500$ | $T_{sat11} = 234.8$ | $w_{net} = 827$ | $w_p = 17.64$ | $w_t = 844.6$ |

| | | | |
|-------------------|------------------|-------------------|--------------------------|
| $h_{10s} = 2917$ | $h_{11} = 1013$ | $h_{12} = 1013$ | $h_{13} = 2465$ |
| $h_5 = 1292$ | $h_{5s} = 1292$ | $h_6 = 3311$ | $h_7 = 2949$ |
| $m_2 = 0.3474$ | $P_b = 150$ | $P_c = 0.1$ | $P_{cfwh} = 30.51$ [bar] |
| $s_{10s} = 6.395$ | $s_{13} = 7.776$ | $s_{13s} = 7.228$ | $s_{2s} = 0.6492$ |
| $s_8 = 7.228$ | $s_9 = 6.395$ | $s_{9s} = 6.348$ | $T_3 = 234.8$ |
| $x_{13} = 0.9503$ | | | |

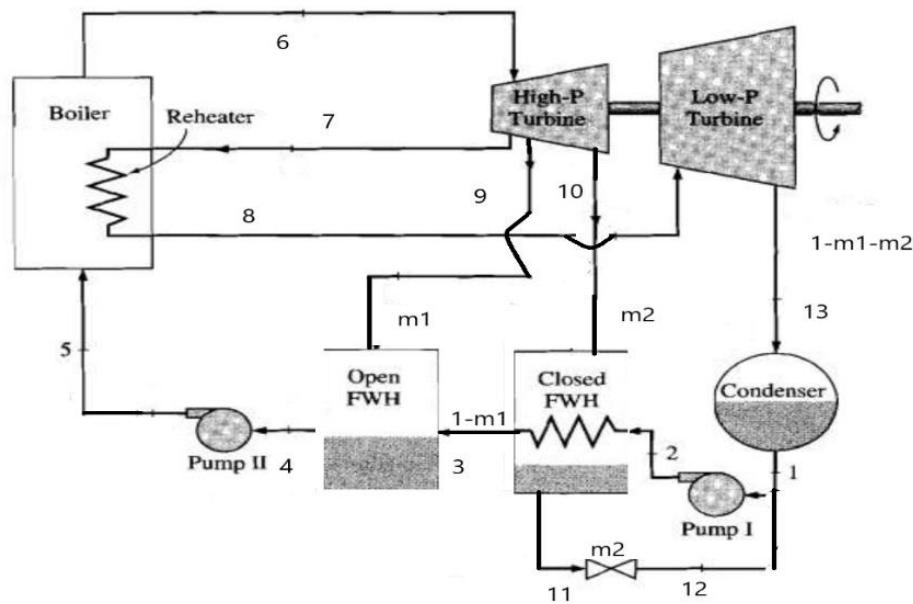
| | 1..10 | η_{lh} | P_{cfwh} [bar] | P_{ofwh} [bar] |
|--------------|-------|-------------|---------------------|---------------------|
| Run 1 | | 0.3572 | 30 | 30 |
| Run 2 | | 0.3563 | 31.11 | 32.22 |
| Run 3 | | 0.3553 | 32.22 | 34.44 |
| Run 4 | | 0.3543 | 33.33 | 36.67 |
| Run 5 | | 0.3532 | 34.44 | 38.89 |
| Run 6 | | 0.3521 | 35.56 | 41.11 |
| Run 7 | | 0.3509 | 36.67 | 43.33 |
| Run 8 | | 0.3497 | 37.78 | 45.56 |
| Run 9 | | 0.3485 | 38.89 | 47.78 |
| Run 10 | | 0.3472 | 40 | 50 |

| | 1..10 | η_{lh} | P_{cfwh} [bar] | P_{ofwh} [bar] |
|--------------|-------|-------------|---------------------|---------------------|
| Run 1 | | 0.3472 | 40 | 50 |
| Run 2 | | 0.3452 | 41.67 | 52.78 |
| Run 3 | | 0.3431 | 43.33 | 55.56 |
| Run 4 | | 0.341 | 45 | 58.33 |
| Run 5 | | 0.3389 | 46.67 | 61.11 |
| Run 6 | | 0.3367 | 48.33 | 63.89 |
| Run 7 | | 0.3345 | 50 | 66.67 |
| Run 8 | | 0.3323 | 51.67 | 69.44 |
| Run 9 | | 0.3301 | 53.33 | 72.22 |
| Run 10 | | 0.3279 | 55 | 75 |

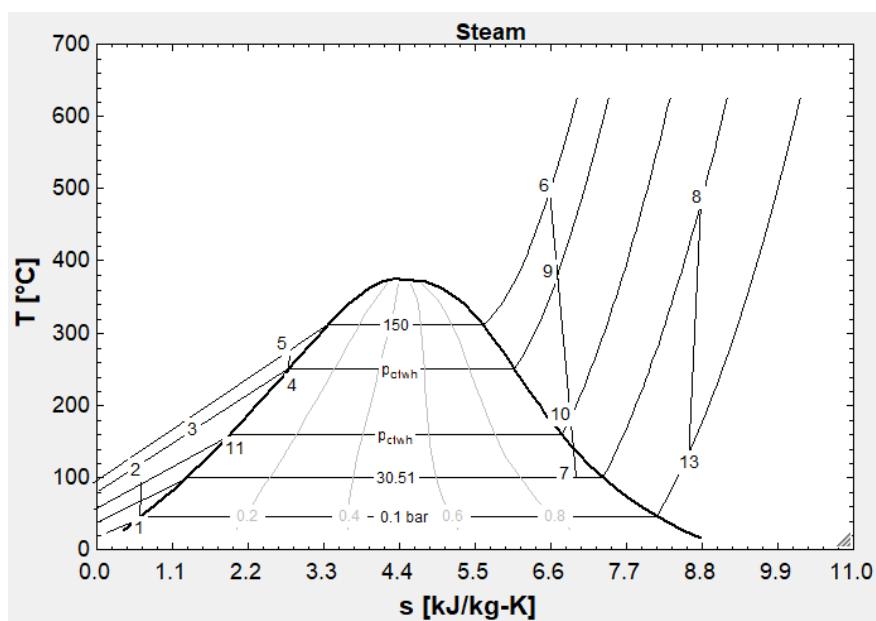
| | 1..10 | η_{lh} | P_{cfwh} [bar] | P_{ofwh} [bar] |
|--------------|-------|-------------|---------------------|---------------------|
| Run 1 | | 0.2924 | 80 | 100 |
| Run 2 | | 0.2892 | 82.22 | 105.6 |
| Run 3 | | 0.2859 | 84.44 | 111.1 |
| Run 4 | | 0.2826 | 86.67 | 116.7 |
| Run 5 | | 0.2793 | 88.89 | 122.2 |
| Run 6 | | 0.2759 | 91.11 | 127.8 |
| Run 7 | | 0.2724 | 93.33 | 133.3 |
| Run 8 | | 0.2689 | 95.56 | 138.9 |
| Run 9 | | 0.2653 | 97.78 | 144.4 |
| Run 10 | | 0.2616 | 100 | 150 |

| | 1..10 | η_{lh} | P_{cfwh} [bar] | P_{ofwh} [bar] |
|--------------|-------|-------------|---------------------|---------------------|
| Run 1 | | 0.3279 | 55 | 75 |
| Run 2 | | 0.324 | 57.78 | 77.78 |
| Run 3 | | 0.3201 | 60.56 | 80.56 |
| Run 4 | | 0.3162 | 63.33 | 83.33 |
| Run 5 | | 0.3123 | 66.11 | 86.11 |
| Run 6 | | 0.3083 | 68.89 | 88.89 |
| Run 7 | | 0.3044 | 71.67 | 91.67 |
| Run 8 | | 0.3004 | 74.44 | 94.44 |
| Run 9 | | 0.2964 | 77.22 | 97.22 |
| Run 10 | | 0.2924 | 80 | 100 |

Flow Diagram



T-s Diagram



Take OFWH pressure from LT & CFWH pressure from HT

{Given}

P_b=150

P_c=0.1

P_r=30.51

T_max=500

eta_p=0.95

eta_t=0.85

{point1}

h_1=Enthalpy(Steam,x=0,P=P_c)

s_1=Entropy(Steam,x=0,P=P_c)

{point2}

s_1=s_2

h_2s=Enthalpy(Steam,s=s_2,P=P_ofwh)

eta_p=(h_2s-h_1)/(h_2-h_1)

{point12}

h_12=Enthalpy(Steam,x=0,P=P_cfwh)

h_12=h_13

T_12=T_sat(Steam,P=P_cfwh)

{point3}

T_3=T_12

h_3=T_3*4.18

{point4}

h_4=Enthalpy(Steam,x=0,P=P_ofwh)

s_4=Entropy(Steam,x=0,P=P_ofwh)

{point5}

s_5=s_4

h_5s=Enthalpy(Steam,s=s_5,P=P_b)

eta_p*(h_5s-h_4)=(h_5s-h_4)

{point6}

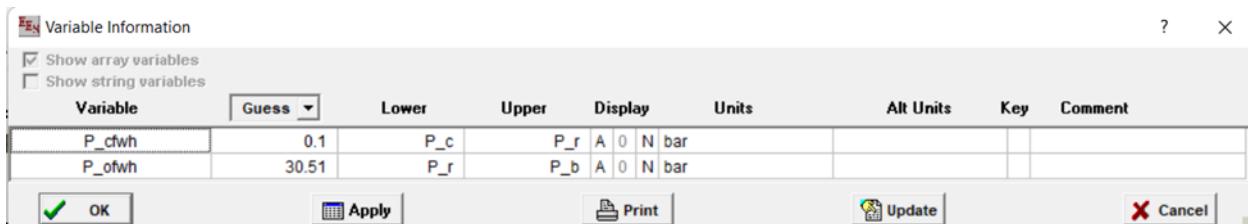
h_6=Enthalpy(Steam,T=T_max,P=P_b)

s_6=Entropy(Steam,T=T_max,P=P_b)

```

s_6=s_9s
h_9s=Enthalpy(Steam,s=s_9s,P=P_ofwh)
eta_t=(h_6-h_9)/(h_6-h_9s)
s_9=Entropy(Steam,h=h_9,P=P_ofwh)
{point7}
s_7s=s_9
h_7s=Enthalpy(Steam,s=s_7s,P=P_r)
eta_t=(h_9-h_7)/(h_9-h_7s)
s_7=Entropy(Steam,h=h_7,P=P_r)
{point8}
h_8=Enthalpy(Steam,T=T_max,P=P_r)
s_8=Entropy(Steam,T=T_max,P=P_r)
{point10}
s_10s=s_8
h_10s=Enthalpy(Steam,s=s_10s,P=P_cfh)
eta_t=(h_8-h_10)/(h_8-h_10s)
s_10=Entropy(Steam,h=h_10,P=P_cfh)
{point11}
s_11s=s_10
h_11s=Enthalpy(Steam,s=s_11s,P=P_c)
eta_t*(h_10-h_11s)=(h_10-h_11)
s_11=Entropy(Steam,h=h_11,P=P_c)
x_11=Quality(Steam,s=s_11,h=h_11)
{mass balance}
m_1=(h_4-h_3)/(h_9-h_3)
(m_2*h_10)+(1-m_1)*h_2=(m_2*h_12)+(1-m_1)*h_3
{calculation}
w_p=(h_5-h_4)+(1-m_1)*(h_2-h_1)
w_t=(h_6-h_9)+(h_9-h_7)*(1-m_1)+(h_8-h_10)*(1-m_1)+(h_10-h_11)*(1-m_1-m_2)
w_net=w_t-w_p
q_add=(h_6-h_5)+(h_8-h_7)*(1-m_1)
eta_th=w_net/q_add

```



Calculations Completed

49 equations in 35 blocks - 97 iterations

Elapsed time = 3.6 sec

eta_th = 0.4109

Optimum OFWH pressure=37.78bar

Optimum CFWH pressure=2.377bar

Max thermal efficiency=0.4109bar

 Continue

| Independent Variable | Value | Best value |
|----------------------|-------|------------|
| P_cfwh | 2.377 | 2.377 |
| P_ofwh | 37.78 | 37.78 |

Results tab

Unit Settings: SI C bar kJ mass deg

Maximization of eta_th(P_cfwh,P_ofwh) = 0.4109 97 iterations: Variable Metric method

$\eta_p = 0.95$ $\eta_l = 0.85$ $\eta_{th} = 0.4109$ $h_1 = 191.8$ $h_{10} = 2881$ $h_{10s} = 2780$ $h_{11} = 2439$ $h_{11s} = 2361$ $h_{12} = 528.3$
 $h_{13} = 528.3$ $h_2 = 195.8$ $h_{2s} = 195.6$ $h_3 = 525.7$ $h_4 = 1071$ $h_5 = 1086$ $h_{5s} = 1085$ $h_6 = 3311$ $h_7 = 2952$
 $h_{7s} = 2944$ $h_8 = 3457$ $h_9 = 2995$ $h_{9s} = 2939$ $m_1 = 0.2209$ $m_2 = 0.1092$ $P_b = 150$ $P_c = 0.1$ $P_{cfwh} = 2.377$ [bar]

$P_{ofwh} = 37.78$ [bar] $P_r = 30.51$ $q_{add} = 2618$ $s_1 = 0.6492$ $s_{10} = 7.451$ $s_{10s} = 7.228$ $s_{11} = 7.696$ $s_{11s} = 7.451$ $s_2 = 0.6492$

$s_4 = 2.766$ $s_5 = 2.766$ $s_6 = 6.348$ $s_7 = 6.459$ $s_{7s} = 6.445$ $s_8 = 7.228$ $s_9 = 6.445$ $s_{9s} = 6.348$ $T_{12} = 125.8$

$T_3 = 125.8$ $T_{max} = 500$ $w_{net} = 1076$ $w_p = 17.75$ $w_t = 1094$ $x_{11} = 0.9396$

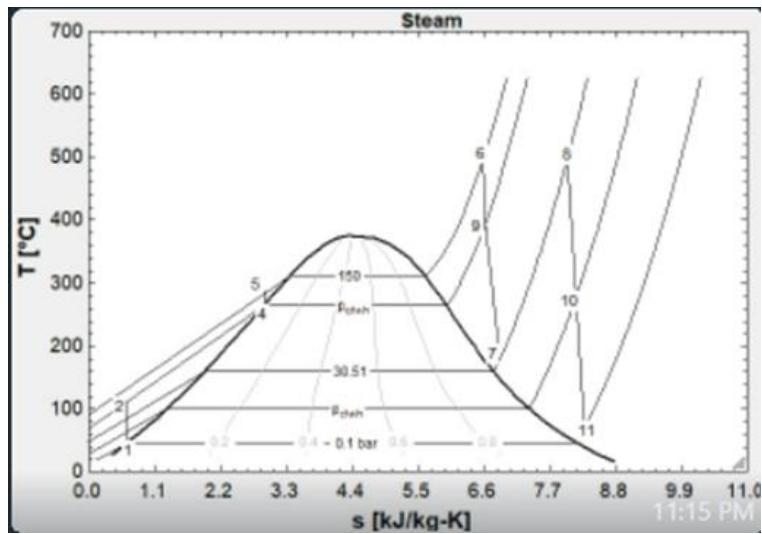
| Table 1 Table 2 Table 3 Table 4 | | | |
|---------------------------------------|-----------------|-------------------------|-------------------------|
| 1..10 | η _{th} | P _{cfwh} [bar] | P _{ofwh} [bar] |
| Run 1 | 0.3931 | 0.1 | 30 |
| Run 2 | 0.4017 | 0.3111 | 32.22 |
| Run 3 | 0.4048 | 0.5222 | 34.44 |
| Run 4 | 0.4066 | 0.7333 | 36.67 |
| Run 5 | 0.4079 | 0.9444 | 38.89 |
| Run 6 | 0.4088 | 1.156 | 41.11 |
| Run 7 | 0.4094 | 1.367 | 43.33 |
| Run 8 | 0.4098 | 1.578 | 45.56 |
| Run 9 | 0.4101 | 1.789 | 47.78 |
| Run 10 | 0.4102 | 2 | 50 |

| Table 1 Table 2 Table 3 Table 4 | | | |
|---------------------------------------|-----------------|-------------------------|-------------------------|
| 1..10 | η _{th} | P _{cfwh} [bar] | P _{ofwh} [bar] |
| Run 1 | 0.4102 | 2 | 50 |
| Run 2 | 0.4102 | 2.889 | 52.78 |
| Run 3 | 0.4094 | 3.778 | 55.56 |
| Run 4 | 0.4082 | 4.667 | 58.33 |
| Run 5 | 0.4068 | 5.556 | 61.11 |
| Run 6 | 0.4052 | 6.444 | 63.89 |
| Run 7 | 0.4036 | 7.333 | 66.67 |
| Run 8 | 0.402 | 8.222 | 69.44 |
| Run 9 | 0.4003 | 9.111 | 72.22 |
| Run 10 | 0.3987 | 10 | 75 |

