

A Technical Review and Re-parameterization of Marginal Cyclic Aging Costs

For LFP-Based BESS Energy Management Systems

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November 8, 2025

Abstract

This report presents a technical review of the marginal cyclic aging cost calculation provided for the TechArena BESS EMS development competition. The analysis confirms that the selected methodological framework—a piecewise-linear cost function derived from a power-law degradation model—is a state-of-the-art approach for integration into a Mixed-Integer Linear Program (MILP) [1, 1]. This methodology correctly translates the convex, non-linear nature of battery degradation into a format that is tractable for linear optimization solvers.

However, the analysis identifies a critical discrepancy in the current model’s parameterization that invalidates its claim of being “physically-grounded and traceable”. [1] The model’s parameters, specifically the cycle life $a = 6,000$ and the resulting “Cost per Full Cycle” of EUR 149.07, are based on a fundamental mismatch between the cited source, which studied NMC (Lithium Nickel Manganese Cobalt Oxide) battery chemistry [1], and the LFP (Lithium Iron Phosphate) chemistry specified for the competition. The user’s parameters are not representative of LFP degradation and appear to be based on a misapplication of a commercial performance metric.

Based on a rigorous re-derivation using LFP-specific academic and commercial data [2] and the competition’s explicit economic and technical specifications [1], this report provides a new, fully-justified set of parameters.

The core recommendations are:

1. **Retain the Power-Law Exponent $b = 2$:** The user’s selection of $b = 2$ [1] is affirmed. While not a direct fit to all academic data, it is a behaviorally superior choice for an EMS, as it more strongly penalizes deep discharges, reflecting known physical stress mechanisms.
2. **Adopt a Traceable Cycle Life Parameter $a = 3,840$:** This new baseline (representing cycle life at 100% Depth of Discharge, or DoD) is derived by fitting the $b = 2$ exponent to traceable, LFP-specific commercial data of 6,000 cycles at 80% DoD.[2]
3. **Implement a Corrected “Cost per Full Cycle” of EUR 232.92:** This new cost is derived by amortizing the BESS’s total investment cost (EUR 894,400, from [1]) over the newly established 3,840-cycle lifetime. This cost is 56% higher than the user’s current value, indicating the model is significantly underestimating degradation.
4. **Implement the New Marginal Cost Vector c_j^{cost} :** A new table of marginal costs (EUR/kWh) for each of the 10 SOC segments is provided, based on the corrected parameters.
5. **Prioritize Calendar Aging Model (Model iii):** The current cyclic-only model (“Model (ii)” [1]) is behaviorally incomplete. An EMS optimizing *only* for cyclic cost will erroneously idle at 100% SOC. This behavior is disastrous for LFP batteries due to high calendar aging.[3, 4] The development of the “Model (iii)” [1]—which adds a calendar aging cost C^{cal} to penalize high-SOC-idling—is not an optional extension but an *essential component* for a competitive and physically-realistic EMS.

This report provides the full derivation for these recommendations and the exact cost parameters for implementation.

1 Validation of the Marginal Costing Methodology

The methodological foundation presented in the query [1] is robust, modern, and well-suited for the task of co-optimizing BESS operation in electricity markets. The framework’s individual components are validated as follows:

1.1 Suitability of the Piecewise-Linear Cost Function

The primary challenge in BESS optimization is reconciling non-linear physical phenomena (like degradation) with the linear or mixed-integer linear frameworks required by high-speed market dispatch programs. The approach of modeling battery cycle aging using a piecewise-linear cost function, as pioneered by Xu et al. (2017), is the canonical solution to this problem.[1]

This method, as adopted by the user [1], correctly identifies that the marginal cost of degradation is not constant. By dividing the battery’s state of charge (SOC) into J discrete segments (in this case, 10 segments of 10%), the model can assign a unique marginal cost c_j^{cost} to discharging the energy within that specific segment. Because the cost of deeper discharge is higher (i.e., $c_1 < c_2 < \dots < c_J$), an MILP optimizer will naturally and automatically dispatch the "cheapest" (shallowest) energy segments first. This correctly mimics the convex cost curve of physical degradation without requiring non-linear constraints, making it an ideal choice for the TechArena competition’s MILP framework.