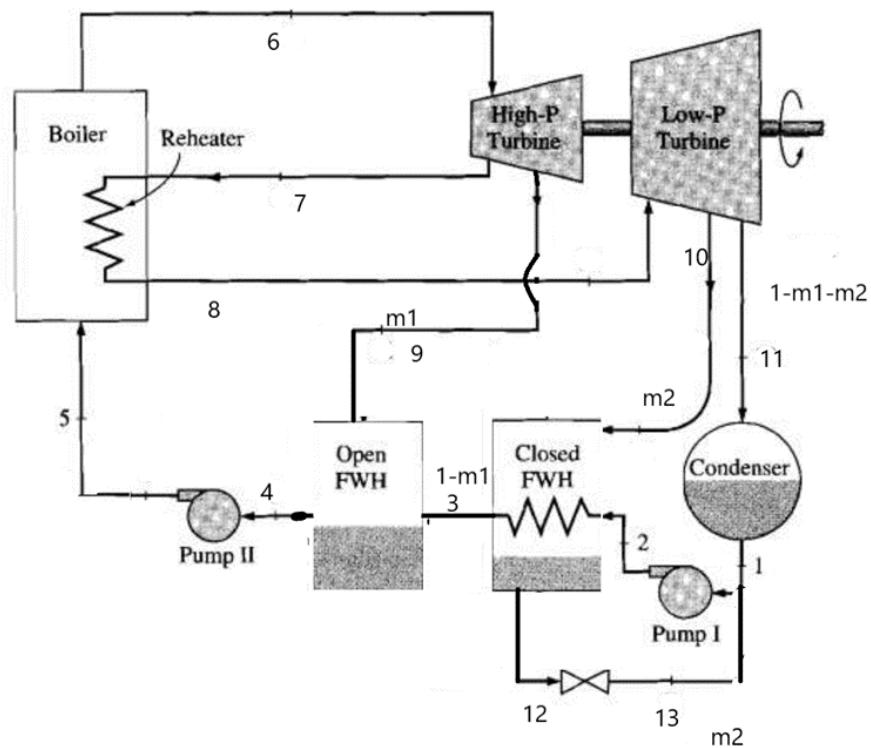
| Table 1 Table 2 Table 3 Table 4 | | | |
|---------------------------------------|-----------------|-------------------------|-------------------------|
| 1..10 | η _{th} | P _{cfwh} [bar] | P _{ofwh} [bar] |
| Run 1 | 0.3987 | 10 | 75 |
| Run 2 | 0.3975 | 10.56 | 77.78 |
| Run 3 | 0.3964 | 11.11 | 80.56 |
| Run 4 | 0.3952 | 11.67 | 83.33 |
| Run 5 | 0.3941 | 12.22 | 86.11 |
| Run 6 | 0.3929 | 12.78 | 88.89 |
| Run 7 | 0.3918 | 13.33 | 91.67 |
| Run 8 | 0.3906 | 13.89 | 94.44 |
| Run 9 | 0.3895 | 14.44 | 97.22 |
| Run 10 | 0.3883 | 15 | 100 |

| Table 1 Table 2 Table 3 Table 4 | | | |
|---------------------------------------|-----------------|-------------------------|-------------------------|
| 1..10 | η _{th} | P _{cfwh} [bar] | P _{ofwh} [bar] |
| Run 1 | 0.3883 | 15 | 100 |
| Run 2 | 0.3851 | 16.67 | 105.6 |
| Run 3 | 0.3819 | 18.33 | 111.1 |
| Run 4 | 0.3788 | 20 | 116.7 |
| Run 5 | 0.3757 | 21.67 | 122.2 |
| Run 6 | 0.3726 | 23.33 | 127.8 |
| Run 7 | 0.3695 | 25 | 133.3 |
| Run 8 | 0.3664 | 26.67 | 138.9 |
| Run 9 | 0.3634 | 28.33 | 144.4 |
| Run 10 | 0.3603 | 30 | 150 |

T-s Diagram



Flow Diagram



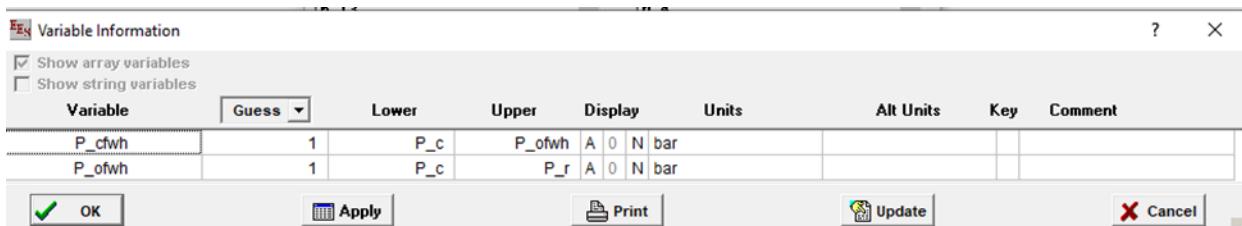
Before the reheat pressure

```
{p_ofwh&p_cfw from LT}
{given}
P_b=150
P_c=0.1
P_r=30.51
T_max=500
eta_t=0.85
eta_p=0.95
{point1}
h_1=enthalpy(Steam,x=0,P=P_c)
s_1=entropy(Steam,x=0,P=P_c)
{point2}
s_1=s_2
h_2s=enthalpy(Steam,s=s_1,P=P_ofwh)
eta_p=(h_2s-h_1)/(h_2-h_1)
{point12}
h_12=enthalpy(Steam,x=0,P=P_cfw)
T_sat12=t_sat(Steam,P=P_cfw)
{point13}
h_12=h_13
{point3}
T_3=T_sat12
h_3=4.18*T_3
{point4}
h_4=enthalpy(Steam,x=0,P=P_ofwh)
s_4=entropy(Steam,x=0,P=P_ofwh)
{point5}
s_4=s_5
h_5s=enthalpy(Steam,s=s_4,P=P_b)
eta_p=(h_5s-h_4)/(h_5-h_4)
{point6}
h_6=enthalpy(Steam,T=T_max,P=P_b)
s_6=entropy(Steam,T=T_max,P=P_b)
```

```

{point7}
s_7=s_6
h_7s=enthalpy(Steam,s=s_6,P=P_r)
eta_t=(h_6-h_7)/(h_6-h_7s)
{point8}
h_8=enthalpy(Steam,T=T_max,P=P_r)
s_8=entropy(Steam,T=T_max,P=P_r)
{point9}
s_8=s_9s
h_9s=enthalpy(Steam,s=s_9s,P=P_ofwh)
eta_t=(h_8-h_9)/(h_8-h_9s)
s_9=entropy(Steam,h=h_9,P=P_ofwh)
{point10}
s_10s=s_9
h_10s=enthalpy(Steam,s=s_10s,P=P_cfh)
eta_t=(h_9-h_10)/(h_9-h_10s)
s_10=entropy(Steam,h=h_10,P=P_cfh)
{point11}
s_11s=s_10
h_11s=enthalpy(Steam,s=s_11s,P=P_c)
eta_t=(h_10-h_11)/(h_10-h_11s)
s_11=entropy(Steam,h=h_11,P=P_c)
x_11=quality(Steam,s=s_11,P=P_c)
{m}
m_1=(h_4-h_3)/(h_9-h_3)
(1-m_1)*h_2+(h_10*m_2)=(m_2*h_12)+(1-m_1)*h_3
{calculation}
w_t=(h_6-h_7)+(h_8-h_9)+(1-m_1)*(h_9-h_10)+(1-m_1-m_2)*(h_10-h_11)
w_p=(1-m_1)*(h_2-h_1)+(h_5-h_4)
w_net=w_t-w_p
q_add=(h_6-h_5)+(h_8-h_7)
eta_th=w_net/q_add

```



Calculations Completed

| 48 equations in 32 blocks - 141 iterations | | |
|--|-------|------------|
| Elapsed time = 3.3 sec | | |
| eta_th = 0.411 | | |
|  Continue | | |
| Independent Variable | Value | Best value |
| P_cfwh | 1.573 | 1.573 |
| P_ofwh | 12.65 | 12.65 |

Optimum OFWH pressure = 12.65bar

Optimum CFWH pressure = 1.573bar

Max thermal efficiency = 0.411

Results Tab

Unit Settings: SI C bar kJ mass deg

Maximization of eta_th(P_cfwh,P_ofwh) = 0.411 141 iterations: Variable Metric method

| | | | | |
|----------------------------------|-----------------------------|---------------------|-----------------|-------------------|
| $\eta_p = 0.95$ | $\eta_t = 0.85$ | $\eta_{th} = 0.411$ | $h_1 = 191.8$ | $h_{10} = 2803$ |
| $h_{13} = 473.2$ | $h_2 = 193.1$ | $h_{2s} = 193.1$ | $h_3 = 471.4$ | $h_4 = 809$ |
| $h_{7s} = 2891$ | $h_8 = 3457$ | $h_9 = 3220$ | $h_{9s} = 3178$ | $m_1 = 0.1228$ |
| $P_{ofwh} = 12.65 \text{ [bar]}$ | $P_r = 30.51 \text{ [bar]}$ | $q_{add} = 2988$ | $s_1 = 0.6492$ | $s_{10} = 7.468$ |
| $s_4 = 2.239$ | $s_5 = 2.239$ | $s_6 = 6.348$ | $s_7 = 6.348$ | $s_8 = 7.228$ |
| $T_{sat12} = 112.8 \text{ [C]}$ | $w_{net} = 1228$ | $w_p = 17.61$ | $w_t = 1246$ | $x_{11} = 0.9365$ |

| | | | |
|-------------------|------------------|---------------------------|----------------------------------|
| $h_{10s} = 2729$ | $h_{11} = 2432$ | $h_{11s} = 2367$ | $h_{12} = 473.2$ |
| $h_5 = 825.5$ | $h_{5s} = 824.6$ | $h_6 = 3311$ | $h_7 = 2954$ |
| $m_2 = 0.1048$ | $P_b = 150$ | $P_c = 0.1$ | $P_{cfwh} = 1.573 \text{ [bar]}$ |
| $s_{10s} = 7.292$ | $s_{11} = 7.673$ | $s_{11s} = 7.468$ | $s_2 = 0.6492$ |
| $s_9 = 7.292$ | $s_{9s} = 7.228$ | $T_3 = 112.8 \text{ [C]}$ | $T_{max} = 500 \text{ [C]}$ |

| | η_{lh} | P_{cfwh} [bar] | P_{ofwh} [bar] |
|--------|-------------|---------------------|---------------------|
| Run 1 | 0.3953 | 2 | 2 |
| Run 2 | 0.3961 | 2.111 | 2.194 |
| Run 3 | 0.3967 | 2.222 | 2.389 |
| Run 4 | 0.3973 | 2.333 | 2.583 |
| Run 5 | 0.3978 | 2.444 | 2.778 |
| Run 6 | 0.3982 | 2.556 | 2.972 |
| Run 7 | 0.3986 | 2.667 | 3.167 |
| Run 8 | 0.3989 | 2.778 | 3.361 |
| Run 9 | 0.3992 | 2.889 | 3.556 |
| Run 10 | 0.3994 | 3 | 3.75 |

| | η_{lh} | P_{cfwh} [bar] | P_{ofwh} [bar] |
|--------|-------------|---------------------|---------------------|
| Run 1 | 0.3695 | 0.1 | 0.1 |
| Run 2 | 0.4032 | 1.756 | 3.422 |
| Run 3 | 0.4043 | 3.411 | 6.744 |
| Run 4 | 0.4028 | 5.067 | 10.07 |
| Run 5 | 0.4005 | 6.722 | 13.39 |
| Run 6 | 0.3979 | 8.378 | 16.71 |
| Run 7 | 0.3951 | 10.03 | 20.03 |
| Run 8 | 0.3923 | 11.69 | 23.36 |
| Run 9 | 0.3894 | 13.34 | 26.68 |
| Run 10 | 0.3866 | 15 | 30 |

| | η_{lh} | P_{cfwh} [bar] | P_{ofwh} [bar] |
|--------|-------------|---------------------|---------------------|
| Run 1 | 0.3907 | 1 | 1 |
| Run 2 | 0.3999 | 1.722 | 2.556 |
| Run 3 | 0.4026 | 2.444 | 4.111 |
| Run 4 | 0.4035 | 3.167 | 5.667 |
| Run 5 | 0.4035 | 3.889 | 7.222 |
| Run 6 | 0.403 | 4.611 | 8.778 |
| Run 7 | 0.4023 | 5.333 | 10.33 |
| Run 8 | 0.4014 | 6.056 | 11.89 |
| Run 9 | 0.4004 | 6.778 | 13.44 |
| Run 10 | 0.3993 | 7.5 | 15 |

| | η_{lh} | P_{cfwh} [bar] | P_{ofwh} [bar] |
|--------|-------------|---------------------|---------------------|
| Run 1 | 0.3936 | 1.5 | 1.5 |
| Run 2 | 0.3976 | 1.75 | 2.167 |
| Run 3 | 0.4 | 2 | 2.833 |
| Run 4 | 0.4015 | 2.25 | 3.5 |
| Run 5 | 0.4026 | 2.5 | 4.167 |
| Run 6 | 0.4033 | 2.75 | 4.833 |
| Run 7 | 0.4037 | 3 | 5.5 |
| Run 8 | 0.404 | 3.25 | 6.167 |
| Run 9 | 0.4042 | 3.5 | 6.833 |
| Run 10 | 0.4042 | 3.75 | 7.5 |

Duplicate Code

```
{given}
P_c=0.1
P_b=150
P_r=30.51
eta_p=0.95
eta_t=0.85
T_max=500
```

Duplicate i=1,13

```
P_ofwh[i]=(P_c)+((i-1)*(P_r-P_c)/13)
h_2s[i]=enthalpy(Steam,s=s_1,P=P_ofwh[i])
h_2[i]=((h_2s[i]-h_1)/eta_p)+h_1
```

{point4}

```
h_4[i]=enthalpy(Steam,x=0,P=P_ofwh[i])
s_4[i]=entropy(Steam,x=0,P=P_ofwh[i])
```

{point5}

```
h_5s[i]=enthalpy(Steam,s=s_4[i],P=P_b)
h_5[i]=((h_5s[i]-h_4[i])/eta_p)+h_4[i]
```

{point9}

```
h_9s[i]=enthalpy(Steam,s=s_8,P=P_ofwh[i])
h_9[i]=h_8-eta_t*(h_8-h_9s[i])
s_9[i]=entropy(Steam,h=h_9[i],P=P_ofwh[i])
q_add[i]=(h_6-h_5[i])+(h_8-h_7)
```

Duplicate j=1,13

```
P_cfwh[j,i]=(P_c)+((j-1)*(P_ofwh[i]-P_c)/13)
```

{point12}

```
h_12[j,i]=enthalpy(Steam,x=0,P=P_cfwh[j,i])
T_sat12[j,i]=t_sat(Steam,P=P_cfwh[j,i])
```

{point13}

```
h_12[j,i]=h_13[j,i]
```

{point3}

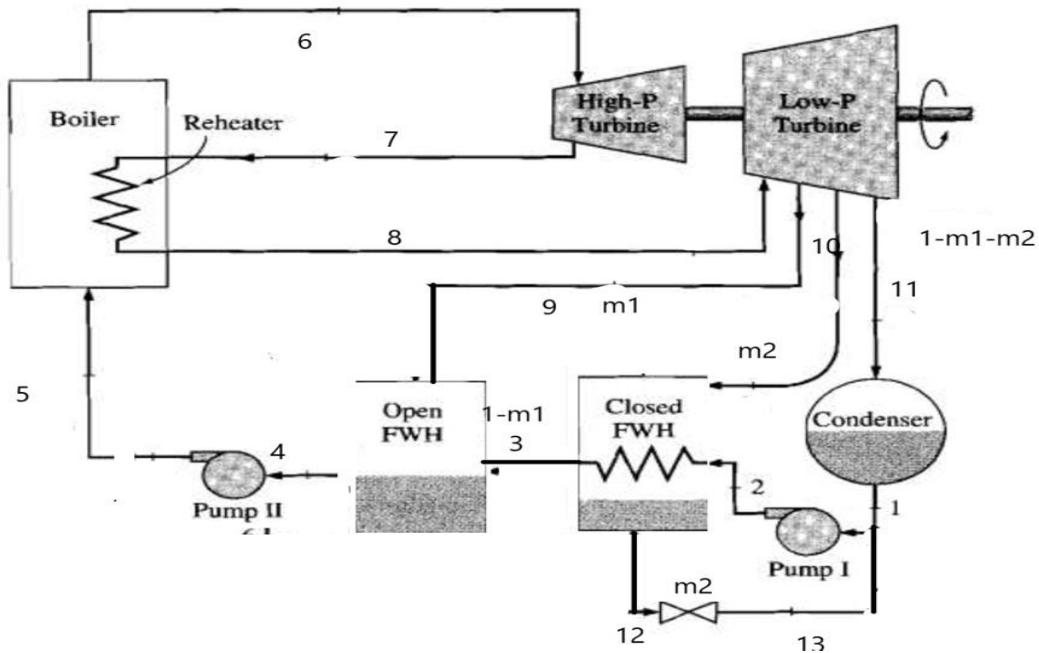
```
h_3[j,i]=4.18*T_sat12[j,i]
```

```

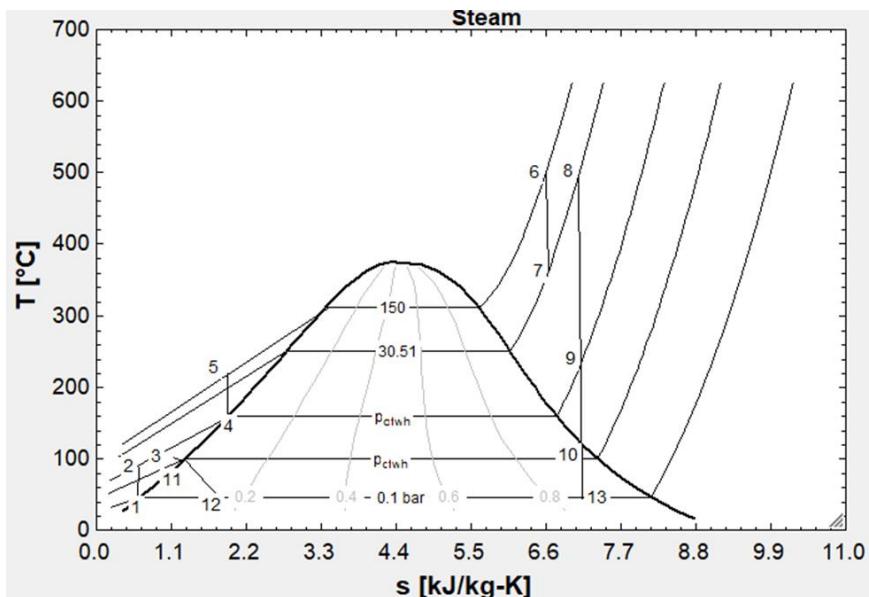
{point10}
h_10s[j,i]=enthalpy(Steam,s=s_9[i],P=P_cfcwh[j,i])
h_10[j,i]=h_9[i]-eta_t*(h_9[i]-h_10s[j,i])
s_10[j,i]=entropy(Steam,h=h_10[j,i],P=P_cfcwh[j,i])
{point11}
h_11s[j,i]=enthalpy(Steam,s=s_10[j,i],P=P_c)
h_11[j,i]=h_10[j,i]-eta_t*(h_10[j,i]-h_11s[j,i])
s_11[j,i]=entropy(Steam,h=h_11[j,i],P=P_c)
{m}
m_1[j,i]=(h_4[i]-h_3[j,i])/(h_9[i]-h_3[j,i])
(1-m_1[j,i])*h_2[i]+(h_10[j,i]*m_2[j,i])=(m_2[j,i]*h_12[j,i])+(1-m_1[j,i])*h_3[j,i]
{calculation}
w_tf[j,i]=(h_6-h_7)+(h_8-h_9[i])+(1-m_1[j,i])*(h_9[i]-h_10[j,i])+(1-m_1[j,i]-m_2[j,i])*(h_10[j,i]-h_11[j,i])
w_pf[j,i]=(1-m_1[j,i])*(h_2[i]-h_1)+(h_5[i]-h_4[i])
w_net[j,i]=w_tf[j,i]-w_pf[j,i]
eta_th[j,i]=w_net[j,i]/q_add[i]
End
End
{point1}
h_1=enthalpy(Steam,x=0,P=P_c)
s_1=entropy(Steam,x=0,P=P_c)
{point6}
h_6=enthalpy(Steam,T=T_max,P=P_b)
s_6=entropy(Steam,T=T_max,P=P_b)
{point7}
s_7=s_6
h_7s=enthalpy(Steam,s=s_6,P=P_r)
h_7=h_6-eta_t*(h_6-h_7s)
{point8}
h_8=enthalpy(Steam,T=T_max,P=P_r)
s_8=entropy(Steam,T=T_max,P=P_r)

```

Flow Diagram



T-s Diagram



Note: It's found that the highest efficiency obtained when the pressure of OFWH & CFWH from low turbine pressure.