1.2 Appropriateness of the Power-Law Model

The selection of the $\text{CycleLife}(D) = a \cdot D^{-b}$ model is a standard and empirically-supported choice for representing cyclic degradation.[1] This power-law relationship effectively captures the fundamental, non-linear observation seen in most battery chemistries: the total number of achievable cycles increases exponentially as the average depth of discharge (DoD) decreases. For example, a battery may achieve only a few thousand cycles at 100% DoD but can achieve tens of thousands of cycles at 10% or 20% DoD.[1, 2] This model serves as the correct physical basis from which to derive the marginal costs.

1.3 Mathematical Validity of Marginal Weight Derivation

The derivation of the marginal aging weights w_j is mathematically sound. The model correctly assumes that the *cumulative* aging stress from discharging to a depth D is proportional to D^b . Therefore, the *marginal* stress (or cost) of discharging *only* the j -th segment (which spans from DoD D_{j-1} to D_j) is correctly calculated as the difference between the cumulative stress at those two points:

$$w_j \propto (D_j^b) - (D_{j-1}^b)$$

As noted in the user’s model [1], with $J = 10$ segments ($D_j = j/10$) and the selected exponent $b = 2$, the weights are proportional to:

$$w_j \propto (j/10)^2 - ((j-1)/10)^2$$

This simplifies to $w_j \propto (j^2 - (j-1)^2)/100 \propto (2j-1)/100$. The user’s calculation that these weights (0.01, 0.03, 0.05, ...) conveniently sum to 1.0 is arithmetically correct and simplifies the model by making the weights self-normalizing.

In summary, the *framework* of the user’s model is correct. The problem lies not in the *method* but entirely in the *input parameters* used to populate the model, which are shown in the next section to be critically flawed.

2 Critical Analysis of the TechArena Model’s Current Parameterization

A rigorous analysis of the model’s numerical assumptions, when cross-referenced with the provided research and competition specifications, reveals three critical flaws that undermine its physical and economic traceability.

2.1 The Fundamental Citation-Chemistry Mismatch

The model’s technical description [1] cites Xu et al. (2017) [1] as its methodological basis. This is an excellent choice from a modeling perspective. However, there is a fundamental mismatch:

- The TechArena competition specifies an **LFP (Lithium Iron Phosphate)** battery.[1]
- The research in Xu et al. (2017) was conducted on **NMC (Lithium Nickel Manganese Cobalt Oxide)** battery cells.[1]

These two chemistries have vastly different degradation characteristics, cycle lives, and cost structures. The research used to validate the user’s cited source [1] notes that the NMC cell studied could perform only **500 cycles at 100% cycle depth**.

This leads to a critical contradiction: the user has (correctly) adopted the *methodology* from Xu et al. but has (incorrectly) used a set of parameters ($a = 6,000$) that are not from that paper, nor are they representative of the LFP chemistry. This invalidates the model’s claim of being “physically-grounded” and necessitates a new parameter search based exclusively on LFP data.

2.2 Deconstructing the Cycle Life Parameter ($a = 6,000$)

The parameter a represents the BESS’s total cycle life at 100% DoD. The user’s assumption of $a = 6,000$ cycles [1] is an unsubstantiated value that appears to be an outlier when compared to LFP-specific literature.

- **Academic Data (Conservative):** A detailed study on LFP cycle life by Miao et al. (2019), referenced in the research [2], provides a much more conservative figure. This data shows an LFP cycle life of only **600 cycles at 100% DoD**.
- **Commercial Data (Optimistic):** Even optimistic “company claims” for LFP, also cited in the same research [2], place the 100% DoD cycle life at approximately **4,000 cycles**.
- **Likely Source of Error:** The user’s $a = 6,000$ value is likely a misinterpretation of a different, more common performance metric. The *same* commercial data from [2] explicitly lists an LFP cycle life of **6,000 cycles at 80% DoD**. Other sources mention even higher numbers, such as 10,000 cycles at 80% DoD.[5, 6]

It is highly probable that the model’s $a = 6,000$ value was derived by conflating an 80% DoD performance claim with a 100% DoD baseline. This is an invalid assumption, as the a parameter is *defined* as the cycle life at $D = 1$.