D.3 One OFWH and two CFWHs were added to the reheat cycle

After the Reheat Pressure

Code

```
{given}
P_b=150
P_c=0.1
T_max=500
eta_turbine=.85;eta_pump=.95
p_reheat=30.51
"point1"
x[1]=0 "sat liq"
h_1=enthalpy(Steam,x=x[1],P=P_c)
s_1=entropy(Steam,x=x[1],P=P_c)
"point2"
s_2s=s_1
h_2s=enthalpy(Steam,s=s_2s,P=P_2)
eta_pump*(h_2s-h_1)=(h_2s-h_1)
{point 16}
T_16=temperature(Steam,P=P_3,x=0)
h_16=enthalpy(Steam,x=0,P=P_3)
h_16=h_17
{h_17=enthalpy(Steam,x=0,P=P_3)}
{point 3}
T_3=T_16
{h_3=enthalpy(Steam,T=T_16,P=P_2)}
h_3=4.18*T_16
{point 4}
h_4=enthalpy(Steam,x=0,P=P_2)
s_4=entropy(Steam,x=0,P=P_2)
{point 5}
s_4=s_5s
h_5s=enthalpy(Steam,s=s_5s,P=P_b)
eta_pump*(h_5s-h_4)=(h_5s-h_4)
{point 14}
T_sat_14=t_sat(Steam,P=P_1)
h_14=enthalpy(Steam,x=0,P=P_1)
h_14=h_15
{point 6}
T_sat_14=T_6
{h_6=enthalpy(Steam,T=T_sat_14,P=P_b)}
h_6=4.18*T_sat_14
```

```

{point 7}
h_7=enthalpy(Steam,T=T_max,P=P_b)
s_7=entropy(Steam,T=T_max,P=P_b)
{point 8}
s_7=s_8s
h_8s=enthalpy(Steam,s=s_8s,P=P_reheat)
eta_turbine*(h_7-h_8s)=(h_7-h_8)
s_8=entropy(Steam,h=h_8,P=P_reheat)
{point 9}
h_9=enthalpy(Steam,T=T_max,P=P_reheat)
s_9=entropy(Steam,T=T_max,P=P_reheat)
{point 10}
s_10s=s_9
h_10s=enthalpy(Steam,s=s_10s,P=P_1)
eta_turbine*(h_9-h_10s)=(h_9-h_10)
s_10=entropy(Steam,h=h_10,P=P_1)
{point 11}
s_10=s_11s
h_11s=enthalpy(Steam,s=s_11s,P=P_2)
eta_turbine*(h_10-h_11s)=(h_10-h_11)
s_11=entropy(Steam,h=h_11,P=P_2)
{point 12}
s_11=s_12s
h_12s=enthalpy(Steam,s=s_12s,P=P_3)
eta_turbine*(h_11-h_12s)=(h_11-h_12)
s_12=entropy(Steam,h=h_12,P=P_3)
{point 13}
s_12=s_13s
h_13s=enthalpy(Steam,s=s_13s,P=P_c)
eta_turbine*(h_12-h_13s)=(h_12-h_13)
s_13=entropy(Steam,h=h_13,P=P_c)
{Energy balance on CFWH2}
m_1*h_10+(1)*h_5=m_1*h_14+h_6
{Energy balance on OFWH}
m_2*h_11+m_1*h_15+(1-m_1-m_2)*h_3=h_4
{Energy balance on CFWH1}
m_3*h_12+(1-m_1-m_2)*h_2=m_3*h_16+(1-m_1-m_2)*h_3

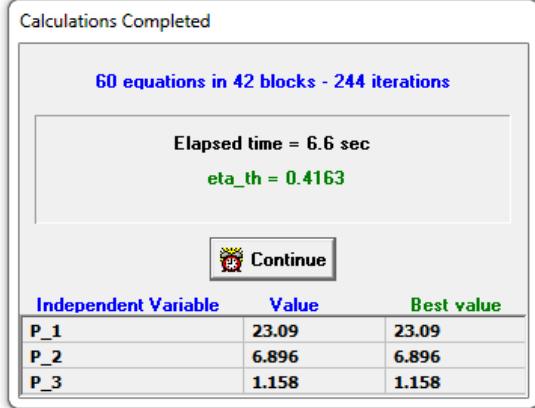
```

```

{outputs}
w_p1=(1-m_1-m_2)*(h_2-h_1)
w_p2=h_5-h_4
w_t=(h_7-h_8)+(h_9-h_10)+(1-m_1)*(h_10-h_11)+(1-m_1-m_2)*(h_11-h_12)+(1-m_1-m_2-m_3)*(h_12-h_13)
w_net=w_t-(w_p1+w_p2)
Q_add=(h_7-h_6)+(h_9-h_8)
eta_th=w_net/Q_add

```

| Variable | Guess | Lower | Upper |
|----------|-------|-------|----------|
| P_1 | 30 | P_2 | p_reheat |
| P_2 | 6 | P_3 | P_1 |
| P_3 | 3 | P_c | P_2 |



Optimum OFWH pressure = 6.8bar

Optimum CFWH1 pressure = 23.09 bar

Optimum CFWH2 pressure = 1.158 bar

Max. thermal efficiency = 0.4163 bar

Results Tab

Unit Settings: SI C bar kJ mass deg

Maximization of eta_th(P_1,P_2,P_3) = 0.4163 244 iterations: Variable Metric method

| | | | |
|-----------------------------|-----------------------------|--------------------------------|-------------------|
| $\eta_{\text{pump}} = 0.95$ | $\eta_{\text{th}} = 0.4163$ | $\eta_{\text{turbine}} = 0.85$ | $h_1 = 191.8$ |
| $h_{13} = 2429$ | $h_{13s} = 2372$ | $h_{14} = 942.5$ | $h_{15} = 942.5$ |
| $h_5 = 711$ | $h_{5s} = 710.2$ | $h_6 = 918.6$ | $h_7 = 3311$ |
| $P_1 = 23.09$ | $P_2 = 6.896$ | $P_3 = 1.158$ | $P_b = 150$ |
| $s_{11} = 7.339$ | $s_{11s} = 7.247$ | $s_{12} = 7.485$ | $s_{12s} = 7.339$ |
| $s_8 = 6.463$ | $s_{8s} = 6.348$ | $s_9 = 7.228$ | $T_{16} = 103.8$ |

| | | |
|-----------------------------|-------------------------|-------------------|
| $h_{11s} = 3026$ | $h_{12} = 2751$ | $h_{12s} = 2693$ |
| $h_{2s} = 192.5$ | $h_3 = 433.7$ | $h_4 = 694.4$ |
| $m_1 = 0.08531$ | $m_2 = 0.08214$ | $m_3 = 0.08672$ |
| $s_1 = 0.6492$ | $s_{10} = 7.247$ | $s_{10s} = 7.228$ |
| $s_4 = 1.986$ | $s_{5s} = 1.986$ | $s_7 = 6.348$ |
| $T_{\text{sat},14} = 219.8$ | $w_{\text{net}} = 1205$ | $w_{p1} = 0.6016$ |

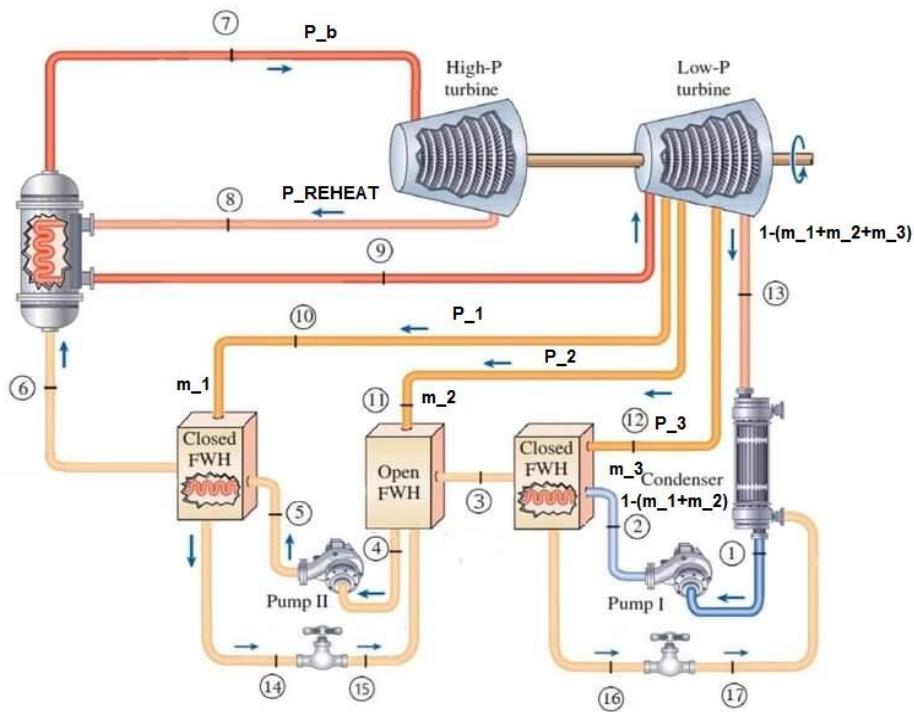
| | 1 1..10 | η_{th} | 2 | P ₁ | 3 | P ₂ | 4 | P ₃ |
|--------|------------|-------------|---|----------------|---|----------------|---|----------------|
| Run 1 | | 0.4053 | | 30 | | 20 | | 6 |
| Run 2 | | 0.4067 | | 26.7 | | 17.8 | | 5.344 |
| Run 3 | | 0.408 | | 23.4 | | 15.6 | | 4.689 |
| Run 4 | | 0.4092 | | 20.1 | | 13.4 | | 4.033 |
| Run 5 | | 0.4103 | | 16.8 | | 11.2 | | 3.378 |
| Run 6 | | 0.4111 | | 13.5 | | 9 | | 2.722 |
| Run 7 | | 0.4113 | | 10.2 | | 6.8 | | 2.067 |
| Run 8 | | 0.4104 | | 6.9 | | 4.6 | | 1.411 |
| Run 9 | | 0.4064 | | 3.6 | | 2.4 | | 0.7556 |
| Run 10 | | 0.3796 | | 0.3 | | 0.2 | | 0.1 |

| | 1 1..10 | η_{th} | 2 | P ₁ | 3 | P ₂ | 4 | P ₃ |
|--------|------------|-------------|---|----------------|---|----------------|---|----------------|
| Run 1 | | 0.4032 | | 30 | | 20 | | 7 |
| Run 2 | | 0.4048 | | 27.78 | | 18.33 | | 6.233 |
| Run 3 | | 0.4065 | | 25.56 | | 16.67 | | 5.467 |
| Run 4 | | 0.4081 | | 23.33 | | 15 | | 4.7 |
| Run 5 | | 0.4098 | | 21.11 | | 13.33 | | 3.933 |
| Run 6 | | 0.4114 | | 18.89 | | 11.67 | | 3.167 |
| Run 7 | | 0.4129 | | 16.67 | | 10 | | 2.4 |
| Run 8 | | 0.414 | | 14.44 | | 8.333 | | 1.633 |
| Run 9 | | 0.4141 | | 12.22 | | 6.667 | | 0.8667 |
| Run 10 | | 0.407 | | 10 | | 5 | | 0.1 |

| | 1 1..10 | η_{th} | 2 | P ₁ | 3 | P ₂ | 4 | P ₃ |
|--------|------------|-------------|---|----------------|---|----------------|---|----------------|
| Run 1 | | 0.3967 | | 30 | | 20 | | 10 |
| Run 2 | | 0.3989 | | 27.56 | | 18.33 | | 8.9 |
| Run 3 | | 0.4011 | | 25.11 | | 16.67 | | 7.8 |
| Run 4 | | 0.4033 | | 22.67 | | 15 | | 6.7 |
| Run 5 | | 0.4055 | | 20.22 | | 13.33 | | 5.6 |
| Run 6 | | 0.4078 | | 17.78 | | 11.67 | | 4.5 |
| Run 7 | | 0.41 | | 15.33 | | 10 | | 3.4 |
| Run 8 | | 0.412 | | 12.89 | | 8.333 | | 2.3 |
| Run 9 | | 0.413 | | 10.44 | | 6.667 | | 1.2 |
| Run 10 | | 0.4051 | | 8 | | 5 | | 0.1 |

| | 1 1..10 | η_{th} | 2 | P ₁ | 3 | P ₂ | 4 | P ₃ |
|--------|------------|-------------|---|----------------|---|----------------|---|----------------|
| Run 1 | | 0.4032 | | 30 | | 20 | | 7 |
| Run 2 | | 0.4048 | | 27.11 | | 18 | | 6.233 |
| Run 3 | | 0.4064 | | 24.22 | | 16 | | 5.467 |
| Run 4 | | 0.4079 | | 21.33 | | 14 | | 4.7 |
| Run 5 | | 0.4094 | | 18.44 | | 12 | | 3.933 |
| Run 6 | | 0.4107 | | 15.56 | | 10 | | 3.167 |
| Run 7 | | 0.4118 | | 12.67 | | 8 | | 2.4 |
| Run 8 | | 0.4123 | | 9.778 | | 6 | | 1.633 |
| Run 9 | | 0.4116 | | 6.889 | | 4 | | 0.8667 |
| Run 10 | | 0.4046 | | 4 | | 2 | | 0.1 |

Flow Diagram



Duplicate code:

{Givens}

P_c=0.1[bar] (compressor pressure)
P_b=150[bar] (boiler pressure)
T_max=500 (max temperature)
eta_t=0.85 (turbine eff)
eta_p=0.95 (pump eff)
P_r=30.51[bar]

{Point 1}

h_1=ENTHALPY(Steam,x=0,P=P_c)
s_1=ENTROPY(Steam,x=0,P=P_c)
s_2s=s_1

Duplicate i=1,5

P_1[i]=(P_c)+(i-1)*(P_r-P_c)/5

{Point 10}

h_10s[i]=ENTHALPY(Steam,s=s_10s,P=P_1[i])
h_10[i]=h_9-((h_9-h_10s[i])*eta_t)
s_10[i]=ENTROPY(Steam,h=h_10[i],P=P_1[i])

{Point 14}

h_14[i]=ENTHALPY(Steam,x=0,P=P_1[i])
s_14[i]=ENTROPY(Steam,x=0,P=P_1[i])
T_14[i]=TEMPERATURE(Steam,x=0,P=P_1[i])

{point15}

h_15[i]=h_14[i]

{Point 6}

T_6[i]=T_14[i]

h_6[i]=ENTHALPY(Steam,T=T_14[i],P=P_b)

q_add[i]=(h_7-h_6[i])+(h_9-h_8)

Duplicate j=1,5

P_2[j,i]=(P_c)+(j-1)*(P_1[i]-P_c)/5

{Point 11}

s_11s[j,i]=s_10[i]
h_11s[j,i]=ENTHALPY(Steam,s=s_11s[j,i],P=P_2[j,i])
h_11[j,i]=h_10[i]-(eta_t*(h_10[i]-h_11s[j,i]))
s_11[j,i]=ENTROPY(Steam,h=h_11[j,i],P=P_2[j,i])

{Point 2}

h_2s[j,i]=ENTHALPY(Steam,s=s_2s,P=P_2[j,i])

h_2[j,i]=((h_2s[j,i]-h_1)/eta_p)+h_1

{Point 4}

h_4[j,i]=ENTHALPY(Steam,x=0,P=P_2[j,i])

s_4[j,i]=ENTROPY(Steam,x=0,P=P_2[j,i])

{Point 5}

s_5s[j,i]=s_4[j,i]

h_5s[j,i]=ENTHALPY(Steam,s=s_5s[j,i],P=P_b)

h_5[j,i]=((h_5s[j,i]-h_4[j,i])/eta_p)+h_4[j,i]

{Energy balance on CFWH1}

$$m_1[j,i] = (h_6[i]-h_5[j,i])/(h_{10}[i]-h_{14}[i])$$

Duplicate k=1,5

$$P_3[k,j,i] = (P_c) + (k-1)*(P_2[j,i]-P_c)/5$$

{Point 12}

$$s_{12s}[k,j,i] = s_{11}[j,i]$$

$$h_{12s}[k,j,i] = \text{ENTHALPY}(\text{Steam}, s=s_{12s}[k,j,i], P=P_3[k,j,i])$$

$$h_{12}[k,j,i] = h_{11}[j,i] - (\eta_t * (h_{11}[j,i] - h_{12s}[k,j,i]))$$

$$s_{12}[k,j,i] = \text{ENTROPY}(\text{Steam}, h=h_{12}[k,j,i], P=P_3[k,j,i])$$

{Point 13}

$$s_{13s}[k,j,i] = s_{12}[k,j,i]$$

$$h_{13s}[k,j,i] = \text{ENTHALPY}(\text{Steam}, s=s_{13s}[k,j,i], P=P_c)$$

$$h_{13}[k,j,i] = h_{12}[k,j,i] - (\eta_t * (h_{12}[k,j,i] - h_{13s}[k,j,i]))$$

{Point 16}

$$h_{16}[k,j,i] = \text{ENTHALPY}(\text{Steam}, x=0, P=P_3[k,j,i])$$

$$T_{16}[k,j,i] = \text{TEMPERATURE}(\text{steam}, x=0, P=P_3[k,j,i])$$

{Point 17}

$$h_{17}[k,j,i] = h_{16}[k,j,i]$$

{Point 3}

$$T_3[k,j,i] = T_{16}[k,j,i]$$

$$h_3[k,j,i] = \text{ENTHALPY}(\text{Steam}, T=T_3[k,j,i], P=P_2[j,i])$$

{Energy balance on OFWH}

$$m_2[k,j,i] = (h_4[j,i]-h_3[k,j,i]+(m_1[j,i]*(h_3[k,j,i]-h_{15}[i])))/(h_{11}[j,i]-h_3[k,j,i])$$

{Energy balance on CFWH2}

$$m_3[k,j,i] = (1-m_1[j,i]-m_2[k,j,i])*(h_2[j,i]-h_3[k,j,i])/(h_{16}[k,j,i]-h_{12}[k,j,i])$$

{Outputs}

$$w_t[k,j,i] = (h_7-h_8)+(h_9-h_{10}[i])+(1-m_1[j,i])*(h_{10}[i]-h_{11}[j,i])+(1-m_1[j,i]-m_2[k,j,i])*(h_{11}[j,i]-h_{12}[k,j,i])+(1-m_1[j,i]-m_2[k,j,i]-m_3[k,j,i])*(h_{12}[k,j,i]-h_{13}[k,j,i])$$

$$w_p[k,j,i] = (1-m_1[j,i]-m_2[k,j,i])*(h_2[j,i]-h_1)+(h_5[j,i]-h_4[j,i])$$

$$\eta_{\text{thermal}}[k,j,i] = (w_t[k,j,i]-w_p[k,j,i])/q_{\text{add}}[i]$$

End

End

End

{Point 9}

$$h_9 = \text{ENTHALPY}(\text{Steam}, T=T_{\max}, P=P_r)$$

$$s_9 = \text{ENTROPY}(\text{Steam}, T=T_{\max}, P=P_r)$$

$$s_{10s} = s_9$$

$$h_7 = \text{ENTHALPY}(\text{Steam}, T=T_{\max}, P=P_b)$$

$$s_7 = \text{ENTROPY}(\text{Steam}, T=T_{\max}, P=P_b)$$

{Point 8}

$s_{8s}=s_7$

$h_{8s}=\text{ENTHALPY}(\text{Steam}, s=s_{8s}, P=P_r)$

$\eta_t = (h_7 - h_{8s}) / (h_7 - h_8)$

$s_8 = \text{ENTROPY}(\text{Steam}, h=h_8, P=P_r)$

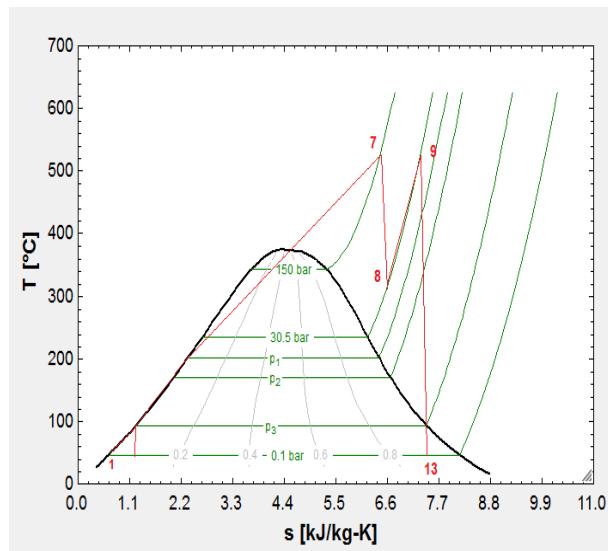
{Point 1}

$h_1 = \text{ENTHALPY}(\text{Steam}, x=0, P=P_c)$

$s_1 = \text{ENTROPY}(\text{Steam}, x=0, P=P_c)$

$s_{2s}=s_1$

T-s Diagram



Conclusion

| | |
|------------------------|--------|
| max thermal efficiency | 0.4167 |
|------------------------|--------|

D.4 One OFWH and three CFWHs were added to the reheat cycle

After the Reheat Pressure

Code

| | |
|----------------|----------------|
| P_b=150 | P_open=P_12 |
| P_c=0.1 | P_open=P_17 |
| T_max=500 | P_open=P_4 |
| eta_t=0.85 | P_open=P_5 |
| eta_p=0.95 | P_open=P_2 |
| T_8=T_max | P_open=P_3 |
| C_p=4.18 | P_closed2=P_13 |
| P_reheat=30.51 | P_closed2=P_18 |
| P_b=P_7 | P_closed1=P_14 |
| P_b=P_8 | P_closed1=P_19 |
| P_b=P_6 | P_closed1=P_20 |
| P_reheat=P_9 | P_c=P_21 |
| P_reheat=P_10 | P_c=P_1 |
| P_closed3=P_11 | |
| P_closed3=P_16 | P_c=P_15 |

“point1 from condenser”

$H_1 = \text{enthalpy}(\text{Steam}, x=0, P=P_c)$

$S_1 = \text{entropy}(\text{Steam}, x=0, P=P_c)$

“point 2 to closed FWH_1”

$H_{2s} = H_1 + 0.1 * (P_2 - P_1)$

$\eta_p * (H_{2s} - H_1) = (H_{2s} - H_1)$

“point 3 from CFWH_1 to CFWH_2”

$T_3 = T_{20}$

$H_3 = T_3 * C_p$

“point 4 from CFWH_2 to OFWH”

$T_4 = T_{18}$

$H_4 = C_p * T_4$

“point 5 out of OFWH”

$H_5 = \text{enthalpy}(\text{Steam}, x=0, P=P_{\text{open}})$

$S_5 = \text{entropy}(\text{Steam}, x=0, P=P_{\text{open}})$

“point 6 pumped to CFWH_3”

$H_{6s} = H_5 + 0.1 * (P_6 - P_5)$

$\eta_p * (H_{6s} - H_5) = (H_{6s} - H_5)$

“point 7 to boiler”

$T_7 = T_{16}$

$H_7 = C_p * T_7$

“point 8 from boiler”

$H_8 = \text{enthalpy}(\text{Steam}, T=T_{\max}, P=P_b)$

$S_8 = \text{entropy}(\text{Steam}, T=T_{\max}, P=P_b)$

“point 9 to be reheated”

$H_{9s} = \text{enthalpy}(\text{Steam}, s=S_8, P=P_{\text{reheat}})$

$\eta_{\text{t}} * (H_{9s} - H_8) = (H_9 - H_8)$

“point 10 to LPT”

$H_{10} = \text{enthalpy}(\text{Steam}, T=T_{\max}, P=P_{\text{reheat}})$

$S_{10} = \text{entropy}(\text{Steam}, T=T_{\max}, P=P_{\text{reheat}})$

“point 11 from LPT to CFWH_3”

$H_{11s} = \text{enthalpy}(\text{Steam}, s=S_{10}, P=P_{\text{closed3}})$

$\eta_{\text{t}} * (H_{11s} - H_{10}) = (H_{11} - H_{10})$

$S_{11} = \text{entropy}(\text{Steam}, h=H_{11}, P=P_{\text{closed3}})$

“point 12 from LPT to open”

$H_{12s} = \text{enthalpy}(\text{Steam}, s=S_{11}, P=P_{\text{open}})$

$\eta_{\text{t}} * (H_{12s} - H_{11}) = (H_{12} - H_{11})$

$S_{12} = \text{entropy}(\text{Steam}, h=H_{12}, P=P_{\text{open}})$

“point 13 from LPT to CFWH_2”

$H_{13s} = \text{enthalpy}(\text{Steam}, s=S_{12}, P=P_{\text{closed2}})$

$\eta_{\text{t}} * (H_{13s} - H_{12}) = (H_{13} - H_{12})$

$S_{13} = \text{entropy}(\text{Steam}, h=H_{13}, P=P_{\text{closed2}})$

“point 14 from LPT to closed CFWH_1”

$H_{14s} = \text{enthalpy}(\text{Steam}, s=S_{13}, P=P_{\text{closed}1})$

$\eta_{\text{t}}(H_{14s} - H_{13}) = (H_{14} - H_{13})$

$S_{14} = \text{entropy}(\text{Steam}, h=H_{14}, P=P_{\text{closed}1})$

“point 15 to condenser”

$H_{15s} = \text{enthalpy}(\text{Steam}, s=S_{14}, P=P_c)$

$\eta_{\text{t}}(H_{15s} - H_{14}) = (H_{15} - H_{14})$

“point 16 out from closed FWH_3”

$H_{16} = \text{enthalpy}(\text{Steam}, x=0, P=P_{\text{closed}3})$

$S_{16} = \text{entropy}(\text{Steam}, x=0, P=P_{\text{closed}3})$

$T_{16} = \text{temperature}(\text{Steam}, x=0, P=P_{\text{closed}3})$

“point 17 throatled to OFWH”

$H_{16} = H_{17}$

“point 18 out from CFWH_2”

$H_{18} = \text{enthalpy}(\text{Steam}, x=0, P=P_{\text{closed}2})$

$S_{18} = \text{entropy}(\text{Steam}, x=0, P=P_{\text{closed}2})$

$T_{18} = \text{temperature}(\text{Steam}, x=0, P=P_{\text{closed}2})$

“point 19 throatled to CFWH_1”

$H_{19} = H_{18}$

“point 20 out from CFWH_1”

$H_{20} = \text{enthalpy}(\text{Steam}, x=0, P=P_{\text{closed}1})$

$S_{20} = \text{entropy}(\text{Steam}, x=0, P=P_{\text{closed}1})$

$T_{20} = \text{temperature(Steam, } x=0, P=P_{\text{closed1}})$

“point 21 throatled to condenser”

$H_{20}=H_{21}$

“energy balance”

$$(m_1*H_{11}) + H_6 = (m_1*H_{16}) + H_7$$

$$(m_2*H_{12}) + (m_1*H_{17}) + (1 - m_1 - m_2)*H_4 = H_5$$

$$(m_3 *H_{13}) + ((1 - m_1 - m_2)*H_3) = ((1 - m_1 - m_2)*H_4) + (m_3 *H_{18})$$

$$(m_4*H_{14}) + (m_3*H_{19}) + (1 - m_1 - m_2)*H_2 = (m_4 + m_3)*H_{20} + (1 - m_1 - m_2)*H_3$$

“Energies”

$$q_{\text{add}} = (H_8 - H_7) + (H_{10} - H_9)$$

$$w_t = (H_8 - H_9) + (H_{10} - H_{11}) + (1 - m_1)*(H_{11} - H_{12}) + (1 - m_1 - m_2)*(H_{12} - H_{13}) + (1 - m_1 - m_2 - m_3)*(H_{13} - H_{14}) + (1 - m_1 - m_2 - m_3 - m_4)*(H_{14} - H_{15})$$

$$w_p = (H_6 - H_5) + (1 - m_1 - m_2)*(H_2 - H_1)$$

$$w_{\text{net}} = w_t - w_p$$

$$\eta_{\text{th}} = w_{\text{net}} / q_{\text{add}}$$

| Variable Information | | | | | | | |
|----------------------|-------|-----------|-----------|---------|-------|-----------|-----|
| Variable | Guess | Lower | Upper | Display | Units | Alt Units | Key |
| P_closed1 | 1 | P_c | P_closed2 | A 0 N | | | |
| P_closed2 | 1 | P_closed1 | P_open | A 0 N | | | |
| P_closed3 | 30 | P_open | P_reheat | A 0 N | | | |
| P_open | 20 | P_closed2 | P_closed3 | A 0 N | | | |

OK Apply Print Update Cancel

Calculations Completed

84 equations in 61 blocks - 596 iterations

Elapsed time = 23.8 sec

eta_th = 0.4204



| Independent Variable | Value | Best value |
|----------------------|--------|------------|
| P_closed1 | 0.7589 | 0.7589 |
| P_closed2 | 3.23 | 3.23 |
| P_closed3 | 30.51 | 30.51 |
| P_open | 13.59 | 13.59 |

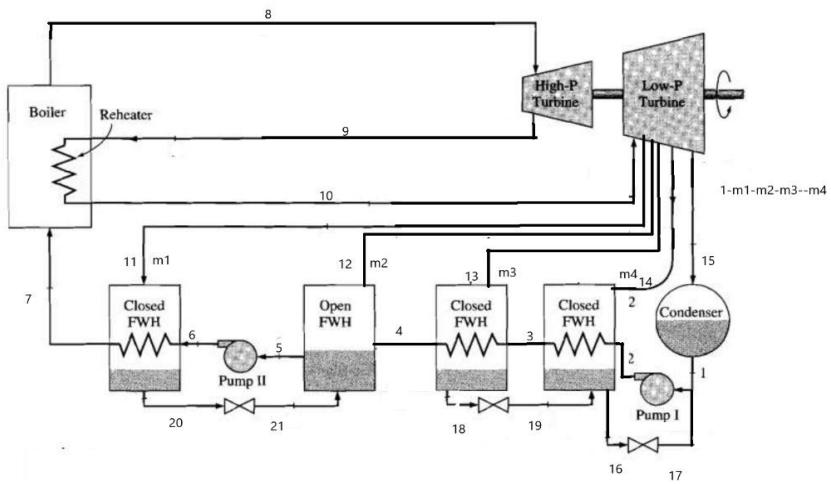
Unit Settings: SI C bar kJ mass deg

Maximization of eta_th(P_closed1,P_closed2,P_closed3,P_open) = 0.4204 574 iterations: Variable Metric method

| | | | | | |
|------------------------|-----------------------|-----------------------|----------------------|----------------------|-------------------|
| C_p = 4.18 | $\eta_p = 0.95$ | $\eta_t = 0.85$ | $\eta_{th} = 0.4204$ | $H_1 = 191.8$ | $H_{10} = 3457$ |
| $H_{11} = 3457$ | $H_{11s} = 3457$ | $H_{12} = 3238$ | $H_{12s} = 3199$ | $H_{13} = 2925$ | $H_{13s} = 2870$ |
| $H_{14} = 2684$ | $H_{14s} = 2641$ | $H_{15} = 2427$ | $H_{15s} = 2382$ | $H_{16} = 1013$ | $H_{17} = 1013$ |
| $H_{18} = 572.6$ | $H_{19} = 572.6$ | $H_2 = 193.2$ | $H_{20} = 384$ | $H_{21} = 384$ | $H_{2s} = 193.2$ |
| $H_3 = 383.1$ | $H_4 = 569.1$ | $H_5 = 824.1$ | $H_6 = 838.5$ | $H_{6s} = 837.8$ | $H_7 = 981.4$ |
| $H_8 = 3311$ | $H_9 = 2954$ | $H_{9s} = 2891$ | $m_1 = 0.05848$ | $m_2 = 0.08586$ | $m_3 = 0.06766$ |
| $m_4 = 0.06508$ | $P_1 = 0.1$ | $P_{10} = 30.51$ | $P_{11} = 30.51$ | $P_{12} = 13.61$ | $P_{13} = 3.237$ |
| $P_{14} = 0.7468$ | $P_{15} = 0.1$ | $P_{16} = 30.51$ | $P_{17} = 13.61$ | $P_{18} = 3.237$ | $P_{19} = 0.7468$ |
| $P_2 = 13.61$ | $P_{20} = 0.7468$ | $P_{21} = 0.1$ | $P_3 = 13.61$ | $P_4 = 13.61$ | $P_5 = 13.61$ |
| $P_6 = 150$ | $P_7 = 150$ | $P_8 = 150$ | $P_9 = 30.51$ | $P_b = 150$ | $P_c = 0.1$ |
| $P_{closed1} = 0.7468$ | $P_{closed2} = 3.237$ | $P_{closed3} = 30.51$ | $P_{open} = 13.61$ | $P_{reheat} = 30.51$ | $q_{add} = 2832$ |
| $S_1 = 0.6492$ | $S_{10} = 7.228$ | $S_{11} = 7.228$ | $S_{12} = 7.287$ | $S_{13} = 7.399$ | $S_{14} = 7.515$ |
| $S_{16} = 2.654$ | $S_{18} = 1.699$ | $S_{20} = 1.212$ | $S_5 = 2.271$ | $S_8 = 6.348$ | $T_{16} = 234.8$ |
| $T_{18} = 136.1$ | $T_{20} = 91.64$ | $T_3 = 91.64$ | $T_4 = 136.1$ | $T_7 = 234.8$ | $T_8 = 500$ |
| $T_{max} = 500$ | $w_{net} = 1190$ | $w_p = 15.57$ | $w_t = 1206$ | | |

| | |
|--------------------------------|-------------------|
| Optimum pressure CFWH 1 | 0.7468 Bar |
| Optimum pressure CFWH 2 | 3.237 Bar |
| Optimum pressure CFWH 3 | 30.51 Bar |
| Optimum pressure OFWH | 13.61 Bar |
| Max thermal efficiency | 42.04% |