2.3 Deconstructing the “Cost per Full Cycle” (EUR 149.07)

The “Cost per Full Cycle” [1] is not an independent constant but a *derived value*. A reverse-engineering of this cost, using the competition’s economic specifications, reveals its direct and flawed linkage to the $a = 6,000$ parameter.

The chain of calculation is as follows:

1. **BESS Investment Cost (CapEx):** The competition specifies a CapEx of **200 EUR/kWh**. [1]

2. **BESS Nominal Energy Capacity (E_{nom}):** The competition specifies $E_{nom} = 4472 \text{ kWh}$. [1]

3. **Total BESS Investment:** Therefore, the total initial investment for the asset is:

$$200 \text{ EUR/kWh} \times 4472 \text{ kWh} = \text{EUR } 894,400$$

4. **Amortized Cost per Cycle:** The "Cost per Full Cycle" is this total investment amortized over the BESS's total lifetime, defined by the 100% DoD cycle life, a .

5. **Validation:** Using the user's assumed $a = 6,000$ [1]:

$$\frac{\text{Total BESS Investment}}{a} = \frac{\text{EUR } 894,400}{6,000 \text{ cycles}} = \text{EUR } 149.07 \text{ per cycle}$$

This calculation is a perfect match for the value presented in the user's model. [1]

This finding is critical for two reasons:

1. It confirms the user's *method* for amortizing the total capital cost is logical and correct.
2. It proves that the EUR 149.07 cost is *not* a fundamental parameter. It is a *direct consequence* of the flawed $a = 6,000$ assumption. Because the $a = 6,000$ input is invalid for LFP, the EUR 149.07 output cost is also invalid.

If the conservative academic value of $a = 600$ [2] were used instead, the cost per cycle would be EUR $894,400 / 600 = \text{EUR } 1,490.70$, an order of magnitude higher. This demonstrates that the current model is underestimating the true cost of degradation by a factor of 10 compared to this conservative academic baseline.

3 Establishing Defensible LFP-Specific Degradation Parameters

The following sections reconstruct the degradation model using traceable, LFP-specific data from the research, providing a set of "best" parameters for the TechArena competition.

3.1 Analysis of the Power-Law Exponent (b)

The user has selected $b = 2$, describing it as a "standard, conservative value" within the typical range of $[1.8, 2.2]$. [1] This assumption can be tested by fitting the power-law model to the academic LFP data from Miao et al. [2]

- **Point 1 (Baseline):** $D_1 = 1.0$ (100% DoD), $\text{CycleLife}_1 = 600$ cycles.
- **Point 2 (Data):** $D_2 = 0.2$ (20% DoD), $\text{CycleLife}_2 = 9000$ cycles.

The power-law model is $\text{CycleLife} = a \cdot D^{-b}$.

1. From Point 1, we find the baseline a : $600 = a \cdot (1.0)^{-b} \implies a = 600$.
2. Using this a , we fit to Point 2 to find b :

$$9000 = 600 \cdot (0.2)^{-b}$$

$$15 = (0.2)^{-b}$$

3. Solving for b using logarithms:

$$\begin{aligned} \log(15) &= -b \cdot \log(0.2) \\ b &= \frac{\log(15)}{-\log(0.2)} \approx \frac{1.176}{0.699} \approx \mathbf{1.68} \end{aligned}$$

This calculation shows that the raw academic data from this specific study [2] suggests a b value closer to 1.7. A higher b (like the user's $b = 2$) results in a *steeper* non-linear cost curve. This means it *more severely* penalizes deep discharges relative to shallow ones.

Recommendation: The user's choice of $b = 2$ **should be retained**. While $b \approx 1.7$ is a closer fit to this *one* dataset, the $b = 2$ value is *behaviorally superior* for an EMS optimization model. It more accurately reflects the advanced electrochemical understanding that the final percentages of DoD (e.g., from 80% to 100%) are disproportionately damaging due to factors like mechanical stress, lithium plating, and phase transitions, which may not be fully captured in a simple two-point fit. The $b = 2$ exponent creates a *stronger* and more physically correct price signal for the optimizer to avoid these highly damaging deep discharges. Thus, the user's "conservative" justification is sound, and the parameter is well-chosen.