Flow Diagram



T-s Diagram

Figure 81: Arrays table tab for maximum thermal efficiency

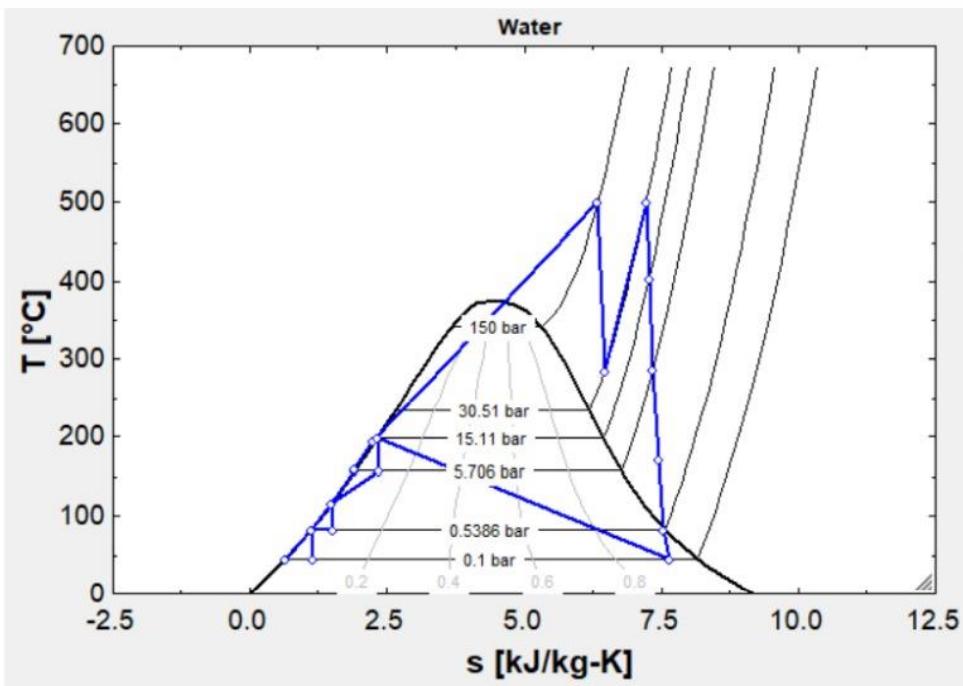


Figure 82: T-s Diagrams for this case of optimized process values

Another soln using for loop in matlab

Code

```
clc,clear ;
addpath("steam");

%%%%%%%%%%%%% the givens %%%%%%
Pb = 150 ; Pc = 0.1 ; Tmax = 500; etaT = 0.85; etaP = 0.95; Cp = 4.18; Pr =
30.53 ; x= 0;

st=.5;

format short;

%constant

%point 1
[h1,s1,P1] = point_1(Pc,x);

%point 8,9,10

[P8,h8,T8,s8,P9,h9s,h9,s9s,P10,h10,T10,s10]= point8_9_10 (Tmax,Pb,Pr,etaT);

%%%%%%%%%%%%% the for loop %%%%%%
r=1;

for i=Pc:st:5%Pr
    P4f=i;
    u=1;
    for ii=(P4f+.01):st:10%Pr-.01)
        P3f=ii;
        o=1;
        for iii=(P3f+.01):st:20%(Pr-.02)
            P2f=iii;
            g=1;

            for iiii=(P2f+.01):st:Pr%(Pr-.03)
                P1f=iiii;
                %point 20,7
                [h20,T20,T7,h7,h21] = point20_7(P1f,x,Cp);

                %point 2
                [h2s,h2,h5,h6s,h6] = point_2 (P2f,Pb,h1,etaP,x,P1);

                %point 16,3
                [h16,T16,h3,T3,h17] = Point_163(P4f,x,Cp);

                %point 18,4
```

```

[h18,T18,T4,h4,h19]= point_18_4(x,Cp,P3f);

%point 11,12,13,14,15
[h11s,h11,h12s,h12,h13s,h13,h14s,h14,h15s,h15] =
point_11(s10,h10,etaT,Pc,P1f,P4f);

%mass balance
[A,B,m1,m2,m3,m4] = mass_balance
(h2,h3,h4,h5,h6,h7,h11,h12,h13,h14,h16,h18,h19,h20,h21);

%q,w calcs
[Qrej(g,:),Qadd(g,:),Wt(g,:),Wp(g,:),Wnet(g,:)] = calc_QW
(h1,h2,h5,h6,h7,h8,h9,h10,h11,h12,h13,h14,h15,h17,m1,m2,m3,m4);

% efficiency
eta(g,:) = Wnet(g,:)/Qadd(g,:);
P_4_f(g,:)=P4f;
P_1_f(g,:)=P1f;

P_2_f(g,:)=P2f;

P_3_f(g,:)=P3f;
g=g+1;
sol=[eta,Wnet,Qadd,Qrej,Wt,Wp,P_4_f,P_3_f,P_2_f,P_1_f];
end

[best3(o,:),n]=max(eta);
best_sol3(o,:)=sol(n,:);
o=o+1;
sol=0;
P_4_f=0;
P_3_f=0;
P_2_f=0;
P_1_f=0;
Qrej=0;
eta=0;
Qadd=0;
Wt=0;
Wp=0;
Wnet=0;
end
P_4_f;
[best2(u,:),n]=max(best3);
best_sol2(u,:)=best_sol3(n,:);
u=u+1;
best_sol3=[0 0 0 0 0 0 0 0 0 0];
best3=0;
best3=0;
end

% h=1;
% [best_sol] = best_sol(Wnet,Qadd,Qrej,P_1_f,P_2_f,P_3_f,P_4_f,eta);
% best=best_sol;

[best(r,:),n]=max(best2);

```

```

best_sol(r,:)=best_sol2(n,:);
r=r+1;
sol=0;
best_sol2=[0 0 0 0 0 0 0 0 0];
best_sol3=[0 0 0 0 0 0 0 0 0];
best2=0;
end
%%%%%%%%%%%%%%%
figure(1)

plot(best_sol(:,7),best_sol(:,1),'red');
title('\'\eta_{th}', 'FontSize', 14, 'FontWeight', 'bold');
xlabel('FWH_1_{(bar)}', 'FontSize', 12, 'FontWeight', 'bold') ;
ylabel('\'\eta_{th} _{(rad)}', 'FontSize', 12, 'FontWeight', 'bold') ;
grid on;
grid minor;
saveas(gcf,'eta_vs_fwh_1.tiff');
%%%%%%%%%%%%%%%

figure(2)

plot((best_sol(:,2)/1000),best_sol(:,1),'red');
title('\'\eta_{th}&_W_n_e_t', 'FontSize', 14, 'FontWeight', 'bold');
xlabel('W_n_e_t_{(MW)}', 'FontSize', 12, 'FontWeight', 'bold') ;
ylabel('\'\eta_{th}', 'FontSize', 12, 'FontWeight', 'bold') ;
grid on;
grid minor;
saveas(gcf,'eta_vs_W_NET.tiff');
%%%%%%%%%%%%%%%

figure(3)

plot(best_sol(:,7),best_sol(:,2),'red');
title('W_n_e_t_{MW}', 'FontSize', 14, 'FontWeight', 'bold');
xlabel('FWH_1_{(bar)}', 'FontSize', 12, 'FontWeight', 'bold') ;
ylabel('W_n_e_t_{MW}', 'FontSize', 12, 'FontWeight', 'bold') ;
grid on;
grid minor;
saveas(gcf,'WORK_vs_fwh_1.tiff');

%%%%%%%%%%%%%% the excel sheet %%%%%%%%
excel=table(best_sol(:,1),best_sol(:,2),best_sol(:,3),best_sol(:,4),best_sol(:,5),best_sol(:,6),best_sol(:,7),best_sol(:,8),best_sol(:,9),best_sol(:,10));
varNames={'eta','Wnet','Qadd','Qrej','Wt','Wp','P_4_f','P_3_f','P_2_f','P_1_f'};
excel.Properties.VariableNames = varNames;

filename = 'the table.xlsx';

writetable(excel,filename);
%%%%%%%%%%%%%% functions %%%%%%%%

```

```

function [best]=etab(eta)
best=max(eta);
end

function [h,s,Pout] = point_1(Pin,x)
Pout = Pin;
h = XSteam('h_px',Pin,x);
s = XSteam('s_ph',Pin,h);
end

function [h2s,h2,h5,h6s,h6] = point_2 (P2f,Pb,h1,etaP,x,P1)

h2s = h1 +0.1*(P2f-P1);
h2 = h1+ (h2s-h1)/etaP;

h5 = XSteam('h_px',P2f ,x);
h6s = h5 +0.1*(Pb - P2f);
h6 = h5 + (h6s -h5)/etaP;
end

function [h18,T18,T4,h4,h19]= point_18_4 (x,Cp,P3f)

h18 = XSteam('h_px',P3f,x);
T18 = XSteam('Tsat_p',P3f);

%point4
T4 = T18;
h4 = Cp*T4;

%point19
h19= h18;
end

function [h16,T16,h3,T3,h17] = Point_163(P4f,x,Cp)

h16 = XSteam('h_px',P4f,x);
T16 = XSteam('Tsat_p',P4f);

%point3
T3 = T16 ;
h3 = Cp*T3 ;

%point 17
h17 = h16 ;

end

function [P8,h8,T8,s8,P9,h9s,h9,s9s,P10,h10,T10,s10]= point8_9_10
(Tmax,Pb,Pr,etaT)

```

```

%point 8
P8 = Pb ; T8 = Tmax;
h8 = XSteam('h_pt',P8 ,T8);
s8 = XSteam('s_pT',P8 ,T8);

%point 9
P9 = Pr ; s9s = s8;
h9s = XSteam('h_ps',P9 ,s9s);
h9 = h8-(h8-h9s)*etaT;

%point 10
P10 = Pr ; T10 = Tmax;
h10 = XSteam('h_pt',P10 ,T10);
s10 = XSteam('s_pT',P10 ,T10);
end

function [h20,T20,T7,h7,h21] = point20_7(P1f,x,Cp)

h20 = XSteam('h_px',P1f,x);
T20 = XSteam('Tsat_p',P1f);
%point 7
T7 = T20;
h7 = T7*Cp;

%point 21
h21= h20;
end

function [h11s,h11,h12s,h12,h13s,h13,h14s,h14,h15s,h15] =
point_11(s10,h10,etaT,Pc,P1f,P4f)

h11s = XSteam('h_ps',P1f,s10);
h11 = h10-(h10-h11s)*etaT;
s11 = XSteam('s_ph',P1f,h11);

%point 12

h12s = XSteam('h_ps',P1f,s11);
h12 = h11-(h11-h12s)*etaT;
s12 = XSteam('s_ph',P1f,h12);

%point 13

h13s = XSteam('h_ps',P1f ,s12);
h13 = h12 -(h12 -h13s)*etaT;
s13 = XSteam('s_ph',P1f,h13);

%point14

h14s = XSteam('h_ps',P4f ,s13);
h14 = h13 -(h13 -h14s)*etaT;
s14 = XSteam('s_ph',P1f,h14);

```

```

%point15

h15s = XSteam('h_ps',Pc ,s14);
h15 = h14 -(h14 -h15s)*etaT;
end

function [A,B,m1,m2,m3,m4] = mass_balance
(h2,h3,h4,h5,h6,h7,h11,h12,h13,h14,h16,h18,h19,h20,h21)

A = [(h11-h20) 0 0 0 ; (h21-h4) (h12-h4) 0 0 ; (h4-h3) (h4-h3) (h13-h18) 0 ;
(h3-h2) (h3-h2) (h19-h16) (h14-h16)];
B = [(h7-h6) ;(h5-h4) ;(h4-h3) ;(h3-h2)];
N = A\B;%inv(A) * B;
m1 = N(1);
m2 = N(2);
m3 = N(3);
m4 = N(4);

m5 = 1-(m1+m2+m3+m4); % to the condenser
end

function [Qrej,Qadd,Wt,Wp,Wnet] = calc_QW
(h1,h2,h5,h6,h7,h8,h9,h10,h11,h12,h13,h14,h15,h17,m1,m2,m3,m4)
%q
Qrej = (m3+m4)*h17 +(1-m1-m2-m3-m4)*h15 - (1-m1-m2)*h1;
Qadd = (h8-h7)+(h10-h9);

%work
Wt = (h8-h9)+(h10-h11)+(1-m1)*(h11-h12)+(1-m1-m2)*(h12-h13)+(1-m1-m2-
m3)*(h13-h14)+(1-m1-m2-m3-m4)*(h14-h15);
Wp = (1-m1-m2)*(h2-h1) + (h6-h5);
Wnet = Wt-Wp;
end

```

solution

| Workspace | |
|-----------|----------------------------|
| Name | Value |
| A | 4x4 double |
| B | [60.6104;159.4701;123...] |
| best | [0.5527;0.5201;0.5061;...] |
| best2 | 0 |
| best3 | 0 |
| best_sol | 10x10 double |
| best_sol2 | [0,0,0,0,0,0,0,0,0] |
| best_sol3 | [0,0,0,0,0,0,0,0,0] |
| Cp | 4.1800 |
| eta | 0 |
| etaP | 0.9500 |
| etaT | 0.8500 |
| excel | 10x10 table |
| filename | 'the table.xlsx' |
| g | 23 |
| h1 | 191.8123 |
| h10 | 3.4565e+03 |
| h11 | 3.4526e+03 |

| Workspace | |
|-----------|------------|
| Name | Value |
| h11s | 3.4519e+03 |
| h12 | 3.4526e+03 |
| h12s | 3.4526e+03 |
| h13 | 3.4526e+03 |
| h13s | 3.4526e+03 |
| h14 | 2.9989e+03 |
| h14s | 2.9189e+03 |
| h15 | 2.2119e+03 |
| h15s | 2.0730e+03 |
| h16 | 626.7299 |
| h17 | 626.7299 |
| h18 | 755.0856 |
| h19 | 755.0856 |
| h2 | 193.8670 |
| h20 | 1.0095e+03 |
| h21 | 1.0095e+03 |
| h2s | 193.7643 |
| h3 | 621.6528 |

| Workspace | |
|-----------|------------|
| Name | Value |
| h4 | 744.7264 |
| h5 | 904.1965 |
| h6 | 917.9207 |
| h6s | 917.2345 |
| h7 | 978.5311 |
| h8 | 3.3108e+03 |
| h9 | 2.9543e+03 |
| h9s | 2.8914e+03 |
| i | 4.6000 |
| ii | 9.6100 |
| iii | 19.6200 |
| iiii | 30.1300 |
| m1 | 0.0248 |
| m2 | 0.0565 |
| m3 | 0.0419 |
| m4 | 0.1634 |
| n | 1 |
| o | 22 |

| Workspace | |
|-----------|---------|
| Name | Value |
| P1 | 0.1000 |
| P10 | 30.5300 |
| P1f | 30.1300 |
| P2f | 19.6200 |
| P3f | 9.6100 |
| P4f | 4.6000 |
| P8 | 150 |
| P9 | 30.5300 |
| P_1_f | 0 |
| P_2_f | 0 |
| P_3_f | 0 |
| P_4_f | 0 |
| Pb | 150 |
| Pc | 0.1000 |
| Pr | 30.5300 |
| Qadd | 0 |
| Qrej | 0 |
| r | 11 |

Workspace

| Name | Value |
|--------------|-----------|
| s1 | 0.6494 |
| s10 | 7.2269 |
| s8 | 6.3479 |
| s9s | 6.3479 |
| sol | 0 |
| st | 0.5000 |
| T10 | 500 |
| T16 | 148.7208 |
| T18 | 178.1642 |
| T20 | 234.0984 |
| T3 | 148.7208 |
| T4 | 178.1642 |
| T7 | 234.0984 |
| T8 | 500 |
| Tmax | 500 |
| u | 12 |
| { } varNames | 1x10 cell |
| Wnet | 0 |

| | | |
|------|----------|-----------|
| () | varNames | 1x10 cell |
| Wnet | 0 | |
| Wp | 0 | |
| Wt | 0 | |
| x | 0 | |

Variables - B

B X best

| | 1 |
|---|----------|
| 1 | 60.6104 |
| 2 | 159.4701 |
| 3 | 123.0736 |
| 4 | 427.7858 |

best

10x1 double

| | 1 |
|----|--------|
| 1 | 0.5527 |
| 2 | 0.5201 |
| 3 | 0.5061 |
| 4 | 0.4964 |
| 5 | 0.4887 |
| 6 | 0.4821 |
| 7 | 0.4764 |
| 8 | 0.4713 |
| 9 | 0.4666 |
| 10 | 0.4623 |