3.2 Recommending a Defensible Cycle Life Parameter (a)

With $b = 2$ established as a sound exponent, a new, traceable a parameter (cycle life at 100% DoD) can be derived. The research provides a spectrum of LFP lifetime data, from which a "best" parameter can be selected.

- **Scenario A (Academic/Conservative):** $a = 600$ (at 100% DoD), taken directly from Miao et al. academic data.[2]
- **Scenario B (Commercial/Optimistic):** $a = 4000$ (at 100% DoD), taken from VTC company claims.[2]
- **Scenario C (User's Flawed):** $a = 6000$ (at 100% DoD).[1]

Proposed "Best" Parameter (Scenario D):

The most defensible approach is to *derive* a by applying the chosen exponent ($b = 2$) to a reliable, non-100% DoD data point. The "company claim" of **6,000 cycles at 80% DoD** [2] is the most credible and clearly-defined data point for this purpose, and it directly addresses the likely source of the user's original error.

Derivation:

1. Model: $\text{CycleLife}(D) = a \cdot D^{-b}$
2. Known Parameters: $\text{CycleLife}(0.8) = 6000$; $b = 2$.
3. Solve for a :

$$\begin{aligned} 6000 &= a \cdot (0.8)^{-2} \\ 6000 &= a \cdot \left(\frac{1}{0.64}\right) \\ a &= 6000 \times 0.64 = \mathbf{3,840} \end{aligned}$$

Conclusion: The recommended, "best" parameter for a (cycle life at 100% DoD) is **3,840 cycles**. This value is:

- **Traceable:** It is derived directly from LFP-specific performance data.[2]
- **Consistent:** It uses the chosen $b = 2$ exponent.
- **Reasonable:** It sits logically between the highly conservative academic value (600) and the optimistic commercial value (4000) for 100% DoD.

3.3 An Aggressive Scenario (Scenario E) for Sensitivity Analysis

To provide a complete set of tools for the competition’s ”Investment Optimization” task, an aggressive scenario should also be defined. This scenario is based on other commercial claims mentioned in the research, such as the 10,000 cycles (at 80% DoD, assumed) from DER-VET [5] and another source.[6]

Derivation:

1. Known Parameters: $\text{CycleLife}(0.8) = 10000$; $b = 2$.
2. Solve for a :

$$10000 = a \cdot (0.8)^{-2}$$

$$a = 10000 \times 0.64 = \mathbf{6,400}$$

This $a = 6,400$ is remarkably close to the user’s original $a = 6,000$. This strongly supports the hypothesis that the user’s original value was an 80% DoD claim that was incorrectly applied as a 100% DoD parameter. This aggressive scenario provides a useful upper bound for sensitivity analysis.

4 Derivation of Updated Marginal Cost Parameters for the EMS Model

This section provides the final, implementable numerical values for the user’s EMS model, based on the preceding analysis.

4.1 Recalculating the ”Cost per Full Cycle”

The ”Cost per Full Cycle” is the Total BESS Investment (EUR 894,400) amortized by the a parameter. The cost varies significantly across the defined scenarios.

- **Scenario A (Conservative, $a = 600$):**

$$\text{EUR } 894,400 / 600 \text{ cycles} = \mathbf{\text{EUR } 1,490.70 \text{ per cycle}}$$

- **Scenario D (Recommended, $a = 3840$):**

$$\text{EUR } 894,400 / 3840 \text{ cycles} = \mathbf{\text{EUR } 232.92 \text{ per cycle}}$$

- **Scenario E (Aggressive, $a = 6400$):**

$$\text{EUR } 894,400 / 6400 \text{ cycles} = \mathbf{\text{EUR } 139.75 \text{ per cycle}}$$

- **User’s (Flawed, $a = 6000$):**

$$\text{EUR } 894,400 / 6000 \text{ cycles} = \text{EUR } 149.07 \text{ per cycle (for comparison)}$$

The recommended, traceable cost of EUR 232.92 is 56% higher than the user’s current value. This means the current model significantly undervalues degradation and will therefore over-cycle the battery, leading to a suboptimal solution in the competition’s 10-year ROI analysis.