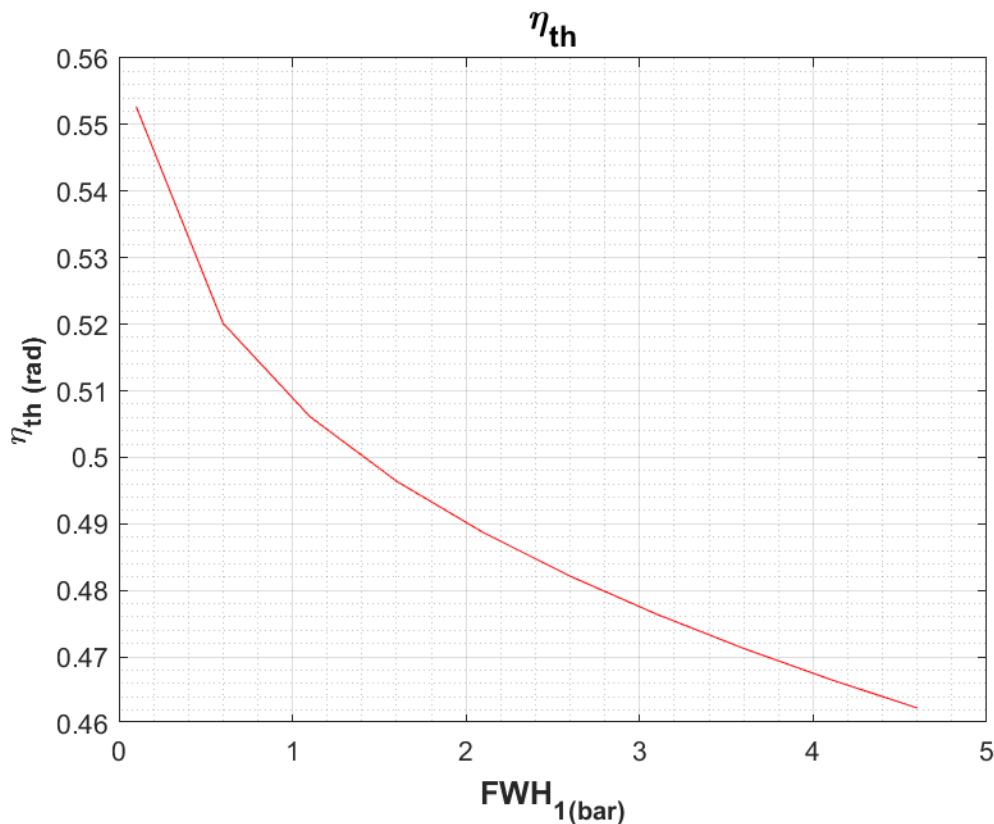
best_sol

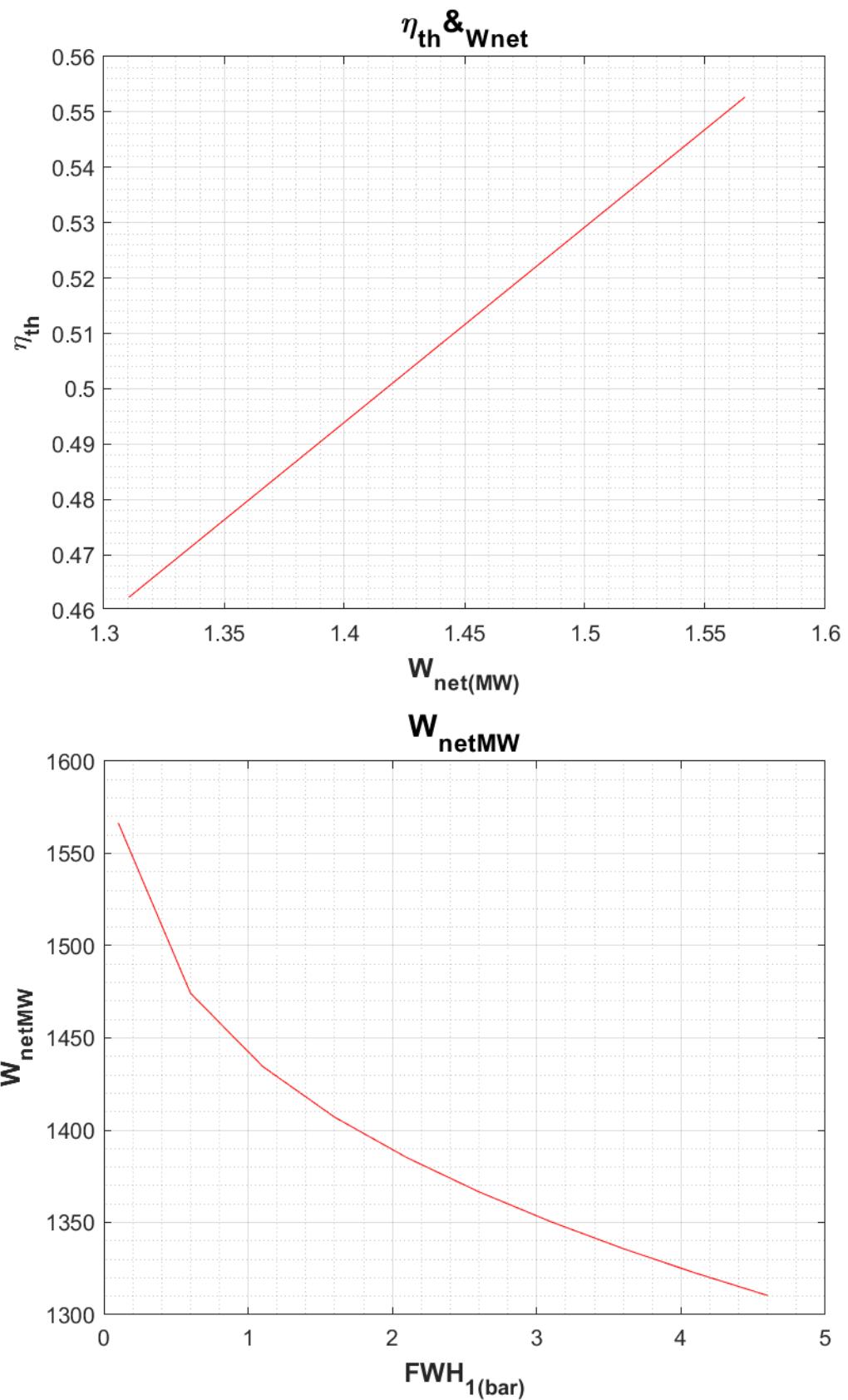
10x10 double

| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |
|----|--------|------------|------------|------------|------------|---------|--------|--------|---------|---------|
| 1 | 0.5527 | 1.5665e+03 | 2.8344e+03 | 1.2679e+03 | 1.5823e+03 | 15.7785 | 0.1000 | 0.1100 | 0.1200 | 30.1300 |
| 2 | 0.5201 | 1.4743e+03 | 2.8344e+03 | 1.3601e+03 | 1.4901e+03 | 15.7683 | 0.6000 | 0.6100 | 0.6200 | 30.1300 |
| 3 | 0.5061 | 1.4346e+03 | 2.8344e+03 | 1.3999e+03 | 1.4503e+03 | 15.7600 | 1.1000 | 1.1100 | 1.1200 | 30.1300 |
| 4 | 0.4964 | 1.4070e+03 | 2.8344e+03 | 1.4274e+03 | 1.4228e+03 | 15.7527 | 1.6000 | 1.6100 | 1.6200 | 30.1300 |
| 5 | 0.4887 | 1.3851e+03 | 2.8344e+03 | 1.4493e+03 | 1.4006e+03 | 15.4611 | 2.1000 | 2.1100 | 19.6200 | 30.1300 |
| 6 | 0.4821 | 1.3666e+03 | 2.8344e+03 | 1.4679e+03 | 1.3820e+03 | 15.4784 | 2.6000 | 2.6100 | 19.6200 | 30.1300 |
| 7 | 0.4764 | 1.3503e+03 | 2.8344e+03 | 1.4841e+03 | 1.3658e+03 | 15.4934 | 3.1000 | 3.1100 | 19.6200 | 30.1300 |
| 8 | 0.4713 | 1.3358e+03 | 2.8344e+03 | 1.4986e+03 | 1.3513e+03 | 15.5068 | 3.6000 | 3.6100 | 19.6200 | 30.1300 |
| 9 | 0.4666 | 1.3226e+03 | 2.8344e+03 | 1.5119e+03 | 1.3381e+03 | 15.5189 | 4.1000 | 4.1100 | 19.6200 | 30.1300 |
| 10 | 0.4623 | 1.3104e+03 | 2.8344e+03 | 1.5240e+03 | 1.3259e+03 | 15.5301 | 4.6000 | 4.6100 | 19.6200 | 30.1300 |

| eta | Wnet | Qadd | Qrej | Wt | Wp | P_4_f | P_3_f | P_2_f | P_1_f |
|-------------|-------------|-------------|-------------|-------------|-------------|-------|-------|-------|-------|
| 0.552682019 | 1566.539387 | 2834.431612 | 1267.892225 | 1582.317841 | 15.77845333 | 0.1 | 0.11 | 0.12 | 30.13 |
| 0.520145753 | 1474.317565 | 2834.431612 | 1360.114048 | 1490.085856 | 15.76829141 | 0.6 | 0.61 | 0.62 | 30.13 |
| 0.50612147 | 1434.566693 | 2834.431612 | 1399.864919 | 1450.326673 | 15.75997963 | 1.1 | 1.11 | 1.12 | 30.13 |
| 0.496401377 | 1407.015754 | 2834.431612 | 1427.415858 | 1422.768455 | 15.75270124 | 1.6 | 1.61 | 1.62 | 30.13 |
| 0.48867866 | 1385.126242 | 2834.431612 | 1449.30537 | 1400.587366 | 15.46112407 | 2.1 | 2.11 | 19.62 | 30.13 |
| 0.482130961 | 1366.567238 | 2834.431612 | 1467.864374 | 1382.045618 | 15.47837921 | 2.6 | 2.61 | 19.62 | 30.13 |
| 0.476399051 | 1350.320531 | 2834.431612 | 1484.111081 | 1365.813933 | 15.4934018 | 3.1 | 3.11 | 19.62 | 30.13 |
| 0.471269835 | 1335.782119 | 2834.431612 | 1498.649493 | 1351.288914 | 15.50679498 | 3.6 | 3.61 | 19.62 | 30.13 |
| 0.466605238 | 1322.560637 | 2834.431612 | 1511.870975 | 1338.079576 | 15.51893951 | 4.1 | 4.11 | 19.62 | 30.13 |
| 0.462311117 | 1310.389243 | 2834.431612 | 1524.042369 | 1325.919336 | 15.53009248 | 4.6 | 4.61 | 19.62 | 30.13 |

Best efficiency by changing the value of pressure for different FWH





D.5 One OFWH and four CFWHs were added to the reheat cycle

After the Reheat Pressure

Code

Code

```
{Givens}  
P_b=150  
P_c=0.1  
P_re=30.51  
eta_t=0.85; eta_p=0.95  
T_max=500
```

```
{Point 1}  
h_1=ENTHALPY(Steam,X=0,P=P_c)  
s_1=ENTROPY(Steam,X=0,P=P_c)
```

```
{Point 2}  
s_2s=s_1  
h_2s=ENTHALPY(Steam,S=s_2s,P=P_o)  
(h_2s-h_1)=(h_2-h_1)*eta_p
```

```
{Point 5}  
h_5=ENTHALPY(Steam,X=0,P=P_o)  
s_5=ENTROPY(Steam,X=0,P=P_o)
```

```
{Point 6}  
s_6s=s_5  
h_6s=ENTHALPY(Steam,S=s_6s,P=P_b)  
(h_6s-h_5)=(h_6-h_5)*eta_p
```

```
{Point 9}  
h_9=ENTHALPY(Steam,T=T_max,P=P_b)  
s_9=ENTROPY(Steam,T=T_max,P=P_b)
```

```
{Point 10}  
s_10s=s_9  
h_10s=ENTHALPY(Steam,S=s_10s,P=P_re)  
(h_9-h_10s)*eta_t=(h_9-h_10)
```

```
{Point 11}  
h_11=ENTHALPY(Steam,T=T_max,P=P_re)  
s_11=ENTROPY(Steam,T=T_max,P=P_re)
```

```
{Point 12}  
s_12s=s_11  
h_12s=ENTHALPY(Steam,S=s_12s,P=P_4cl)  
(h_11-h_12s)*eta_t=(h_11-h_12)
```

```

s_12=ENTROPY(Steam,h=h_12,P=P_4cl)

{Point 13}
s_13s=s_12
h_13s=ENTHALPY(Steam,S=s_13s,P=P_3cl)
(h_12-h_13s)*eta_t=(h_12-h_13)
s_13=ENTROPY(Steam,h=h_13,P=P_3cl)

{Point 14}
s_14s=s_13
h_14s=ENTHALPY(Steam,S=s_14s,P=P_o)
(h_13-h_14s)*eta_t=(h_13-h_14)
s_14=ENTROPY(Steam,h=h_14,P=P_o)

{Point 15}
s_15s=s_14
h_15s=ENTHALPY(Steam,S=s_15s,P=P_2cl)
(h_14-h_15s)*eta_t=(h_14-h_15)
s_15=ENTROPY(Steam,h=h_15,P=P_2cl)

{Point 16}
s_16s=s_15
h_16s=ENTHALPY(Steam,S=s_16s,P=P_1cl)
(h_15-h_16s)*eta_t=(h_15-h_16)
s_16=ENTROPY(Steam,h=h_16,P=P_1cl)

{Point 17}
s_17s=s_16
h_17s=ENTHALPY(Steam,S=s_17s,P=P_c)
(h_16-h_17s)*eta_t=(h_16-h_17)
s_17=ENTROPY(Steam,h=h_17,P=P_c)

{Point 18}
h_18=ENTHALPY(Steam,X=0,P=P_4cl)
T_18=TEMPERATURE(Steam,h=h_18,P=P_4cl)

{Point 19}
h_19=h_18

{Point 8}
T_8=T_18
h_8=ENTHALPY(Steam,T=T_18,P=P_b)

{Point 20}
h_20=ENTHALPY(Steam,X=0,P=P_3cl)
T_20=TEMPERATURE(Steam,h=h_20,P=P_3cl)

{Point 7}
T_7=T_20
h_7=ENTHALPY(Steam,T=T_20,P=P_b)

{Point 21}
h_21=h_20

{Point 22}
h_22=ENTHALPY(Steam,X=0,P=P_2cl)
T_22=TEMPERATURE(Steam,h=h_22,P=P_2cl)

```

{point 23}
h_23=h_22

{Point 4}
T_4=T_22
h_4=ENTHALPY(Steam,T=T_22,P=P_o)

{Point 24}
h_24=ENTHALPY(Steam,X=0,P=P_1cl)
T_24=TEMPERATURE(Steam,h=h_24,P=P_1cl)

{Point 25}
h_25=h_24

{Point 3}
T_3=T_24
h_3=ENTHALPY(Steam,T=T_24,P=P_o)

{Energy Balance of CFWH4}
h_8+h_18*v=h_13*v+h_7

{Energy Balance of CFWH3}
h_14*w+h_19*v+h_6=h_7+h_20*(w+v)

{Energy Balance of OFWH}
h_15*x+h_21*(w+v)+h_4*(1-v-w-x)=h_5

{Energy Balance of CFWH2}
h_16*y+h_3*(1-v-x-w)=h_4*(1-v-x-w)+h_22*y

{Energy Balance of CFWH1}
h_17*z+h_23*y+h_2*(1-v-x-w)=h_3*(1-v-x-w)+h_24*(y+z)

{Calculations}

```
Q_add=(h_9-h_8)+(h_11-h_10)
Q_rej=(h_1-h_12)+(h_1-h_25)
W_p=(h_2-h_1)+(h_6-h_5)
W_t=(h_9-h_10)+(h_11-h_13)+(h_13-h_14)*(1-v)+(h_14-h_15)*(1-v-w)+(h_15-h_16)*(1-v-w-x)+(h_16-
h_17)*(1-v-w-x-y)+(h_17-h_12)*(1-v-w-x-y-z)
W_net=W_t-W_p
eta_th=W_net/Q_add
```

| Variable | Guess | Lower | Upper | Display | Units |
|----------|-------|------------|------------|---------|-------|
| P_1cl | 0.5 | 1.0000E-01 | | P_2cl | A 0 N |
| P_2cl | 3 | P_1cl | | P_o | A 0 N |
| P_3cl | 12 | P_o | | P_4cl | A 0 N |
| P_4cl | 28 | P_3cl | 3.0510E+01 | A 0 N | |
| P_o | 6 | P_2cl | P_3cl | A 0 N | |

Optimum OFWH Pressure = 5.433 bar

Optimum CFWH1 Pressure = 0.4473 bar

Optimum CFWH2 Pressure = 1.656 bar

Optimum CFWH3 Pressure = 12.72 bar

Optimum CFWH4 Pressure = 28.03 bar

Maximum Efficiency = 42.41%

Calculations Completed

78 equations in 62 blocks - 229 iterations

Elapsed time = 10.9 sec

eta_th = 0.4241

 Continue

| Independent Variable | Value | Best value |
|----------------------|--------|------------|
| P_1cl | 0.4473 | 0.4473 |
| P_2cl | 1.656 | 1.656 |
| P_3cl | 12.72 | 12.72 |
| P_4cl | 28.03 | 28.03 |
| P_o | 5.433 | 5.433 |

Results Tab

Unit Settings: [kJ]/[C]/[bar]/[kg]/[degrees]

Maximization of eta_th(P_1cl,P_2cl,P_3cl,P_4cl,P_o) 229 iterations: Variable Metric method

| | | | |
|------------------------------------|-------------------------------------|------------------------------------|-------------------------------------|
| $\eta_p = 0.95$ | $\eta_t = 0.85$ | $\eta_{th} = 0.4241$ | $h_1 = 191.7 \text{ [kJ/kg]}$ |
| $h_{13} = 3431$ | $h_{13s} = 3427 \text{ [kJ/kg]}$ | $h_{14} = 3220$ | $h_{14s} = 3182 \text{ [kJ/kg]}$ |
| $h_{17s} = 2575 \text{ [kJ/kg]}$ | $h_{18} = 990.7 \text{ [kJ/kg]}$ | $h_{19} = 990.7 \text{ [kJ/kg]}$ | $h_2 = 192.3$ |
| $h_{25} = 328.9 \text{ [kJ/kg]}$ | $h_{2s} = 192.3 \text{ [kJ/kg]}$ | $h_3 = 329.3 \text{ [kJ/kg]}$ | $h_4 = 480 \text{ [kJ/kg]}$ |
| $h_g = 3309 \text{ [kJ/kg]}$ | $P_{1cl} = 0.4473$ | $P_{2cl} = 1.656$ | $P_{3cl} = 12.72$ |
| $Q_{add} = 2819$ | $Q_{ref} = -2368$ | $s_1 = 0.6489 \text{ [kJ/kg-K]}$ | $s_{10s} = 6.345 \text{ [kJ/kg-K]}$ |
| $s_{14} = 7.289 \text{ [kJ/kg-K]}$ | $s_{14s} = 7.231 \text{ [kJ/kg-K]}$ | $s_{15} = 7.352 \text{ [kJ/kg-K]}$ | $s_{15s} = 7.289 \text{ [kJ/kg-K]}$ |
| $s_5 = 1.893 \text{ [kJ/kg-K]}$ | $s_{6s} = 1.893 \text{ [kJ/kg-K]}$ | $s_9 = 6.345 \text{ [kJ/kg-K]}$ | $T_{18} = 230.1 \text{ [C]}$ |
| $T_7 = 190.6 \text{ [C]}$ | $T_8 = 230.1 \text{ [C]}$ | $T_{max} = 500$ | $v = 0.07233$ |
| $y = 0.05325$ | $z = 0.04578$ | | |

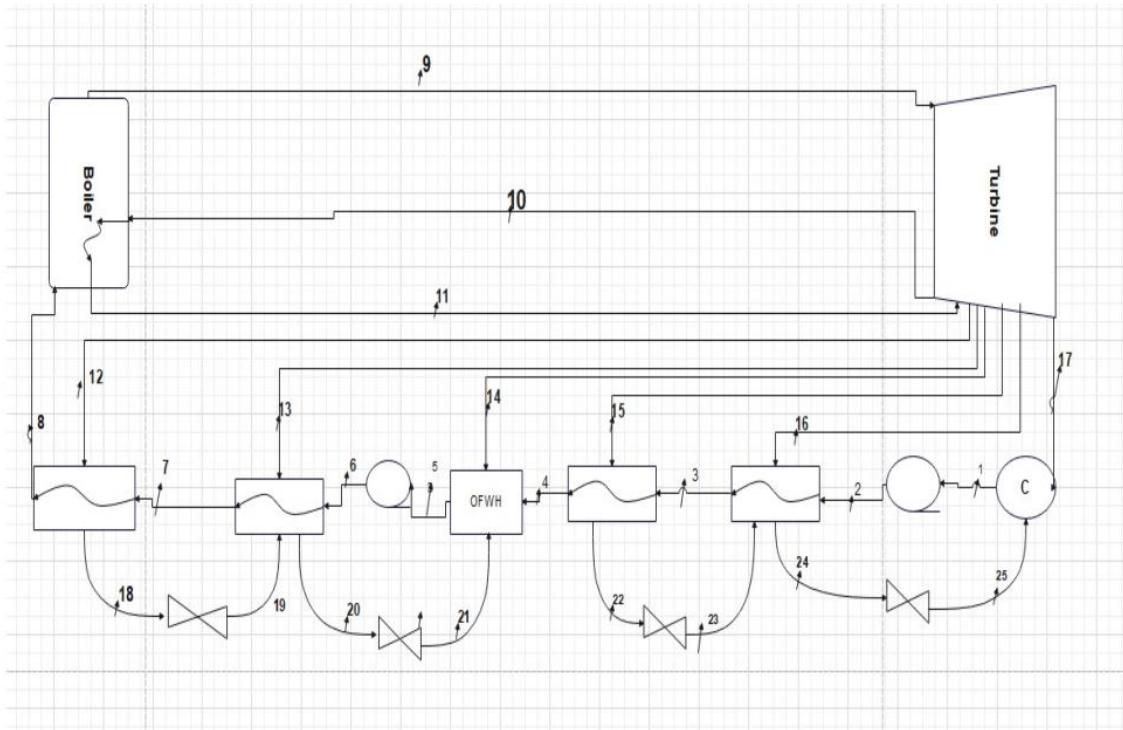
| | | |
|------------------------------------|-------------------------------------|-------------------------------------|
| $h_{10} = 2953$ | $h_{10s} = 2890 \text{ [kJ/kg]}$ | $h_{11} = 3456 \text{ [kJ/kg]}$ |
| $h_{15} = 3025$ | $h_{15s} = 2990 \text{ [kJ/kg]}$ | $h_{16} = 2802$ |
| $h_{20} = 810.4 \text{ [kJ/kg]}$ | $h_{21} = 810.4 \text{ [kJ/kg]}$ | $h_{22} = 479.7 \text{ [kJ/kg]}$ |
| $h_5 = 653.9 \text{ [kJ/kg]}$ | $h_6 = 670.6$ | $h_{6s} = 669.7 \text{ [kJ/kg]}$ |
| $P_{4cl} = 28.03$ | $P_b = 150$ | $P_c = 0.1$ |
| $s_{11} = 7.226 \text{ [kJ/kg-K]}$ | $s_{12} = 7.644 \text{ [kJ/kg-K]}$ | $s_{12s} = 7.541 \text{ [kJ/kg-K]}$ |
| $s_{16} = 7.444 \text{ [kJ/kg-K]}$ | $s_{16s} = 7.352 \text{ [kJ/kg-K]}$ | $s_{17} = 7.541 \text{ [kJ/kg-K]}$ |
| $T_{20} = 190.6 \text{ [C]}$ | $T_{22} = 114.3 \text{ [C]}$ | $T_{24} = 78.56 \text{ [C]}$ |
| $w = 0.05534$ | $W_{net} = 1196$ | $W_p = 17.19$ |

| | |
|-------------------------------------|-------------------------------------|
| $h_{12} = 2423$ | $h_{12s} = 2390 \text{ [kJ/kg]}$ |
| $h_{16s} = 2763 \text{ [kJ/kg]}$ | $h_{17} = 2609$ |
| $h_{23} = 479.7 \text{ [kJ/kg]}$ | $h_{24} = 328.9 \text{ [kJ/kg]}$ |
| $h_7 = 816.9 \text{ [kJ/kg]}$ | $h_8 = 993.5 \text{ [kJ/kg]}$ |
| $P_o = 5.433$ | $P_{re} = 30.51$ |
| $s_{13} = 7.231 \text{ [kJ/kg-K]}$ | $s_{13s} = 7.226 \text{ [kJ/kg-K]}$ |
| $s_{17s} = 7.444 \text{ [kJ/kg-K]}$ | $s_{2s} = 0.6489 \text{ [kJ/kg-K]}$ |
| $T_3 = 78.56 \text{ [C]}$ | $T_4 = 114.3 \text{ [C]}$ |
| $W_t = 1213$ | $x = 0.05177$ |

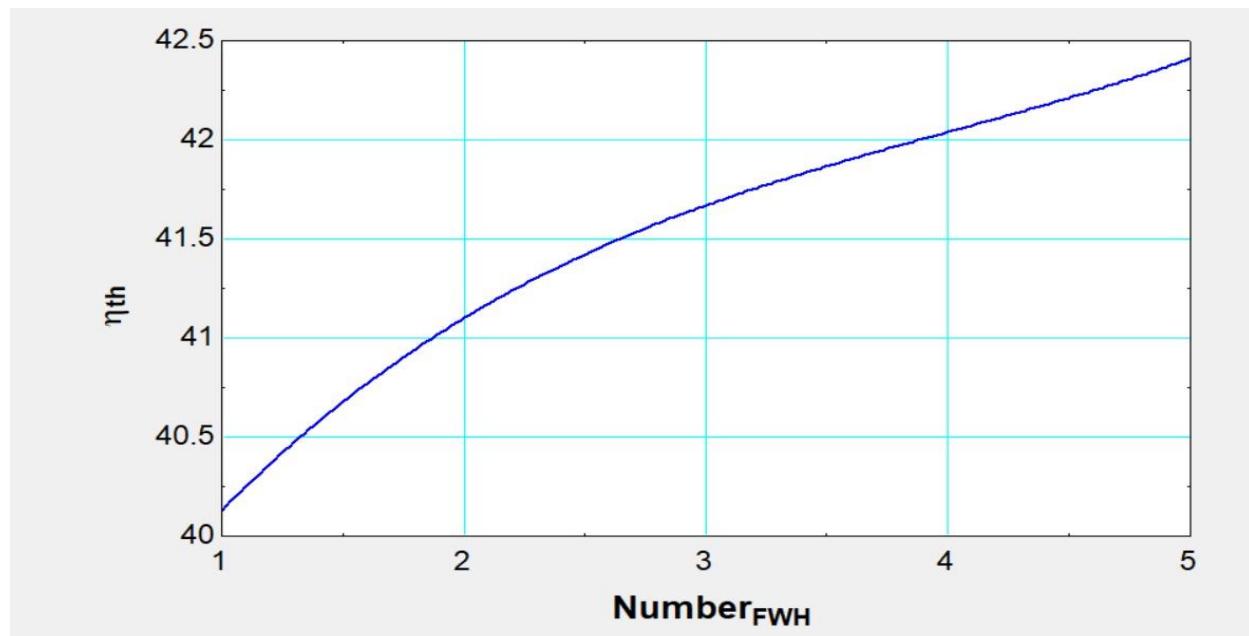
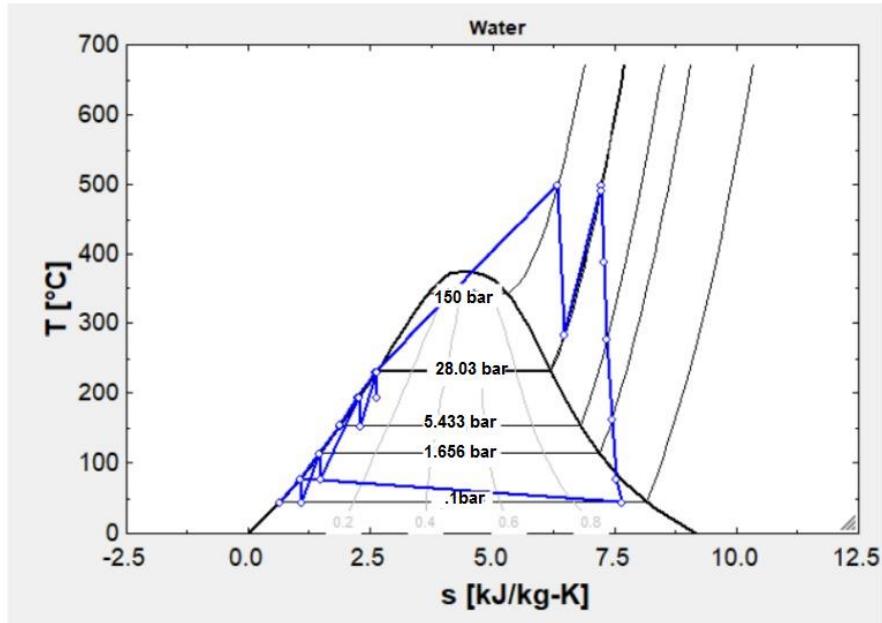
| Run | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | |
|--------|--------|--------|-------|-------|-------|-------|---|---|---|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|--|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | |
| Run 1 | 0.419 | 0.1 | 1 | 6 | 15 | 2 | | | | | | | | | | | | | | | | | | | | | | | | | |
| Run 2 | 0.4202 | 0.131 | 1.034 | 6.31 | 15.53 | 2.138 | | | | | | | | | | | | | | | | | | | | | | | | | |
| Run 3 | 0.421 | 0.1621 | 1.069 | 6.621 | 16.07 | 2.276 | | | | | | | | | | | | | | | | | | | | | | | | | |
| Run 4 | 0.4216 | 0.1931 | 1.103 | 6.931 | 16.6 | 2.414 | | | | | | | | | | | | | | | | | | | | | | | | | |
| Run 5 | 0.4221 | 0.2241 | 1.138 | 7.241 | 17.14 | 2.552 | | | | | | | | | | | | | | | | | | | | | | | | | |
| Run 6 | 0.4224 | 0.2552 | 1.172 | 7.552 | 17.67 | 2.69 | | | | | | | | | | | | | | | | | | | | | | | | | |
| Run 7 | 0.4227 | 0.2862 | 1.207 | 7.862 | 18.21 | 2.828 | | | | | | | | | | | | | | | | | | | | | | | | | |
| Run 8 | 0.4229 | 0.3172 | 1.241 | 8.172 | 18.74 | 2.966 | | | | | | | | | | | | | | | | | | | | | | | | | |
| Run 9 | 0.4231 | 0.3483 | 1.276 | 8.483 | 19.28 | 3.103 | | | | | | | | | | | | | | | | | | | | | | | | | |
| Run 10 | 0.4232 | 0.3793 | 1.31 | 8.793 | 19.81 | 3.241 | | | | | | | | | | | | | | | | | | | | | | | | | |
| Run 11 | 0.4233 | 0.4103 | 1.345 | 9.103 | 20.35 | 3.379 | | | | | | | | | | | | | | | | | | | | | | | | | |
| Run 12 | 0.4234 | 0.4414 | 1.379 | 9.414 | 20.88 | 3.517 | | | | | | | | | | | | | | | | | | | | | | | | | |
| Run 13 | 0.4235 | 0.4724 | 1.414 | 9.724 | 21.42 | 3.655 | | | | | | | | | | | | | | | | | | | | | | | | | |
| Run 14 | 0.4235 | 0.5034 | 1.448 | 10.03 | 21.95 | 3.793 | | | | | | | | | | | | | | | | | | | | | | | | | |
| Run 15 | 0.4236 | 0.5345 | 1.483 | 10.34 | 22.49 | 3.931 | | | | | | | | | | | | | | | | | | | | | | | | | |
| Run 16 | 0.4236 | 0.5655 | 1.517 | 10.66 | 23.02 | 4.069 | | | | | | | | | | | | | | | | | | | | | | | | | |
| Run 17 | 0.4236 | 0.5966 | 1.552 | 10.97 | 23.56 | 4.207 | | | | | | | | | | | | | | | | | | | | | | | | | |
| Run 18 | 0.4236 | 0.6276 | 1.586 | 11.28 | 24.09 | 4.345 | | | | | | | | | | | | | | | | | | | | | | | | | |
| Run 19 | 0.4236 | 0.6586 | 1.621 | 11.59 | 24.63 | 4.483 | | | | | | | | | | | | | | | | | | | | | | | | | |
| Run 20 | 0.4236 | 0.6897 | 1.655 | 11.9 | 25.16 | 4.621 | | | | | | | | | | | | | | | | | | | | | | | | | |
| Run 21 | 0.4236 | 0.7207 | 1.69 | 12.21 | 25.7 | 4.759 | | | | | | | | | | | | | | | | | | | | | | | | | |
| Run 22 | 0.4235 | 0.7517 | 1.724 | 12.52 | 26.23 | 4.897 | | | | | | | | | | | | | | | | | | | | | | | | | |
| Run 23 | 0.4235 | 0.7828 | 1.759 | 12.83 | 26.77 | 5.034 | | | | | | | | | | | | | | | | | | | | | | | | | |
| Run 24 | 0.4235 | 0.8138 | 1.793 | 13.14 | 27.3 | 5.172 | | | | | | | | | | | | | | | | | | | | | | | | | |
| Run 25 | 0.4234 | 0.8448 | 1.828 | 13.45 | 27.84 | 5.31 | | | | | | | | | | | | | | | | | | | | | | | | | |
| Run 26 | 0.4234 | 0.8759 | 1.862 | 13.76 | 28.37 | 5.448 | | | | | | | | | | | | | | | | | | | | | | | | | |
| Run 27 | 0.4233 | 0.9069 | 1.897 | 14.07 | 28.91 | 5.586 | | | | | | | | | | | | | | | | | | | | | | | | | |
| Run 28 | 0.4233 | 0.9379 | 1.931 | 14.38 | 29.44 | 5.724 | | | | | | | | | | | | | | | | | | | | | | | | | |
| Run 29 | 0.4232 | 0.969 | 1.966 | 14.69 | 29.98 | 5.862 | | | | | | | | | | | | | | | | | | | | | | | | | |
| Run 30 | 0.4232 | 1 | 2 | 15 | 30.51 | 6 | | | | | | | | | | | | | | | | | | | | | | | | | |
| Run | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | |
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | |

| 1..30 | 1 η_{th} | 2 P_{1cl} | 3 P_{2cl} | 4 P_{3cl} | 5 P_{4cl} | 6 P_0 |
|--------|------------------|----------------|----------------|----------------|----------------|------------|
| Run 1 | 0.4203 | 0.1 | 1 | 8 | 18 | 3 |
| Run 2 | 0.4213 | 0.131 | 1.069 | 8.345 | 18.43 | 3.172 |
| Run 3 | 0.422 | 0.1621 | 1.138 | 8.69 | 18.86 | 3.345 |
| Run 4 | 0.4224 | 0.1931 | 1.207 | 9.034 | 19.29 | 3.517 |
| Run 5 | 0.4228 | 0.2241 | 1.276 | 9.379 | 19.73 | 3.69 |
| Run 6 | 0.4231 | 0.2552 | 1.345 | 9.724 | 20.16 | 3.862 |
| Run 7 | 0.4233 | 0.2862 | 1.414 | 10.07 | 20.59 | 4.034 |
| Run 8 | 0.4234 | 0.3172 | 1.483 | 10.41 | 21.02 | 4.207 |
| Run 9 | 0.4235 | 0.3483 | 1.552 | 10.76 | 21.45 | 4.379 |
| Run 10 | 0.4236 | 0.3793 | 1.621 | 11.1 | 21.88 | 4.552 |
| Run 11 | 0.4237 | 0.4103 | 1.69 | 11.45 | 22.31 | 4.724 |
| Run 12 | 0.4237 | 0.4414 | 1.759 | 11.79 | 22.75 | 4.897 |
| Run 13 | 0.4238 | 0.4724 | 1.828 | 12.14 | 23.18 | 5.069 |
| Run 14 | 0.4238 | 0.5034 | 1.897 | 12.48 | 23.61 | 5.241 |
| Run 15 | 0.4238 | 0.5345 | 1.966 | 12.83 | 24.04 | 5.414 |
| Run 16 | 0.4238 | 0.5655 | 2.034 | 13.17 | 24.47 | 5.586 |
| Run 17 | 0.4237 | 0.5966 | 2.103 | 13.52 | 24.9 | 5.759 |
| Run 18 | 0.4237 | 0.6276 | 2.172 | 13.86 | 25.33 | 5.931 |
| Run 19 | 0.4237 | 0.6586 | 2.241 | 14.21 | 25.76 | 6.103 |
| Run 20 | 0.4237 | 0.6897 | 2.31 | 14.55 | 26.2 | 6.276 |
| Run 21 | 0.4237 | 0.7207 | 2.379 | 14.9 | 26.63 | 6.448 |
| Run 22 | 0.4236 | 0.7517 | 2.448 | 15.24 | 27.06 | 6.621 |
| Run 23 | 0.4236 | 0.7828 | 2.517 | 15.59 | 27.49 | 6.793 |
| Run 24 | 0.4235 | 0.8138 | 2.586 | 15.93 | 27.92 | 6.966 |
| Run 25 | 0.4235 | 0.8448 | 2.655 | 16.28 | 28.35 | 7.138 |
| Run 26 | 0.4235 | 0.8759 | 2.724 | 16.62 | 28.78 | 7.31 |
| Run 27 | 0.4234 | 0.9069 | 2.793 | 16.97 | 29.22 | 7.483 |
| Run 28 | 0.4233 | 0.9379 | 2.862 | 17.31 | 29.65 | 7.655 |
| Run 29 | 0.4233 | 0.969 | 2.931 | 17.66 | 30.08 | 7.828 |
| Run 30 | 0.4232 | 1 | 3 | 18 | 30.51 | 8 |

Flow Diagram



T-s Diagram



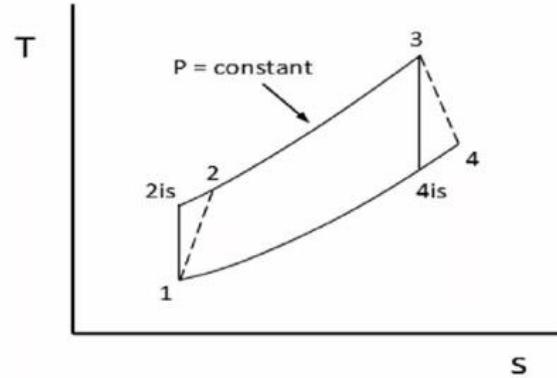
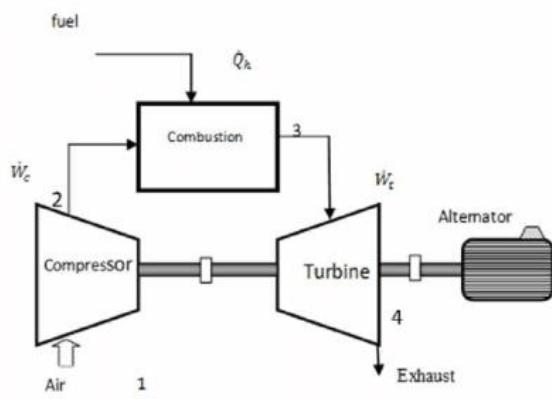
Relation bn no of FWH and the efficiency

Question 2: Gas Cycle

A gas turbine power plant operates on a simple gas turbine cycle with air as the working fluid. The air enters the compressor at 95 kPa and 310 K and the turbine at 1300 K. The isentropic efficiency is 80 % for the compression and 85 % for the expansion. Accounting for the variation of specific heats with temperature.