4.2 Calculating the Final Marginal Cost Vector (c_j^{cost})

The final, per-segment marginal cost c_j^{cost} (in EUR/kWh) is calculated using the user’s correct formula [1]:

$$c_j^{\text{cost}} = \frac{\text{Cost per Full Cycle} \times w_j}{E_{\text{nom}} \times \text{Segment Size}}$$

With parameters:

- Cost per Full Cycle: Varies by scenario (see above).
- Weights (w_j): The user’s correct vector for $b = 2$: [0.01, 0.03, 0.05, 0.07, 0.09, 0.11, 0.13, 0.15, 0.17, 0.19].
- Energy per Segment: $E_{\text{nom}} \times \text{Segment Size} = 4472 \text{ kWh} \times 0.1 = \mathbf{447.2 \text{ kWh}}$.

This calculation leads to the key deliverable of this report, presented in the following table.

4.3 Key Deliverable: Comparative Marginal Cost Table

Table 1 provides the exact, implementable marginal cost vectors (in EUR/kWh) for the EMS model. The "Recommended Cost" column is the primary deliverable, directly answering the query for the "best parameters definition."

Table 1: Marginal Cyclic Aging Costs (c_j^{cost}) under Different Parameter Scenarios

Segment (j)	SOC Range (Discharging)	Weight (w_j) (for $b = 2$)	User’s Flawed Cost ($a = 6000$)	Recommended Cost ($a = 3840$)	Conservative Cost ($a = 1000$)
1	100% → 90%	0.01	0.0033	0.0052	0.0003
2	90% → 80%	0.03	0.0100	0.0156	0.0010
3	80% → 70%	0.05	0.0167	0.0260	0.0017
4	70% → 60%	0.07	0.0233	0.0364	0.0023
5	60% → 50%	0.09	0.0300	0.0469	0.0030
6	50% → 40%	0.11	0.0367	0.0573	0.0037
7	40% → 30%	0.13	0.0433	0.0677	0.0043
8	30% → 20%	0.15	0.0500	0.0781	0.0050
9	20% → 10%	0.17	0.0567	0.0885	0.0057
10	10% → 0%	0.19	0.0633	0.0990	0.0063
Total Cycle Cost		1.00	EUR 149.07	EUR 232.92	EUR 14.91

Analysis: This table clearly shows that the "Recommended Cost" vector provides a much stronger (56% higher) cost signal to the optimizer than the user’s flawed model. This will force the EMS to be more selective about its dispatch, ignoring low-profit arbitrage opportunities that the current model would (incorrectly) deem profitable. The "Conservative Cost" vector, being 10x higher, would likely render the BESS unprofitable in most market conditions, while the "Aggressive Cost" vector is, interestingly, even cheaper than the user’s flawed model.

5 Critical Model Extensions for a High-Fidelity EMS

The new c_j^{cost} vector corrects the "Model (ii)".[1] However, to create a competition-winning EMS, it is critical to understand the limitations of a cyclic-only model and implement the user’s planned "Model (iii)".[1]

5.1 Beyond DoD: Integrating C-Rate and Temperature Stress

The current model simplifies cyclic aging as a function of DoD only: $C^{\text{cyc}} = f(\text{DoD})$. This is an oversimplification. Research confirms that cyclic aging is a multi-variable function that includes, at a minimum, C-rate and temperature: $C^{\text{cyc}} = f(\text{DoD}, C_{\text{rate}}, T)$. [7, 8]

- **C-Rate:** High charge/discharge currents (high C-rates) accelerate degradation.[7] While the competition-specified C-rates (0.25C, 0.33C, 0.50C) [1] are relatively benign for LFP, a high-fidelity model should still penalize the 0.50C rate more than the 0.25C rate.
- **Temperature:** Elevated battery temperatures dramatically accelerate all degradation mechanisms.[7, 9]

A simple model enhancement would be to introduce multipliers to the cost function:

$$C^{\text{cyc}} = \sum_{t \in T} \sum_{j \in J} \left(c_j^{\text{cost}} \cdot k_C(C_{\text{rate}}) \cdot k_T(T) \cdot \frac{p_j^{\text{dis}}(t)}{\eta_{\text{dis}}} \cdot \Delta t \right)$$

Where k_C and k_T are non-linear (or piecewise-linear) penalty functions. While deriving these functions is complex, even a simple implementation would improve the EMS's physical realism.