- A) Find the optimum pressure ratio for maximizing network output of the cycle and plot the $R_p - W_{net}$ relation.
- B) Plot the relation between the pressure ratio and the thermal efficiency then compare it with the simple ideal cycle.
- C) Use an ideal regenerator and plot the relation between the pressure ratio and the thermal efficiency to compare it with the simple ones and find out the maximum pressure ratio can be used with the regenerative cycle.

Simple gas cycle:



Code on EES

"givens"

$$P_1=0.95[\text{kpa}]$$

$$T_1=310[\text{k}]$$

$$T_3=1300[\text{k}]$$

$$\text{eta_compressor}=0.8$$

$$\text{eta_turbine}=0.85$$

$$rp=P_2/P_1$$

"point 1"

$$h_1=\text{ENTHALPY}(\text{Air_ha}, T=T_1, P=P_1)$$

$$s_1=\text{ENTROPY}(\text{Air_ha}, T=T_1, P=P_1)$$

"point 2"

$$s_{2s}=s_1$$

```

h_2s=ENTHALPY(Air_ha,s=s_1,P=P_2)

eta_compressor=(h_2s-h_1)/(h_2-h_1)

T_2=TEMPERATURE(Air_ha,h=h_2,P=P_2)

"point 3"

h_3=ENTHALPY(Air_ha,T=T_3,P=P_2)

s_3=ENTROPY(Air_ha,T=T_3,P=P_2)

"point 4"

s_4s=s_3

h_4s=ENTHALPY(Air_ha,s=s_3,P=P_1)

eta_turbine=(h_3-h_4)/(h_3-h_4s)

T_4=TEMPERATURE(Air_ha,h=h_4,P=P_1)

"calculations"

w_t=h_3-h_4

w_c=h_2-h_1

w_net=w_t-w_c

q_add=h_3-h_2

eta_th=w_net/q_add

" ideal cycle"

w_t_s=h_3-h_4s

w_c_s=h_2s-h_1

w_net_s=w_t_s-w_c_s

q_add_s=h_3-h_2s

eta_th_s=w_net_s/q_add_s

" regeneration "

h_5=h_4

```

w_t_regen=h_3-h_4

w_net_regen=w_t_regen-w_c

q_add_regen=h_3-h_5

eta_th_regen=w_net_regen/q_add_regen

Optimizing Pressure ratio for maximum work net:

| 1..19 | rp | w _{net} |
|--------|----|------------------|
| Run 1 | 2 | 117.2 |
| Run 2 | 3 | 162.2 |
| Run 3 | 4 | 183.8 |
| Run 4 | 5 | 194.6 |
| Run 5 | 6 | 199.6 |
| Run 6 | 7 | 201.1 |
| Run 7 | 8 | 200.4 |
| Run 8 | 9 | 198.2 |
| Run 9 | 10 | 195 |
| Run 10 | 11 | 191.1 |
| Run 11 | 12 | 186.7 |
| Run 12 | 13 | 181.9 |
| Run 13 | 14 | 176.9 |
| Run 14 | 15 | 171.7 |
| Run 15 | 16 | 166.4 |
| Run 16 | 17 | 160.9 |
| Run 17 | 18 | 155.4 |
| Run 18 | 19 | 149.9 |
| Run 19 | 20 | 144.4 |

Calculations Completed

33 equations in 26 blocks - 18 iterations

Elapsed time = 1.0 sec

w_{net} = 201.1

 Continue

| Independent Variable | Value | Best value |
|----------------------|-------|------------|
| rp | 7.116 | 7.116 |

Maximum pressure ratio is 7.116 bar

Results Tab

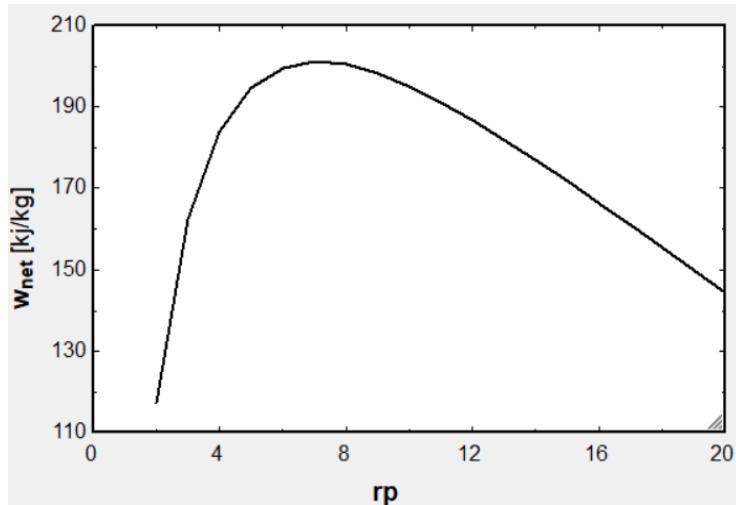
Unit Settings [kJ/(kg·K)]/[bar]/[kg]/[degrees]

Maximization of w_{net}(rp) 10 iterations: Quadratic Approximations method

| | | | | | | | | |
|---------------------------------|------------------------------------|-----------------------------|----------------------------|-------------------------|-------------------------------|--------------------------|---------------------|---------------|
| $\eta_{compressor} = 0.8$ | $\eta_{th} = 0.2533$ | $\eta_{th, regen} = 0.4075$ | $\eta_{th,s} = 0.4067$ | $\eta_{turbine} = 0.85$ | $h_1 = 310.3 \text{ [kJ/kg]}$ | $h_2 = 602.7$ | $h_2s = 544.2$ | $h_3 = 1397$ |
| $h_4 = 903.1$ | $h_{4s} = 816$ | $h_5 = 903.1$ | $P_1 = 0.95 \text{ [kPa]}$ | $P_2 = 6.76$ | $q_{add} = 793.9$ | $q_{add, regen} = 493.5$ | $q_{add,s} = 852.3$ | $rp = 7.116$ |
| $s_1 = 6.918 \text{ [kJ/kg·K]}$ | $s_{2s} = 6.918 \text{ [kJ/kg·K]}$ | $s_3 = 7.894$ | $s_{4s} = 7.894$ | $T_1 = 310 \text{ [K]}$ | $T_2 = 596$ | $T_3 = 1300 \text{ [K]}$ | $T_4 = 672.8$ | $w_c = 292.4$ |
| $w_{c,s} = 233.9$ | $w_{net} = 201.1$ | $w_{net, regen} = 201.1$ | $w_{net,s} = 346.7$ | $w_i = 493.5$ | $w_{i, regen} = 493.5$ | $w_{i,s} = 580.6$ | | |

Calculation time = 1.1 sec

Plotting the R_p against W_{net} relation:



Relation between pressure ratio and thermal efficiency

Calculations Completed

28 equations in 21 blocks - 15 iterations

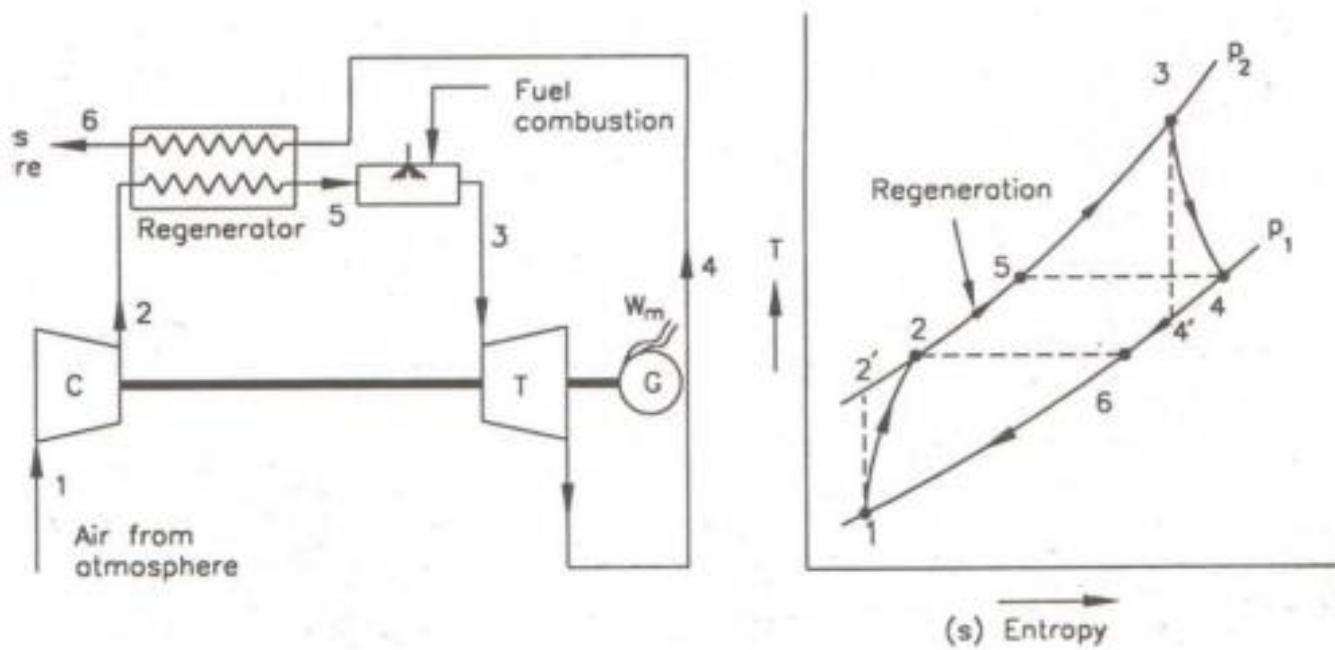
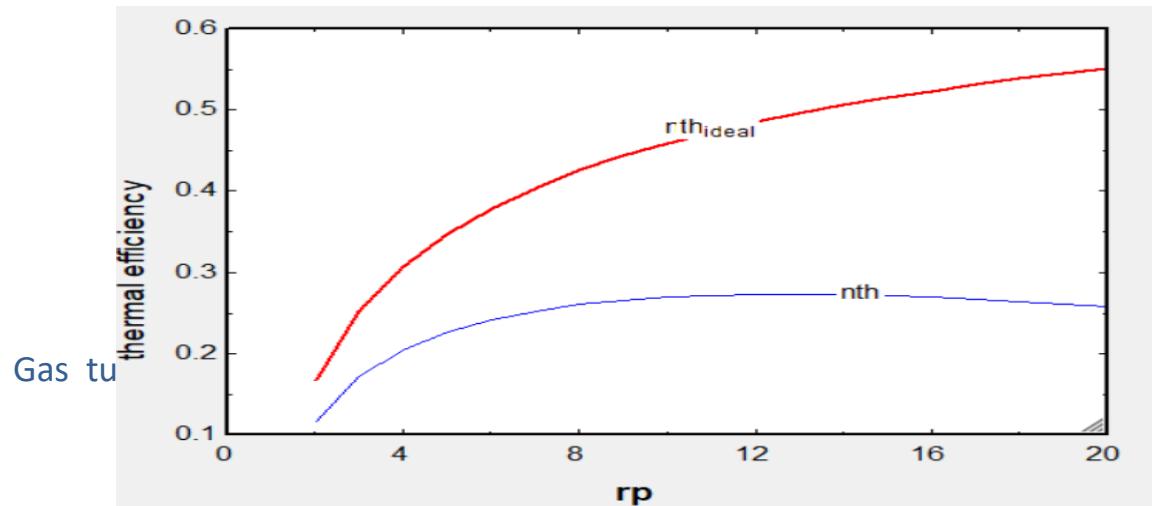
Elapsed time = .5 sec

eta_th = 0.273

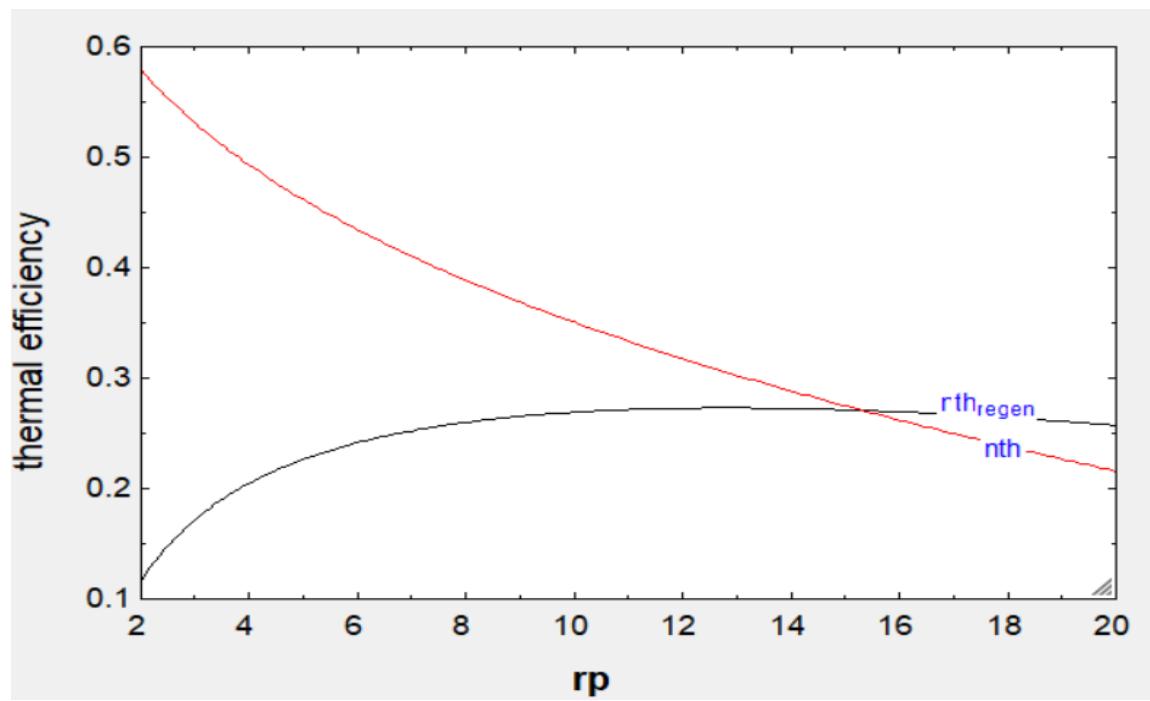
Continue

| Independent Variable | Value | Best value |
|----------------------|-------|------------|
| rp | 12.83 | 12.83 |

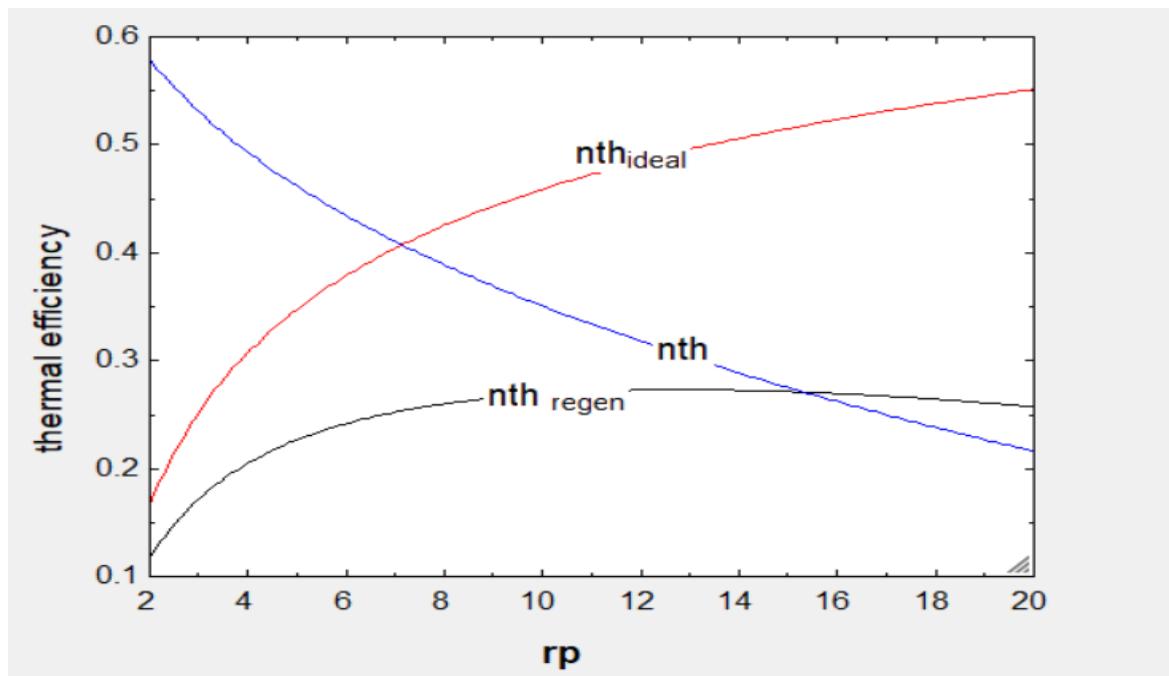
5- plot between pressure ratio and the thermal efficiency



7-Plot relation between the pressure ratio and thermal efficiency:



Maximum pressure ratio is 15.2



Thank you