5.2 The Co-equal Importance of Calendar Aging (Model iii)

The most significant strategic flaw of a cyclic-only model ("Model (ii)") is the behavior it encourages. An optimizer whose *only* degradation cost is C^{cyc} (which is *only* incurred on discharge) will make a critical error: to avoid all costs, it will charge to 100% and **hold at 100% SOC**, waiting indefinitely for the perfect, high-profit discharge opportunity.

This behavior is catastrophic for battery health.

- **The Problem:** Research on LFP calendar aging is unequivocal: high states of charge (SOC) and high temperatures are the *primary drivers* of calendar aging, a separate and parallel degradation mechanism that occurs *even when the battery is not cycling*. [3, 4, 9]
- **The Model:** Calendar aging is typically modeled as a function of time, SOC, and temperature: $\text{CapacityLoss} = f(t, \text{SOC}, T)$. Research [4] notes that for LFP, this is often modeled with a **square-root-of-time** ($t^{0.5}$) dependence, though $t^{0.75}$ is sometimes a better fit.
- **The Solution (SOS2):** The user's plan in [1] to implement calendar aging cost using **Special Ordered Sets of Type 2 (SOS2)** is precisely the correct, state-of-the-art solution. This MILP technique allows the model to approximate the non-linear cost curve $C^{\text{cal}}(\text{SOC})$, which must be defined to have its lowest cost at a low-to-mid "parking" SOC (e.g., 20-50%) and its highest cost at 100% SOC.

5.3 The "Competition-Winning" Combined Objective Function

The full, high-fidelity objective function must be:

$$\max(\text{Profit}) - \alpha \cdot (C^{\text{cyc}} + C^{\text{cal}})$$

The strategic interplay between these two cost components is what produces intelligent, realistic BESS behavior:

- C^{cyc} (**Cyclic Cost**): This is the marginal cost c_j^{cost} from Table 1. It is an *operating* cost that is *only* incurred when discharging. It creates an incentive to **sell energy only when the price is high enough** to justify the cost.

- C^{cal} (**Calendar Cost**): This is a *holding* cost that is incurred *every 15-minute interval* based on the *average SOC** during that interval. It creates an incentive to **not be full**, i.e., to avoid idling at high SOC.

When the optimizer minimizes the sum ($C^{\text{cyc}} + C^{\text{cal}}$), it will naturally balance these two opposing forces. It will avoid idling at 100% SOC (due to high C^{cal}) and will instead "park" the battery at an economically and physically ideal low/mid SOC to await a high-price arbitrage opportunity that is profitable enough to overcome the C^{cyc} of discharging. This emergent, intelligent behavior is impossible to achieve with C^{cyc} alone.

6 Final Recommendations for TechArena EMS Implementation

1. **Immediate Action:** The flawed $a = 6,000$ parameter and the EUR 149.07 cycle cost must be replaced immediately. Implement the **Recommended Parameter Set** ($a = 3840, b = 2$) and the corresponding **"Recommended Cost" vector** (c_j^{cost}) from **Table 1**. This corrects the most significant flaw in the model and provides a 56% stronger, more realistic degradation cost signal.
2. **Strategic Priority:** The user's current "Model (ii)" [1] is behaviorally incomplete and will perform poorly. A robust "Model (iii)" [1] that includes calendar aging is not an optional extra; it is *essential* for a competitive EMS. The user should prioritize developing the SOS2-based calendar aging cost function $C^{\text{cal}}(\text{SOC})$ as their next development sprint.
3. **Parameter Sensitivity:** The "Conservative" and "Aggressive" cost vectors provided in Table 1 should be used to run sensitivity analyses. This will demonstrate how the EMS's optimized bidding strategy and 10-year ROI change based on different lifetime assumptions, which is a key part of the "Investment Optimization" task.
4. **Final Justification:** By adopting this new, traceable parameterization ($a = 3840, b = 2$) derived from LFP-specific data [2] and competition-specific economics [1], the model will be genuinely "physically-grounded and traceable," moving it from a critically flawed state to a competition-ready one